## Conducted Spurious Emissions




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## TM 3 \& Lowest

Reference


Low Band-edge


## Conducted Spurious Emissions




## Conducted Spurious Emissions



TM 3 \& Middle
Reference


Conducted Spurious Emissions


Conducted Spurious Emissions



TM 3 \& Highest
Reference


High Band-edge


## Conducted Spurious Emissions




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### 8.5 Radiated spurious emissions

## Test Requirements and limit, §15.247(d), §15.205, §15.209

In any 100 kHz bandwidth outside the operating frequency band, the radio frequency power that is produced by the intentional radiator shall be at least 20 dB below that in the 100 KHz bandwidth within the band. In case the emission fall within the restricted band specified on 15.205(a) and (b), then the 15.209(a) limit in the table below has to be followed.

- FCC Part 15.209(a) and (b)

| Frequency (MHz) | Limit (uV/m) | Measurement Distance (meter) |
| :---: | :---: | :---: |
| $0.009-0.490$ | $2400 / \mathrm{F}(\mathrm{kHz})$ | 300 |
| $0.490-1.705$ | $24000 / \mathrm{F}(\mathrm{kHz})$ | 30 |
| $1.705-30.0$ | 30 | 30 |
| $30 \sim 88$ | $100 * *$ | 3 |
| $88 \sim 216$ | $150 * *$ | 3 |
| $216 \sim 960$ | $200 * *$ | 3 |
| Above 960 | 500 | 3 |

** Except as provided in 15.209 (g), fundamental emissions from intentional radiators operating under this Section shall not be located in the frequency bands $54-72 \mathrm{MHz}, 76-88 \mathrm{MHz}, 174-216 \mathrm{MHz}$ or $470-806 \mathrm{MHz}$. However, operation within these frequency bands is permitted under other sections of this Part, e.g. 15.231 and 15.241.

- FCC Part 15.205 (a): Only spurious emissions are permitted in any of the frequency bands listed below:

| $\mathbf{M H z}$ | $\mathbf{M H z}$ | $\mathbf{M H z}$ | $\mathbf{M H z}$ | $\mathbf{G H z}$ | $\mathbf{G H z}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $0.009 \sim 0.110$ | $8.41425 \sim 8.41475$ | $108 \sim 121.94$ | $1300 \sim 1427$ | $4.5 \sim 5.15$ | $14.47 \sim 14.5$ |
| $0.495 \sim 0.505$ | $12.29 \sim 12.293$ | $123 \sim 138$ | $1435 \sim 1626.5$ | $5.35 \sim 5.46$ | $15.35 \sim 16.2$ |
| $2.1735 \sim 2.1905$ | $12.51975 \sim 12.52025$ | $149.9 \sim 150.05$ | $1645.5 \sim 1646.5$ | $7.25 \sim 7.75$ | $17.7 \sim 21.4$ |
| $4.125 \sim 4.128$ | $12.57675 \sim 12.57725$ | $156.52475 \sim$ | $1660 \sim 1710$ | $8.025 \sim 8.5$ | $22.01 \sim 23.12$ |
| $4.17725 \sim 4.17775$ | $13.36 \sim 13.41$ | 156.52525 | $1718.8 \sim 1722.2$ | $9.0 \sim 9.2$ | $23.6 \sim 24.0$ |
| $4.20725 \sim 4.20775$ | $16.42 \sim 16.423$ | $156.7 \sim 156.9$ | $2200 \sim 2300$ | $9.3 \sim 9.5$ | $31.2 \sim 31.8$ |
| $6.215 \sim 6.218$ | $16.69475 \sim 16.69525$ | $162.0125 \sim 167.17$ | $2310 \sim 2390$ | $10.6 \sim 12.7$ | $36.43 \sim 36.5$ |
| $6.26775 \sim 6.26825$ | $16.80425 \sim 16.80475$ | $167.72 \sim 173.2$ | $2483.5 \sim 2500$ | $13.25 \sim 13.4$ | Above 38.6 |
| $6.31175 \sim 6.31225$ | $25.5 \sim 25.67$ | $240 \sim 285$ | $2655 \sim 2900$ |  |  |
| $8.291 \sim 8.294$ | $37.5 \sim 38.25$ | $322 \sim 335.4$ | $3260 \sim 3267$ |  |  |
| $8.362 \sim 8.366$ | $73 \sim 74.6$ | $399.90 \sim 410$ | $3332 \sim 3339$ |  |  |
| $8.37625 \sim 8.38675$ | $74.8 \sim 75.2$ | $608 \sim 614$ | $3345.8 \sim 3358$ |  |  |
|  | $960 \sim 1240$ | $3600 \sim 4400$ |  |  |  |

- FCC Part 15.205(b): The field strength of emissions appearing within these frequency bands shall not exceed the limits shown in §15.209. At frequencies equal to or less than 1000 MHz , compliance with the limits in §15.209 shall be demonstrated using measurement instrumentation employing a CISPR quasi-peak detector. Above 1000 MHz , compliance with the emission limits in $\S 15.209$ shall be demonstrated based on the average value of the measured emissions. The provisions in $\S 15.35$ apply to these measurements.
- Test Configuration

Refer to the APPENDIX I.
$\square$ Test Procedure

1. The EUT is placed on a non-conductive table, emission measurements at below 1 GHz , the table height is 80 cm and above 1 GHz , the table height is 1.5 m .
2. The turntable shall be rotated for 360 degrees to determine the position of maximum emission level.
3. EUT is set 1 or 3 m away from the receiving antenna, which is varied from 1 m to 4 m to find out the highest emissions.
4. Maximum procedure was performed on the six highest emissions to ensure EUT compliance.
5. And also, each emission was to be maximized by changing the polarization of receiving antenna both horizontal and vertical.
6. Repeat above procedures until the measurements for all frequencies are complete.

## - KDB558074 D01v05r02 - Section 8.6

## - ANSI C63.10-2013 - Section 11.12

## Peak Measurement

RBW = As specified in below table, VBW $\geq 3 \times$ RBW, Sweep $=$ Auto, Detector $=$ Peak, Trace mode $=$ Max Hold until the trace stabilizes.

| Frequency | RBW |
| :---: | :---: |
| $9-150 \mathrm{kHz}$ | $200-300 \mathrm{~Hz}$ |
| $0.15-30 \mathrm{MHz}$ | $9-10 \mathrm{kHz}$ |
| $30-1000 \mathrm{MHz}$ | $100-120 \mathrm{kHz}$ |
| $>1000 \mathrm{MHz}$ | 1 MHz |

## Average Measurement:

1. RBW $=1 \mathrm{MHz}$ (unless otherwise specified).
2. VBW $\geq 3 \times$ RBW.
3. Detector $=$ RMS (Number of points $\geq 2 \times$ Span $/$ RBW)
4. Averaging type $=$ power. (i.e., RMS)
5. Sweep time = auto.
6. Perform a trace average of at least 100 traces.
7. A correction factor shall be added to the measurement results prior to comparing to the emission limit in order to compute the emission level that would have been measured had the test been performed at 100 percent duty cycle. The correction factor is computed as follows:
1) If power averaging (RMS) mode was used in step 4, then the applicable correction factor is $10 \log (1 / D)$, where $D$ is the duty cycle.
2) If linear voltage averaging mode was used in step 4, then the applicable correction factor is $20 \log (1 / D)$, where $D$ is the duty cycle.
3) If a specific emission is demonstrated to be continuous ( $\geq 98$ percent duty cycle) rather than turning on and off with the transmit cycle, then no duty cycle correction is required for that emission.

## Duty Cycle Correction factor

| Test Mode | Date rate | Ton(ms) | Ton+off (ms) | $\mathbf{D}=T_{\text {on }}$ (Ton+off) | DCCF = 10 log(1/D) <br> (dB) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| TM 1 | 1 Mbps | 12.420 | 12.510 | 0.9928 | $\mathrm{~N} / \mathrm{A}$ |
| TM 2 | 6 Mbps | 2.064 | 2.165 | 0.9533 | 0.21 |
| TM 3 | MCS 0 | 0.249 | 0.350 | 0.7122 | 1.47 |

Note1: Where, T= Transmission duration / D= Duty cycle
Note2: Please refer to the appendix I for duty cycle plots.

■ Test Results: Comply

Radiated Spurious Emissions data( $9 \mathrm{kHz} \sim 25 \mathrm{GHz}$ ) : TM 1 \& MN: ADB10S2ANO

| Tested Frequency | Frequency $(\mathrm{MHz})$ | $\begin{gathered} \text { ANT } \\ \text { Pol } \end{gathered}$ | EUT Position (Axis) | Detector Mode | Reading (dBuV) | $\begin{gathered} \mathrm{T} . \mathrm{F} \\ (\mathrm{~dB} / \mathrm{m}) \end{gathered}$ | DCCF <br> (dB) | $\begin{aligned} & \text { DCF } \\ & \text { (dB) } \end{aligned}$ | Result (dBuV/m) | $\underset{(\mathrm{dBuV} / \mathrm{m})}{\text { Limit }}$ | Margin (dB) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lowest | 2389.32 | V | X | PK | 50.00 | 5.23 | N/A | N/A | 55.23 | 74.00 | 18.77 |
|  | 2388.91 | V | X | AV | 39.57 | 5.23 | N/A | N/A | 44.80 | 54.00 | 9.20 |
|  | 4824.31 | V | X | PK | 49.82 | 1.59 | N/A | N/A | 51.41 | 74.00 | 22.59 |
|  | 4823.76 | V | X | AV | 39.02 | 1.58 | N/A | N/A | 40.60 | 54.00 | 13.40 |
|  | 7234.68 | V | X | PK | 49.94 | 8.97 | N/A | N/A | 58.91 | 74.00 | 15.09 |
|  | 7234.77 | V | X | AV | 41.23 | 8.97 | N/A | N/A | 50.20 | 54.00 | 3.80 |
| Middle | 4873.74 | V | X | PK | 46.88 | 1.82 | N/A | N/A | 48.70 | 74.00 | 25.30 |
|  | 4873.58 | V | X | AV | 36.71 | 1.82 | N/A | N/A | 38.53 | 54.00 | 15.47 |
|  | 7309.47 | V | X | PK | 48.05 | 9.72 | N/A | N/A | 57.77 | 74.00 | 16.23 |
|  | 7309.75 | V | X | AV | 39.31 | 9.73 | N/A | N/A | 49.04 | 54.00 | 4.96 |
| Highest | 2484.03 | V | X | PK | 49.64 | 5.79 | N/A | N/A | 55.43 | 74.00 | 18.57 |
|  | 2483.86 | V | X | AV | 38.88 | 5.79 | N/A | N/A | 44.67 | 54.00 | 9.33 |
|  | 4923.76 | V | X | PK | 50.29 | 2.10 | N/A | N/A | 52.39 | 74.00 | 21.61 |
|  | 4923.53 | V | X | AV | 39.77 | 2.10 | N/A | N/A | 41.87 | 54.00 | 12.13 |
|  | 7385.03 | V | X | PK | 48.91 | 9.78 | N/A | N/A | 58.69 | 74.00 | 15.31 |
|  | 7384.68 | V | X | AV | 40.43 | 9.78 | N/A | N/A | 50.21 | 54.00 | 3.79 |

## Note.

1. The radiated emissions were investigated up to 25 GHz . And no other spurious and harmonic emissions were found above listed frequencies.
2. Sample Calculation.

Margin $=$ Limit - Result $/ \quad$ Result $=$ Reading + T.F + DCCF + DCF / T.F $=$ AF + CL - AG
Where, T.F = Total Factor, $\mathrm{AF}=$ Antenna Factor, $\mathrm{CL}=$ Cable Loss, $\mathrm{AG}=$ Amplifier Gain,
DCCF = Duty Cycle Correction Factor, DCF = Distance Correction Factor
3. Information of Distance Factor.

For finding emissions, the test distance might be reduced from 3 m to 1 m . In this case, the distance factor( -9.54 dB ) is applied to the result.

- Calculation of distance factor $=20 \log ($ applied distance $/$ required distance $)=20 \log (1 \mathrm{~m} / 3 \mathrm{~m})=-9.54 \mathrm{~dB}$

Radiated Spurious Emissions data(9 kHz ~ 25 GHz ) : TM 2 \& MN: ADB10S2ANO

| Tested Frequency | Frequency $(\mathrm{MHz})$ | $\begin{gathered} \text { ANT } \\ \text { Pol } \end{gathered}$ | EUT Position (Axis) | Detector Mode | Reading (dBuV) | $\begin{gathered} \text { T.F } \\ (\mathrm{dB} / \mathrm{m}) \end{gathered}$ | DCCF <br> (dB) | DCF <br> (dB) | Result (dBuV/m) | $\underset{(\mathrm{dBuV} / \mathrm{m})}{\operatorname{Limit}_{\text {( }}^{2}}$ | $\underset{\text { (dB) }}{\text { Margin }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lowest | 2389.32 | V | X | PK | 52.40 | 5.23 | N/A | N/A | 57.63 | 74.00 | 16.37 |
|  | 2389.59 | V | X | AV | 41.82 | 5.24 | 0.21 | N/A | 47.27 | 54.00 | 6.73 |
|  | 4823.67 | V | X | PK | 49.49 | 1.58 | N/A | N/A | 51.07 | 74.00 | 22.93 |
|  | 4823.82 | V | X | AV | 39.37 | 1.58 | 0.21 | N/A | 41.16 | 54.00 | 12.84 |
|  | 7235.63 | V | X | PK | 54.44 | 8.98 | N/A | N/A | 63.42 | 74.00 | 10.58 |
|  | 7235.95 | V | $X$ | AV | 38.75 | 8.99 | 0.21 | N/A | 47.95 | 54.00 | 6.05 |
| Middle | 4873.82 | V | X | PK | 50.10 | 1.82 | N/A | N/A | 51.92 | 74.00 | 22.08 |
|  | 4874.16 | V | X | AV | 39.52 | 1.83 | 0.21 | N/A | 41.56 | 54.00 | 12.44 |
|  | 7311.36 | V | X | PK | 51.51 | 9.74 | N/A | N/A | 61.25 | 74.00 | 12.75 |
|  | 7311.13 | V | X | AV | 36.63 | 9.74 | 0.21 | N/A | 46.58 | 54.00 | 7.42 |
| Highest | 2483.67 | V | X | PK | 49.13 | 5.79 | N/A | N/A | 54.92 | 74.00 | 19.08 |
|  | 2484.12 | V | X | AV | 39.86 | 5.79 | 0.21 | N/A | 45.86 | 54.00 | 8.14 |
|  | 4923.69 | V | X | PK | 50.10 | 2.10 | N/A | N/A | 52.20 | 74.00 | 21.80 |
|  | 4924.19 | V | X | AV | 39.54 | 2.10 | 0.21 | N/A | 41.85 | 54.00 | 12.15 |
|  | 7386.15 | V | X | PK | 53.00 | 9.78 | N/A | N/A | 62.78 | 74.00 | 11.22 |
|  | 7386.10 | V | X | AV | 37.53 | 9.78 | 0.21 | N/A | 47.52 | 54.00 | 6.48 |

Note.

1. The radiated emissions were investigated up to 25 GHz . And no other spurious and harmonic emissions were found above listed frequencies.
2. Sample Calculation.

Margin = Limit - Result / Result $=$ Reading + T.F+ DCCF + DCF / T.F = AF + CL -AG
Where, T.F = Total Factor, $\mathrm{AF}=$ Antenna Factor, $\quad \mathrm{CL}=$ Cable Loss, $\mathrm{AG}=$ Amplifier Gain, DCCF = Duty Cycle Correction Factor, DCF = Distance Correction Factor
3. Information of Distance Factor.

For finding emissions, the test distance might be reduced from 3 m to 1 m . In this case, the distance factor( -9.54 dB ) is applied to the result.

- Calculation of distance factor $=20 \log ($ applied distance $/$ required distance $)=20 \log (1 \mathrm{~m} / 3 \mathrm{~m})=-9.54 \mathrm{~dB}$

Radiated Spurious Emissions data(9 kHz ~ 25 GHz ) : TM 3 \& MN: ADB10S2ANO

| Tested Frequency | Frequency $(\mathrm{MHz})$ | $\begin{gathered} \text { ANT } \\ \text { Pol } \end{gathered}$ | EUT Position (Axis) | Detector Mode | Reading (dBuV) | $\begin{gathered} \text { T.F } \\ (\mathrm{dB} / \mathrm{m}) \end{gathered}$ | DCCF <br> (dB) | DCF <br> (dB) | Result (dBuV/m) | $\underset{(\mathrm{dBuV} / \mathrm{m})}{\operatorname{Limit}_{\text {( }}^{2}}$ | $\underset{\text { (dB) }}{\text { Margin }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lowest | 2389.05 | V | X | PK | 50.84 | 5.23 | N/A | N/A | 56.07 | 74.00 | 17.93 |
|  | 2389.45 | V | X | AV | 40.66 | 5.23 | 1.47 | N/A | 47.36 | 54.00 | 6.64 |
|  | 4824.47 | V | X | PK | 50.07 | 1.59 | N/A | N/A | 51.66 | 74.00 | 22.34 |
|  | 4823.51 | V | X | AV | 39.14 | 1.58 | 1.47 | N/A | 42.19 | 54.00 | 11.81 |
|  | 7236.36 | V | X | PK | 50.30 | 8.99 | N/A | N/A | 59.29 | 74.00 | 14.71 |
|  | 7236.03 | V | $X$ | AV | 36.74 | 8.99 | 1.47 | N/A | 47.20 | 54.00 | 6.80 |
| Middle | 4873.82 | V | X | PK | 49.86 | 1.82 | N/A | N/A | 51.68 | 74.00 | 22.32 |
|  | 4874.43 | V | X | AV | 39.44 | 1.83 | 1.47 | N/A | 42.74 | 54.00 | 11.26 |
|  | 7310.99 | V | X | PK | 50.27 | 9.74 | N/A | N/A | 60.01 | 74.00 | 13.99 |
|  | 7310.55 | V | X | AV | 35.97 | 9.73 | 1.47 | N/A | 47.17 | 54.00 | 6.83 |
| Highest | 2483.84 | V | X | PK | 50.42 | 5.79 | N/A | N/A | 56.21 | 74.00 | 17.79 |
|  | 2483.74 | V | X | AV | 39.63 | 5.79 | 1.47 | N/A | 46.89 | 54.00 | 7.11 |
|  | 4923.86 | V | X | PK | 49.99 | 2.10 | N/A | N/A | 52.09 | 74.00 | 21.91 |
|  | 4923.97 | V | X | AV | 39.47 | 2.10 | 1.47 | N/A | 43.04 | 54.00 | 10.96 |
|  | 7385.76 | V | X | PK | 50.14 | 9.78 | N/A | N/A | 59.92 | 74.00 | 14.08 |
|  | 7386.14 | V | X | AV | 36.37 | 9.78 | 1.47 | N/A | 47.62 | 54.00 | 6.38 |

Note.

1. The radiated emissions were investigated up to 25 GHz . And no other spurious and harmonic emissions were found above listed frequencies.
2. Sample Calculation.

Margin $=$ Limit - Result / Result $=$ Reading + T.F+ DCCF + DCF / T.F = AF + CL -AG
Where, T.F = Total Factor, $\mathrm{AF}=$ Antenna Factor, $\quad \mathrm{CL}=$ Cable Loss, $\mathrm{AG}=$ Amplifier Gain, DCCF = Duty Cycle Correction Factor, DCF = Distance Correction Factor
3. Information of Distance Factor.

For finding emissions, the test distance might be reduced from 3 m to 1 m . In this case, the distance factor( -9.54 dB ) is applied to the result.

- Calculation of distance factor $=20 \log ($ applied distance $/$ required distance $)=20 \log (1 \mathrm{~m} / 3 \mathrm{~m})=-9.54 \mathrm{~dB}$

Radiated Spurious Emissions data(9 kHz ~25 GHz) : TM 1 \& MN: ADB40S2AN

| Tested Frequency | Frequency $(\mathrm{MHz})$ | $\begin{gathered} \text { ANT } \\ \text { Pol } \end{gathered}$ | EUT Position (Axis) | Detector Mode | Reading (dBuV) | $\begin{gathered} \mathrm{T} . \mathrm{F} \\ (\mathrm{~dB} / \mathrm{m}) \end{gathered}$ | $\underset{\text { (dB) }}{\text { DCCF }}$ | $\begin{aligned} & \text { DCF } \\ & \text { (dB) } \end{aligned}$ | Result (dBuV/m) | $\underset{(\mathrm{dBuV} / \mathrm{m})}{\mathrm{Limit}}$ | $\underset{\text { (dB) }}{\substack{\text { Margin }}}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lowest | 2388.98 | V | X | PK | 48.99 | 5.23 | N/A | N/A | 54.22 | 74.00 | 19.78 |
|  | 2389.63 | V | X | AV | 39.11 | 5.24 | N/A | N/A | 44.35 | 54.00 | 9.65 |
|  | 4824.32 | V | X | PK | 49.05 | 1.56 | N/A | N/A | 50.61 | 74.00 | 23.39 |
|  | 4824.08 | V | X | AV | 38.70 | 1.56 | N/A | N/A | 40.26 | 54.00 | 13.74 |
|  | 7234.57 | V | X | PK | 48.60 | 8.97 | N/A | N/A | 57.57 | 74.00 | 16.43 |
|  | 7234.82 | V | X | AV | 39.54 | 8.97 | N/A | N/A | 48.51 | 54.00 | 5.49 |
| Middle | 4874.24 | V | X | PK | 49.60 | 1.80 | N/A | N/A | 51.40 | 74.00 | 22.60 |
|  | 4874.31 | V | X | AV | 38.95 | 1.80 | N/A | N/A | 40.75 | 54.00 | 13.25 |
|  | 7309.91 | V | X | PK | 48.33 | 9.73 | N/A | N/A | 58.06 | 74.00 | 15.94 |
|  | 7309.41 | V | X | AV | 39.34 | 9.72 | N/A | N/A | 49.06 | 54.00 | 4.94 |
| Highest | 2484.62 | V | X | PK | 48.56 | 5.81 | N/A | N/A | 54.37 | 74.00 | 19.63 |
|  | 2484.27 | V | X | AV | 38.89 | 5.81 | N/A | N/A | 44.70 | 54.00 | 9.30 |
|  | 4923.54 | V | X | PK | 49.75 | 2.07 | N/A | N/A | 51.82 | 74.00 | 22.18 |
|  | 4924.45 | V | X | AV | 39.08 | 2.07 | N/A | N/A | 41.15 | 54.00 | 12.85 |
|  | 7384.45 | V | X | PK | 48.59 | 9.78 | N/A | N/A | 58.37 | 74.00 | 15.63 |
|  | 7384.38 | V | X | AV | 39.29 | 9.78 | N/A | N/A | 49.07 | 54.00 | 4.93 |

Note.
4. The radiated emissions were investigated up to 25 GHz . And no other spurious and harmonic emissions were found above listed frequencies.
5. Sample Calculation.

Margin = Limit - Result / Result = Reading + T.F+ DCCF + DCF / T.F = AF + CL - AG
Where, T.F = Total Factor, AF = Antenna Factor, CL = Cable Loss, AG = Amplifier Gain, DCCF = Duty Cycle Correction Factor, DCF = Distance Correction Factor
6. Information of Distance Factor.

For finding emissions, the test distance might be reduced from 3 m to 1 m . In this case, the distance factor( -9.54 dB ) is applied to the result.

- Calculation of distance factor $=20 \log ($ applied distance $/$ required distance $)=20 \log (1 \mathrm{~m} / 3 \mathrm{~m})=-9.54 \mathrm{~dB}$

Radiated Spurious Emissions data(9 kHz ~25 GHz) : TM 2 \& MN: ADB40S2AN

| Tested Frequency | Frequency $(\mathrm{MHz})$ | $\begin{gathered} \text { ANT } \\ \text { Pol } \end{gathered}$ | EUT Position (Axis) | Detector Mode | Reading (dBuV) | $\begin{gathered} \text { T.F } \\ (\mathrm{dB} / \mathrm{m}) \end{gathered}$ | $\begin{gathered} \text { DCCF } \\ \text { (dB) } \end{gathered}$ | DCF <br> (dB) | Result (dBuV/m) | $\underset{\text { (dBuV/m) }}{\text { Limit }}$ | $\underset{\text { (dB) }}{\text { Margin }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lowest | 2389.75 | V | X | PK | 50.28 | 5.24 | N/A | N/A | 55.52 | 74.00 | 18.48 |
|  | 2389.29 | V | X | AV | 40.32 | 5.23 | 0.21 | N/A | 45.76 | 54.00 | 8.24 |
|  | 4823.62 | V | X | PK | 49.28 | 1.56 | N/A | N/A | 50.84 | 74.00 | 23.16 |
|  | 4824.44 | V | X | AV | 38.76 | 1.56 | 0.21 | N/A | 40.53 | 54.00 | 13.47 |
|  | 7235.56 | V | X | PK | 53.27 | 8.98 | N/A | N/A | 62.25 | 74.00 | 11.75 |
|  | 7236.35 | V | $X$ | AV | 37.39 | 8.99 | 0.21 | N/A | 46.59 | 54.00 | 7.41 |
| Middle | 4874.06 | V | X | PK | 49.70 | 1.80 | N/A | N/A | 51.50 | 74.00 | 22.50 |
|  | 4874.23 | V | X | AV | 39.11 | 1.80 | 0.21 | N/A | 41.12 | 54.00 | 12.88 |
|  | 7311.00 | V | X | PK | 53.21 | 9.74 | N/A | N/A | 62.95 | 74.00 | 11.05 |
|  | 7310.61 | V | X | AV | 37.08 | 9.74 | 0.21 | N/A | 47.03 | 54.00 | 6.97 |
| Highest | 2483.68 | V | X | PK | 48.83 | 5.80 | N/A | N/A | 54.63 | 74.00 | 19.37 |
|  | 2483.76 | V | X | AV | 39.59 | 5.80 | 0.21 | N/A | 45.60 | 54.00 | 8.40 |
|  | 4923.56 | V | X | PK | 50.09 | 2.07 | N/A | N/A | 52.16 | 74.00 | 21.84 |
|  | 4924.03 | V | X | AV | 39.03 | 2.07 | 0.21 | N/A | 41.31 | 54.00 | 12.69 |
|  | 7385.56 | V | X | PK | 53.79 | 9.78 | N/A | N/A | 63.57 | 74.00 | 10.43 |
|  | 7386.34 | V | X | AV | 37.20 | 9.78 | 0.21 | N/A | 47.19 | 54.00 | 6.81 |

Note.
4. The radiated emissions were investigated up to 25 GHz . And no other spurious and harmonic emissions were found above listed frequencies.
5. Sample Calculation.

Margin = Limit - Result / Result $=$ Reading + T.F+ DCCF + DCF / T.F = AF + CL -AG
Where, T.F = Total Factor, $\mathrm{AF}=$ Antenna Factor, $\quad \mathrm{CL}=$ Cable Loss, $\mathrm{AG}=$ Amplifier Gain, DCCF = Duty Cycle Correction Factor, DCF = Distance Correction Factor
6. Information of Distance Factor.

For finding emissions, the test distance might be reduced from 3 m to 1 m . In this case, the distance factor( -9.54 dB ) is applied to the result.

- Calculation of distance factor $=20 \log ($ applied distance $/$ required distance $)=20 \log (1 \mathrm{~m} / 3 \mathrm{~m})=-9.54 \mathrm{~dB}$

Radiated Spurious Emissions data(9 kHz ~25 GHz) : TM 3 \& MN: ADB40S2AN

| Tested Frequency | Frequency $(\mathrm{MHz})$ | $\begin{gathered} \text { ANT } \\ \text { Pol } \end{gathered}$ | EUT Position (Axis) | Detector Mode | Reading (dBuV) | $\begin{gathered} \text { T.F } \\ (\mathrm{dB} / \mathrm{m}) \end{gathered}$ | DCCF <br> (dB) | DCF <br> (dB) | Result (dBuV/m) | $\underset{(\mathrm{dBuV} / \mathrm{m})}{\operatorname{Limit}_{\text {( }}^{2}}$ | $\underset{\text { (dB) }}{\text { Margin }}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lowest | 2388.68 | V | X | PK | 50.87 | 5.23 | N/A | N/A | 56.10 | 74.00 | 17.90 |
|  | 2389.16 | V | X | AV | 40.03 | 5.23 | 1.47 | N/A | 46.73 | 54.00 | 7.27 |
|  | 4823.81 | V | X | PK | 48.89 | 1.56 | N/A | N/A | 50.45 | 74.00 | 23.55 |
|  | 4824.12 | V | X | AV | 38.95 | 1.56 | 1.47 | N/A | 41.98 | 54.00 | 12.02 |
|  | 7235.94 | V | X | PK | 52.96 | 8.98 | N/A | N/A | 61.94 | 74.00 | 12.06 |
|  | 7236.02 | V | $X$ | AV | 36.97 | 8.99 | 1.47 | N/A | 47.43 | 54.00 | 6.57 |
| Middle | 4873.94 | V | X | PK | 49.51 | 1.80 | N/A | N/A | 51.31 | 74.00 | 22.69 |
|  | 4874.31 | V | X | AV | 39.77 | 1.80 | 1.47 | N/A | 43.04 | 54.00 | 10.96 |
|  | 7311.07 | V | X | PK | 52.85 | 9.74 | N/A | N/A | 62.59 | 74.00 | 11.41 |
|  | 7310.84 | V | X | AV | 37.98 | 9.74 | 1.47 | N/A | 49.19 | 54.00 | 4.81 |
| Highest | 2485.46 | V | X | PK | 50.62 | 5.82 | N/A | N/A | 56.44 | 74.00 | 17.56 |
|  | 2484.39 | V | X | AV | 39.42 | 5.81 | 1.47 | N/A | 46.70 | 54.00 | 7.30 |
|  | 4923.62 | V | X | PK | 50.86 | 2.07 | N/A | N/A | 52.93 | 74.00 | 21.07 |
|  | 4923.67 | V | X | AV | 39.73 | 2.07 | 1.47 | N/A | 43.27 | 54.00 | 10.73 |
|  | 7385.94 | V | X | PK | 53.93 | 9.78 | N/A | N/A | 63.71 | 74.00 | 10.29 |
|  | 7386.17 | V | X | AV | 37.59 | 9.78 | 1.47 | N/A | 48.84 | 54.00 | 5.16 |

Note.
4. The radiated emissions were investigated up to 25 GHz . And no other spurious and harmonic emissions were found above listed frequencies.
5. Sample Calculation.

Margin $=$ Limit - Result / Result $=$ Reading + T.F+ DCCF + DCF / T.F = AF + CL -AG
Where, T.F = Total Factor, $\mathrm{AF}=$ Antenna Factor, $\quad \mathrm{CL}=$ Cable Loss, $\mathrm{AG}=$ Amplifier Gain, DCCF = Duty Cycle Correction Factor, DCF = Distance Correction Factor
6. Information of Distance Factor.

For finding emissions, the test distance might be reduced from 3 m to 1 m . In this case, the distance factor(-9.54dB) is applied to the result.

- Calculation of distance factor $=20 \log ($ applied distance $/$ required distance $)=20 \log (1 \mathrm{~m} / 3 \mathrm{~m})=-9.54 \mathrm{~dB}$


### 8.6 Power-line conducted emissions

■ Test Requirements and limit, $\S 15.207$
For an intentional radiator which is designed to be connected to the public utility (AC) power line, the radio frequency voltage that is conducted back onto the AC power line on any frequency or frequencies within the band 150 kHz to 30 MHz shall not exceed the limits in the following table, as measured using a $50 \mathrm{uH} / 50$ ohm line impedance stabilization network(LISN).

Compliance with the provision of this paragraph shall on the measurement of the radio frequency voltage between each power line and ground at the power terminal. The lower applies at the boundary between the frequency ranges.

| Frequency Range <br> $(M H z)$ | Conducted Limit (dBuV) |  |
| :---: | :---: | :---: |
|  | Quasi-Peak | Average |
| $0.15 \sim 0.5$ | 66 to $56{ }^{*}$ | 56 to $46{ }^{*}$ |
| $0.5 \sim 5$ | 56 | 46 |
| $5 \sim 30$ | 60 | 50 |

* Decreases with the logarithm of the frequency

Compliance with this provision shall be based on the measurement of the radio frequency voltage between each power line (LINE and NEUTRAL) and ground at the power terminals.

## $\square$ Test Procedure

1. The EUT is placed on a wooden table 80 cm above the reference ground plane.
2. The EUT is connected via LISN to the test power supply.
3. The measurement results are obtained as described below:
4. Detectors - Quasi Peak and Average Detector.

- Test Results: NA

FCC ID: TQ8-ADB10S2AN0

## 9. LIST OF TEST EQUIPMENT

| Type | Manufacturer | Model | Cal.Date (yy/mm/dd) | Next.Cal.Date ( $\mathrm{y} / \mathrm{mm} / \mathrm{dd}$ ) | S/N |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Spectrum Analyzer | Agilent Technologies | N9020A | 19/12/16 | 20/12/16 | MY49060056 |
| Spectrum Analyzer | Agilent Technologies | N9020A | 19/12/16 | 20/12/16 | MY48011700 |
| Spectrum Analyzer | Agilent Technologies | N9020A | 19/12/16 | 20/12/16 | MY48010133 |
| DC Power Supply | Agilent Technologies | 66332A | 19/12/16 | 20/12/16 | US37476998 |
| DC Power Supply | SM techno | SDP30-5D | 19/06/24 | 20/06/24 | 305DMG305 |
| Multimeter | FLUKE | 17B | 19/12/16 | 20/12/16 | 26030065WS |
| Signal Generator | Rohde Schwarz | SMBV100A | 19/12/16 | 20/12/16 | 255571 |
| Signal Generator | ANRITSU | MG3695C | 19/12/16 | 20/12/16 | 173501 |
| Thermohygrometer | BODYCOM | BJ5478 | 19/12/18 | 20/12/18 | 120612-1 |
| Thermohygrometer | BODYCOM | BJ5478 | 19/12/18 | 20/12/18 | 120612-2 |
| Thermohygrometer | BODYCOM | BJ5478 | 19/06/25 | 20/06/25 | N/A |
| Loop Antenna | ETS-Lindgren | 6502 | 19/09/18 | 21/09/18 | 00226186 |
| BILOG ANTENNA | Schwarzbeck | VULB 9160 | 19/04/23 | 21/04/23 | 9160-3362 |
| Horn Antenna | ETS-Lindgren | 3115 | 19/01/11 | 21/01/11 | 9202-3820 |
| Horn Antenna | A.H.Systems Inc. | SAS-574 | 19/07/03 | 21/07/03 | 155 |
| PreAmplifier | tsj | MLA-0118-B01-40 | 19/12/16 | 20/12/16 | 1852267 |
| PreAmplifier | tsj | MLA-1840-J02-45 | 19/06/27 | 20/06/27 | 16966-10728 |
| PreAmplifier | H.P | 8447D | 19/12/16 | 20/12/16 | 2944A07774 |
| High Pass Filter | Wainwright Instruments | WHKX12-935-1000-15000-40SS | 19/06/26 | 20/06/26 | 8 |
| High Pass Filter | Wainwright Instruments | $\begin{aligned} & \text { WHKX10-2838-3300- } \\ & \text { 18000-60SS } \end{aligned}$ | 19/06/26 | 20/06/26 | 1 |
| High Pass Filter | Wainwright Instruments | WHNX8.0/26.5-6SS | 19/06/27 | 20/06/27 | 3 |
| Attenuator | Hefei Shunze | SS5T2.92-10-40 | 19/06/27 | 20/06/27 | 16012202 |
| Attenuator | SRTechnology | F01-B0606-01 | 19/06/27 | 20/06/27 | 13092403 |
| Attenuator | Aeroflex/Weinschel | 20515 | 19/06/27 | 20/06/27 | Y2370 |
| Attenuator | SMAJK | SMAJK-2-3 | 19/06/27 | 20/06/27 | 2 |
| Attenuator | SMAJK | SMAJK-50-10 | 19/06/25 | 20/06/25 | 15081903 |
| Power Meter \& Wide Bandwidth Sensor | Anritsu | $\begin{aligned} & \hline \text { ML2495A } \\ & \text { MA2490A } \end{aligned}$ | 19/06/24 | 20/06/24 | $\begin{aligned} & 1306007 \\ & 1249001 \end{aligned}$ |
| EMI Receiver | ROHDE\&SCHWARZ | ESW44 | 19/07/30 | 20/07/30 | 101645 |
| Cable | Junkosha | MWX241 | 20/01/13 | 21/01/13 | G-04 |
| Cable | Junkosha | MWX241 | 20/01/13 | 21/01/13 | G-07 |
| Cable | DT\&C | Cable | 20/01/13 | 21/01/13 | G-13 |
| Cable | DT\&C | Cable | 20/01/13 | 21/01/13 | G-14 |
| Cable | HUBER+SUHNER | SUCOFLEX 104 | 20/01/13 | 21/01/13 | G-15 |
| Cable | Radiall | TESTPRO3 | 20/01/16 | 21/01/16 | M-01 |
| Cable | Junkosha | MWX315 | 20/01/16 | 21/01/16 | M-05 |
| Cable | Junkosha | MWX221 | 20/01/16 | 21/01/16 | M-06 |
| Cable | Radiall | TESTPRO3 | 20/01/15 | 21/01/15 | RF-65 |

Note 1: The measurement antennas were calibrated in accordance to the requirements of ANSI C63.5-2017
Note 2: The cable is not a regular calibration item, so it has been calibrated by DT \& C itself.

## APPENDIX I

## Test set up diagrams

## - Radiated Measurement



## - Conducted Measurement



Cable A

Path loss information

| Frequency (GHz) | Path Loss (dB) | Frequency (GHz) | Path Loss (dB) |
| :---: | :---: | :---: | :---: |
| 0.03 | 9.63 | 15 | 11.67 |
| 1 | 9.91 | 20 | 12.46 |
| $2.412 \& 2.437 \& 2.462$ | 10.41 | 25 | 12.8 |
| 5 | 10.48 | - | - |
| 10 | 10.60 | - | - |

Note 1: The path loss from EUT to Spectrum analyzer was measured and used for test.
Path loss (S/A's correction factor) = Cable A

## APPENDIX II

## Duty cycle plots

## - Test Procedure

Duty Cycle was measured using section 6.0 b) of KDB558074 D01v05r02 :
The zero-span mode on a spectrum analyzer or EMI receiver if the response time and spacing between bins on the sweep are sufficient to permit accurate measurements of the on and off times of the transmitted signal. Set the center frequency of the instrument to the center frequency of the transmission. Set RBW $\geq$ OBW if possible; otherwise, set RBW to the largest available value. Set VBW $\geq$ RBW. Set detector $=$ peak or average .

The zero-span measurement method shall not be used unless both RBW and VBW are $>50 / \mathrm{T}$ and the number of sweep points across duration T exceeds 100. (For example, if VBW and/or RBW are limited to 3 MHz , then the zero-span method of measuring duty cycle shall not be used if $\mathrm{T} \leq 16.7$ microseconds.)

## Duty Cycle

TM $1 \quad$ \& Middle


Duty Cycle
TM 2


Duty Cycle


## APPENDIX III

Unwanted Emissions (Radiated) Test Plot _ MN: ADB10S2AN0

TM 1 \& Lowest \& X axis \& Ver
Detector Mode : PK


TM 1 \& Lowest \& X axis \& Ver
Detector Mode : AV


TM 1 \& Highest \& X axis \& Ver
Detector Mode : PK


TM 1 \& Highest \& X axis \& Ver
Detector Mode : AV


TM 2 \& Lowest \& X axis \& Ver
Detector Mode : PK


TM 2 \& Lowest \& X axis \& Ver
Detector Mode : AV


TM 2 \& Highest \& X axis \& Ver
Detector Mode : PK


TM 2 \& Highest \& X axis \& Ver
Detector Mode : AV


TM 3 \& Lowest \& $X$ axis \& Ver
Detector Mode : PK


TM 3 \& Lowest \& $X$ axis \& Ver
Detector Mode : AV


TM 3 \& Highest \& X axis \& Ver
Detector Mode : PK


TM 3 \& Highest \& X axis \& Ver
Detector Mode : AV


TM 1 \& Highest \& X axis \& Ver
Detector Mode : AV


TM 2 \& Lowest \& $X$ axis \& Ver
Detector Mode : AV


TM 3 \& Highest \& $X$ axis \& Ver


TM 1 \& Lowest \& X axis \& Ver
Detector Mode : PK


TM 1 \& Lowest \& X axis \& Ver
Detector Mode : AV


TM 1 \& Highest \& X axis \& Ver
Detector Mode : PK


TM 1 \& Highest \& X axis \& Ver
Detector Mode : AV


TM 2 \& Lowest \& $X$ axis \& Ver
Detector Mode : PK


TM 2 \& Lowest \& $X$ axis \& Ver
Detector Mode : AV


TM 2 \& Highest \& X axis \& Ver
Detector Mode : PK


TM 2 \& Highest \& X axis \& Ver
Detector Mode : AV


TM 3 \& Lowest \& $X$ axis \& Ver
Detector Mode : PK


TM 3 \& Lowest \& $X$ axis \& Ver
Detector Mode : AV


TM 3 \& Highest \& X axis \& Ver
Detector Mode : PK


TM 3 \& Highest \& X axis \& Ver
Detector Mode : AV


TM 1 \& Highes \& X axis \& Ver
Detector Mode : AV


TM 2 \& Highest \& X axis \& Ver
Detector Mode : AV


TM 3 \& Middle \& $X$ axis \& Ver
Detector Mode : AV


