# SmartLabs, Inc. 

## TEST REPORT FOR

Inline Dual Load Module, FanLinc ${ }^{\text {TM }}$ \#2475F

## Tested To The Following Standards:

FCC Part 15 Subpart C Sections 15.207, 15.249
and
RSS 210 Issue 8

Report No.: 92499-4

Date of issue: November 18, 2011


Testing Certificates: 803.01,803.02, 803.05, 803.06

This test report bears the accreditation symbol indicating that the testing performed herein meets the test and reporting requirements of ISO/IEC 17025 under the applicable scope of EMC testing for CKC Laboratories, Inc.

We strive to create long-term, trust based relationships by providing sound, adaptive, customer first testing services. We embrace each of our customers' unique EMC challenges, not as an interruption to set processes, but rather as the reason we are in business.

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## ADMINISTRATIVE INFORMATION

## Test Report Information

## REPORT PREPARED FOR:

SmartLabs, Inc.
16542 Millikan Ave.
Irvine, CA 92606

Representative: Chris Sy-Santos
Customer Reference Number: 11-3CS1103-01

DATE OF EQUIPMENT RECEIPT:
DATES) OF TESTING:

REPORT PREPARED BY:

Dianne Dudley
CKC Laboratories, Inc.
5046 Sierra Pines Drive
Mariposa, CA 95338

Project Number: 92499

November 11, 2011
November 11, 2011

## Report Authorization

The test data contained in this report documents the observed testing parameters pertaining to and are relevant for only the sample equipment tested in the agreed upon operational modes) and configurations) as identified herein. Compliance assessment remains the client's responsibility. This report may not be used to claim product endorsement by A2LA or any government agencies. This test report has been authorized for release under quality control from CKC Laboratories, Inc.


Steve Behm
Director of Quality Assurance \& Engineering Services CKC Laboratories, Inc.

Test Facility Information


Our laboratories are configured to effectively test a wide variety of product types. CKC utilizes first class test equipment, anechoic chambers, data acquisition and information services to create accurate, repeatable and affordable test results.

TEST LOCATION(S):
CKC Laboratories, Inc.
110 Olinda Place
Brea, CA 92823

## Site Registration \& Accreditation Information

| Location | CB \# | Japan | Canada | FCC |
| :---: | :---: | :---: | :---: | :---: |
| Brea A | US0060 | R-2945, C-3248 \& T-1572 | 3082D-1 | 90473 |

LABORATORIES, INC.

## SUMMARY OF RESULTS

## Standard / Specification: FCC Part 15 Subpart C

| Description | Test Procedure/Method | Results |
| :--- | :--- | :---: |
|  |  | Pass |
| Voltage Variation | FCC Part 15 Subpart C Section 15.31(e) | Pass |
|  |  | Pass |
| Conducted Emissions | FCC Part 15 Subpart C Section 15.207 / ANSI C63.4 (2003) |  |
|  |  | FCC Part 15 Subpart C Section 15.249(a) |
| RF Power Output |  | Pass |
|  | FCC Part 15 Subpart C Section 15.249 | Pass |
| -20dBc Occupied Bandwidth |  | Pass |
|  | FCC | Pass |
| Bandedge |  |  |
| Radiated Spurious Emissions | FCC Part 15 Subpart C Section 15.249(d) |  |
|  |  | RSS 210 Issue 8 |
| 99\% Bandwidth |  |  |
|  |  |  |

## Conditions During Testing

This list is a summary of the conditions noted for or modifications made to the equipment during testing.

## Summary of Conditions

None

# EQUIPMENT UNDER TEST (EUT) 

## EQUIPMENT UNDER TEST

Inline Dual Load Module
Manuf: SmartLabs, Inc.
Model: FanLinc ${ }^{\text {TM }} \# 2475 F$
Serial: 14.8C.4A

## PERIPHERAL DEVICES

The EUT was tested with the following peripheral device(s):

Suspended Ceiling Fan
Manuf: Hunter
Model: 28683-530
Serial: NA

## FCC PART 15 SUBPART C

This report contains EMC emissions test results under United States Federal Communications Commission (FCC) 47 CFR 15C requirements for Unlicensed Radio Frequency Devices, Subpart C - Intentional Radiators.

### 15.31(e) Voltage Variations

## Test Conditions / Setup

The EUT is placed on the wooden table lined with Styrofoam. Total height is 1.5 meter from the ground plane. Connected to the EUT is a support suspended ceiling fan.
Continuous transmit
914.92MHz-915.08MHz

EUT only operates on $120 \mathrm{Vac} / 60 \mathrm{~Hz}$.
Frequency range of measurement $=30 \mathrm{MHz}-1 \mathrm{GHz}$.
$30 \mathrm{MHz}-1000 \mathrm{MHz}$; RBW=120 kHz, VBW=120 kHz

Temperature: $17^{\circ} \mathrm{C}$, Relative Humidity: $20 \%$
15.31(e): The supply voltage varied between $85 \%$ and $115 \%$ of the nominal rated supply voltage (120Vac), no change in the Fundamental signal level was observed.

Engineer Name: Don Nguyen
Test Equipment

| Asset/Serial \# | Description | Model | Manufacturer | Cal Date | Cal Due |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AN00309 | Preamp | 8447D | HP | $5 / 7 / 2010$ | $5 / 7 / 2012$ |
| AN01995 | Biconilog Antenna | CBL6111C | Chase | $3 / 8 / 2010$ | $3 / 8 / 2012$ |
| ANP05050 | Cable | RG223/U | Pasternack | $3 / 21 / 2011$ | $3 / 21 / 2013$ |
| ANP05198 | Cable | 8268 | Belden | $12 / 21 / 2010$ | $12 / 21 / 2012$ |
| AN02672 | Spectrum Analyzer | E4446A | Agilent | $8 / 9 / 2010$ | $8 / 9 / 2012$ |

Test Setup Photos


X AXIS FRONT VIEW


X AXIS BACK VIEW


Y AXIS FRONT VIEW


Y AXIS BACK VIEW


Z AXIS FRONT VIEW


Z AXIS BACK VIEW

### 15.207 AC Conducted Emissions

## Test Data Sheets

| Test Location: | CKC Laboratories • 110 Olinda Place • Brea, CA 92823 • 714-993-6112 |  |
| :--- | :--- | ---: |
|  |  |  |
| Customer: | SmartLabs, Inc. |  |
| Specification: | $\mathbf{1 5 . 2 0 7}$ AC Mains - Average |  |
| Work Order \#: | $\mathbf{9 2 4 9 9}$ | Date: 11/11/2011 |
| Test Type: | Conducted Emissions | Time: 11:37:20 |
| Equipment: | Inline Dual Load Module | Sequence\#: 13 |
| Manufacturer: | SmartLabs, Inc. | Tested By: |
| Model Nguyen |  | 120 V 60 Hz |
| S/N: | FanLinc |  |

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | ANP06085 | Attenuator | SA18N10W-09 | $12 / 8 / 2010$ | $12 / 8 / 2012$ |
| T2 | ANP01910 | Cable | RG-142 | $3 / 19 / 2010$ | $3 / 19 / 2012$ |
| T3 | AN02343 | High Pass Filter | HE9615-150K- <br> $50-720 B$ | $1 / 4 / 2011$ | $1 / 4 / 2013$ |
|  | AN02672 | Spectrum Analyzer | E4446A | $8 / 9 / 2010$ | $8 / 9 / 2012$ |
| T4 | AN00848.1 | 50uH LISN-Line 1 <br> (dB) | $3816 / 2 \mathrm{~nm}$ | $3 / 22 / 2011$ | $3 / 22 / 2013$ |
|  | AN00848.1 | 50uH LISN-Line 2 <br> $(d B)$ | $3816 / 2 \mathrm{~nm}$ | $3 / 22 / 2011$ | $3 / 22 / 2013$ |

Equipment Under Test (* : EUT):

| Function | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Inline Dual Load Module* | SmartLabs, Inc. | FanLinc $^{\mathrm{TM}} \# 2475 \mathrm{~F}$ | 14.8 C .4 A |
| Support Devices: |  |  |  |
| Function | Manufacturer | Model \# | S/N |
| Suspended Ceiling Fan | Hunter | $28683-530$ | NA |

## Test Conditions / Notes:

The EUT is placed on the wooden table lined with Styrofoam. Total height is 1.5 meter from the ground plane. Connected to the EUT is a support suspended ceiling fan.
Continuous transmit
914.92MHz-915.08MHz

EUT only operates on $120 \mathrm{Vac} / 60 \mathrm{~Hz}$.
Frequency range of measurement $=150 \mathrm{kHz}-30 \mathrm{MHz}$
$150 \mathrm{kHz}-30 \mathrm{MHz}$; RBW=9 kHz, VBW=9 kHz
$17^{\circ} \mathrm{C}, 20 \%$ Relative Humidity

Ext Attn: 0 dB
Measurement Data: Reading listed by margin. Test Lead: L1

| \# | Freq <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 3 \\ & \text { dB } \end{aligned}$ | $\begin{aligned} & \mathrm{T} 4 \\ & \mathrm{~dB} \end{aligned}$ | Dist Table | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} \end{gathered}$ | $\begin{gathered} \hline \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} \end{gathered}$ | $\begin{gathered} \text { Margin } \\ d B \end{gathered}$ | Polar Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 438.701k | 38.7 | +5.7 | +0.1 | +0.3 | +0.1 | +0.0 | 44.9 | 47.1 | -2.2 | L1 |
| 2 | 1.451M | 37.6 | +5.7 | +0.1 | +0.2 | +0.1 | +0.0 | 43.7 | 46.0 | -2.3 | L1 |
| 3 | 459.790k | 38.0 | +5.7 | +0.1 | +0.3 | +0.1 | +0.0 | 44.2 | 46.7 | -2.5 | L1 |
| 4 | 435.792k | 38.3 | +5.7 | +0.1 | +0.3 | +0.1 | +0.0 | 44.5 | 47.1 | -2.6 | L1 |
| 5 | 466.335k | 37.8 | +5.7 | +0.1 | +0.3 | +0.1 | +0.0 | 44.0 | 46.6 | -2.6 | L1 |
| 6 | 347.800k | 40.1 | +5.7 | +0.1 | +0.2 | +0.1 | +0.0 | 46.2 | 49.0 | -2.8 | L1 |
| 7 | 432.156k | 38.1 | +5.7 | +0.1 | +0.3 | +0.1 | +0.0 | 44.3 | 47.2 | -2.9 | L1 |
| 8 | 402.340k | 38.7 | +5.7 | +0.1 | +0.3 | +0.1 | +0.0 | 44.9 | 47.8 | -2.9 | L1 |
| 9 | 380.524 k | 39.2 | +5.7 | +0.1 | +0.2 | +0.1 | +0.0 | 45.3 | 48.3 | -3.0 | L1 |
| 10 | 267.807k | 41.9 | +5.7 | +0.1 | +0.2 | +0.1 | +0.0 | 48.0 | 51.2 | -3.2 | L1 |
| 11 | 167.453k | 45.6 | +5.7 | +0.1 | +0.4 | +0.1 | +0.0 | 51.9 | 55.1 | -3.2 | L1 |
| 12 | 411.067k | 38.2 | +5.7 | +0.1 | +0.3 | +0.1 | +0.0 | 44.4 | 47.6 | -3.2 | L1 |
| 13 | 388.524k | 38.8 | +5.7 | +0.1 | +0.2 | +0.1 | +0.0 | 44.9 | 48.1 | -3.2 | L1 |
| 14 | 456.881k | 37.2 | +5.7 | +0.1 | +0.3 | +0.1 | +0.0 | 43.4 | 46.7 | -3.3 | L1 |
|  | $446.700 \mathrm{k}$ <br> Ave | 26.2 | +5.7 | +0.1 | +0.3 | +0.1 | +0.0 | 32.4 | 46.9 | -14.5 | L1 |
| $\wedge$ | 446.700k | 38.9 | +5.7 | +0.1 | +0.3 | +0.1 | +0.0 | 45.1 | 46.9 | -1.8 | L1 |

CKC Laboratories Date: 11/11/2011 Time: 11:37:20 SmartLabs, Inc. WO\#: 92499 15.207 AC Mains - Average Test Lead: L1 120V 60Hz Sequence\#: 13 Ext ATTN: 0 dB


| Sweep Data | Readings |
| :--- | :--- |
| Peak Readings | $\times$ QP Readings |
| * Average Readings | $\boldsymbol{\nabla}$ Ambient |
|  | $1-15.207$ AC Mains - Average |
|  | $2-15.207$ AC Mains - Quasi-peak |

Test Location: CKC Laboratories • 110 Olinda Place • Brea, CA 92823 • 714-993-6112
Customer: SmartLabs, Inc.
Specification: 15.207 AC Mains - Average
Work Order \#: 92499
Test Type:
Equipment:
Manufacturer:
Model:

## Conducted Emissions

Inline Dual Load Module
SmartLabs, Inc.
FanLinc ${ }^{\text {TM }}$ \#2475F
Date: 11/11/2011
Time: 11:41:12
Sequence\#: 14
Tested By: Don Nguyen
120 V 60 Hz
S/N: 14.8C.4A
Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | ANP06085 | Attenuator | SA18N10W-09 | $12 / 8 / 2010$ | $12 / 8 / 2012$ |
| T2 | ANP01910 | Cable | RG-142 | $3 / 19 / 2010$ | $3 / 19 / 2012$ |
| T3 | AN02343 | High Pass Filter | HE9615-150K- <br> $50-720 B$ | $1 / 4 / 2011$ | $1 / 4 / 2013$ |
|  | AN02672 | Spectrum Analyzer | E4446A | $8 / 9 / 2010$ | $8 / 9 / 2012$ |
|  | AN00848.1 | 50 uH LISN-Line 1 <br> $(\mathrm{~dB})$ | $3816 / 2 \mathrm{~nm}$ | $3 / 22 / 2011$ | $3 / 22 / 2013$ |
| T4 | AN00848.1 | 50 uH LISN-Line 2 <br> $(\mathrm{~dB})$ | $3816 / 2 \mathrm{~nm}$ | $3 / 22 / 2011$ | $3 / 22 / 2013$ |

Equipment Under Test (* = EUT):

| Function | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Inline Dual Load Module* | SmartLabs, Inc. | FanLinc $^{\text {TM }}$ \#2475F | 14.8C.4A |
| Support Devices: |  |  |  |
| Function | Manufacturer | Model \# | S/N |
| Suspended Ceiling Fan | Hunter | 28683-530 | NA |

## Test Conditions / Notes:

The EUT is placed on the wooden table lined with Styrofoam. Total height is 1.5 meter from the ground plane.
Connected to the EUT is a support suspended ceiling fan.
Continuous transmit
914.92MHz-915.08MHz

EUT only operates on $120 \mathrm{Vac} / 60 \mathrm{~Hz}$.
Frequency range of measurement $=150 \mathrm{kHz}-30 \mathrm{MHz}$
$150 \mathrm{kHz}-30 \mathrm{MHz} ;$ RBW $=9 \mathrm{kHz}, \mathrm{VBW}=9 \mathrm{kHz}$
$17^{\circ} \mathrm{C}, 20 \%$ Relative Humidity
Ext Attn: 0 dB
Measurement Data: $\quad$ Reading listed by margin.
Test Lead: L2

| $\#$ | Freq <br> MHz | Rdng <br> $\mathrm{dB} \mu \mathrm{V}$ | T 1 <br> dB | T 2 <br> dB | T 3 <br> dB | T 4 <br> dB | Dist <br> Table | Corr <br> $\mathrm{dB} \mu \mathrm{V}$ | Spec <br> $\mathrm{dB} \mu \mathrm{V}$ | Margin <br> dB | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 265.626 k | 42.7 | +5.7 | +0.1 | +0.2 | +0.2 | +0.0 | 48.9 | 51.3 | -2.4 | L 2 |
| 2 | 355.799 k | 40.1 | +5.7 | +0.1 | +0.2 | +0.2 | +0.0 | 46.3 | 48.8 | -2.5 | L 2 |
| 3 | 1.430 M | 37.3 | +5.7 | +0.1 | +0.2 | +0.2 | +0.0 | 43.5 | 46.0 | -2.5 | L 2 |
| 4 | 301.986 k | 41.5 | +5.7 | +0.1 | +0.2 | +0.2 | +0.0 | 47.7 | 50.2 | -2.5 | L 2 |


| 5 | 196.541k | 45.2 | +5.7 | +0.1 | +0.1 | +0.2 | +0.0 | 51.3 | 53.8 | -2.5 | L2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | 214.721k | 44.3 | +5.7 | +0.1 | +0.1 | +0.2 | +0.0 | 50.4 | 53.0 | -2.6 | L2 |
| 7 | 243.082k | 43.1 | +5.7 | +0.1 | +0.1 | +0.2 | +0.0 | 49.2 | 52.0 | -2.8 | L2 |
| 8 | 327.438k | 40.5 | +5.7 | +0.1 | +0.2 | +0.2 | +0.0 | 46.7 | 49.5 | -2.8 | L2 |
| 9 | 331.802k | 40.4 | +5.7 | +0.1 | +0.2 | +0.2 | +0.0 | 46.6 | 49.4 | -2.8 | L2 |
| $10$ | $\begin{aligned} & \text { 163.090k } \\ & \text { Ave } \end{aligned}$ | 37.6 | +5.7 | +0.1 | +0.5 | +0.2 | +0.0 | 44.1 | 55.3 | -11.2 | L2 |
| $\wedge$ | 163.090k | 47.7 | +5.7 | +0.1 | +0.5 | +0.2 | +0.0 | 54.2 | 55.3 | -1.1 | L2 |
| $\wedge$ | 160.908k | 47.5 | +5.7 | +0.1 | +0.5 | +0.2 | +0.0 | 54.0 | 55.4 | -1.4 | L2 |
|  | $258.354 \mathrm{k}$ <br> Ave | 31.6 | +5.7 | +0.1 | $+0.2$ | +0.2 | +0.0 | 37.8 | 51.5 | -13.7 | L2 |
| $\wedge$ | 258.354k | 43.5 | +5.7 | +0.1 | $+0.2$ | +0.2 | +0.0 | 49.7 | 51.5 | -1.8 | L2 |
|  | $\begin{aligned} & \text { 169.635k } \\ & \text { Ave } \end{aligned}$ | 34.2 | +5.7 | +0.1 | +0.4 | +0.2 | +0.0 | 40.6 | 55.0 | -14.4 | L2 |
| $\wedge$ | 169.635k | 47.6 | +5.7 | +0.1 | +0.4 | +0.2 | +0.0 | 54.0 | 55.0 | -1.0 | L2 |
| 17 | $\begin{aligned} & \text { 189.269k } \\ & \text { Ave } \end{aligned}$ | 32.9 | +5.7 | +0.1 | +0.2 | +0.2 | +0.0 | 39.1 | 54.1 | -15.0 | L2 |
| $\wedge$ | 189.269k | 46.1 | +5.7 | +0.1 | $+0.2$ | +0.2 | +0.0 | 52.3 | 54.1 | -1.8 | L2 |
| $\wedge$ | 192.905k | 45.6 | +5.7 | +0.1 | +0.2 | +0.2 | +0.0 | 51.8 | 53.9 | -2.1 | L2 |

CKC Laboratories Date: 11/11/2011 Time: 11:41:12 SmartLabs, Inc. WO\#: 92499 15.207 AC Mains - Average Test Lead: L2 120V 60Hz Sequence\#: 14 Ext ATTN: 0 dB


| Sweep Data | Readings |
| :--- | :--- |
| Peak Readings | $\times$ QP Readings |
| * Average Readings | $\boldsymbol{\nabla}$ Ambient |
|  | $1-15.207$ AC Mains - Average |
|  | $2-15.207$ AC Mains - Quasi-peak |

## Test Setup Photos



### 15.249(a) RF Power Output

| Test Location: | CKC Laboratories • 110 Olinda Place • Brea, CA 92823 • 714-993-6112 |  |
| :--- | :--- | :--- |
|  |  |  |
| Customer: | SmartLabs, Inc. |  |
| Specification: | $\mathbf{1 5 . 2 4 9}$ Carrier and Spurious Emissions (902-928 MHz Transmitter) |  |
| Work Order \#: | 92499 | Date: 11/11/2011 |
| Test Type: | Maximized Emissions | Time: 08:41:57 |
| Equipment: | Inline Dual Load Module | Sequence\#: 11 |
| Manufacturer: | SmartLabs, Inc. | Tested By: Don Nguyen |
| Model: | FanLinc |  |
| SM $/ \mathrm{N}:$ | 14.8 C .4 A |  |
|  |  |  |

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN00309 | Preamp | 8447D | $5 / 7 / 2010$ | $5 / 7 / 2012$ |
| T2 | AN01995 | Biconilog Antenna | CBL6111C | $3 / 8 / 2010$ | $3 / 8 / 2012$ |
| T3 | ANP05050 | Cable | RG223/U | $3 / 21 / 2011$ | $3 / 21 / 2013$ |
| T4 | ANP05198 | Cable | 8268 | $12 / 21 / 2010$ | $12 / 21 / 2012$ |
|  | AN02672 | Spectrum Analyzer | E4446A | $8 / 9 / 2010$ | $8 / 9 / 2012$ |

Equipment Under Test ( ${ }^{*}=$ EUT):

| Function | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Inline Dual Load Module* | SmartLabs, Inc. | FanLinc $^{\mathrm{TM}} \# 2475 \mathrm{~F}$ | 14.8 C .4 A |
| Support Devices: |  |  |  |
| Function | Manufacturer | Model \# | S/N |
| Suspended Ceiling Fan | Hunter | $28683-530$ | NA |

## Test Conditions / Notes:

The EUT is placed on the wooden table lined with Styrofoam. Total height is 1.5 meter from the ground plane. Connected to the EUT is a support suspended ceiling fan.
Continuous transmit
914.92MHz-915.08MHz

EUT only operates on $120 \mathrm{Vac} / 60 \mathrm{~Hz}$.
Frequency range of measurement $=30 \mathrm{MHz}-1 \mathrm{GHz}$.
$30 \mathrm{MHz}-1000 \mathrm{MHz}$; RBW=120 kHz, VBW=120 kHz
$17^{\circ} \mathrm{C}, 20 \%$ Relative Humidity
Ext Attn: 0 dB
Measurement Data: Reading listed by margin. Test Distance: 3 Meters

| $\#$ | Freq <br> MHz | Rdng <br> $\mathrm{dB} \mu \mathrm{V}$ | T 1 <br> dB | T 2 <br> dB | T 3 <br> dB | T 4 <br> dB | Dist <br> Table | Corr <br> $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$ | Spec <br> $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$ | Margin <br> dB | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 915.066 M | 79.8 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 82.6 | 94.0 <br> X-axis | -11.4 | Horiz |
| 2 | 914.921 M | 79.8 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 82.6 | 94.0 <br> X-axis | -11.4 | Horiz |
| 3 | 914.922 M | 79.6 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 82.4 | 94.0 | -11.6 | Vert |
| 4 | 915.072 M | 79.6 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 82.4 | 94.0 <br> Y-axis | -11.6 | Vert |


| 5 | 914.926 M | 79.1 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 81.9 | 94.0 <br> Z-axis | -12.1 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | 915.072 M | 77.7 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 80.5 | 94.0 <br> Z-axis | -13.5 | Horiz |
| 7 | 914.923 M | 72.7 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 75.5 | 94.0 <br> Y-axis | -18.5 | Horiz |
| 8 | 914.927 M | 72.7 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 75.5 | 94.0 <br> Z-axis | -18.5 | Vert |
| 9 | 915.068 M | 72.6 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 75.4 | 94.0 <br> Y-axis | -18.6 | Horiz |
| 10 | 915.077 M | 72.6 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 75.4 | 94.0 <br> Z-axis | -18.6 | Vert |
| 11 | 915.068 M | 71.6 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 74.4 | 94.0 <br> X-axis | -19.6 | Vert |
| 12 | 914.928 M | 71.5 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 74.3 | 94.0 <br> X-axis | -19.7 | Vert |

## Test Setup Photos



X AXIS FRONT VIEW


X AXIS BACK VIEW


Y AXIS FRONT VIEW


Y AXIS BACK VIEW


Z AXIS FRONT VIEW


Z AXIS BACK VIEW

## -20 dBc Occupied Bandwidth

## Test Conditions / Setup

The EUT is placed on the wooden table lined with Styrofoam. Total height is 1.5 meter from the ground plane. Connected to the EUT is a support suspended ceiling fan. Continuous transmit $914.92 \mathrm{MHz}-915.08 \mathrm{MHz}$ EUT only operates on $120 \mathrm{Vac} / 60 \mathrm{~Hz}$.
Frequency range of measurement
$30 \mathrm{MHz}-1 \mathrm{GHz}$.
$30 \mathrm{MHz}-1000 \mathrm{MHz} ; \mathrm{RBW}=120 \mathrm{kHz}, \mathrm{VBW}=120 \mathrm{kHz}$
Temperature: $17^{\circ} \mathrm{C}$, Relative Humidity: $20 \%$
$15.31(\mathrm{e})$ : The supply voltage varied between $85 \%$ and $115 \%$ of the nominal rated supply voltage (120Vac), no change in the Fundamental signal level was observed.

Engineer Name: Don Nguyen

| Test Equipment |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Asset/Serial \# | Description | Model | Manufacturer | Cal Date | Cal Due |
| AN00309 | Preamp | 8447D | HP | $5 / 7 / 2010$ | $5 / 7 / 2012$ |
| AN01995 | Biconilog Antenna | CBL6111C | Chase | $3 / 8 / 2010$ | $3 / 8 / 2012$ |
| ANP05050 | Cable | RG223/U | Pasternack | $3 / 21 / 2011$ | $3 / 21 / 2013$ |
| ANP05198 | Cable | 8268 | Belden | $12 / 21 / 2010$ | $12 / 21 / 2012$ |
| AN02672 | Spectrum Analyzer | E4446A | Agilent | $8 / 9 / 2010$ | $8 / 9 / 2012$ |

## Test Data



## Test Setup Photos



X AXIS FRONT VIEW


X AXIS BACK VIEW


Y AXIS FRONT VIEW


Y AXIS BACK VIEW


Z AXIS FRONT VIEW


Z AXIS BACK VIEW

## Bandedge

## Test Conditions / Setup

The EUT is placed on the wooden table lined with Styrofoam. Total height is 1.5 meter from the ground plane. Connected to the EUT is a support suspended ceiling fan. Continuous transmit $914.92 \mathrm{MHz}-915.08 \mathrm{MHz}$ EUT only operates on $120 \mathrm{Vac} / 60 \mathrm{~Hz}$.
Frequency range of measurement
$30 \mathrm{MHz}-1 \mathrm{GHz}$.
$30 \mathrm{MHz}-1000 \mathrm{MHz} ; \mathrm{RBW}=120 \mathrm{kHz}, \mathrm{VBW}=120 \mathrm{kHz}$

Temperature: $17^{\circ} \mathrm{C}$, Relative Humidity: $20 \%$
15.31(e): The supply voltage varied between $85 \%$ and $115 \%$ of the nominal rated supply voltage (120Vac), no change in the Fundamental signal level was observed.

Engineer Name: Don Nguyen

## Test Equipment

| Asset/Serial \# | Description | Model | Manufacturer | Cal Date | Cal Due |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AN00309 | Preamp | 8447D | HP | $5 / 7 / 2010$ | $5 / 7 / 2012$ |
| AN01995 | Biconilog Antenna | CBL6111C | Chase | $3 / 8 / 2010$ | $3 / 8 / 2012$ |
| ANP05050 | Cable | RG223/U | Pasternack | $3 / 21 / 2011$ | $3 / 21 / 2013$ |
| ANP05198 | Cable | 8268 | Belden | $12 / 21 / 2010$ | $12 / 21 / 2012$ |
| AN02672 | Spectrum Analyzer | E4446A | Agilent | $8 / 9 / 2010$ | $8 / 9 / 2012$ |

## Test Data



Center Tx on


Left TX on


Left TX off


Right TX on


Right Tx off

## Test Setup Photos



X AXIS FRONT VIEW


X AXIS BACK VIEW


Y AXIS FRONT VIEW


Y AXIS BACK VIEW


Z AXIS FRONT VIEW


Z AXIS BACK VIEW

### 15.249(d) Radiated Spurious Emissions

## Test Data Sheets

Test Location: CKC Laboratories • 110 Olinda Place • Brea, CA 92823 • 714-993-6112
Customer: SmartLabs, Inc.
Specification:
15.249 Carrier and Spurious Emissions (902-928 MHz Transmitter)

Work Order \#:
Test Type:
Equipment:
Manufacturer:
Model:

## 92499

Maximized Emissions
Inline Dual Load Module
SmartLabs, Inc.
FanLinc ${ }^{\text {TM }}$ \#2475F
S/N:

Date: 11/11/2011
Time: 11:18:48
Sequence\#: 12
Tested By: Don Nguyen

## Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN00309 | Preamp | 8447D | $5 / 7 / 2010$ | $5 / 7 / 2012$ |
| T2 | AN01995 | Biconilog Antenna | CBL6111C | $3 / 8 / 2010$ | $3 / 8 / 2012$ |
| T3 | ANP05050 | Cable | RG223/U | $3 / 21 / 2011$ | $3 / 21 / 2013$ |
| T4 | ANP05198 | Cable | 8268 | $12 / 21 / 2010$ | $12 / 21 / 2012$ |
| T5 | AN02672 | Spectrum Analyzer | E4446A | $8 / 9 / 2010$ | $8 / 9 / 2012$ |
| T6 | AN00786 | Preamp | 83017 A | $8 / 5 / 2010$ | $8 / 5 / 2012$ |
| T7 | AN00849 | Horn Antenna | 3115 | $4 / 23 / 2010$ | $4 / 23 / 2012$ |
| T8 | AN03239 | Cable | $32022-2-29094 \mathrm{~K}-8 / 30 / 2011$ | $8 / 30 / 2013$ |  |
|  |  |  | 24 TC |  |  |
| T9 | ANP05421 | Cable | Sucoflex 104A | $2 / 12 / 2010$ | $2 / 12 / 2012$ |
| T10 | AN03169 | High Pass Filter | HM1155-11SS | $9 / 22 / 2011$ | $9 / 22 / 2013$ |
| T11 | ANP06081 | Cable | L1-PNMNM-48 | $4 / 28 / 2011$ | $4 / 28 / 2013$ |
| T12 | AN00314 | Loop Antenna | 6502 | $6 / 30 / 2010$ | $6 / 30 / 2012$ |

## Equipment Under Test (* = EUT):

| Function | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Inline Dual Load Module* | SmartLabs, Inc. | FanLinc $^{\mathrm{TM}}$ \#2475F | 14.8C.4A |
| Support Devices:   S/N <br> Function Manufacturer Model \# NA <br> Suspended Ceiling Fan Hunter $28683-530$  |  |  |  |

Test Conditions / Notes:
The EUT is placed on the wooden table lined with Styrofoam. Total height is 1.5 meter from the ground plane. Connected to the EUT is a support suspended ceiling fan.
Continuous transmit
914.92MHz-915.08MHz

EUT only operates on $120 \mathrm{Vac} / 60 \mathrm{~Hz}$.
Frequency range of measurement $=9 \mathrm{kHz}-10 \mathrm{GHz}$.
$9 \mathrm{kH}-150 \mathrm{kHz} ; \mathrm{RBW}=200 \mathrm{~Hz}, \mathrm{VBW}=200 \mathrm{~Hz} ; 150 \mathrm{kHz}-30 \mathrm{MHz} ;$ RBW=9 kHz, VBW=9 kHz; $30 \mathrm{MHz}-1000$
$\mathrm{MHz} ;$ RBW $=120 \mathrm{kHz}, V B W=120 \mathrm{kHz}, 1000 \mathrm{MHz}-10,000 \mathrm{MHz} ;$ RBW=1 MHz, VBW=1 MHz.
$17^{\circ} \mathrm{C}, 20 \%$ Relative Humidity
Ext Attn: 0 dB
Measurement Data: $\quad$ Reading listed by margin.
Test Distance: 3 Meters

| \# | Freq $\mathrm{MHz}$ | Rdng $\mathrm{dB} \mu \mathrm{~V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~T} 5 \\ & \mathrm{~T} 9 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{gathered} \mathrm{T} 2 \\ \text { T6 } \\ \text { T10 } \\ \text { dB } \end{gathered}$ | $\begin{gathered} \mathrm{T} 3 \\ \mathrm{~T} 7 \\ \mathrm{~T} 11 \\ \mathrm{~dB} \end{gathered}$ | $\begin{gathered} \mathrm{T} 4 \\ \mathrm{~T} 8 \\ \mathrm{~T} 12 \\ \mathrm{~dB} \end{gathered}$ | Dist <br> Table | Corr $\mathrm{dB} \mu \mathrm{~V} / \mathrm{m}$ | Spec $\mathrm{dB} \mu \mathrm{~V} / \mathrm{m}$ | Margin $\mathrm{dB}$ | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1830.000M | 57.8 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +1.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -38.2 \\ +0.4 \end{array}$ | $\begin{array}{r} +0.0 \\ +27.2 \\ +2.8 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \end{aligned}$ | +0.0 | 51.3 | $\begin{aligned} & 54.0 \\ & \text { Z-axis } \end{aligned}$ | -2.7 | Horiz |
| 2 | 1830.057M | 56.9 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +1.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -38.2 \\ +0.4 \end{array}$ | $\begin{array}{r} +0.0 \\ +27.2 \\ +2.8 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \end{aligned}$ | +0.0 | 50.4 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -3.6 | Vert |
| 3 | 2745.050M | 52.6 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +1.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.8 \\ +0.3 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +29.3 \\ +3.4 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 49.6 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -4.4 | Horiz |
| 4 | 2745.507M | 52.6 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +1.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.8 \\ +0.3 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +29.3 \\ +3.4 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 49.6 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -4.4 | Vert |
| 5 | 2744.707M | 52.4 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +1.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.8 \\ +0.3 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +29.3 \\ +3.4 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 49.4 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -4.6 | Vert |
| 6 | 2745.357M | 52.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.8 \\ +0.3 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +29.3 \\ +3.4 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 49.2 | $\begin{gathered} \quad 54.0 \\ \text { Y-axis } \end{gathered}$ | -4.8 | Vert |
| 7 | 2745.117M | 52.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.4 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.8 \\ +0.3 \end{array}$ | $\begin{array}{r} +0.0 \\ +29.3 \\ +3.4 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \end{aligned}$ | +0.0 | 49.1 | $\begin{gathered} \text { 54.0 } \\ \text { Z-axis } \end{gathered}$ | -4.9 | Horiz |
| 8 | 2745.000M | 51.3 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +1.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.8 \\ +0.3 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +29.3 \\ +3.4 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 48.3 | $\begin{gathered} \quad 54.0 \\ \text { Z-axis } \end{gathered}$ | -5.7 | Horiz |
| 9 | 1830.067M | 54.6 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +1.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -38.2 \\ +0.4 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +27.2 \\ +2.8 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | $48.1$ | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -5.9 | Vert |
| 10 | 2745.017M | 50.8 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.8 \\ +0.3 \end{array}$ | $\begin{array}{r} +0.0 \\ +29.3 \\ +3.4 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \end{aligned}$ | +0.0 | 47.8 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -6.2 | Horiz |
| 11 | 1830.067M | 53.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -38.2 \\ +0.4 \end{array}$ | $\begin{array}{r} +0.0 \\ +27.2 \\ +2.8 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \end{aligned}$ | $+0.0$ | $46.7$ | $\begin{aligned} & \text { 54.0 } \\ & \text { Z-axis } \end{aligned}$ | -7.3 | Vert |


| 12 | 2744.967M | 49.0 | +0.0 | ${ }^{+0.0}$ | +0.0 |  | +0.0 | 46.0 | $\begin{array}{r} 54.0 \\ \mathrm{X} \text {-axis } \end{array}$ | $-8.0$ | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | +0.0 | -37.8 | +29.3 | +0.4 |  |  |  |  |  |
|  |  |  | +1.4 | +0.3 | +3.4 | +0.0 |  |  |  |  |  |
| 13 | 1829.967M | 52.0 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 45.5 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -8.5 | Horiz |
|  |  |  | +0.0 | -38.2 | +27.2 | +0.3 |  |  |  |  |  |
|  |  |  | +1.0 | +0.4 | +2.8 | +0.0 |  |  |  |  |  |
| 14 | 1830.050M | 52.0 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 45.5 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -8.5 | Horiz |
|  |  |  | +0.0 | -38.2 | +27.2 | +0.3 |  |  |  |  |  |
|  |  |  | +1.0 | +0.4 | +2.8 | +0.0 |  |  |  |  |  |
| 15 | 2745.067M | 47.8 | +0.0 | +0.0 | +0.0 | +0.0 | $+0.0$ | 44.8 | $\begin{gathered} 54.0 \\ \text { Z-axis } \end{gathered}$ | -9.2 | Vert |
|  |  |  | +0.0 | -37.8 | +29.3 | +0.4 |  |  |  |  |  |
|  |  |  | +1.4 | +0.3 | +3.4 | +0.0 |  |  |  |  |  |
| 16 | 5490.000M | 38.6 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 44.3 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -9.7 | Vert |
|  |  |  | +0.0 | -36.9 | +34.4 | +0.6 |  |  |  |  |  |
|  |  |  | +2.0 | +0.2 | +5.4 | +0.0 |  |  |  |  |  |
| 17 | 5489.967M | 38.5 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 44.2 | $\begin{gathered} 54.0 \\ \text { X-axis } \end{gathered}$ | -9.8 | Vert |
|  |  |  | +0.0 | -36.9 | +34.4 | +0.6 |  |  |  |  |  |
|  |  |  | +2.0 | +0.2 | +5.4 | +0.0 |  |  |  |  |  |
| 18 | 5490.067M | 38.2 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 43.9 | $\begin{gathered} 54.0 \\ \text { Z-axis } \end{gathered}$ | -10.1 | Horiz |
|  |  |  | +0.0 | -36.9 | +34.4 | +0.6 |  |  |  |  |  |
|  |  |  | +2.0 | +0.2 | +5.4 | +0.0 |  |  |  |  |  |
| 19 | 5490.067M | 37.9 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 43.6 | $\begin{gathered} 54.0 \\ \text { Z-axis } \end{gathered}$ | -10.4 | Vert |
|  |  |  | +0.0 | -36.9 | +34.4 | +0.6 |  |  |  |  |  |
|  |  |  | +2.0 | +0.2 | +5.4 | +0.0 |  |  |  |  |  |
| 20 | 4575.000M | 40.7 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 43.4 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -10.6 | Vert |
|  |  |  | +0.0 | -37.2 | +32.5 | +0.5 |  |  |  |  |  |
|  |  |  | +1.9 | +0.3 | +4.7 | +0.0 |  |  |  |  |  |
| 21 | 5490.017M | 37.2 | +0.0 | +0.0 | +0.0 | +0.0 | $+0.0$ | 42.9 | $\begin{gathered} 54.0 \\ \text { X-axis } \end{gathered}$ | -11.1 | Horiz |
|  |  |  | +0.0 | -36.9 | +34.4 | +0.6 |  |  |  |  |  |
|  |  |  | +2.0 | +0.2 | +5.4 | +0.0 |  |  |  |  |  |
| 22 | 3660.067M | 42.1 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 42.6 | $\begin{gathered} 54.0 \\ \text { Z-axis } \end{gathered}$ | -11.4 | Horiz |
|  |  |  | +0.0 | -37.4 | +31.3 | +0.4 |  |  |  |  |  |
|  |  |  | +1.7 | +0.3 | +4.2 | +0.0 |  |  |  |  |  |
| 23 | 3660.000M | 41.9 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 42.4 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -11.6 | Vert |
|  |  |  | +0.0 | -37.4 | +31.3 | +0.4 |  |  |  |  |  |
|  |  |  | +1.7 | +0.3 | +4.2 | +0.0 |  |  |  |  |  |
| 24 | 4574.967M | 39.5 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 42.2 | $\begin{gathered} 54.0 \\ \text { X-axis } \end{gathered}$ | -11.8 | Vert |
|  |  |  | +0.0 | -37.2 | +32.5 | +0.5 |  |  |  |  |  |
|  |  |  | +1.9 | +0.3 | +4.7 | +0.0 |  |  |  |  |  |
| 25 | 3660.067M | 41.6 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 42.1 | $\begin{gathered} 54.0 \\ \text { Z-axis } \end{gathered}$ | -11.9 | Vert |
|  |  |  | +0.0 | -37.4 | +31.3 | +0.4 |  |  |  |  |  |
|  |  |  | +1.7 | +0.3 | +4.2 | +0.0 |  |  |  |  |  |
| 26 | 4575.067M | 39.3 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 42.0 | $\begin{gathered} 54.0 \\ \text { Z-axis } \end{gathered}$ | -12.0 | Vert |
|  |  |  | +0.0 | -37.2 | +32.5 | +0.5 |  |  |  |  |  |
|  |  |  | +1.9 | +0.3 | +4.7 | +0.0 |  |  |  |  |  |
| 27 | 4575.017M | 38.8 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 41.5 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -12.5 | Horiz |
|  |  |  | +0.0 | -37.2 | +32.5 | +0.5 |  |  |  |  |  |
|  |  |  | +1.9 | +0.3 | +4.7 | +0.0 |  |  |  |  |  |
| 28 | 4575.000M | 38.8 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 41.5 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -12.5 | Horiz |
|  |  |  | +0.0 | -37.2 | +32.5 | +0.5 |  |  |  |  |  |
|  |  |  | +1.9 | +0.3 | +4.7 | +0.0 |  |  |  |  |  |


| 29 | 230.010 M | 46.9 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+11.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+2.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 33.2 | $\begin{gathered} \hline 46.0 \\ \text { Z-axis } \end{gathered}$ | -12.8 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 30 | 899.990M | 30.6 | $\begin{array}{r} -27.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+23.3 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +5.8 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 33.1 | $\begin{gathered} 46.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -12.9 | Horiz |
| 31 | 3660.000M | 40.4 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.7 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.4 \\ +0.3 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +31.3 \\ +4.2 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -13.1 | Horiz |
| 32 | 230.035M | 46.5 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+11.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+2.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 32.8 | $\begin{gathered} \quad 46.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -13.2 | Horiz |
| 33 | 110.585M | 44.8 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+11.1 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +1.8 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 30.0 | $\begin{aligned} & 43.5 \\ & \mathrm{X} \text {-axis } \end{aligned}$ | -13.5 | Horiz |
| 34 | 35.000 M | 36.7 | $\begin{array}{r} -27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+16.4 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+1.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 26.4 | $\begin{gathered} \hline 40.0 \\ \text { Z-axis } \end{gathered}$ | -13.6 | Vert |
| 35 | 5490.000 M | 34.6 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +2.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -36.9 \\ +0.2 \end{array}$ | $\begin{array}{r} +0.0 \\ +34.4 \\ +5.4 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ |  | $\begin{gathered} \quad 54.0 \\ \text { Y-axis } \end{gathered}$ | -13.7 | Horiz |
| 36 | 3659.967M | 39.5 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.7 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.4 \\ +0.3 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +31.3 \\ +4.2 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 40.0 | $\begin{aligned} & \quad 54.0 \\ & \mathrm{X} \text {-axis } \end{aligned}$ | -14.0 | Vert |
| 37 | 286.160M | 43.2 | $\begin{array}{r} -27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+13.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+3.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ |  | $\begin{gathered} 46.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -14.1 | Horiz |
| 38 | 373.030M | 40.3 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+15.5 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+3.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} \quad 46.0 \\ \text { Z-axis } \end{gathered}$ | -14.3 | Horiz |
| 39 | 4575.067M | 36.9 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.9 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.2 \\ +0.3 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +32.5 \\ +4.7 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.5 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ |  | $\begin{aligned} & \text { 54.0 } \\ & \text { Z-axis } \end{aligned}$ | -14.4 | Horiz |
| 40 | 900.000 M | 28.5 | $\begin{array}{r} -27.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+23.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+5.8 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} \hline 46.0 \\ \text { Z-axis } \end{gathered}$ | -15.0 | Horiz |
| 41 | 295.060M | 42.2 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+13.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+3.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} 46.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -15.0 | Horiz |
| 42 | 900.000 M | 28.5 | $\begin{array}{r} \hline-27.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+23.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+5.8 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} 46.0 \\ \text { Y-axis } \end{gathered}$ | -15.0 | Vert |
| 43 | 3660.017M | 38.5 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.7 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.4 \\ +0.3 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +31.3 \\ +4.2 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ |  | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -15.0 | Horiz |
| 44 | 900.000M | 27.8 | $\begin{array}{r} -27.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+23.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+5.8 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} \quad 46.0 \\ \text { Z-axis } \end{gathered}$ | -15.7 | Vert |
| 45 | 900.000 M | 26.3 | $\begin{array}{r} \hline-27.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+23.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +5.8 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 28.8 | $\begin{gathered} 46.0 \\ \text { Y-axis } \end{gathered}$ | -17.2 | Horiz |

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| 46 | 192.485M | 42.3 | $\begin{array}{r} \hline-27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+9.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+2.4 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 26.2 | $\begin{aligned} & 43.5 \\ & \text { X-axis } \end{aligned}$ | -17.3 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 47 | 690.010M | 29.4 | -27.2 | +20.9 | +0.5 | +5.0 | $+0.0$ | 28.6 | $\begin{gathered} 46.0 \\ \text { X-axis } \end{gathered}$ | -17.4 | Horiz |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 48 | 192.485M | 41.8 | -27.7 | +9.0 | +0.2 | +2.4 | +0.0 | 25.7 | $\begin{gathered} 43.5 \\ \text { Z-axis } \end{gathered}$ | -17.8 | Horiz |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 49 | 690.000M | 28.6 | -27.2 | +20.9 | +0.5 | +5.0 | +0.0 | 27.8 | $\begin{gathered} 46.0 \\ \text { Z-axis } \end{gathered}$ | -18.2 | Horiz |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 50 | 230.005M | 40.5 | -27.8 | +11.3 | +0.2 | +2.6 | $+0.0$ | 26.8 | $\begin{gathered} 46.0 \\ \text { X-axis } \end{gathered}$ | -19.2 | Vert |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 51 | 373.560M | 35.3 | -27.8 | +15.5 | +0.3 | +3.4 | +0.0 | 26.7 | $\begin{gathered} 46.0 \\ \text { X-axis } \end{gathered}$ | -19.3 | Horiz |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 52 | 295.010M | 37.9 | -27.8 | +13.3 | +0.2 | +3.1 | +0.0 | 26.7 | $\begin{gathered} \hline 46.0 \\ \text { Z-axis } \end{gathered}$ | -19.3 | Horiz |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 53 | 690.000M | 27.2 | -27.2 | +20.9 | +0.5 | +5.0 | $+0.0$ | 26.4 | $\begin{gathered} 46.0 \\ \text { Z-axis } \end{gathered}$ | -19.6 | Vert |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 54 | 110.000M | 38.4 | -27.8 | +11.0 | +0.1 | +1.8 | +0.0 | 23.5 | $\begin{gathered} \quad 43.5 \\ \text { Z-axis } \end{gathered}$ | -20.0 | Vert |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 55 | 230.000M | 39.6 | -27.8 | +11.3 | +0.2 | +2.6 | +0.0 | 25.9 | $\begin{gathered} 46.0 \\ \text { Y-axis } \end{gathered}$ | -20.1 | Vert |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 56 | 373.600M | 33.9 | -27.8 | +15.5 | +0.3 | +3.4 | +0.0 | 25.3 | $\begin{gathered} 46.0 \\ \text { Z-axis } \end{gathered}$ | -20.7 | Vert |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 57 | 381.220M | 33.1 | -27.9 | +15.7 | +0.3 | +3.5 | +0.0 | 24.7 | $\begin{gathered} 46.0 \\ \text { X-axis } \end{gathered}$ | -21.3 | Vert |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 58 | 401.220M | 32.4 | -27.9 | +16.2 | +0.3 | +3.6 | +0.0 | 24.6 | $\begin{gathered} \hline 46.0 \\ \text { X-axis } \end{gathered}$ | -21.4 | Vert |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 59 | 390.790M | 32.8 | -27.9 | +15.9 | +0.3 | +3.5 | +0.0 | 24.6 | $\begin{gathered} 46.0 \\ \text { Z-axis } \end{gathered}$ | -21.4 | Vert |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 60 | 690.000M | 25.4 | -27.2 | +20.9 | +0.5 | +5.0 | +0.0 | 24.6 | $\begin{gathered} 46.0 \\ \text { Y-axis } \end{gathered}$ | -21.4 | Vert |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 61 | 295.070M | 35.7 | -27.8 | +13.3 | +0.2 | +3.1 | +0.0 | 24.5 | $\begin{gathered} 46.0 \\ \text { Z-axis } \end{gathered}$ | -21.5 | Vert |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 62 | 690.000M | 25.1 | -27.2 | +20.9 | +0.5 | +5.0 | +0.0 | 24.3 | Y-axis | -21.7 | Horiz |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |


| 63 | 218.495 M | 38.8 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{array}{r} \hline+10.5 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +2.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $+0.0$ | 24.3 | $\begin{gathered} 46.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -21.7 | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 64 | 230.000 M | 37.6 | $\begin{array}{r} -27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+11.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 23.9 | $\begin{gathered} 46.0 \\ \text { Z-axis } \end{gathered}$ | -22.1 | Vert |
| 65 | 390.050M | 31.8 | $\begin{array}{r} \hline-27.9 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+15.9 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +3.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 23.6 | $\begin{gathered} \hline 46.0 \\ \text { Z-axis } \end{gathered}$ | -22.4 | Horiz |
| 66 | 372.220 M | 32.0 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+15.4 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +3.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 23.3 | $\begin{gathered} \quad 46.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -22.7 | Vert |
| 67 | 230.000 M | 36.8 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+11.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 23.1 | $\begin{gathered} 46.0 \\ \text { Y-axis } \end{gathered}$ | -22.9 | Horiz |
| 68 | 392.720M | 31.1 | $\begin{array}{r} -27.9 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+16.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +3.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 23.1 | $\begin{gathered} 46.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -22.9 | Vert |
| 69 | 390.810M | 30.8 | $\begin{array}{r} -27.9 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+15.9 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +3.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 22.6 | $\begin{gathered} 46.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -23.4 | Horiz |
| 70 | 110.000 M | 34.9 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+11.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.8 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 20.0 | $\begin{gathered} 43.5 \\ \text { Z-axis } \end{gathered}$ | -23.5 | Horiz |
| 71 | 35.160 M | 26.6 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+16.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 16.2 | $\begin{gathered} \quad 40.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -23.8 | Horiz |
| 72 | 1.411 M | 31.7 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +8.9 \\ & \hline \end{aligned}$ | -40.0 | 0.7 | $\begin{gathered} 24.6 \\ \text { Y-axis } \end{gathered}$ | -23.9 | Paral |
| 73 | 192.485M | 34.6 | $\begin{array}{r} \hline-27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +9.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 18.5 | $\begin{gathered} 43.5 \\ \text { Z-axis } \end{gathered}$ | -25.0 | Vert |
| 74 | 192.880M | 34.4 | $\begin{array}{r} -27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +9.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ |  | $\begin{gathered} 43.5 \\ \text { Y-axis } \end{gathered}$ | -25.2 | Horiz |
| 75 | 35.000 M | 24.9 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+16.4 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ |  | $\begin{gathered} \hline 40.0 \\ \text { Z-axis } \end{gathered}$ | -25.4 | Horiz |
| 76 | 286.400 M | 31.3 | $\begin{array}{r} -27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+13.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +3.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ |  | $\begin{gathered} 46.0 \\ \text { Z-axis } \end{gathered}$ | -26.0 | Vert |
| 77 | 192.880M | 33.5 | $\begin{array}{r} \hline-27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +9.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+2.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{aligned} & 43.5 \\ & \text { Y-axis } \end{aligned}$ | -26.1 | Vert |
| 78 | 185.595M | 33.6 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +9.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+2.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ |  | $\begin{gathered} 43.5 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -26.1 | Vert |
| 79 | 286.160M | 31.1 | $\begin{array}{r} -27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+13.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +3.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 19.8 | $\begin{gathered} 46.0 \\ \text { Z-axis } \end{gathered}$ | -26.2 | Vert |

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| 80 | 197.945M | 32.4 | $\begin{array}{r} \hline-27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +9.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+2.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 16.4 | $\begin{array}{r} 43.5 \\ \mathrm{X} \text {-axis } \end{array}$ | -27.1 | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 81 | 295.000 M | 27.6 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+13.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +3.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 16.4 | $\begin{gathered} 46.0 \\ \text { Y-axis } \end{gathered}$ | -29.6 | Vert |
| 82 | 1.860M | 28.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +8.8 \\ & \hline \end{aligned}$ | -40.0 | -2.9 | $\begin{gathered} 29.5 \\ \text { Y-axis } \end{gathered}$ | -32.4 | Paral |
| 83 | 1.765 M | 26.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +8.8 \\ & \hline \end{aligned}$ | -40.0 |  | $\begin{aligned} & 29.5 \\ & \text { Z-axis } \end{aligned}$ | -34.4 | Paral |
| 84 | 1.742 M | 25.3 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +8.8 \\ & \hline \end{aligned}$ | -40.0 | -5.7 | $\begin{aligned} & 29.5 \\ & \text { Y-axis } \end{aligned}$ | -35.2 | Perpe |
| 85 | 1.700M | 16.9 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +8.9 \\ & \hline \end{aligned}$ | -40.0 | $-14.0$ | $\begin{gathered} 22.9 \\ \text { Z-axis } \end{gathered}$ | -36.9 | Perpe |
| 86 | 185.000k | 55.8 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +8.5 \\ & \hline \end{aligned}$ | -80.0 | -15.6 | $\begin{gathered} 22.3 \\ \text { Z-axis } \end{gathered}$ | -37.9 | Perpe |
| 87 | 3.400 M | 22.4 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.3 \\ & +0.0 \\ & +8.8 \\ & \hline \end{aligned}$ | -40.0 | -8.5 | $\begin{gathered} 29.5 \\ \text { Z-axis } \end{gathered}$ | -38.0 | Perpe |
| 88 | 2.370M | 22.5 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +8.8 \\ & \hline \end{aligned}$ | -40.0 | -8.5 | $\begin{array}{r} 29.5 \\ \mathrm{X} \text {-axis } \end{array}$ | -38.0 | Paral |
| 89 | 185.000k | 54.9 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.1 \\ +0.0 \\ +8.5 \\ \hline \end{array}$ | -80.0 | -16.5 | $\begin{gathered} 22.3 \\ \text { Y-axis } \end{gathered}$ | -38.8 | Perpe |
| 90 | 3.335M | 21.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +8.8 \\ & \hline \end{aligned}$ | -40.0 | -9.8 | $\begin{aligned} & 29.5 \\ & \mathrm{X} \text {-axis } \end{aligned}$ | -39.3 | Paral |
| 91 | 2.247 M | 21.1 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +8.8 \\ & \hline \end{aligned}$ | -40.0 | -9.9 | $\begin{aligned} & 29.5 \\ & \text { Y-axis } \end{aligned}$ | -39.4 | Perpe |
| 92 | 14.876 M | 21.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.6 \\ & +0.0 \\ & +7.6 \\ & \hline \end{aligned}$ | -40.0 |  | $\begin{aligned} & 29.5 \\ & \text { Y-axis } \end{aligned}$ | -40.3 | Paral |
| 93 | 220.000k | 51.9 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +8.5 \\ & \hline \end{aligned}$ | -80.0 |  | $\begin{gathered} 20.8 \\ \text { Z-axis } \end{gathered}$ | -40.3 | Paral |
| 94 | 3.710 M | 20.0 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.3 \\ & +0.0 \\ & +8.8 \\ & \hline \end{aligned}$ | -40.0 |  | $\begin{gathered} 29.5 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -40.4 | Perpe |
| 95 | 2.200 M | 18.2 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.2 \\ & +0.0 \\ & +8.8 \\ & \hline \end{aligned}$ | -40.0 | -12.8 | $\begin{gathered} 29.5 \\ \text { Z-axis } \end{gathered}$ | -42.3 | Perpe |
| 96 | 220.000k | 49.9 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +8.5 \\ & \hline \end{aligned}$ | -80.0 | -21.5 | $\begin{gathered} 20.8 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -42.3 | Perpe |

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| 97 | 390.000 k | 43.8 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +8.6 \end{aligned}$ | -80.0 | -27.5 | $\begin{gathered} 15.8 \\ \text { X-axis } \end{gathered}$ | -43.3 | Paral |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 98 | 3.455M | 16.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.3 \\ & +0.0 \\ & +8.8 \end{aligned}$ | -40.0 | $-14.7$ | $\begin{aligned} & 29.5 \\ & \text { Z-axis } \end{aligned}$ | -44.2 | Paral |
| 99 | 3.415 M | 16.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.3 \\ & +0.0 \\ & +8.8 \end{aligned}$ | -40.0 | -14.8 | $\begin{array}{r} 29.5 \\ \text { Y-axis } \end{array}$ | -44.3 | Perpe |
| 100 | 356.000k | 38.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +8.5 \end{aligned}$ | -80.0 | -33.2 | $\begin{gathered} 16.6 \\ \text { Y-axis } \end{gathered}$ | -49.8 | Paral |

CKC Laboratories Date: 11/11/2011 Time: 11:18:48 SmartLabs, Inc. WO\#: 92499
15.249 Carrier and Spurious Emissions (902-928 MHz Transmitter) Test Distance: 3 Meters Sequence\#: 12 Ext ATTN: 0 dB


## Test Setup Photos



X AXIS FRONT VIEW


X AXIS BACK VIEW


Y AXIS FRONT VIEW


Y AXIS BACK VIEW


Z AXIS FRONT VIEW


Z AXIS BACK VIEW

## RSS-210

## 99 \% Bandwidth

## Test Conditions / Setup

The EUT is placed on the wooden table lined with Styrofoam. Total height is 1.5 meter from the ground plane. Connected to the EUT is a support suspended ceiling fan. Continuous transmit $914.92 \mathrm{MHz}-915.08 \mathrm{MHz}$ EUT only operates on $120 \mathrm{Vac} / 60 \mathrm{~Hz}$.
Frequency range of measurement
$30 \mathrm{MHz}-1 \mathrm{GHz}$.
$30 \mathrm{MHz}-1000 \mathrm{MHz}$; RBW=120 kHz, VBW=120 kHz
Temperature: $17^{\circ} \mathrm{C}$, Relative Humidity: $20 \%$
15.31(e): The supply voltage varied between $85 \%$ and $115 \%$ of the nominal rated supply voltage ( 120 Vac ), no change in the Fundamental signal level was observed.

Engineer Name: Don Nguyen

| Test Equipment |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Asset/Serial \# | Description | Model | Manufacturer | Cal Date | Cal Due |
| AN00309 | Preamp | 8447D | HP | $5 / 7 / 2010$ | $5 / 7 / 2012$ |
| AN01995 | Biconilog Antenna | CBL6111C | Chase | $3 / 8 / 2010$ | $3 / 8 / 2012$ |
| ANP05050 | Cable | RG223/U | Pasternack | $3 / 21 / 2011$ | $3 / 21 / 2013$ |
| ANP05198 | Cable | 8268 | Belden | $12 / 21 / 2010$ | $12 / 21 / 2012$ |
| AN02672 | Spectrum Analyzer | E4446A | Agilent | $8 / 9 / 2010$ | $8 / 9 / 2012$ |

Test Data


## Test Setup Photos



X AXIS FRONT VIEW


X AXIS BACK VIEW


Y AXIS FRONT VIEW


Y AXIS BACK VIEW


Z AXIS FRONT VIEW


Z AXIS BACK VIEW

## SUPPLEMENTAL INFORMATION

## Measurement Uncertainty

| Uncertainty Value | Parameter |
| :---: | :---: |
| 4.73 dB | Radiated Emissions |
| 3.34 dB | Mains Conducted Emissions |
| 3.30 dB | Disturbance Power |

The reported measurement uncertainties are calculated based on the worst case of all laboratory environments from CKC Laboratories, Inc. test sites. Only those parameters which require estimation of measurement uncertainty are reported. The reported worst case measurement uncertainty is less than the maximum values derived in CISPR 16-4-2. Reported uncertainties represent expanded uncertainties expressed at approximately the $95 \%$ confidence level using a coverage factor of $\mathrm{k}=2$. Compliance is deemed to occur provided measurements are below the specified limits.

## Emissions Test Details

## TESTING PARAMETERS

Unless otherwise indicated, the following configuration parameters are used for equipment setup: The cables were routed consistent with the typical application by varying the configuration of the test sample. Interface cables were connected to the available ports of the test unit. The effect of varying the position of the cables was investigated to find the configuration that produced maximum emissions. Cables were of the type and length specified in the individual requirements. The length of cable that produced maximum emissions was selected.

The equipment under test (EUT) was set up in a manner that represented its normal use, as shown in the setup photographs. Any special conditions required for the EUT to operate normally are identified in the comments that accompany the emissions tables.

The emissions data was taken with a spectrum analyzer or receiver. Incorporating the applicable correction factors for distance, antenna, cable loss and amplifier gain, the data was reduced as shown in the table below. The corrected data was then compared to the applicable emission limits. Preliminary and final measurements were taken in order to ensure that all emissions from the EUT were found and maximized.

## CORRECTION FACTORS

The basic spectrum analyzer reading was converted using correction factors as shown in the highest emissions readings in the tables. For radiated emissions in $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$, the spectrum analyzer reading in $\mathrm{dB} \mu \mathrm{V}$ was corrected by using the following formula. This reading was then compared to the applicable specification limit.

LABORATORIES, INC.

| SAMPLE CALCULATIONS |  |  |  |
| :--- | :--- | :--- | :---: |
|  | Meter reading | $(\mathrm{dB} \mu \mathrm{V})$ |  |
| + | Antenna Factor | $(\mathrm{dB})$ |  |
| + | Cable Loss | $(\mathrm{dB})$ |  |
| - | Distance Correction | $(\mathrm{dB})$ |  |
| - | Preamplifier Gain | $(\mathrm{dB})$ |  |
| $=$ | Corrected Reading | $(\mathrm{dB} \mu \mathrm{V} / \mathrm{m})$ |  |

## TEST INSTRUMENTATION AND ANALYZER SETTINGS

The test instrumentation and equipment listed were used to collect the emissions data. A spectrum analyzer or receiver was used for all measurements. Unless otherwise specified, the following table shows the measuring equipment bandwidth settings that were used in designated frequency bands. For testing emissions, an appropriate reference level and a vertical scale size of 10 dB per division were used.

| MEASURING EQUIPMENT BANDWIDTH SETTINGS PER FREQUENCY RANGE |  |  |  |
| :---: | :---: | :---: | :---: |
| TEST | BEGINNING FREQUENCY | ENDING FREQUENCY | BANDWIDTH SETTING |
| CONDUCTED EMISSIONS | 150 kHz | 30 MHz | 9 kHz |
| RADIATED EMISSIONS | 30 MHz | 1000 MHz | 120 kHz |
| RADIATED EMISSIONS | 1000 MHz | $>1 \mathrm{GHz}$ | 1 MHz |

## SPECTRUM ANALYZER/RECEIVER DETECTOR FUNCTIONS

The notes that accompany the measurements contained in the emissions tables indicate the type of detector function used to obtain the given readings. Unless otherwise noted, all readings were made in the "positive peak" detector mode. Whenever a "quasi-peak" or "average" reading was recorded, the measurement was annotated with a "QP" or an "Ave" on the appropriate rows of the data sheets. In cases where quasi-peak or average limits were employed and data exists for multiple measurement types for the same frequency then the peak measurement was retained in the report for reference, however the numbering for the affected row was removed and an arrow or carrot ("^") was placed in the far left-hand column indicating that the row above takes precedence for comparison to the limit. The following paragraphs describe in more detail the detector functions and when they were used to obtain the emissions data.

## Peak

In this mode, the spectrum analyzer or receiver recorded all emissions at their peak value as the frequency band selected was scanned. By combining this function with another feature called "peak hold," the measurement device had the ability to measure intermittent or low duty cycle transient emission peak levels. In this mode the measuring device made a slow scan across the frequency band selected and measured the peak emission value found at each frequency across the band.

## Quasi-Peak

Quasi-peak measurements were taken using the quasi-peak detector when the true peak values exceeded or were within 2 dB of a quasi-peak specification limit. Additional QP measurements may have been taken at the discretion of the operator.

## Average

Average measurements were taken using the average detector when the true peak values exceeded or were within 2 dB of an average specification limit. Additional average measurements may have been taken at the discretion of the operator. If the specification or test procedure requires trace averaging, then the averaging was performed using 100 samples or as required by the specification. All other average measurements are performed using video bandwidth averaging. To make these measurements, the test engineer reduces the video bandwidth on the measuring device until the modulation of the signal is filtered out. At this point the measuring device is set into the linear mode and the scan time is reduced.

