## Radiation Hazard Analysis

## SR2000 and SR3000

This analysis predicts the radiation levels around a proposed earth station complex, comprised of a single panel type antenna. This report is developed in accordance with the prediction methods contained in OET Bulletin No. 65, Evaluating Compliance with FCC Guidelines for Human Exposure to Radio Frequency Electromagnetic Fields, Edition 97-01, pp 26-30. The maximum level of non-ionizing radiation to which employees may be exposed is limited to a power density level of 5 milliwatts per square centimeter ( $5 \mathrm{~mW} / \mathrm{cm}^{2}$ ) averaged over any 6 minute period in a controlled environment and the maximum level of non-ionizing radiation to which the general public is exposed is limited to a power density level of 1 milliwatt per square centimeter ( 1 $\mathrm{mW} / \mathrm{cm}^{2}$ ) averaged over any 30 minute period in a uncontrolled environment. Note that the worse-case radiation hazards exist along the beam axis. Under normal circumstances, it is highly unlikely that the antenna axis will be aligned with any occupied area since that would represent a blockage to the desired signals, thus rendering the link unusable.

## Earth Station Technical Parameter Table

| Antenna Aperture Size | $0.59 \mathrm{~m} \times 0.08 \mathrm{~m}$ |
| :--- | :--- |
| Antenna Effective Diameter | 0.245 meters |
| Antenna Surface Area | 0.047 sq . meters |
| Antenna Isotropic Gain | 27.5 dBi |
| Number of Identical Adjacent Antennas 1 |  |
| Nominal Antenna Efficiency ( $\varepsilon$ ) | $42 \%$ |
| Nominal Frequency | 14.25 GHz |
| Nominal Wavelength ( $\lambda$ ) | 0.0211 meters |
| Maximum Transmit Power / Carrier | 40.0 Watts |
| Number of Carriers | 1 |
| Total Transmit Power | 40.0 Watts |
| W/G Loss from Transmitter to Feed | 1.5 dB |
| Total Feed Input Power | 28.32 Watts |
| Radome Losses | 0.5 dB |
| Effective RF Power at radome | 25.24 Watts |
| Near Field Limit | $\mathrm{R}_{\mathrm{nf}}=\mathrm{D}^{2} / 4 \lambda=0.714$ meters |
| Far Field Limit | $\mathrm{R}_{\mathrm{ff}}=0.6 \mathrm{D}^{2} / \lambda=1.71$ meters |
| Transition Region | $\mathrm{R}_{\mathrm{nf}}$ to $\mathrm{R}_{\mathrm{ff}}=0.714$ meters to 1.71 meters |

In the following sections, the power density in the above regions, as well as other critically important areas will be calculated and evaluated. The calculations are done in the order discussed in OET Bulletin 65.

### 1.0 At the Antenna Surface

The power density at the reflector surface can be calculated from the expression:

$$
\begin{equation*}
\mathrm{PD}_{\mathrm{as}}=4 \mathrm{P} / \mathrm{A}=240.29 \mathrm{~mW} / \mathrm{cm}^{2} \tag{1}
\end{equation*}
$$

Where: $\mathrm{P}=$ total power at feed, milliwatts
$A=$ Total area of reflector, sq. cm

In the normal range of transmit powers for satellite antennas, the power densities at or around the reflector surface is expected to exceed safe levels. This area will not be accessible to the general public.

This antenna will incorporate a radome which has 0.5 dB of loss. The worst case power density at the surface of the radome is shown below:

$$
\begin{equation*}
\mathrm{PD}_{\text {radome }}=4 \mathrm{P}_{\mathrm{rad}} / \mathrm{A}=214.16 \mathrm{~mW} / \mathrm{cm}^{2} \tag{2}
\end{equation*}
$$

Where: Prad = total power at feed less radome losses, milliwatts
$A=$ Total area of reflector, sq. cm (this would represent worst case)

Operators and technicians should receive training specifying this area as a high exposure area. Procedures must be established that will assure that all transmitters are rerouted or turned off before access by maintenance personnel to this area is possible.

### 2.0 On-Axis Near Field Region

The geometrical limits of the radiated power in the near field approximate a cylindrical volume with a diameter equal to that of the antenna. In the near field, the power density is neither uniform nor does its value vary uniformly with distance from the antenna. For the purpose of considering radiation hazard it is assumed that the on-axis flux density is at its maximum value throughout the length of this region. The length of this region, i.e., the distance from the antenna to the end of the near field, is computed as Rnf above.

The maximum power density in the near field is given by:

$$
\begin{aligned}
& \mathrm{PD}_{\mathrm{nf}}=(16 \varepsilon \mathrm{P}) /\left(\pi \mathrm{D}^{2}\right)= \mathbf{9 0 . 1 0} \mathrm{mW} / \mathrm{cm}^{2}(3) \\
& \text { from } 0 \text { to } 0.713 \text { meters }
\end{aligned}
$$

Evaluation
Uncontrolled Environment: Does Not Meet Controlled Limits
Controlled Environment: Does Not Meet Uncontrolled Limits

### 3.0 On-Axis Transition Region

The transition region is located between the near and far field regions. As stated in Bulletin 65, the power density begins to vary inversely with distance in the transition region. The maximum power density in the transition region will not exceed that calculated for the near field region, and the transition region begins at that value. The maximum value for a given distance within the transition region may be computed for the point of interest according to:

```
\(\mathrm{PD}_{\text {tr }}=\quad\left(\mathrm{PD}_{\mathrm{nf}}\right)\left(\mathrm{R}_{\mathrm{nf}}\right) / \mathrm{R}=\) dependent on R
where: \(\quad \mathrm{PD}_{\mathrm{nf}}=\) near field power density
    \(\mathrm{R}_{\mathrm{nf}}=\) near field distance
    \(\mathrm{R}=\) distance to point of interest
\(\mathrm{PD}_{\mathrm{tr}}=\mathbf{9 0 . 1 0} \mathrm{mW} / \mathrm{cm}^{2}\)
For: \(\quad 0.713<\mathrm{R}<1.71\) meters
```

We use Eq (4) to determine the safe on-axis distances required for the two occupancy conditions:

## Evaluation

$$
\begin{array}{ll}
\text { Uncontrolled Environment Safe Operating Distance, (meters), } \mathrm{R}_{\text {safeu }}: & 64.2 \\
\text { Controlled Environment Safe Operating Distance, (meters), } \mathrm{R}_{\text {safec }}: & 12.8
\end{array}
$$

### 4.0 On-Axis Far-Field Region

The on- axis power density in the far field region $\left(\mathrm{PD}_{\mathrm{ff}}\right)$ varies inversely with the square of the distance as follows:

$$
\begin{aligned}
& \mathrm{PD}_{\mathrm{ff}}= \mathrm{PG} /\left(4 \pi \mathrm{R}^{2}\right)=\text { dependent on } \mathrm{R}(5) \\
& \text { where: } \mathrm{P}=\text { total power at feed } \\
& \mathrm{G}=\text { Numeric Antenna gain in the direction of interest relative to isotropic radiator } \\
& \mathrm{R}=\text { distance to the point of interest } \\
& \text { For: } \quad \mathrm{R}>\mathrm{R}_{\mathrm{ff}}=1.71 \text { meters } \\
& \mathrm{PD}_{\mathrm{ff}}=\mathbf{3 8 . 6 0} \mathrm{mW} / \mathrm{cm}^{2} \text { at } \mathrm{R}_{\mathrm{ff}}
\end{aligned}
$$

We use Eq (5) to determine the safe on-axis distances required for the two occupancy conditions:
Evaluation

| Uncontrolled Environment Safe Operating Distance,(meters), $\mathrm{R}_{\text {safee }}:$ | See Section 3 |
| :--- | :--- |
| Controlled Environment Safe Operating Distance,(meters), $\mathrm{R}_{\text {safec }}:$ | See Section 3 |

### 5.0 Off-Axis Levels at the Far Field Limit and Beyond

In the far field region, the power is distributed in a pattern of maxima and minima (sidelobes) as a function of the off-axis angle between the antenna center line and the point of interest. Off-axis power density in the far field can be estimated using the antenna radiation patterns prescribed for the antenna in use. Usually this will correspond to the antenna gain pattern envelope defined by the FCC or the ITU, which takes the form of:

$$
\begin{aligned}
& \mathrm{G}_{\text {off }}=32-25 \log (\Theta) \\
& \text { for } \Theta \text { from } 1 \text { to } 48 \text { degrees; }-10 \mathrm{dBi} \text { from } 48 \text { to } 180 \text { degrees } \\
& \text { (Applicable for commonly used satellite transmit antennas) }
\end{aligned}
$$

Considering that satellite antenna beams are aimed skyward, power density in the far field will usually not be a problem except at low look angles. In these cases, the off axis gain reduction may be used to further reduce the power density levels.

For example: At two (2) degrees off axis At the far-field limit, we can calculate the power density as:
$\mathrm{G}_{\text {off }}=32-25 \log (2)=32-7.52 \mathrm{dBi}=280.2$ numeric

$$
\mathrm{PD}_{2 \text { deg off-axis }}=\mathrm{PD}_{\mathrm{ffX}} 280.2 / \mathrm{G}=\mathbf{1 9 . 2 3} \mathrm{mW} / \mathrm{cm}^{2} \mathbf{( 6 )}
$$

### 6.0 Off-Axis power density in the Near Field and Transitional Regions

According to Bulletin 65 , off-axis calculations in the near field may be performed as follows: assuming that the point of interest is at least one antenna diameter removed from the center of the main beam, the power density at that point is at least a factor of $100(20 \mathrm{~dB})$ less than the value calculated for the equivalent on-axis power density in the main beam. Therefore, for regions at least D meters away from the center line of the dish, whether behind, below, or in front under of the antenna's main beam, the power density exposure is at least 20 dB below the main beam level as follows:

$$
\mathrm{PD}_{\mathrm{nf}(\text { (off-axis) }}=\mathrm{PD}_{\mathrm{nf}} / 100=\mathbf{0 . 9 0 1} \mathrm{mW} / \mathrm{cm}^{2} \text { at } \mathrm{D} \text { off axis (7) }
$$

See Section 7 for the calculation of the distance vs. elevation angle required to achieve this rule for a given object height.

### 7.0 Evaluation of Safe Occupancy Area in Front of Antenna

The distance ( S ) from a vertical axis passing through the dish center to a safe off axis location in front of the antenna can be determined based on the dish diameter rule (Item 6.0). Assuming a flat terrain in front of the antenna, the relationship is:
$\mathrm{S}=(\mathrm{D} / \sin \alpha)+(2 \mathrm{~h}-\mathrm{D}-2) /(2 \tan \alpha)(8)$
Where: $\alpha=$ minimum elevation angle of antenna
$\mathrm{D}=$ dish diameter in meters
$\mathrm{h}=$ maximum height of object to be cleared, meters
For distances equal or greater than determined by equation (8), the radiation hazard will be below safe levels for all but the most powerful stations ( $>4$ kilowatts RF at the feed).

For $\quad \alpha=\quad 20$ degrees, minimum elevation angle of antenna
$\mathrm{h}=\quad 2.0$ meters, delta between antenna and object $>1 \mathrm{~m}$
Then:

| $\alpha$ | S |
| :--- | :--- |
| 10 | 0.7 meters |
| 15 | 0.5 meters |
| 20 | 0.4 meters |
| 25 | 0.3 meters |
| 30 | 0.3 meters |

### 8.0 Summary of Results

The earth station site will be protected from uncontrolled access by virtue of the fact that it will be mounted on the roof of a vehicle. There will also be proper emission warning signs placed and all operating personnel will be aware of the human exposure levels at and around the earth station. The applicant agrees to abide by the conditions specified in Condition 18 provided below:
(18) - The Raysat Antenna Systems LLC shall take all reasonable and customary measures to ensure that the MET does not create potential for harmful nonionizing radiation to persons who may be in the vicinty of the MET when it is in operation. At a minimum, permanent warning label(s) shall be affixed to the MET warning of the radiation hazard and including a diagram showing the regions around the MET where the radiation levels could exceed $1.0 \mathrm{~mW} / \mathrm{cm} 2$. The operator of the MET shall be responsible for assuring that individuals do not stray into the region around the MET where there is a potential for exceeding the maximum permissible exposure limits required by Section 1.1310 of the Commission's rules 47 C.F.R § 1.1310. This shall be accomplished by means of signs, caution tape, verbal warnings, placement of the MET so as to minimize access to the hazardous region and/or any other appropriate means

The table below summarizes all of the above calculations.

|  | Abbr. |  | Units |  |
| :---: | :---: | :---: | :---: | :---: |
| Antenna Effective Diameter Antenna Centerline | $\begin{gathered} \text { Df } \\ \text { h } \end{gathered}$ | $\begin{gathered} 0.245 \\ 2 \end{gathered}$ | meters meters |  |
| Antenna Surface Area Antenna Ground Elevation Frequency of Operation Wavelength | $\begin{gathered} \text { Sa } \\ \text { GE } \\ \mathrm{f} \\ \lambda \end{gathered}$ | $\begin{gathered} 0.047 \\ 2 \\ 14.25 \\ 0.0211 \end{gathered}$ | meter $^{2}$ meters GHz <br> meters | $\left(\pi^{*} \mathrm{Df}^{2}\right) / 4$ |
| HPA Output Power | $\mathrm{P}_{\text {HPA }}$ | 40 | watts |  |
| HPA to Antenna Loss | $\mathrm{L}_{\text {TX }}$ | 1.5 | dB |  |
|  | $L_{\text {Rad }}$ | 0.5 | dB |  |
| Transmit Power at Flange | P | 28.32 | watts | $\mathrm{P} / 10 \mathrm{Log}^{-1}\left(\mathrm{~L}_{\mathrm{Tx}} / 10\right)$ |
| Effective Power after Radome Antenna Gain | $\mathrm{G}_{\text {es }}$ | $\begin{gathered} 25.24 \\ 27.5 \end{gathered}$ | watts dBi | P/10Log ${ }^{-1}$ (Radome Loss/10) does not include radome loss |
| Antenna Aperature Efficiency | $\eta$ | 42\% | n/a |  |
| 1. Reflector Surface Region Calculations Antenna Surface Power Density <br> Power at Radome Surface (outside radome) | Pdas Pdrad | $\begin{aligned} & 2402.9 \\ & 240.29 \\ & 2141.6 \\ & 214.16 \end{aligned}$ | $\begin{gathered} \mathrm{W} / \mathrm{m}^{2} \\ \mathrm{~mW} / \mathrm{cm}^{2} \\ \mathrm{~W} / \mathrm{m}^{2} \\ \mathrm{~mW} / \mathrm{cm}^{2} \end{gathered}$ | $\begin{aligned} & (16 * P) /\left(\pi * D^{2}\right) \\ & (16 * P) /\left(\pi * D^{2}\right) \end{aligned}$ <br> Does not meet controlled limits Does not meet uncontrolled limits |
| 2. On Axis Near Field Calculations Extent of Near Field <br> Near Field Power Density | Rn PDnf | $\begin{aligned} & 0.713 \\ & 2.338 \\ & 901.0 \\ & 90.10 \end{aligned}$ | $\begin{gathered} \text { meters } \\ \text { feet } \\ \mathrm{w} / \mathrm{m}^{2} \\ \mathrm{~mW} / \mathrm{cm}^{2} \end{gathered}$ | $\begin{gathered} D^{2} /\left(4^{*} \lambda\right) \\ \left(16^{*} \eta * P\right) /\left(\pi{ }^{*} D^{2}\right) \end{gathered}$ <br> Does not meet controlled limits Does not meet uncontrolled limits |
| 3. On Axis Transition Region Calculations <br> Extent of Transition Region (min) <br> Extent of Transition Region (min) <br> Extent of Transition Region (max) <br> Extent of Transition Region (max) <br> Worst Case Transition Region Power Density <br> Uncontrolled enviorment safe operating distance <br> Controlled enviorment safe operating distance | $\mathrm{R}_{\mathrm{Tr}}$ <br> $\mathrm{R}_{\mathrm{Tr}}$ <br> $\mathrm{PD}_{\text {tr }}$ <br> Rsu <br> Rsc | $\begin{aligned} & 0.713 \\ & 2.338 \\ & 1.711 \\ & 5.612 \\ & 901.0 \\ & 90.10 \\ & \\ & 64.2 \\ & 12.8 \end{aligned}$ | meters feet meters feet $\mathrm{w} / \mathrm{m}^{2}$ $\mathrm{mW} / \mathrm{cm}^{2}$ meters meters | $\begin{aligned} & \mathrm{D}^{2} /\left(4^{*} \lambda\right) \\ & 0.6 * \mathrm{D}^{2} / \lambda \end{aligned}$ <br> Does not meet controlled limits Does not meet uncontrolled limits $\begin{aligned} & \left.\left(\mathrm{PD}_{\mathrm{nf}}\right) / R_{\mathrm{nf}}\right) / \mathrm{Rsu} \\ & \left.\left(\mathrm{PD}_{\mathrm{nf}}\right) / R_{\mathrm{nf}}\right) / R \mathrm{Rc} \end{aligned}$ |
| 4. On Axis Far Field Calculations Distance to Far Field Region <br> On Axis Power Density in the Far Field | Rf $\mathrm{PD}_{\mathrm{ff}}$ | $\begin{gathered} 1.71 \\ 5.61 \\ 386.0 \\ 38.60 \end{gathered}$ | $\begin{gathered} \text { meters } \\ \text { feet } \\ \mathrm{W} / \mathrm{m}^{2} \\ \mathrm{~mW} / \mathrm{cm}^{2} \end{gathered}$ | $\begin{gathered} 0.6 * D^{2} / \lambda \\ \left(G_{\text {es }} * P\right) /\left(4 * \pi * R f^{2}\right) \end{gathered}$ <br> Does not meet controlled limits Does not meet uncontrolled limits |
| 5. Off-axis Power Density in the Far Field Li Antenna Surface Power Density Goa/Ges at a sample angle of $\theta=2$ degrees | PDs | $\begin{aligned} & 192.3 \\ & 0.498 \\ & 19.23 \end{aligned}$ | $\begin{gathered} \mathrm{W} / \mathrm{m}^{2} \\ \mathrm{~mW} / \mathrm{cm}^{2} \end{gathered}$ | $\begin{gathered} \left(\mathrm{G}_{\mathrm{es}}^{*} \mathrm{P}\right) /\left(4^{*} \pi \pi^{*} R f^{2}\right)^{*}(\text { Goa/Ges }) \\ \text { Goa }=32-25^{*} \log (\theta) \end{gathered}$ |
| 6. Off Axis Power Density in the Near Field Power Density of Wn/100 for 1 diameter removed | PDs | $\begin{gathered} \hline \text { Regiol } \\ 9.01 \\ 0.901 \end{gathered}$ | $\begin{gathered} \text { Calculatio } \\ \mathrm{W} / \mathrm{m}^{2} \\ \mathrm{~mW} / \mathrm{cm}^{2} \end{gathered}$ | $\left[(16 * \eta * P) /\left(\pi{ }^{*} D^{2}\right)\right] / 100$ <br> Meets controlled limits Meets Uncontrolled limits |
| 7.0 Off-axis Safe Distances from Earth Stati <br> minimum elevation angle of antenna <br> hieght of object to be cleared <br> Groun elevation delta antenna-obstacle elevation ang | $\alpha$ $h$ GD 10 15 20 25 30 | $\begin{gathered} 10 \\ 2 \\ \mathrm{~S} \\ 0.7 \\ 0.5 \\ 0.4 \\ 0.3 \\ 0.3 \end{gathered}$ | degree meter <br> meter meter meter meter meter | $\mathrm{S}=(\mathrm{D} / \mathrm{sin} \alpha)+(2 \mathrm{~h}-\mathrm{D}-2) /(2 \tan \alpha)$ |

Note: Maximum FCC power density limits for 6 GHz is $1 \mathrm{~mW} / \mathrm{cm} 2$ for general population exposure as per FCC OS\&T

# StealthRay ${ }^{\text {m" }} 2000$ 

## Techspec

## 2-way low-profile in-motion satellite antenna compatible with any external standard Ku band BUC (up to 50W)

| $\therefore$ Physical | Outdoor unit size Outdoor unit weight Indoor unit size Indoor unit weight | $\begin{aligned} & 115 \mathrm{~L} \times 90 \mathrm{~W} \times 15 \mathrm{Hcm}(45 \times 35 \times 6 \mathrm{in}) \\ & 28 \mathrm{~kg}(62 \mathrm{lb}) \\ & 18 \mathrm{~L} \times 23 \mathrm{~W} \times 7 \mathrm{Hcm}(7 \times 9 \times 3 \mathrm{in}) \\ & 1.3 \mathrm{~kg}(2.8 \mathrm{lb}) \\ & \text { (The radome is included in all measurements and dimensions) } \end{aligned}$ |
| :---: | :---: | :---: |
| $\because$ Electrical | Frequency band  <br>  Receive <br>   <br>  Transmit <br> Polarization  <br> Gain Receive <br>  Transmit <br> Antenna G/T  <br> Uplink EIRP  <br> Cross polarization  <br> IF input (Tx)  <br> IF output (Rx)  <br> Ku band input  <br> Power supply  <br> Continuous power consumption  | High band 11.7-12.75 GHz <br> Low band 10.95-11.7 GHz <br> (Factory option) <br> $14.0-14.5 \mathrm{GHz}$ <br> Linear (auto polarization control) <br> 30 dBi <br> 27 dBi <br> $8 \mathrm{~dB} /{ }^{\circ} \mathrm{K}$ at $30^{\circ}$ elevation <br> or $9 \mathrm{~dB} /{ }^{\circ} \mathrm{K}$ at $45^{\circ}$ elevation <br> 41.7 dBW (with external 40 Watt BUC) <br> $>25 \mathrm{~dB}$ <br> 950-1450 MHz <br> 950-2150 MHz <br> 14-14.5 GHz, 50W max. <br> 10-30VDC <br> 55 W (ant. only, excluding BUC) |
| Antenna Performance | Elevation look angle range <br> Azimuth angle range <br> Tracking rate <br> Polarization angle range Initial satellite acquisition \& lock <br> Satellite re-acquisition <br> Azimuth tracking accuracy <br> Elevation tracking accuracy | Automatically adjusted, $25^{\circ}-80^{\circ}$ <br> Automatically adjusted, $360^{\circ}$ continuous <br> $60^{\circ}$ sec <br> Automatically adjusted, $-180^{\circ}$ to $+180^{\circ}$ <br> $<60$ sec, fully automated with integrated GPS <br> $<10 \mathrm{sec}$ (when LoS blocage is $<2$ minutes) <br> $0.5^{\circ} @ 60 \%$ s, $360 \% /^{2}$ <br> $1.0^{\circ} @ 45^{\circ} / \mathrm{s}, 180^{\circ} / \mathrm{s}^{2}$ |
| $\because$ Electrical Interfaces | Tx input <br> Rx output | N (50 2 ) <br> TNC (50 $\Omega$ ) |
| $\because$ Environmental | Temperature range Relative humidity Ground speed | $\begin{aligned} & -25^{\circ} \text { to }+70^{\circ} \mathrm{C}\left(-13^{\circ} \text { to }+158^{\circ} \mathrm{F}\right) \\ & \text { Up to } 95 \% \\ & \text { Up to } 350 \mathrm{Km} / \mathrm{h}(220 \mathrm{mi} / \mathrm{h}) \end{aligned}$ |


#### Abstract

About RAS Established in 2006, Raysat Antenna Systems (RAS) is a world leader in providing low-profile,in-motion, two-way satellite antennas for land mobile applications of COTM (Comms on-the-move). RAS products are used extensively for mobile emergency communications, homeland security, governmental organizations, DSNG, private security, asset tracking, research \& exploration, and general mobile satellite data communications. RAS products operate in both Ku and Ka bands. RAS is a wholly owned subsidiary of Gilat Satellite Networks (NASDAQ: GILT).


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