## SmartLabs, Inc.

ADDENDUM TO TEST REPORT 92438-3

In-Line 0-10VDC Dimmer or Dual-Switch, 2475DA2

Tested To The Following Standards:

FCC Part 15 Subpart C Sections 15.207, 15.249
and
RSS 210 ISSUE 8

Report No.: 92438-3A

Date of issue: December 15, 2011


Testing Certificates: 803.01, 803.02, 803.05, 803.06

This test report bears the accreditation symbol indicating that the testing performed herein meets the test and reporting requirements of ISO/IEC 17025 under the applicable scope of EMC testing for CKC Laboratories, Inc.

We strive to create long-term, trust based relationships by providing sound, adaptive, customer first testing services. We embrace each of our customers' unique EMC challenges, not as an interruption to set processes, but rather as the reason we are in business.

[^0]TABLE OF CONTENTS
Administrative Information ..... 3
Test Report Information .....  3
Revision History ..... 3
Report Authorization .....  3
Test Facility Information ..... 4
Site Registration \& Accreditation Information ..... 4
Summary of Results .....  5
Conditions During Testing .....  5
Equipment Under Test ..... 6
Peripheral Devices ..... 6
FCC Part 15 Subpart C ..... 7
15.31(e) Voltage Variations ..... 7
15.207 AC Conducted Emissions ..... 10
15.249(a) RF Power Output ..... 27
15.249(a) Field Strength of Harmonics / 15.249(d) Field Strength of Spurious Emissions ..... 36
-20dBc Occupied Bandwidth ..... 55
Bandedge ..... 59
RSS-210 ..... 65
99 \% Bandwidth ..... 65
Supplemental Information ..... 69
Measurement Uncertainty ..... 69
Emissions Test Details. ..... 69

# ADMINISTRATIVE INFORMATION 

## Test Report Information

## REPORT PREPARED FOR:

SmartLabs, Inc.
16542 Millikan Ave
Irvine, CA 92606

Representative: John Lockyer
Customer Reference Number: 11-3JL1013-01

DATE OF EQUIPMENT RECEIPT:
DATES) OF TESTING:

REPORT PREPARED BY:

Dianne Dudley
CKC Laboratories, Inc. 5046 Sierra Pines Drive Mariposa, CA 95338

Project Number: 92348

October 27, 2011
October 27, 2011- December 6, 2011

## Revision History

Original: To perform the testing of the In-Line 0-10VDC Dimmer or Dual-Switch, 2475DA2 with the requirements for FCC Part 15 Subpart C Sections 15.207, 15.249 and RSS 210 Issue 8 devices.
Addendum A: To include testing performed of the In-Line 0-10VDC Dimmer or Dual-Switch, 2475DA2 with optional sensor and a section of dedicated cable length installed with the requirements for FCC Part 15 Subpart C Sections 15.249(a) and 15.249(d).

## Report Authorization

The test data contained in this report documents the observed testing parameters pertaining to and are relevant for only the sample equipment tested in the agreed upon operational modes) and configurations) as identified herein. Compliance assessment remains the client's responsibility. This report may not be used to claim product endorsement by A2LA or any government agencies. This test report has been authorized for release under quality control from CKC Laboratories, Inc.


Steve Behm
Director of Quality Assurance \& Engineering Services CKC Laboratories, Inc.

## Test Facility Information



Our laboratories are configured to effectively test a wide variety of product types. CKC utilizes first class test equipment, anechoic chambers, data acquisition and information services to create accurate, repeatable and affordable test results.

TEST LOCATION(S):
CKC Laboratories, Inc.
110 Olinda Place
Brea, CA 92823

## Site Registration \& Accreditation Information

| Location | CB \# | Japan | Canada | FCC |
| :---: | :---: | :---: | :---: | :---: |
| Brea A | US0060 | R-2945, C-3248 \& T-1572 | 3082D-1 | 90473 |

## SUMMARY OF RESULTS

Standard / Specification: FCC Part 15 Subpart C 15.207, 15.249 and RSS 210 Issue 8

| Description | Test Procedure/Method | Results |
| :--- | :--- | :---: |
|  |  |  |
| Voltage Variation | FCC Part 15 Subpart C Section 15.31(e) | Pass |
|  | FCC Part 15 Subpart C Section 15.207 / ANSI C63.4 (2003) | Pass |
| Conducted Emissions | FCC Part 15 Subpart C Section 15.249 (a) | Pass |
|  |  | Pass |
| RF Power Output | FCC Part 15 Subpart C Section 15.249(a) \& 15.249(d ) / <br> ANSI C63.4 (2003) | Pass |
| Field Strength of Harmonics / Field <br> Strength of Spurious Emissions |  | Pass |
|  | FCC Part 15 Subpart C Section 15.249 |  |
| -20dBc Occupied Bandwidth | FCC Part 15 Subpart C Section 15.249 | Pass |
|  |  | FCC Part 15 Subpart C |
| Occupied Bandwidth |  | PSS 210 Issue 8 |
| Bandedge |  | Pass |
|  |  |  |
| 99 \% Bandwidth |  |  |

## Conditions During Testing

This list is a summary of the conditions noted for or modifications made to the equipment during testing.

## Summary of Conditions

None

## EQUIPMENT UNDER TEST (EUT)

## EQUIPMENT UNDER TEST

In-Line 0-10VDC Dimmer or Dual-Switch
Manuf: SmartLabs, Inc.
Model: 2475DA2
Serial: 148B8C

## PERIPHERAL DEVICES

The EUT was tested with the following peripheral device(s):

Dimmable Programmed Start Electronic Ballast
Manuf: Phillips
Model: IZT-132-SC
Serial: NA

## Florescent Light

Manuf: Ecolux
Model: SP35
Serial: F17T8-SP35-ECO

## FCC PART 15 SUBPART C

This report contains EMC emissions test results under United States Federal Communications Commission (FCC) 47 CFR 15C requirements for Unlicensed Radio Frequency Devices, Subpart C - Intentional Radiators.

### 15.31(e) Voltage Variations

## Test Conditions / Setup

The EUT is placed on the wooden table lined with Styrofoam; total height is 1.5 meter from the ground plane. Connected to the EUT is a light bulb.
Continuous transmit
914.92MHz-915.08MHz
15.31(e) compliance: the supply voltage was varied between $85 \%$ and $115 \%$ of the nominal rated supply voltage (120-230Vac), no change in the Fundamental signal level was observed.

Frequency range of measurement $=30 \mathrm{MHz}-1 \mathrm{GHz}$
RBW $=120 \mathrm{kHz}, \mathrm{VBW}=120 \mathrm{kHz}$
$18^{\circ} \mathrm{C}, 22 \%$ Relative Humidity
Engineer Name: D. Nguyen

## Test Equipment

| Asset/Serial \# | Description | Model | Manufacturer | Cal Date | Cal Due |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AN00309 | Preamp | 8447D | HP | $5 / 7 / 2010$ | $5 / 7 / 2012$ |
| AN01995 | Biconilog Antenna | CBL6111C | Chase | $3 / 8 / 2010$ | $3 / 8 / 2012$ |
| ANP05050 | Cable | RG223/U | Pasternack | $3 / 21 / 2011$ | $3 / 21 / 2013$ |
| ANP05198 | Cable | 8268 | Belden | $12 / 21 / 2010$ | $12 / 21 / 2012$ |
| AN02672 | Spectrum Analyzer | E4446A | Agilent | $8 / 9 / 2010$ | $8 / 9 / 2012$ |

## Test Setup Photos


15.31(e) Y Axis

15.31(e) Z Axis

15.31(e) BACK VIEW

### 15.207 AC Conducted Emissions

## Test Data Sheets

Test Location: CKC Laboratories • 110 Olinda Place • Brea, CA 92823 • 714-993-6112
Customer: SmartLabs, Inc.
Specification: $\quad \mathbf{1 5 . 2 0 7}$ AC Mains - Average

Work Order \#: 92348
Test Type: Conducted Emissions
Equipment: In-Line 0-10VDC Dimmer or DualSwitch
Manufacturer: SmartLabs, Inc. Tested By: Don Nguyen
Model: 2475DA2
S/N: 148B8C

Date: 10/27/2011
Time: 15:43:59
Sequence\#: 11

120 V 60 Hz

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :---: | :--- | :--- | :--- | :--- | :--- |
|  | AN02672 | Spectrum Analyzer | E4446A | $8 / 9 / 2010$ | $8 / 9 / 2012$ |
| T1 | AN02610 | High Pass Filter | HE9615-150K- <br> $50-720 B$ | $11 / 16 / 2009$ | $11 / 16 / 2011$ |
| T2 | ANP04358 | Cable | RG142 | $5 / 7 / 2010$ | $5 / 7 / 2012$ |
| T3 | ANP06084 | Attenuator | SA18N10W-06 | $12 / 8 / 2010$ | $12 / 8 / 2012$ |
| T4 | AN00847.1 | 50uH LISN-Line 1 <br> $(d B)$ | $3816 / 2 N M$ | $12 / 21 / 2010$ | $12 / 21 / 2012$ |
|  | AN00847.1 | 50uH LISN-Line 2 <br> $(d B)$ | $3816 / 2 N M$ | $12 / 21 / 2010$ | $12 / 21 / 2012$ |

Equipment Under Test (* = EUT):

| Function | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| In-Line 0-10VDC Dimmer | SmartLabs, Inc. | 2475DA2 | 148B8C |
| or Dual-Switch* |  |  |  |

## Support Devices:

| Function | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Dimmable Programmed <br> Start Electronic Ballast | Phillips | IZT-132-SC | NA |
| Florescent Light | Ecolux | SP35 | F17T8-SP35-ECO |

## Test Conditions / Notes:

The EUT is placed on the wooden table lined with Styrofoam; total height is 1.5 meter from the ground plane. Connected to the EUT is a light bulb.
Continuous transmit
914.92MHz-915.08MHz

Frequency range of measurement $=150 \mathrm{kHz}-30 \mathrm{MHz}$
RBW $=\mathrm{VBW}=9 \mathrm{kHz}$
$18^{\circ} \mathrm{C}$, $22 \%$ Relative Humidity

Ext Attn: 0 dB
Measurement Data: $\quad$ Reading listed by margin.

| \# | Freq <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \text { T3 } \\ & \text { dB } \end{aligned}$ | $\begin{aligned} & \mathrm{T} 4 \\ & \mathrm{~dB} \end{aligned}$ | Dist <br> Table | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} \end{gathered}$ | $\begin{gathered} \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} \\ \hline \end{gathered}$ | Margin dB | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 20.481M | 41.4 | +0.2 | +0.4 | +5.9 | +1.1 | +0.0 | 49.0 | 50.0 | -1.0 | L1 |
| 2 | 20.274 M | 41.4 | +0.2 | +0.4 | +5.9 | +1.1 | +0.0 | 49.0 | 50.0 | -1.0 | L1 |
| 3 | 22.112 M | 41.2 | +0.2 | +0.4 | +5.9 | +1.3 | +0.0 | 49.0 | 50.0 | -1.0 | L1 |
| 4 | 21.670 M | 41.2 | +0.2 | +0.4 | +5.9 | +1.3 | +0.0 | 49.0 | 50.0 | -1.0 | L1 |
| 5 | 21.148 M | 41.0 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 48.7 | 50.0 | -1.3 | L1 |
| 6 | 21.400 M | 41.0 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 48.7 | 50.0 | -1.3 | L1 |
| 7 | 20.148M | 41.0 | +0.2 | +0.4 | +5.9 | +1.1 | +0.0 | 48.6 | 50.0 | -1.4 | L1 |
| 8 | 21.797 M | 40.8 | +0.2 | +0.4 | +5.9 | +1.3 | +0.0 | 48.6 | 50.0 | -1.4 | L1 |
| 9 | 20.355 M | 40.9 | +0.2 | +0.4 | +5.9 | +1.1 | +0.0 | 48.5 | 50.0 | -1.5 | L1 |
| 10 | 21.526 M | 40.8 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 48.5 | 50.0 | -1.5 | L1 |
| 11 | 23.511 M | 40.5 | +0.2 | +0.4 | +5.9 | +1.5 | +0.0 | 48.5 | 50.0 | -1.5 | L1 |
| 12 | 1.026 M | 38.4 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 44.5 | 46.0 | -1.5 | L1 |
| 13 | 453.244 k | 39.2 | +0.3 | +0.1 | +5.7 | +0.0 | +0.0 | 45.3 | 46.8 | -1.5 | L1 |
| 14 | 20.229 M | 40.9 | +0.2 | +0.4 | +5.9 | +1.1 | +0.0 | 48.5 | 50.0 | -1.5 | L1 |
| 15 | 20.310 M | 40.9 | +0.2 | +0.4 | +5.9 | +1.1 | +0.0 | 48.5 | 50.0 | -1.5 | L1 |
| 16 | 20.256M | 40.9 | +0.2 | +0.4 | +5.9 | +1.1 | +0.0 | 48.5 | 50.0 | -1.5 | L1 |
| 17 | 796.485k | 38.3 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 44.4 | 46.0 | -1.6 | L1 |
| 18 | 21.544 M | 40.7 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 48.4 | 50.0 | -1.6 | L1 |
| 19 | 24.292 M | 40.3 | +0.2 | +0.4 | +5.9 | +1.5 | +0.0 | 48.3 | 50.0 | -1.7 | L1 |
| 20 | 20.454 M | 40.6 | +0.2 | +0.4 | +5.9 | +1.1 | +0.0 | 48.2 | 50.0 | -1.8 | L1 |
|  | $836.481 \mathrm{k}$ <br> Ave | 36.2 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 42.3 | 46.0 | -3.7 | L1 |
| $\wedge$ | 836.481 k | 45.1 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 51.2 | 46.0 | +5.2 | L1 |
|  | $\begin{aligned} & \text { 227.292k } \\ & \text { fve } \end{aligned}$ | 39.9 | +0.3 | +0.1 | +5.8 | +0.0 | +0.0 | 46.1 | 52.5 | -6.4 | L1 |
|  | $656.279 \mathrm{k}$ <br> Ave | 32.8 | +0.3 | +0.1 | +5.8 | +0.0 | +0.0 | 39.0 | 46.0 | -7.0 | L1 |

Page 11 of 70

| $\begin{gathered} 25 \begin{array}{c} 636.500 \mathrm{k} \\ \text { Ave } \end{array} \end{gathered}$ | 31.5 | +0.3 | +0.1 | +5.8 | +0.0 | +0.0 | 37.7 | 46.0 | -8.3 | L1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ^ 636.500k | 43.0 | +0.3 | +0.1 | +5.8 | +0.0 | +0.0 | 49.2 | 46.0 | +3.2 | L1 |
| $\begin{gathered} 27{ }^{232.173 \mathrm{k}} \\ \text { Ave } \end{gathered}$ | 37.0 | +0.3 | +0.1 | +5.8 | +0.0 | +0.0 | 43.2 | 52.4 | -9.2 | L1 |
| $\wedge 232.173 \mathrm{k}$ | 47.7 | +0.3 | +0.1 | +5.8 | +0.0 | +0.0 | 53.9 | 52.4 | +1.5 | L1 |
| $\begin{gathered} \hline 29 \begin{array}{c} 622.683 \mathrm{k} \\ \text { Ave } \end{array} \\ \hline \end{gathered}$ | 28.9 | +0.3 | +0.1 | +5.8 | +0.0 | +0.0 | 35.1 | 46.0 | -10.9 | L1 |
| ^ 622.683k | 41.9 | +0.3 | +0.1 | +5.8 | +0.0 | +0.0 | 48.1 | 46.0 | +2.1 | L1 |
| $\begin{gathered} 31 \\ \text { Ave } \\ \hline \end{gathered}$ | 27.4 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 33.5 | 46.0 | -12.5 | L1 |
| $\wedge 1.073 \mathrm{M}$ | 42.4 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 48.5 | 46.0 | +2.5 | L1 |
| $\begin{gathered} 33 \\ \text { Ave } \\ \hline \end{gathered}$ | 25.8 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 31.9 | 46.0 | -14.1 | L1 |
| ^ 1.115 M | 41.8 | +0.2 | +0.1 | +5.8 | +0.0 | $+0.0$ | 47.9 | 46.0 | +1.9 | L1 |
|  | 15.8 | +0.2 | +0.4 | +5.9 | +1.3 | +0.0 | 23.6 | 50.0 | -26.4 | L1 |
| ^ 21.743 M | 44.6 | +0.2 | +0.4 | +5.9 | +1.3 | +0.0 | 52.4 | 50.0 | +2.4 | L1 |
| $\begin{gathered} 37 \begin{array}{c} 18.815 \mathrm{M} \\ \text { Ave } \end{array} \\ \hline \end{gathered}$ | 12.2 | $+0.2$ | +0.4 | +5.9 | +1.0 | +0.0 | 19.7 | 50.0 | -30.3 | L1 |
| ^ 18.815 M | 47.9 | +0.2 | +0.4 | +5.9 | +1.0 | +0.0 | 55.4 | 50.0 | +5.4 | L1 |

CKC Laboratories Date: 10/27/2011 Time: 15:43:59 SmartLabs, Inc. WO\#: 92348 15.207 AC Mains - Average Test Lead: L1 120V 60Hz Sequence\#: 11 Ext ATTN: 0 dB


| Sweep Data |  |
| :--- | :--- |
| Peak Readings | $\times$ Readings |
| * $\quad$ Average Readings Readings |  |
|  | 1-15.207 AC Mains - Average |
|  |  |

Test Location: CKC Laboratories • 110 Olinda Place • Brea, CA 92823 • 714-993-6112
Customer: SmartLabs, Inc.
Specification: 15.207 AC Mains - Average
Work Order \#: 92348
Test Type:
Equipment: In-Line 0-10VDC Dimmer or Dual-
10/27/2011
Time: 15:52:19
Sequence\#: 12

Tested By: Don Nguyen
120 V 60 Hz
Manufacturer:
Model:
SmartLabs, Inc.
2475DA2
S/N: 148B8C
Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | AN02672 | Spectrum Analyzer | E4446A | $8 / 9 / 2010$ | $8 / 9 / 2012$ |
| T1 | AN02610 | High Pass Filter | HE9615-150K- <br> $50-720 B$ | $11 / 16 / 2009$ | $11 / 16 / 2011$ |
| T2 | ANP04358 | Cable | RG142 | $5 / 7 / 2010$ | $5 / 7 / 2012$ |
| T3 | ANP06084 | Attenuator | SA18N10W-06 | $12 / 8 / 2010$ | $12 / 8 / 2012$ |
|  | AN00847.1 | 50uH LISN-Line 1 <br> $(\mathrm{~dB})$ | $3816 / 2 \mathrm{NM}$ | $12 / 21 / 2010$ | $12 / 21 / 2012$ |
| T4 | AN00847.1 | 50uH LISN-Line 2 <br> $(d B)$ | $3816 / 2 \mathrm{NM}$ | $12 / 21 / 2010$ | $12 / 21 / 2012$ |

## Equipment Under Test (* = EUT):

| Function | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| In-Line 0-10VDC Dimmer <br> or Dual-Switch* | SmartLabs, Inc. | 2475DA2 | 148B8C |

Support Devices:

| Function | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Dimmable Programmed <br> Start Electronic Ballast | Phillips | IZT-132-SC | NA |
| Florescent Light | Ecolux | SP35 | F17T8-SP35-ECO |

## Test Conditions / Notes:

The EUT is placed on the wooden table lined with Styrofoam; total height is 1.5 meter from the ground plane. Connected to the EUT is a light bulb.
Continuous transmit
914.92MHz-915.08MHz

Frequency range of measurement $=150 \mathrm{kHz}-30 \mathrm{MHz}$
RBW=VBW=9kHz
$18^{\circ} \mathrm{C}, 22 \%$ Relative Humidity
Ext Attn: 0 dB
Measurement Data: $\quad$ Reading listed by margin.
Test Lead: L2

| $\#$ | Freq <br> MHz | Rdng <br> $\mathrm{dB} \mu \mathrm{V}$ | T 1 <br> dB | T 2 <br> dB | T 3 <br> dB | T 4 <br> dB | Dist <br> Table | Corr <br> $\mathrm{dB} \mu \mathrm{V}$ | Spec <br> $\mathrm{dB} \mu \mathrm{V}$ | Margin <br> dB | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 21.238 M | 41.0 | +0.2 | +0.4 | +5.9 | +1.3 | +0.0 | 48.8 | 50.0 | -1.2 | L 2 |
| 2 | 21.373 M | 40.9 | +0.2 | +0.4 | +5.9 | +1.3 | +0.0 | 48.7 | 50.0 | -1.3 | L 2 |
| 3 | 21.499 M | 40.7 | +0.2 | +0.4 | +5.9 | +1.4 | +0.0 | 48.6 | 50.0 | -1.4 | L 2 |


| $4$ | $\begin{aligned} & 830.464 \mathrm{k} \\ & \text { ve } \end{aligned}$ | 38.4 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 44.5 | 46.0 | -1.5 | L2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5 | 20.508M | 40.8 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 48.5 | 50.0 | -1.5 | L2 |
| 6 | 21.779M | 40.6 | +0.2 | +0.4 | +5.9 | +1.4 | +0.0 | 48.5 | 50.0 | -1.5 | L2 |
| $7$ | $\begin{aligned} & 830.665 \mathrm{k} \\ & \text { ve } \end{aligned}$ | 38.4 | $+0.2$ | +0.1 | +5.8 | $+0.0$ | $+0.0$ | 44.5 | 46.0 | -1.5 | L2 |
| $\wedge$ | 830.665k | 43.0 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 49.1 | 46.0 | +3.1 | L2 |
| 9 | 1.511 M | 38.3 | +0.1 | +0.1 | +5.8 | +0.1 | +0.0 | 44.4 | 46.0 | -1.6 | L2 |
| 10 | 21.175 M | 40.6 | +0.2 | +0.4 | +5.9 | +1.3 | +0.0 | 48.4 | 50.0 | -1.6 | L2 |
| 11 | 3.748 M | 38.2 | +0.1 | +0.2 | +5.8 | +0.1 | +0.0 | 44.4 | 46.0 | -1.6 | L2 |
| 12 | 19.896M | 40.6 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 48.3 | 50.0 | -1.7 | L2 |
| 13 | 20.058M | 40.4 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 48.1 | 50.0 | -1.9 | L2 |
| 14 | 21.562M | 40.2 | $+0.2$ | +0.4 | +5.9 | +1.4 | $+0.0$ | 48.1 | 50.0 | -1.9 | L2 |
| 15 | 19.797M | 40.4 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 48.1 | 50.0 | -1.9 | L2 |
| 16 | 3.956M | 37.8 | +0.1 | +0.2 | +5.8 | +0.1 | $+0.0$ | 44.0 | 46.0 | -2.0 | L2 |
| 17 | 20.148M | 40.3 | $+0.2$ | +0.4 | +5.9 | +1.2 | $+0.0$ | 48.0 | 50.0 | $-2.0$ | L2 |
| 18 | 379.070k | 40.2 | +0.3 | +0.1 | +5.7 | +0.0 | +0.0 | 46.3 | 48.3 | -2.0 | L2 |
| 19 | 232.901k | 44.1 | $+0.3$ | +0.1 | +5.8 | $+0.0$ | $+0.0$ | 50.3 | 52.3 | -2.0 | L2 |
| 20 | 600.868k | 37.7 | +0.3 | +0.1 | +5.8 | +0.0 | $+0.0$ | 43.9 | 46.0 | -2.1 | L2 |
| 21 | 452.518k | 38.6 | +0.3 | +0.1 | +5.7 | +0.0 | +0.0 | 44.7 | 46.8 | -2.1 | L2 |
| 22 | 21.950M | 40.0 | +0.2 | +0.4 | +5.9 | +1.4 | $+0.0$ | 47.9 | 50.0 | -2.1 | L2 |
| 23 | 19.283M | 40.2 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 47.9 | 50.0 | -2.1 | L2 |
| 24 | 19.878M | 40.1 | $+0.2$ | $+0.4$ | +5.9 | +1.2 | +0.0 | 47.8 | 50.0 | -2.2 | L2 |
| 25 | 19.670M | 40.0 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 47.7 | 50.0 | -2.3 | L2 |
| 26 | 22.202 M | 39.6 | +0.2 | +0.4 | +5.9 | +1.4 | +0.0 | 47.5 | 50.0 | -2.5 | L2 |
| 27 | 162.363 k | 46.4 | +0.4 | +0.1 | +5.8 | +0.0 | +0.0 | 52.7 | 55.3 | -2.6 | L2 |
| 28 | 22.058 M | 39.5 | +0.2 | +0.4 | +5.9 | +1.4 | +0.0 | 47.4 | 50.0 | -2.6 | L2 |
| 29 | 20.112M | 39.6 | $+0.2$ | $+0.4$ | +5.9 | +1.2 | $+0.0$ | 47.3 | 50.0 | -2.7 | L2 |

Page 15 of 70

| $30 \quad 21.932 \mathrm{M}$ | 39.4 | +0.2 | +0.4 | +5.9 | +1.4 | +0.0 | 47.3 | 50.0 | -2.7 | L2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} 31 \quad 1.285 \mathrm{M} \\ \text { Ave } \end{gathered}$ | 32.5 | +0.2 | +0.1 | +5.8 | +0.1 | +0.0 | 38.7 | 46.0 | -7.3 | L2 |
| 1.285M | 42.5 | +0.2 | +0.1 | +5.8 | +0.1 | +0.0 | 48.7 | 46.0 | +2.7 | L2 |
| $\begin{gathered} 33 \\ \text { Ave } \\ \hline \end{gathered}$ | 29.9 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 36.0 | 46.0 | -10.0 | L2 |
| $\wedge 1.090 \mathrm{M}$ | 41.0 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 47.1 | 46.0 | +1.1 | L2 |
| $\begin{gathered} 35{ }^{4.241 \mathrm{M}} \\ \text { Ave } \end{gathered}$ | 24.9 | +0.1 | +0.2 | +5.8 | +0.2 | +0.0 | 31.2 | 46.0 | -14.8 | L2 |
| ^ 4.241 M | 40.7 | +0.1 | +0.2 | +5.8 | +0.2 | +0.0 | 47.0 | 46.0 | +1.0 | L2 |
| $\begin{gathered} 37{ }^{21.202 \mathrm{M}} \\ \text { Ave } \end{gathered}$ | 22.3 | +0.2 | +0.4 | +5.9 | +1.3 | +0.0 | 30.1 | 50.0 | -19.9 | L2 |
| ^ 21.202 M | 46.3 | +0.2 | +0.4 | +5.9 | +1.3 | +0.0 | 54.1 | 50.0 | +4.1 | L2 |
| $\begin{gathered} 39{ }^{21.049 \mathrm{M}} \\ \text { Ave } \end{gathered}$ | 21.8 | +0.2 | +0.4 | +5.9 | +1.3 | +0.0 | 29.6 | 50.0 | -20.4 | L2 |
| ^ 21.049 M | 43.2 | +0.2 | +0.4 | +5.9 | +1.3 | +0.0 | 51.0 | 50.0 | +1.0 | L2 |
| $\begin{gathered} 41 \begin{array}{l} 21.112 \mathrm{M} \\ \text { Ave } \\ \hline \end{array}{ }^{2} \\ \hline \end{gathered}$ | 21.1 | $+0.2$ | +0.4 | +5.9 | +1.3 | +0.0 | 28.9 | 50.0 | -21.1 | L2 |
| ^ 21.112 M | 47.4 | +0.2 | +0.4 | +5.9 | +1.3 | +0.0 | 55.2 | 50.0 | +5.2 | L2 |
| $\begin{gathered} 43 \begin{array}{c} 22.022 \mathrm{M} \\ \text { Ave } \end{array} \\ \hline \end{gathered}$ | 20.3 | +0.2 | +0.4 | +5.9 | +1.4 | +0.0 | 28.2 | 50.0 | -21.8 | L2 |
| ^ 22.022 M | 55.1 | +0.2 | +0.4 | +5.9 | +1.4 | +0.0 | 63.0 | 50.0 | +13.0 | L2 |
| $\begin{gathered} \hline 45 \begin{array}{c} 19.571 \mathrm{M} \\ \text { Ave } \\ \hline \end{array}{ }^{2} \\ \hline \end{gathered}$ | 19.2 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 26.9 | 50.0 | -23.1 | L2 |
| ^ 19.571 M | 44.6 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 52.3 | 50.0 | +2.3 | L2 |

CKC Laboratories Date: 10/27/2011 Time: 15:52:19 SmartLabs, Inc. WO\#: 92348 15.207 AC Mains - Average Test Lead: L2 120V 60Hz Sequence\#: 12 Ext ATTN: 0 dB


Test Location: CKC Laboratories • 110 Olinda Place • Brea, CA 92823 • 714-993-6112
Customer: SmartLabs, Inc.
Specification: 15.207 AC Mains - Average
Work Order \#: 92348
Test Type:
Equipment: In-Line 0-10VDC Dimmer or DualSwitch
Manufacturer: SmartLabs, Inc. Tested By: Don Nguyen
Model: 2475DA2
Date: 10/27/2011
Time: 16:09:41
Sequence\#: 14

230 V 50 Hz
S/N: 148B8C

## Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| AN02672 | Spectrum Analyzer | E4446A | $8 / 9 / 2010$ | $8 / 9 / 2012$ |  |
| T1 | AN02610 | High Pass Filter | HE9615-150K- <br> $50-720 B$ | $11 / 16 / 2009$ | $11 / 16 / 2011$ |
| T2 | ANP04358 | Cable | RG142 | $5 / 7 / 2010$ | $5 / 7 / 2012$ |
| T3 | ANP06084 | Attenuator | SA18N10W-06 | $12 / 8 / 2010$ | $12 / 8 / 2012$ |
| T4 | AN00847.1 | 50uH LISN-Line 1 <br> $(\mathrm{~dB})$ | $3816 / 2 \mathrm{NM}$ | $12 / 21 / 2010$ | $12 / 21 / 2012$ |
|  | AN00847.1 | 50uH LISN-Line 2 <br> $(d B)$ | $3816 / 2 \mathrm{NM}$ | $12 / 21 / 2010$ | $12 / 21 / 2012$ |

Equipment Under Test $(*=$ EUT ):

| Function | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| In-Line 0-10VDC Dimmer <br> or Dual-Switch* | SmartLabs, Inc. | 2475DA2 | 148B8C |

Support Devices:

| Function | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Dimmable Programmed <br> Start Electronic Ballast | Phillips | IZT-132-SC | NA |
| Florescent Light | Ecolux | SP35 | F17T8-SP35-ECO |

## Test Conditions / Notes:

The EUT is placed on the wooden table lined with Styrofoam; total height is 1.5 meter from the ground plane. Connected to the EUT is a light bulb.
Continuous transmit
914.92MHz-915.08MHz

Frequency range of measurement $=150 \mathrm{kHz}-30 \mathrm{MHz}$
RBW $=\mathrm{VBW}=9 \mathrm{kHz}$
$18^{\circ} \mathrm{C}, 22 \%$ Relative Humidity
Ext Attn: 0 dB
Measurement Data: $\quad$ Reading listed by margin.
Test Lead: L1

| $\#$ | Freq <br> MHz | Rdng <br> $\mathrm{dB} \mu \mathrm{V}$ | T 1 <br> dB | T 2 <br> dB | T 3 <br> dB | T 4 <br> dB | Dist <br> Table | Corr <br> $\mathrm{dB} \mu \mathrm{V}$ | Spec <br> $\mathrm{dB} \mu \mathrm{V}$ | Margin <br> dB | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 953.754 k | 38.9 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 45.0 | 46.0 | -1.0 | L 1 |
| 2 | 21.670 M | 41.1 | +0.2 | +0.4 | +5.9 | +1.3 | +0.0 | 48.9 | 50.0 | -1.1 | L 1 |
| 3 | 21.337 M | 41.0 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 48.7 | 50.0 | -1.3 | L 1 |


| 4 | 21.616 M | 40.9 | +0.2 | +0.4 | +5.9 | +1.3 | +0.0 | 48.7 | 50.0 | -1.3 | L1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5 | 21.049 M | 40.9 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 48.6 | 50.0 | -1.4 | L1 |
| 6 | 20.661M | 41.0 | +0.2 | +0.4 | +5.9 | +1.1 | +0.0 | 48.6 | 50.0 | -1.4 | L1 |
| 7 | 20.346M | 41.0 | +0.2 | +0.4 | +5.9 | +1.1 | +0.0 | 48.6 | 50.0 | -1.4 | L1 |
| 8 | 22.121 M | 40.8 | +0.2 | +0.4 | +5.9 | +1.3 | +0.0 | 48.6 | 50.0 | -1.4 | L1 |
| 9 | 21.175M | 40.9 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 48.6 | 50.0 | -1.4 | L1 |
| 10 | 4.258 M | 38.3 | +0.1 | +0.2 | +5.8 | +0.1 | +0.0 | 44.5 | 46.0 | -1.5 | L1 |
| 11 | 379.070k | 40.6 | +0.3 | +0.1 | +5.7 | +0.0 | +0.0 | 46.7 | 48.3 | -1.6 | L1 |
| 12 | 23.915M | 40.4 | +0.2 | +0.4 | +5.9 | +1.5 | +0.0 | 48.4 | 50.0 | -1.6 | L1 |
|  | $\begin{aligned} & 828.483 \mathrm{k} \\ & \text { ve } \end{aligned}$ | 38.3 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 44.4 | 46.0 | -1.6 | L1 |
| $\wedge$ | 828.483k | 44.4 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 50.5 | 46.0 | +4.5 | L1 |
| 15 | 20.454M | 40.7 | +0.2 | +0.4 | +5.9 | +1.1 | +0.0 | 48.3 | 50.0 | -1.7 | L1 |
| 16 | 20.436M | 40.6 | +0.2 | +0.4 | +5.9 | +1.1 | +0.0 | 48.2 | 50.0 | -1.8 | L1 |
| 17 | 21.094 M | 40.5 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 48.2 | 50.0 | -1.8 | L1 |
| 18 | 21.202 M | 40.5 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 48.2 | 50.0 | -1.8 | L1 |
| 19 | 20.076 M | 40.5 | +0.2 | +0.4 | +5.9 | +1.1 | +0.0 | 48.1 | 50.0 | -1.9 | L1 |
| 20 | 20.535 M | 40.5 | +0.2 | +0.4 | +5.9 | +1.1 | +0.0 | 48.1 | 50.0 | -1.9 | L1 |
| 21 | 20.202M | 40.4 | +0.2 | +0.4 | +5.9 | +1.1 | +0.0 | 48.0 | 50.0 | -2.0 | L1 |
| 22 | 523.784k | 37.8 | +0.3 | +0.1 | +5.7 | +0.0 | +0.0 | 43.9 | 46.0 | -2.1 | L1 |
| 23 | 21.076M | 39.9 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 47.6 | 50.0 | -2.4 | L1 |
| 24 | 21.896 M | 39.7 | +0.2 | +0.4 | +5.9 | +1.3 | +0.0 | 47.5 | 50.0 | -2.5 | L1 |
| 25 | 545.600k | 37.2 | +0.3 | +0.1 | +5.8 | +0.0 | +0.0 | 43.4 | 46.0 | -2.6 | L1 |
| 26 | 20.049M | 39.7 | +0.2 | +0.4 | +5.9 | +1.1 | +0.0 | 47.3 | 50.0 | -2.7 | L1 |
| 27 | 20.121 M | 39.4 | +0.2 | +0.4 | +5.9 | +1.1 | +0.0 | 47.0 | 50.0 | -3.0 | L1 |
|  | $\begin{aligned} & 1.502 \mathrm{M} \\ & \text { ave } \end{aligned}$ | 36.8 | +0.1 | +0.1 | +5.8 | +0.0 | +0.0 | 42.8 | 46.0 | -3.2 | L1 |
| $\wedge$ | 1.502 M | 42.2 | +0.1 | +0.1 | +5.8 | +0.0 | +0.0 | 48.2 | 46.0 | +2.2 | L1 |

Page 19 of 70

| $\begin{gathered} 30 \quad 452.518 \mathrm{k} \\ \text { Ave } \end{gathered}$ | 35.3 | +0.3 | +0.1 | +5.7 | +0.0 | +0.0 | 41.4 | 46.8 | -5.4 | L1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge \quad 452.518 \mathrm{k}$ | 43.3 | +0.3 | +0.1 | +5.7 | +0.0 | +0.0 | 49.4 | 46.8 | +2.6 | L1 |
| $\begin{gathered} 32 \begin{array}{c} 638.682 \mathrm{k} \\ \text { Ave } \end{array} \end{gathered}$ | 32.6 | +0.3 | +0.1 | +5.8 | +0.0 | +0.0 | 38.8 | 46.0 | -7.2 | L1 |
| $\wedge \quad 638.682 \mathrm{k}$ | 40.9 | +0.3 | +0.1 | +5.8 | +0.0 | +0.0 | 47.1 | 46.0 | +1.1 | L1 |
| $\begin{gathered} 34{ }^{1.273 \mathrm{M}} \\ \text { Ave } \end{gathered}$ | 32.0 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 38.1 | 46.0 | -7.9 | L1 |
| $\wedge 1.273 \mathrm{M}$ | 42.5 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 48.6 | 46.0 | +2.6 | L1 |
| $\begin{gathered} 36 \quad 1.086 \mathrm{M} \\ \text { Ave } \end{gathered}$ | 30.9 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 37.0 | 46.0 | -9.0 | L1 |
| $\wedge 1.086 \mathrm{M}$ | 46.1 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 52.2 | 46.0 | +6.2 | L1 |
| $\begin{gathered} 38 \quad 1.205 \mathrm{M} \\ \text { Ave } \\ \hline \end{gathered}$ | 30.1 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 36.2 | 46.0 | -9.8 | L1 |
| $\wedge 1.205 \mathrm{M}$ | 41.8 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 47.9 | 46.0 | +1.9 | L1 |
| $\begin{gathered} 40{ }^{1.149 \mathrm{M}} \\ \text { Ave } \end{gathered}$ | 28.4 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 34.5 | 46.0 | -11.5 | L1 |
| $\wedge 1.149 \mathrm{M}$ | 41.6 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 47.7 | 46.0 | +1.7 | L1 |
| $\begin{aligned} & 42 \quad 856.844 \mathrm{k} \\ & \text { Ave } \end{aligned}$ | 27.5 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 33.6 | 46.0 | -12.4 | L1 |
| $\wedge 856.844 \mathrm{k}$ | 43.0 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 49.1 | 46.0 | +3.1 | L1 |
| $\begin{aligned} & 44 \begin{array}{l} 873.570 \mathrm{k} \\ \text { Ave } \end{array} \end{aligned}$ | 27.0 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 33.1 | 46.0 | -12.9 | L1 |
| $\wedge 873.570 \mathrm{k}$ | 43.3 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 49.4 | 46.0 | +3.4 | L1 |
| $\begin{gathered} 46 \begin{array}{c} 842.300 \mathrm{k} \\ \text { Ave } \end{array} \end{gathered}$ | 26.5 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 32.6 | 46.0 | -13.4 | L1 |
| $\wedge 842.300 \mathrm{k}$ | 42.5 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 48.6 | 46.0 | +2.6 | L1 |
| $\begin{gathered} \hline 48 \quad 889.963 \mathrm{k} \\ \text { Ave } \\ \hline \end{gathered}$ | 25.4 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 31.5 | 46.0 | -14.5 | L1 |
| $\wedge 8889.963 \mathrm{k}$ | 42.0 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 48.1 | 46.0 | +2.1 | L1 |

CKC Laboratories Date: 10/27/2011 Time: 16:09:41 SmartLabs, Inc. WO\#: 92348 15.207 AC Mains - Average Test Lead: L1 230V 50Hz Sequence\#: 14 Ext ATTN: 0 dB

$\begin{array}{ll} & \text { Sweep Data } \\ \text { O } & \text { Peak Readings } \\ \text { * } & \text { Average Readings } \\ & 1-15.207 \text { AC Mains - Average }\end{array}$

—— Readings<br>$\times$ QP Readings<br>- Ambient<br>2-15.207 AC Mains - Quasi-peak

Test Location: CKC Laboratories • 110 Olinda Place • Brea, CA 92823 • 714-993-6112
Customer: SmartLabs, Inc.
Specification: 15.207 AC Mains - Average
Work Order \#: 92348
Test Type:
Equipment: In-Line 0-10VDC Dimmer or DualSwitch
Manufacturer: SmartLabs, Inc. Tested By: Don Nguyen
Model: 2475DA2
Date: 10/27/2011
Time: 16:01:33
Sequence\#: 13

230 V 50 Hz
S/N: 148B8C

## Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| AN02672 | Spectrum Analyzer | E4446A | $8 / 9 / 2010$ | $8 / 9 / 2012$ |  |
| T1 | AN02610 | High Pass Filter | HE9615-150K- <br> $50-720 B$ | $11 / 16 / 2009$ | $11 / 16 / 2011$ |
| T2 | ANP04358 | Cable | RG142 | $5 / 7 / 2010$ | $5 / 7 / 2012$ |
| T3 | ANP06084 | Attenuator | SA18N10W-06 | $12 / 8 / 2010$ | $12 / 8 / 2012$ |
|  | AN00847.1 | 50 uH LISN-Line 1 <br> $(\mathrm{~dB})$ | $3816 / 2 \mathrm{NM}$ | $12 / 21 / 2010$ | $12 / 21 / 2012$ |
| T4 | AN00847.1 | 50uH LISN-Line 2 <br> $(\mathrm{~dB})$ | $3816 / 2 \mathrm{NM}$ | $12 / 21 / 2010$ | $12 / 21 / 2012$ |

## Equipment Under Test (* = EUT):

| Function | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| In-Line 0-10VDC Dimmer <br> or Dual-Switch* | SmartLabs, Inc. | 2475DA2 | 148B8C |

Support Devices:

| Function | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Dimmable Programmed <br> Start Electronic Ballast | Phillips | IZT-132-SC | NA |
| Florescent Light | Ecolux | SP35 | F17T8-SP35-ECO |

## Test Conditions / Notes:

The EUT is placed on the wooden table lined with Styrofoam; total height is 1.5 meter from the ground plane. Connected to the EUT is a light bulb.
Continuous transmit
914.92MHz-915.08MHz

Frequency range of measurement $=150 \mathrm{kHz}-30 \mathrm{MHz}$
$\mathrm{RBW}=\mathrm{VBW}=9 \mathrm{kHz}$
$18^{\circ} \mathrm{C}, 22 \%$ Relative Humidity
Ext Attn: 0 dB
Measurement Data: $\quad$ Reading listed by margin.
Test Lead: L2

| $\#$ | Freq <br> MHz | Rdng <br> $\mathrm{dB} \mu \mathrm{V}$ | T1 <br> dB | T2 <br> dB | T3 <br> dB | T4 <br> dB | Dist <br> Table | Corr <br> $\mathrm{dB} \mu \mathrm{V}$ | Spec <br> $\mathrm{dB} \mu \mathrm{V}$ | Margin <br> dB | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 4.309 M | 38.7 | +0.1 | +0.2 | +5.8 | +0.2 | +0.0 | 45.0 | 46.0 | -1.0 | L 2 |
| 2 | 803.031 k | 38.8 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 44.9 | 46.0 | -1.1 | L 2 |


| $4$ | $\begin{aligned} & 830.264 \mathrm{k} \\ & \text { Ave } \\ & \hline \end{aligned}$ | 38.4 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 44.5 | 46.0 | -1.5 | L2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 830.665k | 44.3 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 50.4 | 46.0 | +4.4 | L2 |
| 6 | 726.674k | 38.4 | +0.2 | +0.1 | +5.8 | $+0.0$ | +0.0 | 44.5 | 46.0 | -1.5 | L2 |
| 7 | 885.710k | 38.0 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 44.1 | 46.0 | -1.9 | L2 |
| 8 | 309.985k | 41.9 | +0.3 | +0.1 | +5.7 | +0.0 | +0.0 | 48.0 | 50.0 | -2.0 | L2 |
| 9 | 245.991k | 43.4 | +0.3 | +0.1 | +5.8 | +0.0 | +0.0 | 49.6 | 51.9 | -2.3 | L2 |
| 10 | 499.059k | 37.5 | +0.3 | +0.1 | +5.7 | +0.0 | +0.0 | 43.6 | 46.0 | -2.4 | L2 |
| 11 | 21.824 M | 39.5 | +0.2 | +0.4 | +5.9 | +1.4 | +0.0 | 47.4 | 50.0 | -2.6 | L2 |
| 12 | 4.428M | 37.1 | +0.1 | +0.2 | +5.8 | +0.2 | +0.0 | 43.4 | 46.0 | -2.6 | L2 |
| 13 | 788.487k | 37.1 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 43.2 | 46.0 | -2.8 | L2 |
| 14 | 21.292M | 39.3 | $+0.2$ | +0.4 | +5.9 | +1.3 | $+0.0$ | 47.1 | 50.0 | -2.9 | L2 |
| 15 | 3.476M | 36.7 | +0.1 | +0.2 | +5.8 | +0.1 | +0.0 | 42.9 | 46.0 | -3.1 | L2 |
| 16 | 21.788 M | 38.9 | +0.2 | +0.4 | +5.9 | +1.4 | +0.0 | 46.8 | 50.0 | -3.2 | L2 |
| 17 | 20.049 M | 39.0 | $+0.2$ | +0.4 | +5.9 | +1.2 | $+0.0$ | 46.7 | 50.0 | -3.3 | L2 |
| 18 | 2.115 M | 36.5 | +0.1 | +0.1 | +5.8 | +0.1 | +0.0 | 42.6 | 46.0 | -3.4 | L2 |
| 19 | 750.672k | 36.5 | $+0.2$ | +0.1 | +5.8 | $+0.0$ | $+0.0$ | 42.6 | 46.0 | -3.4 | L2 |
| 20 | 21.634 M | 38.6 | +0.2 | +0.4 | +5.9 | +1.4 | +0.0 | 46.5 | 50.0 | -3.5 | L2 |
| 21 | 19.454 M | 38.7 | +0.2 | +0.4 | +5.9 | +1.2 | +0.0 | 46.4 | 50.0 | -3.6 | L2 |
| 22 | 1.966M | 36.3 | $+0.1$ | +0.1 | +5.8 | +0.1 | $+0.0$ | 42.4 | 46.0 | -3.6 | L2 |
| 23 | 744.127k | 36.1 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 42.2 | 46.0 | -3.8 | L2 |
| 24 | 739.037k | 36.1 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 42.2 | 46.0 | -3.8 | L2 |
| 25 | 704.858k | 35.7 | +0.3 | +0.1 | +5.8 | +0.0 | +0.0 | 41.9 | 46.0 | -4.1 | L2 |
| 26 | 21.031 M | 38.1 | +0.2 | +0.4 | +5.9 | +1.3 | +0.0 | 45.9 | 50.0 | -4.1 | L2 |
| 27 | 2.591 M | 35.7 | +0.1 | +0.2 | +5.8 | +0.1 | +0.0 | 41.9 | 46.0 | -4.1 | L2 |
| 28 | 2.357 M | 35.5 | +0.1 | +0.2 | +5.8 | +0.1 | +0.0 | 41.7 | 46.0 | -4.3 | L2 |
| 29 | 764.489k | 35.4 | $+0.2$ | $+0.1$ | +5.8 | $+0.0$ | $+0.0$ | 41.5 | 46.0 | -4.5 | L2 |

Page 23 of 70

| 30 | 3.229 M | 35.0 | +0.1 | +0.2 | +5.8 | +0.1 | +0.0 | 41.2 | 46.0 | -4.8 | L2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & 1.281 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 34.7 | +0.2 | +0.1 | +5.8 | +0.1 | +0.0 | 40.9 | 46.0 | -5.1 | L2 |
| $\wedge$ | 1.281 M | 43.9 | +0.2 | +0.1 | +5.8 | +0.1 | +0.0 | 50.1 | 46.0 | +4.1 | L2 |
| 33 | 22.580 M | 36.8 | +0.2 | +0.4 | +5.9 | +1.5 | +0.0 | 44.8 | 50.0 | -5.2 | L2 |
| 34 | 2.285 M | 34.5 | +0.1 | +0.2 | +5.8 | +0.1 | +0.0 | 40.7 | 46.0 | -5.3 | L2 |
| 35 | 508.513 k | 34.4 | +0.3 | +0.1 | +5.7 | +0.0 | +0.0 | 40.5 | 46.0 | -5.5 | L2 |
| 36 | 2.196 M | 34.1 | $+0.1$ | $+0.1$ | +5.8 | +0.1 | +0.0 | 40.2 | 46.0 | -5.8 | L2 |
| 37 | 2.081 M | 34.1 | $+0.1$ | $+0.1$ | +5.8 | +0.1 | +0.0 | 40.2 | 46.0 | -5.8 | L2 |
| 38 | 2.268 M | 33.9 | +0.1 | +0.2 | +5.8 | +0.1 | +0.0 | 40.1 | 46.0 | -5.9 | L2 |
| 39 | 22.121 M | 36.1 | +0.2 | +0.4 | +5.9 | +1.4 | +0.0 | 44.0 | 50.0 | -6.0 | L2 |
| Ave |  | 36.2 | +0.3 | +0.1 | +5.7 | +0.0 | $+0.0$ | 42.3 | 48.3 | -6.0 | L2 |
| $\wedge$ | 380.524 k | 44.1 | +0.3 | +0.1 | +5.7 | +0.0 | +0.0 | 50.2 | 48.3 | +1.9 | L2 |
| Ave |  | 34.1 | +0.3 | +0.1 | +5.7 | +0.0 | +0.0 | 40.2 | 47.3 | -7.1 | L2 |
| $\wedge$ | 428.520 k | 43.2 | +0.3 | +0.1 | +5.7 | +0.0 | +0.0 | 49.3 | 47.3 | +2.0 | L2 |
| Ave |  | 31.4 | +0.3 | +0.1 | +5.8 | +0.0 | +0.0 | 37.6 | 46.0 | -8.4 | L2 |
| $\wedge$ | 613.957 k | 40.9 | +0.3 | +0.1 | +5.8 | +0.0 | +0.0 | 47.1 | 46.0 | +1.1 | L2 |
| Ave |  | 37.9 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 44.0 | 54.2 | -10.2 | L2 |
|  | $191.451 \mathrm{k}$ | 36.7 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 42.8 | 54.0 | -11.2 | L2 |
| $\wedge$ | 191.451k | 51.4 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 57.5 | 54.0 | +3.5 | L2 |
| $\wedge$ | 195.814k | 50.4 | +0.3 | +0.1 | +5.8 | +0.0 | +0.0 | 56.6 | 53.8 | +2.8 | L2 |
|  | $1.060 \mathrm{M}$ | 28.2 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 34.3 | 46.0 | -11.7 | L2 |
| $\wedge$ | 1.060 M | 41.5 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 47.6 | 46.0 | +1.6 | L2 |
| Ave |  | 35.1 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 41.2 | 54.4 | -13.2 | L2 |
| $\wedge$ | 186.360k | 53.0 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 59.1 | 54.2 | +4.9 | L2 |
| $\wedge$ | 181.997k | 50.5 | +0.2 | +0.1 | +5.8 | +0.0 | +0.0 | 56.6 | 54.4 | +2.2 | L2 |

CKC Laboratories Date: 10/27/2011 Time: 16:01:33 SmartLabs, Inc. WO\#: 92348 15.207 AC Mains - Average Test Lead: L2 230V 50Hz Sequence\#: 13 Ext ATTN: 0 dB


## Test Setup Photos



### 15.249(a) RF Power Output

## Test Data

| Test Location: | CKC Laboratories • 110 Olinda Place • Brea, CA 92823 • 714-993-6112 |  |
| :--- | :--- | :--- |
|  |  |  |
| Customer: | SmartLabs, Inc. |  |
| Specification: | $\mathbf{1 5 . 2 4 9}$ Carrier and Spurious Emissions (902-928 MHz Transmitter) |  |
| Work Order \#: | 92348 | Date: 10/27/2011 |
| Test Type: | Maximized Emissions | Time: 08:56:55 |
| Equipment: | In-Line 0-10VDC Dimmer or Dual- | Sequence\#: 10 |
|  | Switch |  |
| Manufacturer: | SmartLabs, Inc. |  |
| Model: | 2475DA2 |  |
| S/N: | 148B8C |  |

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN00309 | Preamp | 8447 D | $5 / 7 / 2010$ | $5 / 7 / 2012$ |
| T2 | AN01995 | Biconilog Antenna | CBL6111C | $3 / 8 / 2010$ | $3 / 8 / 2012$ |
| T3 | ANP05050 | Cable | RG223/U | $3 / 21 / 2011$ | $3 / 21 / 2013$ |
| T4 | ANP05198 | Cable | 8268 | $12 / 21 / 2010$ | $12 / 21 / 2012$ |
|  | AN02672 | Spectrum Analyzer | E4446A | $8 / 9 / 2010$ | $8 / 9 / 2012$ |

Equipment Under Test $(*=$ EUT):

| Function | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| In-Line 0-10VDC Dimmer <br> or Dual-Switch* | SmartLabs, Inc. | 2475DA2 | 148B8C |

Support Devices:

| Function <br> Dimmable Programmed <br> Start Electronic Ballast | Manufacturer | Phillips | Model \# |
| :--- | :--- | :--- | :--- |
| Florescent Light | Ecolux | SP35 | NA |

## Test Conditions / Notes:

The EUT is placed on the wooden table lined with Styrofoam; total height is 1.5 meter from the ground plane. Connected to the EUT is a light bulb.
Continuous transmit
914.92MHz-915.08MHz
$18^{\circ} \mathrm{C}, 22 \%$ Relative Humidity

Ext Attn: 0 dB
Measurement Data: Reading listed by margin. Test Distance: 3 Meters

| \# | Freq <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{array}{r} \text { T3 } \\ \text { dB } \\ \hline \end{array}$ | $\begin{aligned} & \mathrm{T} 4 \\ & \mathrm{~dB} \end{aligned}$ | Dist <br> Table | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Margin } \\ \mathrm{dB} \\ \hline \end{gathered}$ | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { 914.933M } \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 88.9 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 91.7 | $\begin{gathered} 94.0 \\ \text { Y-axis } \end{gathered}$ | -2.3 | Horiz |
|  | $\begin{aligned} & \text { 915.086M } \\ & \text { QP } \end{aligned}$ | 88.9 | -27.1 | +23.6 | $+0.5$ | +5.8 | +0.0 |  | $\begin{gathered} 94.0 \\ \text { Y-axis } \end{gathered}$ | -2.3 | Horiz |
|  | $\begin{aligned} & \text { 915.085M } \\ & \text { QP } \end{aligned}$ | 88.8 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 91.6 | $\begin{gathered} 94.0 \\ \mathrm{X} \text { axis } \end{gathered}$ | -2.4 | Horiz |
| $\wedge$ | 915.085 M | 89.1 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 91.9 | $\begin{gathered} 94.0 \\ \mathrm{X} \text { axis } \end{gathered}$ | -2.1 | Horiz |
| $\wedge$ | 915.086M | 89.1 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 91.9 | $\begin{gathered} 94.0 \\ \text { Y-axis } \end{gathered}$ | -2.1 | Horiz |
| $\wedge$ | 915.083 M | 80.5 | -27.1 | +23.6 | $+0.5$ | +5.8 | +0.0 | 83.3 | $\begin{gathered} 94.0 \\ \mathrm{Z} \text { axis } \end{gathered}$ | -10.7 | Horiz |
|  | $\begin{aligned} & \text { 914.921M } \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 88.6 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 91.4 | $\begin{array}{r} 94.0 \\ \mathrm{X} \text { axis } \\ \hline \end{array}$ | -2.6 | Horiz |
| $\wedge$ | 914.933 M | 89.0 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 91.8 | $\begin{gathered} 94.0 \\ \text { Y-axis } \end{gathered}$ | -2.2 | Horiz |
| $\wedge$ | 914.921 M | 88.9 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 91.7 | $\begin{gathered} 94.0 \\ \mathrm{X} \text { axis } \end{gathered}$ | -2.3 | Horiz |
| $\wedge$ | 914.933 M | 80.5 | -27.1 | +23.6 | $+0.5$ | +5.8 | +0.0 | 83.3 | $\begin{array}{r} \quad 94.0 \\ \mathrm{Z} \text { axis } \end{array}$ | -10.7 | Horiz |
|  | $$ | 87.7 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 90.5 | $\begin{gathered} 94.0 \\ \mathrm{X} \text { axis } \end{gathered}$ | -3.5 | Vert |
| $\wedge$ | 915.085 M | 88.5 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 91.3 | $\begin{gathered} 94.0 \\ \mathrm{X} \text { axis } \end{gathered}$ | -2.7 | Vert |
| $\wedge$ | 915.085M | 84.5 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 87.3 | $\begin{aligned} & 94.0 \\ & \text { Y-axis } \end{aligned}$ | -6.7 | Vert |
| $\wedge$ | 915.085M | 84.0 | -27.1 | +23.6 | $+0.5$ | +5.8 | +0.0 | 86.8 | $\begin{array}{r} \quad 94.0 \\ \mathrm{Z} \text { axis } \end{array}$ | -7.2 | Vert |
|  | $\begin{aligned} & \text { 914.932M } \\ & \text { QP } \\ & \hline \end{aligned}$ | 87.6 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 90.4 | $\begin{aligned} & 94.0 \\ & \mathrm{X} \text { axis } \end{aligned}$ | -3.6 | Vert |
| $\wedge$ | 914.932 M | 88.0 | -27.1 | +23.6 | $+0.5$ | +5.8 | +0.0 | 90.8 | $\begin{aligned} & \quad 94.0 \\ & \mathrm{X} \text { axis } \end{aligned}$ | -3.2 | Vert |
| $\wedge$ | 914.935M | 84.8 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 87.6 | $\begin{gathered} 94.0 \\ \text { Y-axis } \end{gathered}$ | -6.4 | Vert |
| $\wedge$ | 914.935 M | 83.1 | -27.1 | +23.6 | +0.5 | +5.8 | +0.0 | 85.9 | $\begin{aligned} & \quad 94.0 \\ & \mathrm{Z} \text { axis } \end{aligned}$ | -8.1 | Vert |

CKC Laboratories Date: 10/27/2011 Time: 08:56:55 SmartLabs, Inc. WO\#: 92348 15.249 Carrier and Spurious Emissions (902-928 MHz Transmitter) Test Distance: 3 Meters Sequence\#: 10 Ext ATTN: 0 dB


[^1]| Test Location: | CKC Laboratories • 110 Olinda Place • Brea, CA 92823 • 714-993-6112 |  |  |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
| Customer: | SmartLabs, Inc. |  |  |
| Specification: | 15.249 Carrier and Spurious Emissions (902-928 MHz Transmitter) |  |  |
| Work Order \#: | 92348 | Date: | 12/6/2011 |
| Test Type: | Maximized Emissions | Time: | 17:57:32 |
| Equipment: | In-Line 0-10VDC Dimmer or Dual- | Sequence\#: | 13 |
|  | Switch |  |  |
| Manufacturer: | SmartLabs, Inc. | Tested By: E. Wong |  |
| Model: | 2475DA2 |  |  |
| S/N: | 148B8C |  |  |

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN00309 | Preamp | 8447 D | $5 / 7 / 2010$ | $5 / 7 / 2012$ |
| T2 | AN01995 | Biconilog Antenna | CBL6111C | $3 / 8 / 2010$ | $3 / 8 / 2012$ |
| T3 | ANP05050 | Cable | RG223/U | $3 / 21 / 2011$ | $3 / 21 / 2013$ |
| T4 | ANP05198 | Cable | 8268 | $12 / 21 / 2010$ | $12 / 21 / 2012$ |
| T5 | AN02672 | Spectrum Analyzer | E4446A | $8 / 9 / 2010$ | $8 / 9 / 2012$ |

Equipment Under Test $(*=$ EUT):

| Function | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| In-Line 0-10VDC Dimmer or Dual-Switch* | SmartLabs, Inc. | 2475DA2 | 148B8C |

## Support Devices:

| Function <br> Dimmable Programmed <br> Start Electronic Ballast | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Florescent Light | Ecolux | IZT-132-SC | NA |

## Test Conditions / Notes:

The EUT is placed on the wooden table lined with Styrofoam, total height is 0.8 meter from the ground plane. Connected to the EUT is a light bulb and a Sensor with a section of dedicated wire length attached.
Continuous transmit
914.92MHz-915.08MHz

Frequency range of measurement $=$ Fundamental.
$30 \mathrm{MHz}-1000 \mathrm{MHz} ; \mathrm{RBW}=120 \mathrm{kHz}, \mathrm{VBW}=120 \mathrm{kHz}$
$18^{\circ} \mathrm{C}, 22 \%$
Ext Attn: 0 dB
Measurement Data: $\quad$ Reading listed by margin. Test Distance: 3 Meters


| 5 | $915.087 \mathrm{M}$ QP | 86.5 | $\begin{array}{r} \hline-27.1 \\ +0.0 \end{array}$ | +23.6 | +0.5 | +5.8 | Z |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 915.087 M | 86.7 | $\begin{array}{r} -27.1 \\ +0.0 \end{array}$ | +23.6 | +0.5 | +5.8 | +0.0 | 89.5 | 94.0 | -4.5 | Vert |
| $\wedge$ | 915.075 M | 83.3 | $\begin{array}{r} \hline-27.1 \\ +0.0 \end{array}$ | +23.6 | +0.5 | +5.8 | +0.0 |  | $94.0$ | -7.9 | Vert |
| $\wedge$ | 915.075 M | 82.8 | $\begin{array}{r} -27.1 \\ +0.0 \\ \hline \end{array}$ | +23.6 | +0.5 | +5.8 | +0.0 | 85.6 | 94.0 | -8.4 | Vert |

CKC Laboratories Date: 12/6/2011 Time: 17:57:32 SmartLabs, Inc. WO\#: 92348
15.249 Carrier and Spurious Emissions (902-928 MHz Transmitter) Test Distance: 3 Meters Sequence\#: 13 Ext ATTN: 0 dB


## - Readings <br> $\times$ QP Readings <br> - Ambient

O Peak Readings

* Average Readings
* 1-15.249 Carrier and Spurious Emissions (902-928 MHz Transmitter)


## Test Setup Photos


15.249(a) X AXIS

15.249(a) Y AXIS

15.249(a) Z AXIS

15.249(a) BACK VIEW

Tested: December 6, 2011

15.249(a) X AXIS

15.249(a) Y AXIS

15.249(a) Z AXIS

15.249(a) BACK VIEW

LABORATORIES, INC.

### 15.249(a) Field Strength of Harmonics / 15.249(d) Field Strength of Spurious Emissions

## Test Data

Test Location: CKC Laboratories • 110 Olinda Place • Brea, CA 92823 • 714-993-6112
Customer: SmartLabs, Inc.
Specification: 15.249 Carrier and Spurious Emissions (902-928 MHz Transmitter)
Work Order \#: 92348 Date: 10/27/2011
Test Type: Maximized Emissions
Time: 13:55:50
Equipment:
In-Line 0-10VDC Dimmer or Dual-
Sequence\#: 11
Switch
Manufacturer: SmartLabs, Inc. Tested By: Don Nguyen
Model: 2475DA2
S/N: 148B8C
Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :---: | :--- | :--- | :--- | :--- | :--- |
| T1 | AN00309 | Preamp | 8447 D | $5 / 7 / 2010$ | $5 / 7 / 2012$ |
| T2 | AN01995 | Biconilog Antenna | CBL6111C | $3 / 8 / 2010$ | $3 / 8 / 2012$ |
| T3 | ANP05050 | Cable | RG223/U | $3 / 21 / 2011$ | $3 / 21 / 2013$ |
| T4 | ANP05198 | Cable | 8268 | $12 / 21 / 2010$ | $12 / 21 / 2012$ |
| T5 | AN02672 | Spectrum Analyzer | E4446A | $8 / 9 / 2010$ | $8 / 9 / 2012$ |
| T6 | AN00786 | Preamp | 83017 A | $8 / 5 / 2010$ | $8 / 5 / 2012$ |
| T7 | AN00849 | Horn Antenna | 3115 | $4 / 23 / 2010$ | $4 / 23 / 2012$ |
| T8 | AN03239 | Cable | $32022-2-29094 \mathrm{~K}-8 / 30 / 2011$ | $8 / 30 / 2013$ |  |
|  |  |  | 24 TC |  |  |
| T9 | ANP05421 | Cable | Sucoflex 104A | $2 / 12 / 2010$ | $2 / 12 / 2012$ |
| T10 | ANP05563 | Cable | ANDL-1-PNMN- | $9 / 3 / 2010$ | $9 / 3 / 2012$ |
|  |  |  | 48 |  |  |
| T11 | AN03169 | High Pass Filter | HM1155-11SS | $9 / 22 / 2011$ | $9 / 22 / 2013$ |
| T12 | AN00314 | Loop Antenna | 6502 | $6 / 30 / 2010$ | $6 / 30 / 2012$ |

## Equipment Under Test (* = EUT):

| Function | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| In-Line 0-10VDC Dimmer <br> or Dual-Switch* | SmartLabs, Inc. | 2475DA2 | 148B8C |

## Support Devices:

| Function | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Dimmable Programmed | Phillips | IZT-132-SC | NA |
| Start Electronic Ballast |  |  |  |
| Florescent Light | Ecolux | SP35 | F17T8-SP35-ECO |

Test Conditions / Notes:
The EUT is placed on the wooden table lined with Styrofoam; total height is 1.5 meter from the ground plane. Connected to the EUT is a light bulb.
Continuous transmit
914.92MHz-915.08MHz

Frequency range of measurement $=9 \mathrm{kHz}-10 \mathrm{GHz}$.
$9 \mathrm{kH}-150 \mathrm{kHz} ;$ RBW $=200 \mathrm{~Hz}, \mathrm{VBW}=200 \mathrm{~Hz} ; 150 \mathrm{kHz}-30 \mathrm{MHz} ;$ RBW=9 kHz, VBW=9 kHz; $30 \mathrm{MHz}-1000$
$\mathrm{MHz} ;$ RBW $=120 \mathrm{kHz}, V B W=120 \mathrm{kHz}, 1000 \mathrm{MHz}-10,000 \mathrm{MHz} ; \mathrm{RBW}=1 \mathrm{MHz}, \mathrm{VBW}=1 \mathrm{MHz}$.
$18^{\circ} \mathrm{C}, 22 \%$ Relative Humidity
Ext Attn: 0 dB
Measurement Data: $\quad$ Reading listed by margin.
Test Distance: 3 Meters

| $\#$ Freq <br>   <br>  MHz | Rdng $\mathrm{dB} \mu \mathrm{~V}$ | $\begin{aligned} & \text { T1 } \\ & \text { T5 } \\ & \text { T9 } \\ & \text { dB } \end{aligned}$ | $\begin{gathered} \mathrm{T} 2 \\ \text { T6 } \\ \text { T10 } \\ \text { dB } \end{gathered}$ | $\begin{gathered} \mathrm{T} 3 \\ \mathrm{~T} 7 \\ \mathrm{~T} 11 \\ \mathrm{~dB} \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{T} 4 \\ \mathrm{~T} 8 \\ \mathrm{~T} 12 \\ \mathrm{~dB} \\ \hline \end{gathered}$ | Dist <br> Table | Corr $\mathrm{dB} \mu \mathrm{~V} / \mathrm{m}$ | Spec $\mathrm{dB} \mu \mathrm{~V} / \mathrm{m}$ | Margin $\mathrm{dB}$ | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 181830.050 \mathrm{M} \\ & \text { QP } \end{aligned}$ | 59.5 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -38.2 \\ +2.7 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +27.2 \\ +0.4 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 52.9 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -1.1 | Horiz |
| $\begin{aligned} & 21829.947 \mathrm{M} \\ & \mathrm{QP} \end{aligned}$ | 59.5 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -38.2 \\ +2.7 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +27.2 \\ +0.4 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 52.9 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -1.1 | Horiz |
| $\wedge 1829.947 \mathrm{M}$ | 60.7 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -38.2 \\ +2.7 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +27.2 \\ +0.4 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 54.1 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | +0.1 | Horiz |
| $\wedge 1829.917 \mathrm{M}$ | 56.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -38.2 \\ +2.7 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +27.2 \\ +0.4 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | $\overline{49.4}$ | $\begin{aligned} & \quad 54.0 \\ & \mathrm{Z} \text { axis } \end{aligned}$ | -4.6 | Horiz |
| $\begin{aligned} & 5 \text { 1830.050M } \\ & \text { QP } \end{aligned}$ | 59.5 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -38.2 \\ +2.7 \end{array}$ | $\begin{array}{r} +0.0 \\ +27.2 \\ +0.4 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 52.9 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -1.1 | Horiz |
| 6 1830.197M | 59.4 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -38.2 \\ +2.7 \end{array}$ | $\begin{array}{r} +0.0 \\ +27.2 \\ +0.4 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \end{aligned}$ | +0.0 | 52.8 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -1.2 | Horiz |
| $\begin{aligned} & 7 \text { 1829.697M } \\ & \text { QP } \end{aligned}$ | 59.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -38.2 \\ +2.7 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +27.2 \\ +0.4 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 52.5 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -1.5 | Horiz |
| $\begin{aligned} & 81829.790 \mathrm{M} \\ & \mathrm{QP} \end{aligned}$ | 58.7 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -38.2 \\ +2.7 \end{array}$ | $\begin{array}{r} +0.0 \\ +27.2 \\ +0.4 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \end{aligned}$ | +0.0 | 52.1 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -1.9 | Horiz |
| $\wedge 1829.790 \mathrm{M}$ | 59.6 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -38.2 \\ +2.7 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +27.2 \\ +0.4 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 53.0 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -1.0 | Horiz |
| $\wedge 1829.883 \mathrm{M}$ | 59.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -38.2 \\ +2.7 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +27.2 \\ +0.4 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 52.7 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -1.3 | Horiz |
| $\begin{aligned} & 111830.060 \mathrm{M} \\ & \text { QP } \end{aligned}$ | $58.6$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -38.2 \\ +2.7 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +27.2 \\ +0.4 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | $52.0$ | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -2.0 | Horiz |


| $\wedge$ | 1830.050M | 60.6 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -38.2 \\ +2.7 \end{array}$ | $\begin{array}{r} +0.0 \\ +27.2 \\ +0.4 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \end{aligned}$ | +0.0 | 54.0 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | +0.0 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 131829.950 MQP |  | 58.3 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 51.7 | Z ${ }^{54.0}$ | -2.3 | Vert |
|  |  | +0.0 | -38.2 | +27.2 | +0.3 |  |  |  |  |  |
|  |  | +1.0 | +2.7 | +0.4 | +0.0 |  |  |  |  |  |
| $\wedge$ | 1829.950M |  | 59.0 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 52.4 | $\begin{gathered} \quad 54.0 \\ \text { Z axis } \end{gathered}$ | -1.6 | Vert |
|  |  |  |  | +0.0 | -38.2 | +27.2 | +0.3 |  |  |  |  |  |
|  |  | +1.0 |  | +2.7 | +0.4 | +0.0 |  |  |  |  |  |
| 15 | 1830.225M | 57.8 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 51.2 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -2.8 | Vert |  |
|  |  |  | +0.0 | -38.2 | +27.2 | +0.3 |  |  |  |  |  |  |
|  |  |  | +1.0 | +2.7 | +0.4 | +0.0 |  |  |  |  |  |  |
| 16 | 1829.825M | 57.7 | +0.0 | +0.0 | +0.0 | +0.0 | $+0.0$ | 51.1 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -2.9 | Vert |  |
|  |  |  | +0.0 | -38.2 | +27.2 | +0.3 |  |  |  |  |  |  |
|  |  |  | +1.0 | +2.7 | +0.4 | +0.0 |  |  |  |  |  |  |
| 17 | 1829.775M | 57.3 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 50.7 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -3.3 | Vert |  |
|  |  |  | +0.0 | -38.2 | +27.2 | +0.3 |  |  |  |  |  |  |
|  |  |  | +1.0 | +2.7 | +0.4 | +0.0 |  |  |  |  |  |  |
| 18 | 1830.275M | 57.2 | +0.0 | +0.0 | +0.0 | +0.0 | $+0.0$ | 50.6 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -3.4 | Vert |  |
|  |  |  | +0.0 | -38.2 | +27.2 | +0.3 |  |  |  |  |  |  |
|  |  |  | +1.0 | +2.7 | +0.4 | +0.0 |  |  |  |  |  |  |
| 19 | 129.800M | 53.3 | -27.8 | +11.9 | +0.2 | +1.9 | +0.0 | 39.5 | $\begin{gathered} \quad 43.5 \\ \text { Z-axis } \end{gathered}$ | -4.0 | Horiz |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 20 | 164.920M | 52.9 | -27.8 | +10.2 | +0.2 | +2.2 | $+0.0$ | 37.7 | $\begin{gathered} 43.5 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -5.8 | Horiz |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 21 | 9150.000M | 35.7 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 47.3 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -6.7 | Horiz |  |
|  |  |  | +0.0 | -35.4 | +36.7 | +0.7 |  |  |  |  |  |  |
|  |  |  | +2.7 | +6.7 | +0.2 | +0.0 |  |  |  |  |  |  |
| 22 | 160.800M | 51.5 | -27.7 | +10.6 | +0.1 | +2.2 | +0.0 | 36.7 | $\begin{gathered} 43.5 \\ \text { Z-axis } \end{gathered}$ | -6.8 | Horiz |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 23 | 9150.067M | 35.5 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 47.1 | $\begin{gathered} 54.0 \\ \mathrm{Z} \text { axis } \end{gathered}$ | -6.9 | Horiz |  |
|  |  |  | +0.0 | -35.4 | +36.7 | +0.7 |  |  |  |  |  |  |
|  |  |  | +2.7 | +6.7 | +0.2 | +0.0 |  |  |  |  |  |  |
| 24 | 9150.000M | 35.5 | +0.0 | $+0.0$ | +0.0 | +0.0 | $+0.0$ | 47.1 | $\begin{gathered} 54.0 \\ \mathrm{Z} \text { axis } \end{gathered}$ | -6.9 | Vert |  |
|  |  |  | +0.0 | -35.4 | +36.7 | +0.7 |  |  |  |  |  |  |
|  |  |  | +2.7 | +6.7 | +0.2 | +0.0 |  |  |  |  |  |  |
| 25 | 945.078M | 35.7 | -27.1 | +24.0 | +0.5 | +5.9 | $+0.0$ | 39.0 | $\begin{gathered} 46.0 \\ \text { Y-axis } \end{gathered}$ | -7.0 | Horiz |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 26 | 944.928M | 35.6 | -27.1 | +24.0 | +0.5 | +5.9 | +0.0 | 38.9 | $\begin{gathered} 46.0 \\ \text { Y-axis } \end{gathered}$ | -7.1 | Horiz |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 27 | 127.700M | 49.4 | -27.8 | +12.0 | +0.2 | +1.9 | +0.0 | 35.7 | $\begin{gathered} 43.5 \\ \mathrm{Y} \text {-axis } \end{gathered}$ | -7.8 | Horiz |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 28 | 9150.000M | 34.6 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 46.2 | ( ${ }^{54.0}$ | -7.8 | Vert |  |
|  |  |  | +0.0 | -35.4 | +36.7 | +0.7 |  |  |  |  |  |  |
|  |  |  | +2.7 | +6.7 | +0.2 | +0.0 |  |  |  |  |  |  |


| 29 | 9149.927M | 34.6 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +2.7 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -35.4 \\ +6.7 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +36.7 \\ +0.2 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.7 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 46.2 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -7.8 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 30 | 161.920M | 50.4 | $\begin{array}{r} \hline-27.7 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{array}{r} \hline+10.5 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+2.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 35.5 | $\begin{gathered} 43.5 \\ \text { Y-axis } \end{gathered}$ | -8.0 | Vert |
| 31 | 944.927M | 34.5 | $\begin{array}{r} \hline-27.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+24.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +5.9 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 37.8 | $\begin{gathered} 46.0 \\ \text { Y-axis } \end{gathered}$ | -8.2 | Vert |
| 32 | 945.088M | 34.5 | $\begin{array}{r} \hline-27.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+24.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +5.9 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $+0.0$ | 37.8 | $\begin{gathered} 46.0 \\ \text { Z-axis } \end{gathered}$ | -8.2 | Vert |
| 33 | 945.087M | 34.4 | $\begin{array}{r} \hline-27.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+24.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +5.9 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 37.7 | $\begin{gathered} 46.0 \\ \text { Y-axis } \end{gathered}$ | -8.3 | Vert |
| 34 | 944.928M | 34.4 | $\begin{array}{r} \hline-27.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+24.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +5.9 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 37.7 | $\begin{gathered} 46.0 \\ \text { Z-axis } \end{gathered}$ | -8.3 | Vert |
| 35 | 8235.067M | 35.9 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +2.5 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -36.4 \\ +6.2 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +36.6 \\ +0.2 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.7 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} 54.0 \\ \mathrm{Z} \text { axis } \end{gathered}$ | -8.3 | Horiz |
| 36 | 69.420 M | 52.1 | $\begin{array}{r} -27.9 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +5.9 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 31.6 | $\begin{gathered} 40.0 \\ \text { Y-axis } \end{gathered}$ | -8.4 | Vert |
| 37 | 182.420M | 51.3 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+9.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+2.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 35.1 | $\begin{gathered} 43.5 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -8.4 | Horiz |
| 38 | 170.800M | 50.6 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +9.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+2.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} 43.5 \\ \text { Z-axis } \end{gathered}$ | -8.6 | Horiz |
| 39 | 8235.000M | 35.4 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +2.5 \\ & \hline \end{aligned}$ | $\begin{gathered} +0.0 \\ -36.4 \\ +6.2 \\ \hline \end{gathered}$ | $\begin{array}{r} +0.0 \\ +36.6 \\ +0.2 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.7 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} 54.0 \\ \mathrm{Z} \text { axis } \end{gathered}$ | -8.8 | Vert |
| 40 | 33.420 M | 40.9 | $\begin{array}{r} -27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+17.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 31.1 | $\begin{gathered} 40.0 \\ \text { Y-axis } \end{gathered}$ | -8.9 | Vert |
| 41 | 8235.000M | 35.3 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +2.5 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -36.4 \\ +6.2 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +36.6 \\ +0.2 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.7 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} 54.0 \\ \text { X-axis } \end{gathered}$ | -8.9 | Horiz |
| 42 | 194.800M | 50.5 | $\begin{array}{r} \hline-27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +9.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ |  | $\begin{gathered} 43.5 \\ \text { Z-axis } \end{gathered}$ | -9.0 | Horiz |
| 43 | 9149.975M | 33.4 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +2.7 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -35.4 \\ +6.7 \end{array}$ | $\begin{array}{r} +0.0 \\ +36.7 \\ +0.2 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.7 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -9.0 | Vert |
| 44 | 8235.000M | 35.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +2.5 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -36.4 \\ +6.2 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +36.6 \\ +0.2 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.0 \\ & +0.7 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 44.8 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -9.2 | Vert |
| 45 | 6405.000M | 37.4 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +2.2 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -36.5 \\ +5.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +35.2 \\ +0.3 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 44.7 | $\begin{gathered} 54.0 \\ \mathrm{Z} \text { axis } \end{gathered}$ | -9.3 | Vert |

Page 39 of 70

| 46 | 7320.000M | 36.5 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +2.3 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -36.7 \\ +5.8 \end{array}$ | $\begin{array}{r} +0.0 \\ +35.9 \\ +0.2 \end{array}$ | $\begin{aligned} & \hline+0.0 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 44.6 | $\begin{aligned} & \quad 54.0 \\ & \mathrm{Z} \text { axis } \end{aligned}$ | -9.4 | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 47 | 944.928M | 33.3 | $\begin{array}{r} \hline-27.1 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{array}{r} \hline+24.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +5.9 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 36.6 | $\begin{gathered} 46.0 \\ \text { Z-axis } \end{gathered}$ | -9.4 | Horiz |
| 48 | 155.620 M | 48.5 | $\begin{array}{r} -27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+11.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ |  | $\begin{gathered} 43.5 \\ \text { Z-axis } \end{gathered}$ | -9.5 | Vert |
| 49 | 6405.000M | 37.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +2.2 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -36.5 \\ +5.5 \end{array}$ | $\begin{array}{r} +0.0 \\ +35.2 \\ +0.3 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 44.4 | $\begin{aligned} & \quad 54.0 \\ & \mathrm{X} \text {-axis } \end{aligned}$ | -9.6 | Horiz |
| 50 | 7320.067M | 36.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +2.3 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -36.7 \\ +5.8 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +35.9 \\ +0.2 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 44.3 | $\begin{aligned} & \quad 54.0 \\ & \mathrm{Z} \text { axis } \end{aligned}$ | -9.7 | Horiz |
| 51 | 6405.067M | 36.8 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +2.2 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -36.5 \\ +5.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +35.2 \\ +0.3 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ |  | $\begin{aligned} & \quad 54.0 \\ & \mathrm{Z} \text { axis } \end{aligned}$ | -9.9 | Horiz |
| 52 | 8234.975M | 34.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +2.5 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -36.4 \\ +6.2 \end{array}$ | $\begin{array}{r} +0.0 \\ +36.6 \\ +0.2 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.0 \\ & +0.7 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | $44.0$ | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -10.0 | Vert |
| 53 | 141.800 M | 47.6 | $\begin{array}{r} \hline-27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+11.5 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+2.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 33.5 | $\begin{gathered} 43.5 \\ \text { Z-axis } \end{gathered}$ | -10.0 | Horiz |
| 54 | 7319.975M | 35.8 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +2.3 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -36.7 \\ +5.8 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +35.9 \\ +0.2 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -10.1 | Vert |
| 55 | 86.570 M | 47.3 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +8.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} 40.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -10.2 | Vert |
| 56 | 945.078 M | 32.4 | $\begin{array}{r} \hline-27.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+24.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+5.9 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ |  | $\begin{gathered} 46.0 \\ \text { Z-axis } \end{gathered}$ | -10.3 | Horiz |
| 57 | 2745.327M | 46.8 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.8 \\ +3.3 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +29.3 \\ +0.3 \end{array}$ | $\begin{aligned} & \hline+0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 43.7 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -10.3 | Horiz |
| 58 | 2744.827M | 46.7 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.8 \\ +3.3 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +29.3 \\ +0.3 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 43.6 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -10.4 | Horiz |
| 59 | 8234.927M | 33.6 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +2.5 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -36.4 \\ +6.2 \end{array}$ | $\begin{array}{r} +0.0 \\ +36.6 \\ +0.2 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.7 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ |  | $\begin{gathered} \quad 54.0 \\ \text { Y-axis } \end{gathered}$ | -10.6 | Horiz |
| 60 | 2744.725M | 46.4 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.8 \\ +3.3 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +29.3 \\ +0.3 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 43.3 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -10.7 | Vert |
| 61 | 93.980M | 49.3 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +9.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} 43.5 \\ \text { Z-axis } \end{gathered}$ | -10.8 | Vert |
| 62 | 2745.050M | 46.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.4 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.8 \\ +3.3 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +29.3 \\ +0.3 \end{array}$ | $\begin{aligned} & \hline+0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | $43.1$ | $\begin{aligned} & \quad 54.0 \\ & \mathrm{Z} \text { axis } \end{aligned}$ | -10.9 | Vert |


| 63 | 36.770M | 40.5 | -27.8 | +15.2 | +0.1 | $+1.0$ | +0.0 | $\begin{array}{lc} \hline 29.0 & 40.0 \\ & \text { X-axis } \end{array}$ |  | -11.0 | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 64 | 2745.325M | 46.1 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 43.0 | 54.0 | -11.0 | Horiz |
|  |  |  | +0.0 | -37.8 | +29.3 | +0.4 |  | X -axis |  |  |  |
|  |  |  | +1.4 | +3.3 | +0.3 | +0.0 |  |  |  |  |  |
| 65 | 33.570M | 38.6 | -27.8 | +17.0 | +0.1 | +0.9 | +0.0 | 28.8 | 40.0 | -11.2 | Vert |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  | X -axis |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 66 | 164.710M | 47.5 | -27.8 | +10.2 | +0.2 | +2.2 | +0.0 | 32.3 | 43.5 | -11.2 | Horiz |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  | X -axis |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 67 | 2744.700M | 45.6 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 42.5 | 54.0 | -11.5 | Horiz |
|  |  |  | +0.0 | -37.8 | +29.3 | +0.4 |  |  | X -axis |  |  |
|  |  |  | +1.4 | +3.3 | +0.3 | +0.0 |  |  |  |  |  |
| 68 | 7319.927M | 34.4 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 42.5 | 54.0 | -11.5 | Horiz |
|  |  |  | +0.0 | -36.7 | +35.9 | +0.6 |  |  | Y -axis |  |  |
|  |  |  | +2.3 | +5.8 | +0.2 | +0.0 |  |  |  |  |  |
| 69 | 5490.067M | 37.2 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 42.5 | 54.0 | -11.5 | Horiz |
|  |  |  | +0.0 | -36.9 | +34.4 | +0.6 |  |  | Z axis |  |  |
|  |  |  | +2.0 | +5.0 | +0.2 | +0.0 |  |  |  |  |  |
| 70 | 7320.000M | 34.4 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 42.5 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -11.5 | Horiz |
|  |  |  | +0.0 | -36.7 | +35.9 | +0.6 |  |  |  |  |  |
|  |  |  | +2.3 | +5.8 | +0.2 | +0.0 |  |  |  |  |  |
| 71 | 5490.000 M | 37.1 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 42.4 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -11.6 | Horiz |
|  |  |  | +0.0 | -36.9 | +34.4 | +0.6 |  |  |  |  |  |
|  |  |  | +2.0 | +5.0 | +0.2 | +0.0 |  |  |  |  |  |
| 72 | 2745.350M | 45.5 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 42.4 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -11.6 | Vert |
|  |  |  | +0.0 | -37.8 | +29.3 | +0.4 |  |  |  |  |  |
|  |  |  | +1.4 | +3.3 | +0.3 | +0.0 |  |  |  |  |  |
| 73 | 6404.975M | 35.0 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 42.3 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -11.7 | Vert |
|  |  |  | +0.0 | -36.5 | +35.2 | +0.6 |  |  |  |  |  |
|  |  |  | +2.2 | +5.5 | +0.3 | +0.0 |  |  |  |  |  |
| 74 | 5490.000M | 36.9 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 42.2 | $\begin{gathered} 54.0 \\ \mathrm{Z} \text { axis } \end{gathered}$ | -11.8 | Vert |
|  |  |  | +0.0 | -36.9 | +34.4 | +0.6 |  |  |  |  |  |
|  |  |  | +2.0 | +5.0 | +0.2 | +0.0 |  |  |  |  |  |
| 75 | 30.663M | 36.6 | -27.8 | +18.3 | +0.1 | +0.9 | +0.0 | 28.1 | $\begin{gathered} \hline 40.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -11.9 | Vert |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 76 | 7320.000M | 34.0 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 42.1 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -11.9 | Vert |
|  |  |  | +0.0 | -36.7 | +35.9 | +0.6 |  |  |  |  |  |
|  |  |  | +2.3 | +5.8 | +0.2 | +0.0 |  |  |  |  |  |
| 77 | 2745.317M | 45.1 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 42.0 | $\begin{gathered} 54.0 \\ \mathrm{Z} \text { axis } \end{gathered}$ | -12.0 | Horiz |
|  |  |  | +0.0 | -37.8 | +29.3 | +0.4 |  |  |  |  |  |
|  |  |  | +1.4 | +3.3 | +0.3 | +0.0 |  |  |  |  |  |
| 78 | 6405.000M | 34.7 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 42.0 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -12.0 | Vert |
|  |  |  | +0.0 | -36.5 | +35.2 | +0.6 |  |  |  |  |  |
|  |  |  | +2.2 | +5.5 | +0.3 | +0.0 |  |  |  |  |  |
| 79 | 89.420M | 48.5 | -27.8 | +9.0 | +0.1 | +1.6 | +0.0 | 31.4 | 43.5 | -12.1 | Vert |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  | Z-axis |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |


| 80 | 74.920M | 47.3 | $\begin{gathered} -27.8 \\ +0.0 \\ +0.0 \end{gathered}$ | $\begin{aligned} & \hline+6.8 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +1.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 27.9 | $\begin{gathered} 40.0 \\ \text { Z-axis } \end{gathered}$ | -12.1 | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 81 | 2744.792M | 44.9 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.4 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.8 \\ +3.3 \end{array}$ | $\begin{array}{r} +0.0 \\ +29.3 \\ +0.3 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \end{aligned}$ | +0.0 | 41.8 | $\begin{gathered} 54.0 \\ \mathrm{Z} \text { axis } \end{gathered}$ | -12.2 | Horiz |
| 82 | 131.420M | 45.0 | $\begin{array}{r} -27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +11.9 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+2.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 31.3 | $\begin{gathered} 43.5 \\ \text { Y-axis } \end{gathered}$ | -12.2 | Vert |
| 83 | 52.770 M | 47.0 | $\begin{array}{r} \hline-27.9 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+7.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +1.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 27.7 | $\begin{gathered} 40.0 \\ \text { X-axis } \end{gathered}$ | -12.3 | Vert |
| 84 | 6404.927M | 34.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +2.2 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -36.5 \\ +5.5 \end{array}$ | $\begin{array}{r} +0.0 \\ +35.2 \\ +0.3 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.6 \\ & +0.0 \end{aligned}$ | +0.0 | 41.6 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -12.4 | Horiz |
| 85 | 5490.000M | 36.1 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +2.0 \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -36.9 \\ +5.0 \end{array}$ | $\begin{array}{r} +0.0 \\ +34.4 \\ +0.2 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.6 \\ & +0.0 \end{aligned}$ | +0.0 | 41.4 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -12.6 | Vert |
| 86 | 5489.927M | 36.1 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +2.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -36.9 \\ +5.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +34.4 \\ +0.2 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 41.4 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -12.6 | Horiz |
| 87 | 4575.000M | 38.9 | $\begin{array}{r} +0.0 \\ +0.0 \\ +1.9 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ -37.2 \\ +4.4 \end{array}$ | $\begin{array}{r} +0.0 \\ +32.5 \\ +0.3 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.5 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 41.3 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -12.7 | Horiz |
| 88 | 4575.000M | 38.7 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +1.9 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.2 \\ +4.4 \end{array}$ | $\begin{array}{r} +0.0 \\ +32.5 \\ +0.3 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.5 \\ & +0.0 \end{aligned}$ | +0.0 |  | $\begin{gathered} 54.0 \\ \mathrm{Z} \text { axis } \end{gathered}$ | -12.9 | Vert |
| 89 | 5489.975M | 35.8 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +2.0 \end{aligned}$ | $\begin{gathered} +0.0 \\ -36.9 \\ +5.0 \end{gathered}$ | $\begin{array}{r} +0.0 \\ +34.4 \\ +0.2 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.6 \\ & +0.0 \end{aligned}$ | +0.0 |  | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -12.9 | Vert |
| 90 | 221.800 M | 47.2 | $\begin{array}{r} -27.8 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{array}{r} +10.7 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+2.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 |  | $\begin{gathered} 46.0 \\ \text { Z-axis } \end{gathered}$ | -13.1 | Horiz |
| 91 | 163.840M | 45.3 | $\begin{array}{r} -27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +10.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 30.2 | $\begin{gathered} 43.5 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -13.3 | Vert |
| 92 | 4574.975M | 38.2 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +1.9 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.2 \\ +4.4 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +32.5 \\ +0.3 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.5 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 40.6 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -13.4 | Vert |
| 93 | 206.700M | 45.3 | $\begin{array}{r} -27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +9.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 29.9 | $\begin{gathered} 43.5 \\ \text { Y-axis } \end{gathered}$ | -13.6 | Horiz |
| 94 | 4575.067M | 38.0 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +1.9 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.2 \\ +4.4 \end{array}$ | $\begin{array}{r} +0.0 \\ +32.5 \\ +0.3 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.5 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} 54.0 \\ \mathrm{Z} \text { axis } \end{gathered}$ | -13.6 | Horiz |
| 95 | 4575.000M | 37.7 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +1.9 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.2 \\ +4.4 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +32.5 \\ +0.3 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.5 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 40.1 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -13.9 | Vert |
| 96 | 183.940M | 45.6 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +9.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +2.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 29.4 | $\begin{gathered} 43.5 \\ \text { X-axis } \end{gathered}$ | -14.1 | Vert |

Page 42 of 70

| 97 | 164.620M | 44.6 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+10.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+2.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 29.4 | $\begin{gathered} 43.5 \\ \text { Z-axis } \end{gathered}$ | -14.1 | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 98 | 3659.975M | 39.5 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.7 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.4 \\ +4.1 \end{array}$ | $\begin{array}{r} +0.0 \\ +31.3 \\ +0.3 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \end{aligned}$ | +0.0 | 39.9 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -14.1 | Vert |
| 99 | 76.070 M | 44.9 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +7.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 25.7 | $\begin{gathered} \quad 40.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -14.3 | Vert |
| 100 | 3660.000M | 39.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.7 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.4 \\ +4.1 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +31.3 \\ +0.3 \end{array}$ | $\begin{aligned} & \hline+0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 39.6 | $\begin{aligned} & \quad 54.0 \\ & \mathrm{Z} \text { axis } \end{aligned}$ | -14.4 | Vert |
| 101 | 82.970M | 43.7 | $\begin{array}{r} -27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+8.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 25.6 | $\begin{gathered} 40.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -14.4 | Vert |
| 102 | 3659.927M | 39.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.7 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.4 \\ +4.1 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +31.3 \\ +0.3 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 39.5 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -14.5 | Horiz |
| 103 | 194.910M | 45.0 | $\begin{array}{r} -27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +9.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+2.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | $29.0$ | $\begin{gathered} 43.5 \\ \text { Z-axis } \end{gathered}$ | -14.5 | Vert |
| 104 | 945.096M | 28.1 | $\begin{array}{r} \hline-27.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+24.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+5.9 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 31.4 | $\begin{gathered} 46.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -14.6 | Vert |
| 105 | 4574.927M | 37.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.9 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.2 \\ +4.4 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +32.5 \\ +0.3 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.5 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -14.6 | Horiz |
| 106 | 3660.067M | 39.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.7 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.4 \\ +4.1 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +31.3 \\ +0.3 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{aligned} & \quad 54.0 \\ & \mathrm{Z} \text { axis } \end{aligned}$ | -14.6 | Horiz |
| 107 | 56.942M | 45.6 | $\begin{array}{r} -27.9 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +6.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 25.4 | $\begin{gathered} \quad 40.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -14.6 | Horiz |
| 108 | 2744.700M | 42.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.8 \\ +3.3 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +29.3 \\ +0.3 \end{array}$ | $\begin{aligned} & \hline+0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ |  | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -14.9 | Vert |
| 109 | 952.192M | 27.7 | $\begin{array}{r} \hline-27.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+24.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +5.9 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} 46.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -14.9 | Vert |
| 110 | 2745.000M | 42.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.4 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.8 \\ +3.3 \end{array}$ | $\begin{array}{r} +0.0 \\ +29.3 \\ +0.3 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ |  | $\begin{gathered} \quad 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -15.0 | Vert |
| 111 | 2745.000M | 42.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.8 \\ +3.3 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +29.3 \\ +0.3 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 38.9 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -15.1 | Horiz |
| 112 | 3660.000M | 38.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.7 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.4 \\ +4.1 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +31.3 \\ +0.3 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 38.6 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -15.4 | Horiz |
| 113 | 965.088M | 34.9 | $\begin{array}{r} \hline-27.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+24.3 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +6.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 38.5 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -15.5 | Horiz |


| 114 | 3660.000M | 37.8 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.7 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -37.4 \\ +4.1 \end{array}$ | $\begin{array}{r} +0.0 \\ +31.3 \\ +0.3 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \end{aligned}$ | $+0.0$ | 38.2 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -15.8 | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 115 | 964.968M | 34.6 | $\begin{array}{r} -27.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+24.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+6.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 38.2 | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -15.8 | Horiz |
| 116 | 149.140M | 41.7 | $\begin{array}{r} -27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+11.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+2.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 27.5 | $\begin{gathered} 43.5 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -16.0 | Vert |
| 117 | 965.088M | 34.3 | $\begin{array}{r} -27.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+24.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+6.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 37.9 | $\begin{gathered} \text { 54.0 } \\ \text { Z-axis } \end{gathered}$ | -16.1 | Vert |
| 118 | 975.088M | 33.7 | $\begin{array}{r} \hline-27.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+24.4 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +6.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 37.6 | $\begin{gathered} \quad 54.0 \\ \text { Z-axis } \end{gathered}$ | -16.4 | Vert |
| 119 | 964.928M | 34.0 | $\begin{array}{r} \hline-27.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+24.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +6.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ |  | $\begin{gathered} \text { 54.0 } \\ \text { Z-axis } \end{gathered}$ | -16.4 | Vert |
| 120 | 193.620M | 43.1 | $\begin{array}{r} -27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +9.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 27.1 | $\begin{gathered} 43.5 \\ \text { Z-axis } \end{gathered}$ | -16.4 | Vert |
| 121 | 974.928M | 33.5 | $\begin{array}{r} \hline-27.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+24.4 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +6.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 37.4 | $\begin{aligned} & \quad 54.0 \\ & \text { Z-axis } \end{aligned}$ | -16.6 | Vert |
| 122 | 183.120M | 43.1 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+9.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+2.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ |  | $\begin{gathered} 43.5 \\ \text { Z-axis } \end{gathered}$ | -16.6 | Vert |
| 123 | 975.074M | 33.2 | $\begin{array}{r} \hline-27.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+24.4 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +6.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} \quad 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -16.9 | Horiz |
| 124 | 142.920M | 40.2 | $\begin{array}{r} \hline-27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+11.5 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 26.1 | $\begin{gathered} 43.5 \\ \text { Y-axis } \end{gathered}$ | -17.4 | Vert |
| 125 | 99.380 M | 42.1 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+10.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+1.7 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} 43.5 \\ \text { Z-axis } \end{gathered}$ | -17.4 | Vert |
| 126 | 140.940M | 40.1 | $\begin{array}{r} -27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+11.6 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 |  | $\begin{gathered} 43.5 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -17.4 | Vert |
| 127 | 964.938M | 32.9 | $\begin{array}{r} \hline-27.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+24.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +6.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ |  | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -17.5 | Vert |
| 128 | 974.929M | 32.6 | $\begin{array}{r} \hline-27.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+24.4 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +6.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 36.5 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -17.5 | Horiz |
| 129 | 965.088M | 32.8 | $\begin{array}{r} -27.2 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{array}{r} \hline+24.3 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +6.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 |  | $\begin{gathered} 54.0 \\ \text { Y-axis } \end{gathered}$ | -17.6 | Vert |
| 130 | 974.948M | 32.0 | $\begin{array}{r} -27.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+24.4 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+6.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 35.9 | $\begin{gathered} 54.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -18.1 | Vert |


| 131 | 149.620M | 39.6 | $\begin{array}{r} -27.7 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{array}{r} \hline+11.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +2.1 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 25.4 | $\begin{gathered} 43.5 \\ \text { Z-axis } \end{gathered}$ | -18.1 | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 132 | 94.942M | 41.7 | $\begin{gathered} -27.8 \\ +0.0 \\ +0.0 \end{gathered}$ | $\begin{aligned} & +9.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +1.7 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 25.3 | $\begin{gathered} 43.5 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -18.2 | Horiz |
| 133 | 965.098M | 31.1 | $\begin{array}{r} -27.2 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{array}{r} +24.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +6.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 |  | $\begin{aligned} & \text { 54.0 } \\ & \text { Z-axis } \end{aligned}$ | -19.3 | Horiz |
| 134 | 58.970M | 41.0 | $\begin{array}{r} -27.9 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +5.9 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +1.3 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 20.4 | $\begin{aligned} & \quad 40.0 \\ & \mathrm{X} \text {-axis } \end{aligned}$ | -19.6 | Vert |
| 135 | 964.938M | 30.8 | $\begin{array}{r} -27.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +24.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +6.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 34.4 | $\begin{aligned} & \quad 54.0 \\ & \text { Z-axis } \end{aligned}$ | -19.6 | Horiz |
| 136 | 994.938M | 30.2 | $\begin{array}{r} -27.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +24.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +6.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 34.4 | $\begin{gathered} \quad 54.0 \\ \text { Z-axis } \end{gathered}$ | -19.6 | Vert |
| 137 | 995.108M | 30.0 | $\begin{array}{r} -27.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +24.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +6.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | $34.2$ | $\begin{aligned} & \text { 54.0 } \\ & \text { Z-axis } \end{aligned}$ | -19.8 | Vert |
| 138 | 91.942M | 40.4 | $\begin{array}{r} -27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +9.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 23.6 | $\begin{gathered} 43.5 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -19.9 | Horiz |
| 139 | 975.088 M | 30.0 | $\begin{array}{r} -27.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +24.4 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +6.1 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 |  | $\begin{gathered} \text { 54.0 } \\ \text { Z-axis } \end{gathered}$ | -20.1 | Horiz |
| 140 | 974.938M | 29.9 | $\begin{array}{r} -27.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +24.4 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +6.1 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 |  | $\begin{gathered} \text { 54.0 } \\ \text { Z-axis } \end{gathered}$ | -20.2 | Horiz |
| 141 | 181.340M | 39.4 | $\begin{array}{r} -27.8 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +9.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 23.2 | $\begin{gathered} 43.5 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -20.3 | Vert |
| 142 | 99.292 M | 38.1 | $\begin{array}{r} -27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +10.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.7 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 |  | $\begin{gathered} 43.5 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -21.4 | Horiz |
| 143 | 100.592 M | 37.7 | $\begin{array}{r} -27.8 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{array}{r} +10.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +1.7 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 |  | $\begin{aligned} & 43.5 \\ & \mathrm{X} \text {-axis } \end{aligned}$ | -21.7 | Horiz |
| 144 | 223.140 M | 37.5 | $\begin{array}{r} -27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+10.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +2.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 |  | $\begin{gathered} \quad 46.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -22.7 | Vert |
| 145 | 234.240M | 36.1 | $\begin{array}{r} -27.8 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{array}{r} +11.6 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.7 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 |  | $\begin{gathered} 46.0 \\ \mathrm{X} \text {-axis } \end{gathered}$ | -23.2 | Vert |
| 146 | 195.740M | 35.1 | $\begin{array}{r} -27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +9.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 |  | $\begin{array}{r} 43.5 \\ \mathrm{X} \text {-axis } \end{array}$ | -24.4 | Vert |
| 147 | 90.392M | 34.6 | $\begin{array}{r} -27.8 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +9.1 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +1.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 17.6 | $\begin{array}{r} 43.5 \\ \mathrm{X} \text {-axis } \end{array}$ | -25.9 | Horiz |


| 148 | 172.800k | 68.3 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +8.6 \end{aligned}$ | -80.0 | -3.1 | $\begin{gathered} 22.8 \\ \text { X-axis } \end{gathered}$ | -25.9 | Perpe |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 149 | 221.820k | 65.7 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +8.5 \end{aligned}$ | -80.0 | -5.7 | $\begin{gathered} 20.7 \\ \text { Y-axis } \end{gathered}$ | -26.4 | Perpe |
| 150 | 280.740 M | 30.7 | $\begin{array}{r} -27.7 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{array}{r} \hline+13.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.3 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+2.9 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 19.3 | $\begin{gathered} 46.0 \\ \text { X-axis } \end{gathered}$ | -26.7 | Vert |
| 151 | 99.230 M | 32.3 | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+10.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.7 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 16.3 | $\begin{gathered} 43.5 \\ \text { Y-axis } \end{gathered}$ | -27.2 | Horiz |
| 152 | 258.280k | 62.6 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +8.4 \\ & \hline \end{aligned}$ | -80.0 | -8.9 | $\begin{gathered} 19.4 \\ \text { Y-axis } \end{gathered}$ | -28.3 | Perpe |
| 153 | 138.742 M | 26.9 | $\begin{array}{r} \hline-27.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +11.6 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 12.9 | $\begin{gathered} 43.5 \\ \text { X-axis } \end{gathered}$ | -30.6 | Horiz |
| 154 | 1.785 M | 26.7 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +8.8 \\ & \hline \end{aligned}$ | -40.0 | $-4.3$ | $\begin{gathered} 29.5 \\ \text { Z-axis } \end{gathered}$ | -33.8 | Perpe |
| 155 | 2.005 M | 23.5 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +8.8 \\ & \hline \end{aligned}$ | -40.0 | -7.5 | $\begin{gathered} 29.5 \\ \text { Y-axis } \end{gathered}$ | -37.0 | Paral |
| 156 | 2.502 M | 21.9 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +8.8 \\ & \hline \end{aligned}$ | -40.0 |  | $\begin{gathered} 29.5 \\ \text { Y-axis } \end{gathered}$ | -38.6 | Paral |
| 157 | 1.758 M | 21.6 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +8.8 \\ & \hline \end{aligned}$ | -40.0 | -9.4 | $\begin{gathered} 29.5 \\ \text { Z-axis } \end{gathered}$ | -38.9 | Paral |
| 158 | 338.800k | 36.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +8.5 \\ & \hline \end{aligned}$ | -80.0 | -35.2 | $\begin{gathered} 17.0 \\ \text { X-axis } \end{gathered}$ | -52.2 | Paral |

CKC Laboratories Date: 10/27/2011 Time: 13:55:50 SmartLabs, Inc. WO\#: 92348
15.249 Carrier and Spurious Emissions (902-928 MHz Transmitter) Test Distance: 3 Meters Sequence\#: 11 Ext ATTN: 0 dB


| Test Location: | CKC Laboratories • 110 Olinda Place • Brea, CA 92823 • 714-993-6112 |  |  |
| :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |
| Customer: | SmartLabs, Inc. |  |  |
| Specification: | 15.249 Carrier and Spurious Emissions (902-928 MHz Transmitter) |  |  |
| Work Order \#: | 92348 | Date: | 12/6/2011 |
| Test Type: | Maximized Emissions | Time: | 17:27:55 |
| Equipment: | In-Line 0-10VDC Dimmer or Dual- | Sequence\#: | 12 |
|  | Switch |  |  |
| Manufacturer: | SmartLabs, Inc. | Tested By: E. Wong |  |
| Model: | 2475DA2 |  |  |
| S/N: | 148B8C |  |  |

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | AN00309 | Preamp | 8447D | $5 / 7 / 2010$ | $5 / 7 / 2012$ |
|  | AN01995 | Biconilog Antenna | CBL6111C | $3 / 8 / 2010$ | $3 / 8 / 2012$ |
|  | ANP05050 | Cable | RG223/U | $3 / 21 / 2011$ | $3 / 21 / 2013$ |
|  | ANP05198 | Cable | 8268 | $12 / 21 / 2010$ | $12 / 21 / 2012$ |
| T1 | AN02672 | Spectrum Analyzer | E4446A | $8 / 9 / 2010$ | $8 / 9 / 2012$ |
| T2 | AN00786 | Preamp | 83017 A | $8 / 5 / 2010$ | $8 / 5 / 2012$ |
| T3 | AN00849 | Horn Antenna | 3115 | $4 / 23 / 2010$ | $4 / 23 / 2012$ |
| T4 | AN03239 | Cable | $32022-2-29094 \mathrm{~K}-8 / 30 / 2011$ | $8 / 30 / 2013$ |  |
|  |  |  | Cable | Sucoflex 104A | $2 / 12 / 2010$ |
| T5 | ANP05421 | Cable | ANDL-1-PNMN- | $9 / 3 / 2010$ | $2 / 12 / 2012$ |
| T6 | ANP05563 |  | High Pass Filter | HM1155-11SS | $9 / 22 / 2011$ |
|  |  | T0op Antenna | 6502 | $6 / 30 / 2010$ | $9 / 22 / 2012$ |
|  | AN03169 | AN00314 | LT | $6 / 30 / 2012$ |  |

Equipment Under Test $(*=$ EUT $)$ :

| Function | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| In-Line 0-10VDC Dimmer <br> or Dual-Switch* | SmartLabs, Inc. | 2475DA2 | 148B8C |

Support Devices:

| Function <br> Dimmable Programmed <br> Start Electronic Ballast | Manufacturer | Phillips | Model \# |
| :--- | :--- | :--- | :--- |
| Florescent Light | Ecolux | SP35 | NA |

## Test Conditions / Notes:

The EUT is placed on the wooden table lined with Styrofoam, total height is 0.8 meter from the ground plane. Connected to the EUT is a light bulb and a Sensor with a section of dedicated wire length attached.
Continuous transmit
914.92MHz-915.08MHz

Frequency range of measurement $=9 \mathrm{kHz}-10 \mathrm{GHz}$.
$9 \mathrm{kH}-150 \mathrm{kHz} ; \mathrm{RBW}=200 \mathrm{~Hz}, \mathrm{VBW}=200 \mathrm{~Hz} ; 150 \mathrm{kHz}-30 \mathrm{MHz} ; \mathrm{RBW}=9 \mathrm{kHz}, \mathrm{VBW}=9 \mathrm{kHz} ; 30 \mathrm{MHz}-1000$
$\mathrm{MHz} ; \mathrm{RBW}=120 \mathrm{kHz}, \mathrm{VBW}=120 \mathrm{kHz}, 1000 \mathrm{MHz}-10,000 \mathrm{MHz} ; \mathrm{RBW}=1 \mathrm{MHz}, \mathrm{VBW}=1 \mathrm{MHz}$.
$18^{\circ} \mathrm{C}, 22 \%$
Maximized 10 worse frequency of the original test data. All harmonics are checked.

Ext Attn: 0 dB
Measurement Data: Reading listed by margin. Test Distance: 3 Meters


CKC Laboratories Date: 12/6/2011 Time: 17:27:55 SmartLabs, Inc. WO\#: 92348
15.249 Carrier and Spurious Emissions (902-928 MHz Transmitter) Test Distance: 3 Meters Sequence\#: 12 Ext ATTN: 0 dB

0 Peak Readings

* Average Readings
_1-15.249 Carrier and Spurious Emissions (902-928 MHz Transmitter)


## Test Setup Photos


15.249(a) / 15.249(d) X AXIS

15.249(a) / 15.249(d) Y AXIS

15.249(a) / 15.249(d) Z AXIS

15.249(a) / 15.249(d) BACK VIEW

Tested December 6, 2011

15.249(a) / 15.249(d) X AXIS

15.249(a) / 15.249(d) Y AXIS

15.249(a) / 15.249(d) Z AXIS

15.249(a) / 15.249(d) BACK VIEW

LABORATORIES, INC.

## -20 dBc Occupied Bandwidth

## Test Conditions / Setup

The EUT is placed on the wooden table lined with Styrofoam, total height is 1.5 meter from the ground plane. Connected to the EUT is a light bulb.
Continuous transmit
914.92MHz-915.08MHz
15.31(e) compliance: the supply voltage was varied between $85 \%$ and $115 \%$ of the nominal rated supply voltage (120-230Vac), no change in the Fundamental signal level was observed.

Frequency range of measurement $=30 \mathrm{MHz}-1 \mathrm{GHz}$
RBW=120 kHz, VBW=120 kHz
$18^{\circ} \mathrm{C}, 22 \%$ Relative Humidity

Engineer Name: D. Nguyen

## Test Equipment

| Asset/Serial \# | Description | Model | Manufacturer | Cal Date | Cal Due |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AN00309 | Preamp | 8447D | HP | $5 / 7 / 2010$ | $5 / 7 / 2012$ |
| AN01995 | Biconilog Antenna | CBL6111C | Chase | $3 / 8 / 2010$ | $3 / 8 / 2012$ |
| ANP05050 | Cable | RG223/U | Pasternack | $3 / 21 / 2011$ | $3 / 21 / 2013$ |
| ANP05198 | Cable | 8268 | Selden | $12 / 21 / 2010$ | $12 / 21 / 2012$ |
| AN02672 | Spectrum Analyzer | E4446A | Agilent | $8 / 9 / 2010$ | $8 / 9 / 2012$ |

## Test Plot



## Test Setup Photos


-20dBc OBW X AXIS


-20dBc OBW X AXIS

-20dBc OBW BACK VIEW

## Bandedge

## Test Conditions / Setup

The EUT is placed on the wooden table lined with Styrofoam, total height is 1.5 meter from the ground plane. Connected to the EUT is a light bulb.
Continuous transmit
914.92MHz-915.08MHz
15.31(e) compliance: the supply voltage was varied between $85 \%$ and $115 \%$ of the nominal rated supply voltage (120-230Vac), no change in the Fundamental signal level was observed.

Frequency range of measurement $=30 \mathrm{MHz}-1 \mathrm{GHz}$
RBW $=120 \mathrm{kHz}, \mathrm{VBW}=120 \mathrm{kHz}$
$18^{\circ} \mathrm{C}, 22 \%$ Relative Humidity

Engineer Name: D. Nguyen

| Test Equipment |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Asset/Serial \# | Description | Model | Manufacturer | Cal Date | Cal Due |  |
| AN00309 | Preamp | 8447D | HP | $5 / 7 / 2010$ | $5 / 7 / 2012$ |  |
| AN01995 | Biconilog Antenna | CBL6111C | Chase | $3 / 8 / 2010$ | $3 / 8 / 2012$ |  |
| ANP05050 | Cable | RG223/U | Pasternack | $3 / 21 / 2011$ | $3 / 21 / 2013$ |  |
| ANP05198 | Cable | 8268 | Belden | $12 / 21 / 2010$ | $12 / 21 / 2012$ |  |
| AN02672 | Spectrum Analyzer | E4446A | Agilent | $8 / 9 / 2010$ | $8 / 9 / 2012$ |  |

Test Data


LEFT Tx ON


LEFT Tx OFF


RIGHT Tx ON


RIGHT Tx OFF


CENTER

## Test Setup Photos



FCC BANDEDGE X AXIS


FCC BANDEDGE Y AXIS


FCC BANDEDGE Z AXIS


FCC BANDEDGE BACK VIEW


## RSS-210

## 99 \% Bandwidth

## Test Conditions / Setup

The EUT is placed on the wooden table lined with Styrofoam, total height is 1.5 meter from the ground plane. Connected to the EUT is a light bulb.
Continuous transmit
914.92MHz-915.08MHz
15.31(e) compliance: the supply voltage was varied between $85 \%$ and $115 \%$ of the nominal rated supply voltage (120-230Vac), no change in the Fundamental signal level was observed.

Frequency range of measurement $=30 \mathrm{MHz}-1 \mathrm{GHz}$
RBW=120 kHz, VBW=120 kHz
$18^{\circ} \mathrm{C}, 22 \%$ Relative Humidity

Engineer Name: D. Nguyen

| Test Equipment |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Asset/Serial \# | Description | Model | Manufacturer | Cal Date | Cal Due |  |
| AN00309 | Preamp | 8447D | HP | $5 / 7 / 2010$ | $5 / 7 / 2012$ |  |
| AN01995 | Biconilog Antenna | CBL6111C | Chase | $3 / 8 / 2010$ | $3 / 8 / 2012$ |  |
| ANP05050 | Cable | RG223/U | Pasternack | $3 / 21 / 2011$ | $3 / 21 / 2013$ |  |
| ANP05198 | Cable | 8268 | Selden | $12 / 21 / 2010$ | $12 / 21 / 2012$ |  |
| AN02672 | Spectrum Analyzer | E4446A | Agilent | $8 / 9 / 2010$ | $8 / 9 / 2012$ |  |

## Test Data



## Test Setup Photos



RSS 210 X AXIS


RSS 210 X AXIS


RSS 210 Z AXIS


RSS 210 BACK VIEW

## SUPPLEMENTAL INFORMATION

## Measurement Uncertainty

| Uncertainty Value | Parameter |
| :---: | :---: |
| 4.73 dB | Radiated Emissions |
| 3.34 dB | Mains Conducted Emissions |
| 3.30 dB | Disturbance Power |

The reported measurement uncertainties are calculated based on the worst case of all laboratory environments from CKC Laboratories, Inc. test sites. Only those parameters which require estimation of measurement uncertainty are reported. The reported worst case measurement uncertainty is less than the maximum values derived in CISPR 16-4-2. Reported uncertainties represent expanded uncertainties expressed at approximately the $95 \%$ confidence level using a coverage factor of $k=2$. Compliance is deemed to occur provided measurements are below the specified limits.

## Emissions Test Details

TESTING PARAMETERS
Unless otherwise indicated, the following configuration parameters are used for equipment setup: The cables were routed consistent with the typical application by varying the configuration of the test sample. Interface cables were connected to the available ports of the test unit. The effect of varying the position of the cables was investigated to find the configuration that produced maximum emissions. Cables were of the type and length specified in the individual requirements. The length of cable that produced maximum emissions was selected.

The equipment under test (EUT) was set up in a manner that represented its normal use, as shown in the setup photographs. Any special conditions required for the EUT to operate normally are identified in the comments that accompany the emissions tables.

The emissions data was taken with a spectrum analyzer or receiver. Incorporating the applicable correction factors for distance, antenna, cable loss and amplifier gain, the data was reduced as shown in the table below. The corrected data was then compared to the applicable emission limits. Preliminary and final measurements were taken in order to ensure that all emissions from the EUT were found and maximized.

## CORRECTION FACTORS

The basic spectrum analyzer reading was converted using correction factors as shown in the highest emissions readings in the tables. For radiated emissions in $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$, the spectrum analyzer reading in $\mathrm{dB} \mu \mathrm{V}$ was corrected by using the following formula. This reading was then compared to the applicable specification limit.

LABORATORIES, INC.

| SAMPLE CALCULATIONS |  |  |  |
| :--- | :--- | :--- | :---: |
|  | Meter reading | $(\mathrm{dB} \mu \mathrm{V})$ |  |
| + | Antenna Factor | $(\mathrm{dB})$ |  |
| + | Cable Loss | $(\mathrm{dB})$ |  |
| - | Distance Correction | $(\mathrm{dB})$ |  |
| - | Preamplifier Gain | $(\mathrm{dB})$ |  |
| $=$ | Corrected Reading | $(\mathrm{dB} \mu \mathrm{V} / \mathrm{m})$ |  |

## TEST INSTRUMENTATION AND ANALYZER SETTINGS

The test instrumentation and equipment listed were used to collect the emissions data. A spectrum analyzer or receiver was used for all measurements. Unless otherwise specified, the following table shows the measuring equipment bandwidth settings that were used in designated frequency bands. For testing emissions, an appropriate reference level and a vertical scale size of 10 dB per division were used.

| MEASURING EQUIPMENT BANDWIDTH SETTINGS PER FREQUENCY RANGE |  |  |  |
| :---: | :---: | :---: | :---: |
| TEST | BEGINNING FREQUENCY | ENDING FREQUENCY | BANDWIDTH SETTING |
| CONDUCTED EMISSIONS | 150 kHz | 30 MHz | 9 kHz |
| RADIATED EMISSIONS | 30 MHz | 1000 MHz | 120 kHz |
| RADIATED EMISSIONS | 1000 MHz | $>1 \mathrm{GHz}$ | 1 MHz |

## SPECTRUM ANALYZER/RECEIVER DETECTOR FUNCTIONS

The notes that accompany the measurements contained in the emissions tables indicate the type of detector function used to obtain the given readings. Unless otherwise noted, all readings were made in the "positive peak" detector mode. Whenever a "quasi-peak" or "average" reading was recorded, the measurement was annotated with a "QP" or an "Ave" on the appropriate rows of the data sheets. In cases where quasi-peak or average limits were employed and data exists for multiple measurement types for the same frequency then the peak measurement was retained in the report for reference, however the numbering for the affected row was removed and an arrow or carrot ("^") was placed in the far left-hand column indicating that the row above takes precedence for comparison to the limit. The following paragraphs describe in more detail the detector functions and when they were used to obtain the emissions data.

## Peak

In this mode, the spectrum analyzer or receiver recorded all emissions at their peak value as the frequency band selected was scanned. By combining this function with another feature called "peak hold," the measurement device had the ability to measure intermittent or low duty cycle transient emission peak levels. In this mode the measuring device made a slow scan across the frequency band selected and measured the peak emission value found at each frequency across the band.

## Quasi-Peak

Quasi-peak measurements were taken using the quasi-peak detector when the true peak values exceeded or were within 2 dB of a quasi-peak specification limit. Additional QP measurements may have been taken at the discretion of the operator.

## Average

Average measurements were taken using the average detector when the true peak values exceeded or were within 2 dB of an average specification limit. Additional average measurements may have been taken at the discretion of the operator. If the specification or test procedure requires trace averaging, then the averaging was performed using 100 samples or as required by the specification. All other average measurements are performed using video bandwidth averaging. To make these measurements, the test engineer reduces the video bandwidth on the measuring device until the modulation of the signal is filtered out. At this point the measuring device is set into the linear mode and the scan time is reduced.


[^0]:    This report contains a total of 70 pages and may be reproduced in full only. Partial reproduction may only be done with the written consent of CKC Laboratories, Inc.

[^1]:    O Peak Readings

    * Average Readings
    - 1-15.249 Carrier and Spurious Emissions (902-928 MHz Transmitter)

