## Supplement to Orbital Debris Assessment Report

Provided below are the responses of Hiber, Inc. ("Hiber") to questions from the International Bureau regarding the company's orbital debris assessment report ("ODAR").

## 1. Please provide the inputs/assumptions that were used in your orbital calculation software.

The first TLEs derived for Hiber-1 and Hiber-2 are presented below. They're used to baseline the initial parameters of the satellites.

```
HIBER-1
1 43744U 18096AB 18334.16184889 .00016808 00000-0 64911-3 0 9997
243744 97.4873 39.15320018371328.7415 122.9043 15.26180788 147
HIBER-2
1 43774U 18099S 18339.89354746 .00000485 00000-0 49943-4 0 9992
243774 97.7736 49.02470011038 250.1788 109.8235 14.94763969 316
```


## A. STELA

Hiber entered the following technical and orbital parameters into the STELA software program to produce its Orbital Debris Assessment Report:
A. 1 Orbital evolution from launch to end of year 3, the nominal end-of-mission life

| Parameter | Hiber 1 | Hiber 2 | Hiber 3-24 |
| :---: | :---: | :---: | :---: |
| Satellite mass | 7.5 kg | 7.5 kg | 5 kg |
| Reflecting area | 0.2315 m 2 | 0.2315 m 2 | 0.17025 m 2 |
| Reflectivity <br> coefficient | 1.5 | 1.5 | 1.5 |
| Drag area | 0.03405 m 2 | 0.03405 m 2 | 0.0658 m 2 |
| Drag coefficient | 2.2 | 2.2 | 2.2 |
| Atmospheric model | NRLMSISE-00 | NRLMSISE-00 | NRLMSISE-00 |
| Solar activity | Variable | Variable | Variable |
| Date | $11 / 29 / 2018$ | $12 / 03 / 2018$ | $10 / 01 / 2019$ |
| Perigee | 481.767 km | 582.559 km | 600 km |
| Apogee | 506.991 km | 597.926 km | 600 km |
| Inclination | $97.4873^{\circ}$ | $97.7736^{\circ}$ | $97.8^{\circ}$ |
| RAAN | $39.1532^{\circ}$ | $49.0247^{\circ}$ | $280^{\circ}$ |
| Argument of perigee | $328.7415^{\circ}$ | $250.1788^{\circ}$ | $0^{\circ}$ |
| Mean anomaly | $122.9043^{\circ}$ | $109.8235^{\circ}$ | $0^{\circ}$ |

A. 2 Orbital evolution from end of year 3 to atmospheric reentry

| Parameter | Hiber 1 | Hiber 2 | Hiber 3-24 |
| :---: | :---: | :---: | :---: |
| Satellite mass | 7.5 kg | 7.5 kg | 5 kg |
| Reflecting area | 0.2315 m 2 | 0.2315 m 2 | 0.17025 m 2 |
| Reflectivity <br> coefficient | 1.5 | 1.5 | 1.5 |
| Drag area | 0.1142 m 2 | 0.1142 m 2 | 0.0781 m 2 |
| Drag coefficient | 2.2 | 2.2 | 2.2 |
| Atmospheric model | NRLMSISE-00 | NRLMSISE-00 | NRLMSISE-00 |
| Solar activity | Variable | Variable | Variable |
| Date | $11 / 29 / 2021$ | $12 / 03 / 2021$ | $10 / 01 / 2022$ |
| Perigee | 457.39 km | 575.83 km | 577.34 km |
| Apogee | 505.62 km | 599.25 km | 584.38 km |
| Inclination | $97.40^{\circ}$ | $97.69^{\circ}$ | $97.8^{\circ}$ |
| RAAN | $47.67^{\circ}$ | $44.37^{\circ}$ | $281.74^{\circ}$ |
| Argument of perigee | $67.06^{\circ}$ | $191.28^{\circ}$ | $145.89^{\circ}$ |
| Mean anomaly | $0^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ |

## B. DRAMA

Hiber entered the following technical and orbital parameters into the DRAMA software program to produce its ODAR:

| Time | Parameter | Hiber-1 | Hiber-2 | Hiber 3-24 |
| :---: | :---: | :---: | :---: | :---: |
|  | Launch date | 11/29/18 | 12/03/18 | 10/01/19 |
|  | Lifetime | 3.89 years | 10.4 years | 11.66 years |
|  | Equivalent radius | 0.2335 m | 0.2335 m | 0.1931 m |
| $\begin{aligned} & 0 \\ & \frac{1}{\pi} \\ & \frac{1}{\sim} \end{aligned}$ | Semi-major axis (km) | 6872.38 | 6968.24 | 6978 |
|  | Eccentricity (mean value) | 0.002735 | 0.0023 | 0.001225 |
|  | Inclination ( ${ }^{\circ}$ ) | 97.49 | 97.77 | 97.8 |
|  | RAAN ( ${ }^{\circ}$ ) | 39.15 | 49.02 | 280 |
|  | Arg. of perigee ( ${ }^{\circ}$ ) | 328.74 | 250.18 | 0 |
| $\begin{aligned} & \text { ¡ } \\ & \frac{1}{\pi} \\ & \underset{\sim}{\sim} \end{aligned}$ | Semi-major axis (km) | 6871.08 | 6967.98 | 6977.12 |
|  | Eccentricity | 0.002675 | 0.002275 | 0.001245 |
|  | Inclination ( ${ }^{\circ}$ ) | 97.46 | 97.75 | 97.8 |
|  | RAAN ( ${ }^{\circ}$ ) | 42.89 | 48.68 | 279.84 |
|  | Arg. of perigee ( ${ }^{\circ}$ ) | 100.66 | 116.88 | 117.23 |
|  | Semi-major axis (km) | 6869.15 | 6967.59 | 6972.96 |
|  | Eccentricity | 0.00265 | 0.002275 | 0.00126 |
|  | Inclination ( ${ }^{\circ}$ ) | 97.43 | 97.72 | 97.8 |
|  | RAAN ( ${ }^{\circ}$ ) | 45.50 | 47.11 | 280.02 |
|  | Arg. of perigee ( ${ }^{\circ}$ ) | 253.77 | 26.70 | 55.76 |
| Loss of satellite control |  |  |  |  |
| $\begin{aligned} & \text { m } \\ & \frac{1}{\pi} \\ & \underset{\sim}{\sim} \end{aligned}$ | Semi-major axis (km) | 6859.51 | 6965.54 | 6958.86 |
|  | Eccentricity | 0.00247 | 0.002235 | 0.001275 |
|  | Inclination ( ${ }^{\circ}$ ) | 97.40 | 97.69 | 97.8 |
|  | RAAN ( ${ }^{\circ}$ ) | 47.67 | 44.37 | 281.74 |


|  | Arg．of perigee（ ${ }^{\circ}$ ） | 67.06 | 191.28 | 145.89 |
| :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \pm \\ & \frac{\pi}{0} \\ & \underset{\sim}{\sim} \end{aligned}$ | Semi－major axis（km） |  | 6946.06 | 6933.50 |
|  | Eccentricity |  | 0.001945 | 0.001295 |
|  | Inclination（ ${ }^{\circ}$ ） |  | 97.65 | 97.79 |
|  | RAAN（ ${ }^{\circ}$ ） |  | 42.00 | 287.05 |
|  | Arg．of perigee（ ${ }^{\circ}$ ） |  | 85.51 | 96.37 |
| $\begin{aligned} & \text { n } \\ & \stackrel{\rightharpoonup}{0} \\ & \stackrel{\rightharpoonup}{\sim} \end{aligned}$ | Semi－major axis（km） |  | 6917.13 | 6904.31 |
|  | Eccentricity |  | 0.0016 | 0.00128 |
|  | Inclination（ ${ }^{\circ}$ ） |  | 97.62 | 97.77 |
|  | RAAN（ ${ }^{\circ}$ ） |  | 42.36 | 296.90 |
|  | Arg．of perigee（ ${ }^{\circ}$ ） |  | 317.56 | 60.48 |
| $\begin{aligned} & 0 \\ & \stackrel{0}{0} \\ & \stackrel{y}{x} \end{aligned}$ | Semi－major axis（km） |  | 6883.53 | 6881.04 |
|  | Eccentricity |  | 0.00126 | 0.00127 |
|  | Inclination（ ${ }^{\circ}$ ） |  | 97.58 | 97.74 |
|  | RAAN（ ${ }^{\circ}$ ） |  | 46.89 | 310.47 |
|  | Arg．of perigee（ ${ }^{\circ}$ ） |  | 98.74 | 101.94 |
|  | Semi－major axis（km） |  | 6853.40 | 6863.02 |
|  | Eccentricity |  | 0.001215 | 0.001255 |
|  | Inclination（ ${ }^{\circ}$ ） |  | 97.55 | 97.70 |
|  | RAAN（ ${ }^{\circ}$ ） |  | 55.78 | 326.37 |
|  | Arg．of perigee（ ${ }^{\circ}$ ） |  | 114.42 | 79.40 |
| $\stackrel{\infty}{\frac{\infty}{む}}$ | Semi－major axis（km） |  | 6823.98 | 6849.88 |
|  | Eccentricity |  | 0.00123 | 0.001255 |
|  | Inclination（ ${ }^{\circ}$ ） |  | 97.54 | 97.67 |
|  | RAAN（ ${ }^{\circ}$ ） |  | 69.12 | 343.46 |
|  | Arg．of perigee（ ${ }^{\circ}$ ） |  | 73.97 | 89.91 |
| $\begin{aligned} & \text { on } \\ & \frac{1}{む 凶} \\ & \end{aligned}$ | Semi－major axis（km） |  | 6792.77 | 6838.36 |
|  | Eccentricity |  | 0.001205 | 0.0012525 |
|  | Inclination（ ${ }^{\circ}$ ） |  | 97.54 | 97.65 |
|  | RAAN（ ${ }^{\circ}$ ） |  | 87.80 | 1.42 |
|  | Arg．of perigee（ ${ }^{\circ}$ ） |  | 112.58 | 108.79 |
| $\begin{aligned} & \text { O} \\ & \stackrel{1}{\varpi} \\ & \stackrel{\rightharpoonup}{\sim} \end{aligned}$ | Semi－major axis（km） |  | 6734.91 | 6824.57 |
|  | Eccentricity |  | 0.001105 | 0.00124 |
|  | Inclination（ ${ }^{\circ}$ ） |  | 97.56 | 97.65 |
|  | RAAN（ ${ }^{\circ}$ ） |  | 114.96 | 21.21 |
|  | Arg．of perigee（ ${ }^{\circ}$ ） |  | 96.85 | 75.82 |
| $\begin{aligned} & \underset{\sim}{7} \\ & \vdots \\ & \stackrel{y}{\varpi} \end{aligned}$ | Semi－major axis（km） |  |  | 6795.99 |
|  | Eccentricity |  |  | 0.001165 |
|  | Inclination（ ${ }^{\circ}$ ） |  |  | 97.67 |
|  | RAAN（ ${ }^{\circ}$ ） |  |  | 45.25 |
|  | Arg．of perigee（ ${ }^{\circ}$ ） |  |  | 99.69 |

2. Specifically, please provide the area-to-mass of the satellites (1\&2) as they are during their operational lifetimes.

During the lifetime of the satellites, the cross-sectional area and area-to-mass of each of the satellites during nominal operations are 0.03405 m 2 and $4.54 \times 10-3 \mathrm{~m} 2 / \mathrm{kg}$, respectively.
3. Please provide EOL configurations for each satellite, to include detailed physical orientation.

The satellites have a nominal three-year operational lifetime. At end-of-life ("EOL"), the satellites will be put into safe mode: all the systems will be shut down, except for the onboard computer ("OBC"), telemetry, tracking and command ("TT\&C"), electrical power subsystem ("EPS") and attitude determination and control subsystem ("ADCS"). The satellites will be rotated to place the solar panels in the Ram facing direction. This will result in a cross-sectional area of 0.2315 m 2 and an area-to-mass ratio of $0.0309 \mathrm{~m} 2 / \mathrm{kg}$. This orientation will be maintained as long as the systems are working.

However, some subsystems might not be working at EOL, and it may not be possible to control the satellite's attitude. Accordingly, for purpose of this ODAR, Hiber has assumed a worst-case scenario and assumed that the satellite will begin tumbling immediately at the end of the nominal three-year operational lifetime.

In that situation, the satellite would spin around each of the three axes. Therefore, we can assume that each face of the satellite will be RAM facing at some point. The average crosssectional area and area-to-mass ratio for the three faces is 0.1142 m 2 and $0.0152 \mathrm{~m} 2 / \mathrm{kg}$, respectively. These average values were used to calculate orbital decay.

Provided below are minor corrections to the ODAR to reflect more precise technical and orbital parameters. The corrected text are underlined and in bold. Additionally, Figures 2 and 3 should replace the respective figures in the ODAR.

## Section 3.1

Description of the launch and deployment profile, including all parking, transfer, and operational orbits with apogee, perigee, and inclination:

Hiber-1 was launched into an orbit with a perigee at 481.8 km , apogee at $\underline{507.0} \mathrm{~km}$ and a $97.5^{\circ}$ inclination. Hiber-2 was launched into an orbit with a perigee at $\underline{582.6}$ km , apogee at $\underline{\mathbf{5 9 7 . 9}} \mathrm{km}$ and inclination at $97.8^{\circ}$.

## Section 3.2

Total spacecraft mass at launch, including all propellants and fluids: $\underline{7.5} \mathrm{~kg}$
Dry mass of spacecraft at launch, excluding solid rocket motor propellants: 7.5 kg

## Section 3.5

| Collision probability | Hiber-1 | Hiber-2 | Hiber 3-24 |
| :---: | :---: | :---: | :---: |
| Year 0-1 | $0.1908 \times 10-4$ | $0.3183 \times 10-4$ | $0.3117 \times 10-4$ |
| Year 1-2 | $0.2001 \times 10-4$ | $0.3632 \times 10-4$ | $0.3464 \times 10-4$ |
| Year 2-3 | $0.2378 \times 10-4$ | $0.3122 \times 10-4$ | $0.3604 \times 10-4$ |
| Year 3-4 | $0.1912 \times 10.4$ | $0.3164 \times 10-4$ | $0.2445 \times 10-4$ |
| Year 4-5 |  | 0.2256 $\times 10-4$ | $0.2287 \times 10-4$ |
| Year 5-6 |  | $0.2191 \times 10-4$ | $0.1968 \times 10-4$ |
| Year 6-7 |  | $0.2510 \times 10-4$ | $0.2481 \times 10-4$ |
| Year 7-8 |  | $0.1606 \times 10-4$ | $0.1926 \times 10-4$ |
| Year 8-9 |  | $0.1081 \times 10-4$ | $0.1571 \times 10-4$ |
| Year 9-10 |  | $0.6721 \times 10-5$ | $0.1381 \times 10-4$ |
| Year 10-11 |  | $0.3676 \times 10-6$ | $0.1152 \times 10-4$ |
| Year 11-12 |  |  | $0.6951 \times 10-5$ |
| Total | $\underline{0.8199 \times 10-4}$ | $2.3454 \times 10-4$ | $2.60911 \times 10-4$ |

Table 5: Annual collision probabilities
The total collision probability for both Hiber-1 and Hibert-2 is $\mathbf{3 . 1 6 5 3 \times 1 0 - 4}$, which is under the 0.001 threshold.

When considering the 24 satellite system the total collision probability becomes $\mathbf{6 . 0 5 6 6 \mathbf { x }}$ 10-3, thus exceeding the 0.001 threshold. However, the 223 U satellites, for which Hiber will submit a separate ODAR, are expected to be equipped with propulsion modules. The propulsion modules will enable Hiber to conduct collision avoidance maneuvers as needed, thus mitigating the possibility of collision.

Section 3.6
Description of spacecraft disposal option selected: The spacecraft will decay because of atmospheric drag and de-orbit naturally via atmospheric re-entry.

Simulations were run on CNES' STELA software to assess how long it would take for the satellites to effectuate an atmospheric reentry.

Results show that that it will take Hiber- $\mathbf{1} \mathbf{0 . 8 9}$ years and Hiber- $\mathbf{2} \mathbf{7 . 4}$ years to reenter the atmosphere, after a 3 -year nominal mission life. This is compliant with the guidelines that specify that satellites de-orbiting through atmospheric reentry do so within 25 years of the satellite's end-of-life. The results are demonstrated in Figures 2 and 3.


Figure 2: Hiber-1 altitude evolution


Figure 3: Hiber-2 altitude evolution
Calculation of the area-to-mass ratio after postmission disposal, if the controlled reentry option is not selected: See the response to Question 3 above.

## Technical Certification

I, Maarten Engelen, hereby certify that I am the technically qualified person responsible for the preparation of the engineering information contained in the foregoing supplement to the orbital debris assessment report of Hiber, Inc. I have either prepared or reviewed the engineering information submitted in the supplement, and it is complete and accurate to the best of my knowledge and belief.

Maarten Engelen
Program Executive/Project Manager
Hiber, Inc.

Dated: March 15, 2019

