Calibration Laboratory of<br>Schmid \& Partner<br>Engineering AG<br>Zeughausstrasse 43, 8004 Zurich, Switzerland

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Swiss Calibration Service

## CALIBRATION CERTIFICATE

| Object | D2600V2-SN:1103 |  |  |
| :---: | :---: | :---: | :---: |
| Calibration procedure(s) | QA CAL-05.v9 <br> Calibration procedure for dipole validation kits above 700 MHz |  |  |
| Calibration date: | February 16, 20 |  |  |
| This calibration certificate documents the traceability to national standards, which realize the physical units of measurements (SI). The measurements and the uncertainties with confidence probability are given on the following pages and are part of the certificate. |  |  |  |
| All calibrations have been conducted in the closed laboratory facility: environment temperature (22 $\pm 3)^{\circ} \mathrm{C}$ and humidity $<70 \%$. |  |  |  |
| Calibration Equipment used (M\&TE critical for calibration) |  |  |  |
| Primary Standards | ID \# | Cal Date (Certificate No.) | Scheduled |
| Power meter NRP | SN: 104778 | 04-Apr-17 (No. 217-02521/02522) | Apr-18 |
| Power sensor NRP-Z91 | SN: 103244 | 04-Apr-17 (No. 217-02521) | Apr-18 |
| Power sensor NRP-Z91 | SN: 103245 | 04-Apr-17 (No. 217-02522) | Apr-18 |
| Reference 20 dB Attenuator | SN: 5058 (20k) | 07-Apr-17 (No. 217-02528) | Apr-18 |
| Type-N mismatch combination | SN: 5047,2 / 06327 | 07-Apr-17 (No. 217-02529) | Apr-18 |
| Reference Proba EX3DV4 | SN: 7349 | 30-Dec-17 (No. EX3-7349_Dec17) | Dec-18 |
| DAE4 | SN: 601 | 26-Oct-17 (No. DAE4-601_Oct17) | Oct-18 |
| Secondary Standards | ID \# | Check Date (in house) | Scheduled |
| Power meter EPM-442A | SN: GB37480704 | 07-Oct-15 (in house check Oct-16) | In house |
| Power sensor HP 8481A | SN: US37292783 | 07-Oct-15 (in house check Oct-16) | In house |
| Power sensor HP 8481A | SN: MY41092317 | 07-Oct-15 (in house check Oct-16) | In house |
| RF generator R\&S SMT-06 | SN: 100972 | 15-Jun-15 (in house check Oct-16) | In house |
| Network Analyzer HP 8753E | SN: US37390585 | 18-Oct-01 (in house check Oct-17) | In house |
|  | Name | Function | Signature |
| Calibrated by: | Michael Weber | Laboratory Technician |  |
| Approved by: | Katja Pokovic | Technical Manager | ) |
| This calibration certificate shall | be reproduced except | ull without written approval of the lab |  |

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Accredited by the Swiss Accreditation Service (SAS)


Accreditation No.: SCS 0108

The Swiss Accreditation Service is one of the signatories to the EA Multilateral Agreement for the recognition of calibration certificates

## Glossary:

TSL tissue simulating liquid
ConvF sensitivity in TSL / NORM $x, y, z$
N/A not applicable or not measured
Calibration is Performed According to the Following Standards:
a) IEEE Std 1528-2013, "IEEE Recommended Practice for Determining the Peak SpatialAveraged Specific Absorption Rate (SAR) in the Human Head from Wireless Communications Devices: Measurement Techniques", June 2013
b) IEC 62209-1, "Measurement procedure for the assessment of Specific Absorption Rate (SAR) from hand-held and body-mounted devices used next to the ear (frequency range of 300 MHz to 6 GHz )", July 2016
c) IEC 62209-2, "Procedure to determine the Specific Absorption Rate (SAR) for wireless communication devices used in close proximity to the human body (frequency range of 30 MHz to 6 GHz )", March 2010
d) KDB 865664 , "SAR Measurement Requirements for 100 MHz to 6 GHz "

## Additional Documentation:

e) DASY4/5 System Handbook

## Methods Applied and Interpretation of Parameters:

- Measurement Conditions: Further details are available from the Validation Report at the end of the certificate. All figures stated in the certificate are valid at the frequency indicated.
- Antenna Parameters with TSL: The dipole is mounted with the spacer to position its feed point exactly below the center marking of the flat phantom section, with the arms oriented parallel to the body axis.
- Feed Point Impedance and Return Loss: These parameters are measured with the dipole positioned under the liquid filled phantom. The impedance stated is transformed from the measurement at the SMA connector to the feed point. The Return Loss ensures low reflected power. No uncertainty required.
- Electrical Delay: One-way delay between the SMA connector and the antenna feed point. No uncertainty required.
- SAR measured: SAR measured at the stated antenna input power.
- SAR normalized: SAR as measured, normalized to an input power of 1 W at the antenna connector.
- SAR for nominal TSL parameters: The measured TSL parameters are used to calculate the nominal SAR result.

The reported uncertainty of measurement is stated as the standard uncertainty of measurement multiplied by the coverage factor $\mathrm{k}=2$, which for a normal distribution corresponds to a coverage probability of approximately $95 \%$.

## Measurement Conditions

DASY system configuration, as far as not given on page 1 .

| DASY Version | DASY5 | V52.10.0 |
| :--- | :---: | :---: |
| Extrapolation | Advanced Extrapolation |  |
| Phantom | Modular Flat Phantom |  |
| Distance Dipole Center - TSL | 10 mm | with Spacer |
| Zoom Scan Resolution | $\mathrm{dx}, \mathrm{dy}, \mathrm{dz}=5 \mathrm{~mm}$ |  |
| Frequency | $2600 \mathrm{MHz} \pm 1 \mathrm{MHz}$ |  |

## Head TSL parameters

The following parameters and calculations were applied.

|  | Temperature | Permittivity | Conductivity |
| :--- | :---: | :---: | :---: |
| Nominal Head TSL parameters | $22.0^{\circ} \mathrm{C}$ | 39.0 | $1.96 \mathrm{mho} / \mathrm{m}$ |
| Measured Head TSL parameters | $(22.0 \pm 0.2)^{\circ} \mathrm{C}$ | $37.3 \pm 6 \%$ | $2.04 \mathrm{mho} / \mathrm{m} \pm 6 \%$ |
| Head TSL temperature change during test | $<0.5^{\circ} \mathrm{C}$ | ---- | ---- |

## SAR result with Head TSL

| SAR averaged over $1 \mathrm{~cm}^{3}(1 \mathrm{~g})$ of Head TSL | Condition |  |
| :--- | :---: | :---: |
| SAR measured | 250 mW input power | $14.5 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Head TSL parameters | normalized to 1 W | $\mathbf{5 6 . 4} \mathrm{~W} / \mathrm{kg} \pm 17.0 \%(\mathbf{k}=2)$ |


| SAR averaged over $10 \mathrm{~cm}^{\mathbf{3}}(\mathbf{1 0} \mathbf{~ g})$ of Head TSL | condition |  |
| :--- | :---: | :---: |
| SAR measured | 250 mW input power | $6.45 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Head TSL parameters | normalized to 1 W | $\mathbf{2 5 . 4} \mathbf{W} / \mathrm{kg} \pm \mathbf{1 6 . 5} \%(\mathbf{k}=\mathbf{2})$ |

## Body TSL parameters

The following parameters and calculations were applied.

|  | Temperature | Permittivity | Conductivity |
| :--- | :---: | :---: | :---: |
| Nominal Body TSL parameters | $22.0^{\circ} \mathrm{C}$ | 52.5 | $2.16 \mathrm{mho} / \mathrm{m}$ |
| Measured Body TSL parameters | $(22.0 \pm 0.2)^{\circ} \mathrm{C}$ | $51.0 \pm 6 \%$ | $2.22 \mathrm{mho} / \mathrm{m} \pm 6 \%$ |
| Body TSL temperature change during test | $<0.5^{\circ} \mathrm{C}$ | ---- | ---- |

## SAR result with Body TSL

| SAR averaged over $\mathbf{1} \mathrm{cm}^{\mathbf{3}} \mathbf{( 1 \mathrm { g } ) \text { of Body TSL }}$ | Condition |  |
| :--- | :---: | :---: |
| SAR measured | 250 mW input power | $14.2 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Body TSL parameters | normalized to 1 W | $\mathbf{5 5 . 7} \mathbf{W} / \mathbf{k g} \pm \mathbf{1 7 . 0} \%(\mathbf{k}=\mathbf{2})$ |


| SAR averaged over $10 \mathrm{~cm}^{3}(\mathbf{1 0} \mathbf{g})$ of Body TSL | condition |  |
| :--- | :---: | :---: |
| SAR measured | 250 mW input power | $6.29 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Body TSL parameters | normalized to 1 W | $\mathbf{2 4 . 9 \mathrm { W } / \mathrm { kg } \pm 1 6 . 5 \% ( \mathbf { k } = \mathbf { 2 } )}$ |

## Appendix (Additional assessments outside the scope of SCS 0108)

## Antenna Parameters with Head TSL

| Impedance, transformed to feed point | $49.1 \Omega-6.6 \mathrm{j} \Omega$ |
| :--- | :---: |
| Return Loss | -23.5 dB |

## Antenna Parameters with Body TSL

| Impedance, transformed to feed point | $45.9 \Omega-4.1 \mathrm{j} \Omega$ |
| :--- | :---: |
| Return Loss | -24.4 dB |

## General Antenna Parameters and Design

| Electrical Delay (one direction) | 1.147 ns |
| :--- | :--- |

After long term use with 100 W radiated power, only a slight warming of the dipole near the feedpoint can be measured.
The dipole is made of standard semirigid coaxial cable. The center conductor of the feeding line is directly connected to the second arm of the dipole. The antenna is therefore short-circuited for DC-signals. On some of the dipoles, small end caps are added to the dipole arms in order to improve matching when loaded according to the position as explained in the "Measurement Conditions" paragraph. The SAR data are not affected by this change. The overall dipole length is still according to the Standard.
No excessive force must be applied to the dipole arms, because they might bend or the soldered connections near the feedpoint may be damaged.

## Additional EUT Data

| Manufactured by | SPEAG |
| :--- | :---: |
| Manufactured on | January 13, 2015 |

## DASY5 Validation Report for Head TSL

Date: 16.02.2018
Test Laboratory: SPEAG, Zurich, Switzerland
DUT: Dipole 2600 MHz ; Type: D2600V2; Serial: D2600V2 - SN: 1103
Communication System: UID 0-CW; Frequency: 2600 MHz
Medium parameters used: $\mathrm{f}=2600 \mathrm{MHz} ; \sigma=2.04 \mathrm{~S} / \mathrm{m} ; \varepsilon_{\mathrm{r}}=37.3 ; \rho=1000 \mathrm{~kg} / \mathrm{m}^{3}$
Phantom section: Flat Section
Measurement Standard: DASY5 (IEEE/IEC/ANSI C63.19-2011)
DASY52 Configuration:

- Probe: EX3DV4 - SN7349; ConvF(7.7, 7.7, 7.7); Calibrated: 30.12.2017;
- Sensor-Surface: 1.4 mm (Mechanical Surface Detection)
- Electronics: DAE4 Sn601; Calibrated: 26.10.2017
- Phantom: Flat Phantom 5.0 (front); Type: QD 000 P50 AA; Serial; 1001
- DASY52 52.10.0(1446); SEMCAD X 14.6.10(7417)

Dipole Calibration for Head Tissue/Pin $=\mathbf{2 5 0} \mathbf{~ m W}, \mathrm{d}=10 \mathrm{~mm} /$ Zoom Scan ( $7 \times 7 \times 7$ )/Cube 0:
Measurement grid: $d x=5 \mathrm{~mm}, \mathrm{dy}=5 \mathrm{~mm}, \mathrm{dz}=5 \mathrm{~mm}$
Reference Value $=116.0 \mathrm{~V} / \mathrm{m}$; Power Drift $=-0.09 \mathrm{~dB}$
Peak SAR (extrapolated) $=29.2 \mathrm{~W} / \mathrm{kg}$
$\operatorname{SAR}(1 \mathrm{~g})=14.5 \mathrm{~W} / \mathrm{kg} ; \operatorname{SAR}(10 \mathrm{~g})=6.45 \mathrm{~W} / \mathrm{kg}$
Maximum value of SAR (measured) $=23.2 \mathrm{~W} / \mathrm{kg}$


## Impedance Measurement Plot for Head TSL



## DASY5 Validation Report for Body TSL

Date: 16.02 .2018
Test Laboratory: SPEAG, Zurich, Switzerland
DUT: Dipole 2600 MHz ; Type: D2600V2; Serial: D2600V2 - SN: 1103
Communication System: UID 0 - CW; Frequency: 2600 MHz
Medium parameters used: $\mathrm{f}=2600 \mathrm{MHz} ; \sigma=2.22 \mathrm{~S} / \mathrm{m} ; \varepsilon_{\mathrm{r}}=51 ; \rho=1000 \mathrm{~kg} / \mathrm{m}^{3}$
Phantom section: Flat Section
Measurement Standard: DASY5 (IEEE/IEC/ANSI C63.19-2011)
DASY52 Configuration:

- Probe: EX3DV4 - SN7349; ConvF(7.81, 7.81, 7.81); Calibrated: 30.12.2017;
- Sensor-Surface: 1.4 mm (Mechanical Surface Detection)
- Electronics: DAE4 Sn601; Calibrated: 26.10.2017
- Phantom: Flat Phantom 5.0 (back); Type: QD 000 P50 AA; Serial: 1002
- DASY52 52.10.0(1446); SEMCAD X 14.6.10(7417)

Dipole Calibration for Body Tissue/Pin=250 mW, d=10mm/Zoom Scan (7x7x7)/Cube 0:
Measurement grid: $\mathrm{dx}=5 \mathrm{~mm}, \mathrm{dy}=5 \mathrm{~mm}, \mathrm{dz}=5 \mathrm{~mm}$
Reference Value $=105.4 \mathrm{~V} / \mathrm{m}$; Power Drift $=-0.07 \mathrm{~dB}$
Peak SAR $($ extrapolated $)=29.7 \mathrm{~W} / \mathrm{kg}$
$\operatorname{SAR}(1 \mathrm{~g})=14.2 \mathrm{~W} / \mathrm{kg} ; \operatorname{SAR}(10 \mathrm{~g})=6.29 \mathrm{~W} / \mathrm{kg}$
Maximum value of SAR $($ measured $)=23.1 \mathrm{~W} / \mathrm{kg}$


## Impedance Measurement Plot for Body TSL




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## Glossary:

TSL
ConvF sensitivity in TSL / NORM $x, y, z$
N/A not applicable or not measured


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C Service suisse d'étalonnage
Servizio svizzero di taratura
S Swiss Calibration Service

Accreditation No.: SCS 0108

## Calibration is Performed According to the Following Standards:

a) IEEE Std 1528-2013, "IEEE Recommended Practice for Determining the Peak SpatialAveraged Specific Absorption Rate (SAR) in the Human Head from Wireless Communications Devices: Measurement Techniques", June 2013
b) IEC 62209-1, "Measurement procedure for the assessment of Specific Absorption Rate (SAR) from hand-held and body-mounted devices used next to the ear (frequency range of 300 MHz to 6 GHz )", July 2016
c) IEC 62209-2, "Procedure to determine the Specific Absorption Rate (SAR) for wireless communication devices used in close proximity to the human body (frequency range of 30 MHz to 6 GHz )", March 2010
d) KDB 865664, "SAR Measurement Requirements for 100 MHz to 6 GHz "

## Additional Documentation:

e) DASY4/5 System Handbook

## Methods Applied and Interpretation of Parameters:

- Measurement Conditions: Further details are available from the Validation Report at the end of the certificate. All figures stated in the certificate are valid at the frequency indicated.
- Antenna Parameters with TSL: The dipole is mounted with the spacer to position its feed point exactly below the center marking of the flat phantom section, with the arms oriented parallel to the body axis.
- Feed Point Impedance and Return Loss: These parameters are measured with the dipole positioned under the liquid filled phantom. The impedance stated is transformed from the measurement at the SMA connector to the feed point. The Return Loss ensures low reflected power. No uncertainty required.
- Electrical Delay: One-way delay between the SMA connector and the antenna feed point. No uncertainty required.
- SAR measured: SAR measured at the stated antenna input power.
- SAR normalized: SAR as measured, normalized to an input power of 1 W at the antenna connector.
- SAR for nominal TSL parameters: The measured TSL parameters are used to calculate the nominal SAR result.
The reported uncertainty of measurement is stated as the standard uncertainty of measurement multiplied by the coverage factor $\mathrm{k}=2$, which for a normal distribution corresponds to a coverage probability of approximately $95 \%$.


## Measurement Conditions

DASY system configuration, as far as not given on page 1.

| DASY Version | DASY5 | V52.10.0 |
| :--- | :---: | :---: |
| Extrapolation | Advanced Extrapolation |  |
| Phantom | Modular Flat Phantom V5.0 |  |
| Distance Dipole Center - TSL | 10 mm | with Spacer |
| Zoom Scan Resolution | $\mathrm{dx}, \mathrm{dy}=4.0 \mathrm{~mm}, \mathrm{dz}=1.4 \mathrm{~mm}$ | Graded Ratio $=1.4$ (Z direction) |
|  | $5200 \mathrm{MHz} \pm 1 \mathrm{MHz}$ |  |
| Frequency | $5300 \mathrm{MHz} \pm 1 \mathrm{MHz}$ |  |
|  | $5560 \mathrm{MHz} \pm 1 \mathrm{MHz}$ |  |
|  | $5600 \mathrm{MHz} \pm 1 \mathrm{MHz}$ |  |

## Head TSL parameters at 5200 MHz

The following parameters and calculations were applied.

|  | Temperature | Permittivity | Conductivity |
| :--- | :---: | :---: | :---: |
| Nominal Head TSL parameters | $22.0^{\circ} \mathrm{C}$ | 36.0 | $4.66 \mathrm{mho} / \mathrm{m}$ |
| Measured Head TSL parameters | $(22.0 \pm 0.2)^{\circ} \mathrm{C}$ | $36.4 \pm 6 \%$ | $4.53 \mathrm{mho} / \mathrm{m} \pm 6 \%$ |
| Head TSL temperature change during test | $<0.5^{\circ} \mathrm{C}$ | ---- | --- |

## SAR result with Head TSL at 5200 MHz

| SAR averaged over $1 \mathrm{~cm}^{3}(1 \mathrm{~g})$ of Head TSL | Condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $7.95 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Head TSL parameters | normalized to 1 W | $\mathbf{7 9 . 6 ~ W / k g ~} \pm 19.9 \%(\mathrm{k}=2)$ |


| SAR averaged over $10 \mathrm{~cm}^{3}(10 \mathrm{~g})$ of Head TSL | condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $2.26 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Head TSL parameters | normalized to 1 W | $\mathbf{2 2 . 6} \mathrm{~W} / \mathrm{kg} \pm 19.5 \%(\mathbf{k}=2)$ |

Head TSL parameters at 5300 MHz
The following parameters and calculations were applied.

|  | Temperature | Permittivity | Conductivity |
| :--- | :---: | :---: | :---: |
| Nominal Head TSL parameters | $22.0^{\circ} \mathrm{C}$ | 35.9 | $4.76 \mathrm{mho} / \mathrm{m}$ |
| Measured Head TSL parameters | $(22.0 \pm 0.2)^{\circ} \mathrm{C}$ | $36.3 \pm 6 \%$ | $4.64 \mathrm{mho} / \mathrm{m} \pm 6 \%$ |
| Head TSL temperature change during test | $<0.5^{\circ} \mathrm{C}$ | --- | ---- |

## SAR result with Head TSL at 5300 MHz

| SAR averaged over $1 \mathrm{~cm}^{\mathbf{3}}(1 \mathrm{~g})$ of Head TSL | Condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $8.10 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Head TSL parameters | normalized to 1 W | $81.1 \mathrm{~W} / \mathrm{kg} \pm 19.9 \%(\mathrm{k}=2)$ |


| SAR averaged over $10 \mathrm{~cm}^{3}(10 \mathrm{~g})$ of Head TSL | condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $2.31 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Head TSL parameters | normalized to 1 W | $23.1 \mathrm{~W} / \mathrm{kg} \pm 19.5 \%(\mathrm{k}=2)$ |

Head TSL parameters at 5500 MHz
The following parameters and calculations were applied.

|  | Temperature | Permittivity | Conductivity |
| :--- | :---: | :---: | :---: |
| Nominal Head TSL parameters | $22.0^{\circ} \mathrm{C}$ | 35.6 | $4.96 \mathrm{mho} / \mathrm{m}$ |
| Measured Head TSL parameters | $(22.0 \pm 0.2)^{\circ} \mathrm{C}$ | $36.0 \pm 6 \%$ | $4.84 \mathrm{mho} / \mathrm{m} \pm 6 \%$ |
| Head TSL temperature change during test | $<0.5^{\circ} \mathrm{C}$ | ---- | --- |

## SAR result with Head TSL at 5500 MHz

| SAR averaged over $\mathbf{1} \mathrm{cm}^{\mathbf{3}} \mathbf{( 1 \mathrm { g } ) \text { of Head TSL }}$ | Condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $8.53 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Head TSL parameters | normalized to 1 W | $\mathbf{8 5 . 4} \mathrm{~W} / \mathrm{kg} \pm 19.9 \%(\mathrm{k}=\mathbf{2})$ |


| SAR averaged over $10 \mathrm{~cm}^{\mathbf{3}}(\mathbf{1 0} \mathbf{g})$ of Head TSL | condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $2.40 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Head TSL parameters | normalized to 1 W | $\mathbf{2 4 . 0} \mathrm{~W} / \mathrm{kg} \pm \mathbf{1 9 . 5} \%(\mathbf{k}=\mathbf{2})$ |

Head TSL parameters at 5600 MHz
The following parameters and calculations were applied.

|  | Temperature | Permittivity | Conductivity |
| :--- | :---: | :---: | :---: |
| Nominal Head TSL parameters | $22.0^{\circ} \mathrm{C}$ | 35.5 | $5.07 \mathrm{mho} / \mathrm{m}$ |
| Measured Head TSL parameters | $(22.0 \pm 0.2)^{\circ} \mathrm{C}$ | $35.8 \pm 6 \%$ | $4.95 \mathrm{mho} / \mathrm{m} \pm 6 \%$ |
| Head TSL temperature change during test | $<0.5^{\circ} \mathrm{C}$ | --- | --- |

## SAR result with Head TSL at 5600 MHz

| SAR averaged over $1 \mathrm{~cm}^{3}(1 \mathrm{~g})$ of Head TSL | Condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $8.36 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Head TSL parameters | normalized to 1 W | $83.6 \mathrm{~W} / \mathrm{kg} \pm 19.9 \%(\mathrm{k}=2)$ |


| SAR averaged over $10 \mathrm{~cm}^{3}(\mathbf{1 0} \mathrm{~g})$ of Head TSL | condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $2.38 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Head TSL parameters | normalized to 1 W | $\mathbf{2 3 . 8} \mathrm{~W} / \mathrm{kg} \pm 19.5 \%(\mathrm{k}=2)$ |

Head TSL parameters at 5800 MHz
The following parameters and calculations were applied.

|  | Temperature | Permittivity | Conductivity |
| :--- | :---: | :---: | :---: |
| Nominal Head TSL parameters | $22.0^{\circ} \mathrm{C}$ | 35.3 | $5.27 \mathrm{mho} / \mathrm{m}$ |
| Measured Head TSL parameters | $(22.0 \pm 0.2)^{\circ} \mathrm{C}$ | $35.5 \pm 6 \%$ | $5.16 \mathrm{mho} / \mathrm{m} \pm 6 \%$ |
| Head TSL temperature change during test | $<0.5^{\circ} \mathrm{C}$ | ---- | ---- |

## SAR result with Head TSL at 5800 MHz

| SAR averaged over $1 \mathrm{~cm}^{\mathbf{3}} \mathbf{( 1 \mathrm { g } ) \text { of Head TSL }}$ | Condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $7.95 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Head TSL parameters | normalized to 1 W | $\mathbf{7 9 . 5} \mathrm{~W} / \mathrm{kg} \pm 19.9 \%(\mathbf{k}=\mathbf{2})$ |


| SAR averaged over $10 \mathrm{~cm}^{\mathbf{3}}(\mathbf{1 0} \mathbf{~ g})$ of Head TSL | condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $2.24 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Head TSL parameters | normalized to 1 W | $\mathbf{2 2 . 4} \mathbf{W} / \mathbf{k g} \pm \mathbf{1 9 . 5} \%(\mathbf{k}=\mathbf{2})$ |

Body TSL parameters at 5200 MHz
The following parameters and calculations were applied.

|  | Temperature | Permittivity | Conductivity |
| :--- | :---: | :---: | :---: |
| Nominal Body TSL parameters | $22.0^{\circ} \mathrm{C}$ | 49.0 | $5.30 \mathrm{mho} / \mathrm{m}$ |
| Measured Body TSL parameters | $(22.0 \pm 0.2)^{\circ} \mathrm{C}$ | $47.5 \pm 6 \%$ | $5.41 \mathrm{mho} / \mathrm{m} \pm 6 \%$ |
| Body TSL temperature change during test | $<0.5^{\circ} \mathrm{C}$ | --- | ---- |

## SAR result with Body TSL at 5200 MHz

| SAR averaged over $\mathbf{1} \mathrm{cm}^{\mathbf{3}} \mathbf{( 1 \mathrm { g } ) \text { of Body TSL }}$ | Condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $7.31 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Body TSL parameters | normalized to 1 W | $\mathbf{7 2 . 7} \mathrm{~W} / \mathrm{kg} \pm 19.9 \%(\mathbf{k}=\mathbf{2})$ |


| SAR averaged over $10 \mathrm{~cm}^{3}(10 \mathrm{~g})$ of Body TSL | condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $2.03 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Body TSL parameters | normalized to 1 W | $20.2 \mathrm{~W} / \mathrm{kg} \pm 19.5 \%(\mathrm{k}=2)$ |

## Body TSL parameters at 5300 MHz

The following parameters and calculations were applied.

|  | Temperature | Permittivity | Conductivity |
| :--- | :---: | :---: | :---: |
| Nominal Body TSL parameters | $22.0^{\circ} \mathrm{C}$ | 48.9 | $5.42 \mathrm{mho} / \mathrm{m}$ |
| Measured Body TSL parameters | $(22.0 \pm 0.2)^{\circ} \mathrm{C}$ | $47.3 \pm 6 \%$ | $5.54 \mathrm{mho} / \mathrm{m} \pm 6 \%$ |
| Body TSL temperature change during test | $<0.5^{\circ} \mathrm{C}$ | --- | --- |

## SAR result with Body TSL at 5300 MHz

| SAR averaged over $\mathbf{1} \mathrm{cm}^{\mathbf{3}} \mathbf{( 1 \mathrm { g } ) \text { of Body TSL }}$ | Condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $7.57 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Body TSL parameters | normalized to 1 W | $\mathbf{7 5 . 2} \mathrm{~W} / \mathrm{kg} \pm 19.9 \%(\mathbf{k}=\mathbf{2})$ |


| SAR averaged over $10 \mathrm{~cm}^{3}(10 \mathrm{~g})$ of Body TSL | condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $2.11 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Body TSL parameters | normalized to 1 W | $20.9 \mathrm{~W} / \mathrm{kg} \pm 19.5 \%(\mathbf{k}=2)$ |

Body TSL parameters at 5500 MHz
The following parameters and calculations were applied.

|  | Temperature | Permittivity | Conductivity |
| :--- | :---: | :---: | :---: |
| Nominal Body TSL parameters | $22.0^{\circ} \mathrm{C}$ | 48.6 | $5.65 \mathrm{mho} / \mathrm{m}$ |
| Measured Body TSL parameters | $(22.0 \pm 0.2)^{\circ} \mathrm{C}$ | $47.0 \pm 6 \%$ | $5.80 \mathrm{mho} / \mathrm{m} \pm 6 \%$ |
| Body TSL temperature change during test | $<0.5^{\circ} \mathrm{C}$ | --- | --- |

## SAR result with Body TSL at 5500 MHz

| SAR averaged over $1 \mathrm{~cm}^{\mathbf{3}}(\mathbf{1} \mathrm{g})$ of Body TSL | Condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $8.04 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Body TSL parameters | normalized to 1 W | $79.9 \mathrm{~W} / \mathrm{kg} \pm 19.9 \%(\mathrm{k}=2)$ |


| SAR averaged over $10 \mathrm{~cm}^{3}(10 \mathrm{~g})$ of Body TSL | condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $2.22 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Body TSL parameters | normalized to 1 W | $22.0 \mathrm{~W} / \mathrm{kg} \pm 19.5 \%(\mathrm{k}=2)$ |

Body TSL parameters at 5600 MHz
The following parameters and calculations were applied.

|  | Temperature | Permittivity | Conductivity |
| :--- | :---: | :---: | :---: |
| Nominal Body TSL parameters | $22.0^{\circ} \mathrm{C}$ | 48.5 | $5.77 \mathrm{mho} / \mathrm{m}$ |
| Measured Body TSL parameters | $(22.0 \pm 0.2)^{\circ} \mathrm{C}$ | $46.8 \pm 6 \%$ | $5.95 \mathrm{mho} / \mathrm{m} \pm 6 \%$ |
| Body TSL temperature change during test | $<0.5^{\circ} \mathrm{C}$ | --- | --- |

SAR result with Body TSL at 5600 MHz

| SAR averaged over $1 \mathrm{~cm}^{\mathbf{3}}(\mathbf{1} \mathrm{g})$ of Body TSL | Condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $7.94 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Body TSL parameters | normalized to 1 W | $\mathbf{7 8 . 9} \mathrm{~W} / \mathrm{kg} \pm \mathbf{1 9 . 9} \%(\mathbf{k}=\mathbf{2})$ |


| SAR averaged over $10 \mathrm{~cm}^{\mathbf{3}}(10 \mathrm{~g})$ of Body TSL | condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $2.20 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Body TSL parameters | normalized to 1 W | $21.8 \mathrm{~W} / \mathrm{kg} \pm 19.5 \%(\mathrm{k}=2)$ |

Body TSL parameters at 5800 MHz
The following parameters and calculations were applied.

|  | Temperature | Permittivity | Conductivity |
| :--- | :---: | :---: | :---: |
| Nominal Body TSL parameters | $22.0^{\circ} \mathrm{C}$ | 48.2 | $6.00 \mathrm{mho} / \mathrm{m}$ |
| Measured Body TSL parameters | $(22.0 \pm 0.2)^{\circ} \mathrm{C}$ | $46.4 \pm 6 \%$ | $6.23 \mathrm{mho} / \mathrm{m} \pm 6 \%$ |
| Body TSL temperature change during test | $<0.5^{\circ} \mathrm{C}$ | --- | ---- |

## SAR result with Body TSL at 5800 MHz

| SAR averaged over $1 \mathrm{~cm}^{3}(1 \mathrm{~g})$ of Body TSL | Condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $7.62 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Body TSL parameters | normalized to 1 W | $\mathbf{7 5 . 7} \mathrm{~W} / \mathrm{kg} \pm 19.9 \%(\mathrm{k}=2)$ |


| SAR averaged over $10 \mathrm{~cm}^{\mathbf{3}}(\mathbf{1 0 ~ \mathrm { g } ) \text { of Body TSL }}$ | condition |  |
| :--- | :---: | :---: |
| SAR measured | 100 mW input power | $2.10 \mathrm{~W} / \mathrm{kg}$ |
| SAR for nominal Body TSL parameters | normalized to 1 W | $20.8 \mathrm{~W} / \mathrm{kg} \pm 19.5 \%(\mathrm{k}=2)$ |

## Appendix (Additional assessments outside the scope of SCS 0108)

Antenna Parameters with Head TSL at 5200 MHz

| Impedance, transformed to feed point | $48.3 \Omega-3.7 \mathrm{j} \Omega$ |
| :--- | :---: |
| Return Loss | -27.8 dB |

Antenna Parameters with Head TSL at 5300 MHz

| Impedance, transformed to feed point | $47.8 \Omega-0.1 \mathrm{j} \Omega$ |
| :--- | :---: |
| Return Loss | -33.0 dB |

## Antenna Parameters with Head TSL at 5500 MHz

| Impedance, transformed to feed point | $46.8 \Omega+1.4 \mathrm{j} \Omega$ |
| :--- | :---: |
| Return Loss | -28.8 dB |

Antenna Parameters with Head TSL at 5600 MHz

| Impedance, transformed to feed point | $50.4 \Omega+3.1 \mathrm{j} \Omega$ |
| :--- | :---: |
| Return Loss | -30.2 dB |

## Antenna Parameters with Head TSL at 5800 MHz

| Impedance, transformed to feed point | $52.3 \Omega+3.2 \mathrm{j} \Omega$ |
| :--- | :---: |
| Return Loss | -28.2 dB |

Antenna Parameters with Body TSL at 5200 MHz

| Impedance, transformed to feed point | $47.9 \Omega-3.7 \mathrm{j} \Omega$ |
| :--- | :---: |
| Return Loss | -27.3 dB |

Antenna Parameters with Body TSL at 5300 MiHz

| Impedance, transformed to feed point | $48.6 \Omega+2.0 \mathrm{j} \Omega$ |
| :--- | :---: |
| Return Loss | -32.0 dB |

## Antenna Parameters with Body TSL at 5500 MHz

| Impedance, transformed to feed point | $47.4 \Omega+3.1 \mathrm{j} \Omega$ |
| :--- | :---: |
| Return Loss | -27.5 dB |

## Antenna Parameters with Body TSL at 5600 MHz

| Impedance, transformed to feed point | $50.5 \Omega+4.0 \mathrm{j} \Omega$ |
| :--- | :---: |
| Return Loss | -28.0 dB |

## Antenna Parameters with Body TSL at 5800 MHz

| Impedance, transformed to feed point | $52.5 \Omega+4.4 \mathrm{j} \Omega$ |
| :--- | :---: |
| Return Loss | -26.2 dB |

## General Antenna Parameters and Design

| Electrical Delay (one direction) | 1.191 ns |
| :--- | :--- |

After long term use with 100 W radiated power, only a slight warming of the dipole near the feedpoint can be measured.
The dipole is made of standard semirigid coaxial cable. The center conductor of the feeding line is directly connected to the second arm of the dipole. The antenna is therefore short-circuited for DC-signals. On some of the dipoles, small end caps are added to the dipole arms in order to improve matching when loaded according to the position as explained in the "Measurement Conditions" paragraph. The SAR data are not affected by this change. The overall dipole length is still according to the Standard.
No excessive force must be applied to the dipole arms, because they might bend or the soldered connections near the feedpoint may be damaged.

## Additional EUT Data

| Manufactured by | SPEAG |
| :--- | :---: |
| Manufactured on | November 14, 2014 |

## DASY5 Validation Report for Head TSL

Test Laboratory: SPEAG, Zurich, Switzerland

## DUT: Dipole D5GHzV2; Type: D5GHzV2; Serial: D5GHzV2 - SN:1212

Communication System: UID 0 - CW; Frequency: 5200 MHz , Frequency: 5300 MHz , Frequency: 5500 MHz , Frequency: 5600 MHz , Frequency: 5800 MHz
Medium parameters used: $\mathrm{f}=5200 \mathrm{MHz} ; \sigma=4.53 \mathrm{~S} / \mathrm{m} ; \varepsilon_{\mathrm{r}}=36.4 ; \rho=1000 \mathrm{~kg} / \mathrm{m}^{3}$,
Medium parameters used: $\mathrm{f}=5300 \mathrm{MHz} ; \sigma=4.64 \mathrm{~S} / \mathrm{m} ; \varepsilon_{\mathrm{r}}=36.3 ; \rho=1000 \mathrm{~kg} / \mathrm{m}^{3}$,
Medium parameters used: $\mathrm{f}=5500 \mathrm{MHz} ; \sigma=4.84 \mathrm{~S} / \mathrm{m} ; \varepsilon_{\mathrm{r}}=36 ; \rho=1000 \mathrm{~kg} / \mathrm{m}^{3}$,
Medium parameters used: $\mathrm{f}=5600 \mathrm{MHz} ; \sigma=4.95 \mathrm{~S} / \mathrm{m} ; \varepsilon_{\mathrm{r}}=35.8 ; \rho=1000 \mathrm{~kg} / \mathrm{m}^{3}$,
Medium parameters used: $\mathrm{f}=5800 \mathrm{MHz} ; \sigma=5.16 \mathrm{~S} / \mathrm{m} ; \varepsilon_{\mathrm{r}}=35.5 ; \rho=1000 \mathrm{~kg} / \mathrm{m}^{3}$
Phantom section: Flat Section
Measurement Standard: DASY5 (IEEE/IEC/ANSI C63.19-2011)
DASY52 Configuration:

- Probe: EX3DV4 - SN3503; ConvF(5.75, 5.75, 5.75); Calibrated: 30.12.2017, ConvF(5.5, 5.5, 5.5); Calibrated: 30.12 .2017 , $\operatorname{ConvF}(5.2,5.2,5.2)$; Calibrated: 30.12 .2017 , $\operatorname{ConvF}(5.05,5.05,5.05)$; Calibrated: $30.12 .2017, \operatorname{ConvF}(4.96,4.96,4.96)$; Calibrated: 30.12.2017;
- Sensor-Surface: 1.4 mm (Mechanical Surface Detection)
- Electronics: DAE4 Sn601; Calibrated: 26.10.2017
- Phantom: Flat Phantom 5.0 (front); Type: QD 000 P50 AA; Serial: 1001
- DASY52 52.10.0(1446); SEMCAD X 14.6.10(7417)

```
Dipole Calibration for Head Tissue/Pin=100mW, dist \(=10 \mathrm{~mm}, \mathrm{f}=5200 \mathrm{MHz} /\) Zoom Scan,
dist \(=1.4 \mathrm{~mm}(8 \times 8 \times 7) /\) Cube 0: Measurement grid: \(d x=4 \mathrm{~mm}, \mathrm{dy}=4 \mathrm{~mm}, \mathrm{dz}=1.4 \mathrm{~mm}\)
Reference Value \(=71.98 \mathrm{~V} / \mathrm{m}\); Power Drift \(=-0.08 \mathrm{~dB}\)
Peak SAR (extrapolated) \(=28.5 \mathrm{~W} / \mathrm{kg}\)
\(\operatorname{SAR}(1 \mathrm{~g})=7.95 \mathrm{~W} / \mathrm{kg} ; \operatorname{SAR}(10 \mathrm{~g})=2.26 \mathrm{~W} / \mathrm{kg}\)
Maximum value of SAR \((\) measured \()=18.0 \mathrm{~W} / \mathrm{kg}\)
Dipole Calibration for Head Tissue/Pin \(=100 \mathrm{~mW}\), dist \(=10 \mathrm{~mm}, \mathrm{f}=5300 \mathrm{MHz} /\) Zoom Scan,
dist \(=1.4 \mathrm{~mm}(8 \mathrm{x} 8 \mathrm{x} 7) /\) Cube 0 : Measurement grid: \(\mathrm{dx}=4 \mathrm{~mm}, \mathrm{dy}=4 \mathrm{~mm}, \mathrm{dz}=1.4 \mathrm{~mm}\)
Reference Value \(=72.21 \mathrm{~V} / \mathrm{m}\); Power Drift \(=-0.08 \mathrm{~dB}\)
Peak SAR (extrapolated) \(=29.9 \mathrm{~W} / \mathrm{kg}\)
\(\operatorname{SAR}(1 \mathrm{~g})=8.1 \mathrm{~W} / \mathrm{kg} ; \operatorname{SAR}(10 \mathrm{~g})=2.31 \mathrm{~W} / \mathrm{kg}\)
Maximum value of SAR (measured) \(=18.8 \mathrm{~W} / \mathrm{kg}\)
Dipole Calibration for Head Tissue/Pin \(=100 \mathrm{~mW}\), dist \(=10 \mathrm{~mm}, \mathrm{f}=5500 \mathrm{MHz} /\) Zoom Scan,
dist \(=1.4 \mathrm{~mm}(8 \times 8 \times 7) /\) Cube 0: Measurement grid: \(d x=4 \mathrm{~mm}, d y=4 \mathrm{~mm}, \mathrm{dz}=1.4 \mathrm{~mm}\)
Reference Value \(=73.15 \mathrm{~V} / \mathrm{m}\); Power Drift \(=-0.08 \mathrm{~dB}\)
Peak SAR (extrapolated) \(=33.3 \mathrm{~W} / \mathrm{kg}\)
\(\operatorname{SAR}(1 \mathrm{~g})=8.53 \mathrm{~W} / \mathrm{kg} ; \operatorname{SAR}(10 \mathrm{~g})=2.4 \mathrm{~W} / \mathrm{kg}\)
Maximum value of SAR (measured) \(=20.1 \mathrm{~W} / \mathrm{kg}\)
```

Dipole Calibration for Head Tissue/Pin $=100 \mathrm{~mW}$, dist $=10 \mathrm{~mm}, \mathrm{f}=5600 \mathrm{MHz} /$ Zoom Scan, dist $=1.4 \mathrm{~mm}(8 \times 8 \times 7) /$ Cube 0 : Measurement grid: $\mathrm{dx}=4 \mathrm{~mm}, \mathrm{dy}=4 \mathrm{~mm}, \mathrm{dz}=1.4 \mathrm{~mm}$
Reference Value $=72.01 \mathrm{~V} / \mathrm{m}$; Power Drift $=-0.05 \mathrm{~dB}$
Peak SAR (extrapolated) $=32.2 \mathrm{~W} / \mathrm{kg}$
$\operatorname{SAR}(1 \mathrm{~g})=8.36 \mathrm{~W} / \mathrm{kg} ; \operatorname{SAR}(10 \mathrm{~g})=2.38 \mathrm{~W} / \mathrm{kg}$
Maximum value of SAR (measured) $=20.0 \mathrm{~W} / \mathrm{kg}$
Dipole Calibration for Head Tissue/Pin $=100 \mathrm{~mW}$, dist $=10 \mathrm{~mm}, \mathrm{f}=5800 \mathrm{MHz} /$ Zoom Scan, dist $=1.4 \mathrm{~mm}(8 \times 8 \times 7) /$ Cube $0:$ Measurement grid: $\mathrm{dx}=4 \mathrm{~mm}, \mathrm{dy}=4 \mathrm{~mm}, \mathrm{dz}=1.4 \mathrm{~mm}$
Reference Value $=70.08 \mathrm{~V} / \mathrm{m}$; Power Drift $=-0.03 \mathrm{~dB}$
Peak SAR (extrapolated) $=31.9 \mathrm{~W} / \mathrm{kg}$
$\operatorname{SAR}(1 \mathrm{~g})=7.95 \mathrm{~W} / \mathrm{kg} ; \operatorname{SAR}(10 \mathrm{~g})=2.24 \mathrm{~W} / \mathrm{kg}$
Maximum value of SAR (measured) $=19.4 \mathrm{~W} / \mathrm{kg}$


## Impedance Measurement Plot for Head TSL



## DASY5 Validation Report for Body TSL

Test Laboratory: SPEAG, Zurich, Switzerland

## DUT: Dipole D5GHzV2; Type: D5GHzV2; Serial: D5GHzV2 - SN:1212

Communication System: UID 0 - CW; Frequency: 5200 MHz , Frequency: 5300 MHz ,
Frequency: 5500 MHz , Frequency: 5600 MHz , Frequency: 5800 MHz
Medium parameters used: $\mathrm{f}=5200 \mathrm{MHz} ; \sigma=5.41 \mathrm{~S} / \mathrm{m} ; \varepsilon_{\mathrm{r}}=47.5 ; \rho=1000 \mathrm{~kg} / \mathrm{m}^{3}$,
Medium parameters used: $\mathrm{f}=5300 \mathrm{MHz} ; \sigma=5.54 \mathrm{~S} / \mathrm{m} ; \varepsilon_{\mathrm{r}}=47.3 ; \rho=1000 \mathrm{~kg} / \mathrm{m}^{3}$,
Medium parameters used: $\mathrm{f}=5500 \mathrm{MHz} ; \sigma=5.8 \mathrm{~S} / \mathrm{m} ; \varepsilon_{\mathrm{r}}=47 ; \rho=1000 \mathrm{~kg} / \mathrm{m}^{3}$,
Medium parameters used: $\mathrm{f}=5600 \mathrm{MHz} ; \sigma=5.95 \mathrm{~S} / \mathrm{m} ; \varepsilon_{\mathrm{r}}=46.8 ; \rho=1000 \mathrm{~kg} / \mathrm{m}^{3}$,
Medium parameters used: $\mathrm{f}=5800 \mathrm{MHz} ; \sigma=6.23 \mathrm{~S} / \mathrm{m} ; \varepsilon_{\mathrm{r}}=46.4 ; \rho=1000 \mathrm{~kg} / \mathrm{m}^{3}$
Phantom section: Flat Section
Measurement Standard: DASY5 (IEEE/IEC/ANSI C63.19-2011)
DASY52 Configuration:

- Probe: EX3DV4 - SN3503; ConvF(5.35, 5.35, 5.35); Calibrated: 30.12.2017, ConvF(5.15, 5.15, 5.15); Calibrated: 30.12 .2017 , $\operatorname{ConvF}(4.7,4.7,4.7)$; Calibrated: 30.12 .2017 , $\operatorname{ConvF}(4.65,4.65,4.65)$; Calibrated: $30.12 .2017, \operatorname{ConvF}(4.53,4.53,4.53)$; Calibrated: 30.12.2017;
- Sensor-Surface: 1.4 mm (Mechanical Surface Detection)
- Electronics: DAE4 Sn601; Calibrated: 26.10.2017
- Phantom: Flat Phantom 5.0 (back); Type: QD 000 P50 AA; Serial: 1002
- DASY52 52.10.0(1446); SEMCAD X 14.6.10(7417)

Dipole Calibration for Body Tissue/Pin=100mW, dist=10mm, f=5200 MHz/Zoom Scan,
dist $=1.4 \mathrm{~mm}(8 \times 8 \times 7) /$ Cube 0: Measurement grid: $d x=4 \mathrm{~mm}, d y=4 \mathrm{~mm}, \mathrm{dz}=1.4 \mathrm{~mm}$
Reference Value $=64.59 \mathrm{~V} / \mathrm{m}$; Power Drift $=-0.02 \mathrm{~dB}$
Peak SAR (extrapolated) $=27.2 \mathrm{~W} / \mathrm{kg}$
$\operatorname{SAR}(1 \mathrm{~g})=7.31 \mathrm{~W} / \mathrm{kg} ; \operatorname{SAR}(10 \mathrm{~g})=2.03 \mathrm{~W} / \mathrm{kg}$
Maximum value of SAR $($ measured $)=16.9 \mathrm{~W} / \mathrm{kg}$
Dipole Calibration for Body Tissue/Pin $=100 \mathrm{~mW}$, dist $=10 \mathrm{~mm}, \mathrm{f}=5300 \mathrm{MHz} /$ Zoom Scan,
dist $=1.4 \mathrm{~mm}(8 \times 8 \times 7) /$ Cube $0:$ Measurement grid: $d x=4 \mathrm{~mm}, d y=4 \mathrm{~mm}, \mathrm{dz}=1.4 \mathrm{~mm}$
Reference Value $=64.99 \mathrm{~V} / \mathrm{m}$; Power Drift $=-0.01 \mathrm{~dB}$
Peak SAR $($ extrapolated $)=29.6 \mathrm{~W} / \mathrm{kg}$
$\operatorname{SAR}(1 \mathrm{~g})=7.57 \mathrm{~W} / \mathrm{kg} ; \operatorname{SAR}(10 \mathrm{~g})=2.11 \mathrm{~W} / \mathrm{kg}$
Maximum value of SAR $($ measured $)=17.7 \mathrm{~W} / \mathrm{kg}$
Dipole Calibration for Body Tissue/Pin=100mW, dist=10mm, f=5500 MHz/Zoom Scan,
dist $=1.4 \mathrm{~mm}(8 \times 8 \times 7) /$ Cube 0: Measurement grid: $d x=4 \mathrm{~mm}, \mathrm{dy}=4 \mathrm{~mm}, \mathrm{dz}=1.4 \mathrm{~mm}$
Reference Value $=65.88 \mathrm{~V} / \mathrm{m}$; Power Drift $=-0.07 \mathrm{~dB}$
Peak SAR (extrapolated) $=33.3 \mathrm{~W} / \mathrm{kg}$
$\operatorname{SAR}(1 \mathrm{~g})=8.04 \mathrm{~W} / \mathrm{kg} ; \operatorname{SAR}(10 \mathrm{~g})=2.22 \mathrm{~W} / \mathrm{kg}$
Maximum value of SAR (measured) $=19.3 \mathrm{~W} / \mathrm{kg}$

Dipole Calibration for Body Tissue/Pin $=100 \mathrm{~mW}$, dist $=10 \mathrm{~mm}, \mathrm{f}=5600 \mathrm{MHz} /$ Zoom Scan, dist $=1.4 \mathrm{~mm}(8 \times 8 \times 7) /$ Cube 0: Measurement grid: $\mathrm{dx}=4 \mathrm{~mm}, \mathrm{dy}=4 \mathrm{~mm}, \mathrm{dz}=1.4 \mathrm{~mm}$
Reference Value $=64.59 \mathrm{~V} / \mathrm{m}$; Power Drift $=-0.02 \mathrm{~dB}$
Peak SAR (extrapolated) $=33.4 \mathrm{~W} / \mathrm{kg}$
$\operatorname{SAR}(1 \mathrm{~g})=7.94 \mathrm{~W} / \mathrm{kg} ; \operatorname{SAR}(10 \mathrm{~g})=2.2 \mathrm{~W} / \mathrm{kg}$
Maximum value of SAR $($ measured $)=19.0 \mathrm{~W} / \mathrm{kg}$
Dipole Calibration for Body Tissue/Pin $=100 \mathrm{~mW}$, dist $=10 \mathrm{~mm}, \mathrm{f}=5800 \mathrm{MHz} /$ Zoom Scan, dist $=1.4 \mathrm{~mm}(8 \times 8 \times 7) /$ Cube 0 ; Measurement grid: $\mathrm{dx}=4 \mathrm{~mm}, \mathrm{dy}=4 \mathrm{~mm}, \mathrm{dz}=1.4 \mathrm{~mm}$
Reference Value $=63.42 \mathrm{~V} / \mathrm{m}$; Power Drift $=-0.02 \mathrm{~dB}$
Peak SAR (extrapolated) $=33.2 \mathrm{~W} / \mathrm{kg}$
$\operatorname{SAR}(1 \mathrm{~g})=7.62 \mathrm{~W} / \mathrm{kg} ; \operatorname{SAR}(10 \mathrm{~g})=2.1 \mathrm{~W} / \mathrm{kg}$
Maximum value of SAR (measured) $=18.7 \mathrm{~W} / \mathrm{kg}$


## Impedance Mieasurement Plot for Body TSL



## APPENDIX C. - SAR Tissue Specifications

The brain and muscle mixtures consist of a viscous gel using hydrox-ethylcellulose (HEC) gelling agent and saline solution (see Table C.1). Preservation with a bactericide is added and visual inspection is made to make sure air bubbles are not trapped during the mixing process. The mixture is calibrated to obtain proper dielectric constant (permittivity) and conductivity of the desired tissue. The mixture characterizations used for the brain and muscle tissue simulating liquids are according to the data by C . Gabriel and G. Harts grove.


Figure C. 1 Simulated Tissue

Table C. 1 Composition of the Tissue Equivalent Matter

| Ingredients (\% by weight) | Frequency (MHz) |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 835 |  | 1900 |  | 2450 |  | $5200 \sim 5800$ |  |
| Tissue Type | Head | Body | Head | Body | Head | Body | Head | Body |
| Water | 40.19 | 50.75 | 55.24 | 70.23 | 71.88 | 73.40 | 65.52 | 80.00 |
| Salt ( NaCl ) | 1.480 | 0.940 | 0.310 | 0.290 | 0.160 | 0.060 | - | - |
| Sugar | 57.90 | 48.21 | - | - | - | - | - | - |
| HEC | 0.250 | - | - | - | - | - | - | - |
| Bactericide | 0.180 | 0.100 | - | - | - | - | - | - |
| Triton X-100 | - | - | - | - | 19.97 | - | 17.24 | - |
| DGBE | - | - | 44.45 | 29.48 | 7.990 | 26.54 | - | - |
| Diethylene glycol hexyl ether | - | - | - | - | - | - | 17.24 | - |
| Polysorbate (Tween) 80 | - | - | - | - | - | - |  | 20.00 |
| Target for Dielectric Constant | 41.5 | 55.2 | 40.0 | 53.3 | 39.2 | 52.7 | - | - |
| Target for Conductivity (S/m) | 0.90 | 0.97 | 1.40 | 1.52 | 1.80 | 1.95 | - | - |

Salt:
Water:
DGBE:
Triton X-100(ultra pure):

99 \% Pure Sodium Chloride
De-ionized, 16M resistivity

Sugar: $\quad 98$ \% Pure Sucrose
HEC: Hydroxyethyl Cellulose

99 \% Di(ethylene glycol) butyl ether,[2-(2-butoxyethoxy) ethanol]
Polyethylene glycol mono[4-(1,1,3,3-tetramethylbutyl)phenyl] ether

Table C. 2 HSL/MSL750 (Head and Body liquids for 700 - 800 MHz )

| Item | Head Tissue Simulation Liquids HSL750 |
| :--- | :--- |
|  | Muscle (body) Tissue Simulation Liquids MSL750 |
| Type No | SL AAH 075, SL AAM 075 |
| Manufacturer | SPEAG |
| The item is composed of the following ingredients: |  |
| $\mathrm{H}^{2} \mathrm{O}$ | Water, 35 - 58\% |
| Sucrose | Sucrose, 40 - 60\% |
| NaCl | Sodium Chloride, 0 - 6\% |
| $\mathrm{Hydroxyethyl-cellulose}$ | Medium Viscosity (CAS\# 9004-62-0), < 0.3\% |
| Preventol-D7 | Preservative:aqueous preparation, (CAS\# 55965-84-9), containing 5- <br> chloro-2-methyl-3(2H)-isothiazolone and 2-methyyl-3(2H)-isothiazolone, <br> 0.1-0.6\% |

Table C. 3 HSL/MSL1750 (Head and Body liquids for 1700 - 1800 MHz )

| Item | Head Tissue Simulation Liquids HSL1750 |
| :--- | :--- |
|  | Muscle (body) Tissue Simulation Liquids MSL1750 |
| Type No | SLAAH 175, SL AAM 175 |
| Manufacturer | SPEAG |
| The item is composed of the following ingredients: |  |
| $\mathrm{H}^{2} \mathrm{O}$ | Water, $52-75 \%$ |
| C 8 H 18 O 3 | Diethylene glycol monobutyl ether (DGBE), 25-48\% |
| NaCl | Sodium Chloride, <1.0\% |

## APPENDIX D. - SAR SYSTEM VALIDATION

## SAR System Validation

Per FCC KDB 865664 D02v01r02, SAR system validation status should be documented to confirm measurement accuracy. The SAR systems (including SAR probes, system components and software versions) used for this device were validated against its performance specifications prior to the SAR measurements. Reference dipoles were used with the required tissue- equivalent media for system validation, according to the procedures outlined in FCC KDB 865664 D01v01r04 and IEEE 1528-2013. Since SAR probe calibrations are frequency dependent, each probe calibration point was validated at a frequency within the valid frequency range of the probe calibration point, using the system that normally operates with the probe for routine SAR measurements and according to the required tissue-equivalent media.

A tabulated summary of the system validation status including the validation date(s), measurement frequencies, SAR probes and tissue dielectric parameters has been included.

Table D. 1 SAR System Validation Summary

| SAR <br> System | Freq. <br> [MHz] | Date | Probe SN | Probe Type | Probe CAL. Point |  | PERM. | COND. | CW Validation |  |  | MOD. Validation |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | (عr) | ( $\sigma$ ) | Sensitivity | Probe Linearity | Probe Isortopy | MOD. Type | Duty Factor | PAR |
| D | 750 | 2018.10.15 | 3933 | EX3DV4 | 750 | Head | 42.212 | 0.887 | PASS | PASS | PASS | N/A | N/A | N/A |
| D | 835 | 2018.10.16 | 3933 | EX3DV4 | 835 | Head | 40.978 | 0.919 | PASS | PASS | PASS | GMSK | PASS | N/A |
| D | 1800 | 2018.10.17 | 3933 | Ex3DV4 | 1800 | Head | 39.954 | 1.397 | PASS | PASS | PASS | N/A | N/A | N/A |
| D | 1900 | 2018.10.18 | 3933 | Ex3DV4 | 1900 | Head | 39.547 | 1.369 | PASS | PASS | PASS | GMSK | PASS | N/A |
| c | 2450 | 2018.05.10 | 3916 | Ex3DV4 | 2450 | Head | 38.995 | 1.822 | PASS | PASS | PASS | OFDM/TDD | PASS | PASS |
| D | 2600 | 2018.10.22 | 3933 | EX3DV4 | 2600 | Head | 38.458 | 1.977 | PASS | PASS | PASS | TDD | PASS | N/A |
| c | 5200 | 2018.05.14 | 3916 | Ex3DV4 | 5200 | Head | 34.856 | 4.725 | PASS | PASS | PASS | OFDM | N/A | PASS |
| c | 5300 | 2018.05.15 | 3916 | Ex3DV4 | 5300 | Head | 34.854 | 4.856 | PASS | PASS | PASS | OFDM | N/A | PASS |
| c | 5500 | 2018.05.16 | 3916 | EX3DV4 | 5500 | Head | 34.625 | 5.113 | PASS | PASS | PASS | OFDM | N/A | PASS |
| c | 5600 | 2018.05.17 | 3916 | Ex3DV4 | 5600 | Head | 34.265 | 5.221 | PASS | PASS | PASS | OFDM | N/A | PASS |
| C | 5800 | 2018.05.18 | 3916 | EX3DV4 | 5800 | Head | 34.113 | 5.414 | PASS | PASS | PASS | OFDM | N/A | PASS |
| D | 750 | 2018.10.15 | 3933 | Ex3DV4 | 750 | Body | 54.650 | 0.965 | PASS | PASS | PASS | N/A | N/A | N/A |
| D | 835 | 2018.10.16 | 3933 | Ex3DV4 | 835 | Body | 54.597 | 0.975 | PASS | PASS | PASS | GMSK | PASS | N/A |
| D | 1800 | 2018.10.17 | 3933 | Ex3DV4 | 1800 | Body | 52.381 | 1.553 | PASS | PASS | PASS | N/A | N/A | N/A |
| D | 1900 | 2018.10.18 | 3933 | Ex3DV4 | 1900 | Body | 52.289 | 1.571 | PASS | PASS | PASS | GMSK | PASS | N/A |
| c | 2450 | 2018.05.10 | 3916 | Ex3DV4 | 2450 | Body | 51.454 | 2.011 | PASS | PASS | PASS | OFDM/TDD | PASS | PASS |
| D | 2600 | 2018.10.22 | 3933 | Ex3DV4 | 2600 | Body | 51.142 | 2.221 | PASS | PASS | PASS | TDD | PASS | N/A |
| c | 5200 | 2018.05.14 | 3916 | EX3DV4 | 5200 | Body | 48.156 | 5.467 | PASS | PASS | PASS | OFDM | N/A | PASS |
| c | 5300 | 2018.05.15 | 3916 | EX3DV4 | 5300 | Body | 48.111 | 5.488 | PASS | PASS | PASS | OFDM | N/A | PASS |
| c | 5500 | 2018.05.16 | 3916 | Ex3DV4 | 5500 | Body | 47.774 | 5.822 | PASS | PASS | PASS | OFDM | N/A | PASS |
| c | 5600 | 2018.05.17 | 3916 | Ex3DV4 | 5600 | Body | 47.116 | 5.911 | PASS | PASS | PASS | OFDM | N/A | PASS |
| c | 5800 | 2018.05.18 | 3916 | EX3DV4 | 5800 | Body | 46.774 | 6.223 | PASS | PASS | PASS | OFDM | N/A | PASS |

NOTE: While the probes have been calibrated for both a CW and modulated signals, all measurements were performed using communication systems calibrated for CW signals only. Modulations in the table above represent test configurations for which the measurement system has been validated per FCC KDB Publication 865664 D01v01r04 for scenarios when CW probe calibrations are used with other signal types. SAR systems were validated for modulated signals with a periodic duty cycle, such as GMSK, or with a high peak to average ratio ( $>5 \mathrm{~dB}$ ), such as OFDM according to KDB 865664.

## APPENDIX E. - Downlink LTE CA RF Conducted Powers

## E. 1 LTE Downlink Only Carrier Aggregation Test Reduction Methodology

SAR test exclusion for LTE downlink Carrier Aggregation is determined by power measurements according to the number of component carriers (CCs) supported by the product implementation. Per April 2018 TCBC Workshop Notes, the following test reduction methodology was applied to determine the combinations required for conducted power measurements.

## LTE DL CA Test Reduction Methodology:

(1) Test supported combinations were arranged by the number of component carriers in columns.
(2) Any limitations on the PCC or SCC for each combination were identified alongside the combination (e.g. CA $2 \mathrm{~A}-2 \mathrm{~A}-4 \mathrm{~A}-12 \mathrm{~A}$, but B12 can only be configured as a SCC).
(3) Power measurements were performed for "supersets" (LTE CA combinations with multiple components carriers) and any "subsets" (LTE CA combinations with fewer component carriers) that were not completely covered by the supersets.
(4) Only subsets that have the exact same components as a superset were excluded for measurement.
(5) When there were certain restrictions on component carriers that existed in the superset that were not applied for the subset, the subset configuration was additionally evaluated.
(6) Both inter-band and intra-band downlink carrier aggregation scenarios were considered.

| Index | 2 CC | Restriction | Completely Covered by Measurement Superset | Index | 3 CC | Restriction | Completely Covered by Measurement Superset | Index | 4 CC | Restriction | Completely Covered by Measurement Superset | Index | 5 CC | Restriction | Completely Covered by Measurement Superset |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $2 \mathrm{Cc}{ }^{\text {\% }} 1$ | $\mathrm{CA}_{2} 2 \mathrm{C}$ |  | 3 CCH \# | $3 \mathrm{CCH1}$ | CA $2 \mathrm{~A}-2 \mathrm{~A}-4 \mathrm{~A}$ |  | $4 \mathrm{CCH1}$ | $4 \mathrm{CCH1}$ | CA $2 \mathrm{~A}-2 \mathrm{~A}-4 \mathrm{~A}-4 \mathrm{~A}$ |  | No | SCC\#1 | CA_2A-2A-46D | B46 SCC Only | No |
| $2 \mathrm{CCH2}$ | CA $2 \mathrm{~A}-2 \mathrm{~A}$ |  | $4 \mathrm{CC} \# 1$ | $3 \mathrm{CCH}+2$ | CA $2 \mathrm{~A}-2 \mathrm{~A}-5 \mathrm{~A}$ |  | $4 \mathrm{CCH2}$ | 4CC\#2 | CA $2 \mathrm{~A}-2 \mathrm{~A}-4 \mathrm{~A}-5 \mathrm{~A}$ |  | No | $\mathrm{CCO}+2$ | CA 2 A-5B-30A-66A |  | No |
| 2 CCH | CA $2 \mathrm{~A}-4 \mathrm{~A}(2)$ |  | 4 CC \#1 | 3 CCH | CA $2 \mathrm{~A}-2 \mathrm{~A}-12 \mathrm{~A}$ |  | No | 4CCH3 | CA $2 \mathrm{~A}-2 \mathrm{~A}-4 \mathrm{~A}-12 \mathrm{~A}$ | B12 SCC Only | No | CCOH | CA 2 A-5B-66A-66A |  | No |
| $2 \mathrm{CCH4}$ | CA 2A-5A |  | $4 \mathrm{CC} \# 2$ | $3 \mathrm{CC}+4$ | CA $2 \mathrm{~A}-2 \mathrm{~A}-13 \mathrm{~A}$ |  | 4 CC \#8 | $4 \mathrm{CC} \mathrm{\# H}^{\text {d }}$ | CA 2A-2A-5A-30A |  | No | $\mathrm{SCC}^{\text {\# }} 4$ | CA 2A-46D-66A | B46 SCC Only | No |
| $2 \mathrm{CCH5}$ | CA 2A-7A |  | $4 \mathrm{CC} \# 16$ | 3CC\#5 | CA $2 \mathrm{~A}-2 \mathrm{~A}-29 \mathrm{~A}$ | B29 SCC Only | $4 \mathrm{CC} \# 9$ | 4CC\#5 | CA $2 \mathrm{~A}-2 \mathrm{~A}-5 \mathrm{~A}-66 \mathrm{~A}$ |  | No | SCCH5 | CA 2 2-46A-46C-66A | ${ }^{\text {B46 SCC Only }}$ | No |
| 2Cc\#6 | CA_2A-12A(1) |  | $3 \mathrm{CC} \# 3$ | 3CCH6 | CA $2 \mathrm{~A}-2 \mathrm{~A}-30 \mathrm{~A}$ |  | $4 \mathrm{CC} \# 9$ | 4CCH6 | CA 2 A-2A-12A-30A | B12 SCC Only | No | SCC\#6 | CA 41C-41D |  | No |
| $2 \mathrm{CCH7}$ | CA $2 \mathrm{~A}-13 \mathrm{~A}$ |  | $4 \mathrm{CC} \# 31$ | $3 \mathrm{CC} \# 7$ | CA 2C-66A |  | No | HCC\#7 | CA $2 \mathrm{~A}-2 \mathrm{~A}-12 \mathrm{~A}-66 \mathrm{~A}$ | B12 SCC Only | No | CC\#7 | CA 46D-66A-66A | B46 SCC Only | No |
| $2 \mathrm{CCH8}$ | CA 2 A-14A |  | $3 \mathrm{CC} \# 27$ | 3CC\# ${ }^{\text {c }}$ | CA $2 \mathrm{~A}-2 \mathrm{~A}$-66A |  | $4 \mathrm{CCH7}$ | 4CC\#8 | CA 2 A-2A-13A-66A |  | No | $\mathrm{CCCH}^{\text {\% }}$ |  |  |  |
| $2 \mathrm{CCH9}$ | CA 2A-17A |  | No | 3CC \#9 | CA $2 \mathrm{~A}-2 \mathrm{~A}-71 \mathrm{~A}$ | B71 Scc Only | No | 4CC\#9 | CA $2 \mathrm{~A}-2 \mathrm{~A}-29 \mathrm{~A}-30 \mathrm{~A}$ | B29 Scc Only | No | SCA 9 |  |  |  |
| $2 \mathrm{CCH10}$ | CA $2 \mathrm{~A}-29 \mathrm{~A}(2)$ | B29 Scc Only | 4 CC \#9 | $3 \mathrm{CCH10}$ | CA $2 \mathrm{~A}-4 \mathrm{~A}-4 \mathrm{~A}$ |  | $4 \mathrm{CC} \# 1$ | 4CC\#10 | CA 2 A-2A-66A-66A |  | No | SCA_10 |  |  |  |
| 2 CCH \#11 | CA $2 \mathrm{~A}-30 \mathrm{~A}$ |  | 4 CC \#9 | $3 \mathrm{CCH}+11$ | CA $2 \mathrm{~A}-4 \mathrm{~A}-5 \mathrm{~A}$ |  | 4 CCH + | 4CC\#\#11 | CA $22 \mathrm{~A}-4 \mathrm{~A}-4 \mathrm{~A}-5 \mathrm{~A}$ |  | No | CA, 11 |  |  |  |
| $2 \mathrm{CCH}{ }^{\text {d }}$ | CA 2 2-46A | ${ }^{\text {B46 SCC Only }}$ | $5 \mathrm{CC} \# 5$ | 3 CCH 12 | CA $2 \mathrm{~A}-4 \mathrm{~A}-7 \mathrm{~A}$ |  | $4 \mathrm{CC} \# 16$ | 4CC\#12 | CA $2 \mathrm{~A}-4 \mathrm{~A}-4 \mathrm{~A}-12 \mathrm{~A}$ | B12 SCC Only | No | SCA 12 |  |  |  |
| $2 \mathrm{CC} \# 13$ | CA 2A-66A |  | $5 \mathrm{CC} \# 2$ | $3 \mathrm{CCH13}$ | CA $2 \mathrm{~A}-4 \mathrm{~A}-12 \mathrm{~A}$ |  | No | 4CC\#13 | CA 2A-4A-5B |  | No | CA 13 |  |  |  |
| $2 \mathrm{CCH14}$ | CA 2 A - 71 A | B71 SCC Only | 3 CC \#17 | $3 \mathrm{CCH14}$ | CA 2 2A-4A-13A |  | No | ${ }^{1} \mathrm{CC} \# 14$ | CA 2 2A-4A-5A-30A |  | No | SCA 14 |  |  |  |
| $2 \mathrm{CCH15}$ | CA 4A-4A |  | $4 \mathrm{CC} \# 1$ | $3 \mathrm{CC} \# 15$ | CA $2 \mathrm{~A}-4 \mathrm{~A}-29 \mathrm{~A}$ | B29 Scc Only | 4 CC \#20 | ACC\#15 | CA $2 \mathrm{~A}-4 \mathrm{~A}-7 \mathrm{C}$ |  | No | CCA 15 |  |  |  |
| $2 \mathrm{CC} \mathrm{\# 16}$ | CA 4A-5A (1) |  | 4 CC \#2 | $3 \mathrm{CC} \# 16$ | CA $2 \mathrm{~A}-4 \mathrm{~A}-30 \mathrm{~A}$ |  | $4 \mathrm{CC} \# 19$ | 4CC\#16 | CA $2 \mathrm{~A}-4 \mathrm{~A}-7 \mathrm{~A}-7 \mathrm{~A}$ |  | No | CCA 16 |  |  |  |
| $2 \mathrm{CCH17}$ | CA 4A-7A (1) |  | $4 \mathrm{CC} \mathrm{\# 16}$ | $3 \mathrm{CCH17}$ | CA $2 \mathrm{~A}-4 \mathrm{~A}-71 \mathrm{~A}$ | B71 Scc Only | No | 4CC\#17 | CA $2 \mathrm{~A}-4 \mathrm{~A}-7 \mathrm{~A}-12 \mathrm{~A}$ | B12 SCC Only | No | CCA 17 |  |  |  |
| $2 \mathrm{CCH18}$ | CA 4A-12A(2) |  | $4 \mathrm{CC} \# 3$ | 3CC\#18 | CA $2 \mathrm{~A}-5 \mathrm{~B}$ |  | $4 \mathrm{CC} \mathrm{\# 13}$ | HCC\#18 | CA $2 \mathrm{~A}-4 \mathrm{~A}-12 \mathrm{~B}$ | B12 SCC Only | No | CCA 18 |  |  |  |
| $2 \mathrm{CCH19}$ | CA 4A-13A |  | 3CC\#14 | $3 \mathrm{CCH19}$ | CA 2 2A-5A-30A |  | 4 CC \#23 | 4CC\#19 | CA $2 \mathrm{~A}-4 \mathrm{~A}-12 \mathrm{~A}-30 \mathrm{~A}$ | B12 SCC Only | No | SCA_19 |  |  |  |
| $2 \mathrm{CCH20}$ | CA 4A-17A | B17 SCC Only | No | $3 \mathrm{CCH}+20$ | CA_2A-5A-66A |  | $4 \mathrm{CCH}{ }^{2}$ | 4CC +20 | CA $2 \mathrm{~A}-4 \mathrm{~A}-29 \mathrm{~A}-30 \mathrm{~A}$ | ${ }^{\text {B29 SCC Only }}$ | No | $\mathrm{CCA}_{2} 20$ |  |  |  |
| $2 \mathrm{CCH21}$ | CA 4 4-29A(2) | ${ }^{\text {B29 SCC Only }}$ | 4 CC \#20 | $3 \mathrm{CCH21}$ | CA 2A-7A-7A |  | $4 \mathrm{CC} \# 16$ | 4CC \# 21 | CA 2 2-5B-30A |  | 5 CC \#2 | SCA 21 |  |  |  |
| $2 \mathrm{CCH}+22$ | CA 4A-30A |  | $4 \mathrm{CC} \# 19$ | 3CC +22 | CA $2 \mathrm{~A}-7 \mathrm{~A}-12 \mathrm{~A}$ |  | No | ACC +22 | CA $2 \mathrm{~A}-5 \mathrm{~B}$-66A |  | $5 \mathrm{CC} \# 3$ | CA 22 |  |  |  |
| $2 \mathrm{CCH23}$ | CA 4A-46A | B46 SCC Only | 4 CC \#42 | 3CC+23 | CA $2 \mathrm{~A}-12 \mathrm{~B}$ |  | No | $4 \mathrm{CC} \# 23$ | CA 2 2A-5A-30A-66A |  | No | SCA 23 |  |  |  |
| $2 \mathrm{CCH} \# 24$ | CA 4A-71A | B71 SCC Only | $3 \mathrm{CCH43}$ | $3 \mathrm{CCH}+24$ | CA $2 \mathrm{2A}-12 \mathrm{~A}-30 \mathrm{~A}$ |  | No | 4CC $\# 24$ | CA 2 2A-5A-66B |  | No | CCA 24 |  |  |  |
| $2 \mathrm{CCH}+25$ | CA 5B |  | 5 CCH \# | 3CCH25 | CA 2 2-12A-66A |  | No | 4CC +25 | CA $2 \mathrm{~A}-5 \mathrm{~A}-66 \mathrm{C}$ |  | No | CCA 25 |  |  |  |
| $2 \mathrm{CCH26}$ | CA 5A-25A |  | No | 3CC \#26 | CA 2A-13A-66A |  | $4 \mathrm{CC} \# 31$ | ACC\#26 | CA 2A-5A-66A-66A |  | No | SCA 26 |  |  |  |
| 2CCH27 | CA 5A-30A |  | 4 CC \#23 | 3CC +27 | CA $2 \mathrm{~A}-14 \mathrm{~A}-30 \mathrm{~A}$ |  | No | 4CC $\# 27$ | CA $2 \mathrm{~A}-12 \mathrm{~A}-30 \mathrm{~A}-66 \mathrm{~A}$ | B12 SCC Only | No | SCA 27 |  |  |  |
| 2 CCH \#28 | CA 5 A-66A |  | 4 CC \#23 | $3 \mathrm{CCH28}$ | CA $2 \mathrm{~A}-29 \mathrm{~A}-30 \mathrm{~A}$ | B29 Scc Only | $4 \mathrm{CC} \# 9$ | 4CC $\# 28$ | CA 2 A-12A-66A-66A | B12 SCC Only | No | $\mathrm{CCA}_{2} 8$ |  |  |  |
| 2 CCH +29 | CA 7 7A-7A (1) |  | $4 \mathrm{CC} \# 16$ | $3 \mathrm{CCH}+29$ | CA 22A-30A-66A |  | $4 \mathrm{CC} \# 23$ | HCC $\# 29$ | CA 2 2-13A-66B |  | No | ССА 29 |  |  |  |
| $2 \mathrm{CCH}{ }^{2} 0$ | CA 7 - -12 A |  | 3 CC \#22 | $3 \mathrm{CCH} \# 3$ | CA $2 \mathrm{~A}-46 \mathrm{C}$ | ${ }^{\text {B46 SCC Only }}$ | $5 \mathrm{CCH5}$ | 4CCH30 | CA $2 \mathrm{~A}-13 \mathrm{~A}-66 \mathrm{C}$ |  | No | SCA 30 |  |  |  |
| 2CC\#31 | CA 7A-46A (1) | 346 SCC Only | No | 3CCH31 | CA 2A-46A-46A | ${ }^{\text {B46 SCC Only }}$ | $4 \mathrm{CC} \# 34$ | ACC\#31 | CA 2A-13A-66A-66A |  | No | SCA 31 |  |  |  |
| $2 \mathrm{CCH32}$ | CA 12 B |  | 3 CC \#23 | 3CC\#32 | CA 2 2A-46A-66A | B46 SCC Only | $4 \mathrm{CC} \# 34$ | HCC \#32 | CA $2 \mathrm{~A}-46 \mathrm{D}$ | B46 SCC Only | 5CC\#1 | SCA 32 |  |  |  |
| $2 \mathrm{Cc} \# 33$ | CA_12A-25A |  | No | 3CC\#33 | CA $2 \mathrm{~A}-66 \mathrm{~B}$ |  | 4 CC \#24 | 4СС\#33 | CA_2A-46A-46C | B46 SCC Only | 5CC \#5 | CCA 33 |  |  |  |
| $2 \mathrm{CCH} \# 3$ | CA 12A-30A |  | $4 \mathrm{CC} \# 4$ | 3CCH34 | CA 2A-66C |  | 4 CC \#25 | HCC\#34 | CA 2A-46A-46A-66A | ${ }^{\text {B46 SCC Only }}$ | No | CCA 34 |  |  |  |
| $2 \mathrm{CCH35}$ | CA 12A-66A (1) |  | 3CC $\# 25$ | 3CC\#35 | CA 2A-66A-66A |  | 4 CC \#26 | 4СС $\# 35$ | CA 2A-46C-66A | B46 SCC Only | 5CC\#5 | CCA 35 |  |  |  |
| 2CC\#36 | CA 13A-46A | B46 SCC Only | No | 3CC\#36 | CA 2A-66A-71A | B71 Scc Only | No | 4CC\#36 | CA $4 \mathrm{~A}-4 \mathrm{~A}-5 \mathrm{~B}$ |  | No | CCA 36 |  |  |  |
| $2 \mathrm{Cc} \# 37$ | CA $13 \mathrm{~A}-66 \mathrm{~A}$ |  | $4 \mathrm{CCH8}$ | $3 \mathrm{CC} \# 37$ | CA_4A-4A-5A |  | $4 \mathrm{CC} \# 37$ | HCC\#37 | CA $4 \mathrm{~A}-4 \mathrm{~A}-5 \mathrm{~A}-30 \mathrm{~A}$ |  | No | SCA 37 |  |  |  |
| $2 \mathrm{CCH38}$ | CA $14 \mathrm{~A}-30 \mathrm{~A}$ |  | 3 CC \#27 | 3CC\#38 | CA 4 4 -4A-7A (1) |  | No | 4CC \#38 | CA $4 \mathrm{~A}-4 \mathrm{~A}-12 \mathrm{~A}-30 \mathrm{~A}$ | B12 SCC Only | No | [CA 38 |  |  |  |
| 2 CCH 39 | CA 14 A -66A |  | $3 \mathrm{CC} \# 66$ | 3CCH39 | CA 4 4-4A-12A |  | $4 \mathrm{CC} \# 38$ | 4CCH39 | CA $4 \mathrm{~A}-4 \mathrm{~A}-29 \mathrm{~A}-30 \mathrm{~A}$ | ${ }^{\text {B29 SCC Only }}$ | No | SCA 39 |  |  |  |
| 2 CCH 40 | CA 25A-25A(1) |  | $4 \mathrm{CC} \# 49$ | $3 \mathrm{CCH40}$ | CA 4A-4A-13A |  | No | HCC\#40 | CA 4A-5B-30A |  | No | SCA 40 |  |  |  |

Table E.1.1 Example of Exclusion Table for LTE DL CA

## E. 2 LTE Downlink Only Carrier Aggregation Test Selection and Setup

SAR test exclusion for LTE downlink Carrier Aggregation is determined by power measurements according to the number of component carriers (CCs) supported by the product implementation. For those configurations required by April 2018 TCBC Workshop Notes, conducted power measurements with LTE Carrier Aggregation (CA) (downlink only) active are made in accordance to KDB Publication 941225 D05Av01r02. The RRC connection is only handled by one cell, the primary component carrier (PCC) for downlink and uplink communications. After making a data connection to the PCC, the UE device adds secondary component carrier(s) (SCC) on the downlink only. All uplink communications and acknowledgements remain identical to specifications when downlink carrier aggregation is inactive on the PCC. Additional conducted output powers are measured with the downlink carrier aggregation active for the configuration with highest measured maximum conducted power with downlink carrier aggregation inactive measured among the channel bandwidth, modulation and RB combinations in each frequency band.

Per FCC KDB Publication 941225 D05Av01r02, no SAR measurements are required for carrier aggregation configurations when the average output power with downlink only carrier aggregation active is not more than 0.25 dB higher than the average output power with downlink only carrier aggregation inactive.

General PCC and SCC configuration selection procedure
PCC uplink channel, channel bandwidth, modulation and RB configurations were selected based on section C)3)b)ii) of KDB 941225 D05v01r02. The downlink PCC channel was paired with the selected PCC uplink channel according to normal configurations without carrier aggregation.

To maximize aggregation bandwidth, highest channel bandwidth available for that CA combination was selected for SCC. For inter-band CA, the SCC downlink channels were selected near the middle of their transmission bands. For contiguous intra-band CA, the downlink channel spacing between the component carriers was set to multiple of 300 kHz less than the nominal channel spacing defined in section 5.4.1A of 3GPP TS 36.521. For non-contiguous intraband CA, the downlink channel spacing between the component carriers was set to be larger than the nominal channel spacing and provided maximum separation between the component carriers.

All selected PCC and SCC(s) remained fully within the uplink/downlink transmission band of the respective component carrier.

When a device supports LTE capabilities with overlapping transmission frequency ranges, the standalone powers from the band with a larger transmission frequency range can be used to select measurement configurations for the band with the fully covered transmission frequency range.

## E. 3 LTE DL Carrier Aggregation Conducted Powers

- Below downlink CA configurations were determined based on Manufacturer's information.

| Class | ATBC |  | $\begin{gathered} \text { Maximum } \\ \text { number of CC } \end{gathered}$ |
| :---: | :---: | :---: | :---: |
|  | NRB.agg | MHz |  |
| A | $\mathrm{N} \leq 100$ | 20 | 1 |
| B | $\mathbf{2 5}<\mathrm{N} \leq 100$ | 20 | 2 |
| C | $100<\mathrm{N} \leq 200$ | 40 | 2 |
| D | $200<\mathrm{N} \leq 300$ | 60 | 3 |
| E | $300<\mathrm{N} \leq 400$ | 80 | 4 |
| F | $400<\mathrm{N} \leq 500$ | 100 | 5 |
| 1 | $\mathbf{7 0 0}<\mathbf{N} \leq 800$ | 160 | 8 |


| Index | 2CC | Supported Channel Bandwidth [MHz] |  | Restriction | Completely Covered by Measurement Superset |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | CC1 | CC2 |  |  |
| 2CC \#1 | CA_4A-7A (0) | 5, 10 | 5, 10, 15, 20 |  | No |
| 2CC \#2 | CA_4A-7A (1) | 5, 10, 15, 20 | 5, 10, 15, 20 |  | No |
| 2CC \#3 | CA_5A-7A (0) | 1.4, 3, 5, 10 | 10, 15, 20 |  | No |
| 2CC \#4 | CA_5A-7A (1) | 5, 10 | 10, 15, 20 |  | No |
| 2CC \#5 | CA_7A-7A (0) | 5, 10, 15, 20 | 10, 15, 20 |  | No |
| 2CC \#6 | CA_7A-7A (1) | 5, 10, 15, 20 | 5, 10, 15, 20 |  | No |
| 2CC \#7 | CA_7A-7A (2) | 5, 10, 15, 20 | 5,10 |  | No |
| 2CC \#8 | CA_7A-7A (3) | 10, 15, 20 | 10, 15, 20 |  | No |
| 2CC \#9 | CA_7C (0) | 15, 20 | 15, 20 |  | No |
| 2CC \#10 | CA_7C (1) | 10, 15, 20 | 10, 15, 20 |  | No |
| 2CC \#11 | CA_7C (2) | 15, 20 | 10, 15, 20 |  | No |
| 2CC \#12 | CA_66A-66A (0) | 5, 10, 15, 20 | 5, 10, 15, 20 |  | No |
| 2CC \#13 | CA_66B (0) | 5, 10, 15 | 5, 10, 15 |  | No |
| 2CC \#14 | CA_66C (0) | 5, 10, 15, 20 | 5, 10, 15, 20 |  | No |


| PCC |  |  |  |  |  |  |  |  |  | SCC |  |  |  | Power |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Combination | PCC Band | $\begin{gathered} \text { PCC BW } \\ (\mathrm{MHz}) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{PCC} \\ \text { (UL) CH. } \\ \hline \end{gathered}$ | $\begin{gathered} \text { PCC (UL) } \\ \text { Freq. (MHz) } \end{gathered}$ | Mod. | $\begin{aligned} & \text { PCC } \\ & \text { UL\# RB } \end{aligned}$ | PCC UL RB Offset | $\begin{gathered} \mathrm{PCC}(\mathrm{DL}) \\ \mathrm{CH} . \\ \hline \end{gathered}$ | $\begin{gathered} \text { PCC (DL) } \\ \text { Freq. (MHz) } \end{gathered}$ | $\begin{aligned} & \text { SCC } \\ & \text { Band } \end{aligned}$ | $\underset{(\mathrm{MHz})}{\substack{\mathrm{SCC} \\ \hline}}$ | $\begin{gathered} \mathrm{SCC} \\ (\mathrm{DLL}) \mathrm{CH} . \end{gathered}$ | $\begin{gathered} \text { SCC (DL) } \\ \text { Freq. (MHz) } \end{gathered}$ | LTE Tx. Power with DL CA Enabled $(\mathrm{dBm})$ | LTE Single Carrier <br> Tx. Power <br> (dBm) <br> 2.44 |
| CA_4A-7A (0) | LTE B4 | 10 | 20000 | 1715.0 | QPSK | 1 | 25 | 2000 | 2115.0 | LTE B7 | 20 | 3100 | 2655.0 | 23.11 | 23.44 |
| CA_4A-7A (1) | LTE B4 | 20 | 20175 | 1732.5 | QPSK | 1 | 50 | 2175 | 2132.5 | LTE B7 | 20 | 3100 | 2655.0 | 23.10 | 23.34 |

Table F.3.4 LTE Band 5 as PCC

| PCC |  |  |  |  |  |  |  |  |  | SCC |  |  |  | Power |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Combination | PCC Band | $\begin{gathered} \text { PCC BW } \\ (\mathrm{MHz}) \end{gathered}$ | $\begin{aligned} & \mathrm{PCC} \\ & \text { (UL) } \mathrm{CH} . \end{aligned}$ | $\begin{gathered} \text { PCC (UL) } \\ \text { Freq. (MHz) } \end{gathered}$ | Mod. | $\begin{gathered} \mathrm{PCC} \\ \text { UL\#RB } \end{gathered}$ | PCC UL RB Offset | $\begin{gathered} \mathrm{PCC}(\mathrm{DL}) \\ \mathrm{CH} . \end{gathered}$ | $\begin{gathered} \text { PCC (DL) } \\ \text { Freq. (MHz) } \end{gathered}$ | $\begin{aligned} & \text { SCC } \\ & \text { Band } \end{aligned}$ | $\begin{gathered} \text { Scc Bw } \\ (\mathrm{MHz}) \end{gathered}$ | $\begin{gathered} \mathrm{SCC} \\ \text { (DL) } \mathrm{CH} . \end{gathered}$ | $\begin{gathered} \text { SCC (DL) } \\ \text { Freq. (MHz) } \end{gathered}$ | $\begin{gathered} \hline \text { LTE Tx. Power with } \\ \text { DL CA Enabled } \\ (\mathrm{dBm}) \end{gathered}$ | LTE Single Carrier <br> Tx. Power <br> $(\mathrm{dBm})$ |
| CA_5A-7A (0) | LTE B5 | 10 | 20525 | 836.5 | QPSK | 1 | 0 | 2525 | 881.5 | LTE B7 | 20 | 3100 | 2655.0 | 24.12 | 24.40 |
| CA_5A-7A (1) | LTE B5 | 10 | 20525 | 836.5 | QPSK | 1 | 0 | 2525 | 881.5 | LTE B7 | 20 | 3100 | 2655.0 | 24.12 | 24.40 |


| PCC |  |  |  |  |  |  |  |  |  | SCC |  |  |  | Power |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Combination | PCC Band | $\underset{(\mathrm{MHz})}{\mathrm{PCC} \text { BW }}$ | $\begin{gathered} \mathrm{PCC} \\ (\mathrm{UL}) \mathrm{CH} . \end{gathered}$ | $\begin{gathered} \text { PCC (UL) } \\ \text { Freq. (MHz) } \end{gathered}$ | Mod. | $\begin{aligned} & \text { PCC } \\ & \text { UL\# RB } \end{aligned}$ | PCC UL RB Offset | $\begin{gathered} \mathrm{PCC}(\mathrm{DL}) \\ \mathrm{CH} . \\ \hline \end{gathered}$ | $\begin{gathered} \text { PCC (DL) } \\ \text { Freq. (MHz) } \end{gathered}$ | $\begin{aligned} & \text { SCC } \\ & \text { Band } \end{aligned}$ | $\underset{(\mathrm{MHz})}{\mathrm{SCCBW}}$ | $\begin{gathered} \mathrm{ScC} \\ (\mathrm{DL}) \mathrm{CH} . \end{gathered}$ | $\underset{\substack{\operatorname{SCC}(\mathrm{DL}) \\ \text { Freq. (MHz) }}}{\text { ( }}$ | $\begin{aligned} & \text { LTE Tx. Power with } \\ & \text { DL CA Enabled } \\ & (\mathrm{dBm}) \end{aligned}$ | LTE Single Carrier Tx. Power $(\mathrm{dBm})$ |
| CA_4A-7A (0) | LTE B7 | 20 | 21100 | 2535.0 | QPSK | 1 | 50 | 3100 | 2655.0 | LTE B4 | 10 | 2175 | 2132.5 | 23.13 | 23.29 |
| CA_4A-7A (1) | LTE B7 | 20 | 21100 | 2535.0 | QPSK | 1 | 50 | 3100 | 2655.0 | LTE B4 | 20 | 2175 | 2132.5 | 23.15 | 23.29 |
| CA_5A-7A (0) | LTE B7 | 20 | 21100 | 2535.0 | QPSK | 1 | 50 | 3100 | 2655.0 | LTE B5 | 10 | 2525 | 881.5 | 23.12 | 23.29 |
| CA_5A-7A (1) | LTE B7 | 20 | 21100 | 2535.0 | QPSK | 1 | 50 | 3100 | 2655.0 | LTE B5 | 10 | 2525 | 881.5 | 23.12 | 23.29 |
| CA_7A-7A (0) | LTE B7 | 20 | 21100 | 2535.0 | QPSK | 1 | 50 | 3100 | 2655.0 | LTE B7 | 20 | 3350 | 2680.0 | 23.11 | 23.29 |
| CA_7A-7A (1) | LTE B7 | 20 | 21100 | 2535.0 | QPSK | 1 | 50 | 3100 | 2655.0 | LTE B7 | 20 | 3350 | 2680.0 | 23.11 | 23.29 |
| CA_7A-7A (2) | LTE B7 | 20 | 21100 | 2535.0 | QPSK | 1 | 50 | 3100 | 2655.0 | LTE B7 | 10 | 3400 | 2685.0 | 23.10 | 23.29 |
| CA_7A-7A (3) | LTE B7 | 20 | 21100 | 2535.0 | QPSK | 1 | 50 | 3100 | 2655.0 | LTE B7 | 20 | 3350 | 2680.0 | 23.11 | 23.29 |
| CA_7C (0) | LTE B7 | 20 | 21100 | 2535.0 | QPSK | 1 | 50 | 3100 | 2655.0 | LTE B7 | 20 | 3298 | 2674.8 | 23.14 | 23.29 |
| CA_7C (1) | LTE B7 | 20 | 21100 | 2535.0 | QPSK | 1 | 50 | 3100 | 2655.0 | LTE B7 | 20 | 3298 | 2674.8 | 23.14 | 23.29 |
| CA_7C (2) | LTE B7 | 20 | 21100 | 2535.0 | QPSK | 1 | 50 | 3100 | 2655.0 | LTE B7 | 20 | 3298 | 2674.8 | 23.14 | 23.29 |

Table F.3.6 LTE Band 66 as PCC

| PCC |  |  |  |  |  |  |  |  |  | SCC |  |  |  | Power |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Combination | PCC Band | $\begin{gathered} \text { PCC BW } \\ (\mathrm{MHz}) \\ \hline \end{gathered}$ | $\begin{gathered} \text { PCC } \\ \text { (ULL) CH. } \end{gathered}$ | $\begin{gathered} \hline \text { PCC (UL) } \\ \text { Freq. (MHz) } \\ \hline \end{gathered}$ | Mod. | $\begin{gathered} \text { PCC } \\ \text { UL\# RB } \end{gathered}$ | $\begin{aligned} & \text { PCC UL } \\ & \text { RB Offset } \end{aligned}$ | $\begin{aligned} & \mathrm{PCC}(\mathrm{DL}) \\ & \mathrm{CH} . \end{aligned}$ | $\begin{gathered} \hline \text { PCC (DL) } \\ \text { Freq. (MHz) } \\ \hline \end{gathered}$ | SCC Band | $\begin{gathered} \mathrm{SCCBW} \\ (\mathrm{MHz}) \end{gathered}$ | $\begin{gathered} \mathrm{SCC}(\mathrm{DL}) \\ \mathrm{CH} . \end{gathered}$ | $\begin{gathered} \text { SCC (DL) } \\ \text { Freq. (MHz) } \\ \hline \end{gathered}$ | LTE Tx. Power with DL CA Enabled (dBm) | $\begin{gathered} \text { LTE } \\ \text { Single Carrier } \\ \text { Tx. Power (dBm) } \end{gathered}$ |
| CA_66A-66A (0) | LTE B66 | 20 | 132572 | 1770.0 | QPSK | 1 | 50 | 67036 | 2170.0 | LTE B66 | 20 | 66536 | 2120.0 | 23.36 | 23.51 |
| CA_66B (0) | LTE B66 | 15 | 132597 | 1772.5 | QPSK | 1 | 36 | 67061 | 2172.5 | LTE B66 | 5 | 66968 | 2163.2 | 23.22 | 23.41 |
| CA_66C (0) | LTE B66 | 20 | 132572 | 1770.0 | QPSK | 1 | 50 | 67036 | 2170.0 | LTE B66 | 20 | 66838 | 2150.2 | 23.34 | 23.51 |

1. The device only supports downlink Carrier Aggregation. Uplink Carrier Aggregation is not supported. The DL carrier aggregation powers were measured according to the April 2018 TCB Workshop Notes (LTE Carrier Aggregation). Per Fall 2017 TCB Workshop Notes (LTE Carrier Aggregation) and FCC KDB Publication 941225 D05Av01r02, no further power measurements and SAR measurements are required for DL carrier aggregation configurations when the average output power with downlink only carrier aggregation active is not more than 0.25 dB higher than the average output power with downlink only carrier aggregation inactive.
2. For downlink carrier aggregation combinations, PCC uplink channel was selected based on section C.3)b)ii) of KDB 941225 D05Av01r02.


Figure E.3.1 DL 4CA Power Measurement Setup

## APPENDIX F. - Description of Test Equipment

## F. 1 SAR Measurement Setup

Measurements are performed using the DASY5 automated dosimetric assessment system. The DASY5 is made by Schmid \& Partner Engineering AG (SPEAG) in Zurich, Switzerland and consists of high precision robotics system (Staubli), robot controller, desktop computer, near-field probe, probe alignment sensor, and the generic twin phantom containing the brain equivalent material. The robot is a six-axis industrial robot performing precise movements to position the probe to the location (points) of maximum electromagnetic field (EMF) (see Fig. F.1.1).

A cell controller system contains the power supply, robot controller each pendant (Joystick), and a remote control used to drive the robot motors. The PC consists of the Intel Core i7-3770 3.40 GHz desktop computer with Windows 7 system and SAR Measurement Software DASY5,A/D interface card, monitor, mouse, and keyboard. The Staubli Robotis connected to the cell controller to allow software manipulation of the robot. A data acquisition electronic (DAE) circuit that performs the signal amplification, signal multiplexing, AD-conversion, offset measurements, mechanical surface detection, collision detection, etc. is connected to the Electro-optical coupler (EOC). The EOC performs the conversion from the optical into digital electric signal of the DAE and transfers data to the PC plug-in card.


Figure F.1.1 SAR Measurement System Setup

The DAE4 consists of a highly sensitive electrometer-grade preamplifier with auto-zeroing, a channel and gain-switching multiplexer, a fast 16 bit AD-converter and a command decoder and control logic unit. Transmission to the PC-card is accomplished through an optical downlink for data and status information and an optical uplink for commands and clock lines. The mechanical probe mounting device includes two different sensor systems for frontal and sidewise probe contacts. They are also used for mechanical surface detection and probe collision detection. The robot uses its own controller with a built in VME-bus computer. The system is described in detail.

## F. 2 Probe Specification



Figure F.2.2 Probe Thick-Film Technique


The SAR measurements were conducted with the dosimetric probe EX3DV4 designed in the classical triangular configuration(see F.2.1) and optimized for dosimetric evaluation. The probe is constructed using the thick film technique; with printed resistive lines on ceramic substrates. The probe is equipped with an optical multitier line ending at the front of the probe tip. It is connected to the EOC box on the robot arm and provides an automatic detection of the phantom surface. Half of the fibers are connected to a pulsed infrared transmitter, the other half to a synchronized receiver. As the probe approaches the surface, the reflection from the surface produces a coupling from the transmitting to the receiving fibers. This reflection increases first during the approach, reaches maximum and then decreases. If the probe is flatly touching the surface, the coupling is zero. The distance of the coupling maximum to the surface is independent of the surface reflectivity and largely independent of the surface to probe angle. The DASY5 software reads the reflection during a software approach and looks for the maximum using a 2 nd order fitting. The approach is stopped at reaching the maximum.

DAE System

## F. 3 E-Probe Calibration Process

## Dosimetric Assessment Procedure

Each probe is calibrated according to a dosimetric assessment procedure with accuracy better than $+/-10 \%$. The spherical isotropy was evaluated with the procedure and found to be better than $+/-0.25 \mathrm{~dB}$. The sensitivity parameters (Norm X, Norm Y, Norm Z), the diode compression parameter (DCP) and the conversion factor (Conv $F$ ) of the probe is tested.

## Free Space Assessment

The free space E-field from amplified probe outputs is determined in a test chamber. This is performed in a TEM cell for frequencies below 1 GHz , and in a waveguide above 1 GHz for free space. For the free space calibration, the probe is placed in the volumetric center of the cavity at the proper orientation with the field. The probe is then rotated 360 degrees.

## Temperature Assessment *

E-field temperature correlation calibration is performed in a flat phantom filled with the appropriate simulated brain tissue. The measured free space E-field in the medium, correlates to temperature rise in a dielectric medium. For temperature correlation calibration a RF transparent the remits or based temperature probe is used in conjunction with the E-field probe.

$$
\mathrm{SAR}=C \frac{\Delta \mathrm{~T}}{\Delta t} \quad \operatorname{SAR}=\frac{|\mathrm{E}|^{2} \cdot \sigma}{\rho}
$$

where:
where:
$\Delta t=$ exposure time ( 30 seconds),
$\mathrm{C}=$ heat capacity of tissue (brain or muscle),
$\sigma=$ simulated tissue conductivity,
$\rho=$ Tissue density ( $1.25 \mathrm{~g} / \mathrm{cm}^{3}$ for brain tissue)
$\Delta \mathrm{T}=$ temperature increase due to RF exposure.
SAR is proportional to $\Delta T$ / $\Delta t$, the initial rate of tissue heating, before thermal diffusion takes place. Now it's possible to quantify the electric field in the simulated tissue by equating the thermally derived SAR to the E-field;


Figure F.3.1 E-Field and Temperature Measurements at 900 MHz


Figure F.3.2 E-Field and Temperature Measurements at 1800 MHz

## F. 4 Data Extrapolation

The DASY5 software automatically executes the following procedures to calculate the field units from the microvolt readings at the probe connector. The first step of the evaluation is a linearization of the filtered input signal to account for the compression characteristics of the detector diode. The compensation depends on the input signal, the diode type and the DC-transmission factor from the diode to the evaluation electronics. If the exciting field is pulsed, the crest factor of the signal must be known to correctly compensate for peak power. The formula for each channel can be given like below;

$$
V_{i}=U_{i}+U_{i}^{2} \cdot \frac{c f}{d c p_{i}}
$$

with

$$
\begin{aligned}
& V_{i}=\text { compensated signal of channel } i \\
& U_{1}=\text { input signal of channel } i \\
& c f=c r e s t ~ f a c t o r ~ o f ~ e x c i t i n g ~ f i e l d ~ \\
& d c p_{1}=\text { diode compression point }
\end{aligned}
$$

( $\mathrm{i}=\mathrm{x}, \mathrm{y}, \mathrm{z}$ )
(i=x,y,z)
(DASY parameter)
(DASY parameter)

From the compensated input signals the primary field data for each channel can be evaluated:
E-field probes: $\quad$ with $V_{i} \quad=$ compensated signal of channel $i(i=x, y, z)$
$E_{i}=\sqrt{\frac{V_{i}}{\text { Norm }_{i} \cdot \operatorname{ConvF}}}$

Norm $_{i}=$ sensor sensitivity of channel $i \quad(i=x, y, z)$
$\mu \mathrm{V} /(\mathrm{V} / \mathrm{m})^{2}$ for E-field probes
ConvF $=$ sensitivity of enhancement in solution
$\mathbf{E}_{1} \quad=$ electric field strength of channel i in $\mathrm{V} / \mathrm{m}$

The RSS value of the field components gives the total field strength (Hermetian magnitude):

$$
E_{b t}=\sqrt{E_{x}^{2}+E_{y}^{2}+E_{x}^{2}}
$$

The primary field data are used to calculate the derived field units.

$$
S A R=E_{\text {bot }}^{2} \cdot \frac{\sigma}{\rho \cdot 1000} \quad \text { with } \quad \begin{array}{ll}
\text { SAR } & =\text { local specific absorption rate in } \mathrm{W} / \mathrm{g} \\
E_{\text {tot }} & =\text { total field strength in } \mathrm{V} / \mathrm{m} \\
\sigma & =\text { conductivity in [mho/m] or [Siemens } / \mathrm{m}] \\
\rho & =\text { equivalent tissue density in } \mathrm{g} / \mathrm{cm}^{3}
\end{array}
$$

The power flow density is calculated assuming the excitation field to be a free space field.

$$
P_{\text {fux }}=\frac{E_{b o t}^{2}}{3770} \quad \text { with } \quad \begin{aligned}
& \mathrm{P}_{\text {pue }} \\
& \mathrm{E}_{\mathrm{Lo}}
\end{aligned} \quad \begin{aligned}
& \text { = equivalent power density of a plane wave in } \mathrm{W} / \mathrm{cm}^{2} \\
& \text { = total electric field strength in } \mathrm{V} / \mathrm{m}
\end{aligned}
$$

## F. 5 SAM Twin Phantom

The SAM Twin Phantom V5.0 is constructed of a fiberglass shell integrated in a wooden table. The shape of the shell is based on data from an anatomical study designed to determine the maximum exposure in at least $90 \%$ of all users. It enables the dosimetric evaluation of left and right hand phone usage as well as body mounted usage at the flat phantom region. A cover prevents the evaporation of the liquid.

Reference markings on the Phantom allow the complete setup of all predefined phantom positions and measurement grids by manually teaching three points in the robot. (see Fig. F.5.1)


Figure F.5.1 SAM Twin Phantom

## SAM Twin Phantom Specification:

Construction

Shell Thickness
Filling Volume
Dimensions

The shell corresponds to the specifications of the Specific Anthropomorphic Mannequin (SAM) phantom defined in IEEE 1528 and IEC 62209-1. It enables the dosimetric evaluation of left and right hand phone usage as well as body mounted usage at the flat phantom region. A cover prevents evaporation of the liquid. Reference markings on the phantom allow the complete setup of all predefined phantom positions and measurement grids by teaching three points with the robot.
Twin SAM V5.0 has the same shell geometry and is manufactured from the same material as Twin SAM V4.0, but has reinforced top structure.
$2 \pm 0.2 \mathrm{~mm}$
Approx. 25 liters
Length: 1000 mm
Width: 500 mm
Height: adjustable feet

## Specific Anthropomorphic Mannequin (SAM) Specifications:

The phantom for handset SAR assessment testing is a low-loss dielectric shell, with shape and dimensions derived from the anthropometric data of the 90th percentile adult male head dimensions as tabulated by the US Army. The SAM Twin Phantom shell is bisected along the mid-sagittal plane into right and left halves (see Fig. F.5.2). The perimeter sidewalls of each phantom halves are extended to allow filling with liquid to a depth that is sufficient to minimized reflections from the upper surface. The liquid depth is maintained at a minimum depth of 15 cm to minimize reflections from the upper surface.


Figure F.5.2 Sam Twin Phantom shell

## F. 6 Device Holder for Transmitters

In combination with the Twin SAM Phantom V4.0/V4.0c, V5.0 or ELI4, the Mounting Device enables the rotation of the mounted transmitter device in spherical coordinates. Rotation point is the ear opening point. Transmitter devices can be easily and accurately positioned according to IEC, IEEE, FCC or other specifications. The device holder can be locked for positioning at different phantom sections (left head, right head, flat).
Note: A simulating human hand is not used due to the complex anatomical and geometrical structure of the hand that may produce infinite number of configurations. To produce the worst-case condition (the hand absorbs antenna output power), the hand is omitted during the tests.


Figure F.6.1 Mounting Device

## F. 7 Automated Test System Specifications

Positioner
Robot Stäubli Unimation Corp. Robot Model: TX90XL Repeatability 0.02 mm
No. of axis ..... 6
Data Acquisition Electronic (DAE) System
Cell Controller
Processor ..... Intel Core i7-3770Clock SpeedOperating System Windows 7 Professional3.40 GHzData CardDASY5 PC-Board
Data Converter
Features SAA, multiplexer, A/D converter. \& control logicSoftwareDASY5Connecting Lines
Optical downlink for data and status infoOptical uplink for commands and clock
PC Interface CardFunction
24 bit ( 64 MHz ) DSP for real time processing Link to DAE 4
16 bit $\mathrm{A} / \mathrm{D}$ converter for surface detection system
serial link to robot
direct emergency stop output for robot
E-Field Probes
Model EX3DV4 S/N: 3916/ EX3DV4 S/N: 3933Construction
FrequencyLinearityTriangular core fiber optic detection system10 MHz to 6 GHz$\pm 0.2 \mathrm{~dB}$ ( 30 MHz to 6 GHz )
Phantom

| Phantom | SAM Twin Phantom (V5.0) |
| :--- | :--- |
| Shell Material | Composite |
| Thickness | $2.0 \pm 0.2 \mathrm{~mm}$ |



Figure F.7.1 DASY5 Test System

