

Radiation Hazard Analysis

Phased Array Earth Station Aboard Aircraft

Introduction

This analysis calculates the non-ionizing radiation levels for a SpaceX Services, Inc. (“SpaceX Services”) phased array earth station for use on moving aircraft (“ESAA”). The calculations performed in this analysis comply with the methods described in FCC Office of Engineering and Technology Bulletin, Number 65 (Edition 97-01) (“Bulletin 65”). This analysis demonstrates that SpaceX Services ESAs are compliant and will not result in exposure levels exceeding the applicable radiation hazard limits.

Bulletin 65 and Section 1.1310 of the Commission's rules specify two separate tiers of exposure limits: one for Occupational/Controlled Exposures and one for General Population/Uncontrolled Exposures. Limits for Occupational/Controlled Exposures apply in situations where persons are exposed as a consequence of their employment and are fully aware of and can control their exposure. These limits also apply in situations where a person is transient through a location where such limits would otherwise apply provided the person is made aware of the potential for exposure. The limits for General Population/Uncontrolled Exposure apply in situations in which the general public may be exposed, or in which persons that are exposed as a consequence of their employment may not be fully aware of the potential for exposure or cannot exercise control over their exposure. These ESAs will be installed on the top of commercial aircraft, well away from the public—whether on the airport tarmac (where the public is not allowed) or in flight. Accordingly, this analysis discusses only the Maximum Permissible Exposure (“MPE”) limit for Occupational/Controlled exposures, which for the Ku-band frequencies used by these ESAs is a power density equal to 5 mW/cm² averaged over a six-minute period.¹

SpaceX Services will ensure installation of ESAA terminals on aircraft by qualified installers who have an understanding of the antenna's radiation environment and the measures best suited to maximize protection of the persons operating the aircraft and equipment. In addition, to the extent an ESAA terminal exhibits radiation exposure levels exceeding 1.0 mW/cm² in accessible areas, such as at the exterior surface of the radome, it will have a label attached to the surface of the terminal warning about the radiation hazard and will include thereon a diagram showing the regions around the terminal where the radiation levels could exceed the maximum radiation exposure limit specified in 47 C.F.R. § 1.1310 Table 1.²

As described in the definitional section below, this report analyzes the maximum power density levels in the vicinity of an ESAA antenna in three regions: (1) the far field, (2) the near field, and (3) near the main reflector surface. These radiation regions were analyzed using the definitions and formulas in Bulletin 65 for aperture antennas. Note that the SpaceX Services ESAA is a flat phased array, such that the other region normally included in analyses for parabolic dishes (*i.e.*,

¹ See 47 C.F.R. § 1.1310(e).

² See 47 C.F.R. § 25.228(d).

between the main reflector and the feed) is not applicable in this case.³ The results of this analysis are summarized in Table 1, which identifies the potential exposure under worst-case operating conditions.

ESAA Description

The ESAA is a flat phased array capable of steering its beams to track NGSO satellites passing within its field of view. As the terminal steers the transmitting beam, it also adjusts the power to maintain a constant level at the receiving antenna of its target satellite to the extent possible, compensating for variations in antenna gain and path loss associated with the steering angle. At the phased array's equivalent of an "antenna flange," the highest transmit power is 4.06 W. There is no difference in transmit power between ESAAs at the center or edge of the spot or between clear sky or heavy rain conditions.

The ESAA transmits bursts of information at designated times that are assigned to the terminal by the network. The duty cycle of the uplink transmissions is controlled by the network and independently monitored by the software controlling the ESAA; this ensures that the transmit duty cycle of a terminal cannot exceed 33% under any circumstances.

Explanation of the Analysis

The "Calculated Values" in Table 1 are the exposure rates calculated using the formulae from Bulletin 65 for a system with continuous (100% transmit duty cycle) transmission. SpaceX Services ESAAs, however, transmit only short bursts of data periodically as instructed by the network and are neither designed for nor capable of continuous transmission. Therefore, in order to compute the effective radiated energy of a SpaceX Services ESAA, the terminal's maximum possible transmitter duty cycle has been used to adjust the values calculated using the Bulletin 65 methodology. Accordingly, the calculated figures reflect the total potential for human exposure based on the length of time that the ESAA transmits energy during a rolling six-minute period.

Results of Analysis

This analysis demonstrates that the SpaceX Services ESAA is not a radiation hazard because the terminal does not exceed the MPE limit of 5 mW/cm² averaged over a six-minute period.

Conclusion

This radiation hazard analysis demonstrates that SpaceX Services ESAAs will not result in exposure levels exceeding the applicable MPE limits.

³ Bulletin 65 also calls for consideration of the transition region between near field and far field. However, the power density in the transition region will be less than the maximum power density in the near field and more than the minimum power density in the far field for the purpose of evaluating potential exposure. Accordingly, if the analysis demonstrates compliance for both the near field and far field, it necessarily demonstrates compliance for the transition region.

Definitions

1) Far Field Region

The far field region extends outward from the antenna surface, beginning at a distance of $\frac{0.6D^2}{\lambda}$ meters where the D is the diameter of the antenna. The maximum power density is calculated using the equation recommended in Bulletin 65.

2) Near Field Region

The near field region is a volume co-incident with the direction of the main beam extending outward from the antenna surface the length of the near field $\frac{D^2}{4\lambda}$ meters.

3) Transition Region

The transition region is located between the near field region and the far field region. This region has a power density that decreases with increasing distance. Therefore, the power density in the transition region will be less than the maximum power density in the near field and more than the maximum power density in the far field for the purpose of evaluating potential exposure.

4) Region Near the Antenna Surface

The power density near the antenna surface can be estimated as equal to four times the power divided by the area of the main reflector surface (phased array illumination is uniform).

**TABLE 1: RADIATION FROM SPACEX SERVICES
PHASED ARRAY EARTH STATION ABOARD AIRCRAFT**

Input Parameters

Antenna Dimensions	$D = 0.48 \text{ m}$
Frequency	$f = 14.5 \text{ GHz}$
Max Power into antenna	$P_{max} = 4.06 \text{ W}$
Max EIRP	$EIRP_{max} = 6606.9 \text{ W}$ $10 \log(EIRP_{max}) = 38.2 \text{ dBW}$
Aperture efficiency [%]	$\eta = 56.7\%$
Maximum Transmit Duty Cycle	$DTx = 33 \%$

Calculated Values

Wavelength	$\lambda = \frac{c}{f} = 0.0207 \text{ m}$
Area of Reflector	$A = 0.181 \text{ m}^2$
Max Antenna Gain	$G_{max} = \frac{\eta 4\pi A}{\lambda^2} = 3012$ $10 \log(G_{max}) = 34.79 \text{ dB}$
Length of Near Field	$R_{nf} = \frac{D_1^2}{4\lambda} = 2.78 \text{ m}$
Beginning of Far Field	$R_{ff} = 0.6 \frac{D_1^2}{\lambda} = 6.68 \text{ m}$

Maximum Power Density Calculations

Power Density in Far Field	$S_{ff} = DTx \frac{EIRP_{max}}{4\pi R_{ff}^2} = 0.39 \frac{\text{mW}}{\text{cm}^2}$
Power Density in Near Field	$S_{nf} = DTx \frac{4\eta P_{max}}{A} = 1.68 \frac{\text{mW}}{\text{cm}^2}$
Power Density at Antenna Surface	$S_{ref} = DTx \frac{4P_{max}}{A} = 2.96 \frac{\text{mW}}{\text{cm}^2}$