## EXHIBIT 2

## Exhibit 2 - Technical Exhibit <br> V3 VMES Terminal

## 1. Introduction

KVH Industries, Inc. ("KVH") has developed a small aperture, broadband, highly efficient and affordable terminal that can be used in the vehicle-mounted earth station ("VMES") context with its global mobile communications network. This VMES - the KVH TracPhone V3 Land terminal (the "V3") - operates in Ku-band FSS frequencies (14.0-14.5 GHz transmit, $11.7-12.2 \mathrm{GHz}$ receive, $10.95-11.2 \mathrm{GHz}$ and $11.45-11.7 \mathrm{GHz}$ receive). The V3 terminal will automatically search for and acquire the designated satellite, and maintain precise pointing via automatic control of the azimuth, elevation and polarization angles.

The antenna being used in this VMES terminal is $14.5^{\prime \prime}(37 \mathrm{~cm})$ in diameter, and its main lobe does not conform to the standards specified in Section §25.209(a) and (b). In order to compensate for this performance, KVH will operate with a spread spectrum modulation technique that will bring the off-axis EIRP spectral density of the terminal well within the spectral density limits specified in Section §25.226 of the Commission’s rules. This technical exhibit provides the showing required pursuant to Section §25.226, including detailed information regarding the VMES antenna patterns and off-axis emissions, and a summary of the remote VMES to hub link analysis.

## 2. Description of Antenna

KVH has developed the small aperture, broadband, highly efficient and affordable V3 VMES terminal for use with its global VMES network. The VMES terminal operates in the Ku FSS frequency band, 14.0-14.5 GHz transmit and 10.95-11.2 GHz, 11.45-11.7 GHz and $11.7-12.2 \mathrm{GHz}$ receive. The antenna is a 37 cm parabolic reflector with a rearfed sub-reflector feed assembly design. The VMES terminal will automatically search for and acquire the designated satellite and maintain precise pointing via automatic control of the azimuth, elevation and polarization angles. The RF equipment is integrated into the base of the terminal and includes a 3 watt block upconverter.

The proposed VMES uplink return transmission (inbound) channel supports data rates of $32 \mathrm{kbit} / \mathrm{s}, 64 \mathrm{kbit} / \mathrm{s}, 128 \mathrm{kbit} / \mathrm{s}, 256 \mathrm{kbit} / \mathrm{s}$, and $512 \mathrm{kbit} / \mathrm{s}$. The VMES uplink transmission utilizes a spread spectrum modulation. This authorization will require channel bandwidths of 18 MHz and 36 MHz . The forward channel (outbound from the hub earth station to the VMES) will be between 3-10 Mbits/s aggregate with individual end user rates at $0.5-2 \mathrm{Mbit} / \mathrm{s}$. The forward channel is also spread over the 18 MHz or 36 MHz channel and is overlaid onto the same transponder spectrum using a technique called PCMA. ${ }^{1}$

[^0]

Figure 1 - KVH 37 cm Ku-band antenna

## 3. Description of Service

As is shown in Figure 2 below, the V3 terminal will be operated within KVH's existing broadband mobile services network authorized for maritime service. ${ }^{2}$ Indeed, the V3 terminal was recently licensed by the Commission as a Ku-band earth station onboard vessel ("ESV"). ${ }^{3}$ KVH is seeking authorization to operate within the continental United States (CONUS), Alaska and Hawaii, as well as U.S. territories and possessions.

KVH would like to operate the terminals with ALSAT (including specifically AMC-15 @ $105^{\circ}$ W.L., AMC-21 @ $125^{\circ}$ W.L. and GE-23 @ $172^{\circ}$ E.L.), as well as in extended Ku-band downlink frequencies with GE-23. The VMESs will communicate using existing hub earth stations in Miami, Florida, Carlsbad, California, and Kapolei, Hawaii. ${ }^{4}$ KVH will control all V3 operations using its standard network control capabilities and network management services based in Carlsbad, CA. Additionally, since this service will operate under the control of the KVH VMES network operations center, there will be

[^1]a record of the VMES's location and operating parameters as specified in Section 25.226(a)(6).


Figure 2 - VMES Network Architecture

The VMES terminal will operate in compliance with KVH's coordination agreement with the National Science Foundation with respect to Radio Astronomy Service ("RAS") sites and will not operate within 125 km of the Tracking and Data Relay Satellite System (TDRSS) sites for space research conducted at White Sands, New Mexico and the U.S. Naval Research Lab at Blossom Point, Maryland. ${ }^{5}$

## 4. Off-Axis EIRP Analysis

The data rates transmitted from the terminal will vary from $32 \mathrm{kbits} / \mathrm{s}$ to $512 \mathrm{kbits} / \mathrm{s}$. Additionally, the VMESs will transmit using CRMA spreading ${ }^{6}$ over either an 18 MHz

[^2]channel bandwidth or a 36 MHz channel bandwidth. KVH acknowledges that the small diameter V3 antenna does not meet the FCC 25.209 antenna pattern. However, KVH certifies that the aggregate EIRP levels do not exceed the limits specified for Ku-band VMESs in Section 25.226 of the Commission's rules. The co-pol off-axis EIRP spectral density levels of the KVH VMES terminal are shown in Figures 3 through 6 below. Note that a calculated worst case aggregate EIRP occurs when $\mathrm{N}=13$ users for the 36 MHz channel and when N=6 users for the 18 MHz channel. Figure 7 below shows the V3 worst case cross-pol off-axis EIRP density plots versus the FCC §25.226 mask.


Figure 3 - V3 Off-Axis EIRP Spectral Density - 36 MHz Channel


Figure 4 - V3 Off-Axis EIRP Spectral Density - 18 MHz Channel


Figure 5 - 18 MHz Off-Axis EIRP Spectral Density ${ }^{7}$

[^3]

Figure 6 - 36 MHz Channel Off-Axis EIRP Spectral Density


Figure 7 - 18 MHz Channel Cross-Pol Off-Axis EIRP Spectral Density

Per § 25.226(b)(1)(i), Table 1 below provides the co-pol the E and H plane antenna patterns for the parabolic antenna, as well as the E and H plane EIRP charts, and the FCC GSO and Elevation masks. Table 2 below provides the X-Pol E and H plane antenna gain and EIRP charts versus the FCC mask.

| Table 1 | Antenna Gain (dBi) |  |  |  |  |  |  |  |  | VMES EIRP (dBW/4 kHz) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Off- <br> Axis <br> Angle | $\begin{gathered} 14 \\ \mathrm{GHz} \\ \mathrm{E} \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ \mathrm{GHz} \\ \mathrm{H} \\ \hline \end{gathered}$ | $\begin{gathered} 14.25 \\ \mathrm{GHz} \\ \mathrm{E} \end{gathered}$ | $\begin{gathered} 14.25 \\ \mathrm{GHz} \\ \mathrm{H} \\ \hline \end{gathered}$ | $\begin{gathered} 14.5 \\ \mathrm{GHz} \\ \mathrm{E} \\ \hline \end{gathered}$ | $\begin{gathered} 14.5 \\ \mathrm{GHz} \\ \mathrm{H} \\ \hline \end{gathered}$ | Off- <br> Axis <br> Angle | $\begin{gathered} \text { FCC } \\ \S 25.20 \\ 9 \\ \hline \end{gathered}$ | $\begin{gathered} \text { FCC } \\ \text { §25.226 } \\ \text { EIRP GSO } \\ \text { Mask, N = } \\ 6 \\ \hline \end{gathered}$ | FCC §25.226 EIRP <br> EIRP <br> Elevation Mask, N = 6 | $\begin{gathered} 14 \\ \mathrm{GHz} \\ \mathrm{E} \end{gathered}$ | $\begin{gathered} 14 \\ \mathrm{GHz} \\ \mathrm{H} \end{gathered}$ | $\begin{gathered} 14.25 \\ \mathrm{GHz} \text { E } \\ \hline \end{gathered}$ | $\begin{gathered} 14.25 \\ \mathrm{GHz} \mathrm{H} \end{gathered}$ | $\begin{gathered} 14.5 \\ \mathrm{GHz} \mathrm{E} \\ \hline \end{gathered}$ | $\begin{gathered} 14.5 \\ \mathrm{GHz} \mathrm{H} \\ \hline \end{gathered}$ | Meets <br> Mask |
| -180 | -7.9 | -24.1 | -12.1 | -22.8 | -15.1 | -27.0 | -180 | 0.0 | -21.8 | -21.8 | -39.6 | -55.8 | -43.9 | -54.6 | -46.9 | -58.8 | Y |
| -175 | -11.2 | -19.5 | -12.5 | -20.7 | -15.1 | -13.6 | -175 | 0.0 | -21.8 | -21.8 | -43.0 | -51.3 | -44.3 | -52.4 | -46.9 | -45.3 | Y |
| -170 | -15.4 | -14.6 | -14.3 | -24.1 | -13.2 | -21.1 | -170 | 0.0 | -21.8 | -21.8 | -47.1 | -46.3 | -46.1 | -55.9 | -44.9 | -52.8 | Y |
| -165 | -17.4 | -19.9 | -17.1 | -15.9 | -22.3 | -19.7 | -165 | 0.0 | -21.8 | -21.8 | -49.2 | -51.7 | -48.9 | -47.7 | -54.1 | -51.4 | Y |
| -160 | -14.2 | -16.7 | -16.9 | -29.4 | -16.9 | -29.0 | -160 | 0.0 | -21.8 | -21.8 | -46.0 | -48.4 | -48.6 | -61.2 | -48.6 | -60.7 | Y |
| -155 | -16.4 | -17.7 | -25.2 | -16.5 | -25.2 | -22.2 | -155 | 0.0 | -21.8 | -21.8 | -48.2 | -49.5 | -57.0 | -48.3 | -57.0 | -53.9 | Y |
| -150 | -17.8 | -17.0 | -15.1 | -19.8 | -21.1 | -27.0 | -150 | 0.0 | -21.8 | -21.8 | -49.6 | -48.8 | -46.9 | -51.5 | -52.9 | -58.8 | Y |
| -145 | -16.0 | -21.7 | -15.7 | -23.5 | -29.7 | -24.5 | -145 | 0.0 | -21.8 | -21.8 | -47.8 | -53.4 | -47.4 | -55.3 | -61.5 | -56.2 | Y |
| -140 | -26.6 | -16.7 | -15.9 | -23.6 | -19.2 | -16.9 | -140 | 0.0 | -21.8 | -21.8 | -58.3 | -48.5 | -47.7 | -55.4 | -50.9 | -48.7 | Y |
| -135 | -20.4 | -20.0 | -10.7 | -20.7 | -28.7 | -22.5 | -135 | 0.0 | -21.8 | -21.8 | -52.1 | -51.8 | -42.5 | -52.5 | -60.5 | -54.3 | Y |
| -130 | -22.5 | -10.5 | -14.7 | -18.1 | -20.0 | -32.8 | -130 | 0.0 | -21.8 | -21.8 | -54.3 | -42.3 | -46.5 | -49.9 | -51.7 | -64.6 | Y |
| -125 | -13.0 | -21.0 | -13.7 | -27.5 | -22.7 | -15.7 | -125 | 0.0 | -21.8 | -21.8 | -44.8 | -52.7 | -45.5 | -59.2 | -54.4 | -47.5 | Y |
| -120 | -14.3 | -14.8 | -13.5 | -19.5 | -26.3 | -14.6 | -120 | 0.0 | -21.8 | -21.8 | -46.0 | -46.5 | -45.2 | -51.2 | -58.1 | -46.4 | Y |
| -115 | -14.8 | -12.1 | -15.9 | -16.4 | -15.4 | -19.6 | -115 | 0.0 | -21.8 | -21.8 | -46.6 | -43.9 | -47.7 | -48.1 | -47.1 | -51.4 | Y |
| -110 | -10.8 | -13.9 | -15.4 | -11.9 | -11.9 | -16.9 | -110 | 0.0 | -21.8 | -21.8 | -42.5 | -45.7 | -47.2 | -43.6 | -43.7 | -48.7 | Y |
| -105 | -9.6 | -13.4 | -13.6 | -12.2 | -10.2 | -12.1 | -105 | 0.0 | -21.8 | -21.8 | -41.4 | -45.1 | -45.3 | -44.0 | -41.9 | -43.9 | Y |
| -100 | -9.2 | -9.0 | -10.9 | -9.5 | -13.8 | -7.2 | -100 | 0.0 | -21.8 | -21.8 | -41.0 | -40.8 | -42.7 | -41.3 | -45.6 | -38.9 | Y |
| -95 | -8.5 | -3.8 | -9.0 | -4.7 | -9.4 | -5.7 | -95 | 0.0 | -21.8 | -21.8 | -40.3 | -35.6 | -40.8 | -36.4 | -41.1 | -37.4 | Y |
| -90 | -7.8 | -1.4 | -9.5 | -2.9 | -6.9 | -2.7 | -90 | 0.0 | -21.8 | -21.8 | -39.6 | -33.2 | -41.3 | -34.7 | -38.6 | -34.5 | Y |
| -85 | -9.1 | -0.7 | -9.6 | 0.2 | -7.4 | -0.6 | -85 | -10.0 | -31.8 | -31.8 | -40.9 | -32.5 | -41.3 | -31.6 | -39.2 | -32.4 | N |
| -80 | -8.6 | -0.1 | -12.0 | -0.2 | -8.9 | 0.0 | -80 | -10.0 | -31.8 | -31.8 | -40.4 | -31.8 | -43.8 | -31.9 | -40.6 | -31.8 | Y |
| -75 | -9.7 | -2.6 | -16.4 | -2.7 | -13.7 | -3.8 | -75 | -10.0 | -31.8 | -31.8 | -41.5 | -34.3 | -48.2 | -34.5 | -45.5 | -35.5 | Y |
| -70 | -9.0 | -8.8 | -10.3 | -13.4 | -13.2 | -7.1 | -70 | -10.0 | -31.8 | -31.8 | -40.7 | -40.6 | -42.1 | -45.1 | -44.9 | -38.9 | Y |
| -65 | -8.3 | -14.6 | -13.5 | -11.0 | -11.7 | -5.7 | -65 | -10.0 | -31.8 | -31.8 | -40.1 | -46.3 | -45.3 | -42.8 | -43.5 | -37.5 | Y |
| -60 | -6.4 | -15.3 | -12.6 | -18.7 | -5.6 | -7.8 | -60 | -10.0 | -31.8 | -31.8 | -38.2 | -47.1 | -44.4 | -50.4 | -37.3 | -39.5 | Y |
| -55 | -8.9 | -10.4 | -12.0 | -13.1 | -12.1 | -12.4 | -55 | -10.0 | -31.8 | -31.8 | -40.7 | -42.1 | -43.7 | -44.8 | -43.8 | -44.2 | Y |
| -50 | -9.8 | -18.6 | -8.6 | -22.2 | -8.6 | -12.3 | -50 | -10.0 | -31.8 | -31.8 | -41.6 | -50.4 | -40.3 | -54.0 | -40.3 | -44.1 | Y |
| -48 | -8.9 | -15.6 | -8.8 | -19.5 | -7.5 | -19.2 | -48 | -10.0 | -31.8 | -31.8 | -40.7 | -47.3 | -40.6 | -51.2 | -39.3 | -50.9 | Y |
| -45 | -7.5 | -11.1 | -9.3 | -15.4 | -6.0 | -29.4 | -45 | -9.3 | -31.1 | -31.1 | -39.3 | -42.8 | -41.0 | -47.1 | -37.8 | -61.2 | Y |
| -40 | -5.4 | -8.4 | -7.6 | -9.5 | -14.3 | -13.9 | -40 | -8.1 | -29.8 | -29.8 | -37.2 | -40.2 | -39.4 | -41.2 | -46.1 | -45.7 | Y |
| -35 | -14.5 | -6.5 | -12.9 | -8.9 | -7.5 | -13.1 | -35 | -6.6 | -28.4 | -28.4 | -46.3 | -38.2 | -44.7 | -40.7 | -39.2 | -44.9 | Y |


| -30 | -12.4 | -6.6 | -18.1 | -5.7 | -8.1 | -9.6 | -30 | -4.9 | -26.7 | -26.7 | -44.1 | -38.3 | -49.8 | -37.4 | -39.9 | -41.4 | Y |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -25 | -9.0 | -7.2 | -11.6 | -9.6 | -3.5 | -19.8 | -25 | -2.9 | -24.7 | -24.7 | -40.8 | -39.0 | -43.3 | -41.3 | -35.2 | -51.5 | Y |
| -20 | -9.9 | -11.1 | -4.5 | -9.3 | -6.1 | -7.1 | -20 | -0.5 | -22.3 | -22.3 | -41.6 | -42.9 | -36.2 | -41.1 | -37.8 | -38.8 | Y |
| -15 | 4.3 | -3.0 | 3.5 | -4.0 | 3.1 | -14.3 | -15 | 2.6 | -19.2 | -19.2 | -27.4 | -34.7 | -28.3 | -35.8 | -28.6 | -46.1 | Y |
| -10 | 5.3 | 5.6 | 3.9 | 4.8 | 3.0 | 1.4 | -10 | 7.0 | -14.8 | -14.8 | -26.4 | -26.2 | -27.9 | -26.9 | -28.8 | -30.4 | Y |
| -9.9 | 5.7 | 5.5 | 4.5 | 4.6 | 3.7 | 1.0 | -9.9 | 7.1 | -14.7 | -14.7 | -26.1 | -26.3 | -27.3 | -27.1 | -28.0 | -30.8 | Y |
| -9.8 | 5.9 | 5.3 | 5.0 | 4.4 | 4.4 | 0.6 | -9.8 | 7.2 | -14.6 | -14.6 | -25.9 | -26.4 | -26.8 | -27.4 | -27.4 | -31.1 | Y |
| -9.7 | 6.1 | 5.2 | 5.4 | 4.2 | 4.9 | 0.3 | -9.7 | 7.3 | -14.5 | -14.5 | -25.7 | -26.5 | -26.4 | -27.6 | -26.8 | -31.5 | Y |
| -9.6 | 6.2 | 5.1 | 5.8 | 4.0 | 5.4 | -0.1 | -9.6 | 7.4 | -14.3 | -14.3 | -25.6 | -26.6 | -26.0 | -27.7 | -26.4 | -31.8 | Y |
| -9.5 | 6.2 | 5.1 | 6.0 | 3.9 | 5.8 | -0.4 | -9.5 | 7.6 | -14.2 | -14.2 | -25.6 | -26.7 | -25.7 | -27.9 | -25.9 | -32.2 | Y |
| -9.4 | 6.2 | 5.1 | 6.3 | 3.8 | 6.2 | -0.7 | -9.4 | 7.7 | -14.1 | -14.1 | -25.6 | -26.7 | -25.5 | -28.0 | -25.6 | -32.4 | Y |
| -9.3 | 6.2 | 5.1 | 6.4 | 3.7 | 6.5 | -0.9 | -9.3 | 7.8 | -14.0 | -14.0 | -25.6 | -26.6 | -25.3 | -28.0 | -25.3 | -32.6 | Y |
| -9.2 | 6.1 | 5.2 | 6.6 | 3.7 | 6.7 | -1.0 | -9.2 | 8.0 | -13.8 | -13.9 | -25.7 | -26.5 | -25.2 | -28.0 | -25.0 | -32.7 | Y |
| -9.1 | 6.0 | 5.4 | 6.6 | 3.8 | 7.0 | -1.0 | -9.1 | 8.0 | -13.8 | -13.8 | -25.8 | -26.4 | -25.1 | -28.0 | -24.8 | -32.7 | Y |
| -9 | 5.8 | 5.6 | 6.7 | 4.0 | 7.2 | -0.8 | -9 | 8.0 | -13.8 | -13.6 | -25.9 | -26.2 | -25.0 | -27.8 | -24.6 | -32.5 | Y |
| -8.9 | 5.7 | 5.9 | 6.8 | 4.3 | 7.4 | -0.4 | -8.9 | 8.0 | -13.8 | -13.5 | -26.0 | -25.9 | -25.0 | -27.5 | -24.4 | -32.2 | Y |
| -8.8 | 5.7 | 6.3 | 6.8 | 4.6 | 7.6 | 0.1 | -8.8 | 8.0 | -13.8 | -13.4 | -26.1 | -25.5 | -24.9 | -27.1 | -24.2 | -31.7 | Y |
| -8.7 | 5.7 | 6.7 | 6.9 | 5.1 | 7.8 | 0.7 | -8.7 | 8.0 | -13.8 | -13.3 | -26.1 | -25.1 | -24.9 | -26.7 | -23.9 | -31.0 | Y |
| -8.6 | 5.8 | 7.2 | 7.0 | 5.6 | 8.1 | 1.5 | -8.6 | 8.0 | -13.8 | -13.1 | -26.0 | -24.6 | -24.7 | -26.1 | -23.6 | -30.2 | Y |
| -8.5 | 6.0 | 7.7 | 7.2 | 6.2 | 8.4 | 2.4 | -8.5 | 8.0 | -13.8 | -13.0 | -25.7 | -24.1 | -24.6 | -25.6 | -23.3 | -29.4 | Y |
| -8.4 | 6.4 | 8.3 | 7.4 | 6.8 | 8.8 | 3.3 | -8.4 | 8.0 | -13.8 | -12.9 | -25.4 | -23.5 | -24.3 | -24.9 | -23.0 | -28.5 | Y |
| -8.3 | 6.8 | 8.8 | 7.7 | 7.5 | 9.2 | 4.2 | -8.3 | 8.0 | -13.8 | -12.8 | -24.9 | -22.9 | -24.0 | -24.3 | -22.6 | -27.6 | Y |
| -8.2 | 7.4 | 9.4 | 8.1 | 8.2 | 9.6 | 5.1 | -8.2 | 8.0 | -13.8 | -12.6 | -24.3 | -22.3 | -23.7 | -23.6 | -22.1 | -26.7 | Y |
| -8.1 | 8.1 | 10.0 | 8.5 | 8.9 | 10.1 | 6.0 | -8.1 | 8.0 | -13.8 | -12.5 | -23.7 | -21.8 | -23.2 | -22.9 | -21.7 | -25.8 | Y |
| -8 | 8.8 | 10.6 | 9.1 | 9.5 | 10.6 | 6.8 | -8 | 8.0 | -13.8 | -12.4 | -23.0 | -21.2 | -22.7 | -22.2 | -21.1 | -24.9 | Y |
| -7.9 | 9.5 | 11.2 | 9.6 | 10.2 | 11.2 | 7.7 | -7.9 | 8.0 | -13.8 | -12.2 | -22.2 | -20.6 | -22.1 | -21.6 | -20.6 | -24.1 | Y |
| -7.8 | 10.3 | 11.7 | 10.2 | 10.8 | 11.7 | 8.5 | -7.8 | 8.0 | -13.8 | -12.1 | -21.5 | -20.0 | -21.6 | -20.9 | -20.0 | -23.3 | Y |
| -7.7 | 11.0 | 12.2 | 10.8 | 11.5 | 12.3 | 9.3 | -7.7 | 8.0 | -13.8 | -11.9 | -20.8 | -19.5 | -20.9 | -20.3 | -19.5 | -22.5 | Y |
| -7.6 | 11.7 | 12.8 | 11.4 | 12.0 | 12.9 | 10.0 | -7.6 | 8.0 | -13.8 | -11.8 | -20.1 | -19.0 | -20.3 | -19.7 | -18.9 | -21.8 | Y |
| -7.5 | 12.4 | 13.2 | 12.0 | 12.6 | 13.4 | 10.7 | -7.5 | 8.0 | -13.8 | -11.7 | -19.4 | -18.5 | -19.7 | -19.2 | -18.4 | -21.1 | Y |
| -7.4 | 13.0 | 13.7 | 12.6 | 13.1 | 13.9 | 11.3 | -7.4 | 8.0 | -13.8 | -11.5 | -18.7 | -18.1 | -19.1 | -18.6 | -17.8 | -20.4 | Y |
| -7.3 | 13.7 | 14.1 | 13.2 | 13.6 | 14.5 | 11.9 | -7.3 | 8.0 | -13.8 | -11.4 | -18.1 | -17.6 | -18.5 | -18.1 | -17.3 | -19.8 | Y |
| -7.2 | 14.2 | 14.5 | 13.8 | 14.1 | 15.0 | 12.5 | -7.2 | 8.0 | -13.8 | -11.2 | -17.5 | -17.2 | -18.0 | -17.7 | -16.8 | -19.3 | Y |
| -7.1 | 14.8 | 14.9 | 14.3 | 14.5 | 15.4 | 13.0 | -7.1 | 8.0 | -13.8 | -11.1 | -17.0 | -16.8 | -17.5 | -17.2 | -16.3 | -18.7 | Y |
| -7 | 15.3 | 15.3 | 14.8 | 15.0 | 15.9 | 13.5 | -7 | 7.9 | -13.9 | -10.9 | -16.5 | -16.5 | -17.0 | -16.8 | -15.9 | -18.2 | Y |
| -6.9 | 15.8 | 15.6 | 15.2 | 15.3 | 16.3 | 14.0 | -6.9 | 8.0 | -13.8 | -10.8 | -16.0 | -16.2 | -16.5 | -16.4 | -15.5 | -17.8 | Y |
| -6.8 | 16.2 | 15.9 | 15.7 | 15.7 | 16.7 | 14.4 | -6.8 | 8.2 | -13.6 | -10.6 | -15.6 | -15.9 | -16.1 | -16.1 | -15.1 | -17.4 | Y |
| -6.7 | 16.6 | 16.1 | 16.1 | 16.0 | 17.0 | 14.8 | -6.7 | 8.3 | -13.4 | -10.4 | -15.2 | -15.7 | -15.7 | -15.8 | -14.8 | -17.0 | Y |


| -6.6 | 17.0 | 16.3 | 16.4 | 16.2 | 17.3 | 15.1 | -6.6 | 8.5 | -13.3 | -10.3 | -14.8 | -15.4 | -15.3 | -15.5 | -14.4 | -16.6 | Y |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -6.5 | 17.3 | 16.5 | 16.7 | 16.5 | 17.6 | 15.4 | -6.5 | 8.7 | -13.1 | -10.1 | -14.5 | -15.3 | -15.0 | -15.3 | -14.2 | -16.3 | Y |
| -6.4 | 17.6 | 16.6 | 17.0 | 16.7 | 17.9 | 15.7 | -6.4 | 8.8 | -12.9 | -9.9 | -14.2 | -15.1 | -14.7 | -15.1 | -13.9 | -16.1 | Y |
| -6.3 | 17.8 | 16.8 | 17.3 | 16.8 | 18.1 | 15.9 | -6.3 | 9.0 | -12.8 | -9.8 | -14.0 | -15.0 | -14.5 | -14.9 | -13.7 | -15.9 | Y |
| -6.2 | 18.0 | 16.8 | 17.5 | 17.0 | 18.2 | 16.1 | -6.2 | 9.2 | -12.6 | -9.6 | -13.8 | -14.9 | -14.3 | -14.8 | -13.5 | -15.7 | Y |
| -6.1 | 18.2 | 16.9 | 17.6 | 17.0 | 18.4 | 16.2 | -6.1 | 9.4 | -12.4 | -9.4 | -13.6 | -14.9 | -14.1 | -14.7 | -13.4 | -15.5 | Y |
| -6 | 18.3 | 16.8 | 17.8 | 17.1 | 18.5 | 16.3 | -6 | 9.5 | -12.2 | -9.2 | -13.5 | -14.9 | -14.0 | -14.7 | -13.3 | -15.4 | Y |
| -5.9 | 18.4 | 16.8 | 17.9 | 17.1 | 18.5 | 16.4 | -5.9 | 9.7 | -12.1 | -9.1 | -13.4 | -15.0 | -13.9 | -14.7 | -13.2 | -15.4 | Y |
| -5.8 | 18.4 | 16.7 | 17.9 | 17.0 | 18.6 | 16.4 | -5.8 | 9.9 | -11.9 | -8.9 | -13.4 | -15.1 | -13.9 | -14.7 | -13.2 | -15.3 | Y |
| -5.7 | 18.4 | 16.5 | 17.9 | 17.0 | 18.5 | 16.4 | -5.7 | 10.1 | -11.7 | -8.7 | -13.4 | -15.3 | -13.9 | -14.8 | -13.2 | -15.4 | Y |
| -5.6 | 18.3 | 16.3 | 17.9 | 16.8 | 18.5 | 16.3 | -5.6 | 10.3 | -11.5 | -8.5 | -13.4 | -15.5 | -13.9 | -15.0 | -13.3 | -15.4 | Y |
| -5.5 | 18.2 | 16.0 | 17.8 | 16.6 | 18.3 | 16.2 | -5.5 | 10.5 | -11.3 | -8.3 | -13.5 | -15.8 | -14.0 | -15.2 | -13.4 | -15.6 | Y |
| -5.4 | 18.1 | 15.6 | 17.6 | 16.3 | 18.2 | 16.0 | -5.4 | 10.7 | -11.1 | -8.1 | -13.7 | -16.1 | -14.2 | -15.4 | -13.6 | -15.8 | Y |
| -5.3 | 17.8 | 15.2 | 17.4 | 16.0 | 17.9 | 15.7 | -5.3 | 10.9 | -10.9 | -7.9 | -13.9 | -16.6 | -14.4 | -15.8 | -13.8 | -16.0 | Y |
| -5.2 | 17.6 | 14.6 | 17.1 | 15.6 | 17.6 | 15.4 | -5.2 | 11.1 | -10.7 | -7.7 | -14.2 | -17.2 | -14.6 | -16.2 | -14.1 | -16.4 | Y |
| -5.1 | 17.2 | 13.9 | 16.8 | 15.1 | 17.3 | 15.0 | -5.1 | 11.3 | -10.5 | -7.5 | -14.5 | -17.8 | -15.0 | -16.7 | -14.5 | -16.8 | Y |
| -5 | 16.8 | 13.1 | 16.4 | 14.5 | 16.8 | 14.5 | -5 | 11.5 | -10.3 | -7.3 | -15.0 | -18.6 | -15.3 | -17.3 | -14.9 | -17.2 | Y |
| -4.9 | 16.3 | 12.2 | 16.0 | 13.8 | 16.3 | 14.0 | -4.9 | 11.7 | -10.0 | -7.0 | -15.4 | -19.6 | -15.8 | -18.0 | -15.5 | -17.8 | Y |
| -4.8 | 15.8 | 11.0 | 15.4 | 12.9 | 15.7 | 13.3 | -4.8 | 12.0 | -9.8 | -6.8 | -16.0 | -20.7 | -16.3 | -18.8 | -16.1 | -18.5 | Y |
| -4.7 | 15.2 | 9.7 | 14.9 | 12.0 | 14.9 | 12.6 | -4.7 | 12.2 | -9.6 | -6.6 | -16.6 | -22.0 | -16.9 | -19.8 | -16.8 | -19.2 | Y |
| -4.6 | 14.5 | 8.3 | 14.2 | 10.9 | 14.1 | 11.8 | -4.6 | 12.4 | -9.4 | -6.4 | -17.2 | -23.5 | -17.5 | -20.9 | -17.7 | -19.9 | Y |
| -4.5 | 13.9 | 6.9 | 13.6 | 9.8 | 13.2 | 11.1 | -4.5 | 12.7 | -9.1 | -6.1 | -17.9 | -24.8 | -18.1 | -21.9 | -18.6 | -20.7 | Y |
| -4.4 | 13.3 | 6.4 | 13.1 | 9.0 | 12.2 | 10.5 | -4.4 | 12.9 | -8.9 | -5.9 | -18.5 | -25.4 | -18.6 | -22.8 | -19.6 | -21.2 | Y |
| -4.3 | 12.9 | 7.2 | 12.8 | 8.8 | 11.3 | 10.4 | -4.3 | 13.2 | -8.6 | -5.6 | -18.9 | -24.6 | -18.9 | -23.0 | -20.5 | -21.4 | Y |
| -4.2 | 12.7 | 8.9 | 12.8 | 9.4 | 10.8 | 10.7 | -4.2 | 13.4 | -8.4 | -5.4 | -19.0 | -22.8 | -18.9 | -22.4 | -21.0 | -21.0 | Y |
| -4.1 | 13.0 | 10.9 | 13.2 | 10.7 | 10.8 | 11.6 | -4.1 | 13.7 | -8.1 | -5.1 | -18.7 | -20.8 | -18.5 | -21.1 | -21.0 | -20.2 | Y |
| -4 | 13.7 | 12.9 | 14.0 | 12.3 | 11.5 | 12.8 | -4 | 13.9 | -7.8 | -4.8 | -18.0 | -18.9 | -17.8 | -19.5 | -20.2 | -19.0 | Y |
| -3.9 | 14.7 | 14.6 | 15.0 | 13.9 | 12.8 | 14.1 | -3.9 | 14.2 | -7.6 | -4.6 | -17.1 | -17.1 | -16.8 | -17.9 | -19.0 | -17.6 | Y |
| -3.8 | 15.8 | 16.2 | 16.1 | 15.4 | 14.2 | 15.5 | -3.8 | 14.5 | -7.3 | -4.3 | -15.9 | -15.6 | -15.7 | -16.3 | -17.5 | -16.3 | Y |
| -3.7 | 17.0 | 17.6 | 17.2 | 16.9 | 15.7 | 16.8 | -3.7 | 14.8 | -7.0 | -4.0 | -14.8 | -14.2 | -14.5 | -14.9 | -16.1 | -15.0 | Y |
| -3.6 | 18.2 | 18.8 | 18.4 | 18.2 | 17.1 | 18.0 | -3.6 | 15.1 | -6.7 | -3.7 | -13.6 | -12.9 | -13.4 | -13.6 | -14.7 | -13.7 | Y |
| -3.5 | 19.3 | 20.0 | 19.5 | 19.4 | 18.4 | 19.2 | -3.5 | 15.4 | -6.4 | -3.4 | -12.5 | -11.8 | -12.3 | -12.4 | -13.4 | -12.6 | Y |
| -3.4 | 20.3 | 21.0 | 20.5 | 20.4 | 19.6 | 20.3 | -3.4 | 15.7 | -6.1 | -3.1 | -11.4 | -10.8 | -11.3 | -11.3 | -12.2 | -11.5 | Y |
| -3.3 | 21.3 | 21.9 | 21.4 | 21.5 | 20.7 | 21.2 | -3.3 | 16.0 | -5.7 | -2.7 | -10.5 | -9.8 | -10.3 | -10.3 | -11.1 | -10.5 | Y |
| -3.2 | 22.2 | 22.8 | 22.3 | 22.4 | 21.7 | 22.2 | -3.2 | 16.4 | -5.4 | -2.4 | -9.5 | -8.9 | -9.4 | -9.4 | -10.1 | -9.6 | Y |
| -3.1 | 23.1 | 23.6 | 23.2 | 23.2 | 22.6 | 23.0 | -3.1 | 16.7 | -5.1 | -2.1 | -8.7 | -8.1 | -8.6 | -8.5 | -9.1 | -8.7 | Y |
| -3 | 23.9 | 24.4 | 24.0 | 24.0 | 23.5 | 23.8 | -3 | 17.1 | -4.7 | -1.7 | -7.9 | -7.4 | -7.8 | -7.7 | -8.3 | -7.9 | Y |
| -2.9 | 24.6 | 25.1 | 24.7 | 24.8 | 24.3 | 24.6 | -2.9 | 17.4 | -4.3 |  | -7.1 | -6.7 | -7.0 | -7.0 | -7.5 | -7.2 | Y |


| -2.8 | 25.3 | 25.7 | 25.4 | 25.5 | 25.0 | 25.3 | -2.8 | 17.8 | -4.0 | -6.4 | -6.0 | -6.3 | -6.3 | -6.7 | -6.5 | Y |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -2.7 | 26.0 | 26.4 | 26.1 | 26.1 | 25.7 | 25.9 | -2.7 | 18.2 | -3.6 | -5.8 | -5.4 | -5.7 | -5.7 | -6.0 | -5.8 | Y |
| -2.6 | 26.6 | 26.9 | 26.7 | 26.7 | 26.4 | 26.5 | -2.6 | 18.6 | -3.2 | -5.2 | -4.8 | -5.1 | -5.1 | -5.4 | -5.2 | Y |
| -2.5 | 27.2 | 27.5 | 27.2 | 27.3 | 27.0 | 27.1 | -2.5 | 19.1 | -2.7 | -4.6 | -4.3 | -4.5 | -4.5 | -4.8 | -4.7 | Y |
| -2.4 | 27.7 | 28.0 | 27.8 | 27.8 | 27.5 | 27.6 | -2.4 | 19.5 | -2.3 | -4.1 | -3.8 | -4.0 | -4.0 | -4.2 | -4.1 | Y |
| -2.3 | 28.2 | 28.5 | 28.3 | 28.3 | 28.0 | 28.1 | -2.3 | 20.0 | -1.8 | -3.5 | -3.3 | -3.5 | -3.5 | -3.7 | -3.6 | Y |
| -2.2 | 28.7 | 28.9 | 28.8 | 28.8 | 28.5 | 28.6 | -2.2 | 20.4 | -1.3 | -3.1 | -2.9 | -3.0 | -3.0 | -3.2 | -3.1 | Y |
| -2.1 | 29.1 | 29.3 | 29.2 | 29.2 | 29.0 | 29.1 | -2.1 | 20.9 | -0.8 | -2.6 | -2.4 | -2.6 | -2.6 | -2.8 | -2.7 | Y |
| -2 | 29.5 | 29.7 | 29.6 | 29.6 | 29.4 | 29.5 | -2 | 21.5 | -0.3 | -2.2 | -2.1 | -2.2 | -2.2 | -2.3 | -2.3 | Y |
| -1.9 | 29.9 | 30.1 | 30.0 | 30.0 | 29.8 | 29.9 | -1.9 | 22.0 | 0.2 | -1.8 | -1.7 | -1.8 | -1.8 | -1.9 | -1.9 | Y |
| -1.8 | 30.3 | 30.4 | 30.4 | 30.4 | 30.2 | 30.2 | -1.8 | 22.6 | 0.8 | -1.5 | -1.3 | -1.4 | -1.4 | -1.6 | -1.5 | Y |
| -1.7 | 30.6 | 30.7 | 30.7 | 30.7 | 30.6 | 30.6 | -1.7 | 23.2 | 1.5 | -1.1 | -1.0 | -1.1 | -1.1 | -1.2 | -1.2 | Y |
| -1.6 | 31.0 | 31.0 | 31.0 | 31.0 | 30.9 | 30.9 | -1.6 | 23.9 | 2.1 | -0.8 | -0.7 | -0.8 | -0.8 | -0.9 | -0.9 | Y |
| -1.5 | 31.2 | 31.3 | 31.3 | 31.3 | 31.2 | 31.2 | -1.5 | 24.6 | 2.8 | -0.5 | -0.4 | -0.5 | -0.5 | -0.6 | -0.6 | Y |
| -1.4 | 31.5 | 31.6 | 31.6 | 31.6 | 31.5 | 31.5 | -1.4 |  |  | -0.2 | -0.2 | -0.2 | -0.2 | -0.3 | -0.3 | Y |
| -1.3 | 31.8 | 31.8 | 31.8 | 31.8 | 31.7 | 31.7 | -1.3 |  |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | Y |
| -1.2 | 32.0 | 32.0 | 32.0 | 32.0 | 31.9 | 32.0 | -1.2 |  |  | 0.2 | 0.3 | 0.3 | 0.3 | 0.2 | 0.2 | Y |
| -1.1 | 32.2 | 32.2 | 32.2 | 32.2 | 32.2 | 32.2 | -1.1 |  |  | 0.4 | 0.5 | 0.5 | 0.5 | 0.4 | 0.4 | Y |
| -1 | 32.4 | 32.4 | 32.4 | 32.4 | 32.4 | 32.4 | -1 |  |  | 0.6 | 0.6 | 0.7 | 0.7 | 0.6 | 0.6 | Y |
| -0.9 | 32.6 | 32.6 | 32.6 | 32.6 | 32.5 | 32.5 | -0.9 |  |  | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | Y |
| -0.8 | 32.7 | 32.7 | 32.7 | 32.7 | 32.7 | 32.7 | -0.8 |  |  | 0.9 | 1.0 | 1.0 | 1.0 | 0.9 | 0.9 | Y |
| -0.7 | 32.8 | 32.8 | 32.9 | 32.9 | 32.8 | 32.8 | -0.7 |  |  | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | 1.1 | Y |
| -0.6 | 32.9 | 32.9 | 33.0 | 33.0 | 32.9 | 32.9 | -0.6 |  |  | 1.2 | 1.2 | 1.2 | 1.2 | 1.2 | 1.2 | Y |
| -0.5 | 33.0 | 33.0 | 33.1 | 33.1 | 33.0 | 33.0 | -0.5 |  |  | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | Y |
| -0.4 | 33.1 | 33.1 | 33.2 | 33.2 | 33.1 | 33.1 | -0.4 |  |  | 1.4 | 1.4 | 1.4 | 1.4 | 1.3 | 1.4 | Y |
| -0.3 | 33.2 | 33.2 | 33.2 | 33.2 | 33.2 | 33.2 | -0.3 |  |  | 1.4 | 1.4 | 1.5 | 1.5 | 1.4 | 1.4 | Y |
| -0.2 | 33.2 | 33.2 | 33.3 | 33.3 | 33.2 | 33.2 | -0.2 |  |  | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | Y |
| -0.1 | 33.2 | 33.2 | 33.3 | 33.3 | 33.2 | 33.2 | -0.1 |  |  | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | Y |
| 0 | 33.3 | 33.3 | 33.3 | 33.3 | 33.3 | 33.3 | 0 |  |  | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | Y |
| 0.1 | 33.2 | 33.2 | 33.3 | 33.3 | 33.2 | 33.2 | 0.1 |  |  | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | Y |
| 0.2 | 33.2 | 33.2 | 33.3 | 33.3 | 33.2 | 33.2 | 0.2 |  |  | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | Y |
| 0.3 | 33.2 | 33.2 | 33.2 | 33.2 | 33.2 | 33.2 | 0.3 |  |  | 1.4 | 1.4 | 1.5 | 1.5 | 1.4 | 1.4 | Y |
| 0.4 | 33.1 | 33.1 | 33.2 | 33.2 | 33.1 | 33.1 | 0.4 |  |  | 1.4 | 1.4 | 1.4 | 1.4 | 1.3 | 1.3 | Y |
| 0.5 | 33.0 | 33.0 | 33.1 | 33.1 | 33.0 | 33.0 | 0.5 |  |  | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | 1.3 | Y |
| 0.6 | 32.9 | 33.0 | 33.0 | 33.0 | 32.9 | 32.9 | 0.6 |  |  | 1.2 | 1.2 | 1.2 | 1.2 | 1.2 | 1.2 | Y |
| 0.7 | 32.8 | 32.8 | 32.9 | 32.9 | 32.8 | 32.8 | 0.7 |  |  | 1.1 | 1.1 | 1.1 | 1.1 | 1.0 | 1.1 | Y |
| 0.8 | 32.7 | 32.7 | 32.7 | 32.7 | 32.7 | 32.7 | 0.8 |  |  | 0.9 | 1.0 | 1.0 | 1.0 | 0.9 | 0.9 | Y |
| 0.9 | 32.5 | 32.6 | 32.6 | 32.6 | 32.5 | 32.5 | 0.9 |  |  | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | 0.8 | Y |


| 1 | 32.4 | 32.4 | 32.4 | 32.4 | 32.3 | 32.4 | 1 |  |  |  | 0.6 | 0.7 | 0.7 | 0.7 | 0.6 | 0.6 | Y |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.1 | 32.2 | 32.2 | 32.2 | 32.2 | 32.1 | 32.2 | 1.1 |  |  |  | 0.4 | 0.5 | 0.5 | 0.5 | 0.4 | 0.4 | Y |
| 1.2 | 32.0 | 32.0 | 32.0 | 32.0 | 31.9 | 31.9 | 1.2 |  |  |  | 0.2 | 0.3 | 0.3 | 0.3 | 0.2 | 0.2 | Y |
| 1.3 | 31.8 | 31.8 | 31.8 | 31.8 | 31.7 | 31.7 | 1.3 |  |  |  | 0.0 | 0.1 | 0.0 | 0.0 | -0.1 | 0.0 | Y |
| 1.4 | 31.5 | 31.6 | 31.5 | 31.6 | 31.4 | 31.5 | 1.4 |  |  |  | -0.3 | -0.2 | -0.2 | -0.2 | -0.3 | -0.3 | Y |
| 1.5 | 31.2 | 31.3 | 31.3 | 31.3 | 31.2 | 31.2 | 1.5 | 24.6 | 2.8 |  | -0.5 | -0.4 | -0.5 | -0.5 | -0.6 | -0.6 | Y |
| 1.6 | 30.9 | 31.1 | 31.0 | 31.0 | 30.9 | 30.9 | 1.6 | 23.9 | 2.1 |  | -0.8 | -0.7 | -0.8 | -0.8 | -0.9 | -0.9 | Y |
| 1.7 | 30.6 | 30.8 | 30.7 | 30.7 | 30.5 | 30.6 | 1.7 | 23.2 | 1.5 |  | -1.1 | -1.0 | -1.1 | -1.1 | -1.2 | -1.2 | Y |
| 1.8 | 30.3 | 30.4 | 30.3 | 30.4 | 30.2 | 30.2 | 1.8 | 22.6 | 0.8 |  | -1.5 | -1.3 | -1.4 | -1.4 | -1.6 | -1.5 | Y |
| 1.9 | 29.9 | 30.1 | 30.0 | 30.0 | 29.8 | 29.9 | 1.9 | 22.0 | 0.2 |  | -1.8 | -1.7 | -1.8 | -1.8 | -2.0 | -1.9 | Y |
| 2 | 29.5 | 29.7 | 29.6 | 29.6 | 29.4 | 29.5 | 2 | 21.5 | -0.3 |  | -2.2 | -2.0 | -2.2 | -2.1 | -2.4 | -2.3 | Y |
| 2.1 | 29.1 | 29.3 | 29.2 | 29.2 | 29.0 | 29.1 | 2.1 | 20.9 | -0.8 |  | -2.6 | -2.4 | -2.6 | -2.5 | -2.8 | -2.7 | Y |
| 2.2 | 28.7 | 28.9 | 28.7 | 28.8 | 28.5 | 28.6 | 2.2 | 20.4 | -1.3 |  | -3.1 | -2.8 | -3.0 | -3.0 | -3.3 | -3.1 | Y |
| 2.3 | 28.2 | 28.5 | 28.3 | 28.3 | 28.0 | 28.2 | 2.3 | 20.0 | -1.8 |  | -3.5 | -3.3 | -3.5 | -3.4 | -3.7 | -3.6 | Y |
| 2.4 | 27.7 | 28.0 | 27.8 | 27.8 | 27.5 | 27.7 | 2.4 | 19.5 | -2.3 |  | -4.0 | -3.7 | -4.0 | -3.9 | -4.3 | -4.1 | Y |
| 2.5 | 27.2 | 27.5 | 27.2 | 27.3 | 26.9 | 27.1 | 2.5 | 19.1 | -2.7 |  | -4.6 | -4.2 | -4.5 | -4.4 | -4.8 | -4.6 | Y |
| 2.6 | 26.6 | 27.0 | 26.7 | 26.8 | 26.3 | 26.6 | 2.6 | 18.6 | -3.2 |  | -5.2 | -4.8 | -5.1 | -5.0 | -5.4 | -5.2 | Y |
| 2.7 | 26.0 | 26.4 | 26.1 | 26.2 | 25.7 | 26.0 | 2.7 | 18.2 | -3.6 |  | -5.8 | -5.3 | -5.7 | -5.6 | -6.1 | -5.8 | Y |
| 2.8 | 25.3 | 25.8 | 25.4 | 25.5 | 25.0 | 25.3 | 2.8 | 17.8 | -4.0 |  | -6.4 | -6.0 | -6.3 | -6.2 | -6.8 | -6.4 | Y |
| 2.9 | 24.7 | 25.2 | 24.7 | 24.9 | 24.3 | 24.7 | 2.9 | 17.4 | -4.3 |  | -7.1 | -6.6 | -7.0 | -6.9 | -7.5 | -7.1 | Y |
| 3 | 23.9 | 24.5 | 24.0 | 24.1 | 23.5 | 23.9 | 3 | 17.1 | -4.7 | -1.7 | -7.9 | -7.3 | -7.8 | -7.6 | -8.3 | -7.8 | Y |
| 3.1 | 23.1 | 23.7 | 23.2 | 23.4 | 22.6 | 23.2 | 3.1 | 16.7 | -5.1 | -2.1 | -8.7 | -8.1 | -8.5 | -8.4 | -9.1 | -8.6 | Y |
| 3.2 | 22.3 | 22.9 | 22.4 | 22.5 | 21.7 | 22.3 | 3.2 | 16.4 | -5.4 | -2.4 | -9.5 | -8.9 | -9.3 | -9.2 | -10.1 | -9.4 | Y |
| 3.3 | 21.3 | 22.0 | 21.5 | 21.7 | 20.7 | 21.5 | 3.3 | 16.0 | -5.7 | -2.7 | -10.4 | -9.7 | -10.2 | -10.1 | -11.0 | -10.3 | Y |
| 3.4 | 20.4 | 21.1 | 20.6 | 20.7 | 19.7 | 20.5 | 3.4 | 15.7 | -6.1 | -3.1 | -11.4 | -10.7 | -11.1 | -11.1 | -12.1 | -11.2 | Y |
| 3.5 | 19.3 | 20.1 | 19.7 | 19.7 | 18.5 | 19.5 | 3.5 | 15.4 | -6.4 | -3.4 | -12.4 | -11.7 | -12.1 | -12.1 | -13.2 | -12.2 | Y |
| 3.6 | 18.2 | 19.0 | 18.7 | 18.6 | 17.3 | 18.5 | 3.6 | 15.1 | -6.7 | -3.7 | -13.5 | -12.8 | -13.1 | -13.2 | -14.5 | -13.3 | Y |
| 3.7 | 17.1 | 17.8 | 17.7 | 17.4 | 16.0 | 17.3 | 3.7 | 14.8 | -7.0 | -4.0 | -14.7 | -14.0 | -14.1 | -14.4 | -15.7 | -14.4 | Y |
| 3.8 | 15.9 | 16.5 | 16.7 | 16.1 | 14.8 | 16.2 | 3.8 | 14.5 | -7.3 | -4.3 | -15.9 | -15.3 | -15.1 | -15.7 | -17.0 | -15.6 | Y |
| 3.9 | 14.7 | 15.0 | 15.8 | 14.8 | 13.6 | 15.0 | 3.9 | 14.2 | -7.6 | -4.6 | -17.0 | -16.7 | -16.0 | -17.0 | -18.2 | -16.8 | Y |
| 4 | 13.7 | 13.5 | 15.0 | 13.4 | 12.6 | 13.8 | 4 | 13.9 | -7.8 | -4.8 | -18.0 | -18.3 | -16.8 | -18.3 | -19.2 | -18.0 | Y |
| 4.1 | 13.0 | 11.9 | 14.5 | 12.2 | 12.1 | 12.8 | 4.1 | 13.7 | -8.1 | -5.1 | -18.8 | -19.9 | -17.3 | -19.6 | -19.7 | -19.0 | Y |
| 4.2 | 12.6 | 10.3 | 14.2 | 11.2 | 12.0 | 12.0 | 4.2 | 13.4 | -8.4 | -5.4 | -19.2 | -21.5 | -17.5 | -20.6 | -19.7 | -19.8 | Y |
| 4.3 | 12.6 | 9.0 | 14.3 | 10.6 | 12.4 | 11.6 | 4.3 | 13.2 | -8.6 | -5.6 | -19.1 | -22.7 | -17.5 | -21.2 | -19.3 | -20.2 | Y |
| 4.4 | 13.0 | 8.5 | 14.5 | 10.6 | 13.1 | 11.6 | 4.4 | 12.9 | -8.9 | -5.9 | -18.7 | -23.3 | -17.2 | -21.2 | -18.7 | -20.2 | Y |
| 4.5 | 13.6 | 8.8 | 14.9 | 11.0 | 13.8 | 11.8 | 4.5 | 12.7 | -9.1 | -6.1 | -18.2 | -23.0 | -16.8 | -20.8 | -17.9 | -19.9 | Y |
| 4.6 | 14.3 | 9.7 | 15.4 | 11.7 | 14.6 | 12.3 | 4.6 | 12.4 | -9.4 | -6.4 | -17.5 | -22.1 | -16.3 | -20.1 | -17.2 | -19.4 | Y |
| 4.7 | 14.9 | 10.7 | 15.9 | 12.5 | 15.3 | 12.9 | 4.7 | 12.2 | -9.6 | -6.6 | -16.8 | -21.0 | -15.8 | -19.3 | -16.5 | -18.9 | Y |


| 4.8 | 15.5 | 11.8 | 16.4 | 13.2 | 15.9 | 13.5 | 4.8 | 12.0 | -9.8 | -6.8 | -16.2 | -20.0 | -15.4 | -18.5 | -15.8 | -18.3 | Y |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4.9 | 16.1 | 12.8 | 16.8 | 13.9 | 16.5 | 14.0 | 4.9 | 11.7 | -10.0 | -7.0 | -15.7 | -19.0 | -14.9 | -17.8 | -15.3 | -17.7 | Y |
| 5 | 16.6 | 13.6 | 17.2 | 14.5 | 16.9 | 14.5 | 5 | 11.5 | -10.3 | -7.3 | -15.2 | -18.2 | -14.6 | -17.2 | -14.8 | -17.3 | Y |
| 5.1 | 17.0 | 14.3 | 17.5 | 15.1 | 17.3 | 14.9 | 5.1 | 11.3 | -10.5 | -7.5 | -14.8 | -17.5 | -14.2 | -16.7 | -14.4 | -16.8 | Y |
| 5.2 | 17.4 | 14.9 | 17.8 | 15.5 | 17.7 | 15.3 | 5.2 | 11.1 | -10.7 | -7.7 | -14.4 | -16.9 | -14.0 | -16.2 | -14.1 | -16.5 | Y |
| 5.3 | 17.6 | 15.4 | 18.0 | 15.9 | 17.9 | 15.6 | 5.3 | 10.9 | -10.9 | -7.9 | -14.1 | -16.4 | -13.7 | -15.9 | -13.8 | -16.2 | Y |
| 5.4 | 17.9 | 15.8 | 18.2 | 16.2 | 18.1 | 15.8 | 5.4 | 10.7 | -11.1 | -8.1 | -13.9 | -15.9 | -13.6 | -15.5 | -13.6 | -15.9 | Y |
| 5.5 | 18.1 | 16.2 | 18.3 | 16.5 | 18.3 | 16.0 | 5.5 | 10.5 | -11.3 | -8.3 | -13.7 | -15.6 | -13.4 | -15.3 | -13.5 | -15.8 | Y |
| 5.6 | 18.2 | 16.4 | 18.4 | 16.6 | 18.4 | 16.1 | 5.6 | 10.3 | -11.5 | -8.5 | -13.6 | -15.3 | -13.4 | -15.1 | -13.4 | -15.6 | Y |
| 5.7 | 18.2 | 16.6 | 18.4 | 16.8 | 18.4 | 16.2 | 5.7 | 10.1 | -11.7 | -8.7 | -13.5 | -15.1 | -13.3 | -15.0 | -13.3 | -15.6 | Y |
| 5.8 | 18.3 | 16.8 | 18.4 | 16.9 | 18.4 | 16.2 | 5.8 | 9.9 | -11.9 | -8.9 | -13.5 | -15.0 | -13.3 | -14.9 | -13.3 | -15.6 | Y |
| 5.9 | 18.3 | 16.9 | 18.4 | 16.9 | 18.4 | 16.2 | 5.9 | 9.7 | -12.1 | -9.1 | -13.5 | -14.9 | -13.4 | -14.9 | -13.3 | -15.6 | Y |
| 6 | 18.2 | 17.0 | 18.3 | 16.9 | 18.3 | 16.1 | 6 | 9.5 | -12.2 | -9.2 | -13.6 | -14.8 | -13.5 | -14.9 | -13.4 | -15.7 | Y |
| 6.1 | 18.1 | 17.0 | 18.2 | 16.8 | 18.2 | 16.0 | 6.1 | 9.4 | -12.4 | -9.4 | -13.7 | -14.8 | -13.6 | -14.9 | -13.5 | -15.8 | Y |
| 6.2 | 17.9 | 16.9 | 18.0 | 16.7 | 18.1 | 15.8 | 6.2 | 9.2 | -12.6 | -9.6 | -13.8 | -14.8 | -13.8 | -15.0 | -13.7 | -15.9 | Y |
| 6.3 | 17.8 | 16.9 | 17.8 | 16.6 | 17.9 | 15.7 | 6.3 | 9.0 | -12.8 | -9.8 | -14.0 | -14.9 | -14.0 | -15.2 | -13.8 | -16.1 | Y |
| 6.4 | 17.5 | 16.7 | 17.6 | 16.4 | 17.7 | 15.4 | 6.4 | 8.8 | -12.9 | -9.9 | -14.2 | -15.0 | -14.2 | -15.3 | -14.1 | -16.3 | Y |
| 6.5 | 17.3 | 16.6 | 17.3 | 16.2 | 17.5 | 15.2 | 6.5 | 8.7 | -13.1 | -10.1 | -14.5 | -15.2 | -14.5 | -15.5 | -14.3 | -16.6 | Y |
| 6.6 | 17.0 | 16.4 | 17.0 | 16.0 | 17.2 | 14.8 | 6.6 | 8.5 | -13.3 | -10.3 | -14.8 | -15.3 | -14.8 | -15.8 | -14.6 | -16.9 | Y |
| 6.7 | 16.7 | 16.2 | 16.6 | 15.7 | 16.9 | 14.5 | 6.7 | 8.3 | -13.4 | -10.4 | -15.1 | -15.6 | -15.1 | -16.1 | -14.9 | -17.3 | Y |
| 6.8 | 16.3 | 16.0 | 16.3 | 15.4 | 16.5 | 14.1 | 6.8 | 8.2 | -13.6 | -10.6 | -15.5 | -15.8 | -15.5 | -16.4 | -15.3 | -17.6 | Y |
| 6.9 | 15.9 | 15.7 | 15.9 | 15.0 | 16.1 | 13.7 | 6.9 | 8.0 | -13.8 | -10.8 | -15.9 | -16.1 | -15.9 | -16.7 | -15.6 | -18.1 | Y |
| 7 | 15.4 | 15.4 | 15.4 | 14.7 | 15.7 | 13.2 | 7 | 7.9 | -13.9 | -10.9 | -16.3 | -16.4 | -16.3 | -17.1 | -16.0 | -18.5 | Y |
| 7.1 | 15.0 | 15.0 | 15.0 | 14.3 | 15.3 | 12.7 | 7.1 | 8.0 | -13.8 | -11.1 | -16.8 | -16.7 | -16.8 | -17.5 | -16.5 | -19.0 | Y |
| 7.2 | 14.4 | 14.6 | 14.5 | 13.8 | 14.8 | 12.2 | 7.2 | 8.0 | -13.8 | -11.2 | -17.3 | -17.1 | -17.3 | -17.9 | -16.9 | -19.5 | Y |
| 7.3 | 13.9 | 14.2 | 13.9 | 13.3 | 14.3 | 11.7 | 7.3 | 8.0 | -13.8 | -11.4 | -17.9 | -17.5 | -17.8 | -18.4 | -17.4 | -20.1 | Y |
| 7.4 | 13.3 | 13.8 | 13.4 | 12.8 | 13.8 | 11.0 | 7.4 | 8.0 | -13.8 | -11.5 | -18.4 | -18.0 | -18.4 | -18.9 | -18.0 | -20.7 | Y |
| 7.5 | 12.7 | 13.3 | 12.8 | 12.3 | 13.3 | 10.4 | 7.5 | 8.0 | -13.8 | -11.7 | -19.1 | -18.4 | -18.9 | -19.4 | -18.5 | -21.4 | Y |
| 7.6 | 12.1 | 12.9 | 12.3 | 11.8 | 12.7 | 9.7 | 7.6 | 8.0 | -13.8 | -11.8 | -19.7 | -18.9 | -19.5 | -20.0 | -19.0 | -22.0 | Y |
| 7.7 | 11.4 | 12.3 | 11.7 | 11.2 | 12.1 | 9.0 | 7.7 | 8.0 | -13.8 | -11.9 | -20.4 | -19.4 | -20.1 | -20.6 | -19.6 | -22.7 | Y |
| 7.8 | 10.7 | 11.8 | 11.1 | 10.6 | 11.6 | 8.3 | 7.8 | 8.0 | -13.8 | -12.1 | -21.1 | -19.9 | -20.7 | -21.2 | -20.2 | -23.5 | Y |
| 7.9 | 10.0 | 11.3 | 10.5 | 9.9 | 11.0 | 7.5 | 7.9 | 8.0 | -13.8 | -12.2 | -21.8 | -20.5 | -21.3 | -21.8 | -20.8 | -24.3 | Y |
| 8 | 9.3 | 10.7 | 9.9 | 9.3 | 10.5 | 6.7 | 8 | 8.0 | -13.8 | -12.4 | -22.5 | -21.1 | -21.8 | -22.5 | -21.3 | -25.1 | Y |
| 8.1 | 8.6 | 10.1 | 9.4 | 8.7 | 9.9 | 5.8 | 8.1 | 8.0 | -13.8 | -12.5 | -23.1 | -21.6 | -22.4 | -23.1 | -21.8 | -25.9 | Y |
| 8.2 | 8.0 | 9.5 | 8.9 | 8.0 | 9.4 | 5.0 | 8.2 | 8.0 | -13.8 | -12.6 | -23.8 | -22.2 | -22.9 | -23.8 | -22.3 | -26.8 | Y |
| 8.3 | 7.3 | 9.0 | 8.4 | 7.4 | 8.9 | 4.1 | 8.3 | 8.0 | -13.8 | -12.8 | -24.4 | -22.8 | -23.4 | -24.4 | -22.8 | -27.6 | Y |
| 8.4 | 6.8 | 8.4 | 8.0 | 6.7 | 8.5 | 3.3 | 8.4 | 8.0 | -13.8 | -12.9 | -25.0 | -23.4 | -23.8 | -25.0 | -23.2 | -28.5 | Y |
| 8.5 | 6.3 | 7.8 | 7.6 | 6.2 | 8.1 | 2.5 | 8.5 | 8.0 | -13.8 | -13.0 | -25.4 | -23.9 | -24.1 | -25.6 | -23.6 | -29.3 | Y |


| 8.6 | 6.0 | 7.3 | 7.3 | 5.6 | 7.8 | 1.8 | 8.6 | 8.0 | -13.8 | -13.1 | -25.8 | -24.5 | -24.4 | -26.1 | -24.0 | -30.0 | Y |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8.7 | 5.7 | 6.8 | 7.1 | 5.1 | 7.5 | 1.1 | 8.7 | 8.0 | -13.8 | -13.3 | -26.0 | -25.0 | -24.7 | -26.6 | -24.3 | -30.7 | Y |
| 8.8 | 5.5 | 6.3 | 6.9 | 4.7 | 7.2 | 0.5 | 8.8 | 8.0 | -13.8 | -13.4 | -26.2 | -25.4 | -24.9 | -27.0 | -24.5 | -31.2 | Y |
| 8.9 | 5.5 | 5.9 | 6.7 | 4.4 | 7.0 | 0.1 | 8.9 | 8.0 | -13.8 | -13.5 | -26.3 | -25.8 | -25.1 | -27.4 | -24.8 | -31.6 | Y |
| 9 | 5.4 | 5.6 | 6.5 | 4.1 | 6.7 | -0.1 | 9 | 8.0 | -13.8 | -13.6 | -26.3 | -26.1 | -25.2 | -27.6 | -25.0 | -31.9 | Y |
| 9.1 | 5.4 | 5.4 | 6.4 | 4.0 | 6.5 | -0.3 | 9.1 | 8.0 | -13.8 | -13.8 | -26.3 | -26.4 | -25.4 | -27.8 | -25.3 | -32.0 | Y |
| 9.2 | 5.4 | 5.2 | 6.2 | 3.9 | 6.2 | -0.2 | 9.2 | 8.0 | -13.8 | -13.9 | -26.3 | -26.6 | -25.6 | -27.9 | -25.5 | -32.0 | Y |
| 9.3 | 5.4 | 5.0 | 5.9 | 3.9 | 5.9 | -0.1 | 9.3 | 7.8 | -14.0 | -14.0 | -26.3 | -26.7 | -25.8 | -27.9 | -25.8 | -31.9 | Y |
| 9.4 | 5.4 | 5.0 | 5.7 | 3.9 | 5.6 | 0.1 | 9.4 | 7.7 | -14.1 | -14.1 | -26.4 | -26.8 | -26.1 | -27.9 | -26.2 | -31.7 | Y |
| 9.5 | 5.4 | 4.9 | 5.4 | 4.0 | 5.2 | 0.3 | 9.5 | 7.6 | -14.2 | -14.2 | -26.4 | -26.8 | -26.4 | -27.8 | -26.6 | -31.4 | Y |
| 9.6 | 5.3 | 5.0 | 5.0 | 4.1 | 4.7 | 0.6 | 9.6 | 7.4 | -14.3 | -14.3 | -26.5 | -26.8 | -26.7 | -27.6 | -27.0 | -31.1 | Y |
| 9.7 | 5.1 | 5.1 | 4.6 | 4.3 | 4.2 | 1.0 | 9.7 | 7.3 | -14.5 | -14.5 | -26.6 | -26.7 | -27.2 | -27.5 | -27.5 | -30.8 | Y |
| 9.8 | 4.9 | 5.2 | 4.1 | 4.5 | 3.6 | 1.3 | 9.8 | 7.2 | -14.6 | -14.6 | -26.8 | -26.6 | -27.7 | -27.3 | -28.1 | -30.5 | Y |
| 9.9 | 4.6 | 5.3 | 3.5 | 4.7 | 2.9 | 1.6 | 9.9 | 7.1 | -14.7 | -14.7 | -27.1 | -26.5 | -28.3 | -27.1 | -28.9 | -30.1 | Y |
| 10 | 4.3 | 5.4 | 2.8 | 4.9 | 2.1 | 2.0 | 10 | 7.0 | -14.8 | -14.8 | -27.5 | -26.3 | -29.0 | -26.9 | -29.7 | -29.8 | Y |
| 15 | 4.0 | -3.6 | 3.2 | -4.8 | 2.6 | -20.2 | 15 | 2.6 | -19.2 | -19.2 | -27.8 | -35.4 | -28.6 | -36.6 | -29.1 | -52.0 | Y |
| 20 | -9.3 | -14.7 | -7.1 | -9.0 | -5.8 | -6.5 | 20 | -0.5 | -22.3 | -22.3 | -41.0 | -46.5 | -38.9 | -40.7 | -37.6 | -38.3 | Y |
| 25 | -13.2 | -7.0 | -16.0 | -9.1 | -5.0 | -16.3 | 25 | -2.9 | -24.7 | -24.7 | -45.0 | -38.7 | -47.7 | -40.9 | -36.8 | -48.1 | Y |
| 30 | -19.0 | -5.1 | -13.8 | -4.5 | -7.8 | -8.7 | 30 | -4.9 | -26.7 | -26.7 | -50.7 | -36.9 | -45.6 | -36.3 | -39.5 | -40.5 | Y |
| 35 | -7.0 | -8.8 | -5.9 | -8.1 | -4.0 | -10.2 | 35 | -6.6 | -28.4 | -28.4 | -38.7 | -40.6 | -37.6 | -39.9 | -35.8 | -42.0 | Y |
| 40 | -9.0 | -12.9 | -9.1 | -13.4 | -10.8 | -17.6 | 40 | -8.1 | -29.8 | -29.8 | -40.8 | -44.7 | -40.8 | -45.2 | -42.6 | -49.4 | Y |
| 45 | -8.6 | -10.2 | -10.0 | -10.8 | -10.0 | -16.7 | 45 | -9.3 | -31.1 | -31.1 | -40.4 | -41.9 | -41.8 | -42.6 | -41.8 | -48.4 | Y |
| 48 | -11.4 | -16.0 | -9.2 | -14.4 | -6.9 | -10.6 | 48 | -10.0 | -31.8 | -31.8 | -43.2 | -47.8 | -41.0 | -46.2 | -38.7 | -42.4 | Y |
| 50 | -13.3 | -19.9 | -8.7 | -16.8 | -4.8 | -6.6 | 50 | -10.0 | -31.8 | -31.8 | -45.0 | -51.7 | -40.5 | -48.6 | -36.6 | -38.4 | Y |
| 55 | -4.6 | -8.9 | -6.1 | -12.1 | -9.4 | -8.3 | 55 | -10.0 | -31.8 | -31.8 | -36.4 | -40.7 | -37.9 | -43.9 | -41.2 | -40.1 | Y |
| 60 | -8.6 | -12.9 | -13.6 | -23.4 | -12.4 | -11.7 | 60 | -10.0 | -31.8 | -31.8 | -40.4 | -44.7 | -45.3 | -55.1 | -44.2 | -43.5 | Y |
| 65 | -9.6 | -10.2 | -15.5 | -9.3 | -17.1 | -6.6 | 65 | -10.0 | -31.8 | -31.8 | -41.3 | -42.0 | -47.3 | -41.0 | -48.9 | -38.4 | Y |
| 70 | -9.6 | -8.7 | -12.7 | -9.6 | -8.7 | -10.4 | 70 | -10.0 | -31.8 | -31.8 | -41.3 | -40.4 | -44.4 | -41.4 | -40.5 | -42.1 | Y |
| 75 | -13.8 | -1.8 | -17.1 | -3.1 | -11.2 | -4.1 | 75 | -10.0 | -31.8 | -31.8 | -45.5 | -33.6 | -48.9 | -34.8 | -43.0 | -35.9 | Y |
| 80 | -11.7 | 0.6 | -10.3 | -0.6 | -8.6 | -0.5 | 80 | -10.0 | -31.8 | -31.8 | -43.5 | -31.2 | -42.0 | -32.3 | -40.4 | -32.2 | N |
| 85 | -8.2 | -0.2 | -8.7 | -1.0 | -8.6 | -1.9 | 85 | -10.0 | -31.8 | -31.8 | -39.9 | -31.9 | -40.4 | -32.7 | -40.3 | -33.6 | Y |
| 90 | -6.5 | -1.3 | -8.4 | -3.6 | -8.1 | -1.8 | 90 | 0.0 | -21.8 | -21.8 | -38.2 | -33.0 | -40.1 | -35.3 | -39.9 | -33.5 | Y |
| 95 | -10.0 | -5.2 | -9.4 | -4.9 | -7.4 | -5.3 | 95 | 0.0 | -21.8 | -21.8 | -41.8 | -36.9 | -41.2 | -36.6 | -39.2 | -37.1 | Y |
| 100 | -12.2 | -8.9 | -9.1 | -9.8 | -11.7 | -7.6 | 100 | 0.0 | -21.8 | -21.8 | -44.0 | -40.7 | -40.9 | -41.6 | -43.5 | -39.4 | Y |
| 105 | -13.1 | -12.8 | -11.9 | -11.6 | -14.4 | -12.2 | 105 | 0.0 | -21.8 | -21.8 | -44.9 | -44.5 | -43.6 | -43.4 | -46.2 | -44.0 | Y |
| 110 | -13.6 | -13.0 | -14.7 | -13.5 | -12.9 | -16.4 | 110 | 0.0 | -21.8 | -21.8 | -45.4 | -44.7 | -46.5 | -45.2 | -44.7 | -48.2 | Y |
| 115 | -12.1 | -11.7 | -13.8 | -15.5 | -17.7 | -18.8 | 115 | 0.0 | -21.8 | -21.8 | -43.9 | -43.5 | -45.5 | -47.3 | -49.5 | -50.6 | Y |
| 120 | -19.3 | -23.5 | -20.7 | -17.0 | -14.6 | -31.8 | 120 | 0.0 | -21.8 | -21.8 | -51.1 | -55.2 | -52.4 | -48.7 | -46.3 | -63.5 | Y |


| 125 | -16.1 | -20.6 | -15.1 | -22.8 | -12.3 | -23.0 | 125 | 0.0 | -21.8 | -21.8 | -47.9 | -52.4 | -46.8 | -54.6 | -44.0 | -54.7 | Y |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 130 | -14.6 | -13.8 | -15.6 | -19.5 | -22.8 | -18.4 | 130 | 0.0 | -21.8 | -21.8 | -46.4 | -45.6 | -47.4 | -51.2 | -54.5 | -50.2 | Y |
| 135 | -14.5 | -13.5 | -13.0 | -14.8 | -30.7 | -34.6 | 135 | 0.0 | -21.8 | -21.8 | -46.3 | -45.2 | -44.8 | -46.6 | -62.5 | -66.3 | Y |
| 140 | -17.1 | -22.3 | -38.2 | -16.0 | -34.0 | -36.5 | 140 | 0.0 | -21.8 | -21.8 | -48.8 | -54.1 | -69.9 | -47.8 | -65.8 | -68.2 | Y |
| 145 | -21.4 | -29.2 | -22.4 | -25.5 | -18.2 | -25.4 | 145 | 0.0 | -21.8 | -21.8 | -53.2 | -61.0 | -54.2 | -57.3 | -49.9 | -57.2 | Y |
| 150 | -19.6 | -17.1 | -23.5 | -21.2 | -19.3 | -21.2 | 150 | 0.0 | -21.8 | -21.8 | -51.3 | -48.9 | -55.3 | -53.0 | -51.0 | -53.0 | Y |
| 155 | -26.5 | -19.2 | -19.1 | -18.1 | -25.9 | -24.4 | 155 | 0.0 | -21.8 | -21.8 | -58.2 | -50.9 | -50.9 | -49.8 | -57.6 | -56.1 | Y |
| 160 | -18.7 | -26.6 | -18.1 | -25.5 | -31.7 | -19.3 | 160 | 0.0 | -21.8 | -21.8 | -50.5 | -58.4 | -49.8 | -57.2 | -63.5 | -51.1 | Y |
| 165 | -19.9 | -37.0 | -18.5 | -43.5 | -33.7 | -28.9 | 165 | 0.0 | -21.8 | -21.8 | -51.7 | -68.8 | -50.2 | -75.3 | -65.4 | -60.7 | Y |
| 170 | -14.2 | -18.7 | -11.9 | -20.4 | -16.7 | -16.0 | 170 | 0.0 | -21.8 | -21.8 | -46.0 | -50.4 | -43.7 | -52.2 | -48.4 | -47.8 | Y |
| 175 | -13.3 | -25.8 | -19.6 | -21.6 | -18.1 | -16.3 | 175 | 0.0 | -21.8 | -21.8 | -45.1 | -57.6 | -51.3 | -53.4 | -49.8 | -48.1 | Y |
| 180 | -23.8 | -8.6 | -15.2 | -13.9 | -16.3 | -26.9 | 180 | 0.0 | -21.8 | -21.8 | -55.6 | -40.4 | -47.0 | -45.6 | -48.1 | -58.7 | Y |


| Table 2 | Antenna Gain X-Pol |  |  |  |  |  | VMES EIRP X-Pol |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OffAxis Angle (degree) | $\begin{gathered} 14 \mathrm{GHz} \\ \mathrm{E} \\ \hline \end{gathered}$ | $\begin{gathered} 14.25 \\ \mathrm{GHz} \text { E } \\ \hline \end{gathered}$ | $\begin{gathered} 14.5 \\ \mathrm{GHz} \mathrm{E} \\ \hline \end{gathered}$ | OffAxis Angle (degree) | $\begin{gathered} \text { FCC } \\ 25.209(\mathrm{~b})(1) \\ \hline \end{gathered}$ | $\begin{gathered} \text { §25.226 } \\ \text { X-Pol } \\ \text { Mask,N=6 } \\ \hline \end{gathered}$ | $\begin{gathered} 14 \mathrm{GHz} \\ \mathrm{E} \\ \hline \end{gathered}$ | $\begin{gathered} 14.25 \\ \mathrm{GHz} \\ \mathrm{E} \\ \hline \end{gathered}$ | $\begin{gathered} 14.5 \\ \text { GHz } \\ \mathrm{E} \\ \hline \end{gathered}$ | Worst case Exceedance EIRP (dB) | Meets Mask |
| -9.2 | -18.83 | -16.455 | -31.01 | -9.2 | -2.0 | -23.8 | -50.6 | -48.2 | -62.8 | 26.8 | Y |
| -9.1 | -18.67 | -16.509 | -31.47 | -9.1 | -2.0 | -23.8 | -50.4 | -48.3 | -63.2 | 26.7 | Y |
| -9.0 | -18.53 | -16.594 | -31.99 | -9.0 | -2.0 | -23.8 | -50.3 | -48.4 | -63.7 | 26.5 | Y |
| -8.9 | -18.41 | -16.708 | -32.56 | -8.9 | -2.0 | -23.8 | -50.2 | -48.5 | -64.3 | 26.4 | Y |
| -8.8 | -18.3 | -16.853 | -33.16 | -8.8 | -2.0 | -23.8 | -50.1 | -48.6 | -64.9 | 26.3 | Y |
| -8.7 | -18.22 | -17.028 | -33.74 | -8.7 | -2.0 | -23.8 | -50.0 | -48.8 | -65.5 | 26.2 | Y |
| -8.6 | -18.15 | -17.232 | -34.25 | -8.6 | -2.0 | -23.8 | -49.9 | -49.0 | -66.0 | 26.1 | Y |
| -8.5 | -18.11 | -17.464 | -34.59 | -8.5 | -2.0 | -23.8 | -49.9 | -49.2 | -66.4 | 26.1 | Y |
| -8.4 | -18.09 | -17.725 | -34.7 | -8.4 | -2.0 | -23.8 | -49.8 | -49.5 | -66.5 | 26.1 | Y |
| -8.3 | -18.09 | -18.014 | -34.51 | -8.3 | -2.0 | -23.8 | -49.9 | -49.8 | -66.3 | 26.1 | Y |
| -8.2 | -18.12 | -18.329 | -34.03 | -8.2 | -2.0 | -23.8 | -49.9 | -50.1 | -65.8 | 26.1 | Y |
| -8.1 | -18.18 | -18.67 | -33.3 | -8.1 | -2.0 | -23.8 | -49.9 | -50.4 | -65.1 | 26.2 | Y |
| -8.0 | -18.26 | -19.036 | -32.42 | -8.0 | -2.0 | -23.8 | -50.0 | -50.8 | -64.2 | 26.2 | Y |
| -7.9 | -18.36 | -19.427 | -31.45 | -7.9 | -2.0 | -23.8 | -50.1 | -51.2 | -63.2 | 26.3 | Y |
| -7.8 | -18.49 | -19.841 | -30.45 | -7.8 | -2.0 | -23.8 | -50.3 | -51.6 | -62.2 | 26.5 | Y |
| -7.7 | -18.65 | -20.279 | -29.45 | -7.7 | -2.0 | -23.8 | -50.4 | -52.0 | -61.2 | 26.6 | Y |
| -7.6 | -18.84 | -20.74 | -28.48 | -7.6 | -2.0 | -23.8 | -50.6 | -52.5 | -60.2 | 26.8 | Y |
| -7.5 | -19.06 | -21.222 | -27.56 | -7.5 | -2.0 | -23.8 | -50.8 | -53.0 | -59.3 | 27.0 | Y |
| -7.4 | -19.31 | -21.726 | -26.67 | -7.4 | -2.0 | -23.8 | -51.1 | -53.5 | -58.4 | 27.3 | Y |
| -7.3 | -19.59 | -22.25 | -25.84 | -7.3 | -2.0 | -23.8 | -51.4 | -54.0 | -57.6 | 27.6 | Y |
| -7.2 | -19.91 | -22.794 | -25.06 | -7.2 | -2.0 | -23.8 | -51.7 | -54.6 | -56.8 | 27.9 | Y |
| -7.1 | -20.26 | -23.355 | -24.32 | -7.1 | -2.0 | -23.8 | -52.0 | -55.1 | -56.1 | 28.2 | Y |
| -7.0 | -20.64 | -23.931 | -23.64 | -7.0 | -2.1 | -23.9 | -52.4 | -55.7 | -55.4 | 28.5 | Y |
| -6.9 | -21.07 | -24.519 | -23.02 | -6.9 | -2.0 | -23.8 | -52.8 | -56.3 | -54.8 | 29.1 | Y |
| -6.8 | -21.53 | -25.112 | -22.44 | -6.8 | -1.8 | -23.6 | -53.3 | -56.9 | -54.2 | 29.7 | Y |
| -6.7 | -22.04 | -25.702 | -21.91 | -6.7 | -1.7 | -23.4 | -53.8 | -57.5 | -53.7 | 30.4 | Y |
| -6.6 | -22.6 | -26.279 | -21.44 | -6.6 | -1.5 | -23.3 | -54.4 | -58.0 | -53.2 | 31.1 | Y |
| -6.5 | -23.21 | -26.826 | -21.02 | -6.5 | -1.3 | -23.1 | -55.0 | -58.6 | -52.8 | 31.9 | Y |
| -6.4 | -23.87 | -27.326 | -20.64 | -6.4 | -1.2 | -22.9 | -55.6 | -59.1 | -52.4 | 32.7 | Y |
| -6.3 | -24.59 | -27.758 | -20.32 | -6.3 | -1.0 | -22.8 | -56.3 | -59.5 | -52.1 | 33.6 | Y |
| -6.2 | -25.38 | -28.103 | -20.05 | -6.2 | -0.8 | -22.6 | -57.1 | -59.9 | -51.8 | 34.5 | Y |
| -6.1 | -26.23 | -28.347 | -19.84 | -6.1 | -0.6 | -22.4 | -58.0 | -60.1 | -51.6 | 35.6 | Y |
| -6.0 | -27.16 | -28.481 | -19.67 | -6.0 | -0.5 | -22.2 | -58.9 | -60.2 | -51.4 | 36.7 | Y |


| -5.9 | -28.17 | -28.511 | -19.56 | -5.9 | -0.3 | -22.1 | -59.9 | -60.3 | -51.3 | 37.9 | Y |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -5.8 | -29.28 | -28.451 | -19.51 | -5.8 | -0.1 | -21.9 | -61.0 | -60.2 | -51.3 | 39.2 | Y |
| -5.7 | -30.47 | -28.323 | -19.51 | -5.7 | 0.1 | -21.7 | -62.2 | -60.1 | -51.3 | 40.6 | Y |
| -5.6 | -31.76 | -28.152 | -19.57 | -5.6 | 0.3 | -21.5 | -63.5 | -59.9 | -51.3 | 42.0 | Y |
| -5.5 | -33.15 | -27.962 | -19.69 | -5.5 | 0.5 | -21.3 | -64.9 | -59.7 | -51.4 | 43.6 | Y |
| -5.4 | -34.62 | -27.774 | -19.87 | -5.4 | 0.7 | -21.1 | -66.4 | -59.5 | -51.6 | 45.3 | Y |
| -5.3 | -36.15 | -27.608 | -20.13 | -5.3 | 0.9 | -20.9 | -67.9 | -59.4 | -51.9 | 47.0 | Y |
| -5.2 | -37.68 | -27.477 | -20.45 | -5.2 | 1.1 | -20.7 | -69.4 | -59.2 | -52.2 | 48.8 | Y |
| -5.1 | -39.12 | -27.392 | -20.85 | -5.1 | 1.3 | -20.5 | -70.9 | -59.2 | -52.6 | 50.4 | Y |
| -5.0 | -40.31 | -27.363 | -21.34 | -5.0 | 1.5 | -20.3 | -72.1 | -59.1 | -53.1 | 51.8 | Y |
| -4.9 | -41.07 | -27.394 | -21.93 | -4.9 | 1.7 | -20.0 | -72.8 | -59.2 | -53.7 | 52.8 | Y |
| -4.8 | -41.22 | -27.489 | -22.62 | -4.8 | 2.0 | -19.8 | -73.0 | -59.2 | -54.4 | 53.2 | Y |
| -4.7 | -40.71 | -27.649 | -23.42 | -4.7 | 2.2 | -19.6 | -72.5 | -59.4 | -55.2 | 52.9 | Y |
| -4.6 | -39.62 | -27.868 | -24.36 | -4.6 | 2.4 | -19.4 | -71.4 | -59.6 | -56.1 | 52.0 | Y |
| -4.5 | -38.13 | -28.137 | -25.42 | -4.5 | 2.7 | -19.1 | -69.9 | -59.9 | -57.2 | 50.8 | Y |
| -4.4 | -36.41 | -28.429 | -26.58 | -4.4 | 2.9 | -18.9 | -68.2 | -60.2 | -58.3 | 49.3 | Y |
| -4.3 | -34.61 | -28.707 | -27.73 | -4.3 | 3.2 | -18.6 | -66.4 | -60.5 | -59.5 | 47.8 | Y |
| -4.2 | -32.83 | -28.912 | -28.64 | -4.2 | 3.4 | -18.4 | -64.6 | -60.7 | -60.4 | 46.2 | Y |
| -4.1 | -31.11 | -28.967 | -28.91 | -4.1 | 3.7 | -18.1 | -62.9 | -60.7 | -60.7 | 44.8 | Y |
| -4.0 | -29.47 | -28.798 | -28.31 | -4.0 | 3.9 | -17.8 | -61.2 | -60.6 | -60.1 | 43.4 | Y |
| -3.9 | -27.94 | -28.362 | -27.04 | -3.9 | 4.2 | -17.6 | -59.7 | -60.1 | -58.8 | 42.1 | Y |
| -3.8 | -26.5 | -27.67 | -25.49 | -3.8 | 4.5 | -17.3 | -58.3 | -59.4 | -57.2 | 41.0 | Y |
| -3.7 | -25.16 | -26.783 | -23.91 | -3.7 | 4.8 | -17.0 | -56.9 | -58.5 | -55.7 | 39.9 | Y |
| -3.6 | -23.91 | -25.775 | -22.42 | -3.6 | 5.1 | -16.7 | -55.7 | -57.5 | -54.2 | 39.0 | Y |
| -3.5 | -22.75 | -24.717 | -21.06 | -3.5 | 5.4 | -16.4 | -54.5 | -56.5 | -52.8 | 38.1 | Y |
| -3.4 | -21.66 | -23.657 | -19.81 | -3.4 | 5.7 | -16.1 | -53.4 | -55.4 | -51.6 | 37.4 | Y |
| -3.3 | -20.65 | -22.624 | -18.67 | -3.3 | 6.0 | -15.7 | -52.4 | -54.4 | -50.4 | 36.7 | Y |
| -3.2 | -19.71 | -21.637 | -17.62 | -3.2 | 6.4 | -15.4 | -51.5 | -53.4 | -49.4 | 36.1 | Y |
| -3.1 | -18.83 | -20.703 | -16.67 | -3.1 | 6.7 | -15.1 | -50.6 | -52.5 | -48.4 | 35.5 | Y |
| -3.0 | -18.01 | -19.824 | -15.78 | -3.0 | 7.1 | -14.7 | -49.8 | -51.6 | -47.5 | 35.1 | Y |
| -2.9 | -17.24 | -19.002 | -14.97 | -2.9 | 7.4 | -14.3 | -49.0 | -50.8 | -46.7 | 34.7 | Y |
| -2.8 | -16.53 | -18.233 | -14.21 | -2.8 | 7.8 | -14.0 | -48.3 | -50.0 | -46.0 | 34.3 | Y |
| -2.7 | -15.86 | -17.517 | -13.5 | -2.7 | 8.2 | -13.6 | -47.6 | -49.3 | -45.3 | 34.1 | Y |
| -2.6 | -15.23 | -16.85 | -12.85 | -2.6 | 8.6 | -13.2 | -47.0 | -48.6 | -44.6 | 33.8 | Y |
| -2.5 | -14.65 | -16.229 | -12.23 | -2.5 | 9.1 | -12.7 | -46.4 | -48.0 | -44.0 | 33.7 | Y |
| -2.4 | -14.1 | -15.652 | -11.66 | -2.4 | 9.5 | -12.3 | -45.9 | -47.4 | -43.4 | 33.6 | Y |
| -2.3 | -13.58 | -15.117 | -11.13 | -2.3 | 10.0 | -11.8 | -45.3 | -46.9 | -42.9 | 33.5 | Y |
| -2.2 | -13.1 | -14.622 | -10.64 | -2.2 | 10.4 | -11.3 | -44.9 | -46.4 | -42.4 | 33.5 | Y |


| -2.1 | -12.64 | -14.163 | -10.18 | -2.1 | 10.9 | -10.8 | -44.4 | -45.9 | -41.9 | 33.6 | Y |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| -2.0 | -12.22 | -13.74 | -9.747 | -2.0 | 11.5 | -10.3 | -44.0 | -45.5 | -41.5 | 33.7 | Y |
| -1.9 | -11.81 | -13.35 | -9.349 | -1.9 | 12.0 | -9.8 | -43.6 | -45.1 | -41.1 | 33.8 | Y |
| -1.8 | -11.43 | -12.992 | -8.979 | -1.8 | 12.6 | -9.2 | -43.2 | -44.8 | -40.7 | 34.0 | Y |
| -1.7 | -11.08 | -12.664 | -8.639 | -1.7 |  |  | -42.8 | -44.4 | -40.4 |  | Y |
| -1.6 | -10.74 | -12.365 | -8.324 | -1.6 |  |  | -42.5 | -44.1 | -40.1 |  | Y |
| -1.5 | -10.42 | -12.093 | -8.036 | -1.5 |  |  | -42.2 | -43.9 | -39.8 |  | Y |
| -1.4 | -10.12 | -11.846 | -7.773 | -1.4 |  |  | -41.9 | -43.6 | -39.5 |  | Y |
| -1.3 | -9.835 | -11.624 | -7.533 | -1.3 |  |  | -41.6 | -43.4 | -39.3 |  | Y |
| -1.2 | -9.568 | -11.424 | -7.316 | -1.2 |  |  | -41.3 | -43.2 | -39.1 |  | Y |
| -1.1 | -9.318 | -11.244 | -7.12 | -1.1 |  |  | -41.1 | -43.0 | -38.9 |  | Y |
| -1.0 | -9.084 | -11.084 | -6.946 | -1.0 |  |  | -40.8 | -42.8 | -38.7 |  | Y |
| -0.9 | -8.866 | -10.941 | -6.792 | -0.9 |  |  | -40.6 | -42.7 | -38.6 |  | Y |
| -0.8 | -8.663 | -10.814 | -6.657 | -0.8 |  |  | -40.4 | -42.6 | -38.4 |  | Y |
| -0.7 | -8.477 | -10.7 | -6.541 | -0.7 |  |  | -40.2 | -42.5 | -38.3 |  | Y |
| -0.6 | -8.307 | -10.599 | -6.443 | -0.6 |  |  | -40.1 | -42.4 | -38.2 |  | Y |
| -0.5 | -8.152 | -10.507 | -6.362 | -0.5 |  |  | -39.9 | -42.3 | -38.1 |  | Y |
| -0.4 | -8.015 | -10.425 | -6.297 | -0.4 |  |  | -39.8 | -42.2 | -38.1 |  | Y |
| -0.3 | -7.894 | -10.35 | -6.249 | -0.3 |  |  | -39.7 | -42.1 | -38.0 |  | Y |
| -0.2 | -7.791 | -10.28 | -6.217 | -0.2 |  |  | -39.6 | -42.0 | -38.0 |  | Y |
| -0.1 | -7.705 | -10.215 | -6.201 | -0.1 |  |  | -39.5 | -42.0 | -38.0 |  | Y |
| 0.0 | -7.637 | -10.153 | -6.199 | 0.0 |  |  | -39.4 | -41.9 | -38.0 |  | Y |
| 0.1 | -7.588 | -10.095 | -6.213 | 0.1 |  |  | -39.3 | -41.9 | -38.0 |  | Y |
| 0.2 | -7.557 | -10.038 | -6.242 | 0.2 |  |  | -39.3 | -41.8 | -38.0 |  | Y |
| 0.3 | -7.546 | -9.983 | -6.286 | 0.3 |  |  | -39.3 | -41.7 | -38.0 |  | Y |
| 0.4 | -7.554 | -9.93 | -6.345 | 0.4 |  |  | -39.3 | -41.7 | -38.1 |  | Y |
| 0.5 | -7.582 | -9.879 | -6.42 | 0.5 |  |  | -39.3 | -41.6 | -38.2 |  | Y |
| 0.6 | -7.63 | -9.831 | -6.511 | 0.6 |  |  | -39.4 | -41.6 | -38.3 |  | Y |
| 0.7 | -7.699 | -9.787 | -6.618 | 0.7 |  |  | -39.5 | -41.5 | -38.4 |  | Y |
| 0.8 | -7.789 | -9.748 | -6.742 | 0.8 |  |  | -39.5 | -41.5 | -38.5 |  | Y |
| 0.9 | -7.901 | -9.714 | -6.884 | 0.9 |  |  | -39.7 | -41.5 | -38.6 |  | Y |
| 1.0 | -8.034 | -9.688 | -7.044 | 1.0 |  |  | -39.8 | -41.4 | -38.8 |  | Y |
| 1.1 | -8.19 | -9.67 | -7.223 | 1.1 |  |  | -40.0 | -41.4 | -39.0 |  | Y |
| 1.2 | -8.368 | -9.662 | -7.421 | 1.2 |  |  | -40.1 | -41.4 | -39.2 |  | Y |
| 1.3 | -8.568 | -9.666 | -7.641 | 1.3 |  |  | -40.3 | -41.4 | -39.4 |  | Y |
| 1.4 | -8.792 | -9.682 | -7.882 | 1.4 |  |  | -40.6 | -41.4 | -39.6 |  | Y |
| 1.5 | -9.039 | -9.712 | -8.145 | 1.5 |  |  | -40.8 | -41.5 | -39.9 |  | Y |
| 1.6 | -9.31 | -9.758 | -8.433 | 1.6 |  |  | -41.1 | -41.5 | -40.2 |  | Y |


| 1.7 | -9.605 | -9.821 | -8.744 | 1.7 |  |  | -41.4 | -41.6 | -40.5 |  | Y |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.8 | -9.923 | -9.901 | -9.082 | 1.8 | 12.6 | -9.2 | -41.7 | -41.7 | -40.8 | 32.5 | Y |
| 1.9 | -10.27 | -10 | -9.446 | 1.9 | 12.0 | -9.8 | -42.0 | -41.8 | -41.2 | 32.3 | Y |
| 2.0 | -10.63 | -10.119 | -9.839 | 2.0 | 11.5 | -10.3 | -42.4 | -41.9 | -41.6 | 32.1 | Y |
| 2.1 | -11.03 | -10.259 | -10.26 | 2.1 | 10.9 | -10.8 | -42.8 | -42.0 | -42.0 | 31.9 | Y |
| 2.2 | -11.44 | -10.42 | -10.71 | 2.2 | 10.4 | -11.3 | -43.2 | -42.2 | -42.5 | 31.9 | Y |
| 2.3 | -11.88 | -10.604 | -11.2 | 2.3 | 10.0 | -11.8 | -43.6 | -42.4 | -43.0 | 31.8 | Y |
| 2.4 | -12.35 | -10.81 | -11.72 | 2.4 | 9.5 | -12.3 | -44.1 | -42.6 | -43.5 | 31.8 | Y |
| 2.5 | -12.84 | -11.04 | -12.28 | 2.5 | 9.1 | -12.7 | -44.6 | -42.8 | -44.0 | 31.9 | Y |
| 2.6 | -13.36 | -11.295 | -12.87 | 2.6 | 8.6 | -13.2 | -45.1 | -43.1 | -44.6 | 32.0 | Y |
| 2.7 | -13.9 | -11.574 | -13.51 | 2.7 | 8.2 | -13.6 | -45.7 | -43.3 | -45.3 | 32.1 | Y |
| 2.8 | -14.47 | -11.879 | -14.18 | 2.8 | 7.8 | -14.0 | -46.2 | -43.6 | -45.9 | 32.3 | Y |
| 2.9 | -15.06 | -12.209 | -14.91 | 2.9 | 7.4 | -14.3 | -46.8 | -44.0 | -46.7 | 32.5 | Y |
| 3.0 | -15.67 | -12.565 | -15.68 | 3.0 | 7.1 | -14.7 | -47.4 | -44.3 | -47.4 | 32.7 | Y |
| 3.1 | -16.3 | -12.948 | -16.5 | 3.1 | 6.7 | -15.1 | -48.1 | -44.7 | -48.3 | 33.0 | Y |
| 3.2 | -16.95 | -13.358 | -17.37 | 3.2 | 6.4 | -15.4 | -48.7 | -45.1 | -49.1 | 33.3 | Y |
| 3.3 | -17.62 | -13.795 | -18.3 | 3.3 | 6.0 | -15.7 | -49.4 | -45.6 | -50.1 | 33.6 | Y |
| 3.4 | -18.29 | -14.26 | -19.27 | 3.4 | 5.7 | -16.1 | -50.1 | -46.0 | -51.0 | 34.0 | Y |
| 3.5 | -18.98 | -14.754 | -20.28 | 3.5 | 5.4 | -16.4 | -50.7 | -46.5 | -52.0 | 34.4 | Y |
| 3.6 | -19.66 | -15.276 | -21.32 | 3.6 | 5.1 | -16.7 | -51.4 | -47.0 | -53.1 | 34.7 | Y |
| 3.7 | -20.33 | -15.827 | -22.36 | 3.7 | 4.8 | -17.0 | -52.1 | -47.6 | -54.1 | 35.1 | Y |
| 3.8 | -20.99 | -16.406 | -23.34 | 3.8 | 4.5 | -17.3 | -52.7 | -48.2 | -55.1 | 35.5 | Y |
| 3.9 | -21.62 | -17.014 | -24.19 | 3.9 | 4.2 | -17.6 | -53.4 | -48.8 | -55.9 | 35.8 | Y |
| 4.0 | -22.22 | -17.648 | -24.83 | 4.0 | 3.9 | -17.8 | -54.0 | -49.4 | -56.6 | 36.1 | Y |
| 4.1 | -22.78 | -18.308 | -25.2 | 4.1 | 3.7 | -18.1 | -54.5 | -50.1 | -57.0 | 36.4 | Y |
| 4.2 | -23.28 | -18.99 | -25.28 | 4.2 | 3.4 | -18.4 | -55.0 | -50.8 | -57.0 | 36.7 | Y |
| 4.3 | -23.74 | -19.689 | -25.12 | 4.3 | 3.2 | -18.6 | -55.5 | -51.4 | -56.9 | 36.9 | Y |
| 4.4 | -24.14 | -20.399 | -24.8 | 4.4 | 2.9 | -18.9 | -55.9 | -52.2 | -56.6 | 37.0 | Y |
| 4.5 | -24.49 | -21.109 | -24.4 | 4.5 | 2.7 | -19.1 | -56.2 | -52.9 | -56.2 | 37.1 | Y |
| 4.6 | -24.79 | -21.805 | -23.97 | 4.6 | 2.4 | -19.4 | -56.5 | -53.6 | -55.7 | 37.2 | Y |
| 4.7 | -25.04 | -22.471 | -23.57 | 4.7 | 2.2 | -19.6 | -56.8 | -54.2 | -55.3 | 37.2 | Y |
| 4.8 | -25.27 | -23.085 | -23.22 | 4.8 | 2.0 | -19.8 | -57.0 | -54.8 | -55.0 | 37.2 | Y |
| 4.9 | -25.46 | -23.627 | -22.93 | 4.9 | 1.7 | -20.0 | -57.2 | -55.4 | -54.7 | 37.2 | Y |
| 5.0 | -25.63 | -24.077 | -22.71 | 5.0 | 1.5 | -20.3 | -57.4 | -55.8 | -54.5 | 37.1 | Y |
| 5.1 | -25.79 | -24.423 | -22.56 | 5.1 | 1.3 | -20.5 | -57.5 | -56.2 | -54.3 | 37.1 | Y |
| 5.2 | -25.92 | -24.659 | -22.48 | 5.2 | 1.1 | -20.7 | -57.7 | -56.4 | -54.2 | 37.0 | Y |
| 5.3 | -26.05 | -24.794 | -22.48 | 5.3 | 0.9 | -20.9 | -57.8 | -56.6 | -54.2 | 36.9 | Y |
| 5.4 | -26.15 | -24.842 | -22.56 | 5.4 | 0.7 | -21.1 | -57.9 | -56.6 | -54.3 | 36.8 | Y |


| 5.5 | -26.24 | -24.824 | -22.71 | 5.5 | 0.5 | -21.3 | -58.0 | -56.6 | -54.5 | 36.7 | Y |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5.6 | -26.31 | -24.762 | -22.94 | 5.6 | 0.3 | -21.5 | -58.1 | -56.5 | -54.7 | 36.6 | Y |
| 5.7 | -26.35 | -24.676 | -23.26 | 5.7 | 0.1 | -21.7 | -58.1 | -56.4 | -55.0 | 36.4 | Y |
| 5.8 | -26.36 | -24.582 | -23.65 | 5.8 | -0.1 | -21.9 | -58.1 | -56.3 | -55.4 | 36.2 | Y |
| 5.9 | -26.33 | -24.493 | -24.13 | 5.9 | -0.3 | -22.1 | -58.1 | -56.3 | -55.9 | 36.0 | Y |
| 6.0 | -26.27 | -24.417 | -24.69 | 6.0 | -0.5 | -22.2 | -58.0 | -56.2 | -56.5 | 35.8 | Y |
| 6.1 | -26.18 | -24.359 | -25.33 | 6.1 | -0.6 | -22.4 | -57.9 | -56.1 | -57.1 | 35.5 | Y |
| 6.2 | -26.05 | -24.324 | -26.05 | 6.2 | -0.8 | -22.6 | -57.8 | -56.1 | -57.8 | 35.2 | Y |
| 6.3 | -25.89 | -24.311 | -26.82 | 6.3 | -1.0 | -22.8 | -57.7 | -56.1 | -58.6 | 34.9 | Y |
| 6.4 | -25.71 | -24.32 | -27.6 | 6.4 | -1.2 | -22.9 | -57.5 | -56.1 | -59.4 | 34.5 | Y |
| 6.5 | -25.5 | -24.349 | -28.34 | 6.5 | -1.3 | -23.1 | -57.3 | -56.1 | -60.1 | 34.2 | Y |
| 6.6 | -25.28 | -24.396 | -28.93 | 6.6 | -1.5 | -23.3 | -57.0 | -56.2 | -60.7 | 33.8 | Y |
| 6.7 | -25.05 | -24.457 | -29.25 | 6.7 | -1.7 | -23.4 | -56.8 | -56.2 | -61.0 | 33.4 | Y |
| 6.8 | -24.81 | -24.529 | -29.25 | 6.8 | -1.8 | -23.6 | -56.6 | -56.3 | -61.0 | 33.0 | Y |
| 6.9 | -24.57 | -24.61 | -28.91 | 6.9 | -2.0 | -23.8 | -56.3 | -56.4 | -60.7 | 32.6 | Y |
| 7.0 | -24.34 | -24.696 | -28.31 | 7.0 | -2.1 | -23.9 | -56.1 | -56.5 | -60.1 | 32.2 | Y |
| 7.1 | -24.11 | -24.785 | -27.58 | 7.1 | -2.0 | -23.8 | -55.9 | -56.5 | -59.3 | 32.1 | Y |
| 7.2 | -23.89 | -24.876 | -26.79 | 7.2 | -2.0 | -23.8 | -55.7 | -56.6 | -58.6 | 31.9 | Y |
| 7.3 | -23.68 | -24.97 | -26.02 | 7.3 | -2.0 | -23.8 | -55.4 | -56.7 | -57.8 | 31.7 | Y |
| 7.4 | -23.49 | -25.066 | -25.28 | 7.4 | -2.0 | -23.8 | -55.3 | -56.8 | -57.0 | 31.5 | Y |
| 7.5 | -23.31 | -25.167 | -24.61 | 7.5 | -2.0 | -23.8 | -55.1 | -56.9 | -56.4 | 31.3 | Y |
| 7.6 | -23.15 | -25.275 | -24 | 7.6 | -2.0 | -23.8 | -54.9 | -57.0 | -55.8 | 31.1 | Y |
| 7.7 | -23 | -25.394 | -23.46 | 7.7 | -2.0 | -23.8 | -54.8 | -57.2 | -55.2 | 31.0 | Y |
| 7.8 | -22.86 | -25.526 | -22.97 | 7.8 | -2.0 | -23.8 | -54.6 | -57.3 | -54.7 | 30.8 | Y |
| 7.9 | -22.74 | -25.676 | -22.54 | 7.9 | -2.0 | -23.8 | -54.5 | -57.4 | -54.3 | 30.7 | Y |
| 8.0 | -22.64 | -25.846 | -22.16 | 8.0 | -2.0 | -23.8 | -54.4 | -57.6 | -53.9 | 30.6 | Y |
| 8.1 | -22.55 | -26.039 | -21.83 | 8.1 | -2.0 | -23.8 | -54.3 | -57.8 | -53.6 | 30.5 | Y |
| 8.2 | -22.48 | -26.257 | -21.54 | 8.2 | -2.0 | -23.8 | -54.2 | -58.0 | -53.3 | 30.5 | Y |
| 8.3 | -22.42 | -26.502 | -21.29 | 8.3 | -2.0 | -23.8 | -54.2 | -58.3 | -53.1 | 30.4 | Y |
| 8.4 | -22.38 | -26.774 | -21.08 | 8.4 | -2.0 | -23.8 | -54.1 | -58.5 | -52.8 | 30.4 | Y |
| 8.5 | -22.35 | -27.07 | -20.9 | 8.5 | -2.0 | -23.8 | -54.1 | -58.8 | -52.7 | 30.3 | Y |
| 8.6 | -22.33 | -27.389 | -20.75 | 8.6 | -2.0 | -23.8 | -54.1 | -59.1 | -52.5 | 30.3 | Y |
| 8.7 | -22.33 | -27.725 | -20.63 | 8.7 | -2.0 | -23.8 | -54.1 | -59.5 | -52.4 | 30.3 | Y |
| 8.8 | -22.35 | -28.071 | -20.55 | 8.8 | -2.0 | -23.8 | -54.1 | -59.8 | -52.3 | 30.3 | Y |
| 8.9 | -22.37 | -28.418 | -20.49 | 8.9 | -2.0 | -23.8 | -54.1 | -60.2 | -52.3 | 30.4 | Y |
| 9.0 | -22.42 | -28.753 | -20.47 | 9.0 | -2.0 | -23.8 | -54.2 | -60.5 | -52.2 | 30.4 | Y |
| 9.1 | -22.48 | -29.064 | -20.48 | 9.1 | -2.0 | -23.8 | -54.2 | -60.8 | -52.2 | 30.5 | Y |
| 9.2 | -22.56 | -29.335 | -20.53 | 9.2 | -2.0 | -23.8 | -54.3 | -61.1 | -52.3 | 30.5 | Y |

## 5. Pointing Accuracy

The VMES V3 terminal will utilize a motion stabilized tracking antenna and a direct sequence spread spectrum (DSSS) burst modem manufactured by ViaSat to access the satellite. The VMES terminal uses a common spreading code and a random access method called code reuse multiple access ("CRMA") to access the satellite. CRMA is closely analogous to the more generally understood code division multiple access (CDMA) multiple access method, but differs in that all terminals use a common spreading code rather than a number of individual codes for each transmitter. Individual bursts are distinguished by time difference of arrival. The use of this spreading technique allows the RF spectral density for each VMES to be significantly lower that typical TDMA systems operating at Ku-band.

The antenna system utilizes a conical scanning function and rate gyros to stabilize the antenna and keep it pointed properly at the desired satellite. The conscan is currently set to worst case $0.6^{\circ}$ from boresight. The mean dynamic pointing error for the vehicle accelerations expected during testing operation is expected to be $0.2^{\circ}$, with a standard deviation of $0.8^{\circ}$. Thus the total expected mean pointing error for each vehicle while in motion, including both conscan and dynamic error, is $0.8^{\circ}$ with a declared maximum pointing error of $1.5^{\circ}$.

During the small percentage of time when conditions cause the antenna pointing error to exceed the specified maximum pointing error limit of $1.5^{\circ}$, the antenna system will send a message to the modem, and the modem will inhibit transmission until the aggregate conscan plus dynamic pointing error value is back to within $0.8^{\circ}$. The time lag from detection of exceedance of mispointing to time when transmit is inhibited will be less than 100 ms . This error limit of $1.5^{\circ}$ is the declared maximum antenna pointing error as described in §25.226(b)(1)(iv)(A).

As described above, the VMESs in this network use a spread spectrum multiple access technique whereby the individual off-axis EIRP density of each VMES terminal is well below the maximum aggregate network limit. Thus, each antenna individually will not generate harmful levels of interference - even if the antenna was pointed directly at an adjacent satellite. Random pointing errors across this VMES network will not cause objectionable levels of adjacent satellite interference because the antenna on each VMES will be pointing in a different direction with a different error component. There is an extremely low probability that multiple antennas will be mispointed at an adjacent satellite at the same time in such a way that their power results in harmful interference levels. Because the pointing error is random and momentary, each VMES antenna actually has a higher likelihood of being pointed away from the geostationary satellite arc than at an adjacent satellite in the arc.

The following plots show how random pointing error adds up for several cases. In the first plot, Figure 8, a number of different standard deviations of pointing error are plotted: $1.666^{\circ}, 1.0^{\circ}, 0.666^{\circ}, 0.5^{\circ}, 0.333^{\circ}$ and $0.166^{\circ}$. Each plot represents a long term statistical
sampling of $1,000,000$ random errors for the specified standard deviation. The FCC mask is shown as adjusted to account for the spreading used by each terminal.

The $\pm 12.8^{\circ}$ of topocentric angle used for theta represent $\pm 10^{\circ}$ of geostationary satellite arc. The reference dBi plot on the charts is representative of the average of the antenna pattern for the topocentric angles to the geostationary arc from various locations across CONUS.

The second plot, Figure 9, shows the same reference dBi plot representing the aggregate population of terminals with no pointing error. A single VMES with $2^{\circ}$ of pointing error is shown. It can be seen that even when the VMES is pointed directly at an adjacent satellite, the power density is well below the FCC off-axis EIRP density mask. In this case the VMES's input power density has been reduced by an additional 11.8 dB from the network aggregate - equivalent to a population of 15 co-frequency VMESs transmitting simultaneously.


Figure 8- Aggregate pointing error for several standard deviations


Figure 9- Impact of a single VMES with $2^{\circ}$ of pointing error
Figure 10 shows 15 co-frequency VMESs transmitting simultaneously, each with random error and with conscan active. The aggregate power summation of all 15 VMESs is also plotted along with the reference dBi and adjusted FCC mask.


Figure 10 - Aggregate pointing error for 15 co-frequency VMESs

In summary, the V3 will maintain a deliberate conscan of $0.6^{\circ}$, assumes additional pointing error of $0.2^{\circ}$ for a mean pointing accuracy of $0.8^{\circ}$ (within which it will resume transmission after automated shut-down) and a declared maximum pointing error of $1.5^{\circ}$ (beyond which it will automatically cease transmissions within 100ms). Even considering worst case excursions and additional conservative assumptions, the analysis shows that the VMES system will not cause adjacent satellite interference due to the very low RF power density of the spread spectrum return link.

## 6. Summary of Technical Parameters

The return link channel will support data rates for of $32 \mathrm{kbit} / \mathrm{s}, 64 \mathrm{kbit} / \mathrm{s}, 128 \mathrm{kbit} / \mathrm{s}, 256$ $\mathrm{kbit} / \mathrm{s}$, and $512 \mathrm{kbit} / \mathrm{s}$. The forward channel will be operated with data rates of 3-10 Mbits/s aggregate with individual end user rates between 512-2 Mbit/s. A summary of the V3 operating parameters is shown in the tables below:

| Antenna diameter | 37 cm |
| :--- | :--- |
| Type of Antenna | Parabolic rear-fed |
| Peak Power (SSPA) | 3 watts |
| Transmit Bandwidth | $18,36 \mathrm{MHz}$ |
| Transmit Gain | 33 dBi at 14 GHz |
| EIRP | 38 dBW |
| Transmit Data Rate | 32 kbps to 512 Mbps |
| Transmit Polarization | Horizontal or Vertical |
| Transmit Max PSD | $<10 \mathrm{dBW} / 4 \mathrm{kHz}$ |
| Transmit Azimuth, <br> Elevation Beamwidth | 3.5 degrees |
| Receive G/T | $10 \mathrm{~dB} / \mathrm{K}$ minimum |
| Receive Bandwidth | 500 MHz |
| Receive Polarization | Dual Vertical and Horizontal |

V3 VMES Terminal Parameters

| Azimuth | continuous coverage over full <br> $360^{\circ}$ |
| :--- | :--- |
| Elevation | 10 to $80^{\circ}$ antenna elevation |
| Position accuracy | Static pointing error $0.6^{\circ}$ RMS <br> (AZ); $0.8^{\circ}$ RMS (AZ) in-motion, <br> Declared Maximum Pointing <br> Error $1.5^{\circ}$ ) |
| Dynamic Tracking <br> capability | Roll: $+/-25^{\circ}$ at 8 second period <br> Pitch: $+/-15^{\circ}$ at 5 second period <br> Yaw: $+/-8^{\circ}$ at 50 second period <br> Azimuth Turn rate: $12^{\circ} / \mathrm{s}$ and <br> $15^{\circ} / \mathrm{s}^{2}$ acceleration |

Antenna Control Parameters

| Power a feed Flange | 3 | Watts |
| :--- | :---: | :--- |
| Channel; Bandwidth | 36 | MHz |
| RF Power Density at Flange | -34.8 | $\mathrm{dBW} / 4, \mathrm{kHz}$ |
| Maximum Horizon EIRP Density $\left(10^{\circ}\right.$ Elevation <br> Angle $)$ | -3.79 | $\mathrm{dBW} / \mathrm{MHz}$ |
| Maximum Horizon EIRP | 11.77 | dBW |
| Maximum Number Simultaneous Users N | 13 |  |

Uplink Transmission Parameters - $\mathbf{3 6} \mathbf{~ M H z}$ Channel

| Power a feed Flange | 3 | Watts |
| :--- | :---: | :--- |
| Channel; Bandwidth | 18 | MHz |
| RF Power Density at Flange | -31.8 | $\mathrm{dBW} / 4 \mathrm{kHz}$ |
| Maximum Horizon EIRP Density $\left(10^{\circ}\right.$ <br> Elevation Angle) | -0.78 | $\mathrm{dBW} / \mathrm{MHz}$ |
| Maximum Horizon EIRP | 11.77 | dBW |
| Maximum Number Simultaneous Users N | 6 |  |

Uplink Transmission Parameters - 18 MHz Channel

## 7. FCC §25.226 Compliance Matrix for the V3 Terminal

|  | FCC Part 25 Vehicle Mounted Earth Stations (VMES) <br> Rules for Ku-Band | Complies | Comments |
| :--- | :--- | :--- | :--- |
|  | § 25.226 Blanket licensing provisions for domestic, U.S. <br> Vehicle-Mounted Earth Stations (VMESs) receiving in the <br> 10.95-11.2 GHz (space-to-Earth), 11.45-11.7 GHz (space- <br> to-Earth), and 11.7-12.2 GHz (space-to-Earth) frequency <br> bands and transmitting in the 14.0-14.5 GHz (Earth-to- <br> space) frequency band, operating with Geostationary <br> Satellites in the Fixed-Satellite Service. |  |  |
| $\S 25.226$ | (a) The following ongoing requirements govern all VMES <br> licensees and operations in the 10.95-11.2 GHz (space-to- <br> Earth), 11.45-11.7 GHz (space-to-Earth)11.7-12.2 GHz <br> (space-to-Earth) and 14.0-14.5 GHz (Earth-to-space) <br> frequency bands receiving from and transmitting to <br> geostationary orbit satellites in the fixed-satellite service. <br> VMES licensees shall comply with the requirements in <br> either paragraph (a)(1), (a)(2) or (a)(3) of this section and <br> all of the requirements set forth in paragraphs (a)(4) <br> through (a)(9) and paragraphs (c), (d), and (e) of this <br> section. Paragraph (b) of this section identifies items that <br> shall be included in the application for VMES operations to <br> demonstrate that these ongoing requirements will be met. | Complies |  |
| $\S 25.226(a)$ | Complies with <br> (a)(1) and <br> remaining <br> provisions |  |  |
| (1) The following requirements shall apply to a VMES that <br> uses transmitters with off-axis EIRP spectral-densities <br> lower than or equal to the levels in paragraph (a)(1)(i) of <br> this section. A VMES, or VMES system, operating under <br> this section shall provide a detailed demonstration as <br> described in paragraph (b)(1) of this section. The VMES <br> transmitter also shall comply with the antenna pointing and <br> cessation of emission requirements in paragraphs (a)(1)(ii) <br> and (a)(1)(iii) of this section. |  |  |  |
| 25.226(a)(1) |  |  |  |


| § 25.226(a)(1)(i) | (i) A VMES system shall not exceed the off-axis EIRP spectral-density limits and conditions defined in paragraphs (a)(1)(i)(A) through (D) of this section. | Complies | Section 4 |
| :---: | :---: | :---: | :---: |
| § 25.226(a)(1)(i)(A) | (A) The off-axis EIRP spectral-density emitted from the VMES, in the plane of the geostationary satellite orbit (GSO) as it appears at the particular earth station location, shall not exceed the following values: | Complies | Section 4 |
|  | $\begin{aligned} & 15-10 \log (\mathrm{~N})-25 \operatorname{logTH} \mathrm{dBW} / 4 \mathrm{kHz} \text { for } 1.5 \mathrm{DEG}<=\mathrm{TH}<= \\ & 7 \mathrm{DEG} \end{aligned}$ |  |  |
|  | -6-10log( N ) dBW/4kHz for 7DEG < TH < = 9.2DEG |  |  |
|  | $18-10 \log (\mathrm{~N})-25 \log \mathrm{TH} \mathrm{dBW} / 4 \mathrm{kHz}$ for $9.2 \mathrm{DEG}<\mathrm{TH}<=$ 48DEG |  |  |
|  | -24-10log(N) dBW/4kHz for 48DEG < TH <= 85DEG |  |  |
|  | $-14-10 \log (\mathrm{~N}) \mathrm{dBW} / 4 \mathrm{kHz}$ for 85DEG < TH <= 180DEG |  |  |
|  | where theta (TH) is the angle in degrees from the line connecting the focal point of the antenna to the orbital location of the target satellite, the plane of the GSO is determined by the focal point of the antenna and the line tangent to the arc of the GSO at the orbital location of the target satellite. For VMES networks using frequency division multiple access (FDMA) or time division multiple access (TDMA) techniques, N is equal to one. For VMES networks using multiple co-frequency transmitters that have the same EIRP, N is the maximum expected number of co-frequency simultaneously transmitting VMES earth stations in the same satellite receiving beam. For the purpose of this section, the peak EIRP of an individual sidelobe shall not exceed the envelope defined above for TH between 1.5DEG and 7.0DEG. For TH greater than 7.0DEG, the envelope shall be exceeded by no more than $10 \%$ of the sidelobes, provided no individual sidelobe exceeds the envelope given above by more than 3 dB . |  |  |
| § 25.226(a)(1)(i)(B) | (B) In all directions other than along the GSO, the off-axis EIRP spectral-density for co-polarized signals emitted from the VMES shall not exceed the following values: | Complies | Section 4 |


|  | $18-10 \log (\mathrm{~N})-25 \operatorname{logTH} \mathrm{dBW} / 4 \mathrm{kHz}$ for 3.0DEG <= TH <= 48DEG |  |  |
| :---: | :---: | :---: | :---: |
|  | $-24-10 \log (\mathrm{~N}) \mathrm{dBW} / 4 \mathrm{kHz}$ for 48DEG $<\mathrm{TH}<=85 \mathrm{DEG}$ |  |  |
|  | $-14-10 \log (\mathrm{~N}) \mathrm{dBW} / 4 \mathrm{kHz}$ for 85DEG < TH <= 180DEG |  |  |
|  | where TH and N are defined in paragraph (a)(1)(i)(A) of this section. This off-axis EIRP spectral-density applies in any plane that includes the line connecting the focal point of the antenna to the orbital location of the target satellite with the exception of the plane of the GSO as defined in paragraph (a)(1)(i)(A) of this section. For the purpose of this subsection, the envelope shall be exceeded by no more than $10 \%$ of the sidelobes provided no individual sidelobe exceeds the gain envelope given above by more than 6 dB . The region of the main reflector spillover energy is to be interpreted as a single lobe and shall not exceed the envelope by more than 6 dB . |  |  |
| § 25.226(a)(1)(i)(C) | (C) In all directions, the off-axis EIRP spectral-density for cross-polarized signals emitted from the VMES shall not exceed the following values: | Complies | Section 4 |
|  | $\begin{aligned} & 5-10 \log (\mathrm{~N})-25 \operatorname{logTH} \mathrm{dBW} / 4 \mathrm{kHz} \text { for } 1.8 \mathrm{DEG}<=\mathrm{TH}<= \\ & 7.0 \mathrm{DEG} \end{aligned}$ |  |  |
|  | -16-10log( N ) dBW/4kHz for 7.0DEG < TH < = 9.2DEG |  |  |
|  | where TH and N are defined as set forth in paragraph (a)(1)(i)(A) of this section. This EIRP spectral-density applies in any plane that includes the line connecting the focal point of the antenna to the target satellite. |  |  |
| § 25.226(a)(1)(i)(D) | (D) For non-circular VMES antennas, the major axis of the antenna shall be aligned with the tangent to the arc of the GSO at the orbital location of the target satellite, to the extent required to meet the specified off-axis EIRP spectraldensity criteria. |  |  |
| § 25.226(a)(1)(ii) | (ii) Each VMES transmitter shall meet one of the following antenna pointing requirements: |  |  |


|  | (A) Each VMES transmitter shall maintain a pointing error <br> of less than or equal to 0.2 between the orbital location of <br> the target satellite and the axis of the main lobe of the <br> VMES antenna, or | NA |  |
| :--- | :--- | :--- | :--- |
| 25.226(a)(1)(ii)(A) | (B) Each VMES transmitter shall declare a maximum <br> antenna pointing error that may be greater than 0.2 <br> provided that the VMES does not exceed the off-axis EIRP <br> spectral-density limits in paragraph (a)(1)(i) of this section, <br> taking into account the antenna pointing error. | Complies | Section 5 |


| § 25.226(a)(2)(ii) | (ii) If a good faith agreement cannot be reached between the target satellite operator and the operator of a future satellite that is located within 6 degrees longitude of the target satellite, the VMES operator shall accept the power-density levels that would accommodate that adjacent satellite. |  |  |
| :---: | :---: | :---: | :---: |
| § 25.226(a)(2)(iii) | (iii) The VMES shall operate in accordance with the offaxis EIRP spectral-densities that the VMES supplied to the target satellite operator in order to obtain the certifications listed in paragraph (b)(2) of this section. The VMES shall automatically cease emissions within 100 milliseconds if the VMES transmitter exceeds the off-axis EIRP spectral-densities supplied to the target satellite operator. |  |  |
| § 25.226(a)(3) | (3) The following requirements shall apply to a VMES system that uses variable power-density control of individual simultaneously transmitting co-frequency VMES earth stations in the same satellite receiving beam. A VMES system operating under this subsection shall file certifications and provide a detailed demonstration as described in paragraph (b)(3) of this section. | NA |  |
| § 25.226(a)(3)(i) | (i) Except as defined under paragraph (a)(3)(ii) of this section, the effective aggregate EIRP-density from all terminals shall be at least 1 dB below the off-axis EIRPdensity limits defined in paragraphs (a)(1)(i)(A) through (C) of this section. In this context the term "effective" means that the resultant co-polarized and cross-polarized EIRP-density experienced by any GSO or non-GSO satellite shall not exceed that produced by a single VMES transmitter operating 1 dB below the limits defined in paragraphs (a)(1)(i)(A) through (C) of this section. A VMES system operating under this section shall file certifications and provide a detailed demonstration as described in paragraphs (b)(3)(i) and b)(3)(iii) of this section. |  |  |


| § 25.226(a)(3)(ii) | (ii) The following requirements shall apply to a VMES that uses off-axis EIRP spectral-densities in excess of the levels in paragraph (a)(3)(i) of this section. A VMES system operating under this section shall file certifications and provide a detailed demonstration as described in paragraphs (b)(3)(ii) and (b)(3)(iii) of this section. |  |  |
| :---: | :---: | :---: | :---: |
| § 25.226(a)(3)(ii)(A) | (A) If a good faith agreement cannot be reached between the target satellite operator and the operator of a future satellite that is located within 6 degrees longitude of the target satellite, the VMES shall operate at an EIRP-density defined in paragraph (a)(3)(i) of this section. |  |  |
| § 25.226(a)(3)(ii)(B) | (B) The VMES shall operate in accordance with the offaxis EIRP spectral-densities that the VMES supplied to the target satellite operator in order to obtain the certifications listed in paragraph (b)(3)(ii) of this section. The individual VMES terminals shall automatically cease emissions within 100 milliseconds if the VMES transmitter exceeds the off-axis EIRP spectral-densities supplied to the target satellite operator. The overall system shall be capable of shutting off an individual transmitter or the entire system if the aggregate off-axis EIRP spectraldensities exceed those supplied to the target satellite operator. |  |  |
| § 25.226(a)(3)(ii)(C) | (C) The VMES shall transmit only to the target satellite system(s) referred to in the certifications required by paragraph (b)(3) of this section. |  |  |
| § 25.226(a)(3)(iii) | (iii) The VMES shall file a report one year following license issuance detailing the effective aggregate EIRPdensity levels resulting from its operation, in compliance with paragraph (b)(3)(iii) of this section. |  |  |
| § 25.226(a)(4) | (4) An applicant filing to operate a VMES terminal or system and planning to use a contention protocol shall certify that its contention protocol use will be reasonable. | NA |  |


|  | (5) There shall be a point of contact in the United States, <br> with phone number and address, available 24 hours a day, <br> seven days a week, with authority and ability to cease all <br> emissions from the VMESs. | Complies | Narrative <br> Section II.E.3 |
| :--- | :--- | :--- | :--- |
|  | (6) For each VMES transmitter, a record of the vehicle <br> location (i.e.,latitude/longitude), transmit frequency, <br> channel bandwidth and satellite used shall be time <br> annotated and maintained for a period of not less than one <br> (1) year. Records shall be recorded at time intervals no <br> greater than every five (5) minutes while the VMES is <br> transmitting. The VMES operator shall make this data <br> available upon request to a coordinator, fixed system <br> operator, fixed-satellite system operator, NTIA, or the <br> Commission within 24 hours of the request. | Complies |  |


| § 25.226(b) | (b) Applications for VMES operation in the $14.0-14.5 \mathrm{GHz}$ (Earth-to-space) band to GSO satellites in the fixed-satellite service shall include, in addition to the particulars of operation identified on Form 312, and associated Schedule B, the applicable technical demonstrations in paragraphs (b)(1), (b)(2) or (b)(3) of this section and the documentation identified in paragraphs (b)(4) through (b)(8) of this section. | Complies | Complies with <br> (b)(1) and remaining provisions |
| :---: | :---: | :---: | :---: |
| § 25.226(b)(1) | (1) A VMES applicant proposing to implement a transmitter under paragraph (a)(1) of this section shall demonstrate that the transmitter meets the off-axis EIRP spectral-density limits contained in paragraph (a)(1)(i) of this section. To provide this demonstration, the application shall include the tables described in paragraph (b)(1)(i) of this section or the certification described in paragraph (b)(1)(ii)of this section. The VMES applicant also shall provide the value N described in paragraph (a)(1)(i)(A) of this section. A VMES applicant proposing to implement a transmitter under paragraph (a)(1)(ii)(A) of this section shall provide the certifications identified in paragraph (b)(1)(iii) of this section. A VMES applicant proposing to implement a transmitter under paragraph (a)(1)(ii)(B) of this section shall provide the demonstrations identified in paragraph (b)(1)(iv) of this section. |  |  |
| § 25.226(b)(1)(i) | (i) Any VMES applicant filing an application pursuant to paragraph (a)(1) of this section shall file three tables showing the off-axis EIRP level of the proposed earth station antenna in the direction of the plane of the GSO; the co-polarized EIRP in the elevation plane, that is, the plane perpendicular to the plane of the GSO; and cross polarized EIRP. Each table shall provide the EIRP level at increments of $0.1^{\circ}$ for angles between $0^{\circ}$ and $10^{\circ}$ off-axis, and at increments of $5^{\circ}$ for angles between $10^{\circ}$ and $180^{\circ}$ off-axis. | Complies. | Section 4 |


| § 25.226(b)(1)(i)(A) | (A) For purposes of the off-axis EIRP table in the plane of the GSO, the off-axis angle is the angle in degrees from the line connecting the focal point of the antenna to the orbital location of the target satellite, and the plane of the GSO is determined by the focal point of the antenna and the line tangent to the arc of the GSO at the orbital position of the target satellite. |  |  |
| :---: | :---: | :---: | :---: |
| § 25.226(b)(1)(i)(B) | (B) For purposes of the off-axis co-polarized EIRP table in the elevation plane, the off-axis angle is the angle in degrees from the line connecting the focal point of the antenna to the orbital location of the target satellite, and the elevation plane is defined as the plane perpendicular to the plane of the GSO defined in paragraph(b)(1)(i)(A) of this section. |  |  |
| § 25.226(b)(1)(i)(C) | (C) For purposes of the cross-polarized EIRP table, the offaxis angle is the angle in degrees from the line connecting the focal point of the antenna to the orbital location of the target satellite and the plane of the GSO as defined in paragraph (b)(1)(i)(A) of this section will be used. |  |  |
| § 25.226(b)(1)(ii) | (ii) A VMES applicant shall include a certification, in Schedule B, that the VMES antenna conforms to the gain pattern criteria of § 25.209(a) and (b), that, combined with the maximum input power density calculated from the EIRP density less the antenna gain, which is entered in Schedule B, demonstrates that the off-axis EIRP spectral density envelope set forth in paragraphs (a)(1)(i)(A) through (a)(1)(i)(C) of this section will be met under the assumption that the antenna is pointed at the target satellite. | NA |  |


| § 25.226(b)(1)(iii) | (iii) A VMES applicant proposing to implement a transmitter under paragraph (a)(1)(ii)(A) of this section shall provide a certification from the equipment manufacturer stating that the antenna tracking system will maintain a pointing error of less than or equal to $0.2^{\circ}$ between the orbital location of the target satellite and the axis of the main lobe of the VMES antenna and that the antenna tracking system is capable of ceasing emissions within 100 milliseconds if the angle between the orbital location of the target satellite and the axis of the main lobe of the VMES antenna exceeds $0.5^{\circ}$. | NA |  |
| :---: | :---: | :---: | :---: |
| § 25.226(b)(1)(iv) | (iv) A VMES applicant proposing to implement a transmitter under paragraph (a)(1)(ii)(B) of this section shall: | Complies |  |
| § 25.226(b)(1)(iv)(A) | (A) Declare, in its application, a maximum antenna pointing error and demonstrate that the maximum antenna pointing error can be achieved without exceeding the off-axis EIRP spectral-density limits in paragraph (a)(1)(i) of this section; and | Complies | Section 5 |
| § 25.226(b)(1)(iv)(B) | (B) Demonstrate that the VMES transmitter can detect if the transmitter exceeds the declared maximum antenna pointing error and can cease transmission within 100 milliseconds if the angle between the orbital location of the target satellite and the axis of the main lobe of the VMES antenna exceeds the declared maximum antenna pointing error, and will not resume transmissions until the angle between the orbital location of the target satellite and the axis of the main lobe of the VMES antenna is less than or equal to the declared maximum antenna pointing error. | Complies | Section 5 |
| § 25.226(b)(2) | (2) A VMES applicant proposing to implement a transmitter under paragraph (a)(2) of this section and using off-axis EIRP spectral-densities in excess of the levels in paragraph (a)(1)(i) of this section shall provide the following certifications and demonstration as exhibits to its earth station application: | NA |  |


| § 25.226(b)(2)(i) | (i) A statement from the target satellite operator certifying that the proposed operation of the VMES has the potential to create harmful interference to satellite networks adjacent to the target satellite(s)that may be unacceptable. |  |  |
| :---: | :---: | :---: | :---: |
| § 25.226(b)(2)(ii) | (ii) A statement from the target satellite operator certifying that the power density levels that the VMES applicant provided to the target satellite operator are consistent with the existing coordination agreements between its satellite(s) and the adjacent satellite systems within 6DEG of orbital separation from its satellite(s). |  |  |
| § 25.226(b)(2)(iii) | (iii) A statement from the target satellite operator certifying that it will include the power-density levels of the VMES applicant in all future coordination agreements. |  |  |
| § 25.226(b)(2)(iv) | (iv) A demonstration from the VMES operator that the VMES system is capable of detecting and automatically ceasing emissions within 100 milliseconds when the transmitter exceeds the off-axis EIRP spectral-densities supplied to the target satellite operator. |  |  |
| § 25.226(b)(3) | (3) A VMES applicant proposing to implement VMES system under paragraph (a)(3) of this section and using variable power-density control of individual simultaneously transmitting co-frequency VMES earth stations in the same satellite receiving beam shall provide the following certifications and demonstration as exhibits to its earth station application: | NA |  |


|  | (i) The applicant shall make a detailed showing of the <br> measures it intends to employ to maintain the effective <br> aggregate EIRP-density from all simmultaneously <br> transmitting co-frequency terminals operating with the <br> same satellite transponder at least 1 dB below the EIRP- <br> density limits defined in paragraphs (a)(1)(i)(A) through <br> (C) of this section. In this context the term "effective" <br> means that the resultant co-polarized and cross-polarized <br> EIRP-density experienced by any GSO or non-GSO <br> satellite shall not exceed that produced by a single VMES <br> transmitter operating at 1 dB below the limits defined in <br> paragraphs(a)(1)(i)(A) through (C) of this section. The <br> International Bureau will place this showing on public <br> notice along with the application. |  |
| :--- | :--- | :--- |
| §25.226(b)(3)(i) | (ii) An applicant proposing to implement a VMES under <br> paragraph (a)(3)(ii) of this section that uses off-axis EIRP <br> spectral-densities in excess of the levels in paragraph <br> (a)(3)(i) of this section shall provide the following <br> certifications, demonstration and list of satellites as exhibits <br> to its earth station application: |  |
|  | (A) A detailed showing of the measures the applicant <br> intends to employ to maintain the effective aggregate EIRP- <br> density from all simultaneously transmitting co-frequency <br> terminals operating with the same satellite transponder at <br> the EERP--density limits supplied to the target satellite <br> operator. The International Bureau will place this showing |  |
| on public notice along with the application. |  |  |$\quad$| §25.226(b)(3)(ii) |
| :--- |


| § 25.226(b)(3)(ii)(C) | (C) A statement from the target satellite operator certifying that the aggregate power density levels that the VMES applicant provided to the target satellite operator are consistent with the existing coordination agreements between its satellite(s) and the adjacent satellite systems within 6DEG of orbital separation from its satellite(s). |  |  |
| :---: | :---: | :---: | :---: |
| § 25.226(b)(3)(ii)(D) | (D) A statement from the target satellite operator certifying that it will include the aggregate power-density levels of the VMES applicant in all future coordination agreements. |  |  |
| § 25.226(b)(3)(ii)(E) | (E) A demonstration from the VMES operator that the VMES system is capable of detecting and automatically ceasing emissions within 100 milliseconds when an individual transmitter exceeds the off-axis EIRP spectraldensities supplied to the target satellite operator and that the overall system is capable of shutting off an individual transmitter or the entire system if the aggregate off-axis EIRP spectral-densities exceed those supplied to the target satellite operator. |  |  |
| § 25.226(b)(3)(ii)(F) | (F) An identification of the specific satellite or satellites with which the VMES system will operate. |  |  |
| § 25.226(b)(3)(iii) | (iii) The applicant shall acknowledge that it will maintain sufficient statistical and technical information on the individual terminals and overall system operation to file a detailed report, one year after license issuance, describing the effective aggregate EIRP-density levels resulting from the operation of the VMES system. |  |  |
| § 25.226(b)(4) | (4) There shall be an exhibit included with the application describing the geographic area(s) in which the VMESs will operate. | Complies | Narrative <br> Section II.E. 3 |
| § 25.226(b)(5) | (5) Any VMES applicant filing for a VMES terminal or system and planning to use a contention protocol shall include in its application a certification that will comply with the requirements of paragraph (a)(4) of this section. | NA |  |
| § 25.226(b)(6) | (6) The point of contact referred to in paragraph (a)(5) of this section shall be included in the application. | Complies | Narrative <br> Section II.E. 3 |


| § 25.226(b)(7) | (7) Any VMES applicant filing for a VMES terminal or system shall include in its application a certification that will comply with the requirements of paragraph (a)(6) of this section. | Complies | Narrative <br> Section II.E. 3 |
| :---: | :---: | :---: | :---: |
| §25.226(b)(8) | (8) All VMES applicants shall submit a radio frequency hazard analysis determining via calculation, simulation, or field measurement whether VMES terminals, or classes of terminals, will produce power densities that will exceed the Commission's radio frequency exposure criteria. VMES applicants with VMES terminals that will exceed the guidelines in § 1.1310 of this chapter for radio frequency radiation exposure shall provide, with their environmental assessment, a plan for mitigation of radiation exposure to the extent required to meet those guidelines. All VMES licensees shall ensure installation of VMES terminals on vehicles by qualified installers who have an understanding of the antenna's radiation environment and the measures best suited to maximize protection of the general public and persons operating the vehicle and equipment. A VMES terminal exhibiting radiation exposure levels exceeding 1.0 $\mathrm{mW} / \mathrm{cm} \wedge 2$ in accessible areas, such as at the exterior surface of the radome, shall have a label attached to the surface of the terminal warning about the radiation hazard and shall include thereon a diagram showing the regions around the terminal where the radiation levels could exceed $1.0 \mathrm{~mW} / \mathrm{cm}^{\wedge} \wedge 2$. All VMES licensees shall ensure that a VMES terminal ceases transmission upon encountering an obstruction that degrades the VMES downlink signal. | Complies | Exhibit 4 |


| § 25.226(c)(1) | (c)(1) Operations of VMESs in the 14.0-14.2 GHz (Earth-to-space) frequency band within 125 km of the NASA TDRSS facilities on Guam (latitude 13DEG36'55" N, longitude 144DEG51'22" E) or White Sands, New Mexico (latitude 32DEG20'59" N, longitude 106DEG36'31" W and latitude 32DEG32'40" N, longitude 106DEG36'48" W) are subject to coordination with the National Aeronautics and Space Administration (NASA) through the National Telecommunications and Information Administration (NTIA) Interdepartment Radio Advisory Committee (IRAC). Licensees shall notify the International Bureau once they have completed coordination. Upon receipt of such notification from a licensee, the International Bureau will issue a public notice stating that the licensee may commence operations within the coordination zone in 30 days if no party has opposed the operations. | Complies | Narrative <br> Section II.E. 4 |
| :---: | :---: | :---: | :---: |
| § 25.226(c)(2) | (2) When NTIA seeks to provide similar protection to future TDRSS sites that have been coordinated through the IRAC Frequency Assignment Subcommittee process, NTIA will notify the Commission's International Bureau that the site is nearing operational status. Upon public notice from the International Bureau, all Ku-band VMES licensees shall cease operations in the $14.0-14.2 \mathrm{GHz}$ band within 125 km of the new TDRSS site until the licensees complete coordination with NTIA/IRAC for the new TDRSS facility. Licensees shall notify the International Bureau once they have completed coordination for the new TDRSS site. Upon receipt of such notification from a licensee, the International Bureau will issue a public notice stating that the licensee may commence operations within the coordination zone in 30 days if no party has opposed the operations. The VMES licensee then will be permitted to commence operations in the $14.0-14.2 \mathrm{GHz}$ band within 125 km of the new TDRSS site, subject to any operational constraints developed in the coordination process. |  |  |


|  | (d)(1) Operations of VMESs in the 14.47-14.5 GHz (Earth- <br> to-space) frequency band in the vicinity of radio astronomy <br> service (RAS) observatories observing in the 14.47-14.5 <br> GHz band are subject to coordination with the National <br> Science Foundation (NSF). The appropriate NSF contact <br> point to initiate coordination is Electromagnetic Spectrum <br> Manager, NSF, 4201 Wilson Blvd., Suite 1045,Arlington <br> VA 22603, fax 703-292-9034, e-mail esm@nsf.gov . <br> Licensees shall notify the International Bureau once they <br> have completed coordination. Upon receipt of the <br> coordination agreement from a licensee, the International <br> Bureau will issue a public notice stating that the licensee <br> may commence operations within the coordination zone in <br> 30 days if no party has opposed the operations. | Complies |
| :--- | :--- | :--- |


|  | Los Alamos, NM 35DEG46'30" 106DEG14'44" |  |  |
| :---: | :---: | :---: | :---: |
|  | Fort Davis, TX 30DEG38'06" 103DEG56'41' |  |  |
|  | North Liberty, IA 41DEG46'17" 91DEG34'27" |  |  |
|  | Hancock, NH 42DEG56'01" 71DEG59'12" |  |  |
|  | St. Croix, VI 17DEG45'24" 64DEG35'01" |  |  |
|  | *Owens Valley, CA operates both a VLBA station and single-dish telescopes. |  |  |
| § 25.226(d)(3) | (3) When NTIA seeks to provide similar protection to future RAS sites that have been coordinated through the IRAC Frequency Assignment Subcommittee process, NTIA will notify the Commission's International Bureau that the site is nearing operational status. Upon public notice from the International Bureau, all Ku-band VMES licensees shall cease operations in the $14.47-14.5 \mathrm{GHz}$ band within the relevant geographic zone ( 160 kms for single-dish radio observatories and Very Large Array antenna systems and 50 kms for Very Long Baseline Array antenna systems) of the new RAS site until the licensees complete coordination for the new RAS facility. Licensees shall notify the International Bureau once they have completed coordination for the new RAS site and shall submit the coordination agreement to the Commission. Upon receipt of such notification from a licensee, the International Bureau will issue a public notice stating that the licensee may commence operations within the coordination zone in 30 days if no party opposed the operations. The VMES licensee then will be permitted to commence operations in the $14.47-14.5 \mathrm{GHz}$ band within the relevant coordination distance around the new RAS site, subject to any operational constraints developed in the coordination process. |  |  |
| § 25.226(e) | (e) VMES licensees shall use Global Positioning Satelliterelated or other similar position location technology to ensure compliance with paragraphs (c) and (d) of this section. | Complies | Narrative <br> Section II.E. 4 |

8. Sample Link Analysis


| Forward Link Parameters | Uplink | Downli <br> nk |
| :--- | :---: | :---: |
|  | Carlsba | Var |
| Site | Seattl |  |
| Frequency, GHz | 14.18 | e |
| Availability | $99.75 \%$ | 99.75 |
| Antenna Size, m | 4.5 | 0.37 |
| Modulation | QPSK DSSS |  |
| Coding | Rate 1/3 Turbo |  |
| Data rate (khns) | 4000 |  |


| Uplink C/No budget | Clear Sky | Rain U/L |
| :---: | :---: | :---: |
| Uplink EIRP (incl. UPC compensation) | 65.5 | 66.9 dBW |
| Hub Pointing Loss | 0.5 | 0.5 dB |
| Path Loss | 207.0 | 208.3 dB |
|  | 1.25 | $1.25 \mathrm{~dB} / \mathrm{K}$ |
| Boltzizanni's constant | 228.6 | 228.6 dBW/K/Hz |
| Uplink C/No Transponder input | 87.93 | 87.9 dBHz |
| Carrier Suppression | 0.51 | 0.51 dB |
| Noise Suppression | 1.74 | 1.74 dB |
| Uplink C/No Transponder output | 89.2 | 89.2 dBHz |


| Uplink C/Io terms |  |  |
| :--- | ---: | :---: |
| ASI | Clear Sky | Rain U/L |
| CrossPol | 93.9 | 93.9 dBHz |
| Uplink HPA IM | 94.6 | 94.6 dBHz |
| Uplink CIIO Transponder input | 100 | 100 dBHz |
| Carrier Suppression | 90.7 | 90.7 dBHz |
| Noise Suppression | 0.51 | 0.51 dB |
| Uplink C/lo Transponder output | 1.74 | 1.74 dB |


| Uplink Path Loss | Clear Sky | Rain U/L |
| :--- | ---: | :--- |
| Freespace Path Loss | 206.87 | 206.9 dB |
| Gaseous Attenuation | 0.10 | 0.10 dB |
| Rain Attenuation | 0 | 1.2 dB |
| Cloud Attenuation | 0 | 0.15 dB |
| Scintilltation | 0 | 0.16 dB |
| Total Attenuation | 207.0 | 208.3 dB |


| Uplink Propagation Model |  |
| :--- | :---: |
| Frequency | 14.18 GHzz |
| Availability | $99.75 \%$ |
| Satelite Longitude | $255.0^{\circ} \mathrm{E}$ |
| Site Location | Carlsbad |
| Sitit Latitude | $3.2^{\mathrm{N}}$ |
| Site Lotngitude | $242.7^{\circ} \mathrm{E}$ |
| Site Allitude | 0.0 km |
| Antenna efficiency | $65 \%$ |
| Antenna diameter | 4.5 m |
| Polarization | V |
| Slant Range | 3714.4 km |
| Elevation Angle | $49.21^{\circ}$ |
| Rain Height | 3.2 km |
| Rain Intensity @ 0.01\% | $25.1 \mathrm{~mm} / \mathrm{hr}$ |
| Total Columnar Content of Liquid @ 0.01 | $0.6 \mathrm{~kg} / \mathrm{m} 2$ |
| Wet term of refraction coindex | 45.3 |
| Temperature | 289.6 K |
| Water Vapor Content | $7.2 \mathrm{~g} / \mathrm{m3}$ |
| Polarization Angle | $18.1^{\circ}$ |


| EndtoEnd Link Budget | Clear Sky | $\begin{aligned} & \text { Rain } \\ & \text { U/L } \\ & \text { Rain } \\ & \text { D/ } \end{aligned}$ | Rain U/L <br> Clear Sky D/L | Clear Sky U/L <br> Rain D/L |
| :---: | :---: | :---: | :---: | :---: |
| Uplink C/No | 89.2 | 89.2 | 89.2 | 89.2 dBHz |
| Uplink C/Io | 91.9 | 91.9 | 91.9 | 91.9 dBHz |
| Downlink C/No | 76.6 | 73.7 | 76.6 | 73.7 dBHz |
| Downlink C/lo | 74.2 | 74.2 | 74.2 | 74.2 dBHz |
| Total C/(No+lo) | 72.1 | 70.8 | 72.1 | 70.8 dBHz |
| Required C/( $\mathrm{No}+\mathrm{lo}$ ) | 67.7 | 67.7 | 67.7 | 67.7 dBHz |


| Downlink C/No budget | Clear Sky | Rain | Rain U/L <br> Clear Sky D/L | Clear Sky U/L Rain D/L |
| :--- | ---: | ---: | ---: | :---: |
| Downlink EIRP | 43.49 | 43.5 | 43.5 | 43.5 dBW |
| Path Loss | 205.71 | 206.9 | 205.7 | 206.9 dB |
| Mobile Clearsky G/T | 10.2 | 10.2 | $10.2 \mathrm{~dB} / \mathrm{K}$ |  |
| Rain Noise Temperature9therecs5e3 | 0.51 | 18.3787284 | 1.55 |  |
| Boltzmann's constant | 10.2 | 1.7 | 0 | 1.7 dB |
| Downlink C/No | 228.60 | 228.6 | 228.6 | $228.6 \mathrm{dBW} / \mathrm{K} / \mathrm{Hz}$ |


| Downlink C/Io terms | Clear Sky | Rain | Rain U/L | Clear Sky U/L |
| :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { Rain } \\ & \text { DII } \end{aligned}$ | Clear Sky D/L | Rain D/L |
| ASI | 74.50 | 74.50 | 74.50 | 74.50 dBHz |
| CrossPol | 88.06 | 88.06 | 88.06 | 88.06 dBHz |


| Downlink Path Loss | Clear Sky | Rain D/L |
| :--- | ---: | :--- |
| Freespace Path Loss | 205.60 | 205.6 dB |
| Gaseous Attenuation | 0.11 | 0.11 dB |
| Rain A Attenuation | 0 | 1.0 dB |
| Cloud Attenuation | 0 | 0.16 dB |
| Scintillation | 0 | 0.2 dB |
| Total Attenuation | 205.7 | 206.9 dB |


| Downlink Propagation Model |  |
| :---: | :---: |
| Frequency | 11.88 GHz |
| Availability | 99.75\% |
| Satellite Longitude | $255.0{ }^{\circ} \mathrm{E}$ |
| Site Location | Var Seattle |
| Site Latitude | $46.6{ }^{\circ} \mathrm{N}$ |
| Site Longitude | $237.8{ }^{\circ} \mathrm{E}$ |
| Site Allitude | 0.0 km |
| Antenna efficiency | 60\% |
| Antenna diameter | 0.4 m |
| Polarization | H |
| Slant Range | 38293.1 km |
| Elevation Angle | $33.8{ }^{\circ}$ |
| Rain Height | 2.5 km |
| Rain Intensity @ 0.01\% | 40.0 mm/hr |
| Total Columnar Content of Liquid @ 0.01 | $0.7 \mathrm{~kg} / \mathrm{m} 2$ |
| Wet term of refraction coindex | 35.0 |
| Temperature | 279.0 K |
| Water Vapor Content | $5.2 \mathrm{~g} / \mathrm{m} 3$ |
| Polarization Angle | $74.4{ }^{\circ}$ |
| Tsys, clear sky | 117.0 K |
| Tsys, rain | 173.9 K |



| Uplink C/Io terms | Clear Sky | Rain U/L |
| :--- | ---: | :---: |
| ASI | 65.0 | 63.0 dBHz |
| CrossPol | 65.6 | 63.7 dBHz |
| Uplink HPA IM | 100 | 100 dBHz |
| Uplink C/lo Transponder input | 62.3 | 60.4 dBHz |
| Carrier Suppression | 1.75 | 1.75 dB |
| Noise Suppression | 1.74 | 1.74 dB |
| Uplink C/lo Transponder output | 62.3 | 60.3 dBHz |


| Uplink Path Loss | Clear Sky | Rain U/L |
| :--- | ---: | ---: |
| Freespace Path Loss | 207.14 | 207.1 dB |
| Gaseous Attenuation | 0.13 | 0.13 dB |
| Rain Attenuation | 0 | 1.7 dB |
| Cloud Anttenuation | 0 | 0.22 dB |
| Scintillation | 0 | 0.27 dB |
| Total Attenuation | 207.3 | 209.2 dB |


| EndtoEnd Link Budget | Clear Sky | $\begin{gathered} \hline \text { Rain } \mathbf{U} / \\ \mathbf{L} \\ \text { Rain } \mathbf{D} / \\ \mathbf{L} \\ \hline \mathbf{E} \text { ( } 05 \end{gathered}$ | Rain U/L <br> Clear Sky D/L | Clear Sky U/L <br> Rain D/L |
| :---: | :---: | :---: | :---: | :---: |
| Uplink C/No | 58.97 | 57.05 | 57.05 | 58.97 dBHz |
| Uplink C/Io | 62.26 | 60.34 | 60.34 | 62.26 dBHz |
| Downlink C/No | 71.90 | 67.77 | 69.98 | 69.69 dBHz |
| Downlink C/Io | $55.9662923 \quad 62.19$ | 60.27 | 60.27 | 62.19 dBHz |
| Multiple Access Interference | $55.9662923 \quad 64.27$ | 62.35 | 62.35 | 64.27 dBHz |
| Total C/(No+10) | 55.37 | 53.38 | 53.45 | 55.30 dBHz |
| Required $\mathrm{C} /(\mathrm{No}+\mathrm{lo}$ ) | 53.32 | 53.32 | 53.32 | 53.32 dBHz |
| Margin | 2.0 | 0.1 | 0.1 | 2.0 dB |
|  |  | $\begin{gathered} \text { Rain } \mathbf{U} / \\ \mathbf{L} \end{gathered}$ | Rain U/L | Clear Sky U/L |
| Downlink C/No budget | Clear Sky | $\underset{\mathbf{L}}{\operatorname{Rain}} \mathbf{D /}$ | Clear Sky D/L | Rain D/L |
| Downlink EIRP | 16.27 | 14.4 | 14.4 | 16.3 dBW |
| Path Loss | 205.41 | 206.2 | 205.4 | 206.2 dB |
| Hub Clearsky G/T | 32.44 | 32.4 | 32.4 | 32.4 dB/K |
| Rain Noise Temperature Increase | 0.00 | 1.4 | 0.0 | 1.4 dB |
| Boltzmann's constant | 228.60 | 228.6 | 228.6 | 228.6 dBW/K/Hz |
| Downlink C/No | 71.9 | 67.8 | 70.0 | 69.7 dBHz |


|  |  | Rain U/ <br> $\mathbf{L}$ <br> Rain <br> L/ | Rain U/L <br> Clear Sky D/L | Clear Sky U/L |
| :--- | ---: | ---: | ---: | ---: |
| Downlink C/Io terms | Clear Sky | Rain D/L |  |  |
| ASI | 78.77 | 76.85 | 76.85 | 78.77 dBHz |
| CrossPol | 73.44 | 71.52 | 71.52 | 73.44 dBHz |
| Transponder IM | 63.51 | 61.59 | 61.59 | 63.51 dBHz |
| PCMA C/lo | 70.01 | 68.09 | 68.09 | 70.01 dHz |


| Downlink Path Loss | Clear Sky | Rain |
| :--- | ---: | :--- |
| Freespace Path LLoss | 205.3 | 205.3 dB |
| Gaseous Attenuation | 0.08 | 0.08 dB |
| Rain Attenuation | 0 | 0.7 dB |
| Cloud Attenuation | 0 | 0.11 dB |
| Scintilation | 0 | 0.15 dB |
| Total Attenuation | 205.41 | 206.2 dB |

## 9. Antenna Gain Data



Figure 11 - C0-Pol Gain +/- 10 dgrees


Figure 12 - Co-Pol Gain +/- 180 dgrees


Figure 13 - Cross-pol Gain Pattern +/- 9 degrees


[^0]:    ${ }^{1}$ Paired Carrier Multiple Access is a proprietary technique developed by ViaSat for their spread spectrum ArcLight service.

[^1]:    ${ }^{2}$ See File No. SES-LIC-20081104-01450 (Call Sign E090001).
    ${ }^{3} I d$.
    ${ }^{4}$ Call Signs E040267, E030131 and E010236, respectively.

[^2]:    ${ }^{5}$ See Coordination Agreement with the National Science Foundation, submitted with a letter dated November 20, 2008 in IBFS File No. SES-LIC-20081104-01450 (being expanded to cover VMES operations subject to the same technical limitations applicable to ESV operations). KVH will accept technical limitations imposed on other Ku-band VMES operations necessary to protect TDRSS operations. See 47 C.F.R. § 25.226(c).
    ${ }^{6}$ CRMA, or Code Reuse Multiple Access, is a ViaSat proprietary spread spectrum technique, similar to CDMA, used in the ArcLight satellite system.

[^3]:    ${ }^{7}$ EIRP envelope exceeds mask by as much as 1.55 dB between -75 to -85 degrees and +75 to 85 degrees, $<5.7 \%$ of sidelobes. Per FCC $\S 25.226$ (a)(1)(i)(A) for angles greater than $7.0^{\circ}$, the envelope may be exceeded by no more than $10 \%$ of the sidelobes, provided no individual sidelobe exceeds the envelope given above by more than 3 dB .

