READ INSTRUCTIONS CAREFULLY BEFORE PROCEEDING

(1) LOCKBOX # 358160

FCC/MELLON NOV 07 2001

FEDERAL COMMUNICATIONS COMMISSION

REMITTANCE ADVICE

Approved by OMB 3060-0589

Page No 1 of 1

SPECIAL USE

FCC USE ONLY

A PAYER INFORMATION

(2) PAYER NAME (if paying by credit card, enter name exactly as it appears on your card): COMSAT CORP. /COMSAT WORLD SYSTEMS

(3) TOTAL AMOUNT PAID (U.S. Dollars and cents): $145.00

(4) STREET ADDRESS LINE NO. 1: 6560 ROCK SPRING DRIVE

(5) STREET ADDRESS LINE NO. 2:

(6) CITY: BETHESDA

(7) STATE: MD

(8) ZIP CODE: 20817

(9) DAYTIME TELEPHONE NUMBER (include area code): 301-214-3459

(10) COUNTRY CODE (if not in U.S.A.)

FCC REGISTRATION NUMBER (FRN) AND TAX IDENTIFICATION NUMBER (TIN) REQUIRED

(11) PAYER (FRN): 0004-1317-91-160

(12) PAYER (TIN): 522256227

IF PAYER NAME AND THE APPLICANT NAME ARE DIFFERENT, COMPLETE SECTION B
IF MORE THAN ONE APPLICANT, USE CONTINUATION SHEETS (FORM 159 C)

(13) APPLICANT NAME

(14) STREET ADDRESS LINE NO. 1

(15) STREET ADDRESS LINE NO. 2

(16) CITY

(17) STATE

(18) ZIP CODE

(19) DAYTIME TELEPHONE NUMBER (include area code)

(20) COUNTRY CODE (if not in U.S.A.)

FCC REGISTRATION NUMBER (FRN) AND TAX IDENTIFICATION NUMBER (TIN) REQUIRED

(21) APPLICANT (FRN)

(22) APPLICANT (TIN)

COMPLETE SECTION C FOR EACH SERVICE, IF MORE BOXES ARE NEEDED, USE CONTINUATION SHEET

(23A) CALL SIGN/OTHER ID: 6000296

(24A) PAYMENT TYPE CODE: CGX

(25A) QUANTITY: 1

(26A) FEE DUE FOR (PTC): $145.00

(27A) TOTAL FEE: $145.00

FCC USE ONLY

(28A) FCC CODE 1

(29A) FCC CODE 2

(23B) CALL SIGN/OTHER ID

(24B) PAYMENT TYPE CODE

(25B) QUANTITY

(26B) FEE DUE FOR (PTC)

(27B) TOTAL FEE

FCC USE ONLY

(28B) FCC CODE 1

(29B) FCC CODE 2

SECTION D CERTIFICATION

(30) CERTIFICATION STATEMENT

I, ROBERT A. MANSBACH, certify under penalty of perjury that the foregoing and supporting information is true and correct to the best of my knowledge, information and belief

SIGNATURE [signature] DATE 11/6/01

SECTION E CREDIT CARD PAYMENT INFORMATION

(31)

MASTERCARD/VISA ACCOUNT NUMBER:

EXPIRATION

☐ MASTERCARD

☐ VISA

I hereby authorize the FCC to charge my VISA or MASTERCARD for the service(s)/authorization herein described.

SIGNATURE ______________________ DATE ______________

COMSAT World Systems

Robert A. Mansbach
Senior Counsel

6560 Rock Drive
Bethesda Maryland Spring 2017
Telephone 301 214 3459
Fax 301 214 7145
Internet robert.mansbach@comsat.com

Received
NOV 2 0 2001
Satellite and Radiocommunication Division
Satellite Engineering Branch

November 6, 2001

E000296 SES-STA-20011107-02089
COMSAT CORPORATION

Ms. Magalie Salas
Secretary
Federal Communications Commission
445 12th Street, S.W.
Washington, D.C. 20554

RE: Request for Special Temporary Authority
Clarksburg, Maryland earth station
Call Sign: E000296

Dear Ms. Salas:

COMSAT Corporation (COMSAT) herein requests a grant of Special Temporary Authority from March 6, 2002 through April 5, 2002, to provide tracking, telemetry and command (TT&C) LEOP (launch and early orbit phase) services by the above-referenced earth station in support of the upcoming launch and in-orbit testing phases of the INTELSAT 903 satellite, currently scheduled for March 6, 2002. In support of its request, COMSAT submits the following information.

COMSAT uses this earth station in conjunction with its other licensed earth stations at Clarksburg, Maryland and Paumalu, Hawaii to support certain satellite launches. COMSAT herein requests a grant of Special Temporary Authority to permit it to provide TT&C LEOP services in support of the INTELSAT 903 launch via the above-referenced earth station.

COMSAT is attaching hereto detailed technical information which demonstrates that the provision of TT&C LEOP services by the above-referenced earth station will be compatible with its electromagnetic environment and will not cause harmful interference into any lawfully operated earth station. In the extremely unlikely event that such interference iscaused, CQMSAT will take all reasonable steps to eliminate the interference.

COMSAT will coordinate the frequency and power usage with all existing satellites in orbit, which use the same frequency bands, and are in the INTELSAT 903's path. **COMSAT** will also provide all other satellite operators in that path with an emergency phone number where the licensee or its operators can be immediately contacted in the event that harmful interference occurs. Again, in the extremely unlikely event that such interference is caused, COMSAT will take all reasonable steps to eliminate the interference.

A request of Special Temporary Authority will enable **COMSAT** to provide TT&C LEOP services that are critical to placing and maintaining the INTELSAT 903 spacecraft in its proper orbit at 34.5°W and will thereby promote the public interest.

COMSAT herein certifies that it is not subject to a denial of federal benefits pursuant to the Anti-Drug Abuse Act.

Respectfully submitted,
COMSAT Corporation

By ______________________
Robert A. Mansbach

cc: R. Repasi, S. Lam, S. Crandall

EXHIBIT A

FREQUENCY COORDINATION AND INTERFERENCE ANALYSIS REPORT

FREQUENCY COORDINATION AND INTERFERENCE ANALYSIS REPORT

PREPARED FOR

COMSAT CORPORATION
CLARKSBURG, MARYLAND

SATELLITE EARTH STATION
(CALL SIGN: E000296)

PREPARED BY
COMSEARCH
19700 JANELIA FARM BOULEVARD
ASHBURN, VIRGINIA 20147
MAY 21, 2001

TABLE OF CONTENTS

1. CONCLUSIONS

2. SUMMARY OF RESULTS

3. SUPPLEMENTAL SHOWING, RE: PART 25.203(C)

4. EARTH STATION COORDINATION DATA

5. CERTIFICATION

1. CONCLUSIONS

AN INTERFERENCE STUDY CONSIDERING ALL EXISTING, PROPOSED AND PRIOR COORDINATED MICROWAVE FACILITIES WITHIN THE COORDINATION CONTOURS OF THE PROPOSED EARTH STATION DEMONSTRATES THAT THIS SITE WILL OPERATE SATISFACTORILY WITH THE COMMON CARRIER MICROWAVE ENVIRONMENT. FURTHER, THERE WILL BE NO RESTRICTIONS OF ITS OPERATION DUE TO INTERFERENCE CONSIDERATIONS.

2. SUMMARY OF RESULTS

A NUMBER OF GREAT CIRCLE INTERFERENCE CASES WERE IDENTIFIED DURING THE INTERFERENCE STUDY OF THE PROPOSED EARTH STATION. EACH OF THE CASES WHICH EXCEEDED THE INTERFERENCE OBJECTIVE ON- A LINE-OF-SIGHT BASIS WAS PROFILED AND THE PROPAGATION LOSSES ESTIMATED USING NBS TN101 (REVISED) TECHNIQUES. THE LOSSES WERE FOUND TO BE SUFFICIENT TO REDUCE THE SIGNAL LEVELS TO ACCEPTABLE MAGNITUDES IN EVERY CASE.

THE FOLLOWING COMPANIES REPORTED POTENTIAL GREAT CIRCLE INTERFERENCE CONFLICTS WHICH DID NOT MEET THE OBJECTIVES ON A LINE-OF-SIGHT BASIS. WHEN OVER-THE-HORIZON LOSSES ARE CONSIDERED ON THE INTERFERING PATHS, SUFFICIENT BLOCKAGE EXISTS TO NEGATE HARMFUL INTERFERENCE FROM OCCURRING WITH THE PROPOSED TRANSMIT AND RECEIVE EARTH STATION.

<u>COMPANY</u>

CELLCO PARTNERSHIP – NEWARK-DALLAS ROUTE

NO OTHER CARRIERS REPORTED POTENTIAL INTERFERENCE CASES.

3. SUPPLEMENTAL SHOWING
RE: PART 25.203(C)

PURSUANT TO PART 25.203(C) OF THE FCC RULES AND REGULATIONS, THE SATELLITE EARTH STATION PROPOSED IN THIS APPLICATION WAS COORDINATED BY COMSEARCH USING COMPUTER TECHNIQUES AND IN ACCORDANCE WITH PART 25 OF THE FCC RULES AND REGULATIONS. .

EXPEDITED COORDINATION DATA FOR THIS EARTH STATION WAS FAXED TO THE BELOW LISTED CARRIERS WITH A LETTER DATED MAY 9, 2001.

360 DEGREE COMM COMPANY OF VIRGINIA
AMERICAN TELEVISION & COMMUNICATIONS
AT&T COMMUNICATIONS
AT&T COMMUNICATIONS OF MARYLAND INC
AT&T COMMUNICATIONS OF PENNSYLVANIA, INC
AT&T COMMUNICATIONS OF VIRGINIA INC
AT&T COMMUNICATIONS OF WEST VIRGINIA
ATLANTIC STATES MICROWAVE TRANS CO
BELL ATLANTIC - MARYLAND
BELL ATLANTIC PENNSYLVANIA INC.
CELLCO PARTNERSHIP - MD-NJ-PA Region
CELLCO PARTNERSHIP - Newark-Dallas Route
CELLCO PARTNERSHIP - RICHMOND, VA
CHARTER COMMUNICATIONS VI, LLC.
CORBAN COMMUNICATIONS INC.
DOBSON CELLULAR OF MD, INC. dba CELL ONE
DynCorp
FIRST TELEVISION CORP.(MID-ATLANTIC)
HANOVER COUNTY
HARDY CELLULAR TELEPHONE COMPANY
INTERMEDIA COMMUNICATIONS, INC.
LOUDOUN COUNTY VIRGINIA
MARYLAND STATE OF
MCI WORLDCOM NETWORK SERVICES INC
NATIONAL CABLE SATELLITE CORPORATION
PECO ENERGY COMPANY
PENNSYLVANIA CELLULAR TELEPHONE CORP.
PENNSYLVANIA TURNPIKE COMMISSION
PETERSBURG CELLULAR PARTNERSHIP

PRINCE WILLIAM COUNTY
RCTC WHOLESALE CORPORATION
SPECIALTY ANTENNA SITE RESOURCES, INC.
UNITED TELEPHONE OF PENNSYLVANIA
USCOC OF CUMBERLAND, INC.
VERESTAR, INC
VERIZON NORTH INC.
VIRGINIA CELLULAR LIMITED PARTNERSHIP
VIRGINIA ELECTRIC & POWER COMPANY
VIRGINIA PCS ALLIANCE, L.C.
WASH/BALT CELLULAR LTD PARTNERSHIP, INC.
WASHINGTON D.C. SMSA L.P.
WEST VIRGINIA EMS TSN,INC.
WILMINGTON CELLULAR TELEPHONE COMPANY
WINSTAR WIRELESS FIBER CORPORATION

4. EARTH STATION COORDINATION DATA

THIS SECTION PRESENTS THE DATA PERTINENT TO FREQUENCY COORDINATION OF THE PROPOSED EARTH STATION WHICH WAS CIRCULATE-D TO ALL COMMON CARRIERS WITHIN ITS COOR-DINATION CONTOURS.

SATELLITE EARTH STATION, FREQUENCY COORDINATION DATA

04/27/2001

Company	**COMSAT CORPORATION**
Earth Station Name, State	**CLARKSBURG, MD**
Call Sign	**E000296**
Latitude (DMS) (NAD83)	**39 13 3.3 N**
Longitude (DMS) (NAD83)	**77 16 13.9 W**
Ground Elevation AMSL (Ft/m)	**456.7 / 139.20**
Antenna Centerline AGL (Ft/m)	**19.0 / 5.80**
Receive Antenna Type: V40903	**VERTEX COMMUNICATION 9 KPC**
4.0 GHz **Gain** (dBi) / **Diameter** (m)	**50.1 / 9.0**
3 dB / **15** dB **Half Beamwidth**	**0.27 / 0.60**
Transmit Antenna Type: V60903	**VERTEX COMMUNICATION 9 KPC**
6.0 GHz **Gain** (dBi) / **Diameter** (m)	**53.5 / 9.0**
3 dB / **15** dB **Half Beamwidth**	**0.20 / 0.40**
Operating Mode	**TRANSMIT AND RECEIVE**
Modulation	**ANALOG**
Emission / Receive Band (MHz)	**800KFXD / 3625.0000 - 4200.0000**
Emission / Transmit Band (MHz)	**800KFXD / 5850.0000 - 6425.0000**
Max. Available RF Power (dBW)/4 kHz	**3.50**
(dBW)/MHz	**27.50**
Max. EIRP (dBW)/4 kHz	**57.00**
(dBW)/MHz	**81.00**
Max permissible Interference Power	
4.0 GHz, **20%** (dBW/1 **MHz)**	**-156.0**
4.0 GHz, **0.0100%** (dBW/1 **MHz)**	**-146.0**
6.0 GHz, **20%** (dBW/4 kHz)	**-154.0**
6.0 GHz, **0.0025%** (dBW/4 kHz)	**-131.0**
Leops Earth Station Operations for New Geostationary Satellite Launches	
Leops Azimuth Range (Min/Max) **Degrees**	**0.0 / 360.0**
Minimum Elevation Angle Degrees	**5.0**
Radio Climate	**A**
Rain Zone	**2**
Max Great Circle Coordination Distance (Mi/Km)	
4.0 GHz	**289.2 / 465.4**
6.0 GHz	**188.6 / 303.6**
Precipitation Scatter Contour Radius (Mi/Km)	
4.0 GHz	**62.1 / 100.0**
6.0 GHz	**62.1 / 100.0**

Table of Earth Station Coordination Values
04/27/2001

Earth Station Name **CLARKSBURG** MD
Owner **COMSAT CORPORATION**
Latitude (DMS) **(NAD83) 39 13 3.3 N**
Longitude (DMS) (NAD83) **77 16 13.9 W**
Ground Elevation (Ft/m) 456.7 / 139.20 AMSL
Antenna Centerline (Ft/m) **19.0** / 5.80 **AGL**
Antenna Model **VERTEX COMMUNICATIONS 9 KPC**
Objectives: Receive **-156.0** (dBW /1 **MHz)**
Transmit **-154.0** (dBW /4 kHz) **TX Power** 3.5 (dBW/4 kHz)

Azimuth (Deg)	**Horizon Elevation Angle** (Deg)	**Antenna Disc. Angle** (Deg)	4.0 GHz **Antenna Gain** (dBi)	4.0 GHz **Coordination Distance (Km)**	6.0 GHz **Antenna Gain** (dBi)	6.0 GHz **Coordination Distance (Km)**
0	**1.48**	**98.13**	4.50	304.7	4.50	129.8
5	**1.37**	93.13	4.50	309.8	4.50	135.1
10	**1.31**	88.13	4.50	312.6	4.50	138.0
15	**1.34**	83.13	4.50	311.2	4.50	136.5
20	**1.60**	78.13	4.50	299.5	4.50	124.4
25	**1.70**	73.13	4.50	295.4	4.50	120.1
30	1.63	68.13	4.50	298.3	4.50	123.1
35	1.81	63.13	4.50	291.1	4.50	115.6
40	1.90	58.13	4.50	287.7	4.50	112.0
45	1.76	53.13	4.50	293.0	4.50	117.6
50	1.75	48.13	4.50	293.4	4.50	118.0
55	1.85	43.14	4.50	289.6	4.50	114.0
60	1.96	38.14	4.50	285.5	4.50	109.7
65	1.95	33.14	4.50	285.8	4.50	110.1
70	1.90	28.14	4.50	287.7	4.50	112.0
75	1.60	23.14	4.50	299.5	4.50	124.4
80	1.22	18.13	4.50	317.1	4.50	142.7
85	1.01	13.13	4.50	328.6	4.50	154.7
90	0.97	8.13	4.50	331.0	4.50	157.2
95	1.09	3.13	4.50	324.1	4.50	149.9
100	1.02	1.87	4.50	328.0	4.50	154.7
105	1.09	6.87	4.50	324.1	4.50	149.9
110	1.26	11.87	4.50	315.1	4.50	140.6
115	1.44	16.87	4.50	306.5	4.50	131.7
120	1.48	21.87	4.50	304.7	4.50	129.8
125	1.27	26.87	4.50	314.6	4.50	140.1
130	1.28	31.87	4.50	314.1	4.50	139.6
135	0.99	36.87	4.50	329.8	4.50	155.9
140	0.74	41.87	4.50	346.5	4.50	173.2
145	0.52	46.87	4.50	365.1	4.50	192.6
150	0.62	51.87	4.50	356.0	4.50	183.2
155	0.68	56.87	4.50	351.1	4.50	178.0
160	0.70	61.87	4.50	349.5	4.50	176.4
165	0.74	66.87	4.50	346.5	4.50	173.2
170	0.62	71.87	4.50	356.0	4.50	183.2
175	0.26	76.87	4.50	396.8	4.50	226.0
180	0.00	81.87	4.50	465.4	4.50	303.6

Table of Earth Station Coordination Values
04/27/2001

Earth Station Name **CLARKSBURG MD**
Owner **COMSAT CORPORATION**
Latitude (DMS) (NAD83) **39 13 3.3 N**
Longitude (DMS) (NAD83) **77 16 13.9 W**
Ground Elevation (Ft/m) 456.7 / **139.20** AMSL
Antenna Centerline (Ft/m) 19.0 / 5.80 **AGL**
Antenna Model **VERTEX COMMUNICATIONS 9 KPC**
Objectives: Receive **-156.0** (dBW /1 MHz)
Transmit **-154.0** (dBW /4 kHz) **TX Power** 3.5 (dBW/4 kHz)

Azimuth (Deg)	**Horizon Elevation Angle** (Deg)	**Antenna Disc. Angle** (Deg)	4.0 GHz **Antenna** Gain (dBi)	4.0 GHz **Coordination Distance** (Km)	6.0 GHz **Antenna Gain** (dBi)	6.0 GHz **Coordination Distance** (Km)
185	0.28	**86.87**	4.50	**393.7**	4.50	222.8
190	0.00	91.87	4.50	465.4	4.50	303.6
195	0.00	96.87	4.50	465.4	4.50	303.6
200	0.51	101.87	4.50	366.0	4.50	193.6
205	1.32	106.87	4.50	312.1	4.50	137.5
210	2.01	111.87	4.50	283.7	4.50	107.8
215	2.68	116.86	4.50	261.9	4.50	100.0
220	3.18	121.85	4.50	247.9	4.50	100.0
225	3.55	126.83	4.50	238.3	4.50	100.0
230	3.57	131.82	4.50	237.9	4.50	100.0
235	3.42	136.82	4.50	241.6	4.50	100.0
240	3.12	141.83	4.50	249.5	4.50	100.0
245	2.76	146.83	4.50	259.6	4.50	100.0
250	2.40	151.84	4.50	270.5	4.50	100.0
255	2.42	156.84	4.50	269.9	4.50	100.0
260	2.76	161.80	4.50	259.6	4.50	100.0
265	3.14	166.72	4.50	249.0	4.50	100.0
270	3.56	171.52	4.50	238.1	4.50	100.0
275	3.95	175.79	4.50	228.7	4.50	100.0
280	4.30	176.32	4.50	220.6	4.50	100.0
285	4.36	172.42	4.50	219.3	4.50	100.0
290	4.32	167.72	4.50	220.2	4.50	100.0
295	3.97	**162.90**	4.50	228.2	4.50	100.0
300	3.90	**157.96**	4.50	229.8	4.50	100.0
305	3.89	**153.00**	4.50	230.1	4.50	100.0
310	3.85	**148.03**	4.50	231.0	4.50	100.0
315	3.79	143.05	4.50	232.5	4.50	100.0
320	3.63	138.07	4.50	236.4	4.50	100.0
325	3.79	133.07	4.50	232.5	4.50	100.0
330	3.81	128.08	4.50	232.0	4.50	100.0
335	3.70	123.09	4.50	234.6	4.50	100.0
340	3.49	118.11	4.50	239.9	4.50	100.0
345	3.11	113.12	4.50	249.8	4.50	100.0
350	2.56	108.13	4.50	265.5	4.50	100.0
355	1.86	103.13	4.50	289.2	4.50	113.6

5. CERTIFICATION

I HEREBY CERTIFY THAT I AM THE TECHNICALLY QUALIFIED PERSON RESPONSIBLE FOR THE PREPARATION OF THE FREQUENCY COORDINATION DATA CONTAINED IN THIS APPLICATION, THAT I AM FAMILIAR WITH PARTS 101 AND 25 OF THE FCC RULES AND REGULATIONS, THAT I HAVE EITHER PREPARED OR REVIEWED THE FREQUENCY COORDINATION DATA SUBMITTED WITH THIS APPLICATION, AND THAT IT IS COMPLETE AND CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF.

BY: ______________________________

JEFFREY E. COWLES
SENIOR FREQUENCY COORDINATOR
COMSEARCH
19700 JANELIA FARM BLVD.
ASHBURN, VIRGINIA 20147

DATED: May 21, 2001

EXHIBIT B

RADIATION HAZARD STUDY

Analysis of-Non-Ionizing Radiation . .
for a 9.0 Meter Earth Station System

This report analyzes the non-ionizing radiation levels for a 9.0 mete earth station system. The analysis and calculations performed in this repo are in compliance with the methods described in the FCC Office of Engineer: and Technology Bulletin, No. 65 first published in 1985 and revised in 1! in Edition 97-01. The radiation safety limits used in the analysis are conformance with the FCC R&O 96-326. Bulletin No. 65 and the I R&O specifies that there are two separate tiers of exposure limits that a dependant on the situation in which the exposure takes place and/or t status of the -individuals who are subject to the exposure. The Maxir Permissible Exposure (MPE) limits for persons in a General Populatic Uncontrolled environment are shown in Table 1. The General Populatic Uncontrolled MPE is a 'function of transmit frequency and is for an exposu period of thirty minutes or less. The MPE limits for persons in Occupational/Controlled environment are shown in Table 2. The Occupatio MPE is a function of transmit frequency and is for an exposure period of minutes or less. The purpose of the analysis described in this report is determine the power flux density levels of the earth station in far-field, near-field, transition region, between the subreflector or f and main reflector surface, at the main reflector surface, and betw the antenna edge and the ground and to compare these levels to specified MPEs.

Table 1. Limits for General Population/Uncontrolled Exposure(MPE)

Frequency Range (MHz)	Power Density (mWatts/cm**2)
30-300	0.2
300-1500	Frequency(MHz)*(0.8/1200)
1500-100,000	1.0

Table 2. Limits for Occupational/Controlled Exposure(MPE)

Frequency Range (MHz)	Power Density (mWatts/cm**2)
30-300	1.0
300-1500	Frequency(MHz)*(4.0/1200)
1500-100,000	5.0

Table 3 contains the parameters that are used to calculate the various pov densities for the earth stations.

Table 3. Formulas. and Parameters Used for Determining Power Flux Densities

Parameter	Abbreviation	Value	Units
Antenna Diameter	D	9.0	meters
Antenna Surface Area	Sa	II * D**2/4	meters**2
Subreflector Diameter	Ds	117.0	c m
Area of Subreflector	As	II * Ds**2/4	cm**2
Frequency	Frequency	6175	MHZ
Wavelength	lambda	300/frequency(MHz)	meters
Transmit Power	P	1282.00	Watts
Antenna Gain	Ges	53.5	dBi
Pi	II	3.1415927	n/a
Antenna Efficiency	n	0.66	n/a

1. <u>Far Field Distance Calculation</u>

The distance to the beginning of the far field can be determined from the following equation:(l)

Distance to the Far Field Region, (Rf) = 0.60 * D**2 / lambda
= 1000.4 meters

The maximum main beam power density in the Far Field can be determined from the following equation: (2)

On-Axis Power Density in the Far Field,(Wf) = Ges * P / 4 * II * Rf**2
= 22.823 Watts/meters**2
= 2.282 mWatts/cm**2

2. <u>Near Field Calculation</u>

Power flux density is considered to be at a maximum value throughout the entire length of the defined Near Field region. The region is contained within a cylindrical volume having the same diameter as the antenna. Past the boundary of the Near Field region the power density from the antenna decreases linearly with respect to increasing distance.

The distance to the end of the Near Field can be determined from the following equation:(3)

Extent of the Near Field,(Rn) = D**2 / (4 * lambda)
= 416.8 meters

The maximum power density in the Near Field can be determined from the following equation: (4)

Near Field Power Density,(Wn) = 16.0 * n * P / II * D**2
= 53.279 Watts/meters**2
= 5.328 mWatts/cm**2

3. Transition Region Calculations

The Transition region is located 'between the Near and Far Field regions. The power density begins to decrease linearly with increasing distance in the Transition region. While the power density decreases inversely with distance in the Transition region, the power density decreases inversely with the square of the distance in the Far Field region. The maximum power density in the Transition region will not exceed that calculated for the Near Field region. The power density calculated in Section 1 is the highest power density the antenna can produce in any of the regions away from the antenna. The power density at a distance Rt can be determined from the following equation:(5)

Transition region- Power Density,(Tt) = Wn * Rn / Rt
= 5.328 mWatts/cm**2

4. Region between Main Reflector and Subreflector

Transmissions from the feed assembly are directed toward the subreflector surface, and are reflected back toward the main reflector. The most common feed assemblies are waveguide flanges, horns or subreflectors. The energy between the subreflector and the reflector surfaces can be calculated by determining the power density at the subreflector surface. This can be determined from the following equation:(6)

Power Density at Feed Flange, (Ws) = 4 * P / As
= 476.965 mWatts/cm**2

5. Main Reflector Region

The power density in the main reflector is determined in the same manner as the power density at the subreflector. The area is now the area of the main reflector aperture and can be determined from the following equation:(7)

Power Density at the Main Reflector Surface,(Wm) = 4 * P / Sa
= 80.607 Watts/meters**2
= 8.061 mWatts/cm**2

6. Region between Main Reflector and Ground

Assuming uniform illumination of the reflector surface, the power density between the antenna and ground can be determined from the following equation:(8)

Power Density between Reflector and Ground,(Wg) = P / Sa
= 20.152 Watts/meter
= 2.015 mWatts/cm**2

Table 4. Summary of Expected Radiation levels 'for Uncontrolled Environment

Region	Calculated Maximum Radiation Power Density Level (mWatts/cm**2)	Hazard Assessment
1. Far Field (Rf) = 1000.4 meters	2.282	Potential Hazard
2. Near Field (Rn) = 416.8 meters	5.328	Potential Hazard
3. Transition Region Rn < Rt < Rf, (Rt)	5.328	Potential Hazard
4. Between Main Reflector and Subreflector	476.965	Potential Hazard
5. Main Reflector	8.061	Potential Hazard
6. Between Main Reflector and Ground	2.015	Potential Hazard

Table 5. Summary of Expected Radiation levels for Controlled Environment

Region	Calculated Maximum Radiation Power Density Level (mWatts/cm**2)	Hazard Assessmen
1. Far Field (Rf) = 1000.4 meters	2.282	Satisfies FCC MP
2. Near Field (Rn) = 416.8 meters	5.328	Potential Hazard
3. Transition Region Rn < Rt < Rf, (Rt)	5.328	Potential Hazard
4. Between Main Reflector and Subreflector	476.965	Potential Hazard
5. Main Reflector	8.061	Potential Hazard
6. Between Main Reflector and Ground	2.015	Satisfies FCC MF

It is the applicant's responsibility to ensure that the public ar operational personnel are not exposed to harmful levels of radiatior

7. Conclusions

Based upon the above analysis, it is concluded that during TT&C operations harmful levels of radiation may exist in those regions noted for the Uncontrolled (Table 4) and Controlled (Table 5) Environments.

The transmissions are operational only short periods of time during emergency or testing situations. Those operational periods include TT&C functions, a transponder failure, or if a Transponder's performance is brought into question.

The earth station is installed at COMSAT Corporation's Clarksburg, Maryland Teleport facility. The complex is surrounded by a fence, which will restrict any public access. The earth station will be marked with the standard radiation hazard warnings, as well as the area in the vicinity of the earth stations to inform those in the general population, who might be working or otherwise present in or near the direct path of the main beam.

COMSAT Corporation will ensure that the main beam of the antenna will be pointed at least one diameter away from any building, or other obstacles in those areas that exceed the MPE levels.

Finally, the earth station's operating personnel will not have access to areas that exceed the MPE levels, while the earth station is in operation. The transmitter will be turned off during periods of maintenance, so that the MPE standard of 5.0 mw/cm**2 will be complied with for those regions in close proximity to the main reflector, which could be occupied by operating personnel.

EXHIBIT C

FAA NOTIFICATION

FM Notification Not Required

.

Per PART 17[17.14(a)] of the FCC rules, FAA notification is not required, as the proposed antenna structure will be located in an area with structures of equal or greater height.

EXHIBIT D

ELECTROMAGNETIC COMPATABILITY STUDY

Interference Analysis Report

An Assessment of the Impact of Radiolocation Systems Operating in 3.1-3.7 GHz Band on Fixed Satellite Services Earth Station Receiver

Prepared for

COMSAT Corporation

TRANSMIT-RECEIVE EARTH STATION (9.0 METER)

FCC CALL SIGN: E000296

Site Name: Clarksburg, MD

Prepared By

COMSEARCH

May 21, 2001

19700 Janelia Fram Blvd.• Ashburn, VA 20147 USA • 703.726.5500

1.0 Introduction

Interference calculations were performed to determine the potential for in-band and out-of-band interference from Radiolocation Systems operating in the 3.1 to 3.7 GHz band[1]. The geographical positions and operating parameters of these systems was derived from NTIA Document TR-99-36 1[2].

2.0 Radiolocation Systems in the 3.1 – 3.7 GHz Band

High powered mobile and fixed radar systems operated by the Federal Government operate in the 3.1 – 3.7 GHz band. These radars are used to search for and track near-surface and high-altitude airborne projectiles, sea surveillance, and airborne objects. The NTIA report referenced above has identified the locations for two types of systems: land-based and shipboard based. Also included in the report are the operating characteristics of these radars. There are two prevalent types of shipboard radars, denoted as type A and Type B, and one type of ground-based radar. An Airborne System radar is also specified. This analysis will concern itself with interference from the ground based and shipboard based radars based upon the relative operating positions and parameters specified in the NTIA report

A summary of the operating parameters for the shipboard and ground based radar systems is shown below:

Table 1 -Technical Characteristics of 3.1-3.7 GHz Radiolocation Systems

Characteristic	Shipboard System A	Shipboard System B	Ground Based System
Modulation	PON	Q7N	PON
Tuning Range (GHz)	3.5-3.7	3.1-3.5	3.1-3.4
Peak transmit Power (MW)	1	4	0.12
Pulse Width (μsec.)	1.0	3.5-51.2	10.75
Pulse Repetition Rate (kHz)	1.125	0.152-6.0	2793.3-5050.51
Duty Cycle (%)	0.001	0.8-2.0	0.041
Transmit 3-dB Bandwidth (MHz)	4,16.6	4	1,10
Antenna Type	Reflector	Phased Array	Phase Scan Array
Antenna Mainbeam Gain (dBi)	32	42	36
Antenna Centerline (m)	46	20	46

[1] This report is being provided as required under Footnote US 245.

[2] National Telecommunications and Information Administration, U.S. DEPARTMENT OF COMMERCE, NTIA Report TR 99-361, *TECHNICAL CHARACTERISTICS OF RADIOLOCATION SYSTEMS OPERATING IN THE 3. I-3.7 GHz BAND AND PROCEDURES FOR ASSESSING EMC WITH FIXED EARTH STATION RECEIVERS*, (December 1999).

3.0 Earth Station System Parameters

The Fixed Satellite Service Earth Station's operational parameters are shown in the Tables2 and 3 below;

TABLE 2 - SATELLITE EARTH STATION PARAMETERS AND COORDINATION DATA

Company	COMSAT CORPORATION
Earth Station Name, State	CLARKSBORG, MD
Call Sign	E000296
Latitude (DMS) (NAD83)	39 13 3.3 N
Longitude (DMS) (NAD83)	77 16 13.9 W
Ground Elevation AMSL (Ft/m)	456.7 / 139.20
Antenna Centerline AGL (Ft/m)	19.0 / 5.80
Receive Antenna Type: V40903	VERTEX COMMUNICATION 9 KPC
4.0 GHz Gain (dBi) / Diameter (m)	50.1 / 9.0
3 dB / 15 dB Half Beamwidth	0.27 / 0.60
Transmit Antenna Type: V60903	VERTEX COMMUNICATION 9 KPC
6.0 GHz Gain (dBi) / Diameter (m)	53.5 / 9.0
3 dB / 15 dB Half Beamwidth	0.20 / 0.40
Operating Mode	TRANSMIT AND RECEIVE
Modulation	ANALOG
Emission / Receive Band (MHz)	800KFXD / 3625.0000 - 4200.0000
Emission / Transmit Band (MHz)	800KFXD / 5850.0000 - 6425.0000
Max. Available RF Power (dBW)/4 kHz)	3.50
(dBW)/MHz)	27.50
Max. EIRP (dBW)/4 kHz)	57.00
(dBW)/MHz)	81.00
Max permissible Interference Power	
4.0 GHz, 20% (dBW/1 MHZ)	-156.0
4.0 GHz, 0.0100% (dBW/1 MHz)	-146.0
6.0 GHz, 20% (dBW/4 kHz)	-154.0
6.0 GHz, 0.0025% (dBW/4 kHz)	-131.0
Low Earth Orbit Satellite	
Azimuth Range (Min/Max) Degrees	0.0 / 360.0
Minimum Elevation Angle Degrees	5.0
Radio Climate	A
Rain Zone	2
Max Great Circle Coordination Distance (Mi/Km)	
4.0 GHz	289.2 / 465.4
6.0 GHz	188.6 / 303.6
Precipitation Scatter Contour Radius (Mi/Km)	
4.0 GHz	62.1 / 100.0
6.0 GHz	62.1 / 100.0

TABLE 3 - TABLE OF EARTH STATION COORDINATION VALUES

Earth Station Name CLARKSBURG MD
Owner COMSAT CORPORATION
Latitude (DMS) (NAD83) 39 13 3.3 N
Longitude (DMS) (NAD83) 77 16 13.9 W
Ground Elevation (Ft/m) 456.7 / 139.20 AMSL
Antenna Centerline (Ft/m) 19.0 / 5.80 AGL
Antenna Model VERTEX COMMUNICATIONS 9 KPC
Objectives: Receive -156.0 (dBW /1 MHz)
Transmit -154.0 (dBW /4 kHz) TX Power 3.5 (dBW/4 kHz)

Azimuth (Deg)	Horizon Elevation Angle (Deg)	Antenna Disc. Angle (Deg)	4.0 GHz Antenna Gain (dBi)	4.0 GHz Coordination Distance (Km)	6.0 GHz Antenna Gain (dBi)	6.0 GHz Coordination Distance (Km)
0	1.48	98.13	4.50	304.7	4.50	129.8
5	1.37	93.13	4.50	309.8	4.50	135.1
10	1.31	88.13	4.50	312.6	4.50	138.0
15	1.34	83.13	4.50	311.2	4.50	136.5
20	1.60	78.13	4.50	299.5	4.50	124.4
25	1.70	73.13	4.50	295.4	4.50	120.1
30	1.63	68.13	4.50	298.3	4.50	123.1
35	1.81	63.13	4.50	291.1	4.50	115.6
40	1.90	58.13	4.50	287.7	4.50	112.0
45	1.76	53.13	4.50	293.0	4.50	117.6
50	1.75	48.13	4.50	293.4	4.50	118.0
55	1.85	43.14	4.50	289.6	4.50	114.0
60	1.96	38.14	4.50	285.5	4.50	109.7
65	1.95	33.14	4.50	285.8	4.50	110.1
70	1.90	28.14	4.50	287.7	4.50	112.0
75	1.60	23.14	4.50	299.5	4.50	124.4
80	1.22	18.13	4.50	317.1	4.50	142.7
85	1.01	13.13	4.50	328.6	4.50	154.7
90	0.97	8.13	4.50	331.0	4.50	157.2
95	1.09	3.13	4.50	324.1	4.50	149.9
100	1.02	1.87	4.50	328.0	4.50	154.7
105	1.09	6.87	4.50	324.1	4.50	149.9
110	1.26	11.87	4.50	315.1	4.50	140.6
115	1.44	16.87	4.50	306.5	4.50	131.7
120	1.48	21.87	4.50	304.7	4.50	129.8
125	1.27	26.87	4.50	314.6	4.50	140.1
130	1.28	31.87	4.50	314.1	4.50	139.6
135	0.99	36.87	4.50	329.8	4.50	155.9
140	0.74	41.87	4.50	346.5	4.50	173.2
145	0.52	46.87	4.50	365.1	4.50	192.6
150	0.62	51.87	4.50	356.0	4.50	183.2
155	0.68	56.87	4.50	351.1	4.50	178.0
160	0.70	61.87	4.50	349.5	4.50	176.4
165	0.74	66.87	4.50	346.5	4.50	173.2
170	0.62	71.87	4.50	356.0	4.50	183.2
175	0.26	76.87	4.50	396.8	4.50	226.0
180	0.00	81.87	4.50	465.4	4.50	303.6

TABLE 3 - TABLE OF EARTH STATION COORDINATION VALUES (continued)

Earth Station Name CLARKSBURG MD
Owner COMSAT CORPORATION
Latitude (DMS) (NAD83) 39 13 3.3 N
Longitude (DMS) (NAD83) 77 16 13.9 W
Ground Elevation (Ft/m) 456.7 / 139.20 AMSL
Antenna Centerline (Ft/m) 19.0 / 5.80 AGL
Antenna Model VERTEX COMMUNICATIONS 9 KPC
Objectives: Receive -156.0 (dBW /1 MHz)
Transmit -154.0 (dBW /4 kHz) TX Power 3.5 (dBW/4 kHz)

Azimuth (Deg)	Horizon Elevation Angle (Deg)	Antenna Disc. Angle (Deg)	4.0 GHz Antenna Gain (dBi)	4.0 GHz Coordination Distance (Km)	6.0 GHz Antenna Gain (dBi)	6.0 GHz Coordination Distance (Km)
185	0.28	86.87	4.50	393.7	4.50	222.8
190	0.00	91.87	4.50	465.4	4.50	303.6
195	0.00	96.87	4.50	465.4	4.50	303.6
200	0.51	101.87	4.50	366.0	4.50	193.6
205	1.32	106.87	4.50	312.1	4.50	137.5
210	2.01	111.87	4.50	283.7	4.50	107.8
215	2.68	116.86	4.50	261.9	4.50	100.0
220	3.18	121.85	4.50	247.9	4.50	100.0
225	3.55	126.83	4.50	238.3	4.50	100.0
230	3.57	131.82	4.50	237.9	4.50	100.0
235	3.42	136.82	4.50	241.6	4.50	100.0
240	3.12	141.83	4.50	249.5	4.50	100.0
245	2.76	146.83	4.50	259.6	4.50	100.0
250	2.40	151.84	4.50	270.5	4.50	100.0
255	2.42	156.84	4.50	269.9	4.50	100.0
260	2.76	161.80	4.50	259.6	4.50	100.0
265	3.14	166.72	4.50	249.0	4.50	100.0
270	3.56	171.52	4.50	238.1	4.50	100.0
275	3.95	175.79	4.50	228.7	4.50	100.0
280	4.30	176.32	4.50	220.6	4.50	100.0
285	4.36	172.42	4.50	219.3	4.50	100.0
290	4.32	167.72	4.50	220.2	4.50	100.0
295	3.97	162.90	4.50	228.2	4.50	100.0
300	3.90	157.96	4.50	229.8	4.50	100.0
305	3.89	153.00	4.50	230.1	4.50	100.0
310	3.85	148.03	4.50	231.0	4.50	100.0
315	3.79	143.05	4.50	232.5	4.50	100.0
320	3.63	138.07	4.50	236.4	4.50	100.0
325	3.79	133.07	4.50	232.5	4.50	100.0
330	3.81	128.08	4.50	232.0	4.50	100.0
335	3.70	123.09	4.50	234.6	4.50	100.0
340	3.49	118.11	4.50	239.9	4.50	100.0
345	3.11	113.12	4.50	249.8	4.50	100.0
350	2.56	108.13	4.50	265.5	4.50	100.0
355	1.86	103.13	4.50	289.2	4.50	113.6

4.0 Interference Calculations

The interference was calculated into the earth station receive system for both in-band and out-of-band interference. The interference power level was calculated using the formula below:

$$P_r = P_t + G_t - FSL - OHLOSS + G_{es} - LL_t - LL_{es}$$

Where:

P_r : Interference power level received at victim earth station, in dBW
P_t: Transmitter power of Radiolocation system, in dBW
G_t: Gain of Radiolocation transmit system, in dBi
FSL: Free Space Loss between radiolocation system and earth station, in dB
OHLOSS: Over-the-Horizon losses between radiolocation system and earth station, in dB
G_{es}: Horizon gain of the earth station toward radiolocation transmitter, in dBi
LL_t: Line losses of the radiolocation system, in dB (assume 2dB per NTIA report)
LL_{es}: Line losses of the earth station system in dB (assume 0 dB unless known)

This interference power level was then compared to in-band and out-of-band interference criteria The in-band criteria was developed using ITU and FCC recommendation?. The out-of-band interference criteria was developed using the following:

The earth station's low -noise amplifier front-end overload criteria of was determined using the following calculations:

$$T = C - G$$

Where:

T = input threshold at which front-end overload occurs, dB W
C = output 1 dB gain compression point of the LNA, typical -20 dBW
G = Gain of the LNA, dB

For the purposes of this report it was assumed that the low-noise amplifier would not provide any out-of-band frequency rejection, thus no Frequency Dependent Rejection values based upon any RF selectivity, such as pre-LNA filtering or inherent LNA filtering, have been assumed. The maximum level of interference is the includes the input saturation threshold value minus a 10 dB output backoff value to consider in operation levels

The maximum interference power receive, P, allowable then becomes:

$$\text{Max } P_r \geq T - IPBO$$

For a 65 dB gain LNA this value is -95 dBW. In the absence of manufacturer LNA/LNB specifications the following typical values have been used:

T= -95 dBW
c = -20 dBW
G = 65 dB

The propagation model to determine the over-the-horizon loss is the NSMA OH-Loss model[4]. When the propagation link is very lengthy, over 250 miles, an estimated OH-loss using a rounded earth modeling value has been used.

---

[3] FCC Rules 47CFR25.25 1 by reference ITU Radio Regulations Appendix S7.
[4] National Spectrum Managers Association has developed an industry accepted version which incorporates NBS Tech Note 101.

5.0 Summary of Results

The summary calculations are shown for all shipboard based and land based systems in Tables 4 through 8 below. Whenever Radar A and B are possibly in use, the interference calculations have assumed the higher powered systems (Radar B). The antenna elevation for the Ground Based systems was assumed to be 46 m even though it was not specified in the NTIA *report.*

Table 4 Shipboard Radar A Land-Based Test and Training Sites

Radar Location	Lat (N)	Lon (w)	Bearing (deg.)	Distance (mi)	Profile (Is path under 250 miles?)	FSL (dB)	Estimated OH-Loss (dB)	Profiled OH-Loss (dB)	Total Path Loss (dB)	Interfering Power Level (dBW/MHz)	In-Band Interference?	Out-of Band Overload?
Pensacola, FL	302128	0871626	225.8	834.6	NO	-166.2	-82.3	N/A	-248.6	-198.6	NO	NO
Pascagoula, MS	302200	0882900	229.5	882.5	NO	-166.7	-83.3	N/A	-250.0	-200.0	NO	NO
St.Inigoes, MD	381000	0762300	146.2	86.9	YES	-146.6	-53.5	-53.5	-200.1	-150.1	YES	NO

Table 6 Shipboard Radar B Land-Based Test and Training Sites

Radar Location	Lat (N)	Lon (w)	Bearing (deg.)	Distance (mi)	Profile (Is path under 250 miles?)	FSL (dB)	Estimated OH-Loss (dB)	Profiled OH-Loss (dB)	Total Path Loss (dB)	Interfering Power Level (dBW/MHz)	In-Band Interference?	Out-of Band Overload?
Moorestown, NJ	395849	0745630	66.3	135.0	YES	-150.4	-67.6	-67.6	-218.0	-152.0	YES	NO
Wallops Island, VA	375600	0752800	131.6	131.9	YES	-150.2	-63.5	-63.5	-213.7	-147.7	YES	NO

Table 6 Shipboard Radars A and B Home Ports

Radar Location	Lat (N)	Lon (w)	Bearing (deg.)	Distance (mi)	Profile (Is path under 250 miles?)	FSL (dB)	Estimated OH-Loss (dB)	Profiled OH-Loss (dB)	Total Path Loss (dB)	Interfering Power Level (dBW/MHz)	In-Band Interference?	Out-of Band Overload?
Bath, ME	435425	0694848	47.6	504.1	NO	-161.9	-73.5	N/A	-235.4	-169.4	NO	NO
Bremerton, WA	473324	1223811	299.7	2355.6	NO	-175.3	-100.3	N/A	-275.6	-209.6	NO	NO
Everett, WA	475858	1221354	300.5	2335.6	NO	-175.2	-100.2	N/A	-275.4	-209.3	NO	NO
Mayport, FL	302334	0812427	202.3	652.2	NO	-164.1	-78.0	N/A	-242.1	-176.1	NO	NO
Norfolk, VA	365200	0762100	162.5	169.7	YES	-152.4	-65.1	-65.1	-217.5	-151.5	YES	NO
Pascagoula, MS	302253	0882933	229.5	882.1	NO	-166.7	-83.3	N/A	-250.0	-184.0	NO	NO
Pearl Harbor, HI	212000	1580000	276.0	4981.4	NO	-181.8	-113.3	N/A	-295.1	-229.1	NO	NO'
Portland, ME	434100	0701800	47.3	475.4	NO	-161.4	-72.5	N/A	-233.9	-167.9	NO	NO
San Dleao CA	324105	1170800	270.3	2279.7	NO	-175.0	-99 a	N/A	-274.7	-208.7	NO	NO

Table 7 Naval At-Sea Operational Areas

Operational Area	Lat (N)	Lon (w)	Bearing (deg.)	Distance (mi)	**Profile (Is path under 250 miles?)**	**FSL (dB)**	**Estimated OH-Loss** (dB)	**Profiled OH-Loss** (dB)	**Total Path Loss** (dB)	**Interfering Power Level** (dBW/MHz)	**In-Band Interference?**	Out-of Band Overload?
AFWTF												
(North Range)	**183000**	0670000	**153.9**	**1556.7**	**NO**	**-171.7**	**-93.1**	**N/A**	**-264.8**	**-198.8**	**NO**	**NO**
	200000	0670000	152.4	1460.8	NO	-171.1	-92.0	N/A	-263.1	-197.1	NO	NO
	221000	0654800	146.9	1358.6	NO	-170.5	-90.8	N/A	-261.3	-195.2	NO	NO
	221000	0652000	145.8	1372.8	NO	-170.6	-91.0	N/A	-261.5	-195.5	NO	NO
	185000	0620000	142.9	1680.8	NO	-172.3	-94.5	N/A	-266.8	-200.8	NO	NO
	185000	0620000	142.9	1680.8	NO	-172.3	-94.5	N/A	-266.8	-200.8	NO	NO
	182500	0643000	148.5	1628.5	NO	-172.1	-93.9	N/A	-266.0	-200.0	NO	NO
	183000	0644500	149.0	1616.1	NO	-172.0	-93.8	N/A	-265.8	-199.8	NO	NO
	183000	0663800	153.1	1565.7	NO	-171.7	-93.2	N/A	-264.9	-198.9	NO	NO
AFWTF												
(South Range)	180500	0675500	156.4	1562.4	NO	-171.7	-93.2	N/A	-264.9	-198.9	NO	NO
	180500	0652700	150.9	1622.9	NO	-172.0	-93.9	N/A	-265.9	-199.9	NO	NO
	181500	0651000	150.1	1620.1	NO	-172.0	-93.8	N/A	-265.8	-199.8	NO	NO
	181500	0641000	148.0	1648.5	NO	-172.2	-94.1	N/A	-266.3	-200.3	NO	NO
	170000	0641000	149.3	1726.5	NO	-172.6	-94.9	N/A	-267.5	-201.5	NO	NO
	165800	0642800	149.9	1720.1	NO	-172.5	-94.9	N/A	-267.4	-201.4	NO	NO
	153300	0660600	154.6	1768.3	NO	-172.8	-95.3	N/A	-268.1	-202.1	NO	NO
	153900	0662300	155.1	1755.1	NO	-172.7	-95.2	N/A	-267.9	-201.9	NO	NO
	163000	0662300	154.4	1700.2	NO	-172.4	-94.7	N/A	-267.1	-201.1	NO	NO
	163000	0675500	157.7	1665.7	NO	-172.3	-94.3	N/A	-266.6	-200.5	NO	NO

Table 7 Naval At-Sea Operational Areas (continued)

Operational Area	Lat (N)	Lon (w)	Bearing (deg.)	Distance (mi)	Profile (Is path under250 miles?)	FSL (dB)	Estimated OH-Loss (dB)	Profiled OH-Loss (dB)	Total Path Loss (dB)	Interfering Power Level (dBW/MHz)	In-Band Interference?	Out-of Band Overload?
AUTEC												
	252000	0780500	183.1	957.8	NO	-167.4	-84.7	N/A	-252.1	-186.1	NO	NO
	252000	0774500	181.8	957.1	NO	-167.4	-84.7	N/A	-252.1	-186.1	NO	NO
	232500	0762000	176.8	1090.0	NO	-168.6	-86.9	N/A	-255.5	-189.5	NO	NO
	232500	0771500	179.9	1088.6	NO	-168.6	-86.9	N/A	-255.5	-189.5	NO	NO
FORACS, **Hawaii**												
	1212530	11581100	276.2	4988.3	NO	-181.8	-113.4	N/A	-295.1	-229.1	NO	NO
	212100	1581500	276.2	4995.2	NO	-181.8	-113.4	N/A	-295.2	-229.2	NO	NO
	211500	1580800	276.0	4992.5	NO	-181.8	-113.4	N/A	-295.2	-229.1	NO	NO
	211500	1580700	276.0	4991.6	NO	-181.8	-113.4	N/A	-295.2	-229.1	NO	NO
Gulf of Mexico **OPAREA**												
	293601	0800130	194.1	681.3	NO	-164.5	-78.8	N/A	-243.3	-177.2	NO	NO
	292521	0864800	221.6	867.7	NO	-166.6	-83.0	N/A	-249.6	-183.5	NO	NO
	284101	0864800	219.7	909.2	NO	-167.0	-83.8	N/A	-250.8	-184.8	NO	NO
	285231	0874400	223.0	931.9	NO	-167.2	-84.2	N/A	-251.4	-185.4	NO	NO
Pacific Missile Range Facility (PMRF)												
	220000	1594500	277.4	5055.7	NO	-181.9	-113.6	N/A	-295.5	-229.5	NO	NO
	220800	1620000	278.5	5180.6	NO	-182.1	-114.0	N/A	-296.1	-230.1	NO	NO
	224500	1614000	279.0	5136.2	NO	-182.0	-113.9	N/A	-295.9	-229.9	NO	NO
	260000	1581500	280.9	4810.2	NO	-181.5	-112.7	N/A	-294.2	-228.2	NO	NO
Pearl **Harbor South** OPAREA												
	190800	1591500	274.4	5144.6	NO	-182.0	-113.9	N/A	-295.9	-229.9	NO	NO
	210000	1580800	275.8	5002.7	NO	-181.8	-113.4	N/A	-295.2	-229.2	NO	NO
	210000	1573600	275.5	4971.8	NO	-181.7	-113.3	N/A	-295.1	-229.0	NO	NO
	191800	1562000	273.3	4968.2	NO	-181.7	-113.3	N/A	-295.0	-229.0	NO	NO

	184900	11574500	273.4	5070.5	NO	-181.9	-113.6	N/A	-295.6	-229.5	NO	NO

Table 7 Naval At-Sea Operational Areas (continued)

Operational Area	Lat (N)	Lon (w)	Bearing (deg.)	Distance (mi)	Profile (is path under250 miles?)	FSL (dB)	Estimated OH-Loss (dB)	Profiled OH-Loss (dB)	Total Path Loss (dB)	Interfering Power Level (dBW/MHz)	In-Band Interference?	Out-of Band Overload?
Southern California (SOCAL)												
	385200	1255200	284.8	2614.4	NO	-176.2	-102.1	N/A	-278.3	-212.3	NO	NO
	390000	1240000	284.4	2511.6	NO	-175.8	-101.4	N/A	-277.3	-211.2	NO	NO
	311500	1163000	267.4	2285.9	NO	-175.0	-99.8	N/A	-274.8	-208.8	NO	NO
	300000	1203000	267.8	2544.4	NO	-175.9	-101.7	N/A	-277.6	-211.6	NO	NO
Virginia Capes OPAREA												
	384500	0750000	104.1	126.4	YES	-149.9	-62.7	-62.7	-212.6	-146.5	YES	NO
	384500	0743000	101.3	152.6	YES	-151.5	-65.3	-65.3	-216.8	-150.8	YES	NO
	374500	0724000	110.6	269.4	NO	-156.4	-62.7	N/A	-219.1	-153.1	YES	NO
	350600	0724000	136.8	381.0	NO	-159.4	-68.7	N/A	-228.1	-162.1	NO.	NO
	320000	0771200	179.5	497.6	NO	-161.8	-73.3	N/A	-235.1	-169.1	NO	NO
	342400	0773000	182.3	332.4	NO	-158.3	-66.3	N/A	-224.6	-158.5	NO	NO
	354000	0752500	156.8	265.2	NO	-156.3	-62.4	N/A	-218.7	-152.7	YES	NO
	370000	0755000	152.4	171.8	YES	-152.5	-64.9	-64.9	-217.4	-151.4	YES	NO

Table 8 Land-Based Radar Test and Training Sites

Radar Location		Lat (N)	Lon (w)	Bearing (deg.)	Distance (mi)	Profile (Is path under250 miles?)	FSL(dB)	Estimated OH-Loss (dB)	Profiled OH-Loss (dB)	Total Path Loss (dB)	Interfering Power Level (dBW/MHz)	In-Band Interference7	Out-of Band Overload?
Fort Lewis	WA	470525	1223510	298.8	2353.9	NO	-175.3	-100.3	NJA	-275.6	-209.6	NO	NO
Yakima Firing	WA	464018	1202135	297.9	2245.0	NO	-174.8	-99.5	N/A	-274.3	-208.3	NO	NO
Fort Carson	CO	383810	1044750	277.1	1483.8	NO	-171.2	-92.3	N/A	-263.5	-197.5	NO	NO
Fort Rliey	KS	385813	0965139	275.2	1053.3	NO	-168.3	-86.3	N/A	-254.6	-188.6	NO	.NO
Fort Shafler	HI	211800	1574900	275.9	4972.2	NO	-181.7	-113.3	NJA	-295.1	-229.0	NO	NO
Hunter AAF	GA	320100	0810800	204.8	542.0	NO	-162.5	-74.8	N/A	-237.3	-171.3	NO	NO

Fort Gillem GA	333600	0841900	227.5	551.6	NO	-162.7	-75.1	N/A	-237.8	-171.7	NO	NO
Fort Benning GA	322130	0845815	224.7	640.9	NO	-164.0	-77.7	N/A	-241.7	-175.7	NO	NO
Fort Stewart GA	315145	0813655	207.0	563.1	NO	-162.8	-75.5	N/A	-238.3	-172.3	NO	NO
Fort Rucker AL	311947	0854255	223.7	723.6	NO	-165.0	-79.8	N/A	-244.8	-178.8	NO	NO'
Yuma Proving AZ	330114	1141855	269.3	2115.9	NO	-174.3	-98.5	N/A	-272.8	-206.8	NO	NO
Fort Hood TX	310830	0974550	250.3	1286.6	NO	-170.0	-89.8	N/A	-259.8	-193.8	NO	NO
Fort Knox KY	375350	0855655	261.7	478.8	NO	-161.4	-72.7	N/A	-234.1	-168.1	NO	NO
Fort Bragg NC	350805	0790035	199.3	297.5	NO	-157.3	-64.4	N/A	-221.7	-155.6	YES	NO
Fort Campbell KY	363950	0872820	255.6	584.4	NO	-163.2	-76.1	N/A	-239.3	-173.2	NO	NO
Fort Polk LA	310343	0931226	242.7	1063.3	NO	-168.4	-86.5	N/A	-254.9	-188.8	NO	NO
Fort Leonard MO	374430	0920737	267.4	811.9	NO	-166.0	-81.8	NJA	-247.8	-181.8	NO	NO
Fort Irwin CA	351536	1164102	274.8	2190.2	NO	-174.6	-99.1	N/A	-273.7	-207.7	NO	NO
Fort Sill OK	344024	0982352	261.3	1210.6	NO	-169.5	-88.8	N/A	-258.2	-192.2	NO	NO
Fort Bliss TX	314850	1062533	261.2	1720.8	NO	-172.5	-94.9	N/A	-267.4	-201.4	NO	NO
Fort Leavenworth KS	392115	0945500	276.2	946.1	NO	-167.3	-84.5	N/A	-251.8	-185.8	NO	NO
Fort Drum NY	440115	0754844	12.4	340.0	NO	-158.4	-66.7	N/A	-225.2	-159.1	NO	NO
Fort Gordon GA	332510	0820910	215.7	483.8	NO	-161.5	-72.8	N/A	-234.3	-168.3	NO	NO
Fort McCoy WI	440636	0904127	300.4	772.3	NO	-165.6	-81.0	N/A	-246.5	-180.5	NO	NO
Fort Dix NJ	400025	0743713	68.1	151.5	YES	-151.4	-71.6	-71.6	-223.0	-157.0	NO	NO
Parks Reserve CA	374254	1214218	281.4	2411.9	NO	-175.5	-100.7	N/A	-276.2	-210.2	NO	NO
Aberdeen Proving MD	392825	0760655	73.7	64.4	YES	-144.0	-62.8	-62.8	-206.8	-140.8	YES.	NO
Fort Huachuca AZ	313500	1102000	263.8	1939.1	NO	-173.6	-96.9	N/A	-270.5	-204.5	NO	NO
Fort Monmouth NJ	401900	0740215	65.2	188.1	YES	-153.3	-76.2	-76.2	-229.5	-163.5	NO	NO
Picatinny Arsenal NJ	405600	0743400	49.6	185.9	YES	-153.2	-167.3	-167.3	-320.5	-254.5	NO	NO

Table 8 Land-Based Radar Test and Training Sites (continued)

Radar Location		Lat (N)	Lon (w)	Bearing (deg.)	Distance (mi)	Profile (Is path under 250 miles?)	FSL (dB)	Estimated OH-Loss (dB)	Profiled OH-Loss (dB)	Total Path Loss (dB)	Interfering Power Level (dBW/MHz)	In-Band Interference?	Out-of Band Overload?
Redstone Arsenal	AL	343630	0863610	241.2	606.7	NO	-163.5	-76.8	N/A	-240.2	-174.2	NO	NO
White Sands	NM	322246	1062813	262.5	1706.5	NO	-172.5	-94.7	N/A	-267.2	-201.2	NO	NO
Army Research	MD	390000	0765800	132.5	22.2	YES	-134.7	-99.7	-99.7	-234.4	-168.4	NO	NO
Fort Hunter	CA	355756	1211404	278.1	2423.1	NO	-175.5	-100.8	N/A	-276.3	-210.3	NO	NO
Kelly Support	PA	402357	0800925	298.9	173.9	YES	-152.6	-206.1	-206.1	-358.7	-292.7	NO	NO

Table Headings

Radar Location : The site name of the radar system
Lat (N) : Radar latitude
Lon (w) : Radar Longitude
Bearing (deg.) : Azimuth from earth station toward radar.
Distance (mi) : Distance from earth station to radar
Profile (Is path under 250 miles?) : If path is over 250 miles no OH-loss profile is generated
FSL (dB) : Free Space Loss
Estimated OH-Loss (dB) : Using a rounded-earth model an estimated OH-loss is calculated for long paths
Profiled OH-Loss (dB) : Using the NSMA Tropo Loss actual OH-loss calculcations are performed for shorter paths
Total Path Loss (dB) : Total of Free Space Loss plus Over-the-Horizon loss
Interfering Power Level (dBW/MHz) : Level of RF interference at the earth station's LNA input
In-Band Interference? : If the Radar is operating in-band is the max. permissible interference criteria being met?
Out-of Band Overload? : If the Radar is operating in out-of-band spectrum is the LNA overload threshold being met?

6.0 Conclusions

Calculations were perform to assess the electromagnetic compatibility (EMC) between the radars listed below and adjacent-band FSS earth station receiver at Clarksburg, Maryland. Interference assessment for Earth Stations Operating at 3625 - 3700 MHz at the Clarksburg, VA site identified 11 cases of In-band potential interference. The applicant is aware of this potential for interference and will work with the Government Users to mitigate the problem.

Results

Total Number of Paths 16 sites		Lat (N)	Lon (W)	Out-of-Band Overload?	In-Band Interference?
St.Inigoes,	MD	381000	0762300	No	Yes
Moorestown,	NJ	395849	0745630	No	Yes
Wallops Island,	VA	375600	0752800	No	Yes
Norfolk,	VA	365200	762100	No	Yes
Virginia Capes OPEREA		384500	0750000	No	Yes
Virginia Capes OPEREA		384500	0743000	No	Yes
Virginia Capes OPEREA		342400	0773000	No	Yes
Virginia Capes OPEREA		354000	752500	No	Yes
Virginia Capes OPEREA		370000	755000	No	Yes
Fort Bragg,	NC	350805	790035	No	Yes
Fort Dii	NJ	400025	0743713	No	No
Aberdeen Proving	MD	392825	0760655	No	Yes
Fort Monmouth	NJ	401900	0740215	No	No
Picatinny Arsenal	NJ	405600	0743400	No	No
Army Research	MD	390000	0765800	No	No
Kelly Support	PA	402357	0800925	No	No

202

LMGT FCC FILING FEES
LOCKHEED MARTIN GLOBAL TELECOMUNICATIONS
6560 ROCK SPRING DRIVE
BETHESDA, MD. 20817

DATE 11/6/01

65-270
550

PAY TO THE ORDER OF FCC $ 145.00

One Hundred, Forty Five DOLLARS

SUNTRUST
SunTrust Bank

FOR

⑈0000 2025⑈ ⑆055002707⑆ 0007165786⑈