SAR EVALUATION REPORT

For

Hisense Communication Co., Ltd.

Hisense Infor. Industrial Park, Economic Technology Dev. District, Qingdao, China, 266510

FCC ID: SARHISENSEC389

This Report Concerns: ⊠ Original Report		Equipment Type: CDMA 2000 Mobile Phone	
Test Engineer:	Daniel Deng /	Jor July	
Report No.:	R0405263S		
Report Date:	2004-06-23		
Reviewed By:	Ling Zhang /		
Prepared By:	Bay Area Compliance Laboratory Corporation 230 Commercial Street Sunnyvale, CA 94085 Tel: (408) 732-9162 Fax: (408) 732 9164		

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RIGHT CHEEK TILTED TOUCHING PHANTOM	
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SUMMARY

The US Federal Communications Commission has released the report and order "Guidelines for Evaluating the Environmental Effects of RF Radiation", ET Docket No. 93-62 in August 1996 [1].

The order requires routine SAR evaluation prior to equipment authorization of portable transmitter devices, including portable telephones. For consumer products, the applicable limit is 1.6 mW/g as recommended by the ANSI/IEEE standard C95.1-1992 [6] for an uncontrolled environment (Paragraph 65). According to the Supplement C of OET Bulletin 65 "Evaluating Compliance with FCC Guide-lines for Human Exposure to Radio frequency Electromagnetic Fields", released on Jun 29, 2001 by the FCC, the device should be evaluated at maximum output power (radiated from the antenna) under "worst-case" conditions for normal or intended use, incorporating normal antenna operating positions, device peak performance frequencies and positions for maximum RF energy coupling.

This report describes the methodology and results of experiments performed on wireless data terminal. The objective was to determine if there is RF radiation and if radiation is found, what is the extent of radiation with respect to safety limits. SAR (Specific Absorption Rate) is the measure of RF exposure determined by the amount of RF energy absorbed by human body (or its parts) – to determine how the RF energy couples to the body or head which is a primary health concern for body worn devices. The limit below which the exposure to RF is considered safe by regulatory bodies in North America is 1.6 mW/g average over 1 gram of tissue mass.

The test configurations were laid out on a specially designed test fixture to ensure the reproducibility of measurements. Each configuration was scanned for SAR. Analysis of each scan was carried out to characterize the above effects in the device.

The investigation was limited to the worst-case scenario from the device usage point of view. For the clarity of data analysis, and clarity of presentation, only one tissue simulation was used for the head and body simulation. This means that if SAR was found at the headset position, the magnitude of SAR would be overestimated comparing to SAR to a headset placed in the ear region.

There was no SAR of any concern measured on the device for any of the investigated configurations, please see following table for testing result summary:

1 - REFERENCE

- [1] Federal Communications Commission, \Report and order: Guidelines for evaluating the environmental effects of radiofrequency radiation", Tech. Rep. FCC 96-326, FCC, Washington, D.C. 20554, 1996.
- [2] David L. Means Kwok Chan, Robert F. Cleveland, \Evaluating compliance with FCC guidelines for human exposure to radiofrequency electromagnetic fields", Tech. Rep., Federal Communication Commission, O_ce of Engineering & Technology, Washington, DC, 1997.
- [3] Thomas Schmid, Oliver Egger, and Niels Kuster, \Automated E-field scanning system for dosimetric assessments", IEEE Transactions on Microwave Theory and Techniques, vol. 44, pp. 105{113, Jan. 1996.
- [4] Niels Kuster, Ralph K.astle, and Thomas Schmid, \Dosimetric evaluation of mobile communications equipment with known precision", IEICE Transactions on Communications, vol. E80-B, no. 5, pp. 645 (652, May 1997.
- [5] CENELEC, \Considerations for evaluating of human exposure to electromagnetic fields (EMFs) from mobile telecommunication equipment (MTE) in the frequency range 30MHz 6GHz", Tech. Rep., CENELEC, European Committee for Electrotechnical Standardization, Brussels, 1997.
- [6] ANSI, ANSI/IEEE C95.1-1992: IEEE Standard for Safety Levels with Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 3 kHz to 300 GHz, The Institute of Electrical and Electronics Engineers, Inc., New York, NY 10017, 1992.
- [7] Katja Pokovic, Thomas Schmid, and Niels Kuster, \Robust setup for precise calibration of E-field probes in tissue simulating liquids at mobile communications frequencies", in ICECOM _ 97, Dubrovnik, October 15{17, 1997, pp. 120-24.
- [8] Katja Pokovic, Thomas Schmid, and Niels Kuster, \E-_eld probe with improved isotropy in brain simulating liquids", in Proceedings of the ELMAR, Zadar, Croatia, 23 {25 June, 1996, pp. 172-175.
- [9] Volker Hombach, Klaus Meier, Michael Burkhardt, Eberhard K. uhn, and Niels Kuster, \The dependence of EM energy absorption upon human head modeling at 900 MHz", IEEE Transactions on Microwave Theory and Techniques, vol. 44, no. 10, pp. 1865-1873, Oct. 1996.
- [10] Klaus Meier, Ralf Kastle, Volker Hombach, Roger Tay, and Niels Kuster, \The dependence of EM energy absorption upon human head modeling at 1800 MHz", IEEE Transactions on Microwave Theory and Techniques, Oct. 1997, in press.
- [11] W. Gander, Computermathematik, Birkhaeuser, Basel, 1992.
- [12] W. H. Press, S. A. Teukolsky, W. T. Vetterling, and B. P. Flannery, Numerical Recepies in C, The Art of Scientific Computing, Second Edition, Cambridge University Press, 1992. Dosimetric Evaluation of Sample device, month 1998 9
- [13] NIS81 NAMAS, \The treatment of uncertainty in EMC measurement", Tech. Rep., NAMAS Executive, National Physical Laboratory, Teddington, Middlesex, England, 1994.
- [14] Barry N. Taylor and Christ E. Kuyatt, \Guidelines for evaluating and expressing the uncertainty of NIST measurement results", Tech. Rep., National Institute of Standards and Technology, 1994. Dosimetric Evaluation of Sample device, month 1998 10

2 - TESTING EQUIPMENT

Type / Model	Cal. Date	S/N:
DASY3 Professional Dosimetric System	N/A	N/A
Robot RX60L	N/A	F00/5H31A1/A/01
Robot Controller	N/A	F01/5J72A1/A/01
Dell Computer Optiplex GX110	N/A	N/A
Pentium III, Windows NT	N/A	N/A
SPEAG EDC3	N/A	N/A
SPEAG DAE3	6/04	456
SPEAG E-Field Probe ET3DV6	9/7/02	1604
SPEAG Dummy Probe	N/A	N/A
SPEAG Generic Twin Phantom	N/A	N/A
SPEAG Light Alignment Sensor	N/A	278
Apprel Validation Dipole D-1800-S-2	11/6/04	BCL-049
SPEAG Validation Dipole D900V2	9/3/04	122
Brain Equivalent Matter (800MHz)	Daily	N/A
Brain Equivalent Matter (1900MHz)	Daily	N/A
Brain Equivalent Matter (2450MHz)	Daily	N/A
Muscle Equivalent Matter (800MHz)	Daily	N/A
Muscle Equivalent Matter (1900MHz)	Daily	N/A
Muscle Equivalent Matter (2450MHz)	Daily	N/A
Robot Table	N/A	N/A
Phone Holder	N/A	N/A
Phantom Cover	N/A	N/A
HP Spectrum Analyzer HP8593GM	6/20/04	3009A00791
Microwave Amp. 8349B	N/A	2644A02662
Power Meter HP436A	4/2/04	2709A29209
Power Sensor HP8482A	4/2/04	2349A08568
Signal Generator RS SMIQ O3	2/10/04	1084800403
Network Analyzer HP-8753ES	7/30/04	820079
Dielectric Probe Kit HP85070A	N/A	N/A
Apprel Validation Dipole D-2450-S-1	10/1/04	BCL-141
Dipole Antenna AD-100 (450MHz)	5/7/04	02220

2.2 Equipment Calibration Certificate

Please see the attached file.

Campration Laboratory of Schmid & Partner Engineering AG Zeughausstrasse 43, 8004 Zurich, Switzerland

Client

Bay Area Comp. Lab (BAGL)

CALIBRATION CERTIFICATE ES3DV2 - SN:3019 Object(s) QA CAL-01.v2 Calibration procedure(s) Calibration procedure for dosimetric E-field probes October 9, 2003 Calibration date: In Tolerance (according to the specific calibration document) Condition of the calibrated item This calibration statement documents traceability of M&TE used in the calibration procedures and conformity of the procedures with the ISO/IEC 17025 international standard. All calibrations have been conducted in the closed laboratory facility: environment temperature 22 +/- 2 degrees Celsius and humidity < 75%. Calibration Equipment used (M&TE critical for calibration) Cal Date (Calibrated by, Certificate No.) Scheduled Calibration Model Type Apr-04 Power meter EPM E4419B GB41293874 2-Apr-03 (METAS, No 252-0250) Арг-04 MY41495277 2-Apr-03 (METAS, No 252-0250) Power sensor E4412A Apr-04 Reference 20 dB Attenuator SN: 5086 (20b) 3-Apr-03 (METAS No. 251-0340) 8-Sep-03 (Sintrel SCS No. E-030020) Sep-04 Fluke Process Calibrator Type 702 SN: 6295803 Power sensor HP 8481A MY41092180 18-Sep-02 (Aglient, No. 20020918) In house check: Oct 03 In house check: Aug-05 US3642U01700 4-Aug-99 (SPEAG, in house check Aug-02) RF generator HP 8684C US37390585 18-Oct-01 (Aglient, No. 24BR1033101) In house check: Oct 03 Network Analyzer HP 8753E Name Function Calibrated by: Laboratory Direct Approved by: Date issued: October 9, 2003 This calibration certificate is issued as an intermediate solution until the accreditation process (based on ISO/IEC 17025 International Standard) for Calibration Laboratory of Schmid & Partner Engineering AG is completed.

880-KP0301061-A Page 1 (1)

Zeugnausstrasse 43, 6004 Zurich, Switzeneinu Phone +41 1 245 9700, Fax +41 1 245 9779 info@speag.com, http://www.speag.com

Probe ES3DV2

SN:3019

Additional Conversion Factors

Manufactured: December 5, 2002

Last calibration: July 12, 2003 Add. calibration: October 9, 2003

Calibrated for DASY Systems

(Note: non-compatible with DASY2 system!)

Page 1 of 6

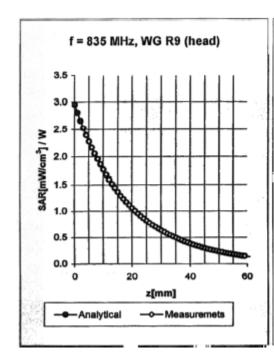
DASY - Parameters of Probe: ES3DV2 SN:3019

Sensitivity in Free	Space	Diode Compression	
NormX	1.05 μV/(V/m) ²	DCP X	99
NormY	1.14 μV/(V/m) ²	DCP Y	99
NormZ	0.98 μV/(V/m) ²	DCP Z	99
Sensor Offset			

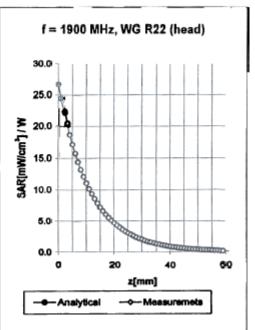
2.1 mm Probe Tip to Sensor Center

Head

Conversion Factor Assessment



1900 MHz



 σ = 1.40 ± 5% mho/m

Head		835 MHz	ε_r = 41.5 ± 5%	σ = 0	0.90 ± 5% mho/	m
Valid for f=7	93-877 N	lHz with Head Ti	ssue Simulating Liquid	according to E	N 50361, P1528-	200X
	ConvF)	← 6.5	± 9.5% (k=2)	ε	Boundary effect	:
	ConvF \	6.5	± 9.5% (k=2)	A	Alpha	0.35

ConvF Z 6.5 ± 9.5% (k=2) Depth 1.46

Valid for f=1805-1995 MHz with Head Tissue Simulating Liquid according to EN 50361, P1528-200X

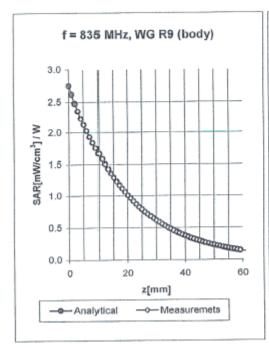
ConvF X 4.7 ± 9.5% (k=2) Boundary effect:

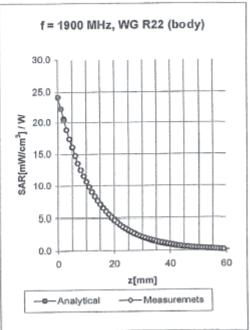
 $\epsilon_{\rm r}$ = 40.0 ± 5%

ConvF Y 4.7 ± 9.5% (k=2) Alpha 0.22 ConvF Z 4.7 ± 9.5% (k=2) Depth 3.48

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Conversion Factor Assessment





Body 835 MHz $\epsilon_r = 55.2 \pm 5\%$ $\sigma = 0.97 \pm 5\%$ mho/m

Valid for f=793-877 MHz with Body Tissue Simulating Liquid according to OET 65 Suppl. C

ConvF X 6.1 ± 9.5% (k=2) Boundary effect:

ConvF Y 6.1 ± 9.5% (k=2) Alpha 0.24

ConvF Z 6.1 ± 9.5% (k=2) Depth 2.00

Body 1900 MHz $\epsilon_r = 53.3 \pm 5\%$ $\sigma = 1.52 \pm 5\%$ mho/m

Valid for f=1805-1995 MHz with Body Tissue Simulating Liquid according to OET 65 Suppl. C

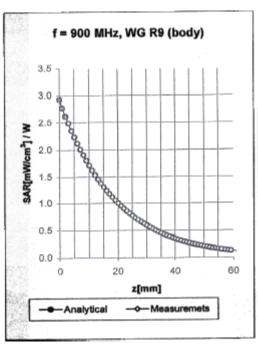
ConvF X 4.6 ± 9.5% (k=2) Boundary effect:

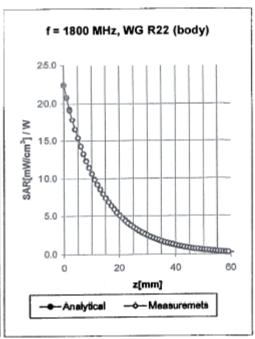
ConvF Y 4.6 ± 9.5% (k=2) Alpha 0.24

ConvF Z 4.6 ± 9.5% (k=2) Depth 2.64

Page 4 of 6

Conversion Factor Assessment





Body	900 MHz	$\epsilon_r = 55.0 \pm 5\%$ $\sigma =$	1.05 ± 5% mho/m
Valid for f=855-945	MHz with Body Tissue \$	Simulating Liquid according to	OET 65 Suppl. C
0	v 64.0	ED/ (k=2)	Boundary effect:

ConvF X	0.1 ± 9.5% (K=Z)	Boundary en	CUL.
ConvF Y	6.1 ± 9.5% (k=2)	Alpha	0.27
ConvE 7	6.1 ± 9.5% (k=2)	Depth	1.82

Body	1800 MHz	$\varepsilon_{\rm r}$ = 53.3 ± 5%	σ = 1.52 ± 5% mho/m
Valid for	f=1710-1890 MHz with Body Tissu	e Simulating Liquid a	ccording to OET 65 Suppl. C

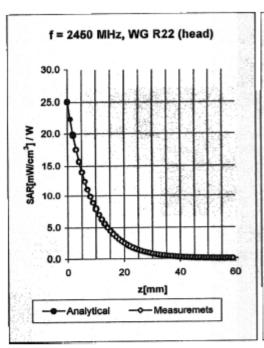
ConvF Y 4.7 ± 9.5% (k=2) Boundary effect:

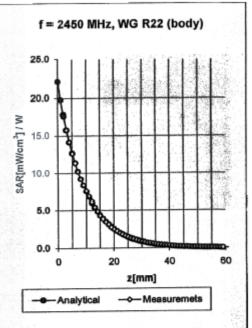
ConvF Y 4.7 ± 9.5% (k=2) Alpha 0.23

ConvF Z 4.7 ± 9.5% (k=2) Depth 2.99

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Conversion Factor Assessment





Head	2450 MHz		ϵ_r = 39.2 ± 5%	σ = 1.80 ± 5% m	nho/m
Valid for f=2400-	2500 MHz with H	lead '	Tissue Simulating Liquid accord	ling to EN 50361,	P1528-200X
Con	vF X	4.5	± 9.5% (k=2)	Boundary ef	fect:
Con	vF Y	4.5	± 9.5% (k=2)	Alpha	0.40
Con	vF Z	4.5	± 9.5% (k=2)	Depth	1.62

Body	2450 MHz	E _f = 52.7 ± 576	0 - 1.50 1 0 /6 111	
Valid	for f=2400-2500 MHz with B	ody Tissue Simulating Liquid ac	cording to OET 65 Sup	ppl. C
	ConvF X	4.2 ± 9.5% (k=2)	Boundary eff	fect:
	ConvF Y	4.2 ± 9.5% (k=2)	Alpha	0.32
	ConvF Z	4.2 ± 9.5% (k=2)	Depth	1.98

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Additional Conversion Factors

for Dosimetric E-Field Probe

'ype:	ES3DV2
Serial Number:	3019
Place of Assessment	Zurich
Date of Assessment:	October 13, 2003
Probe Calibration Date:	October 9, 2003

Schmid & Partner Engineering AG hereby certifies that conversion factor(s) of this probe have been evaluated on the date indicated above. The assessment was performed using the FDTD numerical code SEMCAD of Schmid & Partner Engineering AG. Since the evaluation is coupled with measured conversion factors, it has to be recalculated yearly, i.e., following the re-calibration schedule of the probe. The uncertainty of the numerical assessment is based on the extrapolation from measured value at 900 MHz or at 1800 MHz.

Assessed by:

ES3DV2-SN:3019 October 13, 2003

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Zeughausstresse 43, 8004 Zurich, Switzerland Phone +41 1 245 9700, Fax +41 1 245 9779 info@speeg.com, http://www.speeg.com

Dosimetric E-Field Probe ES3DV2 SN:3019

Conversion factor (± standard deviation)

150 MHz	ConvF	$8.7 \pm 8\%$	$\epsilon_{\rm f} = 52.3 \pm 5\%$
			$\sigma = 0.76 \pm 5\% \text{ mho/m}$
			(head tissue)
150 MHz	ConvF	8.3 ± 8%	$\varepsilon_{\rm r} = 61.9 \pm 5\%$
			$\sigma = 0.80 \pm 5\% \text{ mho/m}$
			(body tissue)
450 MHz	ConvF	7.4 ± 8%	$\varepsilon_r = 43.5 \pm 5\%$
	**		$\sigma = 0.87 \pm 5\% \text{ mho/m}$
			(head tissue)
450 MHz	ConvF	$7.3 \pm 8\%$	$\epsilon_r = 56.7 \pm 5\%$
400 1.2222	-		$\sigma = 0.94 \pm 5\% \text{ mho/m}$
			(body tissue)

ES3DV2-SN:3019 October 13, 2003

835 MHz Body Liquid Validation

```
835MHz Body Liquid validation
Ambient Temp=23 Deg C , Liquid Temp=22 Deg C , 6/11/2004
                                     e''
frequency
                       e '
 815000000.0000
                         53.8436
                                       21.6487
 815800000.0000
                         53.8270
                                       21.6106
                                       21.5509
 816600000.0000
                         53.8738
                                       21.5609
 817400000.0000
                         53.8161
 818200000.0000
                         53.8532
                                       21.5382
                                       21.5274
                         53.7440
 819000000.0000
 819800000.0000
                         53.8197
                                       21.5457
 820600000.0000
                         53.8072
                                       21.4599
                                       21.5114
 821400000.0000
                         53.8993
                         53.8421
 822200000.0000
                                       21.4938
 823000000.0000
                         53.7553
                                       21.5184
 823800000.0000
                         53.7870
                                       21.4661
 824600000.0000
                         53.7889
                                       21.4838
 825400000.0000
                         53.8093
                                       21.4647
                                       21.4345
 826200000.0000
                         53.8058
 827000000.0000
                         53.7859
                                       21.3896
                                       21.4052
 827800000.0000
                         53.7181
                                       21.3880
 828600000.0000
                         53.7808
                                       21.3708
 829400000.0000
                         53.7517
 830200000.0000
                         53.6678
                                       21.3259
                                       21.3289
 831000000.0000
                         53.7450
                         53.7306
 831800000.0000
                                       21.3319
                                       21.3329
 832600000.0000
                         53.7200
 833400000.0000
                                       21.3084
                         53.7240
 834200000.0000
                         53.7134
                                       21.3277
 835000000.0000
                         53.7185
                                       21.3141
 835800000.0000
                         53.7134
                                       21.3115
 836600000.0000
                         53.7073
                                       21,2544
                         53.7222
                                       21.2154
 837400000.0000
                                       21.2237
 838200000.0000
                         53.6973
 83900000.0000
                         53.6904
                                       21.1958
 839800000.0000
                         53.6365
                                       21.1643
                                       21.1254
 840600000.0000
                         53.6514
 841400000.0000
                         53.6410
                                       21.0904
                                       21.1311
 842200000.0000
                         53.6779
 84300000.0000
                         53.6875
                                       21.1267
 843800000.0000
                         53.6411
                                       21.1099
 844600000.0000
                         53.6923
                                       21.1161
                                       21.0743
 845400000.0000
                         53.6151
 846200000.0000
                         53.5523
                                       20.9801
 847000000.0000
                         53.5457
                                       20.9524
 847800000.0000
                         53.6113
                                       20.9783
 848600000.0000
                         53.5992
                                       20.9400
 849400000.0000
                         53.5644
                                       20.9898
                                       20.9842
 850200000.0000
                         53.4880
                                       20.9168
 851000000.0000
                         53.5332
                                       20.9320
 851800000.0000
                         53.5664
 852600000.0000
                         53.5566
                                       20.9331
 853400000.0000
                         53.5162
                                       20.9184
 854200000.0000
                         53.5080
                                       20.9052
 855000000.0000
                         53.5031
                                       20.8456
\sigma = \omega \, \varepsilon_o \, \varepsilon'' = 2 \, \pi f \, \varepsilon_o \, \varepsilon'' = 0.9901
where f = 835 \times 10^6
      \varepsilon_0 = 8.854 \times 10^{-12}

\varepsilon'' = 21.3141
```

835 MHz Head Liquid Validation

835MHz Head Liquid validation Ambient Temp=23 Deg C , Liquid Temp=22 Deg C , 6/11/2004

```
e '
                  e''
frequency
815000000.0000
                    40.1791
                                 19.8695
815800000.0000
                    40.2007
                                 19.8039
                     40.2421
                                 19.8498
816600000.0000
817400000.0000
                    40.1874
                                 19.8164
818200000.0000
                     40.1809
                                 19.8227
819000000.0000
                    40.2430
                                 19.8108
819800000.0000
                                 19.8087
                    40.1280
820600000.0000
                    40.1899
                                 19.8087
                    40.1597
                                 19.8264
821400000.0000
                                 19.7684
822200000.0000
                    40.1951
823000000.0000
                     40.1646
                                 19.8214
823800000.0000
                    40.2085
                                 19.8387
824600000.0000
                    40.1898
                                 19.7825
825400000.0000
                    40.1705
                                 19.7850
826200000.0000
                    40.1699
                                 19.7971
827000000.0000
                    40.1954
                                 19.7696
                                 19.7606
827800000.0000
                     40.1880
                                 19.7196
828600000.0000
                     40.1353
829400000.0000
                     40.1652
                                 19.7179
830200000.0000
                    40.1029
                                 19.7190
831000000.0000
                    40.0964
                                 19.7485
831800000.0000
                    40.1008
                                 19.7396
832600000.0000
                    40.0669
                                 19.7083
833400000.0000
                    40.0850
                                 19.7298
                                 19.7582
834200000.0000
                     40.1054
835000000.0000
                    40.1076
                                 19.7307
835800000.0000
                    40.0885
                                 19.7565
                                 19.7989
836600000.0000
                    40.1367
837400000.0000
                    40.1482
                                 19.7529
838200000.0000
                     40.1109
                                 19.7461
                                 19.7466
83900000.0000
                     40.1453
839800000.0000
                    40.1151
                                 19.7144
840600000.0000
                    40.1471
                                 19.7310
                                 19.7243
841400000.0000
                    40.1099
842200000.0000
                                 19.7963
                    40.1601
84300000.0000
                    40.0955
                                 19.7525
843800000.0000
                    40.0860
                                 19.7596
                                 19.7358
844600000.0000
                    40.1124
845400000.0000
                    40.1352
                                 19.7362
846200000.0000
                    40.1028
                                 19.7433
                    40.0384
                                 19.7227
84700000.0000
                                 19.7404
847800000.0000
                    40.1128
848600000.0000
                    40.0851
                                 19.7383
849400000.0000
                     40.0553
                                 19.6835
850200000.0000
                     40.0896
                                 19.6495
851000000.0000
                     40.1271
                                 19.6945
851800000.0000
                    40.1475
                                 19.6879
852600000.0000
                                 19.6825
                    40.1189
853400000.0000
                     40.1461
                                 19.7306
                                 19.7138
854200000.0000
                    40.1517
855000000.0000
                     40.0877
                                 19.7162
```

$$\sigma = \omega \, \varepsilon_o \, \varepsilon'' = 2 \, \pi f \, \varepsilon_o \, \varepsilon'' = 0.9165$$
where $f = 835 \, x \, 10^6$

$$\varepsilon_o = 8.854 \, x \, 10^{-12}$$

$$\varepsilon'' = 19.7307$$

3 - EUT DESCRIPTION

Applicant: Hisense Communication Co., Ltd.
Product Description: CDMA 2000 Mobile Phone

FCC ID: SARHISENSEC389

Serial Number: C389-001

Transmitter Frequency: 824.73~848.19MHz Maximum Output Power: 0.447 W (ERP)

Dimension: 11.8'L x 4.3'W x1.6'H

RF Exposure environment: General Population/Uncontrolled

Applicable Standard FCC CFR 47, Part 22

Application Type: Certification

Note: The test data gathered are from production sample, serial number: C389-001, provided by the manufacturer.

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¹ Specific Absorption Rate (SAR) is a measure of the rate of energy absorption due to exposure to an RF transmitting source (wireless portable device).

² IEEE/ANSI Std. C95.1-1992 limits are used to determine compliance with FCC ET Docket 93-62.

4 - SYSTEM TEST CONFIGURATION

4.1 Justification

The system was configured for testing in a typical fashion (as normally used by a typical user).

4.2 EUT Exercise Procedure

The EUT exercising program used during SAR testing was designed to exercise the various system components in a manner similar to a typical use.

4.3 Equipment Modifications

No modification(s) were made to the EUT.

5 – CONDUCTED OUTPUT POWER

5.1 Provision Applicable

According to FCC §2.1046 and §22.913 (a), the ERP of mobile transmitters and auxiliary test transmitters must not exceed 7 watts.

5.2 Test Procedure

The RF output of the transmitter was connected to the input of the spectrum analyzer through sufficient attenuation.

5.3 Test equipment

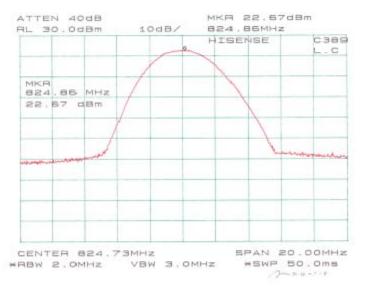
Manufacturer	Description	Model	Serial Number	Cal. Date	
HP	Analyzer, Spectrum	8565EC	3946A00131	2003-06-30	

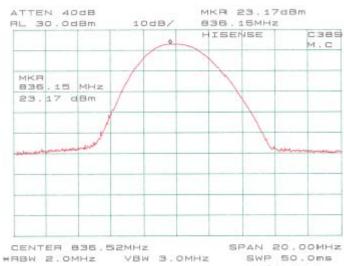
^{*} **Statement of Traceability: BACL Corp.** certifies that all calibrations have been performed in accordance to NVLAP requirements, traceable to the NIST.

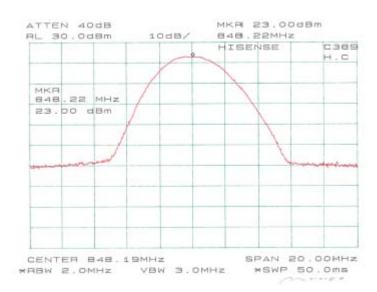
5.4 Test Results

Channel	Frequency (MHz)	Output Power in dBm	Output Power in W	Limit in W
LOW	824.73	22.67	0.185	7
MIDDLE	836.53	23.17	0.207	7
HIGH	848.19	23.00	0.200	7

Please refer to the following plots.







FCC ID: SARHISENSEC389

6 - DOSIMETRIC ASSESSMENT SETUP

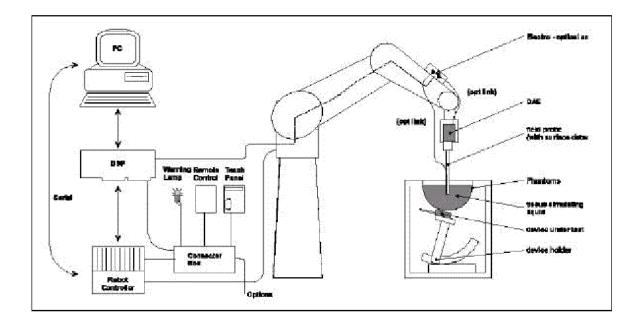
These measurements were performed with the automated near-field scanning system DASY3 from Schmid & Partner Engineering AG (SPEAG). The system is based on a high precision robot (working range greater than 0.9m) which positions the probes with a positional repeatability of better than ± 0.02 mm. Special E- and H-field probes have been developed for measurements close to material discontinuity, the sensors of which are directly loaded with a Schottky diode and connected via highly resistive lines to the data acquisition unit. The system is described in detail in [3].

The SAR measurements were conducted with the dosimetric probe ET3DV6 SN: 1604 (manufactured by SPEAG), designed in the classical triangular configuration [3] and optimized for dosimetric evaluation. The probe has been calibrated according to the procedure described in [7] with accuracy of better than $\pm 10\%$. The spherical isotropy was evaluated with the procedure described in [8] and found to be better than ± 0.25 dB.

The phantom used was the \Generic Twin Phantom" described in [4]. The ear was simulated as a spacer of 4 mm thickness between the earpiece of the phone and the tissue simulating liquid. The Tissue simulation liquid used for each test is in according with the FCC OET65 supplement C as listed below.

Ingredients					Frequer	ncy (MHz)				
(% by weight)	45	0	83	35	9	15	19	00	24	50
Tissue Type	Head	Body	Head	Body	Head	Body	Head	Body	Head	Body
Water	38.56	51.16	41.45	52.4	41.05	56.0	54.9	40.4	62.7	73.2
Salt (Nacl)	3.95	1.49	1.45	1.4	1.35	0.76	0.18	0.5	0.5	0.04
Sugar	56.32	46.78	56.0	45.0	56.5	41.76	0.0	58.0	0.0	0.0
HEC	0.98	0.52	1.0	1.0	1.0	1.21	0.0	1.0	0.0	0.0
Bactericide	0.19	0.05	0.1	0.1	0.1	0.27	0.0	0.1	0.0	0.0
Triton x-100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	36.8	0.0
DGBE	0.0	0.0	0.0	0.0	0.0	0.0	44.92	0.0	0.0	26.7
Dielectric Constant	43.42	58.0	41.5	55.2	42.0	55.9	39.9	53.3	39.8	53.6
Conductivity (s/m)	0.85	0.83	0.9	0.97	1.0	0.98	1.42	1.52	1.88	1.81

6.1 Measurement System Diagram



The DASY3 system for performing compliance tests consist of the following items:

- 1. A standard high precision 6-axis robot (Stäubli RX family) with controller and software.
- 2. An arm extension for accommodating the data acquisition electronics (DAE).
- 3. A dosimetric probe, i.e., an isotropic E-field probe optimized and calibrated for usage in tissue simulating liquid. The probe is equipped with an optical surface detector system.
- 4. A data acquisition electronic (DAE), which performs the signal amplification, signal multiplexing, AD-conversion, offset measurements, mechanical surface detection, collision detection, etc. The unit is battery powered with standard or rechargeable batteries. The signal is optically transmitted to the EOC.
- 5. A unit to operate the optical surface detector, which is connected to the EOC. The Electro-optical coupler (EOC) performs the conversion from the optical into a digital electric signal of the DAE. The EOC is connected to the PC plug-in card. The functions of the PC plug-in card based on a DSP is to perform the time critical task such as signal filtering, surveillance of the robot operation fast movement interrupts.
- 6. A computer operating Windows 95 or larger
- 7. DASY3 software
- 8. Remote control with teaches pendant and additional circuitry for robot safety such as warning lamps, etc.
- 9. The generic twin phantom enabling testing left-hand and right-hand usage.
- 10. The device holder for handheld EUT.
- 11. Tissue simulating liquid mixed according to the given recipes (see Application Note).
- 12. System validation dipoles to validate the proper functioning of the system.

6.2 System Components

ET3DV6 Probe Specification

Construction Symmetrical design with triangular core Built-in optical fiber for surface detection System Built-in shielding against static charges Calibration In air from 10 MHz to 2.5 GHz In brain and muscle simulating tissue at Frequencies of 450 MHz, 900 MHz and

1.8 GHz (accuracy \pm 8%)

Frequency 10 MHz to > 6 GHz; Linearity: \pm 0.2 dB (30 MHz to 3 GHz)

Directivity \pm 0.2 dB in brain tissue (rotation around probe axis)

 \pm 0.4 dB in brain tissue (rotation normal probe axis)

Dynamic 5 mW/g to > 100 mW/g;

Range Linearity: $\pm 0.2 \text{ dB}$

Surface \pm 0.2 mm repeatability in air and clear liquids

Detection over diffuse reflecting surfaces. Dimensions Overall length: 330 mm

Tip length: 16 mm Body diameter: 12 mm Tip diameter: 6.8 mm

Distance from probe tip to dipole centers: 2.7 mm Application General dosimetric up to 3 GHz

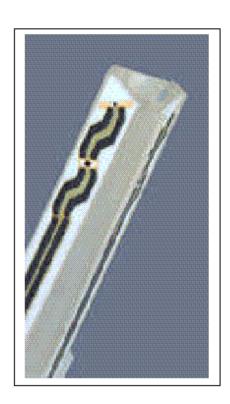
Compliance tests of mobile phones

Fast automatic scanning in arbitrary phantoms

The SAR measurements were conducted with the dosimetric probe ET3DV6 designed in the classical triangular configuration and optimized for dosimetric evaluation. The probe is constructed using the thick film technique; with printed resistive lines on ceramic substrates. The probe is equipped with an optical multi-fiber line ending at the front of the probe tip. It is connected to the EOC box on the robot arm and provides an automatic detection of the phantom surface. Half of the fibers are connected to a pulsed infrared transmitter, the other half to a synchronized receiver. As the probe approaches the surface, the reflection from the surface produces a coupling from the transmitting to the receiving fibers. This reflection increases first during the approach, reaches maximum and then decreases. If the probe is flatly touching the surface, the coupling is zero. The distance of the coupling maximum to the surface is independent of the surface reflectivity and largely independent of the surface to probe angle. The DASY3 software reads the reflection during a software approach and looks for the maximum using a 2 nd order fitting. The approach is stopped when reaching the maximum.



Photograph of the probe



Inside view of ET3DV6 E-field Probe

E-Field Probe Calibration Process

Each probe is calibrated according to a dosimetric assessment procedure described in [6] with accuracy better than +/- 10%. The spherical isotropy was evaluated with the procedure described in [7] and found to be better than +/-0.25dB. The sensitivity parameters (NormX, NormY, NormZ), the diode compression parameter (DCP) and the conversion factor (ConvF) of the probe are tested.

The free space E-field from amplified probe outputs is determined in a test chamber. This is performed in a TEM cell for frequencies bellow 1 GHz, and in a waveguide above 1 GHz for free space. For the free space calibration, the probe is placed in the volumetric center of the cavity and at the proper orientation with the field. The probe is then rotated 360 degrees.

E-field temperature correlation calibration is performed in a flat phantom filled with the appropriate simulated brain tissue. The measured free space E-field in the medium correlates to temperature rise in dielectric medium. For temperature correlation calibration a RF transparent thermistor-based temperature probe is used in conjunction with the E-field probe.

Data Evaluation

The DASY3 software automatically executes the following procedures to calculate the field units from the microvolt readings at the probe connector. The parameters used in the evaluation are stored in the configuration modules of the software:

Probe Parameter:	-Sensitivity	$Norm_i$, a_{i0} , a_{i1} , a_{i2}
	-Conversion Factor	ConvFi
	-Diode compression point	Dcp_i
Device parameter:	-Frequency	f
•	-Crest Factor	cf
Media parameter:	-Conductivity	σ
	-Density	ρ

These parameters must be set correctly in the software. They can either be found in the component documents or be imported into the software from the configuration files issued for the DASY3 components. In the direct measuring mode of the multi-meter option, the parameters of the actual system setup are used. In the scan visualization and export modes, the parameters stored in the corresponding document files are used.

The first step of the evaluation is a linearization of the filtered input signal to account for the compression characteristics of the detector diode. The compensation depends on the input signal, the diode type and the DC-transmission factor from the diode to the evaluation electronics. If the exciting field is pulsed, the crest factor of the signal must be known to correctly compensate for peak power. The formula for each channel can be given as:

$$Vi = Ui + (Ui)^2 cf / dcp_i$$

With Vi = compensated signal of channel i (i = x, y, z)

Ui = input signal of channel i (i = x, y, z)

cf = crest factor of exciting field (DASY parameter)

dcp_i = diode compression point (DASY parameter)

From the compensated input signals the primary field data for each channel can be evaluated:

E-field probes:
$$E_{i} = \sqrt{\frac{V_{i}}{Norm_{i} \cdot ConvF}}$$
H-field probes:
$$H_{i} = \sqrt{Vi} \cdot \frac{a_{i0} + a_{i1}f + a_{i2}f^{2}}{f}$$

With Vi = compensated signal of channel i (i =x, y, z)

 $Norm_i$ = sensor sensitivity of channel i (i = x, y, z)

 $\mu V/(V/m)^2$ for E-field probes

ConF = sensitivity enhancement in solution

a_{ii} = sensor sensitivity factors for H-field probes

f = carrier frequency [GHz]

Ei = electric field strenggy of channel i in V/m H_i = diode compression point (DASY parameter)

The RSS value of the field components gives the total field strength (Hermitian magnitude):

$$E_{tot} = Square Root [(E_x)^2 + (E_y)^2 + (E_z)^2]$$

The primary field data are used to calculate the derived field units.

$$SAR = (E_{tot})^2 \cdot \sigma / (\rho \cdot 1000)$$

With SAR = local specific absorption rate in mW/g

 E_{tot} = total field strength in V/m

 σ = conductivity in [mho/m] or [Siemens/m]

 ρ = equivalent tissue density in g/cm³

Note that the density is normally set to 1 (or 1.06), to account for actual brain density rather than the density of the simulation liquid.

The power flow density is calculated assuming the excitation field as a free space field.

$$P_{\text{nwe}} = (E_{\text{tot}})^2 / 3770 \text{ or } P_{\text{nwe}} = (H_{\text{tot}})2 \cdot 37.7$$

With P_{pwe} = equivalent power density of a plane wave in mW/cm3

 E_{tot} = total electric filed strength in V/m

 H_{tot} = total magnetic filed strength in V/m

Generic Twin Phantom

The Generic Twin Phantom is constructed of a fiberglass shell integrated in a wooden table. The shape of the shell is based on data from an anatomical study designed to determine the maximum exposure in at least 90% of all users [9][10]. It enables the dosimetric evaluation of left and right hand phone usage as well as body mounted usage at the flat phantom region. A cover prevents the evaporation of the liquid. Reference markings on the Phantom allows the complete setup of all predefined phantom positions and measurement grids by manually teaching three points in the robot. Shell Thickness 2 ± 0.1 mm Filling Volume Approx. 20 liters

Dimensions 810 x 1000 x 500 mm (H x L x W)



Generic Twin Phantom

Device Holder

In combination with the Generic Twin Phantom V3.0, the Mounting Device enables the rotation of the mounted transmitter in spherical coordinates whereby the rotation points is the ear opening. The devices can be easily, accurately, and repeatedly positioned according to the FCC and CENELEC specifications. The device holder can be locked at different phantom locations (left head, right head, flat phantom).

* Note: A simulating human hand is not used due to the complex anatomical and geometrical structure of the hand that may produced infinite number of configurations [10]. To produce the worst-case condition (the hand absorbs antenna output power), the hand is omitted during the tests.



Device Holder

6.3 Measurement Uncertainty

The uncertainty budget has been determined for the DASY3 measurement system according to the NIS81 [13] and the NIST1297 [14] documents and is given in the following Table.

Measurement Uncertainty An IEEE P1528-2002	alysis per							
Description	Section	Reported Variance (%)	Probability Distributio n type	Divisor	Ci (1g)	Ui (1g)	Vi	welc/satt series term
Probe Calibration	E.2.1	4.80	N	1	1	4.80	1.00E+09	5.30842E-07
Axial isotropy	E.2.2	4.70	R	1.732	0.707107	1.92	1.00E+09	1.35563E-08
Hemispherical isotropy	E.2.2	9.60	R	1.732	0.707107	3.92	1.00E+09	2.35957E-07
Boundary effects	E.2.3	8.30	R	1.732	1	4.79	1.00E+09	5.27377E-07
Linearity	E.2.4	4.70	R	1.732	1	2.71	1.00E+09	5.4225E-08
System Detection Limit	E.2.5	1.00	R	1.732	1	0.58	1.00E+09	1.11124E-10
Readout Electronics	E.2.6	0.00	N	1	1	0.00	1.00E+09	0
Response time	E.2.7	0.00	R	1.732	1	0.00	1.00E+09	0
Integration time	E.2.8	0.00	R	1.732	1	0.00	1.00E+09	0
RF Ambient conditions	E.6.1	3.00	R	1.732	1	1.73	1.00E+09	9.00106E-09
Probe positioning mechanical tolerance	E.6.2	0.40	R	1.732	1	0.23	1.00E+09	2.84478E-12
Probe positioning wrt phantom shell	E.6.3	2.90	R	1.732	1	1.67	1.00E+09	7.8596E-09
Extra/inter-polation & integration algorithms for max SAR evaluation	E.5.2	3.90	R	1.732	1	2.25	1.00E+09	2.57079E-08
Test sample positioning	8, E.4.2	6.00	R	1.732	1	3.46	1.00E+09	1.44017E-07
Device holder distance tolerance	E.4.1	5.00	N	1	1	5.00		0.000000625
Output power and SAR drift measurement	8, E.6.6.2	5.00	R	1.732	1	2.89		6.94526E-08
Phantom uncertainty, shell thickness tolerance	E.3.1	4.00	R	1.732	1	2.31	1.00E+09	2.84478E-08
Liquid conductivity, deviation from target values	E.3.2	5.00	R	1.732	0.64	1.85	1.00E+09	1.16522E-08
Liquid conductivity, measurement uncertainty	E.3.3	5.00	N	1	0.64	3.20		20.97152
Liquid permitivity, deviation from target values	E.3.2	5.00	R	1.732	0.6	1.73	1.00E+09	9.00106E-09
Liquid permitivity, measurement uncertainty	E.3.3	5.00	N	1	0.6	3.00	5	16.2
Probe isotropy sensitivity coefficient	0.5							689
Combined Standard Uncertainty						12.65		
Expanded Uncertainty, 95% confidence		k=	2.004			25.34	%	

7 - SYSTEM EVALUATION

7.1 Simulated Tissue Liquid Parameter Confirmation

The dielectric parameters were checked prior to assessment using the HP85070A dielectric probe kit. The dielectric parameters measured are reported in each correspondent section:

7.2 Evaluation Procedures

Maximum Search

The maximum search is automatically performed after each coarse scan measurement. It is based on splines in two or three dimensions. The procedure can find the maximum for most SAR distributions even with relatively large grid spacings. After the coarse scan measurement, the probe is automatically moved to a position at the interpolated maximum. The following scan can directly use this position for reference, e.g., for a finer resolution grid or the cube evaluations.

Extrapolation

The extrapolation can be used in z-axis scans with automatic surface detection. The SAR values can be extrapolated to the inner phantom surface. The extrapolation distance is the sum of the probe sensor offset, the surface detection distance and the grid offset. The extrapolation is based on fourth order polynomal functions. The extrapolation is only available for SAR values.

Boundary Corrections

The correction of the probe boundary effect in the vicinity of the phantom surface can be done in two different ways. In the standard (worse case) evaluation, the boundary effect is reduced by different weights for the lowest measured points in the extrapolation routine. The result is a slight overestimation of the extrapolated SAR values (2% to 8%) depending on the SAR distribution and gradient. The advanced evaluation makes a full compensation of the boundary effect before doing the extrapolation. This is only possible of probes with specifications on the boundary effect.

Peak Search for 1g and 10g cube averaged SAR

The 1g and 10g peak evaluations are only available for the predefined cube 4x4x7 and cube 5x5x7 scans. The routine are verified and optimized for the grid dimensions used in these cube measurements. The measured volume of 32x32x35mm contains about 35g of tissue. The first procedure is an extrapolation (incl. Boundary correction) to get the points between the lowest measured plane and the surface. The next step uses 3D interpolation get all points within the measured volume in a 1mm grid (35000 points). In the last step, a 1g cube is place numerically into the volume and its averaged SAR is calculated. This cube is the moved around until the highest averaged SAR is found. This last procedure is repeated for a 10g cube. If the highest SAR is found at the edge of the measured volume, the system will issue a warning,: higher SAR values might be found outside of the measured volume. In that case the cube measurement can be repeated, using the new interpolated maximum as the center.

7.3 System Accuracy Verification

Prior to the assessment, the system validation kit was used to test whether the system was operating within its specifications of $\pm 10\%$. The validation results are tabulated below. And also the corresponding SAR plot is attached as well in the SAR plots files.

IEEE P1528 recommended reference value

Frequency (MHz)	1 g SAR	10 g SAR	Local SAR at surface (above feed point)	Local SAR at surface (v=2cm offset from feed point)
300	3.0	2.0	4.4	2.1
450	4.9	3.3	7.2	3.2
835	9.5	6.2	14.1	4.9
900	10.8	6.9	16.4	5.4
1450	29.0	16.0	50.2	6.5
1800	38.1	19.8	69.5	6.8
1900	39.7	20.5	72.1	6.6
2000	41.1	21.1	74.6	6.5
2450	52.4	24.0	104.2	7.7
3000	63.8	25.7	140.2	9.5

Validation Dipole SAR Reference Test Result for Body

Validation Measurement	SAR @ 0.025W Input averaged over 1g	SAR @ 1W Input averaged over 1g	SAR @ 0.025W Input averaged over 10g	SAR @ 1W Input averaged over 10g
Test 1	0.222	8.88	0.112	4.48
Test 2	0.221	8.84	0.111	4.44
Test 3	0.222	8.88	0.112	4.48
Test 4	0.220	8.80	0.111	4.44
Test 5	0.223	8.92	0.113	4.52
Test 6	0.222	8.88	0.115	4.60
Test 7	0.221	8.84	0.114	4.56
Test 8	0.222	8.88	0.114	4.56
Test 9	0.223	8.92	0.113	4.52
Test 10	0.222	8.88	0.112	4.48
Average	0.2218	8.872	0.1127	4.51

System Validation Result

Ambient Temperature (°C): 23

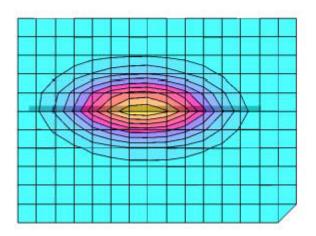
2004-06-11

Simulant	Freq MHz]	Parameters	Liquid Temp [°C]	Target Value	Measured Value	Deviation	Limits [%]
D. J.	025	$\epsilon_{\rm r}$	22	55.2	53.7	-2.72	±5
Body	835	σ	22	0.97	0.99	2.06	±5
		1g SAR	22	8.872	9.36	5.50	±10
		$\varepsilon_{\rm r}$	22	41.5	40.1	-3.37	±5
Head	835	σ	22	0.90	0.92	2.22	±5
		1g SAR	22	9.5	10.03	5.58	±10

 $[\]varepsilon_r$ = relative permittivity, σ = conductivity and ρ =1000kg/m³

Forward Power for body = 20.5 dBm = 112.20 mWForward Power for head = 20.4 dBm = 109.65 mW System Validation 835 MHz Body liquid (Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, Forward Power = 20.5 dBm, 6/11/2004)

SAM Phantom; Flat Section; Position: $(90^\circ, 90^\circ)$; Frequency: 835 MHz Probe: ES3DV2 - SN3019; ConvF(6.10,6.10,6.10); Crest factor: 1.0; 835 Body MHz: $\sigma=0.99$ mho/m $\epsilon_r=53.7$ $\rho=1.00$ g/cm³ Cube 5x5x7; SAR (1g): 1.05 mW/g, SAR (10g): 0.638 mW/g, (Worst-case extrapolation) Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0 Powerdrift: 0.00 dB



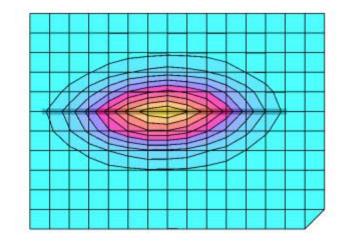


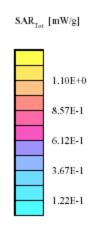
System Validation 835 MHz Head liquid (Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C,Forward Power =20.4 dBm, 6/11/2004)

SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 835 MHz

Probe: ES3DV2 - SN3019; ConvF(6.50,6.50,6.50); Crest factor: 1.0; 835 (Head) MHz: $\sigma = 0.92 \text{ mho/m s}, = 40.1 \text{ } \rho = 1.00 \text{ g/cm}^3$

Cube 5x5x7: SAR (1g): 1.10 mW/g, SAR (10g): 0.673 mW/g, (Worst-case extrapolation)
Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0
Powerdrift: 0.00 dB





7.4 SAR Evaluation Procedure

- a. The evaluation was performed in the applicable area of the phantom depending on the type of device being tested. For device held to the dear during normal operation, both the left and right ear positions were evaluated in accordance with FCC OET Bulletin 65, Supplement C (Edition 01-01) using the SAM phantom. For body-worn and face-held devices a planar phantom was used. The EUT in the test setup for body-worn and face-held devices was placed in three different positions (relative to the phantom): with belt clip, without belt clip and 2.5cm facing left head side and 2.5cm facing right head side.
- b. The SAR was determined by a pre-defined procedure within the DASY3 software. Upon completion of a reference and optical surface check, the exposed region of the phantom was scanned near the inner surface with a grid spacing of 20mm x 20mm.
- c. A 5x5x7 matrix was performed around the greatest special SAR distribution found during the area scan of the applicable exposed region. SAR values were then calculated using a 3-D spline interpolation algorithm and averaged over spatial volumes of 1 and 10 grams.
- d. The depth of the simulating tissue in the planar used for the SAR evaluation and system validation was no less than 15.0cm.
- e. For this particular evaluation, a stack of low-density, low-loss dielectric foamed polystyrene was used in place of the device holder.
- f. Re-measurement of the SAR value at the same location as in a. If the value changed by more than 5%, the evaluation was repeated.

7.5 Exposure Limits

Table 1: Limits for Occupational/Controlled Exposure (W/kg)

Whole-Body	Partial-Body	Hands. Wrists. Feet and Ankles
0.4	8.0	20.0

Table 2: Limits for General Population/Uncontrolled Exposure (W/kg)

Whole-Body	Partial-Body	Hands. Wrists. Feet and Ankles		
0.08	1.6	4.0		

Note: Whole-body SAR is averaged over the entire body, partial-body SAR is averaged over any 1 gram of tissue defined as a tissue volume in the shape of a cube SAR for hands, writs, feet and ankles is averaged over any 10 grams of tissue defined as a tissue volume in the shape of a cube.

Population/Uncontrolled Environments are defined as locations where there is the exposure of individual who have no knowledge or control of their exposure.

Occupational/Controlled Environments are defined as locations where there is exposure that may be incurred by people who are aware of the potential for exposure (i.e. as a result of employment or occupation).

Population/uncontrolled environments Partial-body limit 1.6W/kg applied to the EUT.

8 - TEST RESULTS

This page summarizes the results of the performed dosimeter evaluation. The plots with the corresponding SAR distributions, which reveal information about the location of the maximum SAR with respect to the device could be found in the following pages.

According to the data in section 8.1, the EUT <u>complied with the FCC 2.1093 RF Exposure</u> standards, with worst case of 1.50 mW/g.

8.1 SAR Test Data

Ambient Temperature (°C): 23.0 Relative Humidity (%): 49.3

Position	Frequency (MHz)	Output Power (dBm)	Test Type	Accessories	Liquid	Phantom	Measured (mW/g)	Limit (mW/g)	Plot #
Back Side Touching	825	22.67		headset			1.50		1
Back Side Touching	836	23.17		headset			1.49		2
Back Side Touching	848	23.00	Body	headset	Body	Flat	1.46		3
Face Touching	825	22.67	Worn	headset	Бойу	гіаі	1.06		4
Face Touching	836	23.17		headset			0.993		5
Face Touching	848	23.00		headset			0.976		6
Left Head Cheek Touching	825	22.67		None			1.08		7
Left Head Cheek Touching	836	23.17		None		Head	1.16	1.6	8
Left Head Cheek Touching	848	23.00		None			1.16		9
Left Head Tilted Touching	825	22.67		None			0.826		10
Left Head Tilted Touching	836	23.17		None			0.815		11
Left Head Tilted Touching	848	23.00	Head	None	Head		0.747		12
Right Head Cheek Touching	825	22.67	Ticau	None	Ticau	Head	1.28		13
Right Head Cheek Touching	836	23.17		None			1.32		14
Right Head Cheek Touching	848	23.00		None			1.10		15
Right Head Tilted Touching	825	22.67		None			0.778		16
Right Head Tilted Touching	836	23.17		None			0.781		17
Right Head Tilted Touching	848	23.00		None			0.781		18

8.2 Plots of Test Result

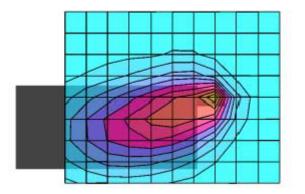
The plots of test result were attached as reference.

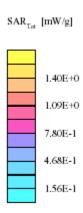
HisenceCommunication Co., Model: C389 (Body Worn, Back touching flat phantom with accessory (headset), Low Channel, Ambient Temp = 23 DegC, Liquid Temp = 22 Deg C, 6/11/2004)

SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 825 MHz Probe: ES3DV2 - SN3019; ConvF(6.10,6.10,6.10); Crest factor: 1.0; (Body) 835 MHz: $\sigma = 0.99$ mho/m $\epsilon_r = 53.7$ $\rho = 1.00$ g/cm³

Cube 5x5x7: SAR (1g): 1.50 $\,$ mW/g, SAR (10g): 0.747 $\,$ mW/g, (Worst-case extrapolation) Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0

Powerdrift: -0.04 dB





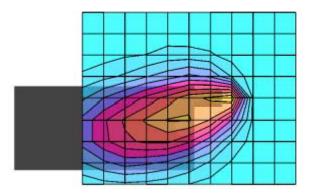
HisenceCommunication Co., Model: C389 (Body Worn, Back touching flat phantom with accessory (headset), Mid channel, Ambient Temp = 23 DegC, Liquid Temp = 22 Deg C, 6/11/2004)

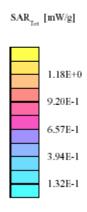
SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 836 MHz

Probe: ES3DV2 - SN3019; ConvF(6.10,6.10,6.10); Crest factor: 1.0; (Body) 835 MHz: $\sigma = 0.99 \text{ mho/m} \, \epsilon_r = 53.7 \, \rho = 1.00 \, \text{g/cm}^3$

Cube 5x5x7: SAR (1g): 1.49 $\,$ mW/g, SAR (10g): 0.732 $\,$ mW/g, (Worst-case extrapolation) Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0 $\,$

Powerdrift: -0.03 dB



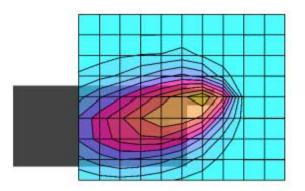


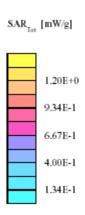
HisenceCommunication Co., Model: C389 (Body Worn, Back touching flat phantom with accessory (headset), High channel, Ambient Temp = 23 DegC, Liquid Temp = 22 Deg C, 6/11/2004)

SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 848 MHz

Probe: ES3DV2 - SN3019; ConvF(6.10,6.10,6.10); Crest factor: 1.0; (Body) 835 MHz: $\sigma = 0.99 \text{ mho/m} \epsilon_{r} = 53.7 \text{ p} = 1.00 \text{ g/cm}^3$

Cube 5x5x7: SAR (1g): 1.46 $\,$ mW/g, SAR (10g): 0.761 $\,$ mW/g, (Worst-case extrapolation) Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0

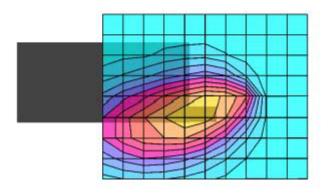




HisenceCommunication Co., Model: C389 (Body Worn, Face touching flat phantom with accessory (headset), Low Channel, Ambient Temp = 23 DegC, Liquid Temp = 22 Deg C, 6/11/2004)

SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 825 MHz

Probe: ES3DV2 - SN3019; ConvF(6.10,6.10,6.10); Crest factor: 1.0; (Body) 835 MHz: $\sigma = 0.99 \text{ mho/m} \, \epsilon_r = 53.7 \, \rho = 1.00 \, \text{g/cm}^3$ Cube 5x5x7: SAR (1g): 1.06 mW/g, SAR (10g): 0.715 mW/g, (Worst-case extrapolation) Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0 Powerdrift: -0.03 dB





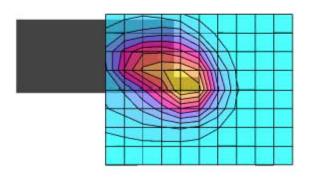
HisenceCommunication Co., Model: C389 (Body Worn, Face touching flat phantom with accessory (headset), Mid Channel, Ambient Temp = 23 DegC, Liquid Temp = 22 Deg C, 6/11/2004)

SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 836 MHz

Probe: ES3DV2 - SN3019; ConvF(6.10,6.10,6.10); Crest factor: 1.0; (Body) 835 MHz: $\sigma = 0.99 \text{ mho/m} \, \epsilon_r = 53.7 \, \rho = 1.00 \, \text{g/cm}^3$

Cube 5x5x7: SAR (1g): 0.993 mW/g, SAR (10g): 0.609 mW/g, (Worst-case extrapolation)

Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0



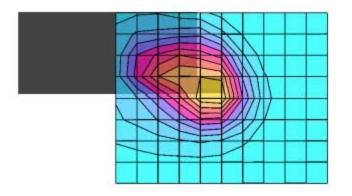


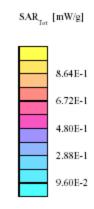
HisenceCommunication Co., Model: C389 (Body Worn, Face touching flat phantom with accessory (headset), High channel, Ambient Temp = 23 DegC, Liquid Temp = 22 Deg C, 6/11/2004)

SAM Phantom; Flat Section; Position: (90°,90°); Frequency: 848 MHz

Probe: ES3DV2 - SN3019; ConvF(6.10,6.10,6.10); Crest factor: 1.0; (Body) 835 MHz: $\sigma = 0.99 \text{ mho/m} \, \epsilon_r = 53.7 \, \rho = 1.00 \, \text{g/cm}^3$

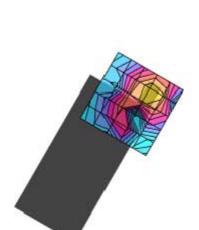
Cube 5x5x7: SAR (1g): 0.976 mW/g, SAR (10g): 0.604 mW/g, (Worst-case extrapolation) Coarse: Dx = 12.0, Dy = 12.0, Dz = 10.0

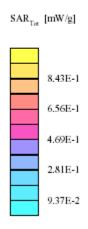




Hisence Comunication Co., Model: C389 (Left Head, Cheek, Low Channel, Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, 6/11/2004)

SAM Phantom; Left Hand Section; Position: $(90^{\circ},60^{\circ})$; Frequency: 825 MHz Probe: ET3DV2 - SN3019; ConvF(6.50,6.50,6.50); Crest factor: 1.0; Head Liquid 835 MHz: $\sigma = 0.92$ mho/m $\epsilon_r = 40.1$ $\rho = 1.00$ g/cm³ Cube 5x5x7: SAR (1g): 1.08 mW/g, SAR (10g): 0.604 mW/g, (Worst-case extrapolation) Coarse: Dx = 10.0, Dy = 10.0, Dz = 10.0 Powerdrift: -0.01 dB

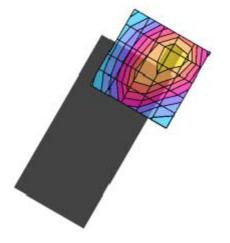


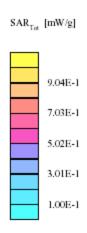


Hisence Comunication Co., Model: C389 (Left Head, Cheek, Mid Channel, Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, 6/11/2004)

SAM Phantom; Left Hand Section; Position: $(90^\circ,60^\circ)$; Frequency: $836\,\text{MHz}$ Probe: ET3DV2 - SN3019; ConvF(6.50,6.50); Crest factor: 1.0; Head Liquid 835 MHz: $\sigma = 0.92\,\text{mho/m}\,\alpha_z = 40.1\,\rho = 1.00\,\text{g/cm}^3$

Cube 5x5x7: SAR (1g): 1.16 $\,$ mW/g, SAR (10g): 0.736 $\,$ mW/g, (Worst-case extrapolation) Coarse: Dx = 10.0, Dy = 10.0, Dz = 10.0

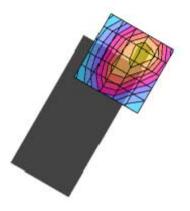


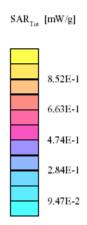


Hisence Comunication Co., Model: C389 (Left Head, Cheek, High Channel, Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, 6/11/2004)

SAM Phantom; Left Hand Section; Position: $(90^{\circ},60^{\circ})$; Frequency: 848 MHz Probe: ET3DV2 - SN3019; ConvF(6.50,6.50,6.50); Crest factor: 1.0; Head Liquid 835 MHz: $\sigma = 0.92$ mho/m $\epsilon_{\tau} = 40.1$ $\rho = 1.00$ g/cm³

Cubes (2): SAR (1g): 1.16 $\,$ mW/g \pm 0.00 dB, SAR (10g): 0.731 $\,$ mW/g \pm 0.01 dB, (Worst-case extrapolation) Coarse: Dx = 10.0, Dy = 10.0, Dz = 10.0





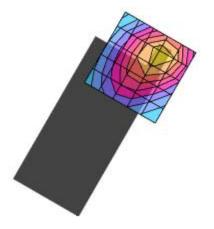
Hisence Comunication Co., Model: C389 (Left Head, Tilt, Low Channel, Ambient Temp = 23

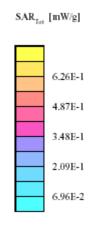
Deg C, Liquid Temp = 22 Deg C, 6/11/2004)

SAM Phantom; Left Hand Section; Position: (90°,60°); Frequency: 825 MHz

Probe: ET3DV2 - SN3019; ConvF(6.50,6.50,6.50); Crest factor: 1.0; Head Liquid 835 MHz: $\sigma = 0.92$ mho/m $\epsilon_r = 40.1$ $\rho = 1.00$ g/cm³

Cube 5x5x7: SAR (1g): 0.826 mW/g, SAR (10g): 0.519 mW/g, (Worst-case extrapolation) Coarse: Dx = 10.0, Dy = 10.0, Dz = 10.0



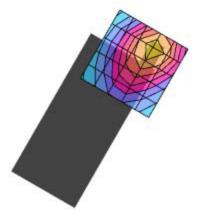


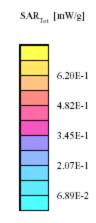
Hisence Comunication Co., Model: C389 (Left Head, Tilt, Mid Channel, Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, 6/11/2004)

SAM Phantom; Left Hand Section; Position: (90°,60°); Frequency: 836 MHz

Probe: ET3DV2 - SN3019; ConvF(6.50,6.50,6.50); Crest factor: 1.0; Head Liquid 835 MHz: σ = 0.92 mho/m s, = 40.1 ρ = 1.00 g/cm³

Cube 5x5x7: SAR (1g): 0.815 mW/g, SAR (10g): 0.500 mW/g, (Worst-case extrapolation)
Coarse: Dx = 10.0, Dy = 10.0, Dz = 10.0
Powerdrift: -0.01 dB

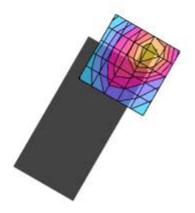


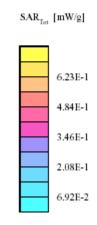


Hisence Comunication Co., Model: C389 (Left Head, Tilt, High Channel, Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, 6/11/2004)

SAM Phantom; Left Hand Section; Position: (90°,60°); Frequency: 848 MHz
Probe: ET3DV2 - SN3019; ConvF(6.50,6.50); Crest factor: 1.0; Head Liquid 835 MHz: $\sigma = 0.92$ mho/m $\epsilon_r = 40.1$ $\rho = 1.00$ g/cm³

Cube 5x5x7: SAR (1g): 0.747 mW/g, SAR (10g): 0.483 mW/g, (Worst-case extrapolation)
Coarse: Dx = 10.0, Dy = 10.0, Dz = 10.0
Powerdrift: 0.02 dB





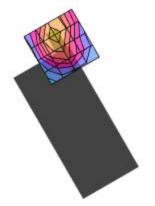
Hisence Communication Co., Model: C389 (Right Head, Cheek, Low Channel, Ambient

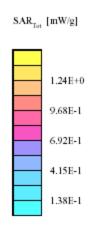
 $Temp = 23 \ Deg \ C, \ Liquid \ Temp = 22 \ Deg \ C, \ 6/11/2004)$ SAM Phantom; Righ Hand Section; Position: (90°,300°); Frequency: 825 MHz

Probe: ET3DV2 - SN3019; ConvF(6.50,6.50,6.50); Crest factor: 1.0; Head Liquid 835 MHz: $\sigma = 0.92 \text{ mho/m } \epsilon_r = 40.1 \text{ p} = 1.00 \text{ g/cm}^3$

Cube 5x5x7: SAR (1g): 1.28 mW/g, SAR (10g): 0.833 mW/g, (Worst-case extrapolation)

Coarse: Dx = 10.0, Dy = 10.0, Dz = 10.0



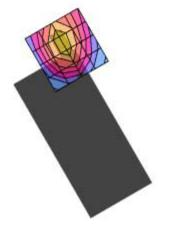


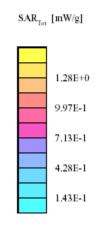
Hisence Communication Co., Model: C389 (Right Head, Cheek, Mid Channel, Ambient

 $\begin{array}{l} Temp=23\ Deg\ C,\ Liquid\ Temp=22\ Deg\ C,\ 6/11/2004)\\ sam\ Phantom;\ Righ\ Hand\ Section;\ Position:\ (90^\circ,300^\circ);\ Frequency:\ 836\ MHz \end{array}$

Probe: ET3DV2 - SN3019; ConvF(6.50,6.50,6.50); Crest factor: 1.0; Head Liquid 835 MHz: $\sigma = 0.92 \text{ mho/m s}_{*} = 40.1 \text{ p} = 1.00 \text{ g/cm}^{3}$

Cube 5x5x7: SAR (1g): 1.32 mW/g, SAR (10g): 0.879 mW/g, (Worst-case extrapolation)
Coarse: Dx = 10.0, Dy = 10.0, Dz = 10.0
Powerdrift: -0.04 dB





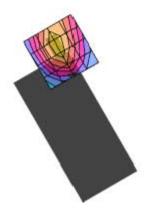
Hisence Communication Co., Model: C389 (Right Head, Cheek, High Channel, Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, 6/11/2004)

SAM Phantom; Righ Hand Section; Position: (90°,300°); Frequency: 848 MHz

Probe: ET3DV2 - SN3019; ConvF(6.50,6.50,6.50); Crest factor: 1.0; Head Liquid 835 MHz: $\sigma = 0.92 \text{ mho/m} \, \epsilon_r = 40.1 \, \rho = 1.00 \, \text{g/cm}^3$

Cube 5x5x7: SAR (1g): 1.10 mW/g, SAR (10g): 0.735 mW/g, (Worst-case extrapolation)

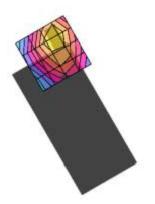
Coarse: Dx = 10.0, Dy = 10.0, Dz = 10.0





Hisence Communication Co., Model: C389 (Right Head, Tilt, Low Channel, Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, 6/11/2004)

SAM Phantom; Righ Hand Section; Position: $(90^\circ,300^\circ)$; Frequency: 825 MHz Probe: ET3DV2 - SN3019; ConvF(6.50,6.50,6.50); Crest factor: 1.0; Head Liquid 835 MHz: $\sigma=0.92$ mho/m $\epsilon_r=40.1$ $\rho=1.00$ g/cm³ Cube 5x5x7: SAR (1g): 0.778 mW/g, SAR (10g): 0.512 mW/g, (Worst-case extrapolation) Coarse: Dx = 10.0, Dy = 10.0, Dz = 10.0 Powerdrift: -0.01 dB





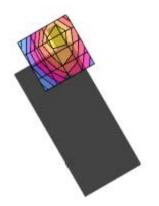
Hisence Communication Co., Model: C389 (Right Head, Tilt, Mid Channel, Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, 6/11/2004)

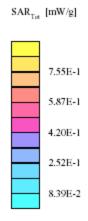
SAM Phantom; Righ Hand Section; Position: (90°,300°); Frequency: 836 MHz

Probe: ET3DV2 - SN3019; ConvF(6.50,6.50,6.50); Crest factor: 1.0; Head Liquid 835 MHz: $\sigma = 0.92 \text{ mho/m} \, \epsilon_{\tau} = 40.1 \, \rho = 1.00 \, \text{g/cm}^3$

Cube 5x5x7: SAR (1g): 0.781 mW/g, SAR (10g): 0.511 mW/g, (Worst-case extrapolation)

Coarse: Dx = 10.0, Dy = 10.0, Dz = 10.0





Hisence Communication Co., Model: C389 (Right Head, Tilt, High Channel, Ambient Temp = 23 Deg C, Liquid Temp = 22 Deg C, 6/11/2004)

SAM Phantom; Righ Hand Section; Position: (90°,300°); Frequency: 848 MHz

Probe: ET3DV2 - SN3019; ConvF(6.50,6.50,6.50); Crest factor: 1.0; Head Liquid 835 MHz: $\sigma = 0.92 \text{ mho/m} \, \epsilon_r = 40.1 \, \rho = 1.00 \, \text{g/cm}^3$

Cube 5x5x7: SAR (1g): 0.781 mW/g, SAR (10g): 0.516 mW/g, (Worst-case extrapolation) Coarse: Dx = 10.0, Dy = 10.0, Dz = 10.0

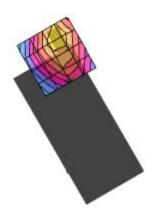


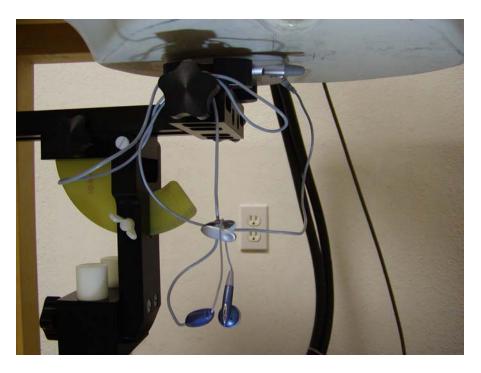


EXHIBIT A - SAR SETUP PHOTOGRAPHS

Back Side Touching Phantom



Face Touching Phantom



Left Cheek Touching Phantom



Left Cheek Tilted Touching Phantom



Right Cheek Touching Phantom



Right Cheek Tilted Touching Phantom

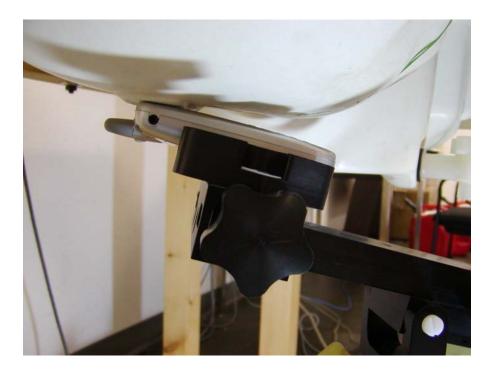


EXHIBIT B - EUT PHOTOGRAPHS

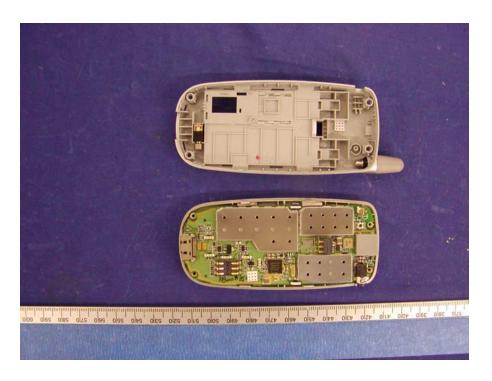
Chassis - Front View



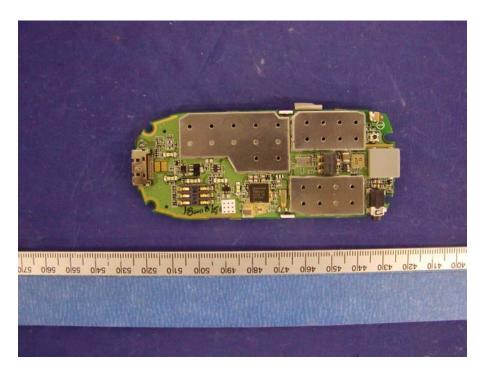
Chassis – Rear View



EUT - Cover off View



EUT - Component View



EUT – Shield Removed View



EUT - Solder View



AC Power Adapter

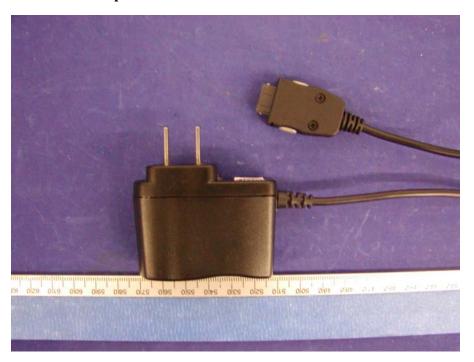


EXHIBIT C – Z-Axis

HisenceCommunication Co., Model: C389 (Body Worn, Back touching flat phantom with accessory (headset), Low Channel, Ambient Temp = 23 DegC, Liquid Temp = 22 Deg C,

SAM Phantom; Section; Position: ; Frequency: 825 MHz

Probe: ES3DV2 - SN3019; ConvF(6.10,6.10,6.10); Crest factor: 1.0; (Body) 835 MHz: $\sigma = 0.99$ mho/m $\epsilon_{\rm c} = 53.7$ $\rho = 1.31$ g/cm³

: , () Z-Axis: Dx = 0.0, Dy = 0.0, Dz = 2.0

