# FCC ID: A3LSMS916U

# Power Density Simulation Report

Revision A

November 07, 2022

SAMSUNG ELECTRONICS

#### 1. Simulation methodology for Power Density (PD)

#### 1.1 Simulation tool

#### 1.1.1 Tool description

For the simulation approach to calculating power density (PD) evaluation for mobile phone with mmWave antenna modules, ANSYS Electromagnetics suite version 2022.R1 (HFSS) is used. ANSYS HFSS is one of several commercial tools for 3D full-wave electromagnetic simulation used for antenna and RF structure design of high frequency component. ANSYS Electromagnetics suite version 2022.R1 (HFSS) is implemented based on Finite Element Method (FEM), which operates in the frequency domain.

### 1.1.2 Mesh and Convergence criteria

To solve the PD analysis using FEM, volume area containing simulated objects should be subdivided into electrically small parts that are called finite elements as the unknown functions. To subdivide system, the adaptive mesh technique in ANSYS Electromagnetics suite version 2022.R1 (HFSS) is used. ANSYS Electromagnetics suite version 2022.R1 (HFSS) starts to refine the initial mesh based on wavelength and calculate the error to iterative process for adaptive mesh refinement. The determination parameter of the number of iteration in ANSYS Electromagnetics suite version 2022.R1 (HFSS) is defined as convergence criteria, delta S, and the iterative adaptive mesh process repeats until the delta S is met. In ANSYS Electromagnetics suite version 2022.R1 (HFSS), the accuracy of converged results depends on the delta S. Figure 1 is an example of adaptive mesh of the device (cross-section of top view).

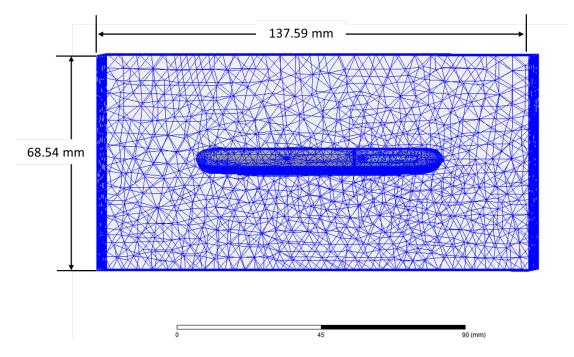


Figure 1 Example of the adaptive mesh technique (Top view)

#### 1.1.3 Power density calculation

After solving 3D full-wave electromagnetic simulation, various kinds of physical quantities can be obtained. To calculate PD evaluation, two physical quantities, an electric field  $(\vec{E})$  and a magnetic field  $(\vec{H})$  are needed. The actual consumption power can be expressed as the real term of the Poynting vector  $(\vec{S})$  from the cross product of  $\vec{E}$  and complex conjugation of  $\vec{H}$  as shown below:

$$\langle \vec{S} \rangle = \text{Re} \left( \frac{1}{2} \vec{E} \times \vec{H}^* \right)$$

 $\langle \vec{S} \rangle$  can be expressed as point power density based on a peak value of each spatial point on mesh grids, and obtained directly from ANSYS Electromagnetics suite version 2022.R1 (HFSS).

From the point power density  $\langle \vec{S} \rangle$ , the spatial-averaged power density  $(PD_{av})$  on an evaluated area (A) can be derived as shown below:

$$PD_{av} = \frac{1}{A} \int_{A} \langle \vec{S} \rangle \cdot ds = \frac{1}{2A_{av}} \iint_{A_{av}} ||Re\{ExH^*\}|| dA$$

, where the spatial-averaged power density (PD<sub>av</sub>) is total power density value considering on x, y and z components of point power density  $\langle \vec{S} \rangle$  and the evaluated area (A) is 4cm<sup>2</sup>.

#### 1.2 Simulation setup

#### 1.2.1 3D modeling

Figure 2 shows the simulation model which is mounted two mmWave antenna modules. The simulation modeling includes most of the entire structure of device itself such as PCB, metal frame, battery, cables, and legacy antennas as well as mmWave antenna modules called as Ant M and Ant N. The modeling contains the entire EUT to enable a Smart transmit GEN2, as well. Ant M is placed on the left side and antennas are facing the back side, and Ant N is placed on the right side and antennas are facing the right side of the device.

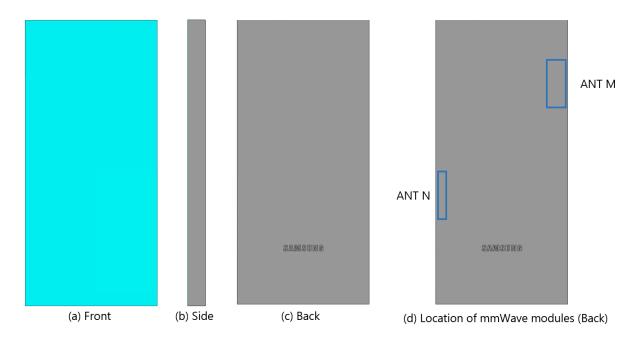


Figure 2 Simulation model which is mounted two mmWave antenna modules

### 1.2.2 PD evaluation planes

Table 1 shows the PD evaluation planes for each mmWave antenna module and Figure 3 shows the PD evaluation planes and truncation area of the simulation model to find worst case of beamforming cases.

Please note that the "right" and "left" edge of mentioned in this report are defined from the perspective of looking at the device from the front side.

Module	Front	Back	Left From Front View	Right From Front View	Тор	Bottom
	S1	S2	S3	S4	S5	S6
Ant M	0	0	О	0	0	0
Ant N	О	О	О	О	О	О

Table 1. PD evaluation planes

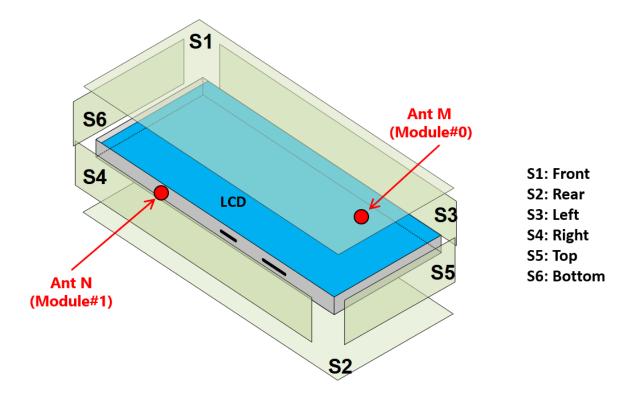


Figure 3. PD evaluation planes

#### 1.2.3 Boundary condition

To simulate electromagnetic tool based on FEM, the boundary condition allows electromagnetic waves to be electrically open at the boundary and radiated far away without reflection. ANSYS Electromagnetics suite version 2022.R1 (HFSS) can support the absorbing boundary condition (ABC) for radiation boundary and make normally a quarter wave length from the radiating structure. In this report, to cover all beamforming cases of mmWave antenna modules, 40 mm spacing from the device for each surfaces were adopted. This distance is sufficiently large enough for "Qualcomm MG script" to extract valid E- and H-fields from all adjacent exposure surfaces of the EUT.

#### 1.2.4 Source excitation condition

The number of antenna ports of ANT M and ANT N for source excitation are the same. The antenna port of ANT M and N is divided into 10 ports for n261 and n258 1 x 5 patch array antennas, 10 ports for n260 1 x 5 patch array antennas. In the 10 ports included in each patch antenna, 5 ports are divided into vertical polarization feeding, and the other 5 ports are divided into horizontal polarization feeding.

Figure 4 shows the ANT M module structure and surrounding structure. The ANT M module is encrypted in the ANSYS Electromagnetics suite (HFSS) and can only check the feeding position.

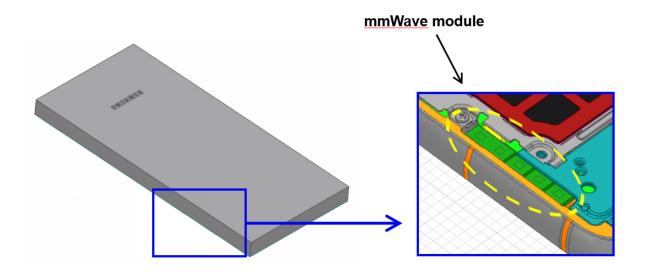


Figure 4. mmWave module (ANT M)

After finishing 3D full wave electromagnetic simulation of modeling structure, the magnitude and phase information can be loaded for each port by using "Edit Sources" function in ANSYS Electromagnetics suite (HFSS). Figure 5 shows an example of antenna port excitations.

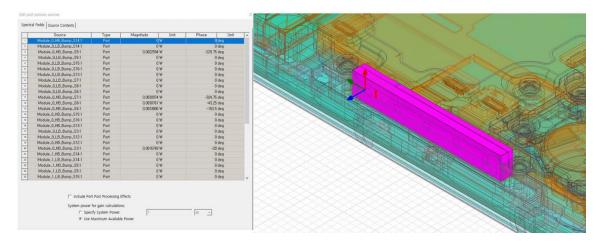


Figure 5. An example of port excitation (ANT N)

Since ANSYS Electromagnetics suite (HFSS) uses FEM solver based on frequency domain analysis method, the input source for the port excitation applies sinusoidal waveform for each frequency.

#### 1.2.5 Condition of simulation completion

The simulation completion condition of ANSYS Electromagnetics suite (HFSS) is defined as delta S. The ANSYS Electromagnetics suite (HFSS) calculates the S-parameter for the mesh conditions of each step and determines whether to proceed with the operation of the next step by comparing the difference

between the S-parameters in the previous step. A difference between the previous step and the current step of S-parameter is expressed as delta S, and the delta S generally sets 0.02. The simulation result of this report is the result of setting delta S to 0.02.

#### 2. Simulation verification

#### 2.1 Spatial-averaged power density and sim.powerlimit

As mentioned in the previous chapter, the Poynting vector  $(\vec{S})$  can be obtained through cross product of an electric field  $(\vec{E})$  and complex conjugate of a magnetic field  $(\vec{H})$ . The real term of the Poynting vector can be described as the point power density or peak power density. Using the point power density, the spatial-averaged power density can be obtained by the integral of 4 cm<sup>2</sup> at 2.5 mm intervals of the point power density result. Figure 6 shows examples of the distribution plot of point power density and the averaged power density.

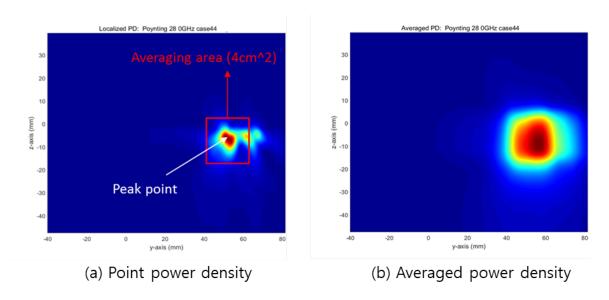


Figure 6. Power density distribution (Example)

For the Smart transmit GEN2, the "Qualcomm MG script" were used to extract E- and H-fields from the validated simulation and to assess the mutual coupling between all the mmWave antenna modules and all the beams in the codebook to determine the backoff value for each mmWave module. Note the assessment and backoff value derivation are automated with "Qualcomm MG script". Once the script is done with assessment, it will provide the sim.powerlimit (backoff is already included) for all the beams for all three channels for the specified PD\_design\_target. This mode take the minimum sim.powerlimit out of all three channels (low, mid and high) and use the resulted sim.powerlimit.

#### 2.2 Comparison between simulation, measurement

In this section, the simulated-power density distributions and measured-power density distributions are compared to each mmWave antenna. Furthermore, to verify the Smart transmit GEN2, the PD distributions printing out from the "Qualcomm MG script" are added.

Based on comparison of power density distributions, the power densities of simulated, measured and the "Qualcomm MG Script" have a good correlation. The discrepancy in amplitude between the "Qualcomm MG Script" 4cm² averaged power density and measured 4cm² averaged power density is considered as housing influence and used in determining input power limit for each beam for RF exposure compliance.

The input powers per each active port are listed below for both Simulation and Measurement validation and power density characterization. For Simulation, these values were entered directly into HFSS model. For measurement, FTM S/W was used to input these values for each active port also.

Mada/Band	Antonna	Input Power (dBm)	Input Power (dBm)
Mode/Band	Antenna	SISO	MIMO
FC ND ~261	M Patch	6.0	6.0
5G NR n261	N Patch	6.0	6.0
EC ND ~260	M Patch	6.0	6.0
5G NR n260	N Patch	6.0	6.0
CC ND ~2E0	M Patch	6.0	6.0
5G NR n258	N Patch	6.0	6.0

<sup>\*</sup> The below simulation and measurement result were performed at 2mm evaluation distance and 28GHz / 38.5GHz / 24.8 GHz. The *input.power.limit* was determined based on below results.

Band	Channel	Module	Type(P or D)	Side	Beam ID	PLS (10 dBm)	Sim. PD (mW/cm2)	Meas. PD (mW/cm2) * Circle Avg	
					Rear	35		1.125	0.486
		М	Patch	Left	33		0.532	0.257	
		101	Fatch	Rear	156		2.400	1.25	
	Mid			Left	154		1.100	0.708	
n261	Ch. 2077891			Rear	39	60	0.729	0.343	
	(27923.5 MHz)			Right	31		1.163	0.646	
		N	Patch	Front	30		0.576	0.277	
				Right	167		1.963	1.23	
				Front	107		1.013	0.624	
			Patch	Rear	24		0.999	0.387	
		М		Left	26		0.606	0.31	
	Mid			Rear	154		1.220	0.61	
n260	Ch. 2253331	N	Patch	Right	29	60	2.259	0.755	
	(38449.9 MHz)			Front	23		0.971	0.447	
		IN	Fatcii	Rear	168		1.040	0.348	
				Right	100		1.511	0.646	
				Rear	27		1.060	0.477	
		М	Patch	Left	26		0.541	0.223	
	Mid			Rear	156		1.691	0.947	
n258	Ch. 2025833			Rear	39	60	0.888	0.387	
11236	(24800.04 MHz)			Right	31	00	1.456	0.607	
	(= 100010 1 11111=)	N	Patch	Rear	166		0.440	0.284	
				Right	167		0.798	0.426	
				Front	107		0.390	0.223	

### • Table 2-1, n261 ANT M-Patch

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
35	S2 (Rear)	ANT M			***
33	S3 (Left)	ANTM			· ·

### • Table 2-2, n261 ANT M-Patch

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
156	S2 (Rear)	ANT M		B	•
154	S3 (Left)	MATERIA			

### • Table 2-3, n261 ANT N-Patch

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
39	S2 (Rear)	ANTM  ANTM	Y		Y
31	S4 (Right)	NTNA	<b>A</b>		*
30	S1 (Front)	ANTM			

### • Table 2-4, n261 ANT N-Patch

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
167	S4 (Right)	ANTN			
167	S1 (Front)	ANTM ANTN			

### • Table 2-5, n260 ANT M-Patch

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
24	S2 (Rear)	ANT M			10/00
26	S3 (Left)	MINA			<b>\\\\</b>

### • Table 2-6, n260 ANT M-Patch

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
154	S2 (Rear)	ANTM			***

### • Table 2-7, n260 ANT N-Patch

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
	S4 (Right)	ANTN			*****
29	S1 (Front)	ANTM			

### • Table 2-8, n260 ANT N-Patch

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
150	S2 (Rear)	ANTM			
168	S4 (Right)	ANTN			3

### • Table 2-9, n258 ANT M-Patch

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
27	S2 (Rear)	ANTN			•
26	S3 (Left)	MIN			*

• Table 2-10, n258 ANT M-Patch

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
156	S2 (Rear)	ANT N			***

### • Table 2-11, n258 ANT N-Patch

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
39	S2 (Rear)	ANTM			*
31	S4 (Right)	NANA	A D		9

### • Table 2-12, n258 ANT N-Patch

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
166	S2 (Rear)	ANTM			
167	S4 (Right)	NTNA	>		•
167	S1 (Front)	ANTM			

The Smart transmit GEN2 cannot be finalized until the additional verifications are performed and passed. Follow the below steps for verifications in the mid channel:

**VERIFICATION 1:** Use "Qualcomm MG script" to print the PD plots for all the beams selected and evaluated for model validation.

- Throughout above comparisons (Table 2-1 to 2-12), the model validation including MG script were verified.

**VERIFICATION 2:** Contribution factors from Qualcomm MG script and from HFSS for selected beams, and normalized combined PD verification, for A3LSMS916U device with 2 QTMs. The printed contribution factor from Qualcomm MG Script was within 2% numerical tolerance of the simulated contribution factor. Additionally, the normalized combined PD is < 1.0.

### [n261 band]

				Worst-case surface:	S4 (Right)	
		Wo	rst-case loc	ation (x,y,z) in meters:	Worst 4cm2 PD value location is 0.04053m, 0.06259m	, -0.00400m
			PD_	design_target (W/m <sup>2</sup> )	6.31	
	Values	printed from Q	ualcomm M	IG Script	Values obtained by OEM using EM simulation	tool
QTM#	Beam ID	c(i,j) i = beam ID j = QTM #	Backoff factor b <sub>j</sub>	verification.sim.  power limit (before backoffs) [dBm]	simulated 4cm2 PD(i,j) at (0.04053m, 0.06259m, -0.00400m) at verification.sim.power <sub>limit</sub> on S4	C <sub>simulated</sub> (i,j)= $4cm^{2}PD(i,j)/$ $PD\_design\_target$
0	13	0.0184	0.955	7.96	0.11629	0.0184
1	161	1.0000	0.9333	3.63	6.30807	0.9997
	Verify 1:	$C(i,j) = C_{simus}$	$l_{ated}(i,j), i =$	= 13, 161; j = 0, 1		
	Verify 2:	$b_0 * c(13,0) +$	$b_1 * c(161)$	(1) = 0.955 *0.0184	$+0.9333*1.0000 = 0.9509 \le 1$	

#### [n260 band]

				Worst-case surface:	S2 (Back)	
		Wor	rst-case loc	ation (x,y,z) in meters:	Worst 4cm2 PD value location is -0.03108m, 0.13759n	n, -0.01100m
			PD_	design_target (W/m <sup>2</sup> )	6.31	
	Values j	printed from Qu	ualcomm M	IG Script	Values obtained by OEM using EM simulation	tool
QTM#	Beam ID	c(i,j) i = beam ID j = QTM #	Backoff factor b <sub>j</sub>	verification.sim.  power limit (before backoffs) [dBm]	simulated 4cm2 PD(i <sub>j</sub> ) at (-0.03108m, 0.13759m, -0.01100m) at verification.sim.power <sub>limit</sub> on S2	C <sub>simulated</sub> (i,j)= $4cm^{2}PD(i,j)/$ $PD\_design\_target$
0	11	1.0000	0.955	8.17	6.31583	1.0009
1	169	0.0048	0.9333	4.19	0.03018	0.0048
	Verify 1:	$C(i,j) = C_{simul}$	$l_{ated}(i,j), i =$	= 11, 169; j = 0, 1		
	Verify 2:	$b_0 *c(11,0) +$	$b_1*c(169)$	(1) = 0.955 * 1.0000 - 1.0000	+ 0.9333*0.0048 = 0.9595 \le 1	

# [n258 band]

				Worst-case surface:	S2 (Back)	
		Wo	rst-case loc	ation (x,y,z) in meters:	Worst 4cm2 PD value location is 0.03492m, 0.06859m	, -0.01100m
			PD_	_design_target (W/m <sup>2</sup> )	6.31	
	Values	printed from Q	ualcomm N	IG Script	Values obtained by OEM using EM simulation	tool
QTM#	Beam ID	c(i,j) i = beam ID j = QTM #	Backoff factor b <sub>j</sub>	verification.sim.  power limit (before backoffs) [dBm]	simulated 4cm2 PD(i,j) at (0.03492m, 0.06859m, -0.01100m) at verification.sim.power <sub>limit</sub> on S2	C <sub>simulated</sub> (i,j)= $4cm^{2}PD(i,j)/$ $PD\_design\_target$
0	165	0.0490	0.955	2.25	0.30915	0.0490
1	145	0.9973	0.9333	10.95	6.29541	0.9977
	Verify 1:	$C(i,j) = C_{simus}$	lated (i,j), i =	= 165, 145; j = 0, 1		
	Verify 2:	$b_0 * c(165,0)$	+ b 1 *c(14	(5,1) = 0.955*0.0490	$+0.9333*0.9973 = 0.9776 \le 1$	

**VERIFICATION3:** Measured 4cm<sup>2</sup> PD on worst surface and combined PD at worst-case location for A3LSMS916U device with 2 QTMS. The device should be measured at the reference power level and scaled to the input.power.limit. The combined PD should be less than or equal to the *PD\_Design\_Target* within the uncertainty at the reference power level.

### [n261 band]

QTM#	Beam ID	c(i,j) i = beam ID j = QTM #	Dominant surface	4cm2 PD at input.power.limit on QTM dominant surface (W/m2)	input.power.limit (before permanent backoff)	Measured PD at reference power level on Beam Dominant Surface (mW/cm2)
0	13	0.0184	S2 (Back)	4.057	8.9	0.210
1	161	1.0000	S4 (Right)	4.319	4.4	0.620
combi	ined PD at the	worst-case lo	ocation (x,y,z)		$^{2}$ PD(13,0) + c(161,1 1.0000*4.319 = 4.39	.)*meas.4cm <sup>2</sup> PD(161,1) 4 W/m <sup>2</sup>
PD_design		ertainty at refe f 0.63 dB	erence power level	= 6.310*10^(0.63/1	$10) = 7.295 \text{ W/m}^2$	
			Verify	combined PD < PI	_design_target + ι	incertainty at reference power level

### [n260 band]

QTM#	Beam ID	c(i,j) i = beam ID j = QTM #	Dominant surface	4cm2 PD at input.power.limit on QTM dominant surface (W/m2)	input.power.limit (before permanent backoff)	Measured PD at reference power level on Beam Dominant Surface (mW/cm2)
0	11	1.0000	S2 (Back)	5.933	10.3	0.223
1	169	0.0048	S4 (Right)	4.531	5.2	0.541
comb	ined PD at the	worst-case k	ocation (x v z)		$^{2}$ PD(11,0) + c(169,10).0048*4.531 = 5.95	1)*meas.4cm <sup>2</sup> PD(169,1) 55 W/m <sup>2</sup>
PD_design		ertainty at refe f 0.63 dB	erence power level	= 6.310*10^(0.63/1	$10) = 7.295 \text{ W/m}^2$	
			Verify	combined PD < PI	D_design_target + ι	incertainty at reference power level

### [n258 band]

QTM#	Beam ID	c(i,j) i = beam ID j = QTM #	Dominant surface	4cm2 PD at input.power.limit on QTM dominant surface (W/m2)	input.power.limit (before permanent backoff)	Measured PD at reference power level on Beam Dominant Surface (mW/cm2)
0	165	0.0490	S2 (Back)	5.011	3.5	0.889
1	145	0.9973	S2 (Back)	2.213	11.3	0.066
comb	ined PD at the	e worst-case k	ocation (x,y,z)		$\frac{\text{m}^2\text{PD}(165,0) + \text{c}(14)}{0.9973*2.213 = 2.45}$	5,1)*meas.4cm <sup>2</sup> PD(145,1) 63 W/m <sup>2</sup>
PD_design		ertainty at refe f 0.63 dB	erence power level	= 6.310*10^(0.63/1	$10) = 7.295 \text{ W/m}^2$	

#### 3 Simulation results

This section shows the PD simulation results of Ant M and Ant N at 28GHz, 39GHz and 24GHz for each evaluation plane specified in Table 1 at two separation distances of 2mm and 10mm. The ratio of PD exposure from front surface to the worst surface at 2mm, and the ratio of PD exposure from 2mm to 10mm evaluation distance for each beam are also reported in this section to support RF exposure analysis for simultaneous transmission scenarios performed in the Part 1 Near Field PD report.

The relative phase between beam pairs is not controlled in the chipset design. Therefore, the relative phase between each beam pair was considered mathematically to identify the worst case conditions. The below MIMO results represent the highest reported MIMO simulation results after sweeping across the relative phase between beams a 5° step interval from 0° to 360°,

The worst-case simulated PD determined from the tables in this section were used for conservativeness in *input.power.limit* determination in RF Exposure Part 0 Report.

#### 3.1 PD for Low/Mid/High Channel at 28GHz / 39GHz / 24GHz

#### 3.1.1 Ant M-Patch Antenna

Table 3 to 5 show the PD simulation evaluation of Ant M patch antenna at 28GHz / 39GHz / 24GHz for the all surfaces.

Table 3. PD of Ant M – patch antenna (28GHz – n261)

#### - M-patch Low CH

								_									max ratio ou	t of all beams													max ratio out of all b	eams		
П		Т							4cm2	PD/mW	/cm2)				5.7%	59.5%	21.1%	12%	14.1%	100.0%	40	m2 PD(n	/W/cm2)	at 10mm e	rvaluation	n distance		67.2%	45%	28.4%	157%	0.9%	5.7%	67.2%
No.	Module 1	lype Be	eam ID_1	Berna ID,2	Feed no.	S4(Right)	S3(Left)	SS(To	p) 51	6(Bottom	\$1(Fro	et) 52	(Rear)	per Beam Back-off (dB)	ratio (Right 2mm)/(worst- surface 2mm)	ratio (Left 2mm)/(wont- surface 2mm)	ratio (Top 2mm)/(worst- surface 2mm)	ratio (Bottom 2mm)/(wont- surface 2mm)	ratio (Fornt 2mm)/(worst- surface 2mm)	ratio (Rear 2mm)/(wont- surface 2mm)	S4(Right)	S3(Left)	SS(Top	) S6(Bots	om) 51)	(Front) S.	2(Rear)	ratio worst-surface (10mm/2mm)	ratio (Right 10mm)/(wont- surface 2mm)	ratio (Left 10mm)/(worst- surface 2mm)	ratio (Top 10mm)/(wont- surface 2mm)	ratio (Bottom 10mm)/(worst- surface 2mm)	ratio (Front 10mm)/(wonst- surface 2mm)	ratio (Rear 10mm)/(worst- surface 2mm)
1		1	0		1	0.00	0.09	0.02	1	0.00	0.01		0.23	1000	1.8%	38.1% 41.2%	10.6%	0.4%	5.8% 9.6%	100.0%	0.00	0.03		0.00		2.00	0.08	34.5%	1.8%	15.0% 19.2%	7.1%	0.4%	1.8%	34.5% 38.8%
3		E	â		1	0.00	0.05	0.01		0.00	0.02	Ĭ	0.21		5.2%	25.7%	6.2%	0.5%	11.0%	100.0%	0.01	0.02	0.01	0.00		2.01	0.00	31.6%	2.8%	1.6%	2.2%	0.5%	2.9%	38.6%
2 3 4 5 6 7 8 9		E	6		1	0.01	300			0.00	0.01		0.17 0.17		1.5% 1.8%	31.8% 37.1%	5.8% 4.7%	12%	5.2% 14.1%	100.0%	0.01	0.02		0.00	- 0	2.00	0.06	31.5% 34.7%	1.5% 1.2%	10.4% 17.6%	4.0%	0.6%	1.7% 4.1%	31.5% 34.7%
6		F	-6			0.01				0.00	0.03	Ī	SE		2.1%	27.9% 46.8%	17.1% 11.2%	0.7%	6.8%		0.01					101	0.16	27.5% 44.8%	1.9%	10.1% 20.6%	11.9% 7.4%	0.5%	2.1% 3.4%	37.5% 44.8%
8		F	12		2 2	0.02	0.19			0.00	0.05		0.49		3.1%	39.5% 38.1%	4.5% 11.2%	0.4%	10.0%	100.0%	0.01	0.08				3.02	0.20	41.3%	2.2%	17.0%	2.9%	0.4%	19%	41.3%
10			18			0.01	0.14			0.00	0.03		0.45		2.4%	30.8%	16.9%	0.7%	5.8%	100.0%	0.01	0.05	0.05	0.00		2.01	0.18	42.4%	2.2%	12.0%	11.5%	0.4%	2.2%	40.4%
11		⊢	19 20		2	0.01	0.27	0.03	+	0.00	0.04	1	0.52		2.5% 1.7%	53.1% 37.9%	5.8% 7.0%	0.4%	8.3% 10.3%	100.0%	0.01	0.13		0.00	- 0	102	0.24	47.3% 41.7%	1.9%	24.8% 18.9%	1.9%	0.2%	1.7% 4.2%	47.2% 41.7%
12		F	24		5	0.02	0.40	0.23		0.01	0.00		1.07		1.5%	36.8% 41.7%	21.1%	0.7%	7.0%		0.01	0.14			- 9	102	0.42	29.3% 45.9%	1.0%	13.0% 20.2%	15.7%	0.5%	145	39.3% 45.9%
12 13 14 15 16 17		⊨	22		- 5	0.05	0.48	0.05	_	0.00	0.54		1.02		17%	47.4% 48.0%	5.0%	0.3%	7.6% 12.2%	100.0%	0.04	0.22	0.03	0.00		104	0.47	45.8% 46.6%	105	22.0% 24.2%	1.0%	0.2%	425 175	45.8% 46.6%
17		-	28			0.03	0.39	0.05		0.01	0.11		1.01		2.6%	38.8%	5.2%	0.5%	9.4%	100.0%	0.02	0.17	0.03	0.00		104	0.50	49.3%	1.9%	17.3%	3.4%	0.3%	3.6%	49.3%
18		F	34 35		5 5	0.03				0.01	0.07		100		2.7%	28.6% 51.7%	16.3%	1.1%	7.0%	100.0%	0.03			0.01		102	0.44	41.7%	2.5% 3.3%	11.1% 26.4%	12.1%	0.7%	1.6%	43.7% 50.9%
18 19 20 21 22 23 24 25 26 27		F	36			0.05	0.42			0.00	0.09		0.91		4.9%	46.4% 41.8%	4.7%	0.4%	9.8% 11.2%	100.0%	0.04	0.21		0.00		2.04	0.20	41.5%	4.1%	22.9%	2.5%	0.4%	4.6%	41.5% 49.7%
22		E	128		1	0.00	0.12	0.03	#	0.00	0.01		0.35		0.6%	35.0%	0.6%	0.3%	1.7%	100.0%	0.00	0.04	0.02	0.00		100	0.16	45.6%	0.3%	10.6%	5.2%	0.2%	0.6%	45.6%
23		⊢	132			0.00				0.00	0.01	H	0.43		0.5% 0.7%	29.8% 38.3%	6.1% 4.3%	0.5%	14%	100.0%	0.00				- 1	100	0.19	44.5% 44.8%	0.2%	13.1%	2.5% 2.9%	0.5%	0.5%	44.5% 44.8%
25		F	134			0.00				0.00	0.01		0.44		0.7%	27.3%	1.4%	0.7%	1.1%	100.0%	0.00		0.01			100	0.18	40.0%	0.5%	10.9%	2.3%	0.5%	0.7%	40.0%
27			128		2	0.01		0.07		0.00	0.01		0.00		0.9%	11.3%	0.1%	0.4%	1.2%	100.0%	0.01	0.09	0.05			200	0.35	43.8%	0.6%	11.1%	6.1%	0.4%	0.5%	43.0%
28 29 30 31 32 33 34 35 36			139		2	0.01	0.41	0.00	+	0.00	0.01		0.87		0.6%	46.9% 40.2%	9.0%	0.0%	0.8%		0.00	0.15	0.05	0.00	- 0	100	0.53	61.3% 57.1%	0.5%	17.5% 14.1%	5.2% 1.6%	0.0%	0.3%	61.3% 57.1%
30		F	141		2	0.01	0.30	0.03	+	0.01	0.02		0.83		0.7%	35.9% 46.1%	1.5%	0.8%	2.3%	100.0%	0.00	0.09	0.02	0.01		2.01	0.25	42.5% 54.1%	0.4%	11.0%	2.3% 5.8%	0.8%	1.0%	42.5% 54.1%
32	M P	atch	147		2	0.00	0.41		#	0.00	0.01		0.89		0.3%	45.7% 19.1%	52% 13%	0.1%	1.1% 2.1%	100.0%	0.00	0.15	0.02	0.00	_	1.01	0.53	59.7% 44.1%	0.2%	16.9%	2.5% 1.2%	0.1%	1.0%	59.7% 44.1%
34			152		- 5	0.04	0.93	0.39	,	0.00	0.05		2.41		14%	18.1%	16.2%	0.1%	225	100.0%	0.03	0.39	0.26	0.00		102	1.17	48.6%	1.15	16.3%	10.6%	0.1%	1.0%	40.6%
36			153			0.03				0.00	0.03		2.17		1.2%	45.9% 51.6%	5.0%	0.0%	1.5%	100.0%	0.02	0.50	0.01			1.02		63.8%	1.0%	21.2%	2.5%	0.0%	0.7%	63.0%
37		F	155		5	0.03		0.03		0.01	0.04		2.09		1.2%	47.7% 17.7%	1.4%	0.2% 0.6%	1.7%	100.0%	0.02			0.01		3.02	1.29	61.8% 47.7%	0.9%	20.7% 15.5%	1.0%	0.2%	0.9%	61.8% 47.7%
29		E	162		5	0.04	0.94	0.21		0.00	0.04		2.26		1.6%	41.7%	12.3%	0.0%	1.9%	100.0%	0.03	0.41	0.14	0.00	- 0	102	1,21	58.0%	1.35	18.2%	6.2%	0.0%	0.9%	58.0%
41		E	163		5	0.02	098	0.04		0.00	0.02		1.01		1.4% 1.2%	46.3% 54.7%	2.9% 2.2% 1.3%	0.0%	1.1% 1.2% 2.7%	100.0%	0.02	0.45	0.02		- 0	2.01	1,24	61.2% 67.2%	1.0%	21.1% 25.2% 17.2%	1.0%	0.0%	0.6%	63.2% 67.2%
37 38 29 40 41 42 43 44 45 46 47 48 49 50 50		F	165	128	5 2	0.03	0.94			0.01	0.00		2.31 0.65		1.2%	40.8% 37.2%	1.3%	0.5%	2.7% 4.2%	100.0% 100.0%	0.02	0.40				3.03	0.26	53.4% 40.6%	0.9%	17.2% 11.5%	0.7% 6.0%	0.2%	1.4%	53.4% 40.6%
44		F	2	110	2 2	0.01				0.00	0.04		0.75		1.2%	46.9% 17.0%	7.4% 6.8%	0.4%	4.8% 4.7%	100.0% 100.0%	0.01	0.14	0.04			3.02	0.33	44.4% 42.0%	0.9% 2.0%	18.4% 12.8%	5.0% 3.5%	0.4%	2.1% 1.6%	44.4% 42.0%
46		E	6	124		0.01	0.21	0.04		0.01	0.02		0.68		1.2%	11.5%	5.2%	0.9%	1.0%	100.0%	0.01	0.07	0.03	0.01		2.01	0.26	37.8%	1.0%	10.2%	3.7%	0.7%	1.0%	37.0%
45		⊢	10	136	4	0.01	0.24	0.04	+	0.00	0.03	1	1.19		1.1%	18.0% 11.4%	7.0% 14.4%	0.3%	5.4% 3.4%	100.0%	0.01	0.09		0.00	- 0	2.01	0.26	41.6%	0.9%	14.9%	5.2% 10.5%	0.3%	1.4%	41.6% 39.2%
49		F	11	139	4	0.02	0.77			0.00	0.05		1.47		1.4%	52.3% 47.1%	12.2%	0.3%	15%	100.0%	0.02			0.00	- 4	103	0.79	51.9%	12%	20.6%	7.8%	0.1%	1.7%	53.9% 55.0%
51		E	- 12	141	4	0.02	0.53	0.06	_	0.01	0.06	_	1.30		128	40.1%	5.85	1.1%	6.15	100.0%	0.01	0.18	0.05	0.01		102	0.59	45.5%	0.9%	14.0%	1.9%	0.9%	235	45.5%
53		F	18	146	- 4	0.02	0.02	0.11		0.01	0.05	,	1.53		1.5%	46.9% 53.7%	13.8%	0.6%	17% 47%	100.0%	0.02	0.34	0.07	0.00		102	0.62	46.9% 56.5%	1.3%	17.9% 22.4%	9.0% 4.3%	0.5%	1.5% 2.0%	46.9% 56.5%
54		F	20	148	4 10	0.02	0.60	0.06		0.01	0.00		1.27		1.7%	47.5% 48.3%	5.0% 16.2%	1.0%	4.6%	100.0%	0.02	0.23	0.04	0.01		2.03	0.62	41.6% 50.3%	1.3%	18.1% 18.5%	3.3% 10.7%	0.8%	2.2%	40.6%
54 55 56 57 58 59 60 61 62		E	25	153		0.09	1.59	0.23		0.01	0.13		2.10		2.7%	50.0%	6.6%	0.3%	4.6%		0.07	0.74	0.12			2.08	2.00	62.8%	2.2%	23.3%	3.8%	0.2%	2.4%	62.0%
57		-	26 27	154	10	0.09		0.00	+	0.01	0.12		1.09		2.8%	56.0% 50.5%	2.7% 1.8%	0.2%	3.8% 5.8%	100.0%	0.07	0.81		0.00	- 0	3.07	2.14	61.4%	2.3%	26.2% 22.7%	1.6%	0.1%	2.1%	63.4% 63.2%
59		F	28	156	10	0.06			#	0.03	0.15		192		1.6%	42.2% 22.5%	3.4%	0.6%	4.9%	100.0%	0.05			0.02	- 5	109	2.05	52.4% 58.3%	125	17.5% 19.2%	2.1%	0.5%	2.3%	52.4% GL5%
61		E	35	163		0.09	1.64	0.14		0.01	0.12		1.22		2.8%	50.8%	4.4%	0.3%	3.8%	100.0%	0.06	0.77		0.01		3.07	2.01	62.4%	1.9%	23.9%	2.7%	0.2%	2.2%	62.4%
62		-	36 37	164		0.09				0.01	0.15		2.84		1.0%	59.5% 42.2%	1.85	0.3%	5.1% 5.6%	100.0%	0.07			0.01		108	1.83	64.6% 57.7%	2.4% 1.3%	28.4% 18.8%	2.4%	0.3%	2.9%	64.6% 57.7%

# - M-patch Mid CH

															max ratio ou	of all beams												max ratio out of all	beams		
$\vdash$	$\neg$	т	$\neg$					4cm2 P	DimW/cn	12)									40	om2 PD(m	W/cm2) a	t 10mm eval	lustion di	tance	<b>-</b>	I					
No.	Module 1	Voe B	eam ID_1	Sema ID <sub>2</sub> 2	Feed no.		_	$\overline{}$				per	67% ratio	60.0% ratio	18.9% ratio	0.8% ratio	14.7% ratio	100.0% ratio		_			Т	$\overline{}$	67.2% ratio	5.7% ratio	29.1% ratio	140% ratio	o.es.	s 2% ratio	67.2% ratio
		"				S4(Right) S3(Li	nt) SS(To	p) 56(I	Bottom)	S1(Front)	S2(Rear)	Beam Back-off	(Right 2mm)/(worst- surface 2mm)	(Left 2mm)/(wont- surface 2mm)	(Top 2mm)/(worst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(worst- surface 2mm)	S4(Right)	\$3(Left)	SS(Top)	SE(Bottom)	S1(Fron	nt) S2(Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(wont- surface 2mm)	(Left 10mm)/(wonst- surface 2mm)	(Top 10mm)/(wonst- surface 2mm)	(Bottom 10mm)/(worst- surface 2mm)	(Front 10mm)/(wont- surface 2mm)	(Rear 10mm)/(wont- surface 2mm)
1		_	0		-		0.00			0.02	0.23	1000	2.6%	40.4% 44.4%	9.6%	0.4%	6.5%		0.01				0.00		41.7% 41.5%	2.2%	14.0%	5.7%	0.4%	1.7%	41.7%
3		E	4		- 1	0.01 0.0	5 0.00		0.00	0.02	0.21		2.0% 4.3%	25.0%	6.3%	0.4%	9.3%	100.0%	0.01	0.02	0.01	0.00	0.01	0.09	42.3%	3.4%	21.0% 8.2%	3.0%	0.4%	4.0% 3.4%	43.5% 42.3%
5		H	6		-		7 0.01		0.00	0.01	0.17	<del> </del>	4.0%	32.2% 39.0%	6.9% 5.1%	0.6%	6.3% 14.7%	100.0% 100.0%	0.01		0.01	0.00	0.00		32.8%	3.4% 1.2%	10.9%	4.6%	0.6%	1.7%	32.8% 30.5%
6		_ F	10 11		2		4 0.00		0.00	0.03	0.43		2.6%	31.8% 49.9%	17.4% 9.9%	0.5%	7.1% 6.2%	100.0%	0.01	0.05	0.05	0.00	0.01		49.9%	2.4% 1.2%	10.8%	10.8%	0.2%	2.4%	40.0% 49.9%
8		E	12		2	0.01 0.1	9 0.00		0.00	0.04	0.45		3.1%	41.4%	4.05	0.4%	9.2%	100.0%	0.01	0.00	0.01	0.00	0.02	0.19	42.7%	2.4%	17.0%	3.1%	0.4%	4.0%	42.7%
2 3 4 5 6 7 8 9		⊢	12 18		2 2	0.01 0.1	0.0	_	0.00	0.05	0.40	<del> </del>	2.0%	33.3% 35.4%	10.0% 16.5%	0.5%	11.2%	100.0%	0.00	0.06			0.02		25.1% 41.0%	1.0% 2.7%	14.2% 12.7%	6.0% 10.5%	0.5%	45% 2.4%	35.1% 43.0%
11		F	19 20		2	0.02 0.3	0.00		0.00	0.04	0.52		3.2% 1.8%	56.9% 42.0%	575 595	0.4%	7.3% 10.6%	100.0%	0.01	0.13	0.02	0.00	0.02		53.4% 41.2%	2.7% 1.4%	24.6%	2.9%	0.2%	1.1% 4.2%	53.4% 43.2%
12		E	24		ŝ	0.01 0.3			0.00	0.07	0.97		1.5%	32.8%	18.9%	0.4%	7.0%	100.0%	0.01	0.10	0.14	0.00	0.02	0.42	43.6%	1.1%	9.9%	14.0%	0.3%	1.7%	43.6%
15		- 1-	25 26		5	0.07 0.4			0.01	0.11	1.09	_	6.7%	42.4% 48.0%	7.8% 4.6%	0.6%	11.3%	100.0%	0.06		0.06	0.00	0.05		46.3%	5.7% 1.9%	19.9%	5.9% 2.4%	0.4%	5.1% 4.1%	46.2% 44.1%
11 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28		F	27 28		5	0.04 0.5	0.00	9	0.00	0.10	0.99		1.6%	50.1% 37.9%	2.8%	0.4%	10.0%	100.0%	0.03	0.24	0.02	0.00	0.05		46.5% 45.3%	1.0%	24.0% 17.4%	2.0%	0.3%	5.2% 4.2%	46.5% 45.3%
18			24 35				4 0.11		0.01	0.07			2.1%	25.6%	18.7%	0.6%	7.5%	100.0%	0.02	0.03	0.12	0.00		0.44	46.2%	2.0%	1.6%	12.4%	0.4%	2.15 4.95	46.2%
20			36		- 5	0.04 0.5	2 0.0-		0.00	0.10	1.13	<del>                                     </del>	4.0%	47.3% 52.0%	445	0.4%	9.0% 8.7%	100.0%	0.03	0.25	0.02	0.00	0.04	0.46	45.5%	1.1%	21.2% 24.3%	2.8% 2.3%	0.2%	445	48.0% 45.5%
21			37 128		5		1 0.00		0.00	0.10	0.95		2.9%	45.1% 32.8%	13%	0.4%	10.0%	100.0%	0.02		0.02	0.00	0.05		45.3%	2.4%	21.4% 9.5%	2.1% 6.2%	0.3%	4.9%	46.5% 45.3%
22			120			0.00 0.1	0.00		0.00	0.01	0.42		0.2%	42.9%	6.1%	0.5%	1.4%	100.0%	0.00	0.06	0.02	0.00	0.00	0.19	45.2%	0.2%	14.2%	3.7%	0.5%	0.5%	45.2%
25		E	132 134		1	0.00 0.1	1 0.00		0.00	0.01	0.42		0.5%	38.7%	1.0%	0.5%	1.4%	100.0%		0.06	0.01	0.00	0.00	0.19	45.2%	0.5%	13.5%	2.6%	0.5%	0.5%	46.2% 41.1%
26		F	126		1		4 0.00		0.00	0.00	0.40		0.8%	34.8% 38.8%	4.5% 7.5%	0.3%	1.0%	100.0%	0.00	0.05	0.01	0.00	0.00	0.17	42.4% 45.8%	0.5%	12.0%	1.5% 5.8%	0.2%	0.3%	42.4% 45.8%
26		E	139		2	0.00 0.4	0.00		0.00	0.01	0.85		0.5%	47.4%	8.9%	0.0%	0.8%	100.0%	0.00	0.15	0.05	0.00	0.00	0.52	60.4%	0.4%	17.0%	5.4%	0.0%	0.4%	60.4%
30		⊢	140		2		2 0.00	1 6	0.00	0.01	0.94	<del>                                     </del>	0.6%	43.8% 29.4%	1.8% 3.5%	0.1%	2.4%	100.0%	0.01	0.15	0.01	0.00	0.00	0.55	58.4% 44.9%	0.5%	15.6%	1.2%	0.0%	0.4%	58.4% 44.9%
21	м	E	146		2		9 0.00		0.00	10.0	0.79		0.9%	49.2% 46.9%	9.45	0.4%	1.85	100.0%	0.01	0.15	0.05	0.00	0.01		54.1% 59.9%	0.8%	18.9% 17.2%	5.7% 2.4%	0.4%	0.9%	54.1%
22			140		2		0.00		0.01	0.02	0.91		0.7%	41.7%	1.9%	0.7%	2.2%	100.0%	0.00	0.13	0.01	0.01	0.01		45.4%	0.4%	14.0%	1.3%	0.6%	0.9%	46.4%
35		E	152 153		5	0.02 0.9	9 0.10		0.00	0.06	2.12		1.3%	42.6% 46.7%	15.2% 4.5%	0.1%	2.4%		0.02		0.23	0.00	0.02	1.35	49.5% 61.6%	1.0%	18.6%	9.7%	0.1%	1.0%	49.5% 63.6%
26 27		F	154 155		5		0 000		0.00	200	2.04		0.9%	\$3.8% \$1.1%	1.0%	0.0%	1.0%		0.01		0.01	0.00	0.01		61.0%	0.7%	25.3% 22.7%	0.5%	0.0%	0.5%	63.6%
38		- =	162		- 5		5 0.00		0.01	0.08	2.40		1.0%	41.0%	13%	0.5%	12%	100.0%	0.02	0.41	0.02	0.01	0.04		50.1%	0.6%	17.3%	0.9% 5.4%	0.4%	1.5%	50.1% 58.0%
40			163		5	0.03 1.0	2 0.00		0.00	0.02	2.09		1.2%	48.7%	2.7%	0.0% 0.0%	2.0%	100.0%	0.02	0.47	0.04	0.00	0.01	1.32	63.2%	0.9%	22.3%	1.8%	0.0%	0.5%	63.2%
41		- 1-	164		5	0.02 0.9	7 0.00		0.00	0.02	1.79	-	1.0%	54.4% 44.6%	1.1%	0.1%	1.1% 2.7%	100.0%	0.01	0.46	0.03	0.00	0.01		67.2%	0.8%	25.4% 19.2%	1.9%	0.1%	0.6%	67.2% 56.1%
43		F	0	128	2	0.01 0.2	5 0.00		0.00	0.03	0.65		1.1%	18.6% 49.9%	10.2%	0.3%	4.5%	100.0%	0.01	0.08	0.04	0.00	0.01	0.28	41.2%	0.9%	12.2%	6.2% 5.2%	0.3%	1.4%	43.2% 45.8%
45		E	4	130	2	0.02 0.2	6 0.00		0.00	0.03	0.70		2.3%	17.2%	6.4%	0.6%	4.4%	100.0%	0.01	0.09	0.02	0.00	0.01	0.30	42.4%	1.2%	12.6%	3.4%	0.6%	1.9%	42.4%
22 33 34 35 35 36 39 40 41 42 43 44 45 46 47 48 48 50 51 52 53 53 55 53 55 55 55 55 55 55 55 55 55		F	6	134	2	0.01 0.2	0.0-		0.01	0.02	0.64	H	1.5%	35.1% 40.2%	5.6%	0.8%	12% 5.1%	100.0%	0.01	0.10	0.03	0.01	0.01	0.27	40.2%	1.2%	10.7%	1.9% 4.2%	0.8%	1.4%	40.2% 42.5%
48		F	10	138	4	0.02 0.4	0.13		0.01	0.04	1.16		1.6%	16.5% 52.8%	14.4%	0.6%	1.7% 2.9%	100.0%	0.02	0.16	0.12	0.01	0.02	0.48	41.3%	1.6%	13.7%	10.4%	0.5%	1.3%	41.3% 55.5%
50		E	12	140	1	0.03 0.7	7 0.0		0.00	0.06	1.55		1.9%	49.8%	2.0%	0.2%	2.6%	100.0%	0.03	0.30	0.03	0.00	0.03		56.0%	1.6%	19.7%	1.7%	0.2%	1.7%	\$6.0%
51		- 1-	13	141	4	0.01 0.5		1 6	0.01	0.09	1.32	-	1.0%	40.7% 49.3%	6.3% 12.7%	0.8%	6.4% 1.2%	100.0%	0.01	0.18	0.05	0.01	0.03		46.7%	1.9%	13.7%	4.0% 8.2%	0.7%	2.6%	46.7% 50.4%
53		F	19	147	4	0.02 0.8	1 0.00		0.00	0.06	1.52		1.5%	54.1% 49.6%	5.1%	0.2%	19% 52%	100.0%	0.02	0.34	0.05	0.00	0.03		58.1% 49.5%	1.2%	22.2%	1.5% 2.9%	0.1%	1.8%	58.1% 49.5%
55		E	24	152		0.06 2.0	0.74			0.12			1.4%	49.5%	16.2%		2.9%	100.0%	0.04	0.79	0.42	0.01	0.05	2.19	53.9%	1.1%	19.6%	10.5%	0.1%	1.1%	53.9%
56		F	25 26	153	10	0.00 1.6	9 0.00		0.01	0.14	1.13	⊢=	3.3%	52.2% 54.7%	2.8%	0.3%	14%	100.0%	0.06	0.79	0.05		0.06	1.07	64.9%	2.4%	24.7% 25.5%	1.6%	0.2%	2.7%	64.9%
58		F	27 28	155	10	0.06 1.8	0.00		0.01	0.19	3.39		1.7%	51.2% 44.4%	2.0%	0.4%	5.6%	100.0%	0.05	0.83	0.05		0.11	2.19	64.7% 55.1%	1.4%	24.5% 18.7%	1.5%	0.3%	3.2% 2.8%	64.7%
60		E	34	162	10	0.07 1.6	3 0.50		0.01	0.11	3.47		1.9%	47.0%	16.9%	0.2%	2.1%	100.0%	0.05	0.74	0.29	0.01	0.05	2.12	61.1%	1.6%	21.2%	0.4%	0.1%	1.4%	61.1%
59 60 61 62		- 1-	35 36	163	10		9 0.13			0.12	2.90	-	2.6%	\$1.1% 60.0%	1.8%	0.2%	17% 425	100.0%		0.78			0.07		62.0%	1.9%	24.2%	2.3%	0.1%	2.2%	62.0%
63			27	165	10	0.05 1.6			0.01	0.20	1.57		1.3%	44.7%	1.7%	0.3%	5.6%	100.0%	0.04				0.12	2.16	60.4%	1.0%	20.3%	1.0%	0.2%	1.2%	60.4%

# - M-patch High CH

																		max ratio ou	t of all beams												max ratio out of all b	eams		
						Г			-	4cm2 P	O(mW)	cm2)				19%	63.0%	21.1%	0.8%	15.4%	100.0%		4cm2 PD)	mW/cm2)	at 10mm evi	slustion d	stance	67.9%	3.0%	21.7%	12.7%	0.6%	5.1%	67.9%
No. Mo	odule 1	lype Sau	am ID_1	Bersa ID,2	Feed no.		ght) S3	(Left)	\$5(Top	0 56(1	Bottom)	S1 (From	nt) 52()		per Beam lack-off (dB)	ratio (Right 2mm)/(worst- surface 2mm)	ratio (Left 2mm)/(wont- surface 2mm)	ratio (Top 2mm)/(wont- surface 2mm)	ratio (Bottom 2mm)/(wonst- surface 2mm)	ratio (Forst 2mm)/(worst- surface 2mm)	ratio (Rear 2mm)/(wont- surface 2mm)	S4(Right	53(Lef	t) SS(Top	S6(Bottom	s) S1(Fee	nt) S2/Rear	ratio worst-surface (10mm/2mm)	ratio (Right 10mm)/(wont- surface 2mm)	ratio (Left 10mm)/(worst- surface 2mm)	ratio (Top 10mm)/(wonst- surface 2mm)	ratio (Bottom 10mm)/(wonst- surface 2mm)	ratio (Front 10mm)/(wont- surface 2mm)	ratio (Rear 10mm)/(wont- surface 2mm)
1		┲	0		1	0.0	0 0	110	0.03	-	0.00	0.02	0.	22		1.3%	41.0%	12.2%	0.4%	7.8% 9.8%	100.0%	0.00	0.04		0.00	0.01	0.10	43.5% 45.0%	135	15.2% 22.6%	6.1%	0.4%	2.2%	43.5% 45.0%
2		-	4		-	0.0	1 0	0.7	0.02	-	0.00	0.03	- 6	21		1.9%	49.6% 36.1%	6.0%	0.4%	10.7%				0.01	0.00	0.0	0.12	43.3%	2.9%	15.1%	4.5%	0.4%	2.9%	42.0%
3 4 5 6 7 8 9 10 11 12 12 13 14 15 16 17 18 19 20 21 21 22 22 23 24 25 26 27			6				1 0					0.01				3.2%	36.4%	6.5%	0.5%	7.6%					0.00	0.00	0.06	22.4%	2.7%	14.7%	4.2%	0.5%	2.2%	30.4%
5		-	10		2	0.0	0 0	115	0.01	- 5	0.00	0.03		43		1.6%	40.4% 35.6%	4.3% 16.4%	0.5%	15.4% 7.5%		0.00	0.04	0.01	0.00	0.00	0.06	29.8%	1.1%	20.2%	3.2% 9.4%	0.5%	43% 21%	29.8% 39.3%
7			11		2	0.0	1 0	130	0.06		0.00	0.04		SI		2.3%	57.3%	11.5%	0.2%	6.6%	100.0%	0.01	0.12	0.03	0.00		0.28	53.1%	1.5%	23.4%	5.2%	0.2%	12%	53.1%
8			12		2 2	ö	1 0	121	0.02		0.00	0.04		AT .		2.3%	48.4% 31.2%	3.8% 9.5%	0.4%	8.7% 12.2%	100.0%	0.01		0.01	0.00	0.00		46.3% 37.9%	1.7%	21.9%	2.5% 5.5%	0.4%	165	46.3% 37.9%
10			10				1 0					0.03		46		1.0%	41.2%	15.4%	0.4%	5.5%					0.00		0.16	41.6%	1.5%	15.6%	8.8%	0.5%	2.25	43.6%
11			19		- 2		9 0				0.00	0.05		57		2.1%	60.9%	7.1%	0.2%	8.7%	100.0%	0.01			0.00	0.00	0.31	55.6%	1.4%	25.7%	1.5%	0.2%	1.7%	55.6%
12		-	20 24		2	0.0	0 0	120			0.00	0.06	- 0	A7		1.3%	41.9%	5.1%	0.2%	12.1%	100.0%				0.00	0.00	0.22	46.4%	0.8%	18.2%	2.0%	0.2%	5.1% 2.1%	46.4%
14			25		- 3	36	4 0	153	0.06	_	0.00	0.12		63		2.3% 3.9%	31.2% 51.0%	20.6% 7.4%	0.3%	9.3% 11.2%	100.0%	0.03	0.24	0.05	0.00	0.00	0.47	45.6%	1.3%	9.2% 23.0%	12.7%	0.3%	4.0%	44.2% 45.6%
15			26		- 5		4 0				0.00	0.07	- 1	.15		3.7% 2.9%	59.3% 54.1%	4.4% 2.2%	0.3%	6.5% 7.8%	100.0%		0.32	0.03	0.00	0.04		48.5% 50.1%	1.0%	27.5% 26.3%	2.8%	0.2%	15%	48.5% 50.1%
17		-	28		5		2 0				0.00	0.10		91		2.2%	41.1%	5.1%	0.4%	10.8%	100.0%		0.17			0.04		44.2%	1.5%	18.7%	2.9%	0.3%	455	44.2%
18			34		- 5	0.0		124			0.01	0.07	0.	.00		2.2%	27.1%	19.0%	0.6%	8.0%	100.0%		0.10			0.00		44.2%	1.7%	10.9%	12.5%	0.5%	1.9%	44.0%
19			35 36		5		4 0				0.00	0.12		22		1.0%	57.6% 56.6%	5.3% 3.8%	0.2%	9.5% 6.5%				0.03	0.00	0.00		50.4% 49.3%	2.6%	25.8% 27.9%	2.0%	0.2%	49%	50.4% 49.3%
21			37		- 5	0.0	2 0	52	0.03			0.10		05		2.4%	49.5%	12%	0.3%	9.2%	100.0%	0.02	0.25	0.02	0.00		0.51	49.0%	1.2%	23.5%	1.9%	0.3%	4.4%	49.0%
22			128				00					0.01		ä		0.6%	11.4%	10.7%	0.3%	15%					0.00	0.00	0.15	44.05	0.2%	9.2%	6.4%	0.2%	0.6%	44.8% 26.6%
24			132				0 0				0.00	0.01		40		0.5%	44.25 38.7%	175	0.5%	1.5%					0.00	0.00		47.9%	0.5%	13.6%	2.5%	0.5%	0.5%	47.9%
25			124		1	o o		114			0.00	0.01		.42		0.5%	12.5%	2.6%	0.5%	1.4%	100.0%	0.00			0.00	0.00		42.7%	0.5%	10.0%	2.1%	0.5%	0.5%	42.7%
26			136		1	0.0		130			0.00	0.00		39		0.5%	35.8% 42.2%	42% 67%	0.3%	1.0%				0.01		0.00		41.4%	0.5%	12.5% 14.4%	3.1% 5.0%	0.3%	0.3%	44.7% 48.4%
28			139		2	0.0	0 0	141	0.08	-	0.00	0.01	- č	82		0.4%	49.3%	9.0%	0.0%	0.8%	100.0%	0.00		0.05	0.00	0.00	0.51	61.2%	0.4%	18.4%	5.4%	0.0%	0.4%	61.2%
29			140		2	ö		141			0.00	0.01	0	.92		0.5%	44.9% 29.8%	1.7%	0.1%	0.9% 2.3%		0.00	0.15	0.01	0.00	0.00	0.55	59.7% 45.7%	0.4%	16.1%	1.0%	0.0%	0.4%	59.7% 45.7%
30			146		2	0.0	0 0					0.02	+ *	76		0.5%	29.80h	9.9%	0.7%	1.05					0.01	0.00	0.47	45.75	0.4%	20.2%	55%	0.6%	0.9%	56.0%
32	M P	atch	147		2	o.	0 0	41	0.04	ď	0.00	0.01	0.	86		0.4%	48.1% 42.6%	4.9%	0.1%	1.1% 2.2%	100.0%	0.00	0.15	0.02	0.00	0.00	0.51	59.6% 41.6%	0.2%	17.7% 14.7%	2.5%	0.1%	0.5%	59.6% 40.6%
28 29 30 31 32 33 34 35			148		- 2			138			0.01	0.02		#		1.1%	42.0%	16.0%	0.7%	2.5%	100.0%		0.13			0.00		48.6% 51.8%	0.3%	14.7%	9.2%	0.6%	1.0%	48.6% 51.8%
35			153		- 5	0.0	2 0	199	0.06		0.00	0.03		.07		1.0%	47.9%	4.1%	0.0%	1.2%	100.0%	0.02	0.46	0.04	0.00	0.00		63.8%	0.7%	22.4%	1.7%	0.0%	0.6%	63.0%
16			154		5	0.0	2 1	10	0.02	-	0.00	0.02		.01		1.0%	54.5% 51.6%	1.1%	0.0%	0.9%				0.01			1.28	63.6%	0.7%	25.7% 22.6%	0.6%	0.0%	0.4%	63.6%
38			156		5	0.0	2 1	.00	0.03	- 5	0.00	0.00		39		0.0%	41.7%	1.25	0.5%	1.7%	100.0%	0.02			0.00	0.00	1.24	51.7%	0.8%	17.9%	0.0%	0.1%	14%	51.7%
29		=	162				g 0				0.00	0.04		.12		1.2%	44.5%	11.4%	0.0%	2.0%		0.02			0.00	0.00	1.25	51.7%	1.0%	19.7%	4.0%	0.0%	1.0%	58.7%
40			163		3	0.0	2 1	97	0.06	-	0.00	0.02	+ 1	<del>%</del>		1.1%	50.6% 51.6%	2.95	0.0%	1.0%		0.02			0.00	0.0	129	67.9%	0.8%	23.4%	1.8%	0.0%	0.5%	63.2% 67.9%
42			165		- 5	0.0	2 1	103	0.03		0.00	0.06		25		0.7%	45.6%	1.5%	0.2%	2.7%		0.01					1.29	57.4%	0.5%	19.9%	0.8%	0.1%	1.3%	57.4%
43		-	0	128	2		1 0		0.07		0.00	0.03		65		0.9%	29.4% 50.5%	10.2% 7.4%	0.3%	5.2% 5.3%	100.0%	0.00	0.08	0.04	0.00	0.00	0.28	41.0%	0.6%	12.5%	6.0% 4.4%	0.3%	1.5%	43.0% 46.0%
45			4	132	2	0.0	1 0	28	0.05		0.00	0.03	- ŏ	.67		1.9%	40.9%	7.1%	0.6%	4.0%	100.0%	0.01	0.10	0.03	0.00	0.00	0.29	43.6%	1.5%	14.6%	4.0%	0.4%	1.6%	43.6%
46			6	134	2	ö	1 0	125			0.01	0.03		8		1.4%	37.4% 40.2%	5.0%	0.8%	4.0%	100.0%	0.01	0.08		0.00	0.00	0.26	39.8% 44.1%	1.1%	12.1%	1.7%	0.6%	1.2%	39.8% 44.1%
45		-	10	138			2 0				0.00	0.04	+ *	14		0.9%	40.7% 36.6%	4.8%	0.5%	6.7% 4.2%				0.11		0.00	0.46	40.6%	0.8%	15.8%	3.7% 9.4%	0.5%	1.6%	40.6%
49			11	139	-4	0.0	2 0	10.2	0.16	-	0.00	0.05		52		1.2%	54.3%	10.5%	0.1%	1.2%	100.0%	0.01	0.32	0.08	0.00	0.00	0.87	56.1%	0.8%	21.2%	5.5%	0.1%	1.4%	56.8%
50			12	140			0 0				0.00	0.05		53	_	1.6%	52.0% 40.4%	2.6%	0.2%	1.4% 6.7%	100.0%	0.02			0.00	0.00		57.1% 48.9%	1.2%	21.0%	1.4%	0.2%	1.6%	57.1% 48.9%
52			18	146	- 4	0.0	2 0	167	0.19		0.01	0.05		39		1.3%	48.1%	13.0%	0.4%	3.6%	100.0%	0.02			0.01	0.00		50.6%	1.3%	19.2%	7.5%	0.4%	1.5%	50.6%
16 17 18 19 40 41 41 41 44 45 46 47 48 49 50 51 52 53 54 55 57 58 58			19	147	4		2 0				0.00	0.07		SI		1.1%	56.1% 48.0%	6.1% 4.2%	0.1%	4.6%	100.0% 100.0%		0.34	0.05	0.00	0.00	0.09	58.0% 52.6%	0.7%	22.4% 17.1%	3.1% 3.0%	0.1%	2.1%	58.0% 52.6%
55			24	152	10	0.0			0.82		0.01	0.14		91		1.4%	49.3%	21.1%	0.7%	3.8%	100.0%	0.01		0.48	0.01	0.0	2.16	55.2%	1.1%	17.1%	12.2%	0.0%	1.1%	55.2%
56		_ <u>_</u>	25	153	10	0.0		33.			0.00	0.16	1	.12		2.8%	53.1%	6.2%	0.1%	525	100.0%	0.06		0.10	0.00	0.00	2.00	64.1%	1.9%	25.1%	3.2%	0.1%	2.4%	64.1%
57		-	26	154	10	0.0	6 1	92		1 5	0.01	0.10	+ 1	21		2.4%	58.2% 55.7%	2.5%	0.2%	10%		0.05		0.05	0.00	0.00	1.91	59.1%	1.6%	28.2% 26.2%	1.4%	0.1%	1.8% 2.8%	59.1% 66.2%
59			26	156	10	0.0	4 1	65	0.12	-	0.02	0.20	- 1	77		1.1%	43.7%	3.1%	0.5%	5.2%	100.0%	0.04	0.71	0.07	0.02		2.16	57.3%	0.9%	10.0%	1.9%	0.4%	2.7%	57.3%
65		F	34	162	10	0.0	6 1	59			0.01	0.11	- 1	39	ļ	1.8%	47.0% 55.1%	18.7%	0.2%	3.1% 4.2%	100.0%	0.05		0.29	0.01	0.00	2.05	60.5%	1.5%	21.3% 25.9%	8.4% 2.7%	0.2%	1.3%	60.7% 60.6%
62			36	164	10	0.0	7 1	.09	0.10		0.01	0.14		.00		2.4%	63.0%	3.4%	0.3%	3.7%	100.0%	0.04	0.95	0.07	0.01	0.00		65.6%	1.5%	31.7%	2.4%	0.3%	2.1%	65.6%
63			37	165	10	0.0	3 1	70	0.07		0.01	0.19	1.	50		1.0%	47.4%	2.0%	0.3%	5.3%	100.0%	0.03	0.77	0.04	0.01	0.11	2.24	62.6%	0.7%	21.6%	1.0%	0.2%	1.0%	62.6%

Table 4. PD of Ant M – patch antenna (39GHz – n260)

# - M-patch Low CH

$\overline{}$												1		may ratio ou	of all beams												max ratio out of all t			
Н		_	_	_			_	2 PD(mW/o	_									-			t 10mm eval			_						
					_		4cm	L PLIJEWYC	(HZ)		- ner	12% ratio	60.6%	27.5%	16%	15.6% mtio	100.0%	- 4	CRL PUIN	Wycmz) a	e tonn eva	suston a	stance	57.2% ratio	2.7% mtio	20.1% min	182% ratio	2.2% ratio	6.8%	\$7.2% (16)
NO.	Wodule Typ	e Beam ID.	1 Berna ID,2	Feed no.	S4(Right) S3	Left) SS(1	Top) S	6(Tottom)	\$1(Front)	S2/Rea	Beam Back-oft	(Right 2mm)/(worst- surface 2mm)	(Left 2mm)/(wont- surface 2mm)	(Top 2mm)/(wonst- surface 2mm)	(Sottom 2mm)/(worst- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)		S4(Right)	\$3(Left)	SS(Top)	SE(Bottom)	S1/Fee	nt) S2/Rear	worst-surface (10mm/2mm)		(Left 10mm)/(worst- surface 2mm)	(Top 10mm(/(wonst- surface 2mm)	(Bottom 10mm)/(worst- surface 2mm)	(Front 10mm)/(wont- surface 2mm)	(Rear 10mm)/(wont- surface 2mm)
1		0				00 00		0.00	0.00	0.21		1.0%	41.3% 34.1%	11.2%	0.5%	1.9%	100.0% 100.0%	0.00	0.03	0.01	0.00	0.00	0.08	39.8%	1.0%	12.6%	5.8% 10.8%	0.5%	0.5% 1.6%	39.8% 30.3%
3 4		4			0.00	0.0	02	0.00	0.01	0.19		1.9%	42.1%	8.4%	0.5%	6.1%	100.0%	0.00		0.01	0.00	0.00		39.7%	1.4%	15.9%	5.6%	0.5%	1.4%	39.7%
4		6	+	-	0.00 0	07 00	01	0.00	0.01	0.15	+	1.4%	45.9% 38.3%	6.8%	0.7%	5.5%	100.0%	0.00	0.03	0.01	0.00	0.00		41.8% 32.2%	1.4%	19.2%	3.4% 4.9%	0.7%	2.1%	41.8% 32.2%
6		10		2	0.01	20 0.0	00	0.00	0.02	0.44		1.1%	44.1%	18.2%	0.5%	3.4%	100.0%	0.00	0.07	0.05	0.00	0.01	0.15	33.8%	0.9%	14.6%	10.6%	0.5%	1.45	33.8%
7		11	+	2		12 0.0	03	0.00	0.02	0.31	+	1.9%	29.9% 48.8%	13.6%	0.6%	5.2% 5.2%	100.0% 100.0%	0.01		0.02		0.01		37.3% 52.7%	1.6%	17.5%	7.8% 5.8%	0.6%	1.6%	37.3% 52.7%
5 7 8 9 10		13		2		20 00 11 00			0.01	0.46	_	1.5%	42.6% 14.2%	14.4%	0.9%	1.1% 8.5%		0.01		0.04		0.00		42.4% 29.4%	1.1%	14.4%	9.0% 7.6%	0.7%	1.1%	42.4% 29.4%
11		19		2	0.01 0	18 0.0	03	0.00	0.02	0.34		2.9%	52.8%	9.0%	0.9%	7.0%	100.0%	0.01	0.08	0.02	0.00	0.00	0.19	54.5%	2.3%	22.7%	6.7%	0.6%	1.2%	54.5%
12		20	+	- 2		19 0.0		0.00	0.02	0.40	-	1.8%	48.1% 50.5%	9.3% 26.0%	0.5%	5.3% 5.2%	100.0%	0.01	0.08	0.02	0.00	0.00		46.1%	1.5%	20.7%	5.3% 18.2%	0.3%	2.0%	46.1% 31.7%
14		25		3	0.01 0	20 0.0	00		0.09	0.43		3.1%	47.8%	19.5%	1.6%	21.4%		0.01				0.00	0.20	47.2%	2.1%	24.2%	8.2%	0.9%	4.9%	47.2%
15		26 27		5		42 0.0		0.00	0.05	0.80	+	2.1%	51.3% 60.5%	1.5%	0.4%	5.9%	100.0%	0.01		0.02	0.00	0.00	0.42	52.9% 53.0%	1.6%	26.3%	2.1%	0.2%	1.4%	52.9% 55.0%
17		28		5	0.01 0	47 0.2	22	0.01	0.05	0.95		1.4%	49.6%	23.5%	0.6%	5.0%	100.0%	0.01	0.23	0.11		0.00	0.55	57.2%	1.2%	24.2%	11.4%	0.5%	2.5%	57.2% 10.9%
19		34		3	0.01	28 01 36 01	67	0.00	0.06	0.49	+	2.0%	57.4% 59.8%	27.5% 12.2%	0.8% 1.2%	11.8% 14.2%	100.0%	0.01	0.18		0.00	0.65	0.34	39.9% 54.5%	1.6%	20.4% 30.1%	17.9% 6.3%	0.4%	115	56.5%
20		36	_	5		46 0.0		0.01	0.03	0.81		1.9%	57.3% 54.8%	4.1% 10.4%	0.9%	3.4% 5.4%	100.0% 100.0%	0.01	0.22	0.02	0.00	0.00		56.1% 55.3%	1.6%	27.7% 26.6%	2.6% 5.6%	0.5%	1.4%	56.1% 55.3%
22		128		í	0.00	06 00	01	0.00	0.02	0.18		1.7%	32.8%	5.0%	23%	11.3%	100.0%	0.00	0.02	0.01	0.00	0.00	0.08	42.4%	1.1%	13.6%	3.4%	1.1%	1.7%	42.4%
23		130	+	1		06 0.0		0.00	0.01	0.15	+	2.6%	41.7% 47.1%	4.7%	2.6%	7.9% 11.0%	100.0%	0.00	0.02	0.01	0.00	0.00		31.4%	2.0%	15.2% 16.2%	4.6% 3.1%	1.3%	2.6%	38.4% 38.7%
25		134		1		05 0.0		0.00	0.03	0.16		1.3%	22.1%	8.2%	0.6%	17.0%	100.0%	0.00	0.02	0.01	0.00	0.01	0.06	37.7%	1.2%	11.9%	4.4%	0.0%	2.1%	37.7%
27		126		2		13 0.0		0.00	0.01	0.13	+	0.8%	51.5% 44.3%	3.15 9.15	0.0%	5.5% 17.4%		0.00		0.00	0.00	0.00		41.3% 30.2%	0.8% 2.3%	23.6%	1.6%	0.0%	1.6%	43.2% 30.2%
28		139	-	2		14 00		0.00	0.02	0.35	-	2.0%	40.3% 29.1%	435 325	0.9%	6.5%	100.0% 100.0%	0.01	0.07	0.01	0.00	0.00		43.5%	1.7%	20.2%	2.1% 1.8%	0.6%	2.3% 1.8%	43.5%
30		141		2	0.00	07 0.0	02	0.00	0.05	0.24		1.7%	29.0%	9.2%	0.4%	21.4%	100.0%	0.00	0.03		0.00	0.01	0.08	31.9%	1.3%	12.2%	5.0%	0.4%	3.8%	31.9%
31	M Date	146 h 147		2		13 00	03	0.00	0.09	0.36	+	2.2%	14.5% 15.6%	9.1% 5.2%	0.8%	24.0% 4.5%	100.0% 100.0%	0.01	0.05	0.02	0.00	0.00		43.4%	1.7%	14.6%	4.7% 2.6%	0.3%	1.9%	43.4% 47.1%
22		140		2	0.01	11 0.0	03	0.01	0.04	0.32		1.6%	15.2%	9.4%	2.8%	11.0%	100.0%	0.00	0.05	0.02	0.01	0.01		45.3%	1.2%	16.4%	5.0%	1.6%	1.9%	46.9%
34		152	+	5	0.02 0	32 00	08	0.02	0.16	0.59	+	2.6%	41.6% 49.5%	12.8% 11.3%	3.1% 1.4%	31.3% 25.2%	100.0% 100.0%	0.01	0.13	0.04	0.01	0.0	0.27	45.5%	1.5%	22.2%	7.0% 5.5%	1.9%	6.0% 1.9%	45.5% 45.9%
26		154		5		39 00		0.00	0.04	0.96	_	1.0% 2.1%	40.4% 44.0%	10%	0.3% 1.2%	425 625	100.0%	0.02	0.20	0.01	0.00	0.00	0.44	45.5%	2.3%	20.4%	1.5% 1.0%	0.2%	2.5% 2.4%	45.5% 46.4%
38		156		5	0.01 0	25 0.1	10	0.02	0.06	0.55		2.5%	45.1%	17.5%	3.6%	11.6%	100.0%	0.01	0.11	0.07	0.01	0.00	0.21	37.8%	1.3%	20.2%	11.0%	2.2%	3.8%	37.0%
29		162	+	5		27 0.0	09	0.01	0.20	0.59	-	2.4%	45.3% 47.6%	14.4%	1.9%	14.5% 4.1%	100.0%	0.01	0.12	0.04	0.01	0.00		45.0%	2.2%	21.1%	7.1%	1.0%	5.8% 1.2%	46.0% 41.3%
41		164		5		35 0.0		0.01	0.04	0.78		1.8%	44.7%	2.8%	0.6%	4.5%	100.0%			0.02	0.00	0.00		46.5%	1.3%	23.9%	1.9%	0.4%	2.2%	46.5%
13 14 15 15 15 15 15 15 15 15 15 15 15 15 15		165	128	2		26 0.0 17 0.0		0.02	0.07	0.63	+	1.9%	42.2% 42.1%	12.6%	2.4%	11.2% 7.6%	100.0%	0.01	0.12	0.05	0.01	0.00		42.9%	1.3% 1.5%	19.2%	7.2% 6.5%	1.4%	1.0%	42.9% 42.8%
44		2	130	2		16 00		0.01	0.03		-	1.7%	29.8% 45.1%	13.8%	2.4%	8.3% 12.8%	100.0%	0.01		0.04		0.01		31.3% 31.8%	1.5%	12.6%	10.0%	1.5%	2.4%	33.3% 38.8%
46		- 2	134	2	0.01	34 04	63		0.06	0.32		2.2%	43.8%	8.55	0.7% 0.6%	18.9%		0.01	0.06	0.01	0.00	0.0	6.13	41.3%	1.6%	18.0%	1.4%	0.3%	2.7% 3.2%	41.3%
47		8	136	4		37 0.1		0.00	0.03	0.36		0.0%	44.5% 44.3%	5.6% 18.7%	0.6%	8.7% 11.8%	100.0% 100.0%	0.00	0.07	0.02	0.00	0.00		38.3%	0.8% 1.6%	18.3%	4.2% 12.8%	0.6%	1.4% 2.8%	38.3% 31.2%
49		11	139	4	0.02 0	28 0.0	00	0.01	0.05	0.71		2.5%	19.5%	11.7%	1.4%	7.1%	100.0%	0.02	0.13	0.05	0.01	0.00	0.28	29.2%	2.1%	18.5%	7.2%	0.8%	1.8%	19.2%
50		12	140	4		22 0.0		0.01	0.04	0.57	+	2.4%	38.7% 42.5%	8.2% 18.1%	1.0%	6.6% 16.7%	100.0%	0.01	0.11	0.03	0.00	0.00		41.6%	1.9%	18.7%	5.4% 12.0%	0.7%	1.9%	43.6% 44.8%
52		18	146		0.02 0	31 0.0	09	0.01	0.19	0.77		2.3%	40.8%	12.0%	0.8%	24.9%	100.0%	0.01	0.13	0.05	0.00	0.0	0.31	23.9%	1.8%	17.1%	6.4%	0.4%	4.0%	19.9%
54		20	147	4	0.02 0	34 0.0 33 0.1	10		0.05	9,71	+	2.0%	42.5% 47.2%	9.5% 13.4%	0.7%	7.8% 7.3%		0.01		0.05	0.01	0.00		46.8% 48.2%	1.7%	18.7%	6.4% 7.6%	0.5%	1.6% 2.8%	46.8% 48.2%
55		24	152	10		76 0. 68 0.		0.04	0.26	1.49	F	1.7%	50.7% 46.0%	23.6%	2.1%	19.0%	100.0%	0.02		0.24	0.02	0.00		41.1%	1.5%	24.0%	16.0%	1.4%	4.45	41.1%
57		26	154	10	0.05	82 0.0	00	0.01	0.08	1.03		2.9%	44.7%	4.2%	0.6%	4.6%	100.0%	0.04	0.40	0.05	0.01	0.00	0.91	49.7%	2.3%	21.7%	2.5%	0.3%	1.8%	49.7%
58		27 28	155	10	0.04 0	91 0.1		0.03	0.13	1.72	₽	2.1%	52.8% 55.2%	7.5% 23.3%	1.9%	7.5% 7.2%	100.0%	0.03	0.45	0.07	0.02	0.00		47.4% 54.0%	2.0%	25.9% 27.1%	1.9%	1.0%	3.1% 3.4%	47.4% 54.0%
60		34	162	10		62 02	25	0.03	0.45	1.26		2.0%	49.9%	20.1%	2.1%	15.6%	100.0%	0.02	0.31	0.15	0.02	0.00	0.60	47.2%	1.6%	24.2%	11.8%	1.2%	6.8%	47.7%
62		35	163	10	0.03 0	92 0.1	07	0.03	0.24	1.74	+	2.4%	52.9% 49.3%	1.85 3.85	15%	13.8%	100.0%	0.03	0.47	0.05	0.02	0.04	0.85	48.9%	2.0%	25.2% 24.6%	1.9% 2.5%	0.9%	2.3% 2.5%	48.9% 48.1%
63		37	165	10	0.03	01 0.	26	0.04	0.13	1.66		2.0%	60.6%	15.7%	2.1%	7.8%	100.0%	0.03	0.49	0.17	0.02	0.00	0.89	53.6%	1.7%	29.6%	10.2%	1.1%	3.8%	53.6%

## - M-patch Mid CH

															max ratio ou	t of all beams												max ratio out of all b	eams.		
							4cn	n2 PD(m)	N/cm2)				16%	66.7%	26.6%	12%	19.1%	100.0%	4cm2 PD(r	nW/cm2	t) at 10mm	evaluati	ion distan	2	62.0%	2.2%	11.6%	184%	1.1%	49%	62.0%
No. M	odule Typ	se Seam ID_1	Berna ID,2	Feed no.		Т	П		Т			per Beam	ratio (Right 2mm)/(worst-	ratio (Left 2mml/Iwont-	ratio (Top 2mm)//wont-	ratio (Bottom 2mml/Iwont-	ratio (Fornt 2mm)/(wont)	ratio (Rear 2mm)//worst-	S4/Right S3/Left						ratio worst-surface	ratio (Right 10mm)//wont-	ratio (Left 10mm)/(wont-	ratio (Top 10mm)//wont-	ratio (Bottom	ratio (Front 10mm)//wont-	ratio (Rear 10mm)//wont-
					S4(Right) S3(Lef	ti 55(	(Top)	SE(Totto	n) 51/F	ront) 1	S2(Rear)	Back-off	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)	54(regit) SJLIR	22(10	b) ze(sce	morn) S	( ) (Hong)	52(9000)	(10mm/2mm)	surface 2mm)	surface 2mm)	surface 2mm)	10mm)/(worst- surface 2mm)	surface 2mm)	surface 2mm)
1				1	0.00 0.09	0.	03	0.00	0.	01	0.24	1000	12%	36.1% 12.1%	12.9%	0.4%	2.5%		0.00 0.03				0.00	0.10	41.1%	0.8%	12.0%	7.1% 8.5%	0.4%	0.8%	41.1%
3		4			0.00 0.10				0	01	0.21		0.8%	40.5%	9.9%	0.4%	2.8%	100.0%	0.00 0.04	0.00	0.0	10	0.00	0.07	35.9%	0.8%	9.4%	6.7%	0.5%	0.8%	16.9%
4		6		-	0.00 0.08	9	25	0.00	90	91	0.16		1.3%	52.9% 43.1%	455	0.6%	5.7%	100.0%	0.00 0.04		0.0		0.00	0.07	46.5%	135	22.9%	12%	0.0%	1.9%	46.5%
6		10		2	0.01 0.20	0.	.10	0.00	0		0.40		1.2%	41.8%	20.7%	0.8%	2.7%		0.01 0.07				0.01	0.16	32.9%	1.0%	15.3%	12.8%	0.6%	1.0%	32.9%
7 0		11	<del>-</del>	2	0.00 0.13			0.00	0	02	0.10		1.0%	13.7% 42.4%	14.4%	0.3%	47% 15%		0.00 0.06	0.0	0.0		0.01	0.16	41.3% 51.9%	0.8%	15.7%	9.4% 3.7%	0.3%	1.3%	41.3% 51.9%
3 6 7 8 9		13		2		0.		0.01	0.	01	0.51		1.6%	40.9% 29.5%	16.2%	1.0%	1.8%		0.01 0.07	0.00	0.0		0.00	0.21	41.3% 30.1%	1.4%	14.2%	10.1% 7.2%	0.8%	0.8%	41.3%
11		19			0.01 0.20	0	03	0.00	o	01	0.39		1.2%	51.8%	7.2%	0.8%	2.1%	100.0%	0.00 0.09		0.0	10	0.00	0.22	55.9%	1.0%	23.7%	6.1%	0.5%	1.0%	55.9%
12		20	-	3	0.00 0.20	0	26	0.00	0	02 04	1.00	_	0.9%	45.3% 46.7%	2.5% 23.8%	0.4%	185		0.00 0.09				0.01	0.22	41.9% 34.9%	135	19.4%	5.8% 18.4%	0.2%	13%	48.9% 34.9%
14		25 26			0.01 0.21			0.00	0	07	0.54		1.5%	18.5% 66.0%	8.9% 8.4%	0.7%	12.3%		0.01 0.11	0.00	0.0	10	0.02	0.25	45.6% 62.0%	1.3%	19.7%	4.8% 5.9%	0.4%	43% 17%	45.6% 62.0%
16		27		5	0.01 0.49	0.	.04	0.00	0	02	0.93		1.5%	52.8%	4.6%	0.4%	2.6%	100.0%	0.01 0.26	0.00	0.0	10	0.01	0.52	55.8%	1.4%	27.6%	3.4%	0.3%	1.5%	55.8%
17		28	1	5	0.02 0.42		18	0.01	0.	03	0.97		1.7%	43.2% 44.0%	18.2%	1.1%	1.2% 5.8%		0.01 0.19	0.00	0.0	10	0.01	0.52	53.8% 45.0%	1.3%	20.1%	8.9% 18.2%	1.1%	1.2%	53.8% 45.0%
19		35 36		5		0		0.00	0.	08	0.64		1.9%	50.8% 57.8%	11.0%	0.5%	11.9%	100.0%	0.01 0.17		0.0		0.02	0.32	49.5% 59.8%	1.4%	26.6%	6.2%	0.3%	2.8%	49.5% 59.8%
20		27			0.02 0.44	0	08		0	02	0.97		1.0%	46.4%	8.2%	0.4%	2.4%	100.0%	0.02 0.23	0.0	0.0	10	0.01	0.58	55.0%	1.6%	23.5%	4.4%	0.2%	1.4%	55.0%
22		128			0.00 0.10					01	622		1.2%	40.8% 41.2%	5.7%	12%	4.9%		0.00 0.04				0.00		42.9%	0.8%	15.9%	13%	0.4%	1.6%	42.9%
24		132		1	0.00 0.09	0.	01	0.00	0	02	0.21		1.4%	42.7%	4.7%	0.5%	8.5%	100.0%	0.00 0.03	0.00	0.0	10	0.00	0.09	42.3%	0.9%	13.7%	3.3%	0.5%	1.4%	40.3%
25		134	-	-		0 0		0.00	0	01	0.18		2.0%	38.0% 42.4%	2.9%	0.0%	3.4% 5.6%	100.0% 100.0%	0.00 0.03		0.0		0.00	0.08	31.0% 45.9%	1.5%	14.1%	2.0%	0.0%	1.5%	38.0% 46.9%
27		138	_	2	0.01 0.14	0.0	03	0.00	Ö	05	0.36		1.9%	29.7% 45.2%	8.5% 2.4%	0.6%	13.8%	100.0%	0.01 0.05	0.00	0.0	10	0.01	0.10	26.7%	1.4%	13.8%	5.2%	0.2%	1.0%	26.7% 48.2%
29		140		2	0.01 0.17	0		0.00	o	01	0.37		1.6%	44.9%	2.9%	0.3%	1.7%	100.0%	0.00 0.01		0.0		0.01	0.17	45.5%	1.1%	21.1%	2.1%	0.2%	1.3%	46.5%
30 31 32 33		141	+		0.01 0.18		62			02 04	0.34	-	1.2% 1.8%	32.4% 40.6%	485	0.3% 0.2%	7.1% 9.0%	100.0%	0.00 0.05	0.0	0.0	10	0.01	0.12	34.2% 47.3%	0.6%	13.7% 18.5%	3.0% 2.8%	0.2%	2.1% 1.6%	34.2% 47.3%
32	M Pat	th 147			0.01 0.19			0.00		62	0.52		1.9%	44.7%	4.5%	0.4%	4.1%		0.01 0.11				0.01	0.26	49.7%	1.2%	21.0%	57%	0.2%	1.4%	49.7%
34		152		5	0.02 0.34	0.	.04	0.01	0.	11	0.84		2.3%	40.0%	4.9%	0.8%	13.4%	100.0%	0.02 0.16	0.00	0.0	10	0.02	0.37	43.5%	1.8%	18.7%	2.0%	0.5%	2.6%	43.5%
35		153	1	5	0.02 0.40	0 0		0.01	0	14	1.22	_	2.2% 3.0%	41.9% 44.3%	6.9%	0.8%	15.0% 2.6%	100.0% 100.0%	0.02 0.20		0.0		0.02	0.44	47.8% 50.3%	1.7% 2.1%	21.7%	3.1% 1.1%	0.4%	2.6%	47.8% 50.3%
37 38		155 156		5	0.02 0.45		06	0.00	a	05	0.98		2.3%	45.9% 47.5%	6.1%	0.3%	435		0.01 0.22		0.0	10	0.02	0.48	48.5% 17.7%	1.4%	22.7% 23.5%	3.7% 11.4%	0.2%	1.9%	48.5% 37.7%
29		162		5	0.02 0.35			0.00	0		0.87		1.0%	40.8%	8.0%	0.8%	19.1%	100.0%	0.01 0.17	0.00			0.03	0.40	45.3%	1.5%	19.3%	3.0%	0.2%	1.0%	46.2%
29 40 41 42		163	_		0.03 0.52				0 0	04 04	1.09		2.7%	47.7% 41.7%	27%	0.6%	125	100.0%	0.02 0.27				0.02	0.54	49.5%	2.1% 1.7%	24.7%	1.6%	0.4%	1.9%	49.5% 50.9%
42		165	128		0.03 0.44			0.01	0	30	0.81		1.6%	54.3% 41.4%	14.3%	0.6%	7.1%		0.02 0.22				0.03	0.34	42.0%	2.1%	26.9%	10.9%	0.2%	3.2% 1.2%	42.0% 42.8%
44		2	120	2	0.01 0.20	_ a	05	0.01	o	03	0.49		1.6%	40.6%	10.0%	0.6%	5.3%	100.0%	0.01 0.07	0.00	0.0		0.01	0.17	34.2%	1.2%	13.9%	6.6%	0.4%	1.6%	34.2%
44 45 46 47 48		- 4	132	2	0.01 0.22	0.	05	0.00	0.0		0.50		1.4%	44.0% 49.6%	9.3%	0.4%	8.1% 8.0%	100.0%	0.01 0.08		0.0	10	0.01	0.19	37.3% 42.4%	1.2%	15.9% 23.1%	6.2% 3.6%	0.2%	1.8% 2.2%	37.3% 42.4%
47			126	2		0		0.00	a	02	0.41		1.2%	46.0%	1.9%	0.5%	5.9%		0.00 0.01		0.0		0.01	0.18	43.8%	1.0%	18.6%	2.9%	0.2%	125	43.8%
49		10	138		0.02 0.38	0		0.01	0	09 05	0.93		2.0%	41.2% 41.0%	17.0% 9.7%	0.5% 0.7%	9.2% 5.3%		0.02 0.15				0.02	0.46	29.0% 50.4%	1.7%	16.1% 19.7%	11.0% 5.4%	0.5%	2.3% 1.7%	29.0%
50		12	140	4	0.01 0.33	0		0.00	0	03	0.75		1.6%	44.0% 27.4%	5.8% 16.8%	0.4%	4.0% 7.3%	100.0%	0.01 0.16	0.00	0.0	10	0.01	0.36	47.6% 38.2%	1.2%	20.7%	11.6%	0.3%	1.7%	47.6% 38.2%
52		18	146	- 4	0.02 0.42	0	09	0.00	0.	08	0.92		2.3%	45.8%	9.9%	0.3%	9.0%	100.0%	0.02 0.18	0.00	0.0	10	0.02	0.29	41.7%	1.7%	19.4%	6.6%	0.2%	2.0%	41.7%
53		19	147	4	0.02 0.48	0		0.01	0 0	05	0.99	_	1.8%	48.2% 49.5%	5.4% 11.5%	0.7%	42%		0.01 0.21				0.02	0.53	53.5% 49.8%	1.1%	21.2%	4.0% 6.7%	0.4%	1.5%	53.5% 49.8%
54 55 56 57 58		24	152	10	0.03 1.01	0	36	0.01	0		1.77		1.9%	56.9%	20.2%	0.7%	9.1%	100.0%	0.03 0.49	0.25	0.0	9	0.05	0.83	46.7% 47.9%	1.6%	27.8%	13.9%	0.4%	2.5%	46.7%
57		25 26	154	10	0.05 1.30	0	12	0.01	0	10	2.24		1.8%	42.5% 57.9%	10.5%	0.9%	4.7%	100.0%	0.03 0.37	0.09	0.0		0.09		57.9%	1.6%	20.5%	5.0%	0.4%	4.9% 1.2%	47.9% 57.9%
58		27	155	10	0.04 1.32	0		0.01	0	11	2.21		1.9%	60.0% 55.6%	4.9%	0.5%	7.1%		0.03 0.67			9	0.06	123	55.6%	1.4%	10.4% 27.2%	1.0%	0.3%	2.6%	55.6% 50.1%
60		34	162	10	0.02 0.80	0.	26	0.01	o.	28	1.64		1.5%	48.5%	15.7%	0.9%	16.9%	100.0%	0.02 0.38	0.13	0.0	11	0.06	0.00	41.5%	1.2%	23.3%	10.1%	0.5%	1.5%	40.5%
62		35 36	163		0.04 1.32		07	0.02			2.20		2.4% 1.7%	49.5% 54.1%	5.7% 2.9%	0.7%	7.4% 3.4%	100.0%	0.04 0.56	0.00	0.0	9	0.04	1.16	52.5% 54.9%	1.9%	25.2% 27.8%	2.7%	0.4%	2.0% 1.2%	52.5% 54.9%
63		37	165	10	0.07 1.27	0.	28	0.01	0.	11	1.90		2.4%	66.7%	14.9%	0.7%	5.9%	100.0%	0.04 0.64	0.71	0.0	11	0.07	1.15	60.5%	2.3%	13.5%	9.7%	0.4%	3.4%	60.5%

# - M-patch High CH

_													_			max ratio out	of of house			_						_			max ratio out of all			
Н		_			_			dam's	PD(mW/c				+			1100 00	G 21 CH2III			-	2 DD/	attition To a	t 10mm eval	tuetas et		-			1	1		
					ŀ		_	40102	PUITMY	:HL2)		per	+	19%	SLES	28.4%	1.7%	9.1%	100.0%	_	CRU PUIT	wycmz) i	e tonn eva	suston a	utance	647%	2.6%	28.2%	21.0%	1.6% ratio	3.5%	64.7%
No.	Module 1	pe Seam	ID_1 Bema	D,2 A	red no.	S4(Right) S31.er	n SS(To		(Tottom)	S1/Empf	52/Res	Dearn		ratio pht 2mm\/(worst-	ratio (Left 2mm)/(wont-	ratio (Top 2mm)/(wonst-	ratio (Bottom 2mm)/(worst-	ratio (Fornt 2mm)/(worst-		54(Right)	53(Left)	SS(Top)	S6(Bottom)	\$1(Fro	nt) S2(Rear)	ratio worst-surface	ratio (Right 10mm)/(worst-	ratio (Left 10mm)/(wont-	ratio (Top 10mm)/(wonst-	(Bottom 10mm)//wont-	ratio (Front 10mm)/(worst-	ratio (Rear 10mm)/(wont-
						. , .	1			STIPPORE	52960	(49)		surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)							(10mm/2mm)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2 mm)	surface 2mm)	surface 2mm)
2		- 2		+	1		0.00		0.00	0.01	0.10	+	+	1.6%	31.3% 30.2%	11.4%	0.8%	3.7% 4.9%	100.0% 100.0%	0.00	0.02	0.02	0.00	0.00	0.12	47.2% 39.0%	1.2%	9.3%	6.9%	0.8%	0.8%	47.2% 39.0%
2 3 4 5 6 7 8 9		- 1		$\pm$	1		0.00		0.00	0.01	0.25	-	7	0.8%	35.9% 48.6%	11.0%	0.4%	2.9%	100.0%	0.00		0.02	0.00	0.00		37.6%	0.4%	12.7%	7.0%	0.4%	0.8%	37.6%
5				_		0.00 0.11	0.00		0.00	0.00	0.24			0.8%	44.3%	1.0%	0.4%	1.7%	100.0%	0.00	0.04	0.01	0.00	0.00	0.10	40.1%	0.8%	15.2%	2.1%	0.4%	0.8%	40.1%
7		11		$\rightarrow$	2		0.00		0.00	0.01	0.49	+	+	1.2%	34.8% 36.2%	17.3% 14.0%	0.8%	2.8% 8.2%	100.0%	0.01	0.06	0.05	0.00	0.01		35.4%	1.2%	12.2%	10.6% 8.2%	0.8%	1.2%	35.4% 51.4%
8		1			2		0.00			0.02	0.34		_	0.9%	27.3% 21.5%	6.1%	0.9%	5.8%		0.00	0.05	0.01	0.00	0.00		59.2% 44.8%	0.9%	14.0%	4.1% 8.1%	0.6%	1.2%	59.2% 44.8%
10		- 11			2	0.00 0.19	0.00	5	0.00	0.01			_	0.9%	42.4%	10.5%	0.4%	23% 635	100.0%	0.00	0.08	0.03	0.00	0.01		35.9%	0.7%	17.0%	7.6%	0.2%	1.1%	35.9%
		20		_	2	0.01 0.21	0.04	4	0.00	0.02	0.47	+-	+	1.1%	33.5% 44.1%	9.1%	0.4%	3.2%	100.0%	0.00	0.05	0.03	0.00	0.00	0.22	59.7% 46.8%	0.8%	13.2%	3.5% 6.5%	0.9%	0.8%	59.7% 46.8%
13		21		+	5	0.02 0.45	0.21		0.00	0.05	1.03	-	7	1.5%	43.6% 46.6%	25.0% 9.5%	0.4%	4.0%	100.0% 100.0%	0.01	0.17	0.18	0.00	0.02		38.6% 50.2%	1.3%	16.8%	16.9%	0.3%	2.0%	38.6% 50.2%
15		21		_	5	0.01 0.44	0.00	5	0.00	0.06	0.79			1.4%	55.5% 48.7%	6.3%	0.5%	8.1%	100.0%	0.01	0.22	0.03	0.00	0.01	0.49	61.6%	1.1%	28.3%	1.9%	0.3%	1.1%	61.6% 64.7%
13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28		21		$\pm$	5	0.01 0.46	0.1		0.01	0.02	1.07		+	0.8%	43.1%	15.0%	0.7% 1.7%	2.4%	100.0%	0.01	0.21	0.03	0.00	0.01		54.5%	0.6%	24.0%	6.7%	0.3%	0.7% 1.6%	54.5%
18						0.01 0.35	0.27			954			_	14%	47.8% 52.8%	28.4%	0.4%	5.3% 6.3%		0.01	0.20	0.17	0.00	0.02		48.0% 55.6%	1.1%	24.2% 26.5%	21.0% 3.0%	0.4%	2.3% 1.4%	48.0% 55.6%
20		31		-	5	0.02 0.43	0.00	5	0.01	0.04	0.89	=	1	1.8%	48.3% 48.7%	6.0%	0.9%	19%	100.0%	0.01	0.23	0.03	0.00	0.01		60.9%	1.6%	25.8%	17%	0.4%	0.9%	60.9%
22		12	0	_			0.00		0.00	0.02	0.27	+	+	1.9%	29.1%	6.4%	0.4%	3.8%	100.0%	0.00	0.03	0.01	0.00	0.00	0.12	43.8%	1.1%	9.8%	3.4%	0.0%	0.8%	43.0%
23		13		-	-	0.00 0.03	0.01		0.00	0.01	0.29	-	+	1.4%	12.6% 17.2%	4.9% 3.4%	0.0%	15% 11%	100.0%	0.00	0.03	0.01	0.00	0.00		35.4%	1.1%	10.9%	3.2% 1.8%	0.0%	1.1%	35.4% 36.9%
25		13	4	_	1		0.01		0.00	0.01	0.26		•	1.1%	15.0%	1.0%	0.0%	2.3%	100.0%	0.00	0.03	0.01	0.00	0.00	0.11	42.3%	0.8%	12.9%	2.3%	0.0%	1.1%	40.3%
26		12	0	$\pm$	2		0.00		0.00	0.00	0.21	_	+	1.5%	36.7% 33.8%	1.9% 5.7%	0.0%	1.9%	100.0%	0.00	0.03	0.00	0.00	0.00	0.10	47.8% 31.8%	0.5%	14.0%	1.0%	0.0%	0.5%	47.8% 31.8%
28		13	9	=	2	0.01 0.17	0.0	-	0.00	0.02	0.54	-	-	2.0%	31.2% 24.0%	2.4%	0.2%	45% 2.8%	100.0%	0.01	0.07	0.01	0.00	0.01	0.29	53.2% 53.2%	1.3%	13.4% 24.5%	1.3%	0.0%	1.3%	53.2%
30		14		=	2	0.00 0.17	0.00		0.00	0.01	0.50		•	0.8%	11.9%	40%	0.2%	2.8%	100.0%	0.00	0.08	0.01	0.00	0.01		37.3% 47.5%	0.6%	15.1%	2.4%	0.2%	1.4%	37.3%
22	M P	tch 14	7	_	2	0.01 0.15			0.00	0.02	0.53	_	-	2.3%	28.9%	4.0%	0.2%	4.5%	100.0%	0.01	0.06	0.02	0.00	0.01		50.0%	1.5%	11.9%	2.3%	0.2%	1.1%	50.0%
22		14	2	-	2 5	0.01 0.17	0.05		0.00	0.02	0.52	_	Ţ	1.9%	33.6% 37.4%	10.1%	0.2%	15% 42%	100.0%	0.01	0.08	0.03	0.00	0.01		38.1% 44.2%	1.4%	15.5% 18.2%	6.0%	0.2%	1.4%	38.1% 44.2%
35		15	2	#			0.00		0.00	0.04	1,31	-	Ł	2.4%	41.0% 23.5%	2.2%	0.2%	2.9% 1.0%		0.02		0.02	0.00	0.02		51.9% 54.4%	1.8%	20.1%	1.5%	0.1%	1.6%	51.9% 54.4%
36		15	5		5	0.03 0.51	0.04			0.03	133	_	÷	2.6%	46.3%	5.8%	0.2%	3.8%	100.0%	0.02	0.25	0.04	0.00	0.02	0.52	46.6%	1.4%	22.9%	1.7%	0.1%	1.9%	46.6%
38		15		+	5	0.02 0.45	0.13	2	0.00	0.05	1.07	_	Ψ.	2.0%	42.2% 29.4%	15.4%	0.4%	5.0% 4.4%	100.0%	0.01	0.22	0.09	0.00	0.03	0.47	47.9%	1.1%	20.8%	1.4%	0.3%	2.8%	44.2%
40		16	3	_	5	0.04 0.48	0.00		0.00	0.03	1.21		•	3.1% 3.2%	39.3% 40.5%	2.1% 4.5%	0.2%	2.2%	100.0%	0.02	0.25	0.02	0.00	0.02		56.0% 47.3%	2.0%	20.5% 19.2%	1.4%	0.2%	1.2%	56.0% 47.3%
42		16	5		5	0.03 0.56		2	0.00	0.05	1.10		Ė	2.6%	47.1%	10.2%	0.2%	4.5%	100.0%	0.02	0.29	0.00	0.00	0.03		46.1%	1.7%	24.2%	6.0%	0.2%	2.3%	46.1%
22 23 34 35 35 36 33 39 40 41 42 43 44 44 45 50 50 51 52 52 53 54 55 55 55 55 55 55 55 55 55 55 55 55		2	121	0	2	0.01 0.17	0.04	4	0.00	0.03	0.53	+	Ŧ	2.1%	32.1% 32.3%	11.4%	0.8%	5.1%	100.0%	0.01	0.07	0.03	0.00	0.01	0.25	46.7% 31.4%	1.5%	12.6%	6.4% 5.2%	0.6%	1.1%	46.7% 38.4%
45			120	2	2		0.0		0.00	0.02	0.62	-	Ł	1.1%	38.7% 44.1%	455	0.3%	155 235	100.0%	0.01	0.09	0.03		0.01		34.7%	0.8%	14.6%	4.2% 3.5%	0.2%	1.6%	34.7% 44.3%
47			134	6	2	0.00 0.21	0.0	-	0.00	0.01	0.40		1	0.0%	43.3%	2.9%	0.4%	2.5%	100.0%	0.00	0.09	0.01	0.00	0.01	0.21	44.3%	0.6%	19.5%	2.1%	0.2%	1.0%	44.3%
48		1	120		4	0.01 0.40			0.01	0.05	0.90	+	+	1.2%	35.4%	11.9%	0.6%	4.6%	100.0%	0.01	0.17	0.09	0.01	0.02		32.7% 51.1%	1.0%	15.2% 18.1%	7.7%	0.6%	1.9%	32.7% 51.1%
50							0.00		0.00	0.03	0.80		Ł	1.4%	44.6%	5.6%	0.5%	4.1%	100.0%	0.01	0.17	0.02	0.00	0.01		54.0%	0.9%	21.4%	2.5%	0.4%	1.4%	54.0%
52		11	149	6	4	0.02 0.62	0.00	9	0.00	0.04	1.10		1	1.4%	52.4%	7.6%	0.3%	3.1%	100.0%	0.01	0.28	0.07	0.00	0.02	0.56	47.0%	1.0%	23.4%	5.5%	0.3%	1.7%	47.0%
53		21	140			0.02 0.44	0.00		0.01	0.08	1.00	+	ŧ	2.1%	34.0% 43.4%	5.5%	0.5%	2.4% 3.7%	100.0%	0.02	0.14	0.04		0.01		51.6% 44.5%	1.6%	13.9%	1.9% 6.7%	0.2%	1.4%	53.6% 44.5%
53		1	15	2		0.04 1.22	0.4	2	0.01	0.11	23	-	+	1.9%	515%	17.6%	0.6% 0.3% 0.3%	165	100.0%	0.03	0.58	0.30	0.01	0.06		50.9%	135	24.3% 26.4%	12.5%	0.5% 0.2%	2.6%	50.9%
57		21		4		0.07 0.92	0.12	2	0.01	0.18	2.06		t	3.2%	44.7%	6.0%	0.4%	0.5%	100.0%	0.05	0.48		0.00	0.02	1.17	54.9%	2.4%	23.2%	3.2%	0.2%	1.1%	56.9%
58		21	19		10	0.05 1.18			0.01	0.07	2.10	₽	ŧ	2.2% 1.7%	51.3% 51.8%	4.0% 19.0%	0.4%	2.9%	100.0%	0.03	0.62	0.06	0.01	0.03		47.5%	1.4%	27.1%	2.7% 9.2%	0.3%	1.3%	56.5% 47.5%
60		3/			10	0.05 1.31			0.01	0.10	2.32		+	1.9%	56.5% 44.0%	13.6%	0.2%	4.4%	100.0%	0.03	0.65	0.24	0.00	0.00		52.1%	1.5%	27.9%	10.2%	0.2%	2.4%	52.1%
59 60 61 62		31	16-	4		0.07 1.10	0.10		0.01	0.09	2.40		t	2.5%	47.8%	1.7% 4.5%	0.3%	15%	100.0%	0.05	0.50	0.07	0.01	0.03	1,20	54.1% 56.3%	1.5% 2.2%	23.4% 25.2%	2.4% 3.2%	0.3%	1.4%	54.1% 56.3%
6.3		33	163	5	10	0.05 1.32	0.25	5	0.01	0.09	2.25			2.3%	58.8%	10.9%	0.4%	4.0%	100.0%	0.03	0.63	0.14	0.01	0.05	1,32	51.1%	1.5%	28.0%	6.3%	0.3%	2.2%	58.8%

Table 5. PD of Ant M- patch antenna (24GHz - n258)

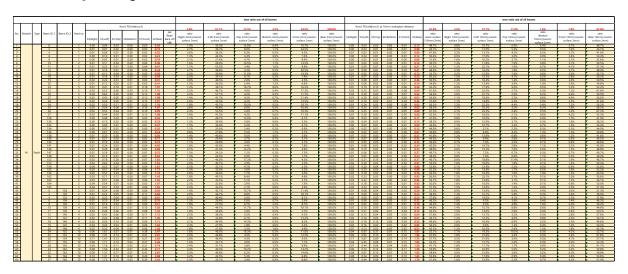
# - M-patch Low CH

_												_				t of all beams												max ratio out of all I			
Н		_	_	_	_							_													-						
					_		- 40	m2 PD/mN	(/cm2)	_			45%	56.6%	20.2%	22%	40.0%	100.0%	4	om2 PD(m	nW/cm2)	t 10mm eva	slustion di	fance	62.2%	40%	27.7%	12.4%	2.2% ratio	12.2%	62.2%
No.	Acclule Typ	e Beam ID.	1 Berna ID,2	Feed no.	S4(Right)	S3(Left)	SS(Top)	S6(Botton	ST(Fee	ont) 52		Bearn lack-off	ratio (Right 2mm)/(worst- surface 2mm)	ratio (Left 2mm)/(wont- surface 2mm)	ratio (Top 2mm)/(wonst- surface 2mm)	ratio (Bottom 2mm)/(wonst- surface 2mm)	ratio (Fornt 2mm)/(worst- surface 2mm)	ratio (Rear 2mm)/(wonst- surface 2mm)	S4(Right)	\$3(Left)	\$5(Top)	S6(Bottom)	s) S1(Fro	st) S2(Read)	ratio worst-surface (10mm/2mm)	ratio (Right 10mm)/(worst- surface 2mm)	ratio (Left 10mm)/(worst- surface 2mm)	ratio (Top 10mm)/(wont- surface 2mm)	(Bottom 10mm)/(worst- surface 2mm)	ratio (Front 10mm)/(worst- surface 2mm)	ratio (Rear 10mm)/(worst- surface 2mm)
1		0			0.00		0.03	0.00	0.00	1 6	121		1.4%	17.6% 17.7%	13.1%	0.9%	11.7%	100.0% 100.0%	0.00	0.03	0.01	0.00	0.01	0.08	36.6%	0.9%	11.6%	6.6%	0.5%	12.3%	36.6% 38.5%
3 4		4			0.01	30.0	0.01	0.00	0.00		1.17		2.9%	34.1%	8.1%	0.6%	9.8%	100.0%	0.00			0.00	0.01		42.8%	2.3%	13.9%	6.2% 6.4%	0.6%	3.5%	42.8%
4		6	+	-	0.00	0.08		0.00	0.00	1 6	1.22		1.2%	36.3% 22.4%	3.1% 3.3%	0.9%	4.9% 8.7%	100.0%	0.00	0.03	0.01	0.00	0.00	0.10	45.7%	0.9%	12.6% 8.7%	2.2%	0.9%	1.8%	45.7% 33.2%
6		10		2	0.01	0.08	0.04	0.00	0.04	4 6	0.22		1.0%	23.4%	10.8%	12%	11.5%	100.0%	0.00	0.03	0.03	0.00	0.01	0.13	31.5%	1.2%	9.2%	8.0%	0.9%	4.0%	20.5%
7		11	+	2	0.01	0.16		0.00	0.00	9 6	1.32		1.7%	46.8% 39.8%	1.4%	0.6%	5.5% 29.2%	100.0% 100.0%	0.00				0.01		48.3% 52.4%	1.1% 2.5%	18.4%	0.9%	0.6%	2.3% 8.8%	48.2% 52.4%
5 7 8 9		13		2	0.01			0.00	0.00	5	26		15%	23.8% 31.9%	9.0% 4.8%	0.8% 0.8%	20.7% 5.4%		0.01		0.01		0.02		41.0% 54.4%	2.7% 1.6%	9.8%	4.2%	0.4%	5.9%	41.0% 54.4%
11		19		2	0.01	0.19	0.01	0.00	0.00	2	2.44		2.0%	43.0%	1.8%	0.9%	3.8%	100.0%	0.01		0.01	0.00	0.01	0.21	48.2%	1.6%	15.6%	1.1%	0.7%	1.1%	48.2%
12		20	+	- 2	0.01	0.11	0.01	0.01	0.0		1.66		2.4%	24.0%	1.0% 17.2%	2.6%	7.8% 14.1%	100.0%	0.01	0.05	0.01	0.01	0.01		30.2% 40.4%	1.5%	10.8%	2.2% 9.7%	1.7%	2.2%	30.2% 40.4%
14		25		3	0.03	0.34	0.07	0.00			0.84		3.7%	40.2%	7.8%	0.5%	15.4%				0.03		0.06	0.43	51.8%	2.9%	18.7%	4.1%	0.4%	6.7%	51.8%
15		26 27		5	0.02	0.44			0.11	9 6	1.04		2.5%	55.1% 42.4%	4.4%	0.8% 1.0%	14.1%	100.0%	0.02		0.02	0.00	0.00		58.9%	2.3%	25.6%	2.4%	0.5%	7.3% 3.6%	58.9% 51.7%
17		28		5	0.03	0.25	0.04	0.02	0.14		0.05		2.9%	29.0%	4.1%	2.0%	16.6%	100.0%	0.02		0.02		0.04	0.32	36.9%	1.9%	13.0%	2.3%	1.4%	4.6%	16.9%
19		35	+	3	0.03	0.38	0.02	0.01	0.1	1	175		2.8%	31.0% 51.0%	13.6% 3.2%	0.3% 0.8%	15.7% 18.0%	100.0%	0.02	0.18		0.01	0.04	0.44	49.4% 55.8%	2.2%	13.7% 23.4%	6.5% 1.7%	0.2%	4.6%	49.4% 55.8%
20		36	_	5	0.01	0.43		0.01	0.12	,	0.76		1.0%	56.6% 43.0%	1.5% 4.5%	0.7% 1.0%	16.3% 11.2%	100.0% 100.0%	0.01	0.21		0.00	0.00		57.9% 51.4%	1.6%	27.7%	2.5%	0.4%	7.2% 3.5%	57.9% 51.4%
22		128		í	0.00	0.05	0.02	0.00	0.01		1.21		1.9%	23.0%	9.9%	0.5%	6.1%	100.0%	0.00	0.02	0.01	0.00	0.00	0.00	36.2%	1.4%	7.5%	6.1%	0.5%	1.9%	36.2%
23		130	+	-	0.00	0.09	0.02	0.00	0.00	2 6	124		1.2%	37.9% 23.1%	8.1% 7.1%	0.8%	6.9% 2.1%	100.0%	0.00	0.03	0.01	0.00	0.01		31.9% 36.1%	0.8%	12.5% 7.1%	4.4% 5.0%	0.4%	2.0%	11.9%
25		124		1	0.00	300		0.00	0.01	1 6	1.25		0.8%	22.9%	3.7%	0.8%	2.0%	100.0%	0.00	0.02	0.01	0.00	0.00	0.11	42.9%	0.8%	6.5%	2.4%	0.4%	0.8%	42.9%
27		126		2	0.00	0.08		0.01	0.00	2 6	1.20		1.2%	35.9% 36.3%	3.4% 11.0%	2.1%	8.1% 4.2%		0.00		0.01	0.00	0.00		32.5% 41.0%	1.35	11.5%	2.6% 7.8%	1.7%	1.7% 1.3%	32.5% 41.0%
28		139	-	2	0.01	0.14		0.00	0.0	1 4	3.52		2.1%	26.6% 28.0%	5.0%	0.4%	2.1%	100.0% 100.0%	0.01	0.05	0.02	0.00	0.00		50.3% 46.2%	1.9%	1.5% 4.5%	3.4%	0.2%	0.6%	50.3% 46.2%
30		141		2	0.01	0.17	0.03	0.01	0.00		1.52		1.9%	11.5%	4.0%	15%	5.2%	100.0%	0.01			0.01	0.01	0.21	41.4%	1.2%	10.3%	2.7%	1.2%	1.9%	41.4%
31	M Par	146 h 147		2	0.01	0.20		0.00	0.00	2 6	150		1.0%	40.9% 23.0%	11.2% 1.5%	0.0%	4.6% 1.2%	100.0% 100.0%	0.00	0.07	0.03	0.00	0.01		46.8%	0.8%	14.0% 7.1%	6.3% 1.0%	0.0%	1.5%	46.8% 51.0%
22		140		2	0.01	0.17	0.00	0.01	0.00	2 6	5.57		1.4%	29.1%	0.5%	1.9%	3.4%	100.0%	0.01	0.05	0.00	0.01	0.01	0.19	34.0%	0.9%	9.3%	0.4%	1.6%	1.1%	34.0%
35		152	+	5	0.02	0.53	0.24	0.00	0.00	5 6	1.98		1.4%	42.5% 42.1%	18.7% 4.2%	0.2%	5.1% 5.1%	100.0%	0.01	0.22	0.14	0.00	0.02	0.61	41.0% 61.0%	1.0%	17.2% 20.2%	11.5% 3.2%	0.2%	1.4%	48.8% 61.8%
26		154		- 5	0.05	0.32		0.00	0.00	1	.17		4.0%	27.3% 28.4%	12%	0.2% 0.1%	2.6%	100.0%	0.04	0.13	0.02	0.00	0.01	0.67	56.85 07.15	12%	11.0%	1.6%	0.1%	1.1%	56.8% 57.1%
38		156		5	0.05	0.52	0.03	0.03	0.00		.59		2.0%	12.3%	1.7%	1.6%	3.3%	100.0%	0.03	0.19	0.02	0.02	0.02	0.65	41.0%	1.6%	11.6%	1.2%	1.3%	1.5%	41.0%
29		162	+	5	0.03	0.45	0.11	0.00	0.00	7	1.00		2.9%	44.8% 15.7%	11.3%	0.2%	415	100.0%	0.02	0.20	0.08	0.00	0.02		56.5%	2.2%	20.5%	7.9%	0.2%	2.0%	56.5%
41		164		5	0.04	0.34		0.00	0.00	1 1	27		2.1%	26.4% 11.9%	13% 22%	0.2%	2.5%	100.0%	0.03	0.11	0.02	0.00	0.02		53.7%	2.5%	8.8% 13.6%	1.3%	0.1%	1.2%	53.7% 52.8%
42		0	128	2	0.01	0.49	0.07	0.01	0.05	6 6	351		2.0%	15.6%	13.4%	0.6%	12.6%	100.0%	0.01	0.20	0.04	0.00	0.02	0.10	52.8% 25.6%	1.6%	11.0%	7.9%	0.4%	3.7%	35.6%
13 14 15 15 15 15 15 15 15 15 15 15 15 15 15		2	110	2		0.19		0.00	0.13		1.49	П	2.0%	39.3% 32.4%	9.8%	0.6%	24.6%		0.01		0.03		0.03	0.19	37.9% 35.7%	1.4%	14.1%	5.9%	0.4%	7.0%	37.9% 35.7%
46		- 2	134	2	0.01	0.16	0.03	0.01	0.00	1	5.60		1.5%	27.3%	4.5%	12% 13%	445	100.0%	0.01	0.05	0.02	0.01	0.01	6.25	41.6%	1.0%	1.4%	1.0%	0.8%	2.1% 1.3%	41.6%
47		8	136	4	0.01	0.16		0.01	0.00		1.45	ļ	2.7%	35.0% 35.9%	11.2%	2.9% 1.2%	12.9%	100.0% 100.0%	0.01	0.05	0.01	0.01	0.01		35.0% 44.5%	2.0%	11.6% 12.5%	2.5% 8.0%	2.2%	2.9% 2.6%	35.0% 44.5%
49		11	139	- 4	0.02	0.37	0.04	0.01	0.0	4	0.98		2.0%	37.7%	3.7%	0.6%	4.0%	100.0%	0.02	0.14	0.03	0.00	0.02	0.51	52.2%	1.9%	14.7%	2.0%	0.4%	1.9%	52.2%
50		12	140	4	0.02	0.29		0.00	0.12		1.02		2.4%	34.6% 25.4%	5.5% 6.7%	0.5% 1.2%	13.7% 13.0%	100.0%	0.02	0.11	0.03	0.00	0.03		48.5% 29.2%	2.0%	12.0%	1.1% 1.5%	0.4%	19% 15%	48.5% 39.2%
52		18	146		0.02	0.30	0.10	0.00	0.00	5 6	1,79		2.7%	28.3%	12.3%	0.5%	6.4%	100.0%	0.02	0.11	0.06	0.00	0.02	0.16	45.4% 47.4%	1.9%	13.0%	7.3%	0.4%	2.7%	45.4% 47.4%
54		20	140	4	0.04		0.03	0.04		9	1.09		2.5%	30.6% 25.8%	2.1%	0.9%	1.0% 8.3%		0.02	0.11	0.02	0.02	0.01		22.4%	2.3% 1.9%	10.8%	1.6%	0.6% 2.2%	1.0%	19.4%
55		24	152	10	0.07	1.11		0.01	0.30		1.96	ļ	2.3%	37.5% 44.6%	20.2%	0.3%	10.0%	100.0%	0.05	0.42	0.37	0.01	0.07		52.8%	1.7%	14.2%	12.4%	0.2%	2.3% 5.1%	52.8%
57		26	154	10	0.10	1.05	0.09	0.01	0.23	1 2	231		4.5%	45.3%	4.0%	0.5%	10.0%	100.0%	0.09	0.49	0.06	0.01	0.11	1.41	60.9%	4.0%	21.1%	2.4%	0.4%	4.9%	60.9%
58		27	155	10	0.07	0.98	0.08	0.02	0.23	5 1	1.05		2.5%	36.8%	3.1% 2.8%	0.6%	8.1% 8.2%	100.0%	0.04	0.42	0.05	0.01	0.10		57.9% 40.1%	1.6% 2.1%	15.9%	1.8%	0.4%	1.6% 2.2%	57.9% 40.1%
60		34	162	10	0.09	1.02		0.01	0.35		.40		1.6%	40.9%	13.6%	0.1%	14.2%	100.0%	0.07	0.44		0.01	0.09		57.4% 62.2%	2.7%	17.7%	8.8%	0.2%	1.6%	57.4%
62		35	164	10	0.06	1.03	0.09	0.01	0.23	1	20		3.6%	47.7% 45.1%	4.1%	0.4%	14.6%	100.0%	0.06	0.45	0.04	0.01	0.12	1.34	51.7%	2.8%	21.9%	1.6%	0.2%	6.2% 5.1%	62.2% 58.7%
63		37	165	10	0.09	1.00	0.11	0.03	0.23	1	1.65		3.4%	37.6%	4.0%	1.0%	0.6%	100.0%	0.05	0.40	0.07	0.02	0.10	1.43	53.8%	2.0%	14.9%	2.7%	0.7%	3.8%	53.8%

# - M-patch Mid CH

															max ratio ou	t of all beams												max ratio out of all b	eams		
								4cm2 PD)	nW/cm2	0			4.65	\$7.3%	18.8%	27%	45.7%	100.0%	40	m2 PD(m	W/cm2)	at 10mm ex	aluation o	Sistance	63.3%	40%	27.5%	11.8%	2.4%	12.2%	63.3%
No.	loclule Typ	e Seam ID_1	Berra ID,	2 Feed no		0 533.46	SS/Top		П.,			per Dearn	ratio (Right 2mm)/(worst-	ratio (Left 2mm)//wont-	ratio (Top 2mm)/(wont-	ratio (Sottom 2mm)//wont-	ratio (Fornt 2mm)/(wont-	ratio (Rear 2mm)//wont-	ram-an	F20 -00	F F C T T T	S6/Botton		onti S2/Rea	ratio	ratio (Right 10mm)//wont-	ratio (Left 10mm)//worst-	ratio (Top 10mm)//wont-	ratio (Bottom	ratio (Front 10mm\//wont-	ratio (Rear 10mm)//wont-
					S4(Righ	() S3(Left	SS(Top	) S6(Bot	tom) S1	(Front)	S2(Rear)	Back-off (dB)	surface Zmm)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)	54(kight)	23(188)	55(10p)	) Se(aceson	2204	22)988	(10mm/2mm)	surface 2mm)	surface 2mm)	surface 2mm)	10mm)/(worst- surface 2mm)	surface 2mm)	surface 2mm)
1		9		-		0.09				0.03	0.23		2.1%	16.1%	11.5%	0.4%	11.2% 45.7%	100.0%	0.00			0.00		0.10	42.3%	1.3%	12.0%	6.0%	0.4%	4.2%	42.3% 41.4%
3		- 4		1	0.01	0.07	0.01	0.0	2	0.02	0.20		3.0%	11.5%	6.6%	0.5%	12.2%	100.0%	0.01	0.03	0.01	0.00	0.0		37.1%	2.5%	13.2%	4.6%	0.5%	4.1%	37.1%
4		6	-	-	0.00	0.10	0.01	0.0		0.01	0.25		1.6%	42.0% 27.5%	13%	0.8%	5.3% 11.4%	100.0%	0.00	0.04	0.01	0.00	0.0		49.8%	1.2%	15.9% 11.4%	2.9%	0.4%	2.0%	49.8% 29.5%
5 6 7 8 9 10		10		2	0.01		0.03				0.25		1.7%	27.7%	9.7%	0.9%	16.3%	100.0%	0.00		0.03	0.00		2 0.14	31.9%	1.1%	11.4%	7.1%	0.9%	4.0%	28.9%
7		11	1	2	0.01	0.22			-	0.03	0.41		1.2%	51.6% 27.1%	2.7%	12%	7.5% 35.0%	100.0%	0.00		0.01	0.00	0.0		50.7% 46.2%	1.0%	21.8% 16.2%	1.7%	0.7%	3.4% 9.8%	50.7% 46.2%
9		12		2	0.01	0.08	0.03	0.0	_	0.06	0.21		2.9%	24.5%	8.9%	1.0%	20.1%	100.0%	0.01		0.02	0.00	o c		34.1%	2.2%	10.2%	4.0%	0.6%	5.1%	24.1%
10		- 18	-	- 3		015	0.02	0.0	-	0.03	0.42		2.4%	36.1%	5.4%	0.5%	7.3%	100.0%	0.01	0.05	0.02	0.00	9.0	0.22	51.9% 49.5%	1.2%	12.3%	14%	0.5%	2.8%	51.9%
12		20		2	0.01	0.15	0.02			0.04	0.48		1.7%	30.1%	3.3%	15%	7.3%	100.0%	0.01	0.07	0.01	0.01	0.0	0.17	34.5%	1.0%	14.3%	2.1%	1.0%	2.1%	34.5%
13		24	-	- 5	0.02	0.34				0.16	0.98		1.6%	35.0% 47.0%	15.6%	0.6%	16.2%	100.0%	0.01		0.09	0.00	0.0		48.7%	1.25	15.3% 23.4%	9.2%	0.4%	5.3% 10.3%	48.7% 55.1%
15		26		- 5	0.03	0.54	0.04			0.17	1.00		2.8%	54.2%	4.2%	0.3%	16.9%	100.0%	0.03	0.25		0.00	0.0	0.50	58.0%	2.0%	25.1%	2.4%	0.2%	7.7%	58.0%
16		27	1	5	0.02		0.05			0.14	1.06		1.9%	44.2% 34.1%	4.5%	1.0%	13.6%	100.0%	0.02	0.23	0.02	0.01	0.0	5 0.56	52.9% 42.5%	1.4%	21.3%	2.1%	0.8%	4.8% 5.1%	52.9% 42.5%
18		34		- 5		0.42	0.10			0.22	0.98		2.1%	42.6%	10.1%	0.9%	22.3%	100.0%	0.02		0.05	0.01	0.0		51.1%	1.6%	20.5%	4.0%	0.6%	8.2%	51.1%
19		35 36	-			0.49				0.24	0.95		2.4%	51.7% 0.3%	425	0.4%	25.7% 17.0%	100.0%	0.02		0.02	0.00	9		56.5% 50.1%	145	24.7%	2.1%	0.2%	11.1%	56.5% GL1%
21		37		5	0.02	0.47	0.05	0.0		0.15	1.06		1.9%	44.5%	4.5%	1.0%	14.0%	100.0%	0.01		0.02		0.0		52.4%	1.3%	21.3%	2.1%	0.8%	4.7%	52.4%
13 14 15 16 17 18 19 20 21 22 22 22 23 24 25 26		128	-	+ :-	0.00	0.07	0.03			0.02	0.24		1.3%	28.1% 38.1%	12.3%	0.4%	7.2%	100.0%	0.00	0.03	0.01	0.00	0.0	0.10	40.9% 35.6%	1.3%	10.6%	6.0% 3.5%	0.4%	1.7%	40.9% 35.6%
24		132		1	0.00	0.08	0.02	0.0		0.01	0.26		1.5%	30.4%	6.9%	0.8%	2.7%	100.0%	0.00		0.01	0.00	0.0	0.09	35.0%	1.5%	8.5%	5.0%	0.8%	1.2%	35.0%
25		134	-	1	0.00	0.07	0.01	0.0	2	0.00	0.30		1.0%	21.8%	4.0%	0.3%	1.3% 7.9%	100.0%	0.00	0.02	0.01	0.00	0.0	0.13	42.6%	1.0%	6.0% 8.8%	1.0%	0.3%	0.3%	42.6% 27.9%
27		120		2	0.01	0.17	0.05	0.0	_	0.01	0.45		1.3%	38.2%	11.1%	0.7%	2.1%	100.0%	0.01	0.05	0.04	0.00	0.0	0.10	40.9%	1.15	12.0%	8.0%	0.7%	0.9%	40.9%
28 29		129		2	0.01	018	0.03	0.0	Ĭ	25	0.62		1.6%	29.3% 34.7%	4.85 5.35	0.1%	1.95	100.0%	0.01	0.06	0.02	0.00	9	0.21	50.2% 45.3%	1.6%	9.6% 7.8%	15%	0.2%	0.6%	50.2% 45.2%
		141		2	0.01	0.22	0.02	0.0		0.04	0.55		1.4%	40.1%	3.6%	1.1%	6.7%	100.0%	0.01	0.03	0.01	0.01	0.0	0.23	42.3%	0.9%	14.3%	2.4%	0.9%	2.4%	42.3%
31	14 2-4	146	_	2	0.01		0.07	0.0		200	0.57		0.9%	41.6%	12.1%	0.2%	6.5%	100.0%	0.00		0.04	0.00	0.0		48.3%	0.7%	15.6%	6.5%	0.0%	2.1%	48.3% 50.4%
2.2		140		2	0.01		0.01	0.0		0.02	0.59		1.2%	24.7%	0.9%	1.7%	2.9%	100.0%	0.01		0.00	0.01	0.0		34.0%	0.9%	7.1%	0.7%	1.2%	0.7%	34.0%
34		152	-	5	0.02	0.65	0.28		-	0.07	1.48		1.5%	44.1% 41.9%	18.0%	0.3%	4.7% 5.8%	100.0%	0.01		0.18	0.00	0.0		41.0%	0.9%	17.5% 19.8%	11.0%	0.2%	1.5%	48.8% 61.5%
26		154			0.05	0.43	0.06	0.0		0.04	1.42		1.2%	30.1%	4.0%	0.2%	2.1%	100.0%	0.04	0.17	0.03		0.0	0.76	53.9%	2.6%	11.9%	2.3%	0.1%	1.1%	53.9%
37		155	-	- 3	0.03	0.49	0.04	0.0		88	159		1.9%	30.6% 30.1%	2.2%	0.3%	15%	100.0%	0.02	0.21	0.02	0.00		0.86	53.8% 41.9%	145	12.9%	1.3%	0.2%	1.6%	53.8% 21.9%
29		162		5	0.02	0.59	0.14	0.0		0.08	1.26		1.0%	46.7%	10.8%	0.4%	6.1%	100.0%	0.02		0.07	0.00	0.0		57.3%	1.6%	21.0%	5.2%	0.2%	2.2%	57.3%
40		163 164	-	- 5	0.04	0.46	0.06	0.0		0.07	1.27		2.8%	36.0% 29.5%	44%	0.2%	5.4% 2.7%	100.0%	0.03	0.21	0.03	0.00	0.0	2 0.75	59.2% 49.3%	2.3%	16.6%	2.5%	0.2%	1.6%	59.2% 49.3%
42		165		- 5	0.03	0.52	0.04	0.0		0.06	1.50		2.1%	35.6%	2.4%	0.9%	1.9%	100.0%	0.02	0.22	0.02	0.01	0.0	3 0.79	52.7%	1.5%	14.5%	1.5%	0.6%	1.7%	52.7%
43		2	128	2	0.01		0.07			0.07	0.54	-	2.0%	41.1% 38.7%	12.6%	0.6%	13.8%	100.0% 100.0%	0.01		0.04		0.0	2 0.23 4 0.22	42.8% 38.3%	1.5%	14.1%	6.9% 5.2%	0.4%	4.1% 7.8%	42.8% 38.3%
32 33 34 35 36 39 40 41 42 43 44 45 46 47 50 50 51 51 52 53 54 55 56 57		â	132	2	0.02	0.20	0.05	0.0	_	0.05	0.56		1.6%	15.5%	1.1%	0.5%	8.0%	100.0%	0.02	0.07	0.04	0.00	0.0	2 0.18	31.8%	1.0%	12.5%	6.2%	0.5%	2.7%	31.8%
46		6	134			0.19				0.03	0.65	-	1.7%	29.2% 12.0%	52%	0.6%	1335	100.0%	0.01		0.03		0.0	0.28	42.1% 34.4%	1.15	9.5%	4.1%	0.5% 2.4%	125 125	42.1% 34.4%
48		10	138	- 4	0.02	0.41	0.13	0.0		0.10	1.00		1.9%	41.3% 40.0%	12.0%	0.6%	9.8%	100.0%	0.01	0.14	0.09	0.01	0.0	0.45	45.1%	1.4%	14.0%	9.2%	0.5%	2.6%	45.1%
49 50		11	139	4						0.16	0.98		2.1%	40.0% 37.9%	45%	12%	5.3% 16.2%	100.0%	0.02		0.04		0.0		50.0% 53.3%	1.9%	16.1%	3.3% 3.6%	0.7%	2.4%	50.0% 53.2%
51		12	141	- 4	0.02					0.18	1.23		1.0%	31.1%	5.2%	0.9%	14.0%	100.0%	0.02		0.04	0.01	0.0		29.3%	1.35	11.2%	3.3%	0.7%	42%	39.3%
52		18	146	4	0.03	0.40	0.13		2	0.09	0.98		2.5%	40.4% 31.7%	12.7%	0.4%	1.9%	100.0% 100.0%	0.02		0.08	0.00	0.0		45.8%	1.8%	14.2%	7.6%	0.3%	3.8% 1.4%	46.0% 47.0%
54		20	140	4	0.02	0.33	0.03	0.0	1	0.07	1.12		2.1%	28.8%	2.7%	2.7%	6.5%	100.0%	0.02	0.13	0.02	0.02	0.0	0.46	41.1%	1.3%	11.7%	1.9%	1.9%	1.9%	41.1%
55		24	152	10	0.07	147	0.59			850	2.61	H	2.0%	42.7% 49.4%	17.4% 5.1%	0.6% 0.8%	11.4% 20.6%	100.0%	0.04	0.58	0.38		0.7	1,73	51.3% 63.3%	135	17.2% 22.7%	11.2% 3.5%	0.4%	15% 7.8%	51.3% 63.3%
57		26	154		0.12	1.25	0.11	0.0		0.36	2.70		4.4%	46.3%	425	0.5%	13.4%	100.0%	0.11	0.58	0.06		0.1	6 1.55	57.4%	4.0%	21.5%	2.0%	0.3%	5.8%	57.4%
58		27	155	10	0.07	117	0.11	0.0		0.33	2.17		2.1%	17.0% 11.0%	3.5% 2.6%	0.6%	10.3%	100.0%	0.05	0.53	0.07	0.01	0.1	1 1.73	54.7% 42.1%	1.5%	16.8%	2.1%	0.4%	4.4%	54.7% 42.1%
60		34	162	10	0.08	1.41	0.31	0.0		0.50	2.92		2.7%	48.3%	10.7%	0.9%	17.3%	100.0%	0.06	0.62	0.18	0.02	0.1		58.9%	2.1%	21.4%	6.2%	0.5%	6.1%	58.9%
61		35	163	10		1.20	0.11			0.54	2.42	-	1.6%	49.6% 44.7%	45% 54%	0.4%	22.3% 11.8%	100.0%	0.07	0.55	0.06	0.01	0.2	1 1.47	60.9%	2.9%	22.6%	2.6%	0.2%	8.7% 4.8%	60.9% 54.2%
63		37	165			1.18				0.35	1.01		2.7%	44.7% 29.1%	3.4%	16%	11.4%	100.0%	0.06		0.08			4 1,61	53.0%	1.85	16.6%	2.6%	1.1%	455	53.0%

# - M-patch High CH

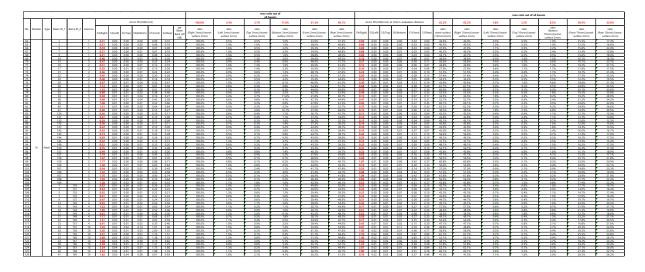


### 3.1.2 Ant N- Patch Antenna

Table 6 to Table 8 show the PD simulation evaluation of Ant N patch antenna at 28 GHz / 39 GHz / 24 GHz for the corresponding evaluation plane specified in Table 1.

Table 6. PD of Ant N- patch antenna (28GHz-n261)

### - N-patch Low CH



# - N-patch Mid CH

		_	_											max rat								_					max ratio out of all	Deams		
$\vdash$		т —	т —	т —	Г		4cm2 PD	Mar Milloren	(2)					all b		I		-	Iom2 PD/m	MM/cm2) i	t 10mm eval	untion dist	100		I	I				
No. I	Andule Type	Seam ID_1	Berra D 2	Feed no.		1	T	1			per	100.0%	3.2% ratio	25% min	13.4%	59.0%	68.3% ratio		T	1	1	T	T	66.3%	66.3% mto	1.0%	23%	10.0% ratio	27.5% ratio	34.9% (160)
		1			S4(Right) S3(Lef	t) SS(To)	p) \$6(Bo	2 (motte	1(Front)	S2(Rear)	Beam Back-off (48)	(Right 2mm)/(wonst- surface 2mm)	(Left 2mm)/(wont- surface 2mm)	(Top 2mm)/(wonst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(wont- surface 2mm)	(Rear 2mm)/(wonst- surface 2mm)	54(Right	\$3(Left)	SS(Top)	S6(Bottom)	S1/Front	S2(Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(wont- surface 2mm)	(Left 10mm)/(wont- surface 2mm)	(Top 10mm)/(wont- surface 2mm)	(Bottom 10mm)/(worst- surface 2mm)	(Front 10mm)/(worst- surface 2mm)	(Rear 10mm)/(wonst- surface 2mm)
64		-		-		0.00			0.09			100.0% 100.0%	0.5%	0.5%	1.0% 1.5%	44.7% 39.2%					0.00	0.03	0.03	46.6%	46.6%	0.5%	0.5%	1.0%	15.0%	16.5% 16.7%
65 66 67 68 69 70 71 72 73		5			0.19 0.00	0.00	0.0	00	0.07	0.08		100.0%	1.6%	0.5%	2.2%	38.7%	44.1%	0.09	0.00	0.00	0.00	0.02	0.04	47.3%	47.3%	1.1%	0.5%	1.6%	11.3%	19.4%
68		7 9	+	++		0.00			0.08	0.09		100.0% 100.0%	0.9%	0.4%	2.2% 1.5%	35.7% 37.6%	41.4% 50.7%		0.00	0.00		0.02	0.03	41.9%	41.9% 45.9%	0.4% 0.5%	0.4%	1.0%	9.7% 12.2%	15.0% 20.0%
69		14		2		0.01			0.16	0.18		100.0% 100.0%	0.5%	1.2%	2.2% 1.0%	37.9% 48.7%	44.5% 53.4%	0.17	0.00	0.00	0.01	0.06		40.6% 60.3%	40.6% 60.3%	0.2% 0.2%	1.0%	1.7%	14.7% 17.8%	16.1%
71		16		2	0.28 0.00	0.00	0.0	01	0.11	0.17		100.0%	0.7%	1.4%	2.1%	44.5%	58.3%	0.12		0.00	0.01	0.05	0.05	44.2%	44.2%	0.7%	1.1%	1.8%	17.7%	17.3%
72		17 21	+	2	0.49 0.00	0.01	0.0	01		0.18		100.0% 100.0%	0.6%	1.7%	2.6% 1.6%	37.3% 45.9%	47.9%		0.00		0.01		0.10	29.5% 53.9%	29.5% 53.9%	0.3% 0.2%	1.2% 0.6%	2.0%	11.6% 17.3%	14.7% 21.2%
74		22		2	0.47 0.01	0.00	0.0	00	0.21	0.25		100.0% 100.0%	1.2%	0.5%	0.6% 3.4%	44.5% 39.2%	54.4% 34.1%	0.28	0.00	0.00	0.00	0.07		60.2%	60.2% 37.5%	0.6%	0.2%	2.6%	14.9%	24.5%
76		29		5	0.66 0.01 1.12 0.01				0.35	0.43		100.0% 100.0%	0.7%	1.8%	6.3% 0.5%	\$1.5% \$1.0%	63.2% 53.6%	0.21	0.00	0.01	0.03	0.11		46.1% 63.4%	46.1% 63.4%	0.4%	1.3%	4.6%	19.4% 22.7%	18.0% 27.2%
78		21		3	1.16 0.01	0.00	0.0	00	0.56	0.72		100.0%	0.9%	0.1%	0.3%	47.8%	62.3%	0.77	0.00	0.00	0.00	0.24	0.37	66.3%	66.3%	0.5%	0.1%	0.2%	20.3%	31.6%
75 76 77 78 79 80 81 82 83		22	$+ \equiv$	5 5		0.00			0.45	0.39		100.0% 100.0%	1.5%	0.5% 2.5%	2.2% 11.8%	\$1.1% \$1.0%	44.9% 68.3%	0.50	0.01	0.00	0.01	0.21		57.0% 37.3%	57.0% 37.3%	1.0%	0.5% 2.3%	1.6%	21.7% 17.3%	22.9%
81		38		- 3	0.92 0.01	0.01	0.0	03	0.47			100.0%	0.5%	1.1%	16%	\$1.6% 46.0%	40.4%	0.50	0.00	0.01	0.02	0.21	0.19	54.7% 66.3%	54.7% 66.3%	0.3%	0.9%	2.1%	23.1% 19.4%	20.7%
83		40	_	- 5	1.12 001	0.00	0.0	00	0.57	0.62		100.0%	0.7%	0.4%	0.2%	50.8%	55.0%	0.72	0.00	0.00	0.00	0.25	0.32	64.0%	64.0%	0.4%	0.1%	0.2%	22.5%	28.1%
84		41 129	-	5		0.01			0.23	0.10		100.0%	3.2% 0.7%	2.1%	12.8%	52.6% 16.8%	68.2%	0.20	0.01	0.01	0.04	0.09		41.5%	44.6% 41.5%	1.8%	1.8% 0.4%	8.9% 1.4%	19.9% 11.6%	25.4% 15.1%
86		131		1		0.00			0.11	0.09		100.0%	0.7%	0.3%	1.3%	17.5% 16.9%	29.9%	0.12	0.00	0.00	0.00	0.04	0.04	42.8% 46.0%	42.8% 46.0%	0.3%	0.3%	1.0%	12.2% 12.2%	11.0%
88		135		-		0.00	0.0	00	0.12	0.10		100.0%	0.6%	0.3%	1.0%	29.7%	33.0%	0.16	0.00	0.00	0.00	0.04	0.04	49.5%	49.5%	0.3%	0.2%	0.6%	14.0%	13.7%
90		137	_	1 2	0.23 0.00 0.47 0.00	0.00	0.0		0.09	0.08		100.0%	0.9%	0.9%	1.8%	41.0% 43.1%	36.6% 34.2%	0.11	0.00	0.00	0.00	0.03	0.03	45.0%	46.7% 45.0%	0.4%	0.4%	1.3%	14.1% 15.3%	12.8% 13.8%
85 86 87 88 89 90 91 92		143		2	0.61 0.00	0.00	0.0	01	0.37	0.31		100.0%	0.2%	0.1%	0.7%	46.2% 41.7%	36.1% 36.1%	0.47	0.00	0.00	0.00	0.14	0.13	58.3% 50.7%	58.3% 50.7%	0.2%	0.0%	0.5%	17.7%	16.4%
93		145		2		0.01			0.14	0.13		100.0%	1.6%	1.6%	42% 2.1%	43.4%	40.2% 35.1%		0.00	0.00	0.01	0.04		41.5%	41.5% 48.3%	1.0%	1.3% 0.2%	3.2%	13.8%	13.0%
95	N Patri	150		2	0.02 0.00	0.00	0.0	00	0.25	0.31		100.0%	0.4%	0.2%	0.1%	44.5%	37.1%	0.46	0.00	0.00	0.00	0.14	0.14	55.9%	55.9%	0.2%	0.2%	0.1%	16.9%	16.5%
96		151	+	- 2		0.01			0.23	0.21		100.0%	1.1%	0.9%	1.1% 4.7%	41.9% 17.5%	38.0% 44.1%	0.26		0.00	0.00	0.08		48.5%	48.5% 47.9%	0.6%	0.7%	0.7% 3.6%	15.1% 13.5%	16.0%
95 96 97 98 99 100 101 102 103 104 105 106 107 108		158 159		- 5		0.00			0.88	0.74		100.0%	0.3%	0.1%	0.6%	48.8% 51.0%	41.0%		0.01	0.00		0.41		59.7% 62.4%	59.7% 62.4%	0.3%	0.1%	0.2%	22.8%	21.2%
100		160		3	1.61 0.01	0.01	0.0	01	0.71	0.72		100.0%	0.7%	0.6%	0.4%	41.9%	44.8%	0.83	0.01	0.01	0.01	0.32	0.37	51.6%	51.6%	0.4%	0.5%	0.3%	20.0%	23.3%
101		161	+	5		0.03			0.47	0.47		100.0%	1.3%	2.5%	1.0%	43.0% 40.8%	42.9%		0.01	0.00	0.01	0.18	0.17	52.6%	19.9% 52.6%	0.8% 0.3%	2.1% 0.2%	0.7% 2.6%	16.1%	15.7%
103		167		5		0.00			1.01	0.83		100.0%	0.3%	0.1%	0.3%	51.6% 46.9%	42.4%		0.00	0.00	0.00	0.48		62.8%	62.8% 57.9%	0.2%	0.1%	0.2%	24.3% 21.9%	22.0%
105		169		Š	1.34 0.02	0.03	0.0		0.59	0.60		100.0%	1.1%	1.9%	0.8%	44.0%	45.1%	0.61		0.02	0.01	0.25		45.9%	45.9%	0.7%	1.6%	0.7%	18.4%	19.2%
106		1	129	2	0.54 0.01 0.58 0.00	0.01	0.0	01	0.27	0.31		100.0%	0.9%	0.9%	1.3%	50.7% 41.0%	56.9% 38.2%	0.25	0.00	0.00	0.01	0.07	0.11	42.6%	45.5% 42.6%	0.6%	0.7%	1.1%	16.2% 12.6%	19.7% 13.5%
108		5	133	2 2	0.58 0.01 0.60 0.01	0.00	88	01 01	0.23	200		100.0% 100.0%	0.9%	0.5%	14%	29.7% 18.6%	34.1% 39.3%	0.27	0.00	0.00	0.01	0.07		45.9%	45.9% 45.5%	0.5%	0.3%	12%	12.1%	16.0%
110		9	137	2	0.47 0.00	0.00	0.0		0.23	0.24		100.0%	0.9%	0.4%	2.6%	48.5% 56.9%		0.22	0.00				0.09	47.2% 46.6%	47.2% 46.6%	0.4%	0.4%	1.9%	17.2%	20.0%
112		15	143	1.	1.22 0.01	0.00	0.0	01	0.68	0.57		100.0%	0.5%	0.2%	1.1%	\$1.6%	43.4%	0.79	0.00	0.00	0.01	0.28	0.27	59.8%	59.8%	0.3%	0.2%	0.6%	21.2%	20.2%
113		16	144	4	1.12 0.01 0.68 0.01	0.01	0.0	01	0.56	0.44		100.0% 100.0%	0.7%	1.0%	0.8% 4.7%	49.8% 41.2%	38.8% 41.8%	0.55	0.01	0.01	0.01	0.23		48.4% 37.4%	48.4% 37.4%	0.4%	0.9%	0.6%	20.1%	15.2%
115		21	149	4	1.23 0.01	0.01	0.0	02	0.70	0.57		100.0%	0.4%	0.7%	1.8%	57.2% 45.9%	46.3% 42.3%	0.63	0.00	0.01	0.02	0.26	0.25	51.5% 56.3%	51.5% 56.3%	0.3%	0.6%	12%	21.1%	20.1%
115 116 117		22	150	1 4		0.00			0.44	0.38		100.0%	1.4%	0.9%	2.6%	44.7%	20.4%	0.49		0.00		0.19	0.16	49.2%	49.2%	0.8%	0.6%	2.1%	18.9%	16.4%
119		30	158		135 002		0.0	0.2		1.60		100.0%	0.7%	0.2%	7.0% 0.5%	\$1.1% \$9.0%	51.9% 47.8%	2.01	0.01	0.01	0.11	0.92		49.1% 60.1%	49.1% 60.1%	0.5%	0.8%	5.1%	18.7% 27.5%	21.9% 24.4%
121		31	159	10		0.00			1.86	1.63		100.0%	0.9%	0.1%	0.3% 1.2%	54.1% 54.6%	47.4%		0.02					64.0% 54.0%	64.0% S4.0%	0.6%	0.1%	0.3%	25.3% 36.1%	25.5%
122		22	161	10	1.89 0.04	0.05	0.1	10	1.05	0.70		100.0%	2.1%	2.4%	5.5%	55.8%	37.3%	0.77	0.02	0.04	0.08	0.41	0.33	40.8%	40.8%	1.3%	2.1%	4.1%	21.9%	17.3%
121 124 125		38 29			1.37 0.02	0.02	0.0	21	1.41	1.28		100.0%	0.6%	0.9%	4.6%	55.8% 56.8%	50.5% 53.1%		0.01		0.01	0.61	0.97	55.1% 64.6%	55.1% 64.6%	0.4% 0.3%	0.7% 0.1%	3.0%	24.1% 25.7%	22.2% 28.7%
125		40	168	10	2.42 0.04 2.28 0.04	0.01			1.89	1.34		100.0%	1.1%	0.2%	0.3% 4.5%	55.0% 55.6%	19.0% 19.6%			0.01	0.01	0.91	0.76	60.6%	46.0%	0.6% 1.1%	0.1%	0.2%	26.4% 21.4%	22.0%

# - N-patch High CH

																	io out of earns												max ratio out of all I	beams		
	Т	Т				Г			4cm	2 PD(mW)/	cm2)			100.0%	2.2%	2.1%	9.7%	\$9.9%	60.2%	-	4cm2 PD/m	nW/cm2) i	10mm evalu	uation dista	nce	63.9%	63.9%	12%	2.1%	7.4%	27.9%	12.7%
Mod	dule Ty	pe Bear	n ID,1	Sema ID.)	Feed no.		Right) S3(Le	nt) SS(	(Top) S	6(Tottom)	\$1(Front	52/Res	per Beam Back-o (dil)	er (Right 2mm)/(worst surface 2mm)	ratio (Left 2mm)/(wont- surface 2mm)	ratio (Top 2mm)/(wont- surface 2mm)	ratio (Bottom 2mm)/(wont- surface 2mm)	ratio (Fornt 2mm)/(wont- surface 2mm)	ratio (Rear 2mm)/(wonst- surface 2mm)	S4(Right	() S3(Left)	SS(Top)	SE(Edition)	S1(Front)	S2(Rear)	ratio worst-surface (10mm/2mm)	ratio (Right 10mm)/(wont- surface 2mm)	ratio (Left 10mm)/(wond- surface 2mm)	ratio (Top 10mm)/(wonst- surface 2mm)	(Bottom (Bottom 10mm)/(worst- surface 2mm)	ratio (Front 10mm)/(wonst- surface 2mm)	ratio (Rear 10mm)/(wo surface 2mm)
		-	1	-	-	-	20 0.00	0 0	00	0.00	0.09	0.10	+-	100.0%	0.5%	0.9%	0.9%	42.7% 29.5%	47.3% 40.5%	0.10	0.00	0.00	0.00	0.04	0.04	41.5%	43.2% 41.5%	0.5%	0.5%	0.9%	15.9% 12.0%	18.2% 17.0%
			5 7		1	0		0		0.00	0.08	0.08		100.0%	1.1%	0.5%	1.6%	42.3%	41.3% 34.1%		0.00	0.00	0.00	0.03	0.03	42.9%	42.9%	1.1%	0.5%	1.6%	14.8%	14.0%
		_	9	-	-				50	0.00				100.0%	0.9%	0.5%	1.9%	42.5% 17.6%	34.1% 49.5%			0.00	0.00			29.25 44.25	39.3% 44.3%	0.5% 0.5%	0.5%	14%	11.2% 12.9%	13.6%
			14		2			0 0		0.01	0.15			100.0%	0.5%	1.5%	2.3%	38.3%	41.6%		0.00			0.06		33.3%	38.3%	0.3%	1.0%	1.0%	14.2%	14.7%
		$\vdash$	15 16	-	2	-	48 0.00	0 0	00	0.00	0.21			100.0%	0.4%	0.4%	0.8% 1.6%	48.4% 44.8%	53.7% 48.9%	0.27	0.00	0.00	0.00	0.09		56.2% 42.6%	56.2% 42.6%	0.2%	0.2%	0.6%	19.3% 18.9%	25.4% 18.0%
			17		2		35 0.00	0 0	.01	0.01	0.13	0.16		100.0%	0.6%	1.7%	2.3%	38.2%	45.7%		0.00	0.00	0.01	0.04	0.04	27.3%	27.3%	0.3%	1.1%	1.7%	10.3%	12.4%
			21 22		2			0 0		0.01	0.22	0.22	_	100.0%	0.4%	0.9%	1.5% 1.2%	46.3% 53.4%	46.6% 47.6%		0.00	0.00	0.01	0.08		50.9%	50.9% 58.5%	0.2% 0.7%	0.6%	1.2%	18.1% 19.3%	21.6%
		-	22	_	2			0 0		0.01		0.13	-	100.0%	0.7%	0.2%	15%	38.8%	32.2%	0.15	0.00	0.00		0.05		36.0%	36.0%	0.5%	0.5%	2.7%	12.2%	11.9%
		_	29		- 5	9	60 00	1 0	01	0.04	0.37			100.0%	0.7%	1.6%	62% 0.7%	51.6% 57.4%	53.6% 40.8%	0.21	0.00	0.01	0.03	0.14		45.7% 63.8%	45.7% 63.8%	0.4% 0.4%	12%	4.7% 0.5%	20.4% 26.0%	17.2% 24.0%
		-	29 20 21	-	5	H	04 00	1 0	00	0.00	0.57		+	100.0%	0.4%	0.1%	0.4%	54.5%	56.9%		0.00	0.00	0.00	0.27		61.0%	61.0%	0.5%	0.1%	0.3%	26.2%	29.4%
					- 5			1 0		0.02				100.0%	1.6%	0.6%	2.6%	\$1.0%	47.3%		0.01		0.02	0.20		61.4%	61.4%	0.8%	0.5%	1.8%	22.9%	21.0%
			22 28	<del>                                     </del>	5	0		1 0		0.05	0.28			100.0% 100.0%	2.2% 0.7%	2.8%	9.7% 2.9%	56.1% 54.6%	57.9% 36.9%	0.22	0.01	0.01	0.04	0.10	0.10	41.7% 55.4%	43.7% 55.4%	1.0%	1.0%	7.4%	19.1% 25.4%	19.1%
			6		5	1	03 0.01	1 0	00	0.01	0.54	0.62		100.0%	0.8%	0.3%	0.8%	52.4%	60.3%	0.63	0.01	0.00	0.00	0.26	0.34	60.9%	60.9%	0.6%	0.2%	0.4%	25.0%	32.7%
			40		5					0.00		0.59		100.0%	0.7% 2.3%	0.4%	0.4%	51.6% 52.2%	55.1% 57.8%		0.00	0.00		0.25		61.6% 41.2%	63.6% 48.2%	0.4%	0.2%	0.2% 6.7%	21.2%	28.0%
			129	_	1			0 0				0.11		100.0%	0.2%	0.7%	1.6%	32.25 27.1%		0.28		0.01		0.11		41.65	41.6%	0.3%	0.2%	1.2%	11.7%	12.4%
			131			•	33 0.00	0 0	50	0.00				100.0%	0.6%	0.3%	12%	15.7%	28.0%				0.00	0.04		42.7%	42.7%	0.1%	0.3%	12%	11.9%	11.3%
			133	-	+ -	1 0		0 0		0.00	0.13			100.0% 100.0%	0.3%	0.3%	0.9%	36.9% 40.5%	31.4% 32.9%	0.16	0.00	0.00	0.00	0.04		46.5%	46.5% 51.1%	0.3%	0.2%	0.6%	12.5% 14.2%	11.9% 12.7%
			7.01		1	ă	22 0.00	0 0	00	0.00	0.09	0.08		100.0%	0.9%	0.4%	1.3%	40.8%	36.8%	0.11	0.00	0.00	0.00	0.03	0.03	48.0%	48.0%	0.4%	0.4%	0.9%	14.3%	13.99
			142		2			0 0		0.02	0.22	0.18	_	100.0% 100.0%	0.4%	0.6%	15% 0.6%	41.7% 45.9%	34.2% 38.5%	0.24	0.00	0.00	0.02	0.08	0.06	45.5% 58.9%	45.5% 58.9%	0.2%	0.6%	2.9%	14.9% 17.6%	12.4% 16.0%
			44	_	2	+ *	72 0.00	0 0	61	0.01	0.39	0.33	+	100.0%	0.6%	0.7%	0.6%	41.2%	36.0%	0.50	0.00	0.00	0.00	0.15	0.14	51.8%	58.9% 51.8%	0.1%	0.6%	0.5%	16.1%	15.5%
			45		2	0		0		0.01	0.14			100.0%	1.3%	1.6%	2.2%	41.5%	40.0%	0.12		0.00	0.01	0.04		42.5%	42.5%	1.0%	1.2%	1.9%	13.7%	15.6%
			149	_	2					0.02	0.27			100.0%	0.2%	0.2%	2.4%	42.3% 44.8%			0.00		0.01	0.10		41.6%	48.6% 57.3%	0.2% 0.2%	0.2%	1.9%	15.6% 17.0%	13.42
		-	151		2		57 0.01	1 0	01	0.01	0.24			100.0%	0.9%	0.9%	0.9%	41.3%	39.2%	0.28	0.00	0.00	0.00	0.09		49.4%	49.4%	0.5%	0.7%	0.7%	15.3%	16.3%
			57		5		22 0.01	1 0	61	0.06	0.51	0.59		100.0% 100.0%	0.6%	0.5%	4.4% 0.5%	38.1% 48.9%	44.6% 41.0%	0.65		0.00	0.04	0.19		49.2%	49.2% 60.7%	0.5%	0.1%	3.2% 0.3%	14.1% 22.6%	16.3% 20.7%
			59	-	5		04 00	1 0	00	0.00	1.03	0.85	_	100.0%	0.4%	0.0%	0.5%	48.9% 50.7%	41.0%		0.00			0.42		63.1%	63.1%	0.2%	0.0%	0.1%	22.0%	21.3%
			160		- 5		21 00:	2 0	01	0.00	0.73	0.76		100.0%	1.0%	0.6%	0.2%	42.9%	44.4%	0.29	0.01	0.01	0.00	0.33		52.0%	52.0%	0.6%	0.4%	0.2%	19.5%	23.8%
			161	_	- 5	-		1 0		0.01	0.50	0.52		100.0% 100.0%	1.2%	2.6%	0.8% 3.3%	42.7% 40.9%	44.5% 44.6%		0.01		0.01	0.19		29.4%	29.4% 51.7%	0.8%	2.1%	0.7% 2.4%	16.0% 17.5%	16.5%
			167		5	ż	001	1 0	00	0.00		0.90		100.0%	0.2%	0.0%	0.2% 0.2%	51.2%	42.9%	1.22	0.00	0.00	0.00	0.51	0.46	63.5%	63.5%	0.1%	0.0%	0.1%	24.5%	22.2%
			60		- 5					0.00	0.60		_	100.0%	0.6%	0.1%	0.2%	46.6% 42.4%	40.7%		0.01	0.00	0.00	0.41		58.3% 45.0%	58.3% 45.0%	0.5%	0.1%	0.1%	21.6% 17.6%	21.99
			1	129	2			0 0		0.01	0.27	0.30		100.0%	0.5%	0.9%	12%	46.5%	51.2%		0.00		0.01	0.09		44.2%	44.2%	0.3%	0.7%	1.0%	15.6%	18.52
			3	131	2	0	\$9 0.00	0 0	00	0.01	0.23	0.21		100.0%	0.7%	0.7%	1.5%	38.7%	34.5%	0.25	0.00	0.00	0.01	0.07	0.08	41.6%	41.6%	0.3%	0.5%	1.2%	12.5%	12.81
		-	7	133	2	1 8	50 000	0 0	00	0.01	0.21	0.20	+	100.0% 100.0%	0.7%	0.7%	1.4% 1.7%	40.3% 41.2%	34.8% 33.4%	0.26	0.00	0.00	0.01	0.08	0.09	45.1%	45.1% 46.0%	0.5%	0.3%	1.0%	13.8% 12.6%	14.69
			9	137		0		0 0		0.01	0.23	0.24		100.0%	0.7%	0.7%	2.0%	49.0%	52.7%	0.22	0.00	0.00	0.01	0.08		41.4%	48.4%	0.4%	0.4%	1.5%	17.4%	21.59
			14	142		1		1 0		0.03	0.55	0.44	_	100.0%	0.6%	1.4%	3.1%	54.4% 50.6%	43.7% 42.2%		0.00		0.03	0.20		46.2% 58.9%	46.2% 58.9%	0.4%	1.1% 0.1%	2.5%	19.9% 21.4%	16.69
			16	144		H		1 8		0.01	0.60		+	100.0%	0.7%	0.8%	0.9%	49.3%	15.7%		0.00			0.24		47.6%	47.6%	0.2%	0.7%	0.5%	20.0%	15.15
			17	145				1 0		0.02	0.32	0.27		100.0%	1.3%	1.5%	2.8%	45.1%	37.5%		0.01	0.01	0.02	0.09		38.1%	38.1%	0.8%	1.4%	2.2%	13.1%	13.99
			21	149				1 0		0.03	0.68			100.0%	0.4%	0.8%	2.1% 0.5%	55.5% 47.8%	46.0% 39.5%		0.00		0.02	0.26		50.5% 57.5%	50.5% 57.5%	0.2%	0.7%	1.7%	20.9% 17.8%	19.99
			22	151	4		02 0.01	1 0	01	0.03	0.47	0.39		100.0%	1.0%	1.4%	2.8%	46.0%	28.4%	0.49	0.01	0.01	0.02	0.18	0.15	41.4%	48.4%	0.6%	0.9%	2.2%	17.9%	14.9%
		⊨	29	157	10	1 2		1 0		0.14	1.13	1.05	+=	100.0% 100.0%	0.6%	1.2%	6.5% 0.6%	52.5% 59.9%	40.0% 43.4%	1.04	0.01	0.02	0.10	0.43	0.42	48.2%	48.2% 61.0%	0.5%	0.9%	4.6%	20.0% 27.9%	19.6%
		-	21	159	10	1 1	42 00:	1 0	00	0.01	1.82	1.40	-	100.0%	0.0%	0.15	0.0%	51.4%	46.0%	2.18	0.02	0.00	0.01	0.89	0.82	61.0%	63.9%	0.4%	0.1%	0.4%	26.2%	24.19
	- 1	=	22	160	10		.10 0.0-	4 0	02	0.04	1.68	133		100.0%	1.1%	0.6%	1.1%	54.3%	42.9%	1.20	0.02	0.02	0.03	0.80		54.9%	54.9%	0.6%	0.5%	0.9%	25.8%	21.41
		_	18	161				2 0		0.09	1.53			100.0% 100.0%	1.9%	3.1% 1.0%	4.0% 1.9%	56.9% 56.2%	33.9% 44.4%		0.03	0.04		0.50		42.2% 54.4%	42.2% 54.4%	1.2%	1.8% 0.7%	3.1% 2.5%	22.0% 25.4%	15.61
			29	167	10	1	34 0.00	2 0	01	0.01	1.86	1.77		100.0%	0.7%	0.1%	0.4%	55.6%	53.0%	2.12	0.01	0.00	0.01	0.91	0.96	63.7%	63.7%	0.4%	0.1%	0.3%	27.4%	28.7%
		-	40	168	10			0	01	0.01	1.94	1.40		100.0%	0.8%	0.2%	0.3% 3.3%	55.1% 55.3%	39.6% 37.6%	2.15		0.01	0.01	0.91	0.79	61.0% 46.2%	61.0% 46.2%	0.5%	0.2%	0.2%	25.9% 21.3%	22.5% 18.0%
_			41	169	10	, 2	10 00	4   0	06	0.09	1.44	0.98		100.0%	1.5%	42%	43%	35.3%	21.6%	1.20	0.03	0.04	0.07	0.61	0.47	49.2%	46.2%	1.0%	1.4%	2.5%	23%	18.0%

Table 7. PD of Ant N – patch antenna (39GHz – n260)

# - N-patch Low CH

_																																	
																		io out of earns												max ratio out of all I	beams		
ш									4cm	2 PD(mW)	cm2)				100.0%	3.9%	3.9%	13.8%	66.3%	\$3.9%	4	lom2 PD(r	nW/cm2)	at 10mm ev	slustion di	tance	66.8%	66.8%	2.1%	1.6%	10.8%	32.2%	20.4%
Ш	Module Ty	pe Bean	n ID,1 B	ena D,2	Feed no.	S4(Rig	ht) S3(Lef	t) \$5(1	Top) 1	6(Bettom)	S1/Fro		lear) p	per Beam ack-off (dB)	ratio (Right 2mm)/(worst- surface 2mm)	ratio (Left 2mm)/(wont- surface 2mm)	ratio (Top 2mm)/(worst- surface 2mm)	ratio (Bottom 2mm)/(wont- surface 2mm)	ratio (Fornt 2mm)/(worst- surface 2mm)	surface 2mm)		\$3(Left)			1		ratio worst-surface (10mm/2mm)	surface 2mm)	ratio (Left 10mm)/(worst- surface 2mm)	ratio (Top 10mm(y/wonst- surface 2mm)	fatio (Bottom 10mm)/(worst- surface 2mm)	ratio (Front 10mm)/(worst- surface 2mm)	ratio (Rear 10mm)/(worst- surface 2mm)
65		$\vdash$	3		- 1	0.1	0.00	0.0	00	0.01	0.11	0.0	29	_	100.0%	0.6%	0.3%	21% 45%	11.6% 11.1%	16.4% 28.2%	0.17	0.00	0.00	0.01	0.05		51.8% 40.5%	51.8% 40.5%	0.3%	0.3%	15%	11.6% 10.2%	15.1%
65 65 65 65 65 65 65 65 65 65 65 65 65 6			5 7		1	0.21	0.00			0.02	0.13				100.0% 100.0%	0.8%	1.0%	5.2% 4.1%	33.3% 31.7%	30.2% 29.2%	0.17		0.00		0.04		42.9% 40.4%	42.9% 40.4%	0.3%	0.8%	19%	10.6% 9.7%	12.1% 10.0%
68			9		-	0.4	0.00	0.0	00	0.01	0.12	0.3	5		100.0%	0.2%	0.5%	1.4%	27.6%	22.5%	0.21	0.00	0.00	0.00	0.05	0.06	49.1%	49.1%	0.2%	0.5%	0.9%	11.9%	13.5%
20			14		2	0.9	0.01	0.0		0.06	0.31	0.3			100.0%	0.8%	1.2%	62% 4.9%	34.1% 26.9%	11.0% 27.6%	0.33	0.00	0.01	0.04	0.09		36.2%	16.2% 10.8%	0.3%	1.1%	4.0% 3.6%	9.6% 8.6%	11.5%
21			16		2	0.60				0.01	0.32	0.2			100.0%	0.6%	0.5%	2.1%	\$1.1%	44.7%			0.00			0.14	66.2%	66.2%	0.5%	0.3%	1.0%	19.7%	21.8%
72			21			85	0.01	0.0	21	0.02	0.27	6.2	22		100.0% 100.0%	0.6%	1.0%	3.3% 7.5%	33.1% 35.8%	29.5%	0.25	0.00	0.01	0.04	0.09	0.09		42.3% 31.2%	0.3% 0.4%	0.9%	2.6% 5.8%	12.4% 10.5%	15.8% 11.2%
74			22		2	0.71		0.0		0.03	0.28				100.0% 100.0%	0.9%	0.4%	4.5% 2.4%	40.6%	37.3% 38.5%	0.38		0.00	0.02	0.11		54.0% 52.5%	\$4.0% \$2.5%	0.4%	0.3%	3.3% 1.9%	16.1% 16.1%	17.3% 17.2%
76			29		ŝ	2.14	0.02	0.0	03	0.15	0.81	0.7	76		100.0%	0.8%	1.4%	7.0%	37.6%	16.6%	0.82	0.01	0.03	0.12	0.28	0.34	31.2%	38.2%	0.3%	1.4%	5.5%	13.1%	15.6%
77		$\vdash$	30		5	2.2		0.0		0.26	0.73				100.0%	1.2%	0.4%	11.7% 2.0%	32.6% 51.1%	15.0% 46.5%	0.69	0.01	0.01	0.20	0.21		31.2% 65.6%	31.2% 65.6%	0.5%	0.4%	9.1%	9.5% 23.7%	12.8%
79			22		5	1.8	0.01	0.0	00	0.01	0.96	0.8	19		100.0%	0.5%	0.2%	0.6%	51.4%	47.1%	1.24	0.01	0.00	0.01	0.45	0.51	65.8%	65.8%	0.4%	0.1%	0.3%	24.0%	27.0%
80			22 28		5	1.8	0.02	90	05	0.07	0.74				100.0%	1.1%	2.7% 2.5%	1.5% 4.1%	40.4% 41.0%	16.6% 16.6%		0.01	0.05	0.05	0.31		46.45	46.4% 44.8%	0.7%	2.4%	2.5%	17.0% 15.8%	18.6%
82		=	40		- 5	1.3		0.0		0.18	0.47		10		100.0%	1.5%	0.5%	11.8% 0.5%	16.4% 52.2%	29.7% 46.0%		0.01	0.00	0.14	0.22		45.3%	45.3% 66.8%	0.6%	0.3%	0.8%	16.8% 21.7%	15.4% 25.9%
84		_	41		5	1.0		0.0		0.01	0.87				100.0%	0.8%	0.6%	0.4%	47.9%	45.1%		0.01	0.01	0.01	0.42		61.4%	61.4%	0.4%	0.5%	0.3%	23.1%	25.3%
85			129		-	0.21	0.00	0.0		0.00	0.11			L	100.0%	1.6%	0.4%	1.6% 2.0%	43.9% 52.0%	44.2% 24.2%	0.11	0.00	0.00	0.00	0.05		42.0%	42.0% 42.1%	0.8%	0.4%	12%	19.6% 17.3%	20.0%
87			122		- 1	0.21	0.01	Q.	00	0.01	0.16	0.1			100.0%	1.7%	1.0%	1.7%	55.9%	15.9%	0.13	0.00	0.00	0.00	0.05	0.04	43.8%	43.8%	0.7%	0.7%	0.7%	18.6%	13.0%
88			135		- 1	0.30		0.0		0.01	0.15	0.1	11		100.0%	1.3%	0.7%	2.0%	49.0% 44.3%	35.6% 41.3%	0.12		0.00	0.00	0.05		43.0%	43.0% 45.4%	0.7%	0.7%	1.0%	16.4% 17.5%	12.4%
90			42		- 2	0.5		0.0		0.02	0.22	0.1			100.0%	1.5%	1.9%	1.4%	422% 412%		0.17		0.01		0.00	0.05	31.95 46.75	31.9% 46.7%	1.0%	1.3%	1.5%	14.4%	9.7% 15.1%
92		- 1	144		2	0.5		0.0		0.01	0.32				100.0% 100.0%	2.4%	0.8%	1.4%	66.3%	47.5%	0.33		0.00	0.00	0.16		51.3%	58.3%	0.5% 1.2%	0.7%	0.9%	28.6%	22.0%
93			145		2	0.5		0.0		0.01	0.20			L	100.0%	2.6%	1.0%	2.8% 1.9%	39.5% 38.0%	31.4%		0.01	0.00	0.01	0.06	0.05	31.8%	11.0% 16.9%	1.4%	0.8%	2.0%	12.1% 13.1%	10.7%
95	N Par	tch 1	50		2	87	0.01	0.0	00	0.01	0.37				100.0%	1.8%	0.3%	1.4%	52.0%	47.5%	0.29		0.00	0.01	0.16	0.14	55.2%	55.2%	0.8%	0.1%	0.7%	23.2%	20.4%
96			157		- 2	0.53		0.0		0.01	0.24	0.2	22		100.0%	1.9%	1.5%	1.9%	47.0% 54.7%	41.8% 15.9%	0.26	0.01	0.01	0.01	0.10		49.5%	49.5% 49.1%	1.0%	1.0%	1.2%	19.5% 21.3%	17.7% 15.4%
98			58		5	1.2		0.0		0.04	0.62	0.4	17		100.0% 100.0%	2.2%	1.8%	1.4%	49.3% 57.7%	17.0%	0.57	0.01	0.02	0.03	0.29		45.3% 57.2%	45.3%	1.1%	1.5%	2.6%	21.2%	16.2%
100			60		3	13	0.03	0.0	61	0.02	0.74	85			100.0%	3.2% 2.7%	0.3%	1.5% 0.8%	63.4%			0.02	0.00	0.01	0.36	0.28	57.1%	57.2% 57.1%	15%	0.2%	0.7%	28.9% 29.8%	24.2% 23.6%
101			161		5	1.60	0.04	0.0	24	0.03	0.51	0.3			100.0% 100.0%	3.7% 3.7%	19%	12% 17%	50.0% 53.8%	37.5% 31.9%	0.51	0.02	0.03	0.02	0.20		50.1% 41.0%	50.1% 43.0%	2.1% 1.7%	2.7%	1.6%	19.3% 21.8%	15.7% 13.5%
103			67		5	1.4	0.01			0.06	0.73	0.0	53		100.0%	2.2%	0.5%	1.9%	50.0%	43.2%	0.83	0.01	0.00	0.03	0.35	0.29	56.6%	56.6%	1.0%	0.3%	1.9%	24.0%	19.4%
104			160		5	1.4	0.04			0.00	0.95	0.7			100.0% 100.0%	2.1%	0.4% 2.5%	0.2%	64.1% 59.5%	51.7% 45.8%	0.77	0.02	0.00	0.00	0.46		52.1% 63.7%	52.1% 63.7%	1.3%	0.3%	0.1%	31.3% 27.7%	26.7%
106			1	129	2	0.64		0.0		0.01	0.27	0.2	29		100.0%	1.1%	0.6%	17%	40.2% 41.2%	44.2% 11.2%	0.31	0.00	0.00		0.11	0.12	47.6%	47.6% 40.3%	0.6%	0.3%	1.5%	16.2% 11.4%	18.0% 12.5%
107		$\vdash$	5	133	2	0.6	0.01	9.0	01	0.03		0.2	36		100.0%	15%	1.2%	47%	45.1%	35.7%	0.22	0.01	0.01	0.02	0.11	0.11	40.3%	44.0%	0.7%	1.1%	1.2%	15.0%	14.6%
109		┍		135	2	0.75	0.01			0.03					100.0%	0.9%	1.1%	1.5%	40.8% 41.1%	33.8% 35.2%			0.01	0.02	0.10	0.10	42.7%	42.7% 47.9%	0.5%	0.8%	2.7%	11.8%	12.9%
111			14	142	-4	1.4	0.03	0.0	03	0.09	0.68	0.5	14		100.0%	1.9%	1.9%	62%	47.0%	37.5%	0.56	0.01	0.03	0.07	0.23	0.22	31.9%	38.9%	0.8%	1.7%	4.9%	15.9%	15.2%
112			15	143	4	12		90		0.06	0.67	0.0		_	100.0% 100.0%	1.2%	0.9%	3.2% 2.9%	37.2% 57.2%	34.5% 46.2%	0.76	0.01	0.01	0.04	0.27		41.7%	41.7% 61.1%	0.6%	0.7%	2.4%	15.0% 21.1%	14.1%
114				145	4	12	0.02	0.0	02	0.04					100.0%	1.4%	1.1%	2.7%	27.8%	19.2%		0.01	0.01	0.03	0.20	0.24	35.7%	16.7%	0.7%	1.0%	2.2%	14.4%	17.6%
115		$\vdash$	21	149	4			0.0		0.08	0.50	0.4	14		100.0%	1.6%	2.1%	5.9% 2.8%	37.1% 51.1%	32.5% 39.7%	0.53	0.01	0.03		0.17		38.9% 57.9%	38.9% 57.9%	0.7%	1.9%	4.6%	12.7% 21.7%	11.6% 17.6%
117		=	23	151	4		0.02	0.0	03	0.03	0.61	9.5	1		100.0%	1.2%	2.1%	2.1% 5.9%	48.3%	10.9% 42.7%	921	0.01	0.02	0.02	0.26		56.25 41.85	56.2% 41.8%	1.3%	1.2%	1.7%	20.3% 19.8%	18.2% 19.0%
119			30	158	10		0.10	0.0	04	0.36	1.38				100.0%	2.9%	1.2%	10.8%	41.3%	15.6%			0.04	0.28	0.63	0.53	41.0%	41.0%	1.3%	1.1%	8.5%	18.5%	15.9%
120			21	159	10	2.40		0.0		0.09	1.99				100.0% 100.0%	2.0%	0.4%	2.6% 0.7%	58.4% 62.2%	40.6% 51.9%		0.04		0.04	0.97		63.5%	63.5% 60.9%	1.0%	0.2%	1.2%	28.4% 30.1%	19.9% 30.4%
122			22	161	10	1.00	0.10	0	12	0.12	1.58	1 13	5		100.0%	1.2%	1.9%	1.9%	51.6%	43.9%	1.47	0.05	0.11	0.08	0.71	0.68	47.9%	47.9%	1.7%	3.6%	2.7%	23.1%	22.1%
123			38	166	10			9		0.14	1.68			Τ	100.0%	2.8% 2.3%	2.8% 0.6%	4.6% 9.1%	\$3.8% \$1.8%	44.7%		0.05	0.11		0.74		45.5%	45.5% 56.0%	1.5% 1.2%	3.5% 0.3%	3.5% 7.2%	21.5% 25.2%	21.9% 17.7%
102 1031 104 105 106 107 108 109 110 1112 113 114 115 116 117 118 119 120 121 122 123 124 124 125			40	168	10	1.2	0.06	. 0.0	01	0.02	1.92	1.0	10		100.0%	1.8%	0.4%	0.5%	56.6%	53.1%	2.12	0.03	0.01	0.01	0.95	0.98	62.6%	62.6%	0.8%	0.2%	0.3%	27.9%	28.8%
126			41	169	10	2.14	0.05	0.0	05	0.02	2.02	1.6	53		100.0%	1.6%	1.5%	0.7%	64.3%	52.0%	2.04	0.03	0.03	0.01	1.01	0.92	65.1%	65.1%	0.9%	0.8%	0.4%	12.2%	29.3%

# - N-patch Mid CH

$\Box$																		tio out of										-	-	max ratio out of all I	HATE.	-	
									40	m2 PD/m	W/cm2	2)			100.0%	5.1%	9.4%	11.2%	\$3.3%	75.4%	40	cm2 PD(r	nW/cm2)	at 10mm ev	aluation dis	tance	68.3%	68.3%	2.9%	4.9%	8.9%	25.6%	40.9%
No.	Module	Type	Beam ID_1	Berna ID,2	Feed no.	54(Rig	he) 53(L	ett) SS	S(Top)	S6(Botto	om) 51	1(Front)	S2(Rear)	Dearn Back-oft (dB)	ratio (Right 2mm)/(worst- surface 2mm)	ratio (Left 2mm)/(wont- surface 2mm)	ratio (Top 2mm)/(worst- surface 2mm)	ratio (Bottom 2mm)/(wont- surface 2mm)	ratio (Forst 2mm)/(worst- surface 2mm)	ratio (Rear 2mm)/(wonst- surface 2mm)	S4(Right)	S3(Left)	SS(Top)	\$6(Botton	m) S1(Fron	nt) S2/Rea	ratio t) worst-surface (10mm/2mm)	ratio (Right 10mm)/(wont- surface 2mm)	ratio (Left 10mm)/(worst- surface 2mm)	ratio (Top 10mm)/(worst- surface 2mm)	ratio (Bottom 10mm)/(wonst- surface 2mm)	ratio (Front 10mm)/(worst- surface 2mm)	ratio (Rear 10mm)/(worst- surface 2mm)
64		7	-			93		9		0.01		0.12	0.12		100.0% 100.0%	0.9%	0.6%	14%	16.6% 12.6%		0.17			0.00		0.05	49.9%	49.9% 42.0%	0.6% 0.3%	0.2%	12% 27%	11.0%	15.2%
66		Ŀ	5		1	0.4	0.0	10 0	0.01	0.02	$\neg$	0.15	0.13		100.0%	0.6%	1.1%	3.4%	31.7%	28.9%	0.18	0.00	0.00	0.01		0.05	39.4%	29.4%	0.2%	0.9%	2.8%	9.7%	11.0%
67		ŀ	7 9			0.40		10 0		0.01		0.13	0.12	-	100.0%	0.7%	0.5%	2.7% 1.6%	12.8% 17.6%	29.9%	0.17			0.01	0.04	0.04	42.3%	42.3% 49.8%	0.5% 0.2%	0.5%	2.0%	10.2% 12.7%	10.9%
69 70		Ė	14		2	0.90	0.0		0.01	0.04		0.29	0.33		100.0%	0.6%	1.4%	3.7%	40.6%	34.7%	0.43	0.00		0.03	0.13		45.0%	45.0% 34.1%	0.4%	1.2%	2.9%	11.9%	14.4%
71		ŀ	15		2	0.8	0.0	11 0	0.00	0.03	+	0.26	0.24	_	100.0%	0.6%	0.3%	15% 0.7%	30.3% 50.1%	28.1% 44.6%	0.30	0.00	0.00	0.02	0.10	0.10	34.1%	34.1% 66.1%	0.2%	0.2%	2.8%	11.0%	12.0%
72		- F	17		2	0.80	0.0	1 0	0.00	0.02		0.29	0.28		100.0%	0.6%	0.5%	2.1%	15.6% 11.9%	35.0%	0.27			0.01	0.10	0.13	45.5%	45.5% 31.5%	0.5%	0.4%	1.7%	12.4%	15.9%
73 74 75 76		H	21		2	8.7		8		0.02	-	0.32	0.10	_	100.0%	0.4%	0.1%	2.7%	40.6%	19.2%	0.30				0.10	0.11	54.4%	54.4%	0.1%	0.0%	2.0%	16.2%	19.4%
75		F	21 29		2 5	0.8	0.0	11 0	0.01	0.02		0.38	0.78	_	100.0%	0.8%	0.9%	1.9%	41.4%	39.0% 34.5%	0.48	0.00	0.01	0.01	0.13		55.6% 41.6%	55.6% 41.6%	0.5%	0.9%	1.4%	15.4% 17.4%	17.2% 16.3%
		- H	30		- 5	2.00	0.0	12 0	0.01	0.20		0.79	0.69	_	100.0%	1.1%	0.4%	9.6%	37.9%	32.9%	0.71	0.01	0.01	0.16	0.26	0.27	34.0%	34.0%	0.6%	0.2%	7.4%	12.5%	12.0%
78 79		F	31		5	1.4	0.0		10.0	0.01		0.70	0.68		100.0%	0.8% 1.7%	0.7%	0.8%	48.2% 51.0%	47.1% 45.6%	0.91			0.01	0.32	0.40	62.8%	62.8% 67.0%	0.8%	0.3%	0.5%	22.3% 25.5%	27.3% 26.1%
80		Ŀ	22		3		0.0	2 0	0.04	0.01		0.93	0.06		100.0%	0.7%	1.8%	3.7%	41.7%	28.4%	1.12	0.01	0.04	0.05	0.42	0.47	49.9%	49.9%	0.5%	1.6%	2.4%	18.6%	21.1%
81		- 1	38 29			13	0.0	11 0		0.09		0.97	0.86	-	100.0%	0.6%	1.2%	42% 11.3%	41.2% 16.0%	38.3% 38.0%				0.07	0.42	0.45	41.9% 51.3%	48.9% 51.3%	0.4%	1.5%	1.0%	18.7%	20.0%
83 84		Ŀ	40		- 3	130	0.0	F1 0	0.00	0.01	$\neg$	0.96			100.0%	0.5%	0.2%	0.1%	52.8%	45.9%	1.25	0.01	0.00	0.00		0.47	61.25	68.3%	0.5% 0.4%	0.1%	0.2%	15.2% 24.3%	20.1% 23.7%
85		ŀ	41 129		5	1.80		13 0	0.00	0.01		0.88	0.79	+	100.0%	1.4%	0.7% 1.2%	0.6% 1.2%	48.8% 40.5%	44.0% 47.0%	0.11	0.01	0.01	0.01	0.42	0.45	63.7% 43.7%	63.7% 43.7%	0.7% 0.4%	0.6%	0.3%	23.3% 16.2%	25.0% 23.5%
26		Ŀ	131		1	02	0.0		0.00	0.00		0.10	0.13		100.0%	1.9%	1.1%	1.5%	18.6%	49.4%	0.12		0.00	0.00	0.03	0.06	44.2%	44.2%	0.7%	0.7%	1.1%	12.7%	21.3%
87		H	133		-	0.21			0.01	0.01		0.11	0.14	_	100.0%	2.4%	3.1% 2.0%	2.8% 1.7%	29.4% 27.2%	40.4% 40.7%			0.01		0.03		45.6%	44.6% 45.6%	1.0%	1.7%	1.4%	10.5% 10.4%	20.2%
29			137		1	0.2	0.0		000	0.00		0.12	0.17		100.0%	2.1%	1.2%	0.6%	16.9%	51.5%	0.15				0.05		44.2%	44.2%	0.9%	0.6%	0.3%	14.0%	22.0%
88 89 90 91 92 93 94 95		H	142		2 2			2 0		0.02		0.21	0.17	_	100.0%	2.0%	5.1%	1.0%	39.6% 38.1%		0.17			0.01	0.06	9.11	31.9% 44.1%	31.9% 44.1%	1.9%	1.0% 0.5%	2.4% 1.2%	12.0%	13.7%
92		F	144		2					0.01		0.21	0.39	-	100.0%	2.3%	1.8%	1.4%	37.9% 41.1%	69.0% 34.5%	0.35			0.00		0.19		12.6%	1.1%	0.9%	0.7%	14.4%	33.5% 14.7%
94		Ŀ	149		2		0.0	11 0	0.01	0.01		0.23	0.19		100.0%	2.0%	2.0%	1.7%	38.4%	31.5%	0.20	0.01	0.01	0.01	0.07	0.06	33.3%	11.1%	0.8%	1.2%	1.3%	11.9%	10.6%
95	N S	Patich	150		2	0.63	0.0		0.00	0.01		0.25	0.40	-	100.0%	2.7%	0.3%	1.6%	37.6% 33.1%	60.4% 58.1%	0.38			0.01	0.10		56.2% 49.3%	56.2% 49.3%	1.2%	0.1%	0.9%	15.6%	28.2%
96		Ŀ	157		ŝ	19	0.0	12 0	0.04	0.03		0.47	0.30		100.0%	2.9%	15%	3.4%	46.7%	29.3%	0.29	0.02	0.03	0.03	0.19	0.14	31.25	28.3%	1.6%	2.5%	2.7%	18.9%	14.1%
98		ŀ	158		5	1.00	0.0	2 0	0.02	0.07	+	0.53	0.33	+-	100.0%	1.6%	1.7%	6.0% 1.9%	48.8% 40.3%	30.7% 64.6%	0.48			0.05	0.24		44.0% 58.7%	44.0%	0.8%	1.5%	4.9%	21.7% 19.3%	12.6% 33.5%
100		Ė	160		- 5	12		4 5		0.00	_	0.29	0.93		100.0%	2.9%	1.1% 4.5%	0.3%	32.1% 42.8%	75.4%	0.78	0.02		0.00	0.16		63.1%	63.1%	1.5% 2.1%	0.6%	0.2%	11.0%	40.9% 16.1%
102		H	166		3	1.00		12 0		0.01		0.49	0.29	+	100.0%	2.5%	2.9%	16%	46.4%	27.6%	9.41			0.02	0.16		38.7%	38.7%	1.3%	2.2%	2.9%	18.7%	12.5%
103		- 1	167		5	1.10		4 0	0.01	0.06		0.62	0.54		100.0% 100.0%	3.8% 2.9%	0.4%	5.3% 0.2%	53.3% 36.3%	46.7% 60.0%	0.70			0.03	0.29		60.2% 59.8%	60.2% 59.8%	2.0% 1.5%	0.3%	2.8%	24.9% 14.1%	21.6%
104		- t	169		3	0.9	0.0	15 0	90.0	0.01		0.43	0.67		100.0%	5.1%	9.4%	1.3%	44.6%	70.1%	0.59	0.03	0.05	0.01	0.19	0.36	61.8%	61.0%	2.9%	4.9%	0.6%	20.3%	37.7%
105		F	-	129	2	3.0	0.0		10.0	0.01		0.27	0.32		100.0%	1.3%	1.2%	1.5% 1.6%	29.7% 22.7%	47.0% 42.4%	0.22		0.01	0.01	0.10	0.14	47.9%	47.9% 44.2%	0.6%	0.7%	1.2%	15.3% 9.3%	20.1%
108		Ŀ	ŝ	122	2	0.81	0.0	11 0	0.02	0.03		0.31	0.35		100.0%	1.2%	2.5%	1.9%	18.5%	43.5%	0.22	0.01	0.01	0.02	0.09	0.15	40.0%	40.0%	0.6%	1.4%	1.0%	11.3%	18.9%
109		- 1	7	135	- 3	9.2	90	1 9	0.01	0.02		0.29	0.35	-	100.0%	1.6%	135	2.9%	17.8% 19.4%	45.8% 47.2%	0.35	0.01	0.01	0.02		0.14	45.95	45.9%	0.9%	0.8%	22%	11.9%	18.4%
111		Ŀ	14	142	- 4	1.6	0.0	13 0	0.05	0.08		0.83	0.70		100.0%	1.7%	12%	4.9%	50.3%	42.8%	0.72	0.02	0.03	0.06	0.31		44.0%	44.0%	1.0%	1.9%	1.9%	18.9%	18.0%
112		ŀ	15	143	4	1.7	9.0		0.01	0.06		0.59	0.59	+	100.0%	1.4%	0.7% 1.3%	32% 1.1%	31.9% 45.0%	34.1% 55.3%	0.76			0.04	0.23	0.22	41.7% 62.6%	43.7% 62.6%	0.6%	0.6%	2.5% 0.7%	13.4% 18.2%	12.6%
114		ŀ	17	145	4	1.4	0.0	2 0	0.02	0.04		0.48	0.60		100.0%	1.2%	1.1%	2.7%	12.7%	40.9%	0.62	0.01	0.01	0.03	0.16	0.27	42.2%	42.2%	0.5%	0.8%	2.1%	11.0%	18.4%
115		ŀ	21	149	4	15	9.0		0.00	0.07		0.60	0.50	_	100.0%	1.2%	1.8%	4.6% 2.1%	39.5% 43.4%	33.3% 47.8%	1.00	0.02		0.05	0.23		11.2% 60.6%	11.2%	1.0%	1.5%	1.6%	15.5% 17.7%	14.7% 24.1%
117		- 1	23	151	-4	2	9	12 0		0.03		0.50	0.59		100.0%	1.7%	2.3%	2.6%	29.0%	46.1%	0.66	0.01	0.02	0.03	0.19	0.28	51.8% 44.4%	\$1.0%	0.9%	1.5%	2.0%	14.5%	22.2%
118 119 120		Ŀ	29 30	157 158	10	13		7 0	0.04	0.24		132	128		100.0%	2.0% 1.9%	2.2% 1.0%	6.5% 8.2%	53.2% 49.0%	38.7% 34.4%	1.69	0.04	0.03	0.24	0.71	0.68	45.6%	44.4% 45.6%	1.0%	2.0%	5.1% 6.4%	23.1% 19.7%	18.3%
120		F	31 32	159	10	2.12		2 0		0.07		1.56	1.87	_	100.0%	2.4% 1.2%	0.9%	2.1%	49.8% 47.7%	59.8% 62.2%	2.05		0.01	0.03	0.74		65.6%	65.6%	12%	0.4%	1.1%	23.6% 22.8%	34.9%
122		- E	33	161	10	27	0.0	6 0	0.12	0.16		1.89	1.63		100.0%	1.6%	3.3%	4.4%	50.4%	43.2%	1.92	0.03	0.11	0.12	0.88	0.06	51.2%	51.2%	0.9%	1.0%	12%	21.5%	22.8%
123		F	38 29	166	10	19		9 0		0.20		2.04	1.67	+ =	100.0%	1.5%	2.9%	5.1% 9.6%	52.3% 49.0%	42.8% 37.8%	1.92		0.10	0.15	0.94	0.87	49.2% 60.3%	49.2% 60.1%	0.7% 1.4%	2.6%	1.9% 7.4%	24.1% 22.4%	22.2% 18.4%
125		Ŀ	40	160	10	2.8	0.0	7 0	0.02	0.02		1.59	2.37		100.0%	1.0%	0.5%	0.4%	41.6%	62.2%	2.34	0.03	0.01	0.01	0.72	1.37	61.4%	61.4%	0.9%	0.2%	0.2%	18.8%	26.1%
126								3 0		0.03		1.71	1.96																				

# - N-patch High CH

														max rat													max ratio out of all I	beams		
$\Box$			T	Т			4cm2 PD	l/mW/cm	(2)			100.00			sant	70.00	77.00	-	lom2 PD(m	W/cm2) i	t 10mm eval	luation dis	tance	l	71.00	179		I		0.0%
No.	Andule Typ	e Beam ID_1	Sens D.J	Feed no.		Т	Т	Т			per Bears	ratio	ratio	ntio	ratio	ratio	ratio		T			П	T	ratio	ratio	ntio	ratio	natio (Sottom	ratio	ratio
					S4(Right) S3(Le	n) SS(To	p) 56(Bo	ottom) S	1(Front)	S2(Rear)	Back-off	(Right 2mm)/(worst- surface 2mm)	(Left 2mm)/(wont- surface 2mm)	(Top 2mm)/(wonst- surface 2mm)	(Bottom 2mm)/(worst- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(worst- surface 2mm)	S4(Right	(fa.1,62	SS(Top)	S6(Bottom)	S1/Fron	t) S2(Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(worst- surface 2mm)	(Left 10mm)/(wont- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	10mm)/(worst- surface 2mm)	(Front 10mm)/(wonst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
64		-		-		0.00			0.10		-	100.0% 100.0%	1.4%	0.3%	1.4% 1.2%	17.5% 14.8%					0.00		0.04	49.1% 46.3%	49.1% 46.3%	0.7% 0.3%	0.7%	1.1% 2.7%	12.6%	13.0% 13.6%
66		5 7			0.42 0.00	0.01	0.0	01	0.15	0.13		100.0%	1.0%	12%	22% 15%	34.7% 36.1%	30.4% 20.8%	0.18	0.00	0.00	0.01	0.04		42.6% 45.6%	42.6% 46.6%	0.5%	1.0%	17%	10.5%	11.2% 11.0%
64 65 66 67 68 69 70 71 72 73		9	_	-	0.16 0.00	0.00	0.0	01	0.14	0.12		100.0%	0.6%	0.8%	1.7%	38.0%	36.4%	0.18	0.00	0.00	0.00	0.05	0.05	50.7%	50.7%	0.3%	0.3%	1.1%	12.9%	14.0%
69		14		2		0.01			0.33	0.27		100.0% 100.0%	1.6%	1.5%	2.7% 2.8%	37.8% 28.1%	10.6% 27.9%	0.38	0.01	0.01	0.02	0.12		41.3%	41.3%	0.8% 0.4%	1.4%	2.0%	11.9% 10.1%	13.8%
21		16		2		0.01			0.33	0.28		100.0%	0.9%	0.9%	1.3%	52.1%	44.2%	0.43		0.01	0.00	0.13		66.5%	66.5%	0.5%	0.8%	0.6%	20.7%	22.5%
72		21		2	0.84 0.0	0.01	0.1	03	0.29	0.24		100.0% 100.0%	1.1%	0.6%	22% 3.7%	37.4% 34.3%	28.3%	0.30	0.01		0.02	0.09	0.11	45.5% 35.9%	45.5% 35.9%	0.6% 0.6%	0.4%	1.7%	12.1% 11.1%	15.2% 12.6%
74		22		2	0.02 0.01	0.00	0.0	01	0.31	0.31		100.0% 100.0%	0.7% 1.5%	0.4%	1.7%	41.5% 47.6%	43.7% 20.4%	0.42	0.00	0.00	0.01	0.12		58.6%	58.6% 59.8%	0.4% 0.7%	0.1%	1.3%	17.1% 18.3%	21.0% 17.0%
76		29		5	1.62 0.0				0.76	0.60		100.0% 100.0%	1.5%	0.9%	5.4% 8.0%	41.6% 29.1%	32.8% 33.6%	0.73	0.01	0.02	0.08	0.32		39.8% 41.7%	29.8% 41.7%	0.7% 0.6%	0.8% 0.2%	4.2% 6.2%	17.5% 13.4%	17.0% 17.6%
78		21		3	1.21 0.01	0.02	0.		0.63	0.64		100.0%	1.0%	1.6%	0.9%	48.3%	48.7%	0.83		0.01	0.01	0.29	0.37	63.1%	63.1%	0.8%	0.7%	0.5%	22.0%	28.2%
75 76 77 78 79 80 81 82 83		22		5	1.66 0.03	0.01	0.	01	0.98	0.77		100.0%	1.9%	0.4%	0.4% 3.4%	58.0% 43.1%	45.8% 38.7%	1.20	0.02	0.00	0.00	0.47		71.2% 52.3%	71.2% 52.3%	1.0%	0.2%	0.2%	28.0% 20.3%	24.6%
81		28 29		- 5	1.79 0.04	0.03	0.0	97	0.78			100.0%	2.1%	1.7%	4.1% 8.2%	41.6% 40.5%	28.4%	0.91	0.02	0.03	0.05	0.36	0.39	50.9% 50.8%	50.9% 55.8%	1.1%	1.5%	2.8%	19.8% 18.1%	21.6%
82		40	_	- 5	1.61 0.0	0.01	0.0	0.2	0.90	0.72		100.0%	0.9%	0.3%	14%	55.7%	45.0%	133	0.01	0.00	0.01	0.42	0.40	70.0%	70.0%	0.7%	0.1%	0.7%	25.9%	24.6%
84		41 129	-	5		0.02			0.87	0.73		100.0%	2.2%	1.0%	0.5%	52.7% 40.6%	44.3% 47.5%	0.11	0.02	0.01		0.40	0.41	67.3% 48.7%	67.3% 48.7%	1.2% 0.8%	0.8%	0.4%	24.5% 16.1%	24.7%
85 86 87 88 89 90 91 92		131			0.30 0.00	0.00	0.0	01	0.11	0.14		100.0%	1.3%	0.3%	1.7%	36.6% 40.1%	45.6% 49.2%	0.12	0.00	0.00	0.00	0.03	0.06	40.6%	40.6% 42.4%	0.7% 1.2%	0.3%	1.0%	11.1%	20.1%
88		135		1	0.35 0.01	0.00	0		0.14	0.17		100.0%	2.0%	0.6%	1.4%	16.6%	49.0%	0.15	0.00	0.00	0.00	0.05		42.4%	42.4%	1.2%	0.3%	12%	13.5%	19.3%
89		137		1 2	0.35 0.01	0.00	0 0		0.14	0.18		100.0% 100.0%	1.7%	0.9%	0.6%	29.1% 35.5%	52.6% 34.3%	0.16	0.00	0.00	0.00	0.06	0.08	46.8% 31.7%	46.8% 33.7%	0.9%	0.6% 1.0%	0.6%	16.7% 12.2%	23.0%
91		143		2	0.74 00:	0.01	0.	01	0.29	0.31		100.0%	2.4%	0.7%	15%	39.2% 41.4%	42.7%	0.32	0.01	0.00	0.01	0.11		42.9% 57.4%	42.9% 57.4%	12%	0.4%	12%	11.6% 21.4%	19.9%
92		145		2		0.00			0.21	0.17		100.0%	1.4%	0.5%	2.0%	40.3%	30.9%		0.00	0.00	0.00	0.08	0.08	32.3%	12.1%	0.5%	0.5%	1.6%	14.7%	13.3%
94	N Patr	149 h 150	+	2		0.01			0.26	0.24		100.0%	1.9%	1.2%	1.9%	37.8% 40.7%	35.2% 62.0%	0.22	0.01	0.00	0.01	0.09		32.1% 57.2%	32.1% 57.2%	1.0%	0.6%	1.4%	12.5% 19.5%	12.5%
96		151		2		0.00			0.22	0.28		100.0%	1.2%	0.7% 2.2%	1.1%	39.2% 44.2%	50.0% 33.8%	0.28	0.00	0.00	0.01	0.09		41.0%	48.6% 43.7%	0.5% 1.5%	0.4%	0.9%	16.1% 20.5%	27.0%
98		158		3	1.14 0.03	0.01	0.0	97	0.59	0.31		100.0%	1.7%	1.2%	5.9%	51.2%	26.9%	0.51	0.01	0.01	0.05	0.27	0.12	44.2%	44.2%	0.7%	2.0%	2.8%	21.6%	10.6%
100		159	+	- 3		0.00			0.62	1.04		100.0% 100.0%	2.5%	0.5%	1.9%	40.9% 18.6%	68.2% 72.9%	0.89	0.03	0.00			0.56	58.7% 60.0%	58.7% 60.0%	1.9%	0.2%	0.9%	22.2% 22.1%	36.5% 41.7%
101		161		3		0.02			0.52	0.38		100.0%	1.0% 2.5%	2.1%	1.4%	48.5% 42.7%	15.5% 11.4%		0.02	0.02	0.03	0.22	0.16	45.0%	45.0% 41.7%	1.5%	2.0%	2.4%	20.8% 19.4%	15.0%
103		167		5	1.17 0.01	0.01	0.1	05	0.64	0.57		100.0%	5.4%	0.4%	4.1%	54.5%	48.9%	0.68	0.03	0.00	0.04	0.29	0.26	51.3%	58.3%	2.7%	0.3%	1.3%	24.8%	22.4%
104		160	_	5	1.22 0.05	0.01	0.1		0.44	1.00 0.85	_	100.0%	1.7%	2.2%	1.1%	11.6% 45.0%	75.6% 64.1%	0.75	0.01	0.00	0.01	0.31		61.2% 56.3%	63.2% 56.3%	0.8% 1.7%	0.2% 1.5%	0.5%	18.5% 21.5%	42.6% 34.8%
106		1	129	2	0.58 0.01	0.01	0.0	01	0.24	0.28		100.0% 100.0%	1.5%	1.2%	12% 15%	41.8% 12.0%	46.1%	0.29	0.00	0.00	0.01	0.09		49.5%	49.5% 46.6%	0.7% 0.7%	0.5%	1.0%	15.6% 11.1%	21.3% 20.3%
95 96 97 98 99 100 101 102 103 104 105 106 107 108		-	123	2		0.01		02	0.32	0.38		100.0% 100.0%	2.0%	1.2%	2.7%	37.0% 36.1%	44.1%	0.36	0.01	0.01	0.02	0.11	0.17	41.85 42.95	41.8% 42.9%	10%	1.2%	20%	12.3%	19.4% 17.1%
110		7	135		0.01 0.01	0.01	0.1	01	0.32	0.40		100.0%	1.7%	1.4%	2.1%	39.1%	49.0%		0.01	0.01	0.01	0.12	0.15	47.3%	47.3%	0.9%	0.6%	1.0%	12.2% 15.2%	22.8%
111		14	142	4	1.76 0.01	0.03	0.0	07	0.80	0.73		100.0%	2.7%	0.7%	1.0% 2.9%	45.7% 16.0%	41.4% 24.5%	0.81	0.02	0.03	0.05	0.32	0.33	45.0%	46.0% 42.0%	1.3% 0.7%	1.5% 0.6%	2.9%	18.3% 11.4%	18.6% 16.7%
113		16	144	1 4	1.62 0.03	0.02	0.	03	0.71	0.88		100.0%	1.8%	1.1%	1.7%	45.2%	\$4.5%	0.22	0.02	0.01	0.01	0.32		61.3%	61.3%	0.9%	0.6%	0.7%	19.5%	28.5%
114		17 21	145 149	4	1.39 0.0				0.56	0.52		100.0%	1.4%	1.2%	12% 17%	40.4% 41.9%	37.5% 38.0%	0.00	0.01	0.01	0.04	0.21	0.25	41.9% 29.7%	41.9% 29.7%	0.7% 1.3%	0.7% 1.1%	2.5%	15.1% 17.0%	18.0% 16.9%
115 116 117		22	150	4	1.50 0.00	0.01	0.0	02	0.57	0.91		100.0%	1.5%	0.3%	1.5%	36.1% 44.1%	57.5% 41.9%	0.92	0.01	0.00	0.02	0.26		51.2%	58.2% 57.1%	0.7% 1.2%	0.2%	12%	16.6% 17.8%	31.1% 23.3%
116		29			2.21 0.01	0.06	0.	22	1.80	1.35		100.0% 100.0%	2.6%	1.9%	15% 66%	54.3%	40.6%	1.61	0.04	0.06	0.17	0.85	0.67	48.5%	37.1% 48.5% 51.3%	1.3%	1.7%	1.4% 5.0% 5.8%	25.7%	20.2%
119		31	159	10		0.05	0.0	08	1.30	2.20		100.0%	2.6%	1.5%	2.4%	40.8%	68.5%	2.04	0.05	0.02		0.61	1.29	51.3% 63.6%	63.6%	1.0% 1.7%	0.7% 0.7%	1.1%	22.3% 18.9%	14.8% 40.2%
121		32 11	160	10		0.04			1.87	2.27 1.58		100.0%	11%	1.1% 2.7%	0.2% 4.4%	46.6% 54.2%	56.6% 43.4%	2.48	0.07	0.02		0.96	1.36	61.9% 54.9%	61.9% 54.9%	1.6%	0.5% 2.5%	2.9%	24.0% 26.2%	34.0% 22.6%
123		38	166	10	2.59 0.13	0.09	0.	19	1.97	1.57		100.0%	1.5%	2.5%	5.4%	54.9%	43.8%	1.94	0.06	0.06	0.14	0.96	0.83	53.9%	53.9%	1.7%	2.2%	2.8%	26.7%	23.2%
124		29 40	160	10	1.65 0.01	0.01		06	1.44			100.0%	3.2% 1.8%	0.5%	8.5% 1.8%	48.7% 40.5%	43.7% 59.9%	2.29		0.01	0.03	0.66	1.30	62.1%	62.1% 62.7%	1.6%	0.3%	6.6%	22.4% 18.3%	24.0% 35.6%
126		41	169		2.71 0.11				1.94			100.0%	4.1%	2.1%	0.9%	52.2%	55.8%	2.26			0.03			61.0%	61.0%	2.1%	0.9%	0.7%	26.4%	12.6%

Table 8. PD of Ant N- patch antenna (24GHz - n258)

# - N-patch Low CH

_																io out of												max ratio out of all I			
$\vdash$		_		_	_			4cm2 PD:		_					all b				-			t 10mm eval			<del>                                     </del>						
11					$\vdash$		_	4CEL PU	mwycnu	0	_	ner.	100.0%	2.3%	5.2%	11.0%	46.0%	100.0%	•	CRU PUIT	wycmz) i	it tomin eva	uston as	tance	54.6%	\$4.6%	1.8%	445	8.1% ratio	22.0%	41.1%
No.	Module Tys	pe Beam	ID_1 Berna B	0,2 Feed		(Right) S3(Left)	SS(Top	s6(Bot	ttom) S1	(Front)	S2(Rear)	Beam Back-off	ratio (Right 2mm)/(worst- surface 2mm)	ratio (Left 2mm)/(wont- surface 2mm)	ratio (Top 2mm)/(wont- surface 2mm)	ratio (Bottom 2mm)/(wont- surface 2mm)	ratio (Fornt 2mm)/(worst- surface 2mm)	ratio (Rear 2mm)/(wont- surface 2mm)	S4(Right)	S3(Left)	SS(Top)	S6(Bottom)	\$1(Fron	s2(Read	ratio worst-surface (10mm/2mm)	ratio (Right 10mm)/(worst- surface 2mm)	ratio (Left 10mm)/(wont- surface 2mm)	ratio (Top 10mm)/(wonst- surface 2mm)	(Bottom 10mm)/(worst- surface 2mm)	ratio (Front 10mm)/(wonst- surface 2mm)	ratio (Rear 10mm)/(wont- surface 2mm)
64				-	#			0.0		0.06	0.15	1280	100.0%	1.6%	0.5%	5.8%	28.8%	78.5%	0.07	0.00		0.01		0.06	38.2%	38.2%	1.6%	0.5%	17%	8.9%	30.9%
64 65 66 67 68 69 71 72 71 72 73 74 75 76 77 78 80 81 80 81		3	_	-	+		0.00			0.07	0.11		100.0%	0.5% 2.1%	0.5%	4.8% 5.5%	15.5% 22.1%	58.6% 64.0%	0.06	0.00	0.00	0.01	0.02		41.9%	41.9% 29.3%	0.5% 0.7%	0.5%	12% 41%	12.9%	22.0% 25.5%
6.7		7 9		- 1	-	0.15 0.00	0.00			0.05	0.10		100.0% 100.0%	1.3%	0.7%	1.9% 2.4%	12.9% 12.5%	65.1% 70.7%	0.06	0.00	0.00	0.01	0.02		36.8% 29.0%	16.8% 29.0%	0.7% 1.6%	0.7% 0.8%	3.3% 1.6%	11.8% 10.6%	21.1%
69		14	4	- 2	$\pm$	0.12 0.00	0.00	0.0	13	0.04	0.27		100.0%	1.6%	0.6%	11.0%	25.2%	88.4%	0.05	0.00	0.00	0.00	0.02	0.10	35.5%	35.5%	1.3%	0.2%	8.1%	6.8%	31.6%
70		15		2	+	0.39 0.00	0.00	0.0	12	0.15	0.23		100.0%	1.0%	0.3%	2.6%	29.3% 35.1%	59.7%	0.18	0.00	0.00	0.01	0.06		46.5%	46.5% 46.0%	0.8%	0.3%	2.1%	15.5% 12.1%	25.6% 27.2%
72		17	7	- 2	#			0.0			0.16		100.0%	1.7%	145	72% 56%	36.6% 33.1%	54.8%	0.11	0.00	0.00		0.04	0.07	45.55 29.45	45.5% 19.4%	1.0%	1.0%	5.1% 4.2%	12.7%	23.6% 22.8%
74		22	2	2		0.37 0.01	0.00	0.0	10	0.12	0.28		100.0%	1.3%	0.3%	1.1%	31.8%	75.1%	0.19		0.00	0.00	0.05	0.13	50.0%	50.0%	0.8%	0.3%	0.8%	12.0%	15.6%
75		23	1	2	+	0.26 0.01	0.00			0.07	0.19		100.0% 100.0%	2.3%	1.15	3.4% 6.8%	28.1% 32.2%	73.8% 64.6%	0.10	0.00	0.00	0.01	0.03		39.2%	19.2% 16.0%	1.5%	0.8%	2.7% 5.5%	9.5% 11.2%	30.8% 29.9%
77		20	0	- 5		0.95 0.01	0.00	0.0	12	0.36	0.57		100.0%	1.0%	0.4%	1.0%	27.8%	60.2%	0.44	0.01	0.00	0.01	0.14	0.28	45.9%	46.9%	0.7%	0.2%	1.1%	14.9%	30.1%
78		21		- 5	+		0.00			0.36	0.76		100.0%	1.9%	0.3%	0.7% 1.3%	23.3% 23.1%	70.9% 62.7%	0.57	0.02	0.00	0.00	0.17		52.9% 46.2%	52.9% 46.2%	1.4%	0.2%	0.3%	16.0% 13.1%	41.1% 31.2%
80		23	1	- 3	#	0.71 0.01	0.02	0.0	13	0.28	0.16		100.0%	1.4%	2.4%	1.9%	29.2%	50.6%	0.21	0.01	0.01		0.08	0.17	44.1%	44.1%	1.0%	2.0%	2.0%	11.0%	23.8%
82		31		3	_	1.06 0.01	0.00	0.0		0.37	0.57		100.0%	1.3%	0.2%	6.0% 0.9%	11.2% 15.3%	64.7%	0.54	0.01	0.00	0.01	0.16	0.41	29.8% 51.4%	39.8% 51.4%	0.6% 0.9%	0.1%	5.4% 0.7%	12.5% 13.5%	30.4% 38.9%
83		40		- 5		0.86 0.02	0.00			0.30	0.64		100.0%	1.9%	0.3% 1.9%	0.6% 3.7%	31.9% 36.8%	72.2% 51.7%	0.46	0.01	0.00	0.00	0.14	0.36	51.7% 41.6%	51.7% 41.6%	1.1%	0.2% 1.6%	0.3%	15.4% 11.2%	40.2% 24.2%
85		121	9	1	_	0.15 0.00	0.00	0.0	10	0.05	0.10		100.0%	0.6%	1.3%	1.3%	33.8%	61.7%	0.06	0.00	0.00	0.00	0.02	0.04	36.4%	36.4%	0.6%	1.3%	1.3%	11.0%	28.6%
86		12		- 1		0.12 0.00 0.12 0.00	0.00			0.03	0.08		100.0%	0.8%	3.3% 1.6%	25% 32%	27.9% 34.9%	65.6%	0.04	0.00	0.00	0.00	0.01		34.4% 41.2%	34.4% 41.3%	0.8%	2.5%	1.6%	9.8%	20.5%
88		120		- 1	#		0.00			0.04	0.08		100.0% 100.0%	1.5%	1.5%	4.4% 2.9%	21.4% 22.4%	61.3%	0.05		0.00	0.00	0.02		29.4%	29.4% 11.1%	0.7% 1.0%	0.7%	2.9%	10.9% 11.4%	20.4%
90		16	2	- 2	_	0.22 0.00	0.01	0.0	10	0.08	0.16		100.0%	1.2%	1.5%	4.2%	35.7%	69.6%	0.00	0.00	0.01		0.03	0.07	34.8%	34.8%	0.9%	2.6%	1.0%	11.7%	32.2%
91		14		2			0.00	0.0		0.12	0.16		100.0%	0.9%	2.2%	2.7%	29.7% 22.8%	54.3% 70.5%	0.14	0.00	0.00	0.01	0.04	0.08	45.3%	45.3% 40.7%	0.3% 0.7%	1.9%	2.0%	14.7% 11.2%	26.7%
93		140		2			0.01			0.06	0.23		88.9% 100.0%	1.3% 0.7%	4.3%	18% 55%	24.8% 36.1%	100.0%	0.07	0.00	0.01	0.01	0.02		31.2% 44.2%	28.6% 44.3%	0.9%	3.8% 0.2%	2.6%	9.4% 11.7%	31.2% 26.5%
95	N Pat	th 15	0	2	$\pm$	0.35 0.00	0.00			0.11	0.18		100.0%	0.6%	0.9%	0.6%	36.1%	48.0%	0.14	0.00	0.00	0.00	0.05		44.2%	44.8%	0.3%	0.6%	0.2%	13.3%	19.1%
96		15		- 2	+	0.26 0.00	0.00	0.0	10	0.08	0.21		100.0%	1.2% 0.7%	1.6%	2.7% 8.9%	29.2% 30.1%	82.5%	0.09	0.00	0.00	0.00	0.03	0.08	35.4% 36.2%	15.4% 14.6%	1.2%	1.2%	1.6% 7.2%	9.7% 10.3%	31.9% 36.2%
98		15	4	- 5	#	0.76 0.00	0.00	0.0	12	0.22	0.19		100.0%	0.4%	0.1%	2.1%	41.8% 46.8%	51.2% 46.2%	0.29		0.00	0.01	0.15		50.9% 54.1%	50.9%	0.4%	0.1%	1.2%	19.2%	29.1%
100		16	0	3	+		0.01	0.0	9		0.52		100.0%	1.1%	1.1%	0.3% 0.9%	35.1%	65.6%	0.39		0.01	0.01	0.12	0.26	41.5%	54.1% 41.5%	0.6%	1.0%	0.1%	22.0% 13.1%	32.8%
101		16		- 5	+	0.64 0.01	0.03	0.0	12	0.17	0.58		100.0% 100.0%	1.7% 0.5%	5.3% 0.5%	2.4%	26.8% 35.3%	91.4% 60.2%	0.18	0.01	0.03	0.01	0.06		28.9% 42.1%	28.9% 42.1%	1.1%	4.4% 0.4%	1.9%	8.6% 14.7%	27.0% 32.9%
103		16	7	5		0.75 0.00	0.00			0.35	0.32		100.0%	0.5%	0.1%	0.7%	46.5%	43.0%	0.40		0.00	0.00	0.16	0.19	53.4%	53.4%	0.4%	0.1%	0.5%	21.8%	25.2%
104		16	9	5	+	0.72 0.01	0.02	0.0		0.33	0.41		100.0%	0.5%	0.3% 3.3%	0.8% 1.7%	41.4% 31.2%	51.9% 76.2%	0.40		0.00		0.15		50.5% 34.9%	50.5% 14.9%	0.4%	0.1%	0.6%	18.7% 11.8%	29.0%
84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100 100 100 100 100 100 100 100 100		-1		2			0.00			0.14	0.29		100.0%	1.8%	2.1%	5.0% 6.2%	15.6% 14.6%	76.8% 59.5%	0.13	0.01	0.00	0.01	0.04	0.13	35.4% 37.6%	15.4% 17.6%	1.6%	0.8%	14%	11.3% 12.7%	33.8% 21.3%
108		- 5	111	- 2			0.00	0.0	2	0.12	0.16		100.0% 100.0%	15%	125	6.4%	16.8% 11.7%	54.2% 61.6%	0.14	0.00	0.00		0.04	0.06	42.0% 33.1%	42.0% 18.1%	0.9%	0.9%	165	12.6%	16.1%
110		9	135			0.35 0.01 0.28 0.01	0.00	0.0	11		0.22		100.0%	1.7%	1.1%	12%	29.6%	63.6%		0.00				0.09	38.1%	38.1%	1.8%	0.9%	4.3% 2.1%	11.7%	24.4%
111		14	4 142 5 143				0.01			0.22	0.55		100.0% 100.0%	1.7%	2.0%	10.5%	32.4% 44.4%	79.6% 56.1%	0.20	0.01	0.01	0.05	0.06		35.5% 46.4%	29.3% 46.4%	1.3%	1.7%	7.7% 2.9%	8.8% 16.9%	35.5% 22.8%
113		10	G 144	- 4		0.71 0.01	0.01	0.0	13	0.27	0.45		100.0%	1.3%	2.0%	4.4%	27.2%	63.8%	0.22	0.01	0.01	0.02	0.10	0.18	45.9%	45.9%	0.7%	1.7%	2.8%	13.5%	25.6%
114		17	7 145				0.02			0.17	0.43		100.0%	2.1%	42%	9.1% 7.6%	12.6% 19.1%	80.9% 63.8%	0.22		0.02	0.03	0.07		42.1% 45.8%	42.1% 45.8%	0.9%	3.4% 0.4%	6.4% 5.6%	11.0% 15.5%	26.6% 22.5%
116		22	2 150	4	Н	0.82 0.01	0.01	0.0		0.32	0.49		100.0%	1.0%	0.6%	12%	29.7%	59.4%	0.40	0.01	0.00	0.01	0.12	0.21	49.4%	49.4%	0.6%	0.5%	0.7%	15.3%	25.4%
112 113 114 115 116 117 118 119 120 121 122 123		21	157	10	+			0.0			1.67		100.0% 100.0%	1.9%	1.2% 0.7%	4.3% 9.1%	11.6% 11.4%	83.8% 74.2%	0.76	0.01	0.01		0.06	0.85	35.2% 37.8%	15.2% 11.5%	1.4%	1.4% 0.5%	2.6% 7.3%	9.9% 11.5%	31.6% 37.8%
119		30				1.89 0.02	0.01	0.0	15	0.80	1.05		100.0%	0.8%	0.4%	2.5% 0.5%	42.4%	55.8% 56.4%	0.90		0.01	0.03	0.36	0.61	47.6% 54.6%	47.6% 54.6%	0.6%	0.3%	1.5%	18.8% 21.4%	32.0%
121		32	2 160	10		1.72 0.02	0.02	0.0	13	0.63	1.25		100.0%	1.0%	1.0%	1.6%	36.5%	72.5%	0.00		0.02	0.02	0.28	0.63	46.2%	46.2%	0.6%	0.9%	0.9%	16.5%	16.5%
122		33		10		1.75 0.01 2.15 0.01	0.08			0.57	1.20		100.0% 100.0%	1.7% 0.6%	4.45 0.45	3.3% 7.1%	12.6% 17.8%	66.9%	0.63	0.02	0.06	0.03	0.18		36.0%	16.0% 29.1%	1.0%	3.6% 0.4%	1.9%	10.3% 14.7%	23.6%
124		25	9 167				0.01			0.95	1.06		100.0%	1.1%	0.2%	1.1%	44.2%	49.4%	1.09	0.02	0.01	0.02	0.44	0.62	50.6% 52.2%	50.6% C) 2%	0.8%	0.2%	0.8%	20.3%	28.9%
125		- 41				002				0.61	1.12		100.0% 100.0%	1.4%	0.4% 3.0%	0.8% 3.3%	29.6% 11.6%		0.65	0.02		0.01				52.2% 15.9%	0.9%	0.2% 2.5%	0.4% 1.9%	18.2% 12.0%	26.2%

# - N-patch Mid CH

																max ra	tio out of													max ratio out of all b	eams		
П		Т							4cm2 PD(r	nW/cm2	0			100.0%	1.8%	15%	10.5%	\$4.0%	100.0%	4	cm2 PD(r	nW/cm2)	at 10mm e	rvaluation	n distance		\$7.3%	\$7.2%	12%	1.0%	7.5%	24.9%	16.6%
No. 1	fodule Typ	e Sear	m ID_1	Berna ID,2	Feed no	S4(Rig	hr) 53)	Left) SS(Top	) S6(Bott	om) S1	(Front)	S2(Rear)	per Beam Back-off (dB)	ratio (Right 2mm)/(worst- surface 2mm)	ratio (Left 2mm)/(wont- surface 2mm)	ratio (Top 2mm)/(wonst- surface 2mm)	ratio (Bottom 2mm)/(wont- surface 2mm)	ratio (Fornt 2mm)/(wonst- surface 2mm)	ratio (Rear 2mm)/(wonst- surface 2mm)	S4(Right)	S3(Left)	SS(Top	SE(Bots	om) 51)	(Front) 1	S2(Rear)	ratio worst-surface (10mm/2mm)	ratio (Right 10mm)/(wont- surface 2mm)	ratio (Left 10mm)/(wonst- surface 2mm)	ratio (Top 10mm)/(wont- surface 2mm)	(Sottom (Sottom 10mm)/(worst- surface 2mm)	ratio (Front 10mm)/(wont- surface 2mm)	ratio (Rear 10mm)/(wont- surface 2mm)
64		Н	_		+	0.15	9	00 0.00	000		0.08	0.13		100.0%	1.6% 0.8%	0.0%	52% 46%	29.6% 27.4%	69.8% 53.8%	0.00	0.00	0.00	0.01	T	102	0.06	29.6% 44.1%	29.6% 44.1%	1.0%	0.0%	14%	12.5% 12.6%	28.6% 19.2%
66		⊨	5 7		1	0.22	0	00 0.00	0.01		0.07	0.13		100.0%	1.4%	0.5%	41% 12%	32.9% 35.3%	56.8% 58.8%	0.09	0.00	0.00	0.01	- 9	3.02	0.05	41.9% 42.3%	41.9% 40.3%	0.9%	0.5% 0.5%	3.2% 2.3%	10.8%	24.3% 20.4%
68			9		1	0.16	0	00 0.00			0.05	0.11		100.0%	1.3%	0.6%	1.9%	33.1%	71.2%	0.06		0.00	0.00			0.04	40.1%	40.1%	1.3%	0.6%	1.3%	8.9%	27.4%
70			14		2	0.15	0	00 0.00		-		0.29	_	100.0% 100.0%	1.4%	0.3%	10.1% 2.0%	28.1% 38.1%	83.5% 60.6%	0.12	0.00	0.00	0.03	- 6	101	0.11	35.1% 50.1%	35.1% 50.1%	12%	0.3%	7.2% 1.5%	13.4%	33.0% 26.7%
71		⊨	16		2	0.44	0	01 0.00				0.27		100.0%	1.1%	0.5%	4.8%	15.2% 14.1%	61.4% 58.6%	0.21	0.00	0.00	0.01		106	0.12	47.4% 46.5%	47.4% 46.5%	0.7% 1.0%	0.5% 0.5%	12%	13.1%	26.7% 25.8%
73		_	22		2	9.42		00 0.00	0.02		0.17	0.25		100.0% 100.0%	0.8%	0.2% 0.2%	5.1% 0.5%	36.4% 39.0%	52.9% 61.9%	0.21	0.00	0.00	0.02		3.06	0.11	44.4%	44.4%	0.4% 0.5%	0.2% 0.2%	18% 04%	12.5% 14.8%	22.4% 20.2%
75			22 23		2	0.41	0	01 0.00	0.01		0.11	0.26	-	100.0%	0.9% 1.7%	0.5%	2.9%	12.2%	63.1%	0.18	0.00	0.00	0.01	-		0.12	44.5%	51.9% 44.5%	1.0%	0.5%	2.2%	11.1%	28.7%
76			29		- 5	1.00		01 0.00			0.40	0.59		100.0%	0.7% 0.6%	0.3%	6.6% 1.8%	36.9% 36.9%	54.3% 59.7%	0.42		0.00	0.06		2.15	0.40	39.0% 47.6%	29.0% 47.6%	0.5% 0.5%	0.2% 0.2%	5.1% 1.0%	13.7% 15.2%	25.4%
78			21		5	1.46	0	01 0.00	0.01		33.0	0.06		100.0%	0.9%	0.1%	0.3%	45.1%	59.3%	0.02	0.01	0.00	0.00		1.29	0.49	56.0%	56.0%	0.7%	0.1%	0.2%	19.7%	23.5%
80			22		5	1.12		02 0.01			0.36	0.74	_	100.0%	1.4%	0.6%	0.7% 2.9%	12.3% 17.2%	66.5% 51.8%	0.52		0.01			2.14		46.5%	46.5% 44.7%	0.8%	0.4%	0.5%	12.7% 15.1%	32.7% 23.4%
81		⊨	38		5	1.15	0	01 0.00			0.41	0.66		100.0%	0.5%	0.2%	5.7%	15.9%	57.6% 63.3%	0.47	0.00	0.00	0.05	- 9	1.17	0.33	40.5% 54.2%	40.5%	0.3%	0.2%	4.1%	14.5%	28.8%
85			40		- 3	1.83		02 0.01	0.01		0.48	0.76		100.0% 100.0%	1.1% 1.5%	0.1%	0.8% 0.8%	40.3% 41.6%	66.0%	0.43		0.00	0.00	ľ	321	0.40	54.4%	54.3% 54.8%	0.8% 0.9%	0.1%	0.6%	17.1% 18.0%	34.1% 34.4% 24.6%
85			41 129		1	0.15	0	00 0.00			0.37	0.56	<del>                                     </del>	100.0% 100.0%	1.2% 0.7%	0.7%	2.5% 1.4%	35.6% 36.6%	54.6% 62.8%	0.05	0.01	0.00	0.01		3.15	0.04	41.0% 36.6%	41.0% 36.6%	0.8%	0.9%	1.4%	11.7%	29.7%
86			131		-	0.12		00 0.00				0.07		100.0%	0.8%	2.4%	2.4%	30.6% 36.5%	58.1% 41.3%	0.05		0.00	0.00			0.02	37.1% 42.1%	37.1% 42.1%	0.8%	1.6% 0.8%	1.6%	10.5% 12.7%	18.5% 14.2%
88			135		-	0.14		00 0.00	0.01		0.05	0.07		100.0%	1.4%	1.4%	15%	15.4%	50.7%	0.06	0.00	0.00	0.00			0.02	31.9%	38.9%	0.7%	0.7%	2.8%	12.5%	16.0%
90			137		2	0.12	0	00 0.00			0.04	0.08	<del>                                     </del>	100.0%	0.8%	0.8% 2.3%	2.4%	35.0% 37.3%	64.2% 69.1%	0.04		0.00		- 6	3.03	0.03	35.0%	15.0% 11.6%	0.8%	0.8%	1.6%	11.4% 11.5%	26.8% 25.5%
91		$\Box$	143		- 2	9.27		00 0.00			0.14			100.0% 100.0%	0.6%	0.3%	2.7% 1.9%	42.4% 11.0%	49.4% 57.4%	0.15		0.00	0.01		105		47.0% 40.0%	47.0% 40.0%	0.3% 0.7%	0.0% 1.5%	2.1%	15.5% 11.5%	23.8% 21.5%
93		1	145		2	0.20	0	0.01	0.01		0.06	0.20		99.5%	1.5%	1.5%	4.0%	28.2%	100.0%	0.06	0.00	0.01	0.01	-	3.02	0.06	30.7%	30.7%	1.0%	3.0%	2.5%	10.4%	28.2%
94	N Pate		149		2 2	0.30	0					0.16	_	100.0%	0.7% 0.6%	0.7%	4.7% 0.6%	41.5% 37.2%	54.5% 45.2%	0.13		0.00			105	0.06	44.5%	44.5% 45.5%	0.7% 0.6%	0.7% 0.2%	3.7% 0.3%	15.4% 11.6%	21.4% 18.2%
96			151		2	0.20	0	00 0.00			0.09	0.17		100.0%	1.2% 0.6%	1.2%	2.0% 8.4%	36.1% 35.8%	65.1% 56.9%	0.10		0.00	0.00		101	0.07	37.3% 35.7%	17.1% 15.7%	0.8%	1.2% 0.3%	1.6%	11.8% 12.7%	27.1% 28.2%
98			158		5	0.75	9	00.00	0.02		0.33	0.37		100.0%	0.5%	0.1%	2.0%	44.0%	49.1%	0.29	0.00	0.00	0.01	- 0	2.15		51.9%	51.9%	0.4%	0.1%	1.2%	20.2%	27.5%
100			159		5	0.75	0	01 0.00			0.37	0.33	-	100.0%	1.1%	0.1%	0.3%	48.8% 37.5%	44.3% 57.4%	0.42		0.00	0.00		117		55.4%	55.4% 41.1%	0.8%	0.1%	0.1%	23.1%	24.5% 30.6%
101			161		- 3	8.63		00 0.00			0.21	0.42		100.0%	1.5% 0.5%	3.4% 0.3%	1.6%	33.3%	68.0% 55.1%	0.19		0.02			106		32.7% 42.0%	30.7% 42.0%	1.0%	2.9% 0.3%	1.1%	15.4%	24.7% 29.7%
103			167		5	0.00	0	01 0.00	0.01		0.39	0.34		100.0%	0.6%	0.1%	0.6%	48.9%	42.4%	0.43	0.00	0.00	0.00		2.18	0.19	54.3%	54.3%	0.5%	0.1%	0.5%	22.7%	24.1%
65 66 67 77 77 78 80 80 80 80 80 80 80 80 80 80 80 80 80			168		5 5	0.78	0	01 0.00				0.38	├	100.0%	0.8% 1.5%	0.3%	0.8% 1.2%	44.0% 35.1%	48.9% 61.7%	0.41		0.00	0.00		109	0.19	52.4% 36.5%	52.4% 16.5%	0.5%	0.1%	0.5%	20.0% 12.1%	27.3% 28.1%
106		$\vdash$	1	129	2	0.37	0	01 0.00				0.28		100.0%	1.4%	0.5%	4.9% 6.4%	47.0% 29.2%	76.2% 57.9%	0.14		0.00	0.01	- 9	106	0.12	37.2% 40.5%	37.2% 26.0%	1.1% 0.8%	0.5% 1.0%	3.3% 4.6%	15.3%	33.6% 21.3%
108		$\vdash$	Š	122	2	0.41	0	01 0.00	0.03		0.16	0.21		100.0%	1.5%	1.0%	6.4%	40.4%	51.2%	0.17	0.00	0.00	0.02	-	106	0.08	41.4%	41.4%	1.0%	0.7%	4.7%	14.2%	19.7%
109		$\vdash$		135	- 2	0.45	0	01 0.01 00 0.00			0.17	0.21	-	100.0%	1.0%	1.1%	45%	38.8% 32.7%	47.7% 60.3%	0.17		0.00			106		38.5% 37.3%	18.5% 17.1%	0.9%	0.9%	11%	12.2% 9.7%	18.9% 22.7%
111			14	142	4	0.72		0.01	0.00			0.56		100.0%	1.3%	1.1%	10.5% 1.7%	37.7% 48.1%	77.7% 50.5%	0.22		0.01	0.05		107	0.26	36.6%	30.6% 40.7%	1.0%	1.0%	7.5%	10.3%	36.6% 22.8%
113			16	144	- 4	0.80	0	01 0.01	0.04		0.30	0.47		100.0%	1.0%	1.4%	5.3%	27.3%	58.0%	0.20	0.01	0.01	0.03	- 0	2.11	0.20	47.4%	47.4%	0.7%	1.0%	3.6%	14.1%	24.6%
114			17	145	4							0.45	⊢=	100.0%	1.5%	2.3%	9.5% 7.8%	33.0% 50.1%	73.2% 55.9%	0.27		0.01	0.04			0.18	44.0%	44.0% 49.2%	1.0%	2.0% 0.4%	6.7% 5.7%	13.6% 18.4%	29.2% 20.8%
116		$\vdash$		150	4		0	01 0.00	0.01		0.45	0.50		100.0%	0.9%	0.4%	0.7%	45.0%	50.3%	0.50	0.01	0.00	0.00		2.17	0.23	50.6%	50.6%	0.7%	0.2%	0.4%	17.2%	22.9%
117		$\vdash$	29	151	10	2.44	0	02 0.01	0.15		1.04	1.41		100.0% 100.0%	1.8% 0.6%	1.1%	3.3% 8.0%	39.6% 42.5%	62.2% 58.0%	0.31	0.01	0.01	0.02		2.27	0.20	42.9% 35.8%	42.9% 35.8%	1.3%	1.0% 0.2%	2.2% 6.1%	11.9% 15.3%	27.1%
119		F	35	158	10		0	0.01	0.05		1.66			100.0% 100.0%	0.7%	0.3%	2.0%	45.9% 54.0%	49.1% 52.1%	1.12		0.01			162	0.66		48.5% 57.3%	0.5% 1.2%	0.2%	12%	20.1% 24.9%	28.5%
121		$\vdash$	32	160	10	1.91	0	0.02	0.02		0.73	1.30		100.0%	1.2%	0.9%	0.8%	38.3%	67.7%	0.92	0.01	0.01	0.01	-	2.21	0.70	41.3%	48.3%	0.7%	0.7%	0.6%	16.3%	36.5%
122		$\vdash$	38	161	10	2.41		01 0.05			1.06	1.15	├	100.0%	1.4% 0.5%	2.5%	2.6% 5.9%	38.0% 43.9%	62.9% 55.6%	0.68		0.04	0.03		1.27	0.50	37.2%	17.2% 19.0%	1.0%	2.1% 0.2%	15%	14.4% 17.8%	27.0% 30.2%
124			39 40	167	10		0	03 0.00	0.03		1.34	1.39		100.0%	1.3%	0.2%	1.0%	50.7% 45.0%	52.7%	1.41		0.00	0.02			0.76	51.2%	53.3%	1.0%	0.1%	0.7%	22.2%	28.8%
125				168	10			02 0.03				1.10	_	100.0%	1.8%	0.3% 1.7%	2.1%	45.0% 38.3%	57.1% 62.1%	0.71	0.02	0.01	0.01				54.1% 37.5%	54.1% 37.5%	1.1% 0.7%	0.2% 1.4%	0.5%	20.5% 15.6%	32.2% 29.8%

# - N-patch High CH

											max ratio out of							max ratio out of all beams											
П		Т	4cm2 PD(mW/cm2)							1.00	380				4cm2 PD(mW/cm2) at 10mm evaluation distance					ance		F7.00			T	22.00			
No. I	Wodule Typ	e Seam ID.	Sens D.J	Feed no.		1	Т	Т	Т	per	ratio	ratio	ratio	ratio	ratio	95.6% ratio		T				T	ratio	ratio	ratio	ratio	natio (Sottom	ratio	ratio
					S4(Right) S3(Let	t) SS(Top	S6(Botto	m) S1(Fro	s2/Res	e) Back-off	(Right 2mm)/(worst- surface 2mm)	(Left 2mm)/(wont- surface 2mm)	(Top 2mm)/(wont- surface 2mm)	(Sottom 2mm)/(worst- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(worst- surface 2mm)	54(Right	(fa.1,62	SS(Top)	SE(Bottom)	S1/Front	S2(Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(wont- surface 2mm)	(Left 10mm)/(wont- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	10mm)/(worst- surface 2mm)	(Front 10mm)/(wonst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
64		-					0.01		0.13		100.0% 100.0%	0.9%	0.5%	185	19.1% 11.0%			0.00		0.01	0.03	0.05	41.25	41.2% 46.3%	0.9%	0.0%	2.4% 3.3%	14.2% 11.5%	24.2% 20.0%
66		5 7		1	0.24 0.00	0.00		0.00	0.13		100.0%	0.8%	0.4%	3.8%	32.2% 36.4%	54.0% 55.6%	0.10	0.00	0.00	0.01	0.02		42.7%	42.7% 43.1%	0.4%	0.4%	2.9%	9.6%	24.3% 18.0%
60		9	_	-	0.16 0.00	0.00	0.00	0.04	0.12		100.0%	1.3%	1.3%	1.9%	27.6%	79.5%	0.00	0.00	0.00	0.00	0.01		41.1%	48.1%	0.6%	0.6%	1.3%	7.7%	27.6%
69		14		2		0.00		0.00	0.31	_	100.0% 100.0%	1.1% 0.7%	0.3%	8.7% 2.1%	22.8% 40.4%	87.6% 56.9%	0.13	0.00	0.00	0.02	0.03	0.12	35.1% 52.3%	35.1% 52.3%	0.8% 0.4%	0.2%	6.5%	7.3% 14.5%	34.8% 26.2%
71		16		2		0.00	0.02	0.16	0.29		100.0%	1.0%	0.4%	4.0%	21.9%	58.8%	0.23		0.00	0.02	0.06		47.0% 46.2%	47.0%	0.6%	0.4%	1.0%	12.0%	25.2%
65 66 67 68 69 70 71 72 73		21		2	0.51 0.00	0.00	0.02	0.17	0.26		100.0% 100.0%	0.9%	0.2%	62% 47%	12.4% 11.9%	52.1%	0.22	0.00		0.02	0.06	0.11	43.4%	46.2% 43.4%	0.7% 0.4%	0.4%	4.7% 3.7%	12.4% 11.6%	23.3% 21.3%
74		22		2	0.60 0.01	0.00	0.00	0.15	0.36		100.0%	0.8% 1.4%	0.2%	0.7% 2.7%	12.9% 11.1%	62.4% 59.1%	0.32	0.00	0.00	0.00	0.07	0.18	53.0% 45.0%	\$1.0% 45.0%	0.5%	0.2%	0.5% 2.1%	11.8%	30.5% 26.9%
75 76 77 78 79 80 81 82 83 84 85		29 30		5	1.04 0.01		0.08	0.38	0.65		100.0% 100.0%	1.1% 0.5%	0.3%	7.6% 1.3%	15.9% 41.0%	62.0% 52.5%	0.45	0.01	0.00	0.06	0.13		43.0% 50.5%	43.0% 50.5%	0.7% 0.4%	0.3%	6.1%	12.7% 16.7%	28.7% 26.9%
		21		5	1.50 0.01	0.00	0.00	0.61	0.96		100.0%	0.9%	0.1%	0.3%	38.8%	60.4%	0.90		0.00	0.00	0.27	0.55	56.6%	56.6%	0.6%	0.1%	0.2%	17.1%	24.2%
		32 33	_	5	1.11 0.01	0.01	0.01	0.39	0.68		100.0%	1.0%	1.2%	0.5% 2.4%	15.2% 16.2%	61.2% 54.2%	0.52	0.01	0.01	0.00	0.16		47.1% 47.8%	47.1% 47.8%	0.5%	0.5%	0.4%	14.0%	30.7% 26.5%
		38 29		- 5	1.19 0.01	0.00	0.07	0.45	0.68		100.0%	0.8% 0.7%	0.3%	5.5% 0.5%	17.8% 16.4%			0.01			0.17		44.85	44.8% 54.3%	0.4% 0.5%	0.2%	4.4%	14.4%	26.8% 34.5%
		40	_	- 5	1.35 0.02	0.00	0.00	0.53			100.0%	1.2%	0.3%	0.3%	39.6% 16.1%	61.2%		0.01		0.00		0.46	53.1% 45.6%	55.1% 45.6%	0.8%	0.2%	0.2%	18.6%	34.3% 34.3%
		129	+	1	0.15 0.00	0.00	0.00	0.00	0.10	_	100.0%	0.6%	1.3%	1.3%	36.4%	61.7%	0.06	0.00	0.00	0.00	0.02	0.04	37.0%	37.0%	0.6%	1.3%	1.3%	12.3%	27.3%
86		131		-		0.00					100.0%	0.7%	2.2%	1.5% 2.8%	12.6% 14.0%	57.8% 19.0%	0.05	0.00	0.00	0.00	0.02		38.5% 42.4%	38.5% 40.4%	0.7% 0.7%	2.2%	15%	11.1% 11.3%	17.0% 13.5%
88		135				0.00					100.0%	0.6%	0.6%	2.6%	16.4% 17.8%	50.0% 57.8%	0.06	0.00	0.00	0.00	0.02		39.0% 17.8%	29.0% 27.8%	0.6%	0.6%	1.9%	11.0%	16.9%
90		142		2	0.14 0.00	0.00	0.01	0.09	0.15		100.0%	1.4%	3.8%	22% 18%	41.3%	70.7%	0.07	0.00	0.01	0.00	0.02	0.06	35.1%	35.1%	1.0%	0.7% 3.4%	2.4%	11.0%	20.8%
85 86 87 88 89 90 91 92		143	+	2 2	0.35 0.00	0.00	0.01	0.16	0.16	+	100.0%	0.6%	1.75	2.6% 1.7%	44.3% 16.2%	46.6% 53.4%		0.00	0.00	0.01	0.06		40.25	48.0% 40.1%	0.6%	0.3%	13%	17.0%	22.2%
93		145		2		0.01		0.06			100.0% 100.0%	1.8%	4.45	2.6% 1.9%	27.8% 40.2%	95.6% 51.8%		0.00	0.01	0.00	0.02		29.1%	29.1% 45.0%	0.9%	1.5% 0.6%	1.8%	10.1% 15.1%	26.0%
95	N Pate	h 150		2	0.38 0.00	0.00	0.00	0.15	0.17		100.0%	0.8%	0.5%	0.5%	40.3%	43.5%	0.18		0.00	0.00	0.06	0.07	46.6%	46.6%	0.5%	0.3%	0.3%	14.9%	18.2%
96		151		5		0.00		0.10	0.14	_	100.0%	1.2% 0.4%	1.2% 0.4%	1.9% 7.3%	40.5%	54.1% 49.0%	0.11	0.00	0.00	0.00	0.04		41.2% 37.4%	41.2% 37.4%	0.8%	1.2% 0.4%	1.6%	11.6% 11.7%	25.2% 25.8%
98		158		5		0.00	0.01	0.36		_	100.0%	0.8% 1.4%	0.3%	1.8%	44.8% 50.2%	46.5% 43.0%	0.42		0.00		0.17		53.0%	\$1.0% \$6.1%	0.6% 1.1%	0.1%	1.1%	20.8% 23.8%	25.2% 23.7%
100		160		- 3			0.01		0.42		100.0%	0.8%	1.1%	0.7% 1.3%	19.6% 15.8%	55.6% 62.5%		0.00	0.01			0.22		44.4% 11.8%	0.4%	0.9%	0.4%	16.8%	28.9%
102		166		- 5	0.81 0.00	0.00	0.04	0.32	0.42		100.0%	0.5%	0.2%	5.3%	29.8%	52.0%	0.35	0.00	0.00	0.03	0.13	0.23	41.2%	41.2%	0.4%	0.2%	3.7%	16.4%	28.4%
103		167	-	5		0.00		0.42			100.0%	0.7%	0.1%	0.7%	48.6% 45.5%	42.3% 48.9%		0.01	0.00	0.00	0.20		55.2% 51.7%	55.2% 51.7%	0.6%	0.1%	0.5%	22.9%	22.4%
95 96 97 98 99 100 101 102 103 104 105 106 107		169	130	5	0.72 0.01	0.02	0.01	0.27	0.42		100.0% 100.0%	1.0%	2.2%	1.0%	16.7% 48.1%	57.8% 66.8%	0.27	0.00	0.01	0.01	0.10	0.19	37.4%	37.4% 39.2%	0.6%	1.9%	0.7% 2.5%	14.1%	26.1%
107		- 3	131	2	0.46 0.01	0.01	0.02	0.17	0.27		100.0%	1.2%	1.1%	4.0%	16.7%	59.6%	0.20	0.00	0.00	0.02	0.06	0.09	41.1%	42.1%	0.7%	0.9%	1.7%	11.2%	19.8%
109		- 5	135			0.01			0.20	+	100.0%	1.0%	1.1%	5.4% 4.0%	36.2% 40.7%		0.19		0.00		0.07	0.09	40.1%	40.0% 40.1%	0.7% 0.6%	0.7% 0.6%	4.2% 2.9%	11.6% 14.8%	19.2% 17.7%
110		14	137	2		0.00					100.0%	1.3%	1.6%	1.0%	21.8% 26.4%	55.1% 76.0%		0.00	0.00	0.01	0.04	0.08	41.5% 36.0%	41.5% 31.0%	1.0%	0.5% 1.3%	1.3%	9.7%	21.0% 36.0%
112		15	143	- 4	1.03 0.01	0.00	0.03	0.55	0.51		100.0%	0.8%	0.4%	10%	51.2% 40.8%	49.3% 55.2%	0.54	0.01	0.00	0.03	0.21	0.24	52.4% 44.2%	52.4% 44.2%	0.5%	0.3%	2.4%	20.4%	23.6% 22.4%
113		17	145	1 4	0.21 0.01			0.21	0.50		100.0%	1.6%	2.0%	7.2%	29.5%	70.6%	0.30	0.01	0.01	0.04	0.09	0.19	42.1%	42.1%	0.9%	2.0%	5.4%	12.6%	26.5%
115		21	149	4	0.85 0.01 1.11 0.01	0.00	0.01	0.35	0.44	+ =	100.0%	0.7% 0.7%	0.6%	7.7%	46.0% 45.1%	52.0% 51.4%	0.41	0.00	0.00	0.05	0.15		41.1%	48.1% 51.3%	0.5%	0.5%	5.9%	18.0% 16.9%	21.8% 25.6%
115 116 117		23	151	4		0.01	0.02	0.32	0.44		100.0%	1.5%	0.9%	11%	43.1% 43.3%	59.2%	0.22		0.01		0.12		44.7%	44.7% 38.0%	0.8%	0.8%	2.1%	15.7% 15.2%	27.6% 27.2%
119		30	158	10	2.51 0.02	0.01	0.04	1.27	1.22	-	100.0%	0.7%	0.2%	15%	50.5%	48.5%	1.26	0.01	0.00	0.02	0.56	0.62	50.0%	50.0% 57.6%	0.5%	0.2%	1.0%	22.4%	24.5%
120 121 122 123 124 125		31	159	10	1.92 0.02	0.02		0.83	1.22	_	100.0%	1.3% 1.1%	0.1% 1.0%	0.5%	50.8% 43.1%	51.2% 63.1%	0.93		0.02	0.01	0.34		57.9% 48.3%	48.3%	1.0% 0.6%	0.1% 0.8%	0.4%	23.8% 17.5%	31.1% 34.5%
		33	161 166	10		0.05					100.0%	1.3% 0.6%	2.4%	2.4%	29.8% 47.0%	57.5% 49.2%	0.73		0.04		0.27		38.4% 41.9%	38.4% 41.9%	0.9%	1.9%	1.4%	13.9% 18.3%	26.6% 26.9%
		29	167	10	2.89 0.03	0.00	0.02	1.40	1.51		100.0%	1.0%	0.1%	0.8%	41.4%	52.3%	1.52	0.02	0.00	0.02	0.64	0.83	52.6%	52.6%	0.8%	0.1%	0.6%	22.3%	28.5%
		40	160	10	2.43 0.04 1.97 0.02	0.01				+	100.0%	1.5%	1.7%	0.5%	45.6% 41.3%	57.9% 57.7%			0.00	0.01	0.52		42.4%	55.2% 40.4%	1.0%	0.2% 1.4%	0.4%	21.5% 15.5%	31.9% 28.7%