The California Channel Exhibit B
Radiation Hazard

# The California Channel 

## Radiation Hazard

General description of installation and summary of proposed measures used to protect human exposure to radio frequency electromagnetic fields.

The transmit earth station will be located on the secured roof of an office building in a controlled environment. The access door leading to the roof will be locked and access provided only to authorized building maintenance personnel. A sign warning of potential hazard from RF Electromagnetic Fields will be posted on the door leading to the roof.

The roof mounted earth station antenna will be located within a personnel barrier adequate to prevent human exposure to unsafe levels of RF electromagnetic fields, including occupancy of the area in front of the antenna. The personnel barrier will be equipped with radio frequency hazard warning signs in all accessible directions.

Description of specific areas and proposed measures to prevent human exposure to radio frequency electromagnetic fields.

Antenna surface and region between the feed horn and surface:
Operators and technicians shall receive training specifying these areas as high exposure areas. Procedures will be established that will assure that all transmitters are turned off before access by maintenance personnel to this area is possible.

## On-axis near, transition and far regions:

In any operating position, the antenna pointing requires that the on-axis regions be well clear of directions that would cause human exposure to radio frequency electromagnetic fields. The antenna requires manual alignment prior to use by personnel at the antenna on the rooftop. The requirement to manually align the antenna will allow personnel to insure that the antenna is not improperly aligned in such a way to cause a RF hazard.

## Off axis, near, transition and far regions:

The potential exposure levels fall below that established for both the controlled and uncontrolled environment.

## ANDREW.

## Radiation Hazard Analysis

This analysis predicts the radiation levels around a proposed earth station complex, comprised of one or more aperture (reflector) type antennas. This report is developed in accordance with the prediction methods contained in OET Bulletin No. 65,
"Evaluating Compliance with FCC Guidelines for Human Exposure to Radio Frequency Electromagnetic Fields," Edition 97-01, pp 26-30. The maximum level of non-ionizing radiation to which employees may be exposed is limited to a power density level of 5 milliwatts per square centimeter ( $5 \mathrm{~mW} / \mathrm{cm}^{2}$ ) averaged over any 6 minute period in a controlled environment and the maximum level of non-ionizing radiation to which the general public is exposed is limited to a power density level of 1 milliwatt per square centimeter ( $1 \mathrm{~mW} / \mathrm{cm}^{2}$ ) averaged over any 30 minute period in a
uncontrolled evironment. Note that the worse-case radiation hazards exist along the beam axis. Under normal circumstances, it is highly unlikely that the antenna axis will be aligned with any occupied area since that would represent a blockage to the desired signals, thus rendering the link unuseable.

## Earth Station Technical Parameter Table

| Antenna Actual Diameter | 2.4 | meters |  |
| :---: | :---: | :---: | :---: |
| Antenna Surface Area | 4.5 | sq. meters |  |
| Antenna Isotropic Gain |  | 42.4 | dBi |
| Number of Identical Adjacent Antennas* |  | 1 |  |
| Nominal Antenna Efficiency ( $\varepsilon$ ) |  | 72 \% |  |
| Nominal Frequency |  | 6185 | MHz |
| Nominal Wavelength ( $\lambda$ ) |  | 0.0485 | meters |
| Maximum Transmit Power / Carrier |  | 50 | Watts |
| Number of Carriers |  | 2 |  |
| Total Transmit Power |  | 100 | Watts |
| W/G Loss from Transmitter to Feed |  | 0 | dB |
| Total Feed Input Power |  | 100 | Watts |
| Near Field Limit | $\mathrm{R}_{\mathrm{nf}}=\mathrm{D}^{2 / 4 \lambda}=$ |  | 30 |
| Far Field Limit | $\mathrm{R}_{\mathrm{ff}}=0.6 \mathrm{D}^{2} / \lambda=$ |  | 71 |
| Transition Region | $\mathrm{R}_{\mathrm{nf}}$ to $\mathrm{R}_{\mathrm{ff}}$ |  |  |

* The Radiation Levels will be increased directly by the number of antennas indicated, on the assumption that all antennas may illuminate the same area.
In the following sections, the power density in the above regions, as well as other critically important areas will be calculated and evaluated. The calculations are done in the order discussed in OET Bulletin 65. In addition to the input parameters above, input cells are provided below for the user to evaluate the power density at specific distances or angles.


### 1.0 At the Antenna Surface

The power density at the reflector surface can be calculated from the expression:

$$
\begin{array}{lll}
P D_{\text {reff }}= & 4 P / A= & 8.84 \mathrm{~mW} / \mathrm{cm}^{2} \\
\text { Where: } & P=\text { total power at feed, milliwatts }  \tag{1}\\
& A=\text { Total area of reflector, sq. } \mathrm{cm}
\end{array}
$$

In the normal range of transmit powers for satellite antennas, the power densities at or around the reflector surface is expected to exceed safe levels. This area will not be accessible to the general public. Operators and technicians should receive training specifying this area as a high exposure area. Procedures must be established that will assure that all transmitters are rerouted or turned off before access by maintenance personnel to this area is possible.

### 2.0 On-Axis Near Field Region

The geometrical limits of the radiated power in the near field approximate a cylindrical volume with a diameter equal to that of the antenna. In the near field, the power density is neither uniform nor does its value vary uniformly with distance from the antenna. For the purpose of considering radiation hazard it is assumed that the on-axis flux density is at its maximum value throughout the length of this region. The length of this region, i.e., the distance from the antenna to the end of the near field, is computed as Rnf above.
The maximum power density in the near field is given by:

$$
\begin{array}{ll}
P D_{\mathrm{nf}}=(16 \varepsilon P) /\left(\cap D^{2}\right)= & 6.36 \mathrm{~mW} / \mathrm{cm}^{2}  \tag{2}\\
& \text { from } 0 \text { to } \quad 30 \text { meters }
\end{array}
$$

Evaluation

```
Uncontrolled Environment: Mitigation Required, See Note 1
Controlled Environment: Mitigation Required, See Note 1
```


### 3.0 On-Axis Transition Region

The transition region is located between the near and far field regions. As stated in Bulletin 65, the power density begins to vary inversely with distance in the transition region. The maximum power density in the transition region will not exceed that calculated for the near field region, and the transition region begins at that value. The maximum value for a given distance within the transition region may be computed for the point of interest according to:

$$
\begin{array}{ll}
P D_{t}= & \left(P D_{n f}\right)\left(R_{n f}\right) / R=\text { dependent on } R  \tag{3}\\
\text { where: } & P D_{n f}=\text { near field power density } \\
& R_{n f}=\text { near field distance } \\
& R=\text { distance to point of interest } \\
& \text { For: } \quad 30<R<\quad 71 \text { meters }
\end{array}
$$

We use Eq (3) to determine the safe on-axis distances required for the two occupancy conditions:
Evaluation

| Uncontrolled Environment Safe Operating Distance, | In F-F region, See |
| :--- | :--- |
| (meters), $R_{\text {safeu }}$ : | Section 4 |

Controlled Environment Safe Operating Distance,(meters),
$\mathrm{R}_{\text {safec }}$ :

### 4.0 On-Axis Far-Field Region

The on- axis power density in the far field region ( $\mathrm{PD}_{\mathrm{ff}}$ ) varies inversely with the square of the distance as follows:
$P D_{f f}=P G /\left(4 \Pi R^{2}\right)=$ dependent on $R$
where: $P=$ total power at feed
$\mathrm{G}=$ Numeric Antenna gain in the direction of interest relative to isotropic radiator
$R=$ distance to the point of interest

$$
\begin{array}{ll}
\text { For: } \mathrm{R}>\mathrm{R}_{\mathrm{ff}}= & 71 \text { meters } \\
\mathrm{PD}_{\mathrm{ff}}= & 2.72 \mathrm{~mW} / \mathrm{cm}^{2} \\
& \text { at } R_{\mathrm{ff}}
\end{array}
$$

We use Eq (4) to determine the safe on-axis distances required for the two occupancy conditions:
Evaluation
Uncontrolled Environment Safe Operating Distance,(meters), $\mathrm{R}_{\text {safeu }}$ : 118
Controlled Environment Safe Operating Distance,(meters), $\mathrm{R}_{\text {safec }}$ : See Section 3

### 5.0 Off-Axis Levels at the FarField Limit and Beyond

In the far field region, the power is distributed in a pattern of maxima and minima (sidelobes) as a function of the off-axis angle between the antenna center line and the point of interest. Off-axis power density in the far field can be estimated using the antenna radiation patterns prescribed for the antenna in use. Usually this will correspond to the antenna gain pattern envelope defined by the FCC or the ITU, which takes the form of:
$\mathrm{G}_{\text {off }}=32-25 \log (\theta)$
for $\Theta$ from 1 to 48 degrees; -10 dBi from 48 to 180 degrees
(Applicable for commonly used satellite transmit antennas)
Considering that satellite antenna beams are aimed skyward, power density in the far field will usually not be a problem except at low look angles. In these cases, the off axis gain reduction may be used to further reduce the power density levels.
For example: At one (1) degree off axis At the far-field limit, we can calculate the power density as:

$$
\begin{array}{ll}
G_{\text {off }}=32-25 \log (1)=32-0 \mathrm{dBi}=1585 \text { numeric } & \\
P D_{1 \text { deg off-axis }}=P D_{\text {ff }} \times 1585 / \mathrm{G}= & 0.2484 \mathrm{~mW} / \mathrm{cm}^{2} \tag{5}
\end{array}
$$

6.0 Off-Axis power density in the Near Field and Transitional Regions

According to Bulletin 65, off-axis calculations in the near field may be performed as follows: assuming that the point of interest is at least one antenna diameter removed from the center of the main beam, the power density at that point is at least a factor of $100(20 \mathrm{~dB})$ less than the value calculated for the equivalent on-axis power density in the main beam. Therefore, for regions at least $D$ meters away from the center line of the dish, whether behind, below, or in front under of the antenna's main beam, the power density exposure is at least 20 dB below the main beam level as follows:

$$
P D_{n f(o f f-a x i s)}=P D_{n f} / 100=\quad 0.064 \mathrm{~mW} / \mathrm{cm}^{2} \text { at } D \text { off axis (6) }
$$

See page 5 for the calculation of the distance vs elevation angle required to achieve this rule for a given object height.

### 7.0 Region Between the Feed Horn and Sub-reflector

Transmissions from the feed horn are directed toward the subreflector surface, and are confined within a conical shape defined by the feed horn. The energy between the feed horn and subreflector is conceded to be in excess of any limits for maximum
permissible exposure. This area will not be accessible to the general public. Operators and technicians should receive training specifying this area as a high exposure area. Procedures must be established that will assure that all transmitters are rerouted or turned off before access by maintenance personnel to this area is possibie.
Note 1:
Mitigation of the radiation level may take several forms. First, check the distance from the antenna to the nearest potentially occupied area that the antenna could be pointed toward, and compare to the distances appearing in Sections 2, $3 \& 4$. If those distances lie within the potentially hazardous regions, then the most common solution would be to take steps to insure that the antenna(s) are not capable of being pointed at those areas while RF is being transmitted. This may be accomplished by setting the tracking system to not ailow the antenna be pointed below certain eievation angies. Other techniques, such as shielding may also be used effectively.

Evaluation of Safe Occupancy Area in Front of Antenna
The distance ( S ) from a vertical axis passing through the dish center to a safe off axis location in front of the antenna can be determined based on the dish diameter ruie (Item 6.0). Assuming a flat terrain in front of the antenna, the relationship is:

$$
\begin{equation*}
S=(D / \sin a)+(2 h-D-2) /(2 \tan a) \tag{7}
\end{equation*}
$$

Where: $\quad \mathrm{a}=$ minimum elevation angle of antenna
$D=$ dish diameter in meters
$h=$ maximum height of object to be cleared, meters
For distances equal or greater than determined by equation (7), the radiation hazard will be below safe leveis for all but the most powerful stations (> 4 kilowatts RF at the feed).

| For | D | 2.4 | meters |
| :--- | :--- | :--- | :--- |
| $h=$ | 2.5 | meters |  |

Then:

| $a$ | $S$ |  |  |
| :--- | :--- | :--- | :--- |
| 10 |  | 15.5 | meters |
| 15 | 10.4 | meters |  |
| 20 | 7.8 | meters |  |
| 25 | 6.3 | meters |  |
| 30 | 5.3 | meters |  |
| 33.5 | 4.8 | meters |  |
| 41.3 | 4 | meters |  |

Suitable fencing or other barrier should be provided to prevent casual occupancy of the area in front of the antenna within the limits prescribed above at the iowest elevation angle required.
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The California Channel Exhibit C
Sketch of Antenna Site

## The California Channel Site Sketch



The California Channel
Exhibit D
Frequency Coordination

## Multicomm Sciences Int'I, Inc

May 10, 2004

TO: All Coordinators
RE: The California Channel
T/R Earth Station Sacramento, CA PCN dated March 26, 2004 Information Only Letter

Dear Sir or Madam:
On behalf of our client, The California Channel, we are enclosing an information- only letter on the above prior coordination notice.

Our client has dropped the power and increased the bandwidth only. Please do not report any cases already resolved at a higher power.

For your convenience, we have enclosed data sheets reflecting this change. Should you have any questions, please do not hesitate to contact MSI.

Sincerely,


Andrea Palsulich, Manager
Data Processing Dept
Enc.

SATELLITE EARTH STATION EREQUENCY COORDINATION DATA 05/10/04


MULTICOMM SCIENCES INTERNATIONAL,INC. Denville, NJ 07834 (973)-627-7400

SACRAMENTO, CA
$\begin{array}{lll}38 & 34 & 40.5\end{array}$
1212930.2

| AZ | DISC | HOR ANG | 4GHZ | 6 GHz | 4GHz | 6GHZ | RAIN 4 | RAIN 6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DEG | DEG D | DEGREES | HOR GAIN | HOR GAIN | COORD KM | COORD KM | SCAT KM | SCAT KM |
| 5. | 121. | . 0 | -12.0 | -13.0 | 116.0 | 102.0 | 103.0 | 127.1 |
| 10. | 117. | . 0 | -12.0 | -13.0 | 117.1 | 102.0 | 103.0 | 127.1 |
| 15. | 113. | . 0 | -12.0 | -13.0 | 118.3 | 102.0 | 103.0 | 127.1 |
| 20. | 109. | . 0 | -12.0 | -13.0 | 119.6 | 102.0 | 103.0 | 127.1 |
| 25. | 105. | . 0 | -12.0 | -13.0 | 120.9 | 102.0 | 103.0 | 127.1 |
| 30. | 101. | . 0 | -12.0 | -13.0 | 122.3 | 102.0 | 103.0 | 127.1 |
| 35. | 97. | . 0 | -12.0 | -13.0 | 123.9 | 102.0 | 103.0 | 127.1 |
| 40. | 93. | . 0 | -12.0 | -13.0 | 125.5 | 102.0 | 103.0 | 127.1 |
| 45. | 89. | . 0 | -12.0 | -13.0 | 127.2 | 102.0 | 103.0 | 127.1 |
| 50. | 84. | . 0 | -12.0 | -13.0 | 129.0 | 102.0 | 103.0 | 127.1 |
| 55. | 80. | . 0 | -12.0 | -13.0 | 130.9 | 102.0 | 103.0 | 127.1 |
| 60. | 76. | . 0 | -12.0 | -13.0 | 133.0 | 102.0 | 103.0 | 127.1 |
| 65. | 72. | . 0 | -12.0 | -13.0 | 135.1 | 102.0 | 103.0 | 127.1 |
| 70. | 68. | . 0 | -12.0 | -13.0 | 137.5 | 102.0 | 103.0 | 127.1 |
| 75. | 64. | . 0 | -12.0 | -13.0 | 139.9 | 102.0 | 103.0 | 127.1 |
| 80. | 60. | . 0 | -12.0 | -13.0 | 142.5 | 102.0 | 103.0 | 127.1 |
| 85. | 56. | . 0 | -12.0 | -13.0 | 145.3 | 102.0 | 103.0 | 127.1 |
| 90. | 53. | . 0 | -12.0 | -13.0 | 148.2 | 102.0 | 103.0 | 127.1 |
| 95. | 49. | . 0 | -12.0 | -13.0 | 151.3 | 102.0 | 103.0 | 127.1 |
| 100. | 46. | . 0 | -9.5 | -9.5 | 154.4 | 102.0 | 103.0 | 127.1 |
| 105. | 43. | . 0 | -8.8 | -8.8 | 157.6 | 102.0 | 103.0 | 127.1 |
| 110. | 40. | . 0 | -8.0 | -8.0 | 160.7 | 102.0 | 103.0 | 127.1 |
| 115. | 38. | . 0 | -7.4 | -7.4 | 163.6 | 101.8 | 103.0 | 127.1 |
| 120. | 36. | . 0 | -6.8 | -6.8 | 166.1 | 103.3 | 103.0 | 127.1 |
| 125. | 34. | . 0 | -6.4 | -6.4 | 168.0 | 104.5 | 103.0 | 127.1 |
| 130. | 34. | . 0 | -6.2 | $-6.2$ | 169.1 | 105.2 | 103.0 | 127.1 |
| 135. | 33. | . 0 | -6.1 | -6.1 | 169.3 | 105.3 | 103.0 | 127.1 |
| 140. | 34. | . 0 | -6.3 | -6.3 | 168.5 | 104.8 | 103.0 | 127.1 |
| 145. | 35. | . 0 | -6.7 | -6.7 | 166.8 | 103.8 | 103.0 | 127.1 |
| 150. | 37. | . 0 | -7.2 | -7.2 | 164.5 | 102.3 | 103.0 | 127.1 |
| 155. | 39. | . 0 | -7.8 | -7.8 | 161.7 | 100.6 | 103.0 | 127.1 |
| 160. | 41. | . 0 | -8.4 | -8.4 | 159.2 | 102.0 | 103.0 | 127.1 |
| 165. | 43. | . 0 | -8.8 | -8.8 | 157.3 | 102.0 | 103.0 | 127.1 |
| 170. | 44. | . 0 | -9.2 | -9.2 | 155.9 | 102.0 | 103.0 | 127.1 |
| 175. | 45. | . 0 | -9.3 | -9.3 | 155.1 | 102.0 | 103.0 | 127.1 |
| 180. | 45. | . 0 | -9.4 | -9.4 | 154.9 | 102.0 | 103.0 | 127.1 |
| 185. | 45. | . 0 | -9.3 | -9.3 | 155.1 | 102.0 | 103.0 | 127.1 |
| 190. | 44. | . 0 | -9.2 | -9.2 | 155.9 | 102.0 | 103.0 | 127.1 |
| 195. | 43. | . 0 | -8.8 | -8.8 | 157.3 | 102.0 | 103.0 | 127.1 |
| 200. | 42. | . 0 | -8.6 | -8.6 | 158.4 | 102.0 | 103.0 | 127.1 |
| 200. | . | . 0 | -8.4 | -8.4 | 159.0 | 102.0 | 103.0 | 127.1 |

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| $\begin{array}{r} \text { SACRAMENTO, CA } \\ 38 \quad 3440.5 \\ 121 \quad 2930.2 \end{array}$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AZ | DISC | HOR ANG | 4 GHZ | 6GHZ | 4GHZ | 6GHz | RAIN 4 | RAIN 6 |
| DEG | DEG | DEGREES | HOR GAIN | HOR GAIN | COORD KM | COORD KM | SCAT KM | SCAT KM |
| 210. | 41. | . 0 | -8.4 | -8.4 | 159.1 | 102.0 | 103.0 | 127.1 |
| 215. | 42. | . 0 | -8.5 | -8.5 | 158.6 | 102.0 | 103.0 | 127.1 |
| 220. | 43. | . 0 | -8.8 | -8.8 | 157.6 | 102.0 | 103.0 | 127.1 |
| 225. | 44. | . 0 | -9.1 | -9.1 | 156.2 | 102.0 | 103.0 | 127.1 |
| 230. | 46. | . 0 | -9.5 | -9.5 | 154.4 | 102.0 | 103.0 | 127.1 |
| 235. | 48. | . 0 | -10.0 | -10.0 | 152.4 | 102.0 | 103.0 | 127.1 |
| 240. | 50. | . 0 | -12.0 | -13.0 | 150.2 | 102.0 | 103.0 | 127.1 |
| 245. | 53. | . 0 | -12.0 | -13.0 | 147.9 | 102.0 | 103.0 | 127.1 |
| 250. | 56. | . 0 | -12.0 | -13.0 | 145.6 | 102.0 | 103.0 | 127.1 |
| 255. | 59. | . 0 | -12.0 | -13.0 | 143.3 | 102.0 | 103.0 | 127.1 |
| 260. | 62. | . 0 | -12.0 | -13.0 | 141.0 | 102.0 | 103.0 | 127.1 |
| 265. | 66. | . 0 | -12.0 | -13.0 | 138.9 | 102.0 | 103.0 | 127.1 |
| 270. | 69. | . 0 | -12.0 | -13.0 | 136.8 | 102.0 | 103.0 | 127.1 |
| 275. | 73. | . 0 | -12.0 | -13.0 | 134.7 | 102.0 | 103.0 | 127.1 |
| 280. | 76. | . 0 | -12.0 | -13.0 | 132.8 | 102.0 | 103.0 | 127.1 |
| 285. | 80. | . 0 | -12.0 | -13.0 | 131.0 | 102.0 | 103.0 | 127.1 |
| 290. | 84. | . 0 | -12.0 | -13.0 | 129.3 | 102.0 | 103.0 | 127.1 |
| 295. | 88. | . 0 | -12.0 | -13.0 | 127.6 | 102.0 | 103.0 | 127.1 |
| 300. | 91. | . 0 | -12.0 | -13.0 | 126.0 | 102.0 | 103.0 | 127.1 |
| 305. | 95. | . 0 | -12.0 | -13.0 | 124.6 | 102.0 | 103.0 | 127.1 |
| 310. | 99. | . 0 | -12.0 | $-13.0$ | 123.2 | 102.0 | 103.0 | 127.1 |
| 315. | 103. | . 0 | -12.0 | -13.0 | 121.8 | 102.0 | 103.0 | 127.1 |
| 320. | 106. | . 0 | -12.0 | -13.0 | 120.6 | 102.0 | 103.0 | 127.1 |
| 325. | 110. | . 0 | -12.0 | -13.0 | 119.4 | 102.0 | 103.0 | 127.1 |
| 330. | 113. | . 0 | -12.0 | -13.0 | 118.3 | 102.0 | 103.0 | 127.1 |
| 335. | 117. | . 0 | -12.0 | -13.0 | 117.3 | 102.0 | 103.0 | 127.1 |
| 340. | 120. | . 0 | -12.0 | -13.0 | 116.3 | 102.0 | 103.0 | 127.1 |
| 345. | 123. | . 0 | -12.0 | -13.0 | 115.4 | 102.0 | 103.0 | 127.1 |
| 350. | 126. | . 0 | -12.0 | -13.0 | 114.6 | 102.0 | 103.0 | 127.1 |
| 355. | 129. | . 0 | -12.0 | -13.0 | 114.0 | 102.0 | 103.0 | 127.1 |
| 360. | 125. | 0 | -12.0 | -13.0 | 114.9 | 102.0 | 103.0 | 127.1 |

MULTICOMM SCIENCES INTERNATIONAL, INC.
Denville,NJ 07834 (973)-627-7400

# Multicomm Sciences Int'I, Inc 

# FREQUENCY COORDINATION REPORT 

# 4 AND 6 GHZ TRANSMIT-RECEIVE EARTH STATION 

## THE CALIFORNLA CHANNEL

SACRAMENTO, CA

MAY 3, 2004

## 1. CONCLUSIONS

An Interference Study considering all existing, proposed and prior coordinated microwave facilities within the coordination contours of the proposed Earth Station demonstrates that this site will operate satisfactorily with the Microwave Environment as defined on the frequency coordination data sheet.

## 2. SUMMARY OF RESULTS

There were no potential great circle interference cases at 4 GHz All of the potential great cirlce interference cases at 6 GHz were found to be acceptable on the basis that harmful interference will not likely result from the proposed operation, considering the criteria, the potential interference receive levels, and the total propagation losses.

There were no reported cases of rain scatter beam intersections.

## 3. SUPPLEMENTAL SHOWING

The Satellite Earth station proposed in this Application was coordinated by Multicomm Sciences International, Inc., Frequency Coordinators Group, ușing computer techniques and in accordance with Parts 25 and 101 of the FCC Rules and Regulations.

## 4. FREOUENCY COORDINATION DATA

Frequency Coordination Data which is attached, contains the following:
Technical Characteristics of Proposed Earth Station
Horizon Antenna Gain Plot
Discrimination Angle Plot
Local Horizon Plot
Satellite Elevation Plot
4 and 6 GHz Coordination Contour
4 and 6 GHz Rain Scatter

## 5. FREQUENCY COORDINATION STATEMENT (FCC PART 101)

Holders of licenses, permittees, prior filed applicants or planners of 6 GHz transmitting stations were notified on March 26, 2004 of the proposed Earth Station technical details in accordance with Section 25.203 (c-2) of the FCC Rules and Regulations. Satisfactory coordination was achieved on the basis that harmful interference would not occur, or that sufficient terrestrial blocking exists.

## AT\&T

AT\&T Wireless Services
Cagal Cellular Communications
Napa Cellular Telphone
Bay Area Cellular Telephone
Citizens Communications Services
GTE Mobilnet of California LP
Marin County of California
Pacific Gas and Electric
Sonoma County California
Ubiquitel BCS
Pacific Bell
Sacramento Valley LP
Loral Spacecom DBA Loral Skynet
MCI Network Services
Sacramento Municipal Utility District
Western States Teleport
Union Pacific Railroad
California, State of
Corban Communications
6. Certification of Person Responsible for Preparing Frequency Coordination Information Submitted in this Application

I hereby certify that I am the technically qualified person responsible for preparation of the frequency coordination information contained in this application; that I am familiar with Parts 101 and 25 of the Commission's Rules;
that I have either prepared or reviewed the frequency coordination information submitted in this application; and, that it is complete and accurate to the best of my knowledge.

## SATELLITE EARTH STATION FREQUENCY COORDINATION DATA 03/22/04

```
COMPANY NAME:
EARTH STATION LOCATION:
LATITUDE (DMS):
LONGITUDE (DMS) :
SITE GROUND ELEVATION (FT. AMSL):
ANTENNA CENTER LINE( FT)
ANTENNA TYPE:
    ANTENNA DIAMETER(METERS) :
    4 GHZ ANTENNA GAIN(DBI):
    15 DB HALF BEAMWIDTH(DEG):
    6 GHZ ANTENNA GAIN (DBI):
    15 DB HALF BEAMWIDTH(DEG):
OPERATING MODE:
    RECEIVE BAND(MHZ):
    TRANSMIT BAND (MHZ) :
EMISSION DESIGNATOR
MODULATION:
MAX. AVAILABLE RF POWER(DBW/4KHZ):
    (DBW/3MHZ):
MAX. EIRP
(DBW/4 KHZ):
(DBW/3MHZ):
62.
MAX. PERMISSIBLE INTERFERENCE POWER
```

4 GHZ 208 (DBW)
$4 \mathrm{GHZ} 0.0100 \%$ (DBW)
$6 \mathrm{GHZ} 20 \%$ (DBW/4KHZ)
$6 \mathrm{GHZ} 0.0025 \%$ (DBW/4KHZ)

SATELLITE ARC (MIN/MAX) AZ IMUTH ELEVATION

RADIO CLIMATE

RAIN ZONE
MAXIMUM GREAT CIRCLE COORDINATION DISTANCE (KM)


6 GHZ
361.4
115.0

PRECIPITATION SCATTER CONTOUR RADIUS(KM)
4 GHZ
6 GHz
-128.0
$-156.0$
-154.0
$-131.0$

A

3
321.6
127.1

THE CALIFORNIA CHANNEL
SACRAMENTO, CA
383440.5 (NAD83)
1212930.2
21.0
125.0

PATRIOT
TXFCC-240CSC
2.4
38.4
3.30
42.4
2.10
$T / R$
3700-4200
5925-6425
3M00G1F

DIGITAL
$-8.75$
20.0
33.65
62.4

88/140 DEG
133.3/208.2 DEG
33.5/41.3 DEG

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Denville,NJ 07834 (973)-627-7400

SACRAMENTO, CA
$\begin{array}{lll}38 & 34 & 40.5\end{array}$
1212930.2

| AZ | DISC | HOR ANG | 4GHZ | 6GHZ | 4 GHZ | 6GHZ | RAIN 4 | RAIN 6 <br> SCAT KM |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DEG | DEG | degrees | HOR GAIN | HOR GAIN | COORD KM | COORD KM | SCAT KM | SCAT KM |
| 5. | 121. | . 0 | -12.0 | -13.0 | 247.6 | 102.0 | 321.6 | 127.1 |
| 10. | 117. | . 0 | -12.0 | -13.0 | 250.0 | 102.0 | 321.6 | 127.1 |
| 15. | 113. | . 0 | -12.0 | -13.0 | 252.6 | 102.0 | 321.6 | 127.1 |
| 20. | 109. | . 0 | -12.0 | -13.0 | 255.3 | 102.0 | 321.6 | 127.1 |
| 25. | 105. | . 0 | -12.0 | -13.0 | 258.1 | 102.0 | 321.6 | 127.1 |
| 30. | 101. | . 0 | -12.0 | -13.0 | 261.2 | 102.0 | 321.6 | 127.1 |
| 35. | 97. | . 0 | -12.0 | -13.0 | 264.4 | 102.0 | 321.6 | 127.1 |
| 40. | 93. | . 0 | -12.0 | -13.0 | 267.9 | 102.0 | 321.6 | 127.1 |
| 45. | 89. | . 0 | -12.0 | -13.0 | 271.5 | 102.0 | 321.6 | 127.1 |
| 50. | 84. | . 0 | -12.0 | -13.0 | 275.4 | 102.0 | 321.6 | 127.1 |
| 55. | 80. | . 0 | $-12.0$ | -13.0 | 279.5 | 102.0 | 321.6 | 127.1 |
| 60. | 76. | . 0 | -12.0 | -13.0 | 283.9 | 102.0 | 321.6 | 127.1 |
| 65. | 72. | . 0 | -12.0 | -13.0 | 288.6 | 102.0 | 321.6 | 127.1 |
| 70. | 68. | . 0 | -12.0 | -13.0 | 293.5 | 102.0 | 321.6 | 27.1 |
| 75. | 64. | . 0 | -12.0 | -13.0 | 298.8 | 102.0 | 321.6 | 127.1 |
| 80. | 60. | . 0 | -12.0 | -13.0 | 304.3 | 102.0 | 321.6 | 127.1 |
| 85. | 56. | . 0 | -12.0 | -13.0 | 310.3 | 102.0 | 321.6 | 127.1 |
| 90. | 53. | . 0 | -12.0 | -13.0 | 316.5 | 100.7 | 321.6 | 127.1 |
| 95. | 49. | . 0 | -12.0 | -13.0 | 323.0 | 102.8 | 321.6 | 127.1 |
| 100. | 46. | . 0 | -9.5 | -9.5 | 329.7 | 104.9 | 321.6 | 127.1 |
| 105. | 43. | . 0 | -8.8 | -8.8 | 336.5 | 107.1 | 321.6 | 127.1 |
| 110. | 40. | . 0 | -8.0 | -8.0 | 343.1 | 109.2 | 321.6 | 127.1 |
| 115. | 38. | . 0 | -7.4 | -7.4 | 349.3 | 111.2 | 321.6 | 127.1 |
| 120. | 36. | . 0 | -6.8 | -6.8 | 354.7 | 112.9 | 321.6 | 127.1 |
| 125. | 34. | . 0 | -6.4 | -6.4 | 358.8 | 114.2 | 321.6 | 127.1 |
| 130. | 34. | . 0 | -6.2 | -6.2 | 361.1 | 114.9 | 321.6 | 127.1 |
| 135. | 33. | . 0 | -6.1 | -6.1 | 361.4 | 115.0 | 321.6 | 127.1 |
| 140. | 34. | . 0 | -6.3 | -6.3 | 359.7 | 114.5 | 321.6 | 127.1 |
| 145. | 35. | . 0 | -6.7 | -6.7 | 356.2 | 113.3 | 321.6 | 127.1 |
| 150. | 37. | . 0 | -7.2 | -7.2 | 351.1 | 111.7 | 321.6 | 127.1 |
| 155. | 39. | . 0 | -7.8 | -7.8 | 345.2 | 109.8 | 321.6 | 127.1 |
| 160. | 41. | . 0 | -8.4 | -8.4 | 339.9 | 108.2 | 321.6 | 127.1 |
| 165. | 43. | . 0 | -8.8 | -8.8 | 335.8 | 106.9 | 321.6 | 127.1 |
| 170. | 44. | . 0 | -9.2 | -9.2 | 332.9 | 105.9 | 321.6 | 127.1 |
| 175. | 45. | . 0 | -9.3 | -9.3 | 331.2 | 105.4 | 321.6 | 127.1 |
| 180. | 45. | . 0 | -9.4 | -9.4 | 330.7 | 105.2 | 321.6 | 127.1 |
| 185. | 45. | . 0 | -9.3 | -9.3 | 331.2 | 105.4 | 321.6 | 127.1 |
| 190. | 44. | . 0 | -9.2 | -9.2 | 333.0 | 105.9 | 321.6 | 127.1 |
| 195. | 43. | . 0 | -8.8 | -8.8 | 335.7 | 106.8 | 321.6 | 127.1 |
| 200. | 42. | . 0 | -8.6 | -8.6 | 338.2 | 107.6 | 321.6 | 127.1 |
| 205. | 41. | . 0 | -8.4 | -8.4 | 339.5 | 108.0 | 321.6 | 127.1 |

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SACRAMENTO, CA
383440.5
1212930.2

| AZ | DISC | HOR ANG | 4 GHZ | 6GHZ | 4 GHZ | 6GHZ | RAIN 4 | RAIN 6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DEG | DEG | DEGREES | HOR GAIN | HOR GAIN | COORD KM | COORD KM | SCAT KM | SCAT KM |
| 210. | 41. | . 0 | -8.4 | -8.4 | 339.7 | 108.1 | 321.6 | 127.1 |
| 215. | 42. | . 0 | -8.5 | -8.5 | 338.7 | 107.8 | 321.6 | 127.1 |
| 220. | 43. | . 0 | -8.8 | -8.8 | 336.6 | 107.1 | 321.6 | 127.1 |
| 225. | 44. | . 0 | -9.1 | -9.1 | 333.5 | 106.1 | 321.6 | 127.1 |
| 230. | 46. | . 0 | -9.5 | -9.5 | 329.7 | 104.9 | 321.6 | 127.1 |
| 235. | 48. | . 0 | -10.0 | -10.0 | 325.3 | 103.5 | 321.6 | 127.1 |
| 240. | 50. | . 0 | -12.0 | -13.0 | 320.6 | 102.0 | 321.6 | 127.1 |
| 245. | 53. | . 0 | -12.0 | -13.0 | 315.8 | 100.5 | 321.6 | 127.1 |
| 250. | 56. | . 0 | -12.0 | -13.0 | 310.8 | 102.0 | 321.6 | 127.1 |
| 255. | 59. | . 0 | -12.0 | -13.0 | 305.9 | 102.0 | 321.6 | 127.1 |
| 260. | 62. | . 0 | $-12.00$ | -13.0 | 301.1 | 102.0 | $\because 321.6$ | 127.1 |
| 265. | 66. | . 0 | -12.0 | -13.0 | 296.5 | 102.0 | 321.6 | 127.1 |
| 270. | 69. | . 0 | -12.0 | -13.0 | 292.0 | 102.0 | 321.6 | 127.1 |
| 275. | 73. | . 0 | -12.0 | -13.0 | 287.7 | 102.0 | 321.6 | 127.1 |
| 280. | 76. | . 0 | -12.0 | -13.0 | 283.6 | 102.0 | 321.6 | 127.1 |
| 285. | 80. | . 0 | -12.0 | -13.0 | 279.7 | 102.0 | 321.6 | 127.1 |
| 290. | 84. | . 0 | -12.0 | -13.0 | 276.0 | 102.0 | 321.6 | 127.1 |
| 295. | 88. | . 0 | -12.0 | -13.0 | 272.4 | 102.0 | 321.6 | 127.1 |
| 300. | 91. | . 0 | -12.0 | -13.0 | 269.1 | 102.0 | 321.6 | 127.1 |
| 305. | 95. | . 0 | -12.0 | -13.0 | 265.9 | 102.0 | 321.6 | 127.1 |
| 310. | 99. | . 0 | -12.0 | -13.0 | 262.9 | 102.0 | 321.6 | 127.1 |
| 315. | 103. | . 0 | -12.0 | -13.0 | 260.1 | 102.0 | 321.6 | 127.1 |
| 320. | 106. | . 0 | -12.0 | -13.0 | 257.4 | 102.0 | 321.6 | 127.1 |
| 325. | 110. | . 0 | -12.0 | -13.0 | 254.9 | 102.0 | 321.6 | 127.1 |
| 330. | 113. | . 0 | -12.0 | -13.0 | 252.6 | 102.0 | 321.6 | 127.1 |
| 335. | 117. | . 0 | -12.0 | -13.0 | 250.4 | 102.0 | 321.6 | 127.1 |
| 340. | 120. | . 0 | -12.0 | -13.0 | 248.3 | 102.0 | 321.6 | 127.1 |
| 345. | 123. | . 0 | -12.0 | -13.0 | 246.4 | 102.0 | 321.6 | 127.1 |
| 350. | 126. | . 0 | -12.0 | -13.0 | 244.7 | 102.0 | 321.6 | 127.1 |
| 355. | 129. | . 0 | -12.0 | -13.0 | 243.4 | 102.0 | 321.6 | 127.1 |
| 360. | 125. | . 0 | -12.0 | -13.0 | 245.4 | 102.0 | 321.6 | 127.1 |

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HORIZON ANTENNA GAIN PLOT 6 GHZ


HORIZON ANTENNA PLOT 4 GHZ


THE CALIFORNIA
SACRAMENTO. CA
$\begin{array}{llllllllllllllll}38 & 34 & 40 & N & 121 & 29 & & \end{array}$
MSI

LOCAL HORIZON PLOT



THE CALIFORNIA SACRAMENTO. CA
$\begin{array}{lllllllllllllllll}38 & 34 & 40 & N & 121 & 29 & 30 & W\end{array}$
MSI 03-30-2004




