Analysis of Non-Ionizing Radiation for a 1.2M Skyware Type 123

This report presents an analysis of the non-ionizing radiation levels for a 1.2M Skyware Type 123 system. The calculations used in this analysis were derived from and comply with the procedures outlined in the Federal Communication Commission, Office of Engineering and Technology Bulletin Number 65, which establishes guidelines for human exposure to Radio Frequency Electromagnetic Fields. Bulletin 65 defines exposure levels in two separate categories, the General Population/Uncontrolled Areas limits, and the Occupational/Controlled Area limits. The Maximum Permissible Exposure (MPE) limit of the General Population/Uncontrolled Area is defined in Table (1), and represents a maximum exposure limit averaged over a 30 minute period. The MPE limit of the Occupational/Controlled Area is defined in Table (2), and represents a maximum exposure limit averaged over a 6 minute period. The purpose of this report is to provide an analysis of the earth station power flux densities, and to compare those levels to the specified MPE's. This report provides predicted density levels in the near field, far field, transition region, main reflector surface area, area between the main reflector and sub reflector or feed assembly, as well as the area between the antenna edge and ground.

MPE Limits for General Population/Uncontrolled Area

| Frequency Range (MHz) | Power Density (mW/cm²) | |
|-----------------------|------------------------|--|
| 1500 — 100,000 | 1.0 | |

Table 1

MPE Limits for Occupational/Controlled Area

| Frequency Range (MHz) | Power Density (mW/cm²) | |
|-----------------------|------------------------|--|
| 1500 — 100,000 | 5.0 | |

Table 2

1.2M Skyware Type 123

Table 3 contains formulas, equations and parameters that were used in determining the Power Flux Density levels for the 1.2M Skyware Type123:

| Data Type | Data Symbol | Data Formula | Data Value | Unit of Measure |
|---|--------------------|--|-------------|--------------------|
| Power Input | Р | Input | 4 | W |
| Antenna Size | D | Input | 1.2 | М |
| Antenna Area | А | $A = (\Pi D^2) \div 4$ | 1.131 | M^2 |
| Subreflector Size | Sub | Input | 10.8 | cm |
| Subreflector Area | A _{sub} | $A_{sub} = (\Pi Sub^2) \div 4$ | 91.61 | cm ² |
| Gain dBi | G_{dbi} | Input | 43.3 | dBi |
| Gain Factor | G | $G = 10^{Gdbi/10}$ | 21379.62 | Gain Factor |
| Frequency | f | Input | 14,300 | MHz |
| Wavelength | λ | 299.79 / f | 0.020965 | Meters |
| Aperture Efficiency | η | $\eta = [(G\lambda^{2}) \div (4\Pi)] \div A$ | .66 | n/a |
| Pi | П | Input | 3.14159 | Numeric |
| Constant | M/Sec | Input | 299,792,458 | Numeric |
| Conversion W to mW | mW | $mW = W \times 1000$ | n/a | n/a |
| Conversion M to cm | cm | $cm = M \times 100$ | n/a | n/a |
| Conversion M ² to cm ² | cm ² | $cm^2 = M^2 \times 10000$ | n/a | n/a |
| Conversion W/M ² to mW/cm ² | mW/cm ² | $mW/cm^2 = W/M^2 \div 10$ | n/a | n/a |

Table 3

1. Far Field Analysis

The distance to the far field can be calculated using the following formula:

$$R_{ff} = \frac{0.6D^2}{\lambda} = 41.21 \text{ Meters}$$

The power density in the far field can be calculated using the following formula. Note: this formula requires the use of power in milliwatts and far field distance in centimeters, or requires a post calculation conversion from W/M²:

$$S_{ff} = \frac{PG}{4\Pi R_{ff}^{2}} = 0.401 \text{ mW/cm}^{2}$$

2. Near Field Analysis

The extent of the Near Field region can be calculated using the following formula:

$$R_{nf} = \frac{D^2}{4\lambda} = 17.17 \text{ Meters}$$

The power density of the near field can be calculated using the following formula. Note: this formula requires the use of power in milliwatts and diameter in centimeters, or requires a post calculation conversion from W/M²:

$$S_{nf} = \frac{16\eta P}{\Pi D^2} = 0.935 \text{ mW/cm}^2$$

3. Transition Region Analysis

The transition region extends from the end of the near field out to the beginning of the far field. The power density in the transition region decreases inversely with distance from the antenna, while power density in the far-field decreases inversely with the square of the distance. However the power density in the transition region will not exceed the density in the near field, and can be calculated for any point in the transition region (R), using the following formula. Note: This formula requires the use of distance in centimeters, or requires a post calculation conversion from W/M².

$$S_t = \frac{S_{nf} R_{nf}}{R} = 0.935 \text{ mW/cm}^2$$

4. Main Reflector Surface Area Analysis

The maximum power density at the antenna surface area can be calculated using the following formula. Note: this formula requires the use of Power in milliwatts and Area in centimeters squared, or requires a post calculation conversion from W/M².

$$S_{surface} = \frac{4P}{A} = 1.415 \text{ mW/cm}^2$$

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5. Subreflector Area Analysis

The area between the sub reflector and main reflector presents a potential hazard, with the highest density being located at the sub reflector area. The power density at the sub reflector can be calculated using the following formula. Note: this formula requires the use of Power in milliwatts and Area in centimeters squared, or requires a post calculation conversion from W/M².

$$Sub_{surface} = \frac{4P}{A_{sub}} = 174.656 \text{ mW/cm}^2$$

6. Power Density between Reflector and Ground Analysis

The power density between the reflector and the ground can be calculated using the following formula. Note: this formula requires the use of Power in milliwatts and Area in centimeters squared, or requires a post calculation conversion from W/M².

$$S_{ground} = \frac{P}{A} = 0.354 \text{ mW/cm}^2$$

Tables 4 and 5 present a summary of the radiation hazard findings on the 1.2M Skyware Type 1223 123 terminal for both the General Population/Uncontrolled Area, as well as the Occupational/Controlled area environments.

MPE Limits for General Population/Uncontrolled Area

| Area | Range Meters | Power Density (mW/cm²) | Finding |
|------------------------|---------------|----------------------------|------------------|
| Far Field | 41.21 | 0.401 mW/cm ² | Meets FCC |
| | | | Requirements |
| Near Field | 17.17 | 0.935 mW/cm ² | Meets FCC |
| | | | Requirements |
| Transition Region | 17.17 – 41.21 | 0.935 mW/cm ² | Meets FCC |
| | | | Requirements |
| Main Reflector Surface | N/A | 1.415 mW/cm ² | Potential Hazard |
| Sub-reflector Surface | N/A | 174.656 mW/cm ² | Potential Hazard |
| Area between Reflector | N/A | 0.354 mW/cm ² | Meets FCC |
| and Ground | | | Requirements |

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| Near Field | 17.17 | 0.935 mW/cm ² | Meets FCC |
| | | | Requirements |
| Transition Region | 17.17 – 41.21 | 0.935 mW/cm ² | Meets FCC |
| | | | Requirements |
| Main Reflector Surface | N/A | 1.415 mW/cm ² | Potential Hazard |
| Sub-reflector Surface | N/A | 174.656 mW/cm ² | Potential Hazard |
| Area between Reflector | N/A | 0.354 mW/cm ² | Meets FCC |
| and Ground | | | Requirements |

Table 5

Based on the above finding there is a potential hazard of radio frequency exposure with use of the 1.2M Skyware Type 1223 123. In order to mitigate the risk of these hazards, this terminal will only be operated in a controlled area. Additionally, the unit will be shut down prior to performing maintenance in any of the occupational hazard areas.