Engineering Statement

Intelsat License LLC ("Intelsat") proposes to relocate its Intelsat 702 ("IS 702") spacecraft to 33.0° E.L. and to operate from that location. The spacecraft will utilize the frequency bands 5925 – 6425 MHz, 14000 – 14500 MHz, 3700 – 4200 MHz, 10950 – 11200 MHz, 11450 – 11700 MHz and 12500 – 12750 MHz to provide service to Europe, Africa, and Asia.¹ Intelsat 702 will be collocated with Intelsat New Dawn, which currently operates at 32.8° E.L.

Intelsat also requests that the Part 25 waivers originally granted to the Intelsat 702 spacecraft continue to apply at the 33.0° E.L. location, namely, the waivers of Sections $25.202(g)$, $25.210(a)(1)$, $25.210(a)(3)$, $25.210(i)(1)$ and $25.211(a)$ of the Commission's rules.²

In April 2009, the Commission granted Intelsat authorization to operate Intelsat 702 from 66.0° E.L. (see FCC File No.: SAT-MOD-20081217-00233). The Commission subsequently granted a Special Temporary Authority ("STA") to Intelsat to relocate and operate Intelsat 702 at 47.5° E.L. Currently the satellite is operating from 47.5° E.L. as authorized under a Special Temporary Authority (see FCC File No.: SAT-STA-20120416-00068). As part of its overall satellite fleet management, Intelsat now proposes to relocate Intelsat 702 from 47.5° E.L. to 33.0° E.L.

This engineering statement provides and updates, as appropriate, the following technical information for Intelsat 702: (1) frequency plan (2) beam performance and gain contours, (3) emission designators, (4) power flux density calculations, (5) link budget analysis, (6) adjacent satellite link analysis, (7) Schedule S information and (8) orbital debris mitigation plan. In all other respects, the characteristics of Intelsat 702 are the same as those described in SAT-MOD-20081217-00233.

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¹ Intelsat 702 also has the capability to transmit in the $11700 - 11950$ MHz frequency band; however, this capability will not be utilized from the proposed orbital location.

² See Applications of Intelsat LLC for Authority to Operate and Further Construct, Launch, and Operate C-Band and Ku-Band Satellites that Form a Global Communications System in Geostationary Orbit, 15 FCC Rcd 15460, 15529 (Appendix C)(2000)(Memorandum Opinion and Order and Authorization), *recon. denied*, 15 FCC Rcd 25234(2000)(Order on Reconsideration).

1.0) Frequency Plan

The Intelsat 702 frequency and polarization plan is provided in Exhibit 1. The plan details all of the transponder combinations , channel bandwidths and channel gains. The channel gain for the transponders were calculated using the specific parameters for each transponder.

2.0) Gain Contours

The co-polarized coverage patterns of Intelsat 702 operating from 33.0º E.L. are shown in Exhibit 2. The peak antenna gain, G/T, SFD ("Saturaturation Flux Density") and EIRP levels for each uplink and downlink beam, as appropriate, are also provided in these exhibits.

Given that the cross-polarization isolation performance of Intelsat 702 with respect to the axis of each satellite beam will not change as a result of the proposed relocation of Intelsat 702 to 33.0° E.L., no cross-polarization patterns are provided herein.

3.0) Emission Designators

Emission designators and allocated bandwidths for representative communication carriers are provided in Exhibit 3.

4.0) Power Flux Density Levels

The power flux density ("PFD") limits for space stations operating in the 3650 – 4200 MHz, 10950 – 11200 MHz and 11450 – 11700 MHz bands are contained in section 25.208 of the Commission's rules. With respect to the 12500 – 12750 MHz bands, the PFD limits are specified in No. 21.16 of the ITU Radio Regulations.

The maximum PFD levels for the Intelsat 702 transmissions were calculated for a number of TV/FM and digital carriers listed in Exhibit 3 operating in the 3700 – 4200 MHz, 10950 – 11200 MHz, 11450 – 11700 MHz and 12500 – 12750 MHz bands. These carriers were chosen because they generally produce high PFD levels on the Earth's surface. The maximum PFD levels for the Intelsat 702 telemetry and uplink power control beacons were also calculated. The results are provided in Exhibit 4 and show that the downlink power flux density levels of the Intelsat 702 carriers do not exceed the limits specified in section 25.208 of the Commission's rules or No. 21.16 of the ITU Radio Regulations.

5.0) Link Budgets and Interference Analysis

Link analysis for Intelsat 702 was conducted for a number of representative carriers at C- and Ku-band frequencies. For the analysis in C-Band, it was assumed that the nearest satellites to Intelsat 702 were a hypothetical satellite operating at 31.0 $^{\circ}$ E.L. and a hypothetical satellite operating at 35.0 $^{\circ}$ E.L.³ The uplink power density of emissions for each of the hypothetical satellites was assumed to be -38.7 dBW/Hz, the maximum level specified in section 25.212(d)(2) of the Commission's rules for digital C-Band carriers. At C-band, the maximum downlink EIRP density of each of the hypothetical satellites was assumed to be -32 dBW/Hz. All other operational parameters for the hypothetical satellites were assumed be the same as Intelsat 702.

For the 12500 – 12750 MHz band analysis, it was assumed that the nearest satellites to Intelsat 702 were Astra 1G, located at 31.5º E.L., and a hypothetical satellite located at 35.0° E.L.⁴ The hypothetical satellite was assumed to have the same characteristics as Intelsat 702. The maximum uplink power density of emissions for each of these satellites was assumed to be -45 dBW/Hz.

Astra 1G utilizes the downlink frequencies spanning 11700 - 12750 MHz to provide service to Eastern and Western Europe using two Ku-band beams. It was assumed that this satellite utilized the uplink frequency band of 14000 – 14500 MHz.⁵ The maximum EIRP of the Astra 1G downlink beams is 52 dBW with a channel bandwidth of 26 MHz.⁶ The maximum downlink EIRP density of the Astra 1G carriers was assumed to be -21.4 dBW (corresponding to the maximum EIRP of 52 dBW being evenly distributed within an occupied bandwidth of 21.7 MHz). No beam isolation was considered between Astra 1G and Intelsat 702 due to the fact that the Intelsat 702 Ku-Band utilizes steerable beams.

For the hypothetical satellite at 35.0º E.L. in Ku-Band, the downlink EIRP density was assumed to be -20 dBW/Hz. All other operational parameters were assumed to be the same as those specified for Intelsat 702.

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³ Arabsat 2B is located at 34 $^{\circ}$ E.L. and has the capability to operate in the 5925 – 6425 MHz, 3700 – 4200 MHz, 13750 – 14000 MHz and 12500 – 12750 MHz bands. However, the operational status of this satellite is unknown and for the purposes of the link budget analysis was not considered.

⁴ *Supra* footnote 3.

 $⁵$ No information was available for the Astra 1G uplink beams.</sup>

⁶ Both the maximum EIRP and minimum channel bandwidth for Astra 1G were obtained from The Satellite Encyclopedia website (http://www.tbs-satellite.com/tse/online/sat astra 1g html).

For the $10950 - 11200$ MHz and $11450 - 11700$ MHz band analysis, it was assumed that the nearest satellites to Intelsat 702 were a hypothetical satellite located at 31.5° E.L. and a hypothetical satellite located at 35.0° E.L. The hypothetical satellites were assumed to be identical to Intelsat 702 and operated with a maximum downlink EIRP density of -20.0 dBW/Hz. The maximum uplink power density of -45 dBW/Hz was assumed for each of these satellites.

Other assumptions made for the link budget analysis were as follows:

- a) In the plane of the geostationary satellite orbit, all transmitting and receiving earth station antennas have off-axis co-polar gains that are compliant with the limits specified in section $25.209(a)(1)$ and $25.209(a)(2)$ of the FCC's rules.
- b) All transmitting and receiving earth stations have a cross-polarization isolation value of at least 30 dB within their main beam lobe.
- c) At C-band frequencies, degradation due to rain is not considered, given that rain (attenuation) effects are insignificant at C-band.
- d) At Ku-band frequencies, rain attenuation predictions are derived using Recommendation ITU-R P.618.
- e) At Ku-band frequencies, increase in noise temperature of the receiving earth station due to rain is taken into account.
- f) For the cases where the transponder operates in a multi-carrier mode, the effects due to intermodulation interference are taken into account.

The impact of the TV/FM carriers from the adjacent satellites at 31.0° E.L, 31.5º E.L, and 35.0º E.L on the transmissions of Intelsat 702 was not considered due to the fact that TV/FM carriers are known to be high-density carriers with most of the energy contained within the near vicinity of the carrier center frequency. Operation of sensitive narrow-band carriers is typically precluded within these high power density areas of the TV/FM carrier. Accordingly, placement and operation of TV/FM carriers are normally achieved through internal coordination and/or coordination discussions with the adjacent satellite operator, whichever may be the case, rather than through C/I calculations – since the results of such calculations would show that narrow-band carriers typically could not operate on a co-frequency basis with TV/FM carriers.

As shown in Exhibit 1, the Intelsat 702 beam connectivities are extensive. In order to keep the number of Intelsat 702 link calculations to a manageable number, worst-case performance values were assumed for each beam type. The worst-case beam parameters were derived from the beam parameters listed in Exhibit 2 and chosen in such a manner that would make carrier links utilizing any specific

uplink/downlink beam combination as sensitive to adjacent satellite interference as possible. This would ensure that the link performance objectives would be achieved for all possible Intelsat 702 uplink/downlink beam combinations. The worst-case beam performance for each Intelsat 702 beam type is provided below:

Table 1: Worst-Case Beam Performance

As shown in Exhibit 1, Intelsat 702 utilizes beam channels having varying bandwidths. In an effort to keep the number of link calculations to a manageable level, link calculations were not performed for each channel size, but rather for largest channel size for each possible beam combination. Also, link budgets for the C- band to Ku-band and the Ku-band to C-band transponders are not shown since the results are an amalgamation of the results of the C-band and Ku-band analyses.

As previously mentioned, at Ku-band, Intelsat 702 can utilize the downlink frequency bands of 10950 - 11200 MHz, 11450 - 11700 MHz and 12500 - 12750

MHz. In order to keep the number the Intelsat 702 link calculations to a manageable number, all Ku-band link calculations were conducted at the single representative uplink frequency of 14250 MHz and downlink frequency of 11950 MHz (that is approximately midway between 10950 MHz and 12750 MHz). At Cband, all calculations were conducted at the single representative frequency of 6175 MHz for the uplink and 3950 MHz for the downlink.

The results of the C-band and Ku-band analyses are shown in Exhibit 5 and demonstrate that operation of the Intelsat 702 satellite from 33.0º E.L. would permit the intended services to achieve their respective performance objectives while maintaining sufficient link margin. Additionally, the EIRP density levels of the carriers listed in Exhibit 5 comply with the FCC limits contained in section $25.212(c)$ and $25.212(d)$ of the Commission's rules.

It is noted that Intelsat has an agreement in place with Eutelsat with respect to its operation at 33.1° E.L. Intelsat 702 operations will be conducted in accordance with the terms of the coordination agreement with Eutelsat, as well as other applicable agreements (with other satellite operators).

6.0) Adjacent Satellite Link Analysis

At C-band, the impact of the Intelsat 702 emissions on a hypothetical satellite located at 31.0º E.L. and a hypothetical satellite located 35.0º E.L. was analyzed. The hypothetical satellites were assumed to have the same operating characteristics as Intelsat 702. All calculations were conducted at the single representative frequency of 6175 MHz for the uplink and 3950 MHz for the downlink. As with the Intelsat 702 link budgets, link calculations for the hypothetical satellites at 31° E.L. and 29° E.L. were performed only for the largest channel bandwidth applicable to the particular uplink-downlink beam combination. The results of the analysis are found in Exhibits 6 and 7.

For the hypothetical satellite at 31.0º E.L., it was assumed that the nearest cofrequency satellites were Intelsat 702 at 33.0º E.L. and a hypothetical satellite located at 29.0 $^{\circ}$ E.L.⁷ The hypothetical satellite located at 29.0 $^{\circ}$ E.L. was assumed to have the same operational characteristics as Intelsat 702. The maximum uplink power density of the carriers transmitted to Intelsat 702 and the hypothetical satellite at 29.0 \degree E.L. was assumed to be -38.7 dBW/Hz, the maximum level

<u>.</u> ⁷ Arabsat 5A is located at 30.5 ° E.L but was not used in the C-Band analysis of the hypothetical 31.0 ° E.L satellite since the two satellites are separated only by 0.5º and would not effectively show the impact of adjacent satellite interference in a 2º environment.

specified in section 25.212(d)(2) of the Commission's rules for digital C-band carriers. On downlink, the Intelsat 702 transmissions and those of the hypothetical satellite located at 29.0° E.L. were assumed to have a maximum EIRP density of - 32 dBW/Hz.

For the hypothetical satellite at 35.0º E.L., it was assumed that the nearest cofrequency satellites were Intelsat 702 at 33.0º E.L. and a hypothetical satellite located at 37.0 $^{\circ}$ E.L.⁸ The hypothetical satellite located at 37.0 $^{\circ}$ E.L. was assumed to have the same operational characteristics as Intelsat 702. The maximum uplink power density of the carriers transmitted to Intelsat 702 and the hypothetical satellite located at 37.0° E.L. was assumed to be -38.7 dBW/Hz, the maximum level specified in section 25.212(d)(2) of the Commission's rules for digital Cband carriers. On downlink, the Intelsat 702 transmissions and those of the hypothetical satellite located at 37.0° E.L. were assumed to have a maximum EIRP density of -32 dBW/Hz.

In the 12500 – 12700 MHz band, the impact of the Intelsat 702 emissions on Astra 1G located at 31.5º E.L. and a hypothetical satellite located at 35.0º E.L. were analyzed. The results of the analysis are found in Exhibits 7 and 8.

Astra 1G has two linearly polarized Ku-band beams covering Eastern and Western Europe. Both beams have identical downlink characteristics and it was assumed that the uplink characteristics were also identical. Consequently, only one Astra 1G representative beam was used in the link analysis to illustrate the impact of the Intelsat 702 emissions. It was assumed that the Astra 1G beam uplink beam had a beam peak G/T of 9.8 dB/K with a beam peak saturation flux density ranging from -93.2 to -79.2 dBW/m^2 . Astra 1G downlink beams can transmit with a maximum EIRP of 52 dBW between 11700 and 12750 MHz and utitlize transponders that have a bandwidth of 26 MHz between the frequencies 11700 and 12500 MHz and 33 MHz between the frequencies 12500 and 12750 MHz.

For Astra 1G at 31.5º E.L., it was assumed that the nearest co-frequency satellites were Intelsat 702 at 33.0° E.L. and a hypothetical satellite located at 29.5° E.L.¹⁰ The hypothetical satellite at 29.5° E.L. was assumed to have the same

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⁸ *See supra* n. 3.

 9 Intelsat was unable to obtain information pertaining to the SFD and G/T performance of Astra 1G uplink beams. Accordingly, it was assumed that the Astra 1G uplink beam performance was the same as the Intelsat 702 Ku-band Spot beam as specified in section 5.0 of this Engineering Statement.

¹⁰ Arabsat 5A is located at 30.5 ° E.L but was not used in the Ku-band analysis of Astra 1G at 31.5 ° E.L since the two satellites are separated by 1.0º and would not effectively show the impact of adjacent satellite interference in a 2º environment.

characteristics as Astra 1G. It was assumed that the uplink EIRP transmitted to both adjacent satellites was -45 dBW/Hz. It was assumed that the maximum downlink EIRP density of Intelsat 702 was -20 dBW/Hz. The downlink EIRP density of the hypothetical satellite located at 29.5º E.L was assumed to be -21.4 dBW/Hz.

For the 10950 – 11200 MHz and 11450 – 11700 MHz band analysis, a hypothetical satellite identical to Intelsat 702 was assumed to be operating at 31.5° E.L. The nearest satellites to the hypothetical satellite at 31.5° E.L. were assumed to be a hypothetical satellite identical to Intelsat 702 located at 29.5° E.L. and Intelsat 702 located at 33.0° E.L. Intelsat 702 and the hypothetical satellite at 29.5 \degree E.L. were assumed to operate with a maximum uplink power density of -45.0 dBW/Hz and a maximum downlink EIRP density of -20.0 dBW/Hz. The results of the analysis are provided in Exhibit 8.

At Ku-band, the hypothetical satellite located at 35.0º E.L. was assumed to have the same operating characteristics as the Intelsat 702 Ku-band. The nearest cofrequency satellites to the hypothetical satellite at 35.0° E.L. satellite were assumed to be Intelsat 702 and a hypothetical satellite located at 37.0° E.L.¹¹ It was assumed that the uplink EIRP transmitted to both adjacent satellites was -45 dBW/Hz. It was also assumed that Intelsat 702 and the hypothetical satellite located at 37.0° E.L. operated with a maximum downlink EIRP density transmitted of -20 dBW/Hz. The results of the analysis are provided in Exhibit 7.

The results of the C- and Ku-band analysis are listed in Exhibits 6 through 8. The Intelsat 702 transmissions will be limited to those levels contained in Sections 25.212(c) and (d), as applicable, unless higher levels are coordinated with affected adjacent satellite operators. In any case, the uplink power density of the Intelsat 702 digital carriers operating in the $5925 - 6425$ MHz and $14000 - 14500$ MHz band will not exceed -38.7 dBW/Hz and -45 dBW/Hz, respectively; and within the 3700 – 4200 MHz band the downlink EIRP density of the Intelsat 702 digital carriers will not exceed -32 dBW/Hz; and within the $10950 - 11200$ MHz, $11450 -$ 11700 MHz, and 12500 – 12750 MHz bands the downlink EIRP density of the Intelsat 702 digital carriers will not exceed -20 dBW/Hz.

 \overline{a} ¹¹ Arabsat 2B is located at 34° E.L. and has the capability to operate in the 5925 – 6425 MHz, 3700 – 4200 MHz, 13750 – 14000 MHz and 12500 – 12750 MHz bands. However, the operational status of this satellite is unknown and for the purposes of the link budget analysis was not considered. Eutelsat 36A and 36B at 36.0 º E.L. were not used in the Ku-band analysis of the hypothetical 35.0 º E.L satellite since the satellites are only by 1.0º away and would not effectively show the impact of adjacent satellite interference in a 2º environment.

7.0) Schedule S Submission

Intelsat is providing with its application a Schedule S for the operations of Intelsat 702 from 33.0º E.L. The Schedule S contains only those Intelsat 702 data items that have changed as a result of the proposed modification and data items whose inclusion was required in order for the software application to function properly.

In column "g" of section S13 of the Schedule S, a link budget file has been included for the first link (i.e. the first of row of data) contained in that section. This link budget file is applicable to all of the links listed in section S13 and should have been included with each row of data in that section of the Schedule S. However, given that the link budget file is rather large and its inclusion with each link (or data row) would lead to the Schedule S file having an unmanageable size, all other links (or rows of data) contain a small ASCII file that references the link budget file that is attached to the first link (*i.e.*, the link budget file attached to the first row of data).

8.0) Orbital Debris Mitigation Plan

Intelsat is proactive in ensuring safe operation and disposal of this and all spacecraft under its control. The four elements of debris mitigation are addressed below.

8.1) Spacecraft Hardware Design: The spacecraft is designed such that no debris will be released during normal operations. Intelsat has assessed the probability of collision with meteoroids and other small debris (<1 cm diameter) and has taken the following steps to limit the effects of such collisions: (1) critical spacecraft components are located inside the protective body of the spacecraft and properly shielded; and (2) all spacecraft subsystems have redundant components to ensure no single-point failures. The spacecraft does not use any subsystems for end-oflife disposal that are not used for normal operations.

8.2) Minimizing Accidental Explosions: Intelsat has assessed the probability of accidental explosions during and after completion of mission operations. The spacecraft is designed in a manner to minimize the potential for such explosions. Propellant tanks and thrusters are isolated using redundant valves and electrical power systems are shielded in accordance with standard industry practices. At the completion of the mission, and upon disposal of the spacecraft, Intelsat will ensure the removal of all stored energy on the spacecraft by depleting all propellant tanks, venting all pressurized systems, and turning off all active units.

8.3) Safe Flight Profiles: Intelsat has assessed and limited the probability of the space station becoming a source of debris as a result of collisions with large debris or other operational space stations. Intelsat is not aware of any other FCC licensed system, or any other system applied for and under consideration by the FCC, having an overlapping station-keeping volume with Intelsat 702. Intelsat is also not aware of any non-Intelsat system with an overlapping station-keeping volume with Intelsat 702 that is the subject of an ITU filing and that is progressing towards launch. 12

8.4) Post Mission Disposal: At the end of the mission, Intelsat expects to dispose of the spacecraft by moving it to a planned minimum altitude of 150 kilometers (perigee) above the geostationary arc ¹³ Nevertheless, as the Commission is aware, because there is no mechanism for precisely calculating the amount of fuel left on the spacecraft once it is in orbit, it is possible that the spacecraft will not meet the planned minimum de-orbit altitude.

In its Second Report and Order in IB Docket 02-54 (FCC Document Number: 04- 130), the FCC declared that satellites launched prior to March 18, 2002, such as Intelsat 702, would be designated as grandfathered satellites not subject to a specific disposal altitude. Therefore, the Intelsat 702 planned disposal orbit complies with the FCC's rules.

In addition, Intelsat provides the following information:

- 1) Planned orbital eccentricity: 1.7846E-04 (This is a best estimate of optimal eccentricity to match the natural eccentricity circle due to Sun and Moon perturbations after decommission.¹⁴)
- 2) Planned apogee altitude: 165 km^{15}

 \overline{a} ¹² Eutelsat operates the Eutelsat 33A spacecraft at the orbital location of 33.1° E.L. As best as can be determined, the position of this spacecraft is maintained to within ±0.05º of this orbital location. Consequently, there would be no overlap of the station-keeping volumes of Intelsat 702 and Eutelsat 33A.

 13 Intelsat has reserved 30.22 kilograms of fuel for this purpose. The fuel gauging uncertainty has been taken into account in these calculations.

¹⁴ Because it is extremely difficult to anticipate end-of-life thruster performance and operational conditions, it is extremely difficult to achieve the planned eccentricity. Intelsat's priority is to achieve the planned minimum perigee of 150 kilometers. In order to achieve the planned eccentricity, not only must there be sufficient propellant reserved but, in addition, individual thrusters must be fired at specific times during satellite decommissioning because the timing of thruster firing will affect eccentricity. Due to difficulties in predicting the thruster end-of-life performance, as well as earth station availability and visibility as the satellite drifts, it may not be possible to fire the right thrusters at the optimal times. Thus, optimal eccentricity may not be achieved, which, in turn, will affect the apogee altitude.

¹⁵ *See supra* n. 2.

3) Information concerning the methods that will be used to assess and provide adequate margins concerning fuel gauging uncertainty: For the Intelsat 702 spacecraft, in addition to the nominal hold-back and reserves provided to us by the manufacturer, Intelsat propulsion engineers review the current propellant usage – particularly the mixing ratio – to properly allocate sufficient margin to account for unavailable propellant that may result from a non-optimal mixing ratio. In addition, Intelsat performs thermal gauging near the spacecraft's end of life by inferring the remaining propellant from the thermal signature when Intelsat applies heat to different parts of the propellant tank system. This information is considered when determining the additional hold-back and adjustments to book values to attempt to ensure sufficient propellant to achieve the planned minimum altitude. There are, however, many uncertainties to both methods that could lead to incorrect conclusions regarding remaining fuel.

Certification Statement

I hereby certify that I am a technically qualified person and am familiar with Part 25 of the Commission's Rules and Regulations. The contents of this engineering statement were prepared by me or under my direct supervision and to the best of my knowledge are complete and accurate.

/s/ Abdolmajid Khalilzadeh October 1, 2012

Abdolmajid Khalilzadeh Date Intelsat Senior Principle Engineer Spectrum Strategy

Exhibit 1: Frequency and Beam Assignments

Note:

H: Linear horizontal polarization V: Linear vertical polarization

RHCP: Right hand circular polarization
LHCP: Left hand circular polarization

Exhibit 2: Gain Contours

Exhibit 2-1: C-Band Global A Uplink Beam

[Schedule S Beam Designation: GAUL]

Beam Peak Gain: 20.3 dBi Beam Polarization: Left Hand Circular Beam Peak G/T: -7.0 dB/K Saturated Flux Density @ Beam Peak G/T: -93.3 to -79.3 dBW/m²

Exhibit 2-2: C-Band Global A Downlink Beam

[Schedule S Beam Designation: GADL]

Beam Peak Gain: 20.5 dBi Beam Polarization: Right Hand Circular Beam Peak EIRP: 32.4 dBW

Exhibit 2-3: C-Band Global B Uplink Beam

[Schedule S Beam Designation: GBUL]

Beam Peak Gain: 20.3 dBi Beam Polarization: Right Hand Circular Beam Peak G/T: -7.0 dB/K Saturated Flux Density @ Beam Peak G/T: -93.2 to -79.2 dBW/m²

Exhibit 2-4: Global B Downlink Beam

[Schedule S Beam Designation: GBDL]

Beam Peak Gain: 20.5 dBi Beam Polarization: Left Hand Circular Beam Peak EIRP: 31.6 dBW

Exhibit 2-5: C-Band Spot A Uplink Beam

[Schedule S Beam Designation: CAUL]

Beam Peak Gain: 30.3 dBi Beam Polarization: Left Hand Circular Beam Peak G/T: 3.0 dB/K Saturated Flux Density @ Beam Peak G/T: -95.8 to -81.8 dBW/m²

Exhibit 2-6: C-Band Spot A Downlink Beam

[Schedule S Beam Designation: CADL]

Beam Peak Gain: 27.5 dBi Beam Polarization: Right Hand Circular Beam Peak EIRP: 39.5 dBW

Exhibit 2-7: C-Band Spot B Uplink Beam

[Schedule S Beam Designation: CBUL]

Beam Peak Gain: 30.3 dBi Beam Polarization: Right Hand Circular Beam Peak G/T: 3.0 dB/K Saturated Flux Density @ Beam Peat G/T: -96.3 to -82.3 dBW/m²

Exhibit 2-8: C-Band Spot B Downlink Beam

[Schedule S Beam Designation: CBDL]

Beam Peak Gain: 27.5 dBi Beam Polarization: Left Hand Circular Beam Peak EIRP: 38.6 dBW

Exhibit 2-9: C-Band West Hemi Uplink Beam

[Schedule S Beam Designation: WHUL]

Beam Peak Gain: 23.2 dBi Beam Polarization: Left Hand Circular Beam Peak G/T: -3.5 dB/K Saturated Flux Density @ Beam Peat G/T: -91.8 to -77.8 dBW/m²

Exhibit 2-10: C-Band West Hemi Downlink Beam

[Schedule S Beam Designation: WHDL]

Beam Peak Gain: 24.5 dBi Beam Polarization: Right Hand Circular Beam Peak EIRP: 37.5 dBW

Exhibit 2-11: C-Band East Hemi Uplink Beam

[Schedule S Beam Designation: EHUL]

Beam Peak Gain: 25.9 dBi Beam Polarization: Left Hand Circular Beam Peak G/T: -1.5 dB/K Saturated Flux Density @ Beam Peat G/T: -91.4 to -77.4 dBW/m²

Exhibit 2-12: C-Band East Hemi Downlink Beam

[Schedule S Beam Designation: EHDL]

Beam Peak Gain: 27.2 dBi Beam Polarization: Right Hand Circular Beam Peak EIRP: 38.9dBW

Exhibit 2-13: C-Band Northwest Zone Uplink Beam

[Schedule S Beam Designation: NWUL]

Beam Peak Gain: 25.6 dBi Beam Polarization: Right Hand Circular Beam Peak G/T: -1.5 dB/K Saturated Flux Density @ Beam Peat G/T: -92.4 to -78.4 dBW/m²

Exhibit 2-14: C-Band Northwest Downlink Beam

[Schedule S Beam Designation: NWDL]

Beam Peak Gain: 26.9dBi Beam Polarization: Left Hand Circular Beam Peak EIRP: 36.9 dBW

Exhibit 2-15: C-Band Southeast Zone Uplink Beam

[Schedule S Beam Designation: SEUL]

Beam Peak Gain: 26.8 dBi Beam Polarization: Right Hand Circular Beam Peak G/T: -0.7 dB/K Saturated Flux Density @ Beam Peat G/T: -92.9 to -78.9 dBW/m²

Exhibit 2-16: C-Band Southeast Downlink Beam

[Schedule S Beam Designation: SEDL]

Beam Peak Gain: 28.7 dBi Beam Polarization: Left Hand Circular Beam Peak EIRP: 39.5 dBW

Exhibit 2-17: C-Band Northeast Zone Uplink Beam

[Schedule S Beam Designation: NEUL]

Beam Peak Gain: 27.8 dBi Beam Polarization: Right Hand Circular Beam Peak G/T: 0.3 dB/K Saturated Flux Density @ Beam Peat G/T: -90.2 to -76.2 dBW/m²

Exhibit 2-18: C-Band Northeast Downlink Beam

[Schedule S Beam Designation: NEDL]

Beam Peak Gain: 30.8 dBi Beam Polarization: Left Hand Circular Beam Peak EIRP: 39.2 dBW

Exhibit 2-19: C-Band Southwest Zone Uplink Beam

[Schedule S Beam Designation: SWUL]

Beam Peak Gain: 27.8 dBi Beam Polarization: Right Hand Circular Beam Peak G/T: 0.4 dB/K Saturated Flux Density @ Beam Peat G/T: -90.3 to -76.3 dBW/m²

Exhibit 2-20: C-Band Southwest Downlink Beam

[Schedule S Beam Designation: SWDL]

Beam Peak Gain: 30.8 dBi Beam Polarization: Left Hand Circular Beam Peak EIRP: 37.2 dBW

Exhibit 2-21: C-Band Combined Northwest and Southeast Zone Uplink Beam

[Schedule S Beam Designation: X1UL]

Beam Peak Gain: 22.7 dBi Beam Polarization: Right Hand Circular Beam Peak G/T: -5.0 dB/K Saturated Flux Density @ Beam Peat G/T: -91.1 to -77.1 dBW/m²

Exhibit 2-22: C-Band Combined Northeast and Southwest Zone Uplink Beam

[Schedule S Beam Designation: X2UL]

Beam Peak Gain: 24.3 dBi Beam Polarization: Right Hand Circular Beam Peak G/T: -3.6 dB/K Saturated Flux Density @ Beam Peat G/T: -88.8 to -74.8 dBW/m²

Exhibit 2-23: Ku-Band Spot 1 Uplink Beam

[Schedule S Beam Designation: S1UL]

Beam Peak Gain: 36.9 dBi Beam Polarization: Horizontal Beam Peak G/T: 9.3 dB/K Saturated Flux Density @ Beam Peat G/T: -92.6 to -78.6 dBW/m²

Exhibit 2-24: Ku-Band Spot 1 Downlink Beam

[Schedule S Beam Designation: S1DL]

Beam Peak Gain: 36.2 dBi

Exhibit 2-25: Ku-Band Spot 2 Uplink Beam

[Schedule S Beam Designation: S2UL]

Beam Peak Gain: 34.8 dBi Beam Polarization: Vertical Beam Peak G/T: 6.9 dB/K Saturated Flux Density @ Beam Peat G/T: -92.8 to -78.8 dBW/m²

Exhibit 2-26: Ku-Band Spot 2 Downlink Beam

[Schedule S Beam Designation: S2DL]

Beam Peak Gain: 34.8 dBi Beam Polarization: Horizontal Beam Peak EIRP: 49.6 dBW

Exhibit 2-27: Ku-Band Spot 2A Uplink Beam

[Schedule S Beam Designation: S2AU]

Beam Peak Gain: 32.9 dBi Beam Polarization: Vertical Beam Peak G/T: 5.0 dB/K Saturated Flux Density @ Beam Peat G/T: -92.9 to -78.9 dBW/m²

Exhibit 2-28: Ku-Band Spot 2A Downlink Beam

[Schedule S Beam Designation: S2AD]

Beam Peak Gain: 32.7 dBi Beam Polarization: Horizontal Beam Peak EIRP: 47.7 dBW

Exhibit 2-29: Ku-Band Spot 3 Uplink Beam

[Schedule S Beam Designation: S3UL]

Beam Peak Gain: 37.8 dBi Beam Polarization: Horizontal Beam Peak G/T: 9.8 dB/K Saturated Flux Density @ Beam Peat G/T: -93.2 to -79.2 dBW/m²

[Schedule S Beam Designation: S3DL]

Beam Peak Gain: 36.6 dBi Beam Polarization: Vertical Beam Peak EIRP: 51.5 dBW

Note: This beam can also be operated in a low power mode with a corresponding beam peak EIRP of 50.7 dBW.

Exhibit 2-31: Command Uplink Beam
[Schedule S Beam Designation: CMD]

Peak Beam Gain: 8.3 dBi Polarization: Left Hand Circular Peak G/T: -28.5 dB/K Command Threshold Flux Density @ Peak G/T: -107.4 dBW/m²

Peak Beam Gain: 16.5 dBi Polarization: Right Hand Circular
Peak EIRP: 8.2 dBW

Exhibit 2-33: Back-up Telemetry Downlink Beam

[Schedule S Beam Designation: TLMB]

Peak Beam Gain: -5.3 dBi Polarization: Right Hand Circular
Peak EIRP: 0.7 dBW

Exhibit 2-34: C-Band Uplink Power Control Downlink Beam

[Schedule S Beam Designation: BNC]

Peak Beam Gain: 10.7 dBi Polarization: Linear Vertical Peak EIRP: 11.7 dBW

Exhibit 2-35: Ku-Band Uplink Power Control Global Downlink Beams

[Schedule S Beam Designation: BNK1, BNK2]

Peak Beam Gain: 16.7 dBi Polarization: Right Hand Circular Peak EIRP: 8.0 dBW

Ku-Band Uplink Power Control Spot 1 Downlink Beams

[Schedule S Beam Designation: BNK3, BNK8]

Peak Beam Gain: 36.2 dBi

Exhibit 2-36: Ku-Band Uplink Power Control Spot 2 Downlink Beams

[Schedule S Beam Designation: BNK4, BNK9]

Peak Beam Gain: 34.5 dBi Polarization: Linear Horizontal Peak EIRP: 10.3 dBW

Exhibit 2-37: Ku-Band Uplink Power Control Spot 2A Downlink Beams

[Schedule S Beam Designation: BNK5, BNK10]

Peak Beam Gain: 32.7 dBi Polarization: Linear Horizontal Peak EIRP: 8.5 dBW

Exhibit 2-38: Ku-Band Uplink Power Control Spot 3 Downlink Beams

[Schedule S Beam Designation: BNK6, BNK11]

Peak Beam Gain: 36.6 dBi Polarization: Linear Vertical Peak EIRP: 12.3 dBW

Exhibit 3: EMISSION DESIGNATORS

Exhibit 4: POWER FLUX DENSITY CALCULATIONS

Exhibit 4-1: C-Band PFD Calculations

Exhibit 4-2: Ku-Band (10.95-11.2 GHz & 11.45-11.70 GHz) PFD Calculations

* This is the maximum allowable EIRP level at the specified elevation angle. The actual EIRP level of the beam at
this particular elevation angle will be made to be equal to or lower than the value listed in the table thro

*This is the maximum allowable EIRP level at the specified elevation angle. The actual EIRP level of the beam at this particular elevation angle will be made to be equal to or lower than the value listed in the table through reduction in
the output power of the channel and/or restriction on the movement/placement of the beam.

Exhibit 4-3: Ku-Band (12.50-12.75 GHz) PFD Calculations

*This is the maximum allowable EIRP level at the specified elevation angle. The actual EIRP level of the beam at this particular elevation angle will be made to be equal to or lower than the value listed in the table through reduction in the output power of the channel and/or restriction on the movement/placement of the beam.

Exhibit 4-4: Ku-Band ULPC PFD Calculations

**Exhibit 5: IS-702 Link Budgets
Exhibit 5-1: C-Band Global Uplink/Global Downlink**

Exhibit 5-2: C-Band Global Uplink/C-Band Spot Downlink

Exhibit 5-3: C-Band Global Uplink/Hemi Downlink

Exhibit 5-4: C-Band Spot Uplink/C-Band Spot Downlink

Exhibit 5-5: C-Band Spot Uplink/Global Downlink

Exhibit 5-6: C-Band Spot Uplink/Hemi Downlink

Exhibit 5-7: C-Band Hemi Uplink/Hemi Downlink

Exhibit 5-8: C-Band Hemi Uplink/Zone Downlink

Exhibit 5-9: C-Band Hemi Uplink/Global Downlink

Exhibit 5-10: C-Band Hemi Uplink/C-Band Spot Downlink

Exhibit 5-11: C-Band Zone Uplink/Zone Downlink

Exhibit 5-12: C-Band Zone Uplink/Hemi Downlink

Exhibit 5-13: Ku-Band Spot Uplink/Ku-Band Spot Downlink 12.5-12.75 GHz

Exhibit 5-14: Ku-Band Spot Uplink/Ku-Band Spot Downlink 10.95-11.2 & 11.45-11.7 GHz

Exhibit 6 Adjacent Satellite 31.0° E.L. Link Budgets

Exhibit 6-1: 31.0° E.L. C-Band Global Uplink/Global Downlink

Exhibit 6-2: 31.0° E.L. C-Band Global Uplink/C-Band Spot Downlink

Exhibit 6-3: 31.0° E.L. C-Band Global Uplink/Hemi Downlink

Exhibit 6-4: 31.0° E.L. C-Band Spot Uplink/C-Band Spot Downlink

Exhibit 6-5: 31.0° E.L. C-Band Spot Uplink/Global Downlink

Exhibit 6-6: 31.0° E.L. C-Band Spot Uplink/Hemi Downlink

Exhibit 6-7: 31.0° E.L. C-Band Hemi Uplink/Hemi Downlink

Exhibit 6-8: 31.0° E.L. C-Band Hemi Uplink/Zone Downlink

Exhibit 6-9: 31.0° E.L. C-Band Hemi Uplink/Global Downlink

Exhibit 6-10: 31.0° E.L. C-Band Hemi Uplink/C-Band Spot Downlink

Exhibit 6-11: 31.0° E.L. C-Band Zone Uplink/Zone Downlink

Exhibit 6-12: 31.0° E.L. C-Band Zone Uplink/Hemi Downlink

Exhibit 7: Adjacent Satellite 35.0° E.L. Link Budgets

Exhibit 7-1: 35.0° E.L. C-Band Global Uplink/Global Downlink

Exhibit 7-2: 35.0° E.L. C-Band Global Uplink/C-Band Spot Downlink

Exhibit 7-3: 35.0° E.L. C-Band Global Uplink/Hemi Downlink

Exhibit 7-4: 35.0° E.L. C-Band Spot Uplink/C-Band Spot Downlink

Exhibit 7-5: 35.0° E.L. C-Band Spot Uplink/Global Downlink

Exhibit 7-6: 35.0° E.L. C-Band Spot Uplink/Hemi Downlink

Exhibit 7-7: 35.0° E.L. C-Band Hemi Uplink/Hemi Downlink

Exhibit 7-8: 35.0° E.L. C-Band Hemi Uplink/Zone Downlink

Exhibit 7-9: 35.0° E.L. C-Band Hemi Uplink/Global Downlink

Exhibit 7-10: 35.0° E.L. C-Band Hemi Uplink/C-Band Spot Downlink

Exhibit 7-11: 35.0° E.L. C-Band Zone Uplink/Zone Downlink

Exhibit 7-12: 35.0° E.L. C-Band Zone Uplink/Hemi Downlink

Exhibit 7-13: 35.0° E.L. Ku-Band

Exhibit 8: Adjacent Satellite 31.5°E.L. Link Budgets

Exhibit 8-1: Astra 1G 31.5 °E.L. 12.5 - 12.75 GHz Downlink

Exhibit 8-2: Hypothetical 31.5 ° E.L. 10.95-11.2 & 11.45-11.7 GHz

