

FCC SAR EVALUATION REPORT

In accordance with the requirements of

FCC Report and Order: ET Docket 93-62, and OET Bulletin 65 Supplement C ANSI/IEEE Std. C95.1-1992

For

Ultra Low Power 802.11b/g/n Module

MODEL: RS9110-N-11-02

Trade Name: LiteFi

Prepared for

Redpine Signals Inc

2107 N.first Street, Suite 680, San Jose, CA95131-2019

Prepared by

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1. EUT DESCRIPTION

Applicant:	Redpine Signals Inc	Redpine Signals Inc				
	2107 N.first Street, Suite 680	2107 N.first Street, Suite 680, San Jose, CA95131-2019				
Equipment Under T	est: Ultra Low Power 802.11b/g/	Ultra Low Power 802.11b/g/n Module				
Trade Name:	LiteFi					
Model Number:	RS9110-N-11-02					
Device Category:	PORTABLE DEVICES					
Exposure Category:	GENERAL POPULATION/L	GENERAL POPULATION/UNCONTROLLED EXPOSURE				
Report Number:	SZ090401B04	SZ090401B04				
Date of Test:	July 24, 2009	July 24, 2009				
Test Sample is a:	Production unit					
Modulation Type:	DSSS/OFDM					
Operating Mode:	Maximum continuous output					
Frequency Range: Max. O/P Power: (Conducted) Max. SAR (1g):	2412MHz~2462MHz 12.36dBm (2437MHz B Mode) 10.51dBm (2462MHz G Mode) 10.62dBm (2462MHz HT20n Mode) 0.679W/kg (2412MHz B Mode) 0.664W/kg(2412MHz G Mode) 0.706 W/kg(2412MHz HT20n Mode)					

Application Type:

 APPLICABLE STANDARDS

 STANDARD
 TEST RESULT

 FCC OET 65 Supplement C
 No non-compliance noted

 Deviation from Applicable Standard
 None

The above wireless portable device was tested by Compliance Certification Services Inc. in accordance with the measurement methods and procedures specified in OET Bulletin 65 Supplement C(Edition 01-01). The test results in this report apply only to the tested sample of the stated device/equipment. Other similar device/equipment will not necessarily produce the same results due to production tolerance and measurement uncertainties.

Approved by:

Certification

Miro Chueh EMC Manager Compliance Certification Services Inc. Reviewed by:

Lin Zhang EMC Section Manager Compliance Certification Services Inc.



2. REQUIREMENTS FOR COMPLIANCE TESTING DEFINED BY THE FCC

The US Federal Communications Commission has released the report and order "Guidelines for Evaluating the Environmental Effects of RF Radiation", ET Docket No. 93-62 in August 1996. The order requires routine SAR evaluation prior to equipment authorization of portable transmitter devices, including portable telephones. For consumer products, the applicable limit is 1.6 mW/g for an uncontrolled environment and 8.0 mW/g for an occupational/controlled environment as recommended by the ANSI/IEEE standard C95.1-1992. According to the Supplement C of OET Bulletin 65 "Evaluating Compliance with FCC Guide-lines for Human Exposure to Radio frequency Electromagnetic Fields", released on Jun 29, 2001 by the FCC, the device should be evaluated at maximum output power (radiated from the antenna) under "worst-case" conditions for normal or intended use, incorporating normal antenna operating positions, device peak performance frequencies and positions for maximum RF energy coupling.

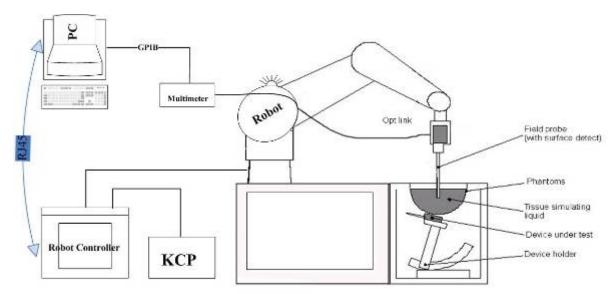
3. DOSIMETRIC ASSESSMENT SYSTEM

These measurements were performed with the automated near-field scanning system OPENSAR from ANTENNESSA. The system is based on a high precision robot (working range greater than 0.9 m), which positions the probes with a positional repeatability of better than \pm 0.02 mm. Special E- and H-field probes have been developed for measurements close to material discontinuity, the sensors of which are directly loaded with a Schottky diode and connected via highly resistive lines to the data acquisition unit. The SAR measurements were conducted with the dosimetric probe EP74 SN0807 (manufactured by ANTENNESSA), designed in the classical triangular configuration and optimized for dosimetric evaluation. The probe has been calibrated according to the procedure described in [7] with accuracy of better than \pm 10%. The spherical isotropy was evaluated with the procedure described in [8] and found to be better than \pm 0.25 dB. The phantom used was the SAM Phantom as described in FCC supplement C, IEE P1528 and CENELEC EN50361.

Ingredients	Frequency (MHz)									
(% by weight)	% by weight) 450		835		915		1900		2450	
Tissue Type	Head	Body	Head	Body	Head	Body	Head	Body	Head	Body
Water	38.56	51.16	41.45	52.4	41.05	56.0	54.9	40.4	62.7	73.2
Salt (NaCl)	3.95	1.49	1.45	1.4	1.35	0.76	0.18	0.5	0.5	0.04
Sugar	56.32	46.78	56.0	45.0	56.5	41.76	0.0	58.0	0.0	0.0
HEC	0.98	0.52	1.0	1.0	1.0	1.21	0.0	1.0	0.0	0.0
Bactericide	0.19	0.05	0.1	0.1	0.1	0.27	0.0	0.1	0.0	0.0
Triton X-100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	36.8	0.0
DGBE	0.0	0.0	0.0	0.0	0.0	0.0	44.92	0.0	0.0	26.7
Dielectric Constant	43.42	58.0	42.54	56.1	42.0	56.8	39.9	54.0	39.8	52.5
Conductivity (S/m)	0.85	0.83	0.91	0.95	1.0	1.07	1.42	1.45	1.88	1.78

The Tissue simulation liquid used for each test is in according with the FCC OET65 supplement C as listed below.

3.1 MEASUREMENT SYSTEM DIAGRAM



The OPENSAR system for performing compliance tests consist of the following items:

- 1. A standard high precision 6-axis robot (KUKA) with controller and software.
- 2. KUKA Control Panel (KCP).
- 3. A dosimetric probe, i.e., an isotropic E-field probe optimized and calibrated for usage in tissue simulating liquid. The probe is equipped with an optical surface detector system.
- 4. The functions of the PC plug-in card are to perform the time critical task such as signal filtering, surveillance of the robot operation fast movement interrupts.
- 5. A computer operating Windows 95.
- 6. OPENSAR software.
- 7. Remote control with teaches pendant and additional circuitry for robot safety such as warning lamps, etc.
- 8. The SAM phantom enabling testing left-hand right-hand and body usage.
- 9. The Position device for handheld EUT.
- 10. Tissue simulating liquid mixed according to the given recipes (see Application Note).
- 11. System validation dipoles to validate the proper functioning of the system.

3.2 SYSTEM COMPONENTS

SN11/09 EP100 Probe Specification

Construction Symmetrical design with triangular core Built-in optical fiber for surface detection System Built-in shielding against static charges Calibration in air from 100 MHz to 2.5 GHz In brain and muscle simulating tissue at frequencies of 835 MHz, 897MHz ,1747 MHz,1880 MHz,1950 MHz and 1.8 GHz (accuracy of \pm 8%) Frequency 100 MHz to > 30GHz; Linearity: \pm 0.25 dB (100 MHz to 30 GHz) Directivity \pm 0.25 dB in brain tissue (rotation around probe axis)

 \pm 0.5 dB in brain tissue (rotation normal probe axis)

Dynamic 5 mW/g to > 100 mW/g;

Range Linearity: ± 0.25 dB

Surface ± 0.2 mm repeatability in air and clear liquids

Detection over diffuse reflecting surfaces

Dimensions Overall length: 330 mm

Tip length: 16 mm

Body diameter: 8 mm

Tip diameter: 6.5 mm

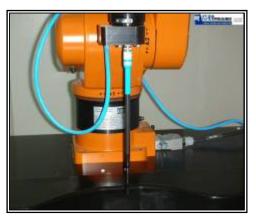
Distance from probe tip to dipole centers: <2.7 mm

Application General dosimetric up to 3 GHz

Compliance tests of mobile phones

Fast automatic scanning in arbitrary phantoms

The SAR measurements were conducted with the dosimetric probe <u>SN11/09 EP100</u> designed in the classical triangular configuration and optimized for dosimetric evaluation. The probe is constructed using the thick film technique, with printed resistive lines on ceramic substrates. The probe is equipped with an optical multi-fiber line ending at the front of the probe tip. It is connected to the KRC box on the robot arm and provides an



Photograph of the Probe



Inside View of <u>SN11/09 EP100</u> E-field

automatic detection of the phantom surface. Half of the fibers are connected to a pulsed infrared transmitter, the other half to a synchronized receiver. As the probe approaches the surface, the reflection from the surface produces a coupling from the transmitting to the receiving fibers. This reflection increases first during the approach, reaches maximum and then decreases. If the probe is flatly touching the surface, the coupling is zero. The distance of the coupling maximum to the surface is independent of the surface reflectivity and largely independent of the surface to probe angle. The OPENSAR software reads the reflection during a software approach and looks for the maximum using a 2nd order fitting. The approach is stopped when reaching the maximum.

E-Field Probe Calibration Process

Each probe is calibrated according to a dosimetric assessment procedure described in [6] with accuracy better than +/- 10%. The spherical isotropy was evaluated with the procedure described in [7] and found to be better than +/-0.25dB. The sensitivity parameters (NormX, NormY, NormZ), the diode compression parameter (DCP) and the conversion factor (ConvF) of the probe are tested.

The free space E-field from amplified probe outputs is determined in a test chamber. This is performed in a TEM cell for frequencies bellow 1 GHz, and in a waveguide above 1 GHz for free space. For the free space calibration, the probe is placed in the volumetric center of the cavity and at the proper orientation with the field. The probe is then rotated 360 degrees.

E-field temperature correlation calibration is performed in a flat phantom filled with the appropriate simulated brain tissue. The measured free space E-field in the medium correlates to temperature rise in dielectric medium. For temperature correlation calibration a RF

transparent thermistor-based temperature probe is used in conjunction with the E-field probe.

SAM Phantom

The SAM Phantom SAM29 is constructed of a fiberglass shell integrated in a wooden table. The shape of the shell is in compliance with the specification set in IEEE P1528 and CENELEC EN50361. The phantom enables the dosimetric evaluation of left and right hand phone usage as well as body mounted usage at the flat phantom region. A cover prevents the evaporation of the liquid. Reference markings on the Phantom allow the complete setup of all predefined phantom positions and measurement grids by manually teaching three points in the robot.

Shell Thickness: 2 ± 0.2 mm Filling Volume: Approx. 25 liters Dimensions (H x L x W): 810 x 1000 x 500 mm

Device Holder for Transmitters

In combination with the Generic Twin Phantom V3.0, the Mounting Device enables the rotation of the mounted transmitter in spherical coordinates whereby the rotation points is the ear opening. The devices can be easily, accurately, and repeatedly positioned according to the FCC and CENELEC specifications. The device holder can be locked at different phantom locations (left head, right head, flat phantom).

Note: A simulating human hand is not used due to the complex anatomical and geometrical structure of the hand that may produced infinite number of configurations [10]. To produce the worst-case condition (the hand absorbs antenna output power), the hand is omitted during the tests.



SAM Phantom





4.1 DATA EVALUATION

The OPENSAR software automatically executes the following procedure to calculate the field units from the microvolt readings at the probe connector. The parameters used in the evaluation are stored in the configuration modules of the software:

Probe parameters:	- Sensitivity	Norm _i , a_{i10} , a_{i11} , a_{i12}
	- Conversion factor	ConvFi
	- Diode compression point	Dcpi
Device parameters:	- Frequency	f
	- Crest factor	cf
Media parameters:	- Conductivity	σ
	- Density	ρ

These parameters must be set correctly in the software. They can either be found in the component documents or be imported into the software from the configuration files issued for the OPENSAR components. In the direct measuring mode of the multi-meter option, the parameters of the actual system setup are used. In the scan visualization and export modes, the parameters stored in the corresponding document files are used.

The first step of the evaluation is a linearization of the filtered input signal to account for the compression characteristics of the detector diode. The compensation depends on the input signal, the diode type and the DC-transmission factor from the diode to the evaluation electronics. If the exciting field is pulsed, the crest factor of the signal must be known to correctly compensate for peak power. The formula for each channel can be given as:

$$V_{i} = U_{i} + U_{i}^{2} \cdot \frac{cf}{dcp_{i}}$$
Where $V_{i} = Compensated signal of channel i$ $(i = x, y, z)$
 $U_{i} = Input signal of channel i$ $(i = x, y, z)$
 $cf = Crest factor of exciting field$ (ANTENNESSA parameter)
 $dcp_{i} = Diode compression point$ (ANTENNESSA parameter)

From the compensated input signals the primary field data for each channel can be evaluated:

$$E\text{-field probes:} \qquad E_i = \sqrt{\frac{V_i}{Norm_i \cdot ConvF}}$$

$$H\text{-field probes:} \qquad H_i = \sqrt{Vi} \cdot \frac{a_{i10} + a_{i11}f + a_{i12}f^2}{f}$$

$$Where \quad V_i \qquad = Compensated \ signal \ of \ channel \ i \ (i = x, \ y, \ z)$$

$$Norm_i = Sensor \ sensitivity \ of \ channel \ i \ (i = x, \ y, \ z)$$

$$\mu V/(V/m)2 \ for \ E0 \ field \ Probes$$

$$ConvF = Sensitivity \ enhancement \ in \ solution$$

$$a_{ij} \qquad = Sensor \ sensitivity \ factors \ for \ H\text{-field probes}$$



f = Carrier frequency (GHz) $E_i = Electric field strength of channel i in V/m$ $H_i = Magnetic field strength of channel i in A/m$

The RSS value of the field components gives the total field strength (Hermitian magnitude):

 $E_{tot} = \sqrt{E_x^2 + E_y^2 + E_z^2}$

The primary field data are used to calculate the derived field units.

$$SAR = E_{tot}^{2} \cdot \frac{\sigma}{\rho \cdot 1000}$$
where $SAR = local specific absorption rate in mW/g$

$$E_{tot} = total field strength in V/m$$

$$\sigma = conductivity in [mho/m] or [siemens/m]$$

$$\rho = equivalent tissue density in g/cm3$$

Note that the density is normally set to 1 (or 1.06), to account for actual brain density rather than the density of the simulation liquid.

The power flow density is calculated assuming the excitation field as a free space field.

$$P_{pwe} = \frac{E_{tot}^{2}}{3770} \quad or \quad P_{pwe} = H_{tot}^{2} \cdot 37.7$$
where $P_{pwe} = Equivalent \text{ power density of a plane wave in mW/cm2}$

$$E_{tot} = total \text{ electric field strength in V/m}$$

$$H_{tot} = total \text{ magnetic field strength in A/m}$$

4.2 SAR EVALUATION PROCEDURES

The procedure for assessing the peak spatial-average SAR value consists of the following steps:

• Power Reference Measurement

The reference and drift jobs are useful jobs for monitoring the power drift of the device under test in the batch process. Both jobs measure the field at a specified reference position, at a selectable distance from the phantom surface. The reference position can be either the selected section's grid reference point or a user point in this section. The reference job projects the selected point onto the phantom surface, orients the probe perpendicularly to the surface, and approaches the surface using the selected detection method.

• Area Scan

The area scan is used as a fast scan in two dimensions to find the area of high field values, before doing a finer measurement around the hot spot. The sophisticated interpolation routines implemented in OPENSAR software can find the maximum locations even in relatively coarse grids. The scan area is defined by an editable grid. This grid is anchored at the grid reference point of the selected section in the phantom. When the area scan's property sheet is brought-up, grid was at to 15 mm by 15 mm and can be edited by a user.

Zoom Scan

Zoom scans are used to assess the peak spatial SAR values within a cubic averaging volume containing 1 g and 10 g of simulated tissue. The default zoom scan measures $5 \times 5 \times 7$ points within a cube whose base faces are centered around the maximum found in a preceding area scan job within the same procedure. If the preceding Area Scan job indicates more then one maximum, the number of Zoom Scans has to be enlarged accordingly (The default number inserted is 1).

• Power Drift measurement

The drift job measures the field at the same location as the most recent reference job within the same procedure, and with the same settings. The drift measurement gives the field difference in dB from the reading conducted within the last reference measurement. Several drift measurements are possible for one reference measurement. This allows a user to monitor the power drift of the device under test within a batch process. In the properties of the Drift job, the user can specify a limit for the drift and have OPENSAR software stop the measurements if this limit is exceeded.

4.3 SPATIAL PEAK SAR EVALUATION

The procedure for spatial peak SAR evaluation has been implemented according to the IEEE1529 standard. It can be conducted for 1 g and 10 g.

The OPENSAR system allows evaluations that combine measured data and robot positions, such as:

- maximum search
- extrapolation
- boundary correction
- peak search for averaged SAR

During a maximum search, global and local maximum searches are automatically performed in 2-D after each Area Scan measurement with at least 6 measurement points. It is based on the evaluation of the local SAR gradient calculated by the Quadratic Shepard's method. The algorithm will find the global maximum and all local maxima within -2 dB of the global maxima for all SAR distributions.

Extrapolation

Extrapolation routines are used to obtain SAR values between the lowest measurement points and the inner phantom surface. The extrapolation distance is determined by the surface detection distance and the probe sensor offset. Several measurements at different distances are necessary for the extrapolation.

Extrapolation routines require at least 10 measurement points in 3-D space. They are used in the Cube Scan to obtain SAR values between the lowest measurement points and the inner phantom surface. The routine uses the modified Quadratic Shepard's method for extrapolation. For a grid using 5x5x7 measurement points with 5mm resolution amounting to 343 measurement points, the uncertainty of the extrapolation routines is less than 1% for 1 g and 10 g cubes.

Boundary effect

For measurements in the immediate vicinity of a phantom surface, the field coupling effects between the probe and the boundary influence the probe characteristics. Boundary effect errors of different dosimetric probe types have been analyzed by measurements and using a numerical probe model. As expected, both methods showed an enhanced sensitivity in the immediate vicinity of the boundary. The effect strongly depends on the probe dimensions and disappears with increasing distance from the boundary. The sensitivity can be approximately given as:

$$S \approx S_o + S_b exp(-\frac{z}{a})cos(\pi \frac{z}{\lambda})$$

Since the decay of the boundary effect dominates for small probes ($a << \lambda$), the cos-term can be omitted. Factors *Sb* (parameter Alpha in the OPENSAR software) and *a* (parameter Delta in the OPENSAR software) are assessed during probe calibration and used for numerical compensation of the boundary effect. Several simulations and measurements have confirmed that the compensation is valid for different field and boundary configurations.

This simple compensation procedure can largely reduce the probe uncertainty near boundaries. It works well as long as:

- the boundary curvature is small
- the probe axis is angled less than 30_ to the boundary normal
- the distance between probe and boundary is larger than 25% of the probe diameter
- the probe is symmetric (all sensors have the same offset from the probe tip)

Since all of these requirements are fulfilled in a OPENSAR system, the correction of the probe boundary effect in the vicinity of the phantom surface is performed in a fully automated manner via the measurement data extraction during postprocessing.

5. MEASUREMENT UNCERTAINTY

UNCERTAINTY EVALUATION FOR HANDSET SAR TEST

а	Ь	с	d	e= f(d,k)	f	g	h= cxf/e	i= cxg/e	k
Uncertainty Component	Sec.	Tol. (± %)	Prob. Dist.	Div.	c _i (1 g)	c _i (10 g)	1 g u _i (± %)	10 g u _i (± %)	Vi
Measurement System	1								
Probe Calibration	E.2.1.	7	N	1	1	1	7	7	
Axial Isotropy	E.2.2.	2,5	R	√3	$(1-c_p)^{1/2}$	$(1-c_p)^{1/2}$	1.02062	1,02062	
Hemispherical Isotropy	E.2.2.	4	R	√3	√Cp	√C _p		1,63299	
Boundary Effect	E.2.3.	1	R	√3	1	1		0,57735	
Linearity	E.2.4.	5	R	√3	1	1		2,88675	
System Detection Limits	E.2.5.	1	R	√3	1	1		0,57735	
Readout Electronics	E.2.6.	0,02	N	1	1	1	0,02		
Response Time	E.2.7.	3	R	√3	1	1		1,73205	
Integration Time	E.2.8.	2	R	√3	1	1	1,1547		
RF Ambient Conditions	E.6.1.	3	R	√3	1	1	· ·	1,73205	
Probe Positioner Mechanical									
Tolerance	E.6.2.	2	R	√3	1	1	1,1547	1,1547	œ
Probe Positioning with respect to									
Phantom Shell	E.6.3.	0,05	R	√3	1	1	0,02887	0,02887	œ
Extrapolation, interpolation and									
Integration Algorithms for Max. SAR									
Evaluation	E.5.2.	5	R	√3	1	1	2,88675	2,88675	œ
Test sample Related									
Test Sample Positioning	E.4.2.1.	0,03	N	1	1	1	0,03		
Device Holder Uncertainty	E.4.1.1.	5	N	1	1	1	5	5	N-1
Output Power Variation - SAR drift									
measurement	6.6.2.	3	R	√3	1	1	1,73205	1,73205	œ
Phantom and Tissue Parameters									
Phantom Uncertainty (shape and									
thickness tolerances)	E.3.1.	0,05	R	√3	1	1	0,02887	0,02887	œ
Liquid Conductivity - deviation from				.					
target values	E.3.2.	5	R	√3	0,64	0,43	1,84752	1,2413	œ
Liquid Conductivity - measurement		_							
uncertainty	E.3.3.	5	N	1	0,64	0,43	3,2	2,15	М
Liquid Permittivity - deviation from		-	_	-			1.000000		
target values	E.3.2.	3	R	√3	0,6	0,49	1,03923	0,8487	00
Liquid Permittivity - measurement							-		
uncertainty	E.3.3.	10	N	1	0,6	0,49	6	4,9	M
Combined Standard Uncertainty			000				11 1005	10 5700	
Combined Standard Uncertainty Expanded Uncertainty			RSS				11,1205	10,5799	
(95% CONFIDENCE INTERVAL)			k				21 8079	20,7366	
			n I				21,0013	20,7000	



Whole-Body	Partial-Body	Hands, Wrists, Feet and Ankles
0.4	8.0	20.0

(B). Limits for General Population/Uncontrolled Exposure (W/kg)

Whole-Body	Partial-Body	Hands, Wrists, Feet and Ankles
0.08	1.6	4.0

Note: Whole-Body SAR is averaged over the entire body, partial-body SAR is averaged over any 1 gram of tissue defined as a tissue volume in the shape of a cube. SAR for hands, wrists, feet and ankles is averaged over any 1 grams of tissue defined as a tissue volume in the shape of a cube.

<u>Population/Uncontrolled Environments</u> are defined as locations where there is the exposure of individuals who have no knowledge or control of their exposure.

<u>Occupational/Controlled Environments</u> are defined as locations where there is exposure that may be incurred by people who are aware of the potential for exposure, (i.e. as a result of employment or occupation).

NOTE

GENERAL POPULATION/UNCONTROLLED EXPOSURE PARTIAL BODY LIMIT

1.6 W/kg

7. EUT ARRANGEMENT

Please refer to IEEE P1528 illustration below.

The EUT was connected to base station simulator to meet the test parameter required by IEEE P1528.

7.1 ANTHROPOMORPHIC HEAD PHANTOM

Figure 7-1a shows the front, back and side views of SAM. The point "M" is the reference point for the center of mouth, "LE" is the left ear reference point (ERP), and "RE" is the right ERP. The ERPs are 15 mm posterior to the entrance to ear canal (EEC) along the B-M line (Back-Mouth), as shown in Figure 7-1b. The plane passing through the two ear reference points and M is defined as the Reference Plane. The line N-F (Neck-Front) perpendicular to the reference plane and passing through the RE (or LE) is called the Reference Pivoting Line (see Figure 7-1c). Line B-M is perpendicular to the N-F line. Both N-F and B-M lines should be marked on the external phantom shell to facilitate handset positioning. Posterior to the N-F line, the thickness of the phantom shell with the shape of an ear is a flat surface 6 mm thick at the ERPs. Anterior to the N-F line, the ear is truncated as illustrated in Figure 7-1b. The ear truncation is introduced to avoid the handset from touching the ear lobe, which can cause unstable handset positioning at the cheek.

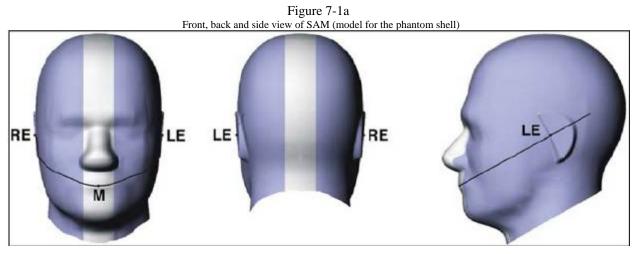
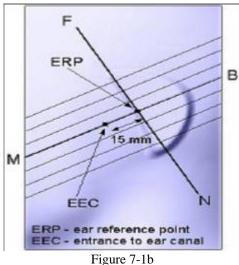


Figure 7-1b Close up side view of phantom showing the ear region



Close up side view of phantom showing the ear region

Figure 7-1c Side view of the phantom showing relevant markings and the 7 cross sectional plane locations

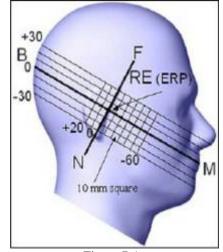


Figure 7-1c Side view of the phantom showing relevant markings and the 7 cross sectional plane locations

DEFINITION OF THE "CHEEK/TOUCH" POSITION

The "cheek" or "touch" position is defined as follows:

- a. Ready the handset for talk operation, if necessary. For example, for handsets with a cover piece, open the cover. (If the handset can also be used with the cover closed both configurations must be tested.)
- b. Define two imaginary lines on the handset: the vertical centerline and the horizontal line. The vertical centerline passes through two points on the front side of the handset: the midpoint of the width wt of the handset at the level of the acoustic output (point A on Figures 7-2a and 7-2b), and the midpoint of the width wb of the bottom of the handset (point B). The horizontal line is perpendicular to the vertical centerline and passes through the center of the acoustic output (see Figure 7-2a). The two lines intersect at point A. Note that for many handsets, point A coincides with the center of the acoustic output. However, the acoustic output may be located elsewhere on the horizontal line. Also note that the vertical centerline is not necessarily parallel to the front face of the handset (see Figure 7-2b), especially for clamshell handsets, handsets with flip pieces, and other irregularly-shaped handsets.
- c. Position the handset close to the surface of the phantom such that point A is on the (virtual) extension of the line passing through points RE and LE on the phantom (see Figure 7-2c), such that the plane defined by the vertical center line and the horizontal line of the handset is approximately parallel to the sagittal plane of the phantom.
- d. Translate the handset towards the phantom along the line passing through RE and LE until the handset touches the pinna.
- e. e) While maintaining the handset in this plane, rotate it around the LE-RE line until the vertical centerline is in the plane normal to MB-NF including the line MB (called the reference plane).
- f. Rotate the handset around the vertical centerline until the handset (horizontal line) is symmetrical with respect to the line NF.
- g. While maintaining the vertical centerline in the reference plane, keeping point A on the line passing through RE and LE and maintaining the handset contact with the pinna, rotate the handset about the line NF until any point on the handset is in contact with a phantom point below the pinna (cheek). See Figure 7-2c. The physical angles of rotation should be noted.

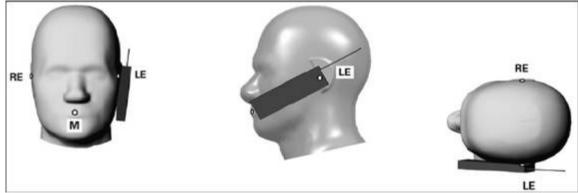
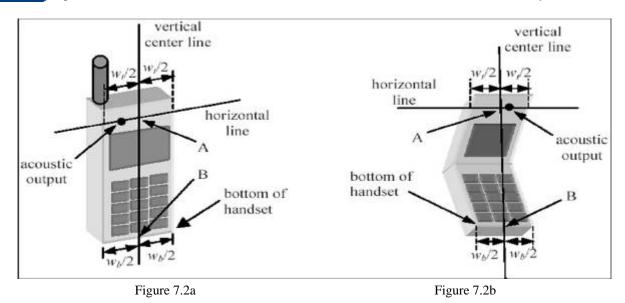


Figure 7.2c

Phone "cheek" or "touch" position. The reference points for the right ear (RE), left ear (LE) and mouth (M), which define the reference plane for handset positioning, are indicated.



DEFINITION OF THE "TILTED" POSITION

The "tilted" position is defined as follows:

- a. Repeat steps (a) (g) of 7.2 to place the device in the "cheek position."
- b. While maintaining the orientation of the handset move the handset away from the pinna along the line passing through RE and LE in order to enable a rotation of the handset by 15 degrees.
- c. Rotate the handset around the horizontal line by 15 degrees.
- d. While maintaining the orientation of the handset, move the handset towards the phantom on a line passing through RE and LE until any part of the handset touches the ear. The tilted position is obtained when the contact is on the pinna. If the contact is at any location other than the pinna (e.g., the antenna with the back of the phantom head), the angle of the handset should be reduced. In this case, the tilted position is obtained if any part of the handset is in contact with the pinna as well as a second part of the handset is contact with the phantom (e.g., the antenna with the back of the phantom (e.g., the antenna with the back of the phantom (e.g., the antenna with the back of the head).

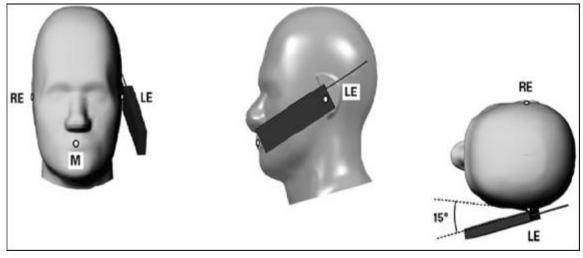


Figure 7-3 Phone "tilted" position. The reference points for the right ear (RE), left ear (LE) and mouth (M), which define the reference plane for handset positioning, are indicated.

8. MEASUREMENT RESULTS

8.1 SYSTEM VALIDATION

The system performance check is performed prior to any usage of the system in order to guarantee reproducible results. The system performance check verifies that the system operates within its specifications of $\pm 10\%$. The system performance check results are tabulated below. And also the corresponding SAR plot is attached as well in the SAR plots files.

Frequency (MHz)	1g SAR	10g SAR	Local SAR at Surface (Above Feed Point)	Local SAR at Surface (y = 2cm offset from feed point)
300	3.0	2.0	4.4	2.1
450	4.9	3.3	7.2	3.2
835	9.5	6.2	14.1	4.9
900	10.8	6.9	16.4	5.4
1450	29.0	16.0	50.2	6.5
1800	38.1	19.8	69.5	6.8
1900	39.7	20.5	72.1	6.6
2000	41.1	21.1	74.6	6.5
2450	52.4	24.0	104.2	7.7
3000	63.8	25.7	140.2	9.5

IEEE P1528 Recommended Reference Value:

SYSTEM PERFORMANCE CHECK MEASUREMENT CONDITIONS

- The measurements were performed in the flat section of the SAM twin phantom filled with Head and Body simulating liquid of the following parameters.
- The OPENSAR system with an E-field probe EP74 SN0807 was used for the measurements.
- The dipole was mounted on the small tripod so that the dipole feed point was positioned below the center marking of the flat phantom section and the dipole was oriented parallel to the body axis (the long side of the phantom). The standard measuring distance was 15 mm (below 1 GHz) and 10 mm (above 1 GHz) from dipole center to the simulating liquid surface.
- The 1g and 10 g spatial average SAR values normalized to 1 W dipole input power give reference data for comparisons.



8.2 TEST LIQUID CONFIRMATION

Simulated Tissue Liquid Parameter confirmation

The dielectric parameters were checked prior to assessment using the HP85070C dielectric probe kit. The dielectric parameters measured are reported in each correspondent section.

IEEE SCC-34/SC-2 P1528 recommended Tissue Dielectric Parameters

The head tissue dielectric parameters recommended by the IEEE SCC-34/SC-2 in P1528 have been incorporated in the following table. These head parameters are derived from planar layer models simulating the highest expected SAR for the dielectric properties and tissue thickness variations in a human head. Other head and body tissue parameters that have not been specified in P1528 are derived from the tissue dielectric parameters computed from the 4-Cole-Cole equations and extrapolated according to the head parameters specified in P1528

Target Frequency	Head		Bo	ody
(MHz)	٤r	σ (S/m)	٤r	σ (S/m)
150	52.3	0.76	61.9	0.80
300	45.3	0.87	58.2	0.92
450	43.5	0.87	56.7	0.94
835	41.5	0.90	55.2	0.97
900	41.5	0.97	55.0	1.05
915	41.5	0.98	55.0	1.06
1450	40.5	1.20	54.0	1.30
1610	40.3	1.29	53.8	1.40
1800-2000	40.0	1.40	53.3	1.52
2450	39.2	1.80	52.7	1.95
3000	38.5	2.40	52.0	2.73
5800	45.3	5.27	48.2	6.00

Note: ε_r = relative permittivity, σ = conductivity and ρ = 1000 kg/m³

System validation Results

Ambient condition:

Temperature: <u>22</u> °C

Relative humidity: <u>58</u>%

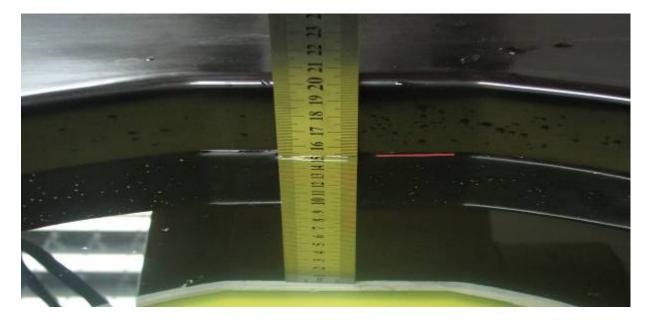
Date: July 24, 2009

Medium		Parameter Target	Measured	Deviation	Limit		
Туре	Temp (°C)	Depth (± 0.5 cm)	1 ur uniceer	Iurget	Wicusureu	(%)	(%)
Muscle	20.00		Permitivity	53.12	52.403	1.35	+/-5
2450 MIL			15.00	Conductivity	1.95	1.940	0.51
2450 MHz			1g SAR	50.22	51.234	-2.02	+/- 10

8.3 EUT TUNE-UP PROCEDURE

The following procedure had been used to prepare the EUT for the SAR test.

- The EUT was link with base station simulator in SAR testing periods, the base station simulator allowing it to continually transmit the maximum power and change the channel frequency.
- The conducted power was measured at the high, middle and low channel frequency before and after the SAR measurement.
- the depth of Liquid must above 15cm.

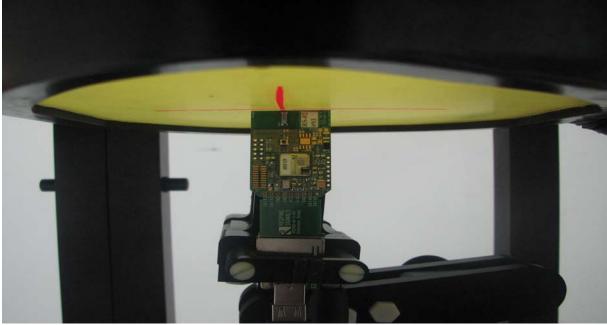


Date of Issue: July 28, 2009

8.4 EUT SETUP PHOTOS

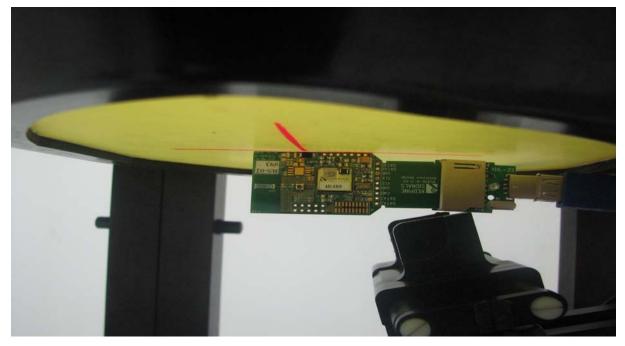
<u>EUT Setup Configuration 1</u>

1. Spacing between **EUT** and phantom - In contact (0 cm).



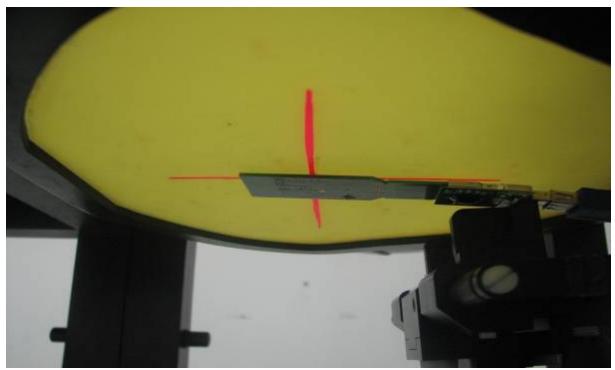
EUT Setup Configuration 2

1. Spacing between **EUT** and phantom - In contact (0 cm).



EUT Setup Configuration 3

2. Spacing between EUT and phantom - In contact (0 cm).





8.5 SAR MEASUREMENT RESULT

Date of Measurement: July 24, 2009

SAR Meas	urement	EUT Setup	Configu	ration 1				
Crest Facto	or: 1 (Duty	cycle: 100%)				Depth of	of Liquid: <u>15.</u>	<u>0</u> cm
B mode								
EUT Conc	Setup lition	Freque	iency Conducted Peak Liquid Power (dBm) Temp	Frequency		SAR(1g)	Limit	
Position	Antenna	Channel	MHz	Before	After	[°C]	(W/kg)	(W/kg
		802.11b 1	2412	12.12	12.11	20.0	0.156	
Flat	Fixed	802.11b 6	2437	12.36	12.33	20.0	0.142	1.6
		802.11b 11	2462	12.29	12.27	20.0	0.123	
G mode	-							
EUT Conc	Setup lition	Freque	ncy		Conducted Peak Power (dBm)		SAR(1g)	Limit
Position	Antenna	Channel	MHz	Before	After	Temp [°C]	(W/kg)	(W/kg)
		802.11g 1	2412	10.32	10.30	20.0	0.141	
Flat	Fixed	802.11g 6	2437	10.46	10.44	20.0	0.132	1.6
		802.11g 11	2462	10.51	10.50	20.0	0.121	
20n mode								
EUT Conc	Setup lition	Freque	ncy		tted Peak (dBm)	Liquid Temp	SAR(1g)	Limit (W/kg)
Position	Antenna	Channel	MHz	Before	After	[°C]	(W/kg)	
		802.11n HT20 1	2412	10.38	10.37	20.0	0.183	
Flat	Fixed	802.11n HT20 6	2437	10.27	10.25	20.0	0.165	1.6
		802.11n HT20 11	2462	10.62	10.60	20.0	0.144	



Date of Measurement: July 24, 2009

SAR Measurement EUT Setup Configuration 2

Crest Factor: 1 (Duty cycle: 100%)

Depth of Liquid: <u>15.0</u> cm

B mode

EUT Setup Condition		Frequency		Conducted Peak Power (dBm)		Liquid Temp	SAR(1g)	Limit
Position	Antenna	Channel	MHz	Before	After	[°C]	(W/kg)	(W/kg)
		802.11b 1	2412	12.12	12.11	20.0	0.359	1.6
Flat Fixe	Fixed	802.11b 6	2437	12.36	12.33	20.0	0.345	
		802.11b 11	2462	12.29	12.27	20.0	0.332	

G mode

EUT Setup Condition		Frequency		Conducted Peak Power (dBm)		Liquid Temp	SAR(1g)	Limit
Position	Antenna	Channel	MHz	Before	After	[°C]	(W/kg)	(W/kg)
	Flat Fixed	802.11g 1	2412	10.32	10.30	20.0	0.357	
Flat		802.11g 6	2437	10.46	10.44	20.0	0.355	1.6
		802.11g 11	2462	10.51	10.50	20.0	0.351	

20n mode

EUT S Cond	-	Frequency		Conducted Peak Power (dBm)		Liquid Temp	SAR(1g)	Limit
Position	Antenna	Channel	MHz	Before	After	[°C]	(W/kg)	(W/kg)
Flat Fixed	802.11n HT20 1	2412	10.38	10.37	20.0	0.362		
	Fixed	802.11n HT20 6	2437	10.27	10.25	20.0	0.359	1.6
		802.11n HT20 11	2462	10.62	10.60	20.0	0.354	

Date of Issue:July 28, 2009

Date of Measurement: July 24, 2009

SAR Measurement EUT Setup Configuration 3

Crest Factor: 1 (Duty cycle: 100%)

Depth of Liquid: 15.0 cm

B mode

Dinoue								
EUT S Cond	-	Freque	ncy	Conducted Peak Power (dBm)		Liquid Temp	SAR(1g)	Limit
Position	Antenna	Channel	MHz	Before	After	[°C]	(W/kg)	(W/kg)
	Flat Fixed	802.11b 1	2412	12.12	12.11	20.0	0.679	
Flat		802.11b 6	2437	12.36	12.33	20.0	0.665	1.6
		802.11b 11	2462	12.29	12.27	20.0	0.646	

G mode

	EUT Setup Condition		Frequency		Conducted Peak Power (dBm)		SAR(1g)	Limit
Position	Antenna	Channel	MHz	Before	After	[°C]	(W/kg)	(W/kg)
		802.11g 1	2412	10.32	10.30	20.0	0.664	
Flat Fixed	802.11g 6	2437	10.46	10.44	20.0	0.655	1.6	
		802.11g 11	2462	10.51	10.50	20.0	0.644	

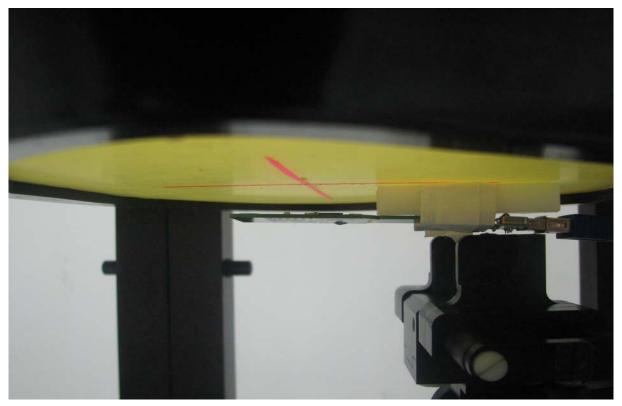
20n mode

EUT S Cond	-	Frequency		Conducted Peak Power (dBm)		Liquid Temp	SAR(1g)	Limit
Position	Antenna	Channel	MHz	Before	After	[°C]	(W/kg)	(W/kg)
	802.11n HT20 1	2412	10.38	10.37	20.0	0.706		
Flat	Fixed	802.11n HT20 6	2437	10.27	10.25	20.0	0.689	1.6
		802.11n HT20 11	2462	10.62	10.60	20.0	0.667	



Enhanced energy coupling test: <u>EUT Setup Configuration 4</u>

1. Spacing between EUT and phantom –0.5cm.



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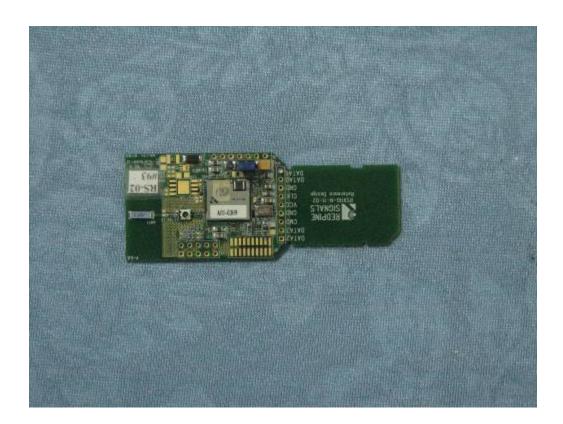


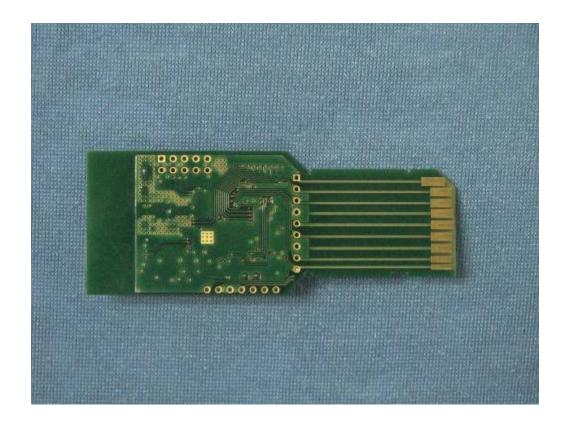
Date of Measurement: July 24, 2009

SAR Measurement EUT Configuration 4						enhanced energy coupling test				
Crest Factor: 1 (Duty cycle: 100%)							Depth of Liquid: <u>15.0</u> cm			
20n mode										
EUT S Cond	-	Frequency		Conducted Peak Power (dBm)		Liquid	SAR(1g)	Limit		
Position	Antenna	Channel	MHz	Before	After	Temp [°C]	(W/kg)	(W/kg)		
Flat	Fixed	802.11n HT20 1	2412	10.38	10.37	20.0	0.350	1.6		
Enhanced e	energy coup	oling test, 0.3	50 is less	than (0.706	5/2=0.353)	•				

Date of Issue: July 28, 2009

9. EUT PHOTOES





10. EQUIPMENT LIST & CALIBRATION

Name of Equipment	Manufacturer	Type/Model	Serial Number	Calibration Due
РС	HP	PV 3.06GHz	375052-AA1	N/A
Signal Generator	Agilent	E8257C	MY43321570	12/11/2009
MultiMeter	Keithley	2000	1015843	05/01/2010
S-Parameter Network Analyzer	Agilent	E5071B	MY42301382	08/07/2009
Wireless Communication Test Set	Agilent	E5515C	QB44051695	06/17/2010
Wireless Communication Test Set	R&S	CMU200	B23-03291	07/29/2009
Power Meter	Agilent	E4416A	QB41292714	12/11/2009
E-field PROBE	ANTENNESSA	EP_100	SN11/09	04/16/2010
DIPOLE 835	ANTENNESSA	DIPC32	SN 48_05	12/10/2009
DIPOLE 900	ANTENNESSA	DIPD33	SN 48_05	12/10/2009
DIPOLE 1800	ANTENNESSA	DIPF34	SN 48_05	12/10/2009
DIPOLE 1900	ANTENNESSA	DIPG35	SN 48_05	12/10/2009
DIPOLE 2000	ANTENNESSA	DIPI36	SN 48_05	12/10/2009
DIPOLE 2450	ANTENNESSA	DIPJ37	SN 48_05	12/10/2009
POSITIONING DEVICE	ANTENNESSA	MSH_14	SN 41_05	N/A
DUMMY PROBE	ANTENNESSA	DP_12	SN 39_05	N/A
SAM PHANTOM	ANTENNESSA	SAM29	SN 41_05	N/A
PHANTON WOOD TABLE	ANTENNESSA	N/A	N/A	N/A
6 AXIS ROBOT	KUKA	KR3	846428	N/A
ROBOT KRC	KUKA	KCP2	01436	N/A
CHANELS SCAN CARD	KEITHLEY	2000	2000-172-01B	N/A
PROBE/ROBOT POSITIONING DEVICE	ANTENNESSA	MSH14	SN 41_05	N/A
LIQUID CALIBRATION KIT	ANTENNESSA	41/05 OCP9	00425167	N/A

Compliance Certification Services (Kunshan) Inc. Report No: SZ090401B04 11. FACILITIES

All measurement facilities used to collect the measurement data are located at

No.10, Weiye Rd., Innovation Park, Eco & Tec. Development Part, Kunshan City, Jiangsu Province, PRC.

12. REFERENCES

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13. ATTACHMENT

Exhibit	Content
1	System Validation Plots
2	SAR Test Plots
3	Dosimetric E-Field Probe – EP74 SN 0807
4	Validation Dipole

End of Report