



beyond frontiers

September 14, 2017

By Electronic Filing

Ms. Marlene H. Dortch  
Secretary  
Federal Communications Commission  
445 12th Street, S.W.  
Washington, DC 20554

Re: SES Americom, Inc., Application for Ku-Band Earth Station Operating in South Mountain, CA,  
File No. SES-LIC-20170726-00806 (Call Sign E170139)

Dear Ms. Dortch,

SES Americom, Inc. ("SES"), pursuant to Section 1.65 of the Commission's rules, 47 C.F.R. § 1.65, hereby updates the record with respect to the above-captioned request for earth station operating authority to provide an updated analysis of the proposed operations in the 13.75-14.0 GHz band. As described in the application, SES seeks authority to communicate with satellites on the Permitted Space Station list authorized to transmit in the 13.75-14.0 GHz band and operating between 52.0° W.L. and 186.0° W.L. The attached updated analysis demonstrates that the proposed operations across the requested arc will not cause harmful interference to either Naval radar or TDRSS stations.

Please address any questions regarding this matter to the undersigned.

Yours Sincerely,

/s/ Petra Vorwig

Petra Vorwig  
Senior Legal & Regulatory Counsel  
SES Americom, Inc.

**Exhibit For  
SES Americom, LLC  
South Mountain (Somis), California  
GD Satcom 9 Meter Earth Station**

**Compliance with FCC Report & Order (FCC96-377) for the 13.75 - 14.0 GHz Band  
Analysis and Calculations**

**1. Background**

This Exhibit is presented to demonstrate the extent to which the SES Americom, LLC satellite earth station in South Mountain (Somis), California is in compliance with FCC REPORT & ORDER 96-377. The potential interference from the earth station to US Navy shipboard radiolocation operations (RADAR) and the NASA space research activities in the 13.75 - 14.0 GHz Band is addressed in this exhibit. The parameters for the earth station are:

**Table 1. Earth Station Characteristics**

- Coordinates (NAD83): 34° 19' 32.3" N, 118° 59' 43.2" W
- Satellite Location for Earth Station: (52° W) and (186° W)
- Frequency Band: 13.75-14.0 GHz for uplink
- Polarizations: H,V
- Emissions: N0N, 100KG7W, 1M00G7W, 36M0G7W, 54M0G7W and 72M0G7W
- Modulation: No Modulation and Digital
- Maximum Aggregate Uplink EIRP: 39.5 dBW for the N0N Carrier  
53.5 dBW for the 100 kHz Carriers  
63.5 dBW for the 1 MHz Carriers  
79.0 dBW for the 36 MHz Carriers  
80.8 dBW for the 54 MHz Carriers  
82.0 dBW for the 72 MHz Carriers
- Transmit Antenna Characteristics
  - Antenna Size: 9.0 meters in Diameter
  - Antenna Type/Model: GD Satcom
  - Gain: 60.1 dBi
- RF power into Antenna Flange: No Modulation (N0N)  
-20.6 dBW  
or -20.6 dBW/4 kHz (Maximum)

- RF power into Antenna Flange (Continued)
  - 100 kHz  
-6.6 dBW  
or -20.6 dBW/4 kHz
  - 1 MHz  
3.4 dBW  
or -20.6 dBW/4 kHz (Maximum)
  - 36 MHz  
18.9 dBW  
or -20.6 dBW/4 kHz (Maximum)
  - 54 MHz  
20.7 dBW  
or -20.6 dBW/4 kHz (Maximum)
  - 72 MHz  
21.9 dBW  
or -20.6 dBW/4 kHz (Maximum)
  
- Minimum Elevation Angle: Somis, CA
  - 10.3° @ 103.5° Az. and 10.3° @ 256.5° Az
  
- Side Lobe Antenna Gain:
  - 32 - 25\*log( $\theta$ )

Because the above uplink spectrum is shared with the Federal Government, coordination in this band requires resolution data pertaining to potential interference between the earth station and both Navy Department and NASA systems. Potential interference from the earth station could impact with the Navy and/or NASA systems in two areas. These areas are noted in FCC Report and Order 96-377 dated September 1996, and consist of (1) Radiolocation and radio navigation, (2) Data Relay Satellites.

Summary of Coordination Issues:

- 1) Potential Impact to Government Radiolocation (Shipboard Radar)
- 2) Potential Impact to NASA Data Relay Satellite Systems (TDRSS)

## 2. Potential Impact to Government Radiolocation (Shipboard Radar)

Radiolocation operations (RADAR) may occur anywhere in the 13.4 – 14.0 GHz frequency band aboard ocean going United States Navy ships. The Federal Communication Commission (FCC) order 96-377 allocates the top 250 MHz of this 600 MHz band to the Fixed Satellite Service (FSS) on a co-primary basis with the radiolocation operations and provides for an interference protection level of  $-167 \text{ dBW/m}^2/4 \text{ kHz}$ .

The closest distance to the shoreline from the South Mountain earth station is approximately 28.77 km Southwest toward the Pacific Ocean. The calculation of the power spectral density at this distance is given by:

|  | <u>N0N</u>            | <u>100 kHz</u> | <u>1.0 MHz</u> | <u>36.0 MHz</u> | <u>54 MHz</u> | <u>72 MHz</u> |
|--|-----------------------|----------------|----------------|-----------------|---------------|---------------|
| 1. Clear Sky EIRP (dBW):               | 39.5                  | 53.5           | 63.5           | 79.0            | 80.8          | 82.0          |
| 2. Carrier Bandwidth:                  | CW                    | 100 kHz        | 1 MHz          | 36 MHz          | 54 MHz        | 72 MHz        |
| 3. PD at antenna Input:<br>(dBW/4 kHz) | -20.6                 | -20.6          | -20.6          | -20.6           | -20.6         | -20.6         |
| 4. Transmit Antenna Gain:              | 60.1 dBi              |                |                |                 |               |               |
| 5. Antenna Gain Horizon:               | FCC Reference Pattern |                |                |                 |               |               |
| 6. Antenna Elevation Angle:            | 10.3°                 |                |                |                 |               |               |

The proposed earth station will radiate interference toward the Pacific Ocean according to its off-axis side-lobe performance. A conservative analysis, using FCC standard reference pattern, results in off-axis antenna gains of 2.6 dBi toward the Pacific Ocean.

The signal density at the shoreline, through free space is:

N0N Carriers (CW Carrier)

PFD = Antenna Feed Power density (dBW/4 kHz) + Antenna Off-Axis Gain (dBi) – Spread Loss ( $\text{dBw-m}^2$ ).

$$\begin{aligned}
 &= -20.6 \text{ dBw/4 kHz} + (2.6) \text{ dBi} - 10 \cdot \log[4\pi \cdot (28770\text{m})^2] \\
 &= -118.1 \text{ dBW/m}^2/4 \text{ kHz} + \text{Additional Path Losses } (\sim 90.7 \text{ dB}) \\
 &= -208.8 \text{ dBW/m}^2/4 \text{ kHz}
 \end{aligned}$$

100 kHz Carriers

PFD = Antenna Feed Power density (dBW/4 kHz) + Antenna Off-Axis Gain (dBi) – Spread Loss ( $\text{dBw-m}^2$ ).

$$\begin{aligned}
 &= -20.6 \text{ dBw/4 kHz} + (2.6) \text{ dBi} - 10 \cdot \log[4\pi \cdot (28770\text{m})^2] \\
 &= -118.1 \text{ dBW/m}^2/4 \text{ kHz} + \text{Additional Path Losses } (\sim 90.7 \text{ dB}) \\
 &= -208.8 \text{ dBW/m}^2/4 \text{ kHz}
 \end{aligned}$$

### 1 MHz Carriers

PFD = Antenna Feed Power density (dBW/4 kHz) + Antenna Off-Axis Gain (dBi) – Spread Loss (dBw-m<sup>2</sup>).

$$\begin{aligned} &= -20.6 \text{ dBw/4 kHz} + (2.6) \text{ dBi} - 10*\log[4\Pi*(28770\text{m})^2] \\ &= -118.1 \text{ dBW/m}^2/4 \text{ kHz} + \text{Additional Path Losses } (\sim 90.7 \text{ dB}) \\ &= -208.8 \text{ dBW/m}^2/4 \text{ kHz} \end{aligned}$$

### 36 MHz Carriers

PFD = Antenna Feed Power density (dBW/4 kHz) + Antenna Off-Axis Gain (dBi) – Spread Loss (dBw-m<sup>2</sup>).

$$\begin{aligned} &= -20.6 \text{ dBw/4 kHz} + (2.6) \text{ dBi} - 10*\log[4\Pi*(28770\text{m})^2] \\ &= -118.1 \text{ dBW/m}^2/4 \text{ kHz} + \text{Additional Path Losses } (\sim 90.7 \text{ dB}) \\ &= -208.8 \text{ dBW/m}^2/4 \text{ kHz} \end{aligned}$$

### 54 MHz Carriers

PFD = Antenna Feed Power density (dBW/4 kHz) + Antenna Off-Axis Gain (dBi) – Spread Loss (dBw-m<sup>2</sup>).

$$\begin{aligned} &= -20.6 \text{ dBw/4 kHz} + (2.6) \text{ dBi} - 10*\log[4\Pi*(28770\text{m})^2] \\ &= -118.1 \text{ dBW/m}^2/4 \text{ kHz} + \text{Additional Path Losses } (\sim 90.7 \text{ dB}) \\ &= -208.8 \text{ dBW/m}^2/4 \text{ kHz} \end{aligned}$$

### 72 MHz Carriers

PFD = Antenna Feed Power density (dBW/4 kHz) + Antenna Off-Axis Gain (dBi) – Spread Loss (dBw-m<sup>2</sup>).

$$\begin{aligned} &= -20.6 \text{ dBw/4 kHz} + (2.6) \text{ dBi} - 10*\log[4\Pi*(28770\text{m})^2] \\ &= -118.1 \text{ dBW/m}^2/4 \text{ kHz} + \text{Additional Path Losses } (\sim 90.7 \text{ dB}) \\ &= -208.8 \text{ dBW/m}^2/4 \text{ kHz} \end{aligned}$$

Our calculations identified additional path losses of approximately 90.7 dB including absorption loss and earth diffraction loss for the actual path profiles from the earth station to the nearest shoreline.

The worst case calculated PFD including additional path losses to the closest shoreline location is -208.8 dBW/m<sup>2</sup>/4 kHz for the CW Carriers, 100 kHz, 1 MHz, 36 MHz, 54 MHz and 72 MHz carriers. This is 41.8 dB above the -167 dBW/ m<sup>2</sup>/4 kHz interference criteria of R&O 96-377. Therefore, there should be no interference to the US Navy RADAR from the South Mountain earth station due to the distance and the terrain blockage between the site and the shore.

### **3. Potential Impact to NASA's Data Relay Satellite System (TDRSS)**

The geographic location of the SES Americom earth station in South Mountain (Somis), California is outside the 390 km radius coordination contour surrounding NASA's White Sands, New Mexico ground station complex. Therefore, the TDRSS space-to-earth link will not be impacted by the SES Americom earth station in South Mountain, California.

The TDRSS space-to-space link in the 13.772 to 13.778 GHz band is assumed to be protected if an earth station produces an EIRP less than 71 dBW/6 MHz in this band. The 9 meter earth station antenna will have an EIRP less than 71 dBW/6 MHz for both the CW carrier, 100 kHz, 1 MHz and 72 MHz carriers in this band. The total EIRP for the CW Carrier is 39.5 dBW and the equivalent EIRP per 6 MHz segment will remain at 39.5 dBW/6 MHz. The total EIRP for the 100 kHz, carriers is 53.5 dBW. The equivalent EIRP per 6 MHz segment will remain at 53.5 dBW/6 MHz. The total EIRP for the 1 MHz, carriers is 63.5 dBW. The equivalent EIRP per 6 MHz segment will remain at 63.5 dBW/6 MHz. The total EIRP for the 72 MHz, carriers is 82.0 dBW. The equivalent EIRP per 6 MHz segment will be 70.0 dBW/6 MHz. Therefore, there should not be interference to the TDRSS space-to-space link for the CW carriers or the 100 kHz, 1 MHz and 72 MHz carriers.

For the 36 MHz and 54 MHz the total EIRP of 79.0 dBW (36 MHz) and 80.8 dBW (54 MHz) equate to an EIRP per 6 MHz of 73.0 dBW/6 MHz and 71.8 dBW/6 MHz respectively. To avoid interference to the TDRSS space-to-space link the 36 MHz and 54 MHz carriers will not be used for the transmit spectrum of 13.772 to 13.778 GHz by this earth station.

### **4. Coordination Issue Result Summary and Conclusions**

The results of the analysis and calculations performed in this exhibit indicate that compatible operation between the earth station at the South Mountain (Somis) facility and the US Navy and NASA systems space-to-earth link are possible for all of the proposed carriers. Operations in NASA systems space-to-space link (13772.0 to 13778.0 MHz) will also be permitted for all of the carriers with the exception of the 36 MHz and 54 MHz emissions.