

# **HEARING AID COMPATIBILITY RF EMISSIONS TEST REPORT**

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<span id="page-0-0"></span>**We, Sporton International Inc. (Kunshan), would like to declare that the tested sample provide by manufacturer and the test data has been evaluated in accordance with the test procedures given in ANSI C63.19-2019 / 47 CFR Part 20.19 and has been in compliance with the applicable technical standards.**

**The test results in this report apply exclusively to the tested model / sample. Without written approval of Sporton International Inc. (Kunshan), the test report shall not be reproduced except in full.**

Si Zhang

**Approved by: Si Zhang**



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### **History of this test report**





### <span id="page-3-0"></span>*1. General Information*





### <span id="page-4-0"></span>*2. Testing Location*

Sporton International Inc. (Kunshan) is accredited to ISO/IEC 17025:2017 by American Association for Laboratory Accreditation with Certificate Number 5145.02.



### <span id="page-4-1"></span>*3. Applied Standards*

- ‧ FCC CFR47 Part 20.19
- ‧ ANSI C63.19-2019
- FCC KDB 285076 D01 HAC Guidance v06r04
- ‧ FCC KDB 285076 D03 HAC FAQ v01r06



### <span id="page-5-0"></span>*4. Air Interfaces*



**Type Transport:**

VO= Voice only

DT= Digital Transport only (no voice) VD= CMRS and IP Voice Service over Digital Transport

**Remark:**

1. The air interface max power plus MIF is complies with ANSI C63.19-2019 Table 4.1 RFAIPL

2. For 5GNR n41/n77 HPUE, 5GNR n41/n77 PC2 Maximum Duty Cycle is 50%, using FTM (Factory Test Mode) with 50% duty cycle is considered during testing. For 5G NR other bands test, using FTM (Factory Test Mode) with default 100% duty cycle transmission to perform evaluation.

3. The UMTS/LTE/5GFR1 and WIFI set to highest device transmit maximum power.

4. There are two samples under test: Sample 1 is with camera, sample 2 is without camera, there is no other difference. According to the differences, so choose sample 1 to perform full testing and sample 2 to verify the worst case of sample 1.

5. For the different model names, please refer to the Operational Description of Product Equality Declaration which is exhibit separately



### <span id="page-6-0"></span>*5. WD Emission Requirements*

The WD's conducted power must be at or below either the stated RFAIPL (Table 4.1 ) or the stated peak power level (Table 4.2), or the average near-field emissions over the measurement area must be at or below the stated RFAIL (Table 4.3), or the stated peak field strength (Table 4.4). The WD may demonstrate compliance by meeting any of these four requirements, but it must do so in each of its operating bands at its established worst-case normal speech-mode operating condition.









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### <span id="page-7-0"></span>*6. System Description and Operation*

### **<System Components>**



#### **Remark:**

A typical al DASY system for HAC measurements consists of

- 6-axis robotic arm (Staubli TX2-60L/ TX2-90XL) for positioning the probe
- Mounting Platform for keeping the phantoms at a field location relative to the robot
- Measurement Server for handling all time-critical tasks, such as measurement data acquisition and supervision of safety features
- EOC (Electrical to Optical Converter) for converting the optical signal from the Data Acquisition Electronics (DAE) to electrical before being transmitted to the measurement server
- LB (Light Beam unit) for probe alignment (measurement of the exact probe length and eccentricity)
- Test Arch for Device Under Test (DUT) testing
- DAE that reads the probe voltages and transmits them to the DASY PC. It is also used to detect probe touch and collision signals
- Device Holder for positioning the DUT beneath the phantom
- ANT (wideband Antenna) for broadcasting the downlink signals emitted by base station simulators (BSS) to the WD
- Operator PC for running the DASY software to define/execute the measurements.

The following components are needed for RFail measurements only:

- Modulation Interference Factor (MIF)
- Isotropic E-field, free-space probe (e.g., EF3DVx)
- Radiofrequency (RF) emission calibration dipoles for system check / validation purposes.



### **<EF3DV3 E-Field Probe Specification>**



### **Voltage to E-field Conversion**

The measured voltage is first linearized to a quantity proportional to the square of the E-field using the (a, b, c, d) set of parameters specific to the communication system and sensor:

$$
V_{compi}=U_i+U_i^2\cdot\frac{10\frac{d}{10}}{dcp_i}
$$

where  $V_{\text{compi}} =$  compensated signal of channel i ( $\mu V$ ) (i = x, y, z)

 $U_i$  = input signal of channel i ( $\mu$ V) ( $i = x, y, z$ )

d = PMR factor d (dB) (Probe parameter)

 $dcp_i$  = diode compression point of channel i ( $\mu$ V) (Probe parameter, i = x, y, z)

$$
V_{compi}^{dB} \sqrt{\mu V}} = 10 + log_{10} (V_{compi})
$$

$$
corr_i = a_i \cdot e - \left(\frac{V_{compi}^{dB} \sqrt{\mu V}}{C_i}\right)^2
$$

where coor<sub>i</sub> = correction factor of channel i (dB) ( $i = x, y, z$ )  $V_{\text{compi dB}}\sqrt{d}V =$  compensated voltage of channel i (dB $\sqrt{V}$ ) (i = x, y, z)  $a_i$  = PMR factor a of channel i (dB) (Probe parameter,  $i = x, y, z$ )  $b_i$  = PMR factor b of channel i (dB $\forall \mu \forall$ ) (Probe parameter, i = x,y,z)  $c_i$  = PMR factor c of channel i (Probe parameter,  $i = x,y,z$ )

The voltage V<sub>idB</sub>√<sub>µV</sub> is the linearized voltage in dB√µV:

 $\mathbf{V_{i}}$  dB $_{\sqrt{\mu V}}=\mathbf{V_{compi}}$  dB $_{\sqrt{\mu}}$ 

where  $V_{i \text{ dB}}\sqrt{\psi}$  = linearized voltage of channel i (dB $\sqrt{\psi}$ ) (i = x,y,z)  $V_{\text{compi dB}}\sqrt{\mu}V =$  compensated voltage of channel i (dB $\sqrt{\mu}V$ ) (i = x,y,z) Corr<sub>i</sub> = correction factor of channel i (dB) ( $i = x, y, z$ )



Finally, the linearized voltage is converted in  $\mu V$ :

$$
V_i=10^{\frac{V_i\,dB_{\!\sqrt{\mu V}}}{10}}
$$

where  $V_i$  = linearized voltage of channel i ( $\mu V$ ) ( $i = x, y, z$ )  $V_{i \text{dB}}\sqrt{d}V_{\text{UV}}$  = linearized voltage of channel i (dB $\sqrt{\mu}V$  (i = x,y,z)

The E-field data for each channel are calculated using the linearized voltage:

$$
\text{E-field Probes}: E_i = \sqrt{\frac{v_i}{Norm_i \cdot ConvF}}
$$

where  $V_i$  = compensated signal of channel i, (i = x, y, z) Norm<sub>i</sub> = sensor sensitivity ( $\mu V/(V/m)^2$  of channel i (i = x, y, z) ConvF = sensitivity enhancement in solution  $E_i$  = electric field strength of channel i in  $V/m$ 

The RMS value of the field components gives the total field strength (Hermitian magnitude):

$$
E_{tot} = \sqrt{E_x^2 + E_y^2 + E_z^2}
$$

### **Averaged E-field Calculation**

The averaged E-field is defined by

$$
E_{avg} = \frac{1}{n} \cdot \sum_{i=1}^n E_i
$$

where  $n =$  = the number of measurement grid point  $E_i$  = the E-field measured at point i

### **RFail Calculation**

The RFail is finally computed with

$$
[RFail[dB(V/m)] = 20 \cdot log_{10}(E_{avg}) + MIF
$$

where RFail = the Radio Frequency Audio Interference Level in dB(V/m)  $E_{avg}$  = the averaged E-field in (V/m) calculated MIF = the Modulation Interference Factor in dB.



### <span id="page-10-0"></span>*7. RF Emissions Test Procedure*



**Figure of WD near-field emission scan flowchart according to ANSI C63.19:2019**





#### **The references and reference plane that shall be used in the WD emissions measurement**



#### **Test procedure: Indirect measurement—preferred**

- a. The measurement procedure using a probe and instrumentation chain with a response of <10 kHz (see ANSI C63.19-2019 section4.5.1) is identical to the direct measurement method of ANSI C63.19-2019 section4.5.3.2.2: however, because of the bandwidth limitations, it cannot include the direct use of the spectral and temporal weighting functions. The output of such measurement systems must be readings of steady state rms field strength in dB(V/m).
- b. The RF audio interference level in dB(V/m) is obtained by adding the Modulation Interference Factor (in decibels) to the average steady state rms field strength reading over the measurement area, in dB(V/m), from Step c). Use this result to determine the WD's compliance per ANSI C63.19-2019 section4.7.
- c. Scan the entire 50 mm by 50 mm measurement area in equally spaced step sizes and record the reading at each measurement point. The step size shall meet the specification for step size in ANSI C63.19:2019 section 4.5.3.
- d. Calculate the average of the measurements taken in Step c
- e. Convert the average value found in Step d) to RF audio interference level, in volts per meter, by taking the square root of the reading and then dividing it by the measurement system transfer function, as established in ANSI C63.19:2019 section4.5.3.2.1 pre-test procedure. Convert the result to dB(V/m) by taking the base-10 logarithm and multiplying it by 20. Expressed as a formula

RF audio interference level in db(V/M) 20  $*$  log( $R_{ave}^{1/2}$  / TF) where

Rave is the average reading

- f. Compare this RF audio interference level to the limits in ANSI C63.19:2019 section4.7 and record the result
- g. Per ANSI C63.19-2019 section4.6, WDs capable of operating multiple transmitters shall be subject to emissions requirements for all such transmitters expected to be operated when the WD is in voice mode operation positioned at a user's ear. Each qualified transmitter is tested individually using the method of Clause 4. Other WD transmitters shall be temporarily disabled or reduced in power level such that their average antenna input power is at least 6 dB lower than the average antenna input power of the transmitter under test. The transmitter under test is set to the fixed and repeatable combination of power and modulation characteristic that is representative of the worst case (highest interference potential) likely to be encountered while the WD is experiencing normal voice mode operation. The limiting measurement for device qualification is the highest RF audio interference potential measured for any of the WD transmitters. If the highest interference measurement is from a transmitter that is not required for normal voice mode operation, a secondary rating may be given that applies when that transmitter is disabled



### <span id="page-12-0"></span>*8. Test Equipment List*



**Note:**<br>1. **N** 

NCR: "No-Calibration Required"

2. The dipole calibration interval can be extended to 3 years with justification. The dipoles are also not physically damaged, or repaired during the interval. The justification data in appendix C can be found which the return loss is < -20dB, within 20% of prior calibration, the impedance is within 5 ohm of prior calibration for each dipole.



### <span id="page-13-0"></span>*9. System Validation*

Obtaining accurate measurements and relevant quantities in Module HAC depends on the proper functioning of many components and the correct parameter settings. Faulty results due to drift, failures, or incorrect parameters might not be recognized, as the differences might not be obvious in the measurements.

SPEAG DASY incorporates a system check, also called system verification procedure, to test for the proper functioning of the system based on the tests described in ANSI C63.19-2019: the RF interference potential test setup is verified with RF Emission Calibration Dipoles.

### **<Test Setup>**

- 1. Set the RF signal generator for either CW. Set its output power so the peak power applied to the antenna is equal to that recorded for the real or emulated signal using the WD modulation format
- 2. Average input power P = 100 mW (20 dBm) after adjustment for return loss. An input power that generates field levels similar to those from the WD or other suitable level may also be used
- 3. The test fixture should meet the two-wavelength separation criterion
- 4. The probe-to-dipole separation, which is measured from closest surface of the dipole to the center point of the probe sensor element, should be 15 mm



**Figure of Setup Diagram**

### **<Validation Procedure>**

Place a dipole antenna meeting the requirements given in ANSI C63.19: 2019 D.11 in the position normally occupied by the WD. The dipole antenna serves as a known source for an electrical and magnetic output. Position the E-field probe so that:

- a. The probe and its cable are parallel to the coaxial feed of the dipole antenna
- b. The probe cable and the coaxial feed of the dipole antenna approach the measurement area from opposite directions; and
- c. The center point of the probe element(s) is 15 mm from the closest surface of the dipole elements

Scan the length of the dipole with the E-field probe and record the two maximum values found near the dipole ends. Average the two readings and compare the reading to expected value in the calibration certificate or expected value in this standard.





### <span id="page-14-0"></span>*10. Modulation Interference Factor*

For any specific fixed and repeatable modulated signal, a Modulation Interference Factor (MIF, expressed in decibels) may be developed that relates its interference potential to its steady state rms signal level or average power level. This factor is a function only of the audio frequency amplitude modulation characteristics of the signal and is the same for field strength or conducted power measurements. It is important to emphasize that the MIF is valid only for a specific repeatable audio frequency amplitude modulation characteristic. Any change in modulation characteristic requires determination and application of a new MIF.

MIF may be determined using a radiated RF field, a conducted RF signal, or, in a preliminary stage, a mathematical analysis of a modeled RF signal.

- a. Verify the slope accuracy and dynamic range capability over the desired operating frequency band of a fast probe or sensor, square-law detector, as specified in ANSI C63.19: 2019 D.3, and weighting system as specified in ANSI C63.19: 2019 D.4 and ANSI C63.19: 2019 D.5. For the probe and instrumentation included in the measurement of MIF, additional calibration and application of calibration factors are not required.
- b. Using RF illumination, or conducted coupling, apply the specific modulated signal in question to the measurement system at a level within its confirmed operating dynamic range
- c. Measure the steady-state rms level at the output of the fast probe or sensor
- d. Measure the steady-state average level at the weighting output
- e. Without changing the square-law detector or weighting system, and using RF illumination, or conducted coupling, substitute for the specific modulated signal a 1 kHz, 80% amplitude modulated carrier at the same frequency and adjust its strength until the level at the weighting output equals the Step d) measurement
- f. Without changing the carrier level from Step e), remove the 1 kHz modulation and again measure the steady-state rms level indicated at the output of the fast probe or sensor.
- g. The MIF for the specific modulation characteristic is given by the ratio of the Step f) measurement to the Step c) measurement, expressed in decibels (20\*log(step6/step3)

In practice, Step e) and Step f) need not be repeated for each MIF determination if the relationship between the two measurements has been pre-established for the measurement system over the operating frequency and dynamic ranges. In such cases, only the modulation characteristic being tested needs to be available during WD testing Since indirect measurement procedure was using for RF audio interference power level evaluation, the MIF values applied in this test report were provided by the HAC equipment provider of SPEAG, and the worst values for all air interface are listed below to be determine the Wireless device RF audio interference power level.





### <span id="page-15-0"></span>*11. Evaluation of WD RF interference potential*

#### **General Note:**

- 1. In this report, max conducted power from each air interface was first used to evaluate whether it complies with ANSI C63.19-2019 Table 4.1 RF<sub>AIPL</sub>, compliance with table 4.1 means compliance with WD emission requirements. the RFAIPL evaluation refer to section 11.1 for detail.
- 2. If there some air interface were not meet ANSI C63.19-2019 table 4.1 requirement, these air interfaces were further evaluation ANSI C63.19-2019 Table 4.3 RFAIL requirement. And the RFAIL evaluation result refer to section 13.

### <span id="page-15-1"></span>*11.1Evaluation RFAIPL*

#### **<WWAN Max Tune-up Limit>**



#### **<Ant.2>**





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**<Ant.4>**



#### **<Ant.6>**



#### **<WLAN Max Tune-up Limit>**





#### **<Evaluation RF audio interference power level>**

#### **General Note:**

- 1. Use maximum power plus worst case MIF to determine whether it complies with  $\text{RF}_{\text{AlPL}}$
- 2. If maximum power plus worst case MIF does not complies with  $RF_{A|PL}$ , then further evaluation  $RF_{AL}$  include in section 13.
- 3. According to ANSI C63.19 2019, if maximum power plus worst case MIF is complies with RFAIPL, means compliance with WD emission requirements.

#### **<Ant.1>**



#### **<Ant.2>**



#### **<Ant.4>**



#### **<Ant.6>**





#### **<WLAN Ant>**





### <span id="page-19-0"></span>*12. Conducted RF Output Power (Unit: dBm)*



#### **<5GNR>**









### <span id="page-20-0"></span>*13. RFAIL Test Results*

#### **General Note:**

- 1. The HAC measurement system applies MIF value onto the measured RMS E-field, which is indirect method in ANSI C63.19-2019 version, and reports the RF audio interference level.
- 2. Phone Condition: Mute on; Backlight off; Max Volume.
- 3. Since the LTE B41 and NR n41/n77 power class 3 maximum power plus MIF is complies with ANSI63.19-2019 Table 4.1 RF $_{APL}$ , therefore, only power class2 evaluated RF $_{AIL}$ .



**Test Engineer**: Martin Li, Varus Wang, Light Wang, Ricky Gu



### <span id="page-21-0"></span>*14. Uncertainty Assessment*

The component of uncertainly may generally be categorized according to the methods used to evaluate them. The evaluation of uncertainly by the statistical analysis of a series of observations is termed a Type A evaluation of uncertainty. The evaluation of uncertainty by means other than the statistical analysis of a series of observation is termed a Type B evaluation of uncertainty. Each component of uncertainty, however evaluated, is represented by an estimated standard deviation, termed standard uncertainty, which is determined by the positive square root of the estimated variance.

The combined standard uncertainty of the measurement result represents the estimated standard deviation of the result. It is obtained by combining the individual standard uncertainties of both Type A and Type B evaluation using the usual "root-sum-squares" (RSS) methods of combining standard deviations by taking the positive square root of the estimated variances. Expanded uncertainty is a measure of uncertainty that defines an interval about the measurement result within which the measured value is confidently believed to lie. It is obtained by multiplying the combined standard uncertainty by a coverage factor. For purpose of this document, a coverage factor two is used, which corresponds to confidence interval of about 95 %. The DASY uncertainty Budget is showed below Table.

The judgment of conformity in the report is based on the measurement results excluding the measurement uncertainty.



The test results with all measurement uncertainty excluded are presented in accordance with the regulation limits or requirements declared by manufacturers.

Comments and Explanations:

The declared of product specification for EUT presented in the report are provided by the manufacturer, and the manufacturer takes all the responsibilities for the accuracy of product specification.

**Uncertainty Budget of HAC free field assessment**



### <span id="page-22-0"></span>*15. References*

- [1] ANSI C63.19:2019, "American National Standard for Methods of Measurement of Compatibility between Wireless Communications Devices and Hearing Aids", Aug. 2019.
- [2] FCC KDB 285076 D01v06r04, "Equipment Authorization Guidance for Hearing Aid Compatibility", Sep 2023.
- [3] FCC KDB 285076 D03v01r06, "Hearing aid compatibility frequently asked questions", Jul. 2022
- [4] SPEAG DASY System Handbook