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## Specific Absorption Rate (SAR) Test Report

for

Wistron Corporation

on the

Notebook PC

**Model Number: Travel Mate C300** 

Test Report: EME-040039 Date of Report: Jan. 15, 2004 Date of test: Jan. 14, 2004

Total No of Pages Contained in this Report: 77



Accredited for testing to FCC Part 15

Tested by:  Kevin Chen	Levin Chi
Reviewed by: Elton Chen	At Chen

Review Date: <u>Jan. 15, 2004</u>

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#### STATEMENT OF COMPLIANCE

The Wistron sample device, model # Travel Mate C300 was evaluated in accordance with the requirements for compliance testing defined in FCC OET Bulletin 65, Supplement C (Edition 01-01). Testing was performed at the Intertek Testing Services facility in Hsinchu, Taiwan.

For the evaluation, the dosimetric assessment system INDEXSAR SARA2 was used. The phantom employed was the box phantom of 2mm thick in one wall. The total uncertainty for the evaluation of the spatial peak SAR values averaged over a cube of 1g tissue mass had been assessed for this system to be  $\pm 29.7\%$ .

The device was tested at their maximum output power declared by the Wistron.

In summary, the maximum spatial peak SAR value for the sample device averaged over 1g was found to be:

Phantom	Position	SAR <sub>1g</sub> , mW/g
2mm thick box phantom	EUT top to the phantom,	0.066 mW/g.
wall	0 mm separation.	0.000 mw/g.

In conclusion, the tested Sample device was found to be in compliance with the requirements defined in OET Bulletin 65, Supplement C (Edition 01-01) for body configurations.



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## 1.0 Job Description

#### 1.1 Client Information

The Travel Mate C300 has been tested at the request of:

**Company:** Wistron Corporation

No. 10-1, Li-hsin Road I, Science-based Industrial Park

Hsinchu 300, Taiwan

#### 1.2 Equipment under test (EUT)

#### **Product Descriptions:**

Equipment	Notebook PC		
Trade Name	Wistron	Model No:	Travel Mate C300
FCC ID	PU5MS2140BG	S/N No.	Not Labeled
Category	Portable	RF Exposure	Uncontrolled Environment
<b>Frequency Band</b>	2412 – 2462 MHz	System	DSSS, OFDM

EUT Antenna Description						
Type PIFA Configuration Fixed						
Dimensions	42 x 7 mm	Gain	2.42 dBi			
Location	<b>Location</b> Embedded					

**Use of Product:** Wireless Data Communication

**Manufacturer:** Wistron

**Production is planned:** [X] Yes, [] No

**EUT receive date:** Jan. 13, 2004

**EUT received condition:** Good operating condition prototype

Test start date: Jan. 14, 2004

**Test end date:** Jan. 14, 2004



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## 1.3 Test plan reference

FCC Rule: Part 2.1093, FCC's OET Bulletin 65, Supplement C (Edition 01-01) and IEEE 1528/D1.2

## 1.4 System test configuration

## 1.4.1 System block diagram & Support equipment

Support Equipment						
Item #	Item #   Equipment   Brand   Model No.   S/N					
1	1 N/A N/A N/A N/A					





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#### 1.4.2 Test Position

See the photographs as section 2.2

#### 1.4.3 Test Condition

During tests the worst-case data (max RF coupling) was determined with following conditions:

Usage	Operates with a portable computer	Distance between antenna axis at the joint and the liquid surface:	top position, seg 15mm, in right	ng the Phantom in parating 0mm and and rear position, mm and 15mm
Simulating human Head/ Body/Hand	Body	EUT Battery	Device is powered from host computer through battery.	
802.11b	Channel	Frequency MHz	Before SAR Test (dBm)	After SAR Test (dBm)
Conducted	Low Channel - 1	2412	15.91	-
output Power	Mid Channel - 6	2437	15.54	-
	High Channel- 11	2462	15.67	-
802.11g	Channel	Frequency MHz	Before SAR Test (dBm)	After SAR Test (dBm)
Conducted	Low Channel - 1	2412	16.97	-
output Power	Mid Channel - 6	2437	16.75	16.71
	High Channel- 11	2462	16.58	-

The spatial peak SAR values were assessed for lowest, middle and highest operating channels, defined by the manufacturer.

The conducted output power was measured before and after the test using a diode detector, oscilloscope and signal generator.

Run the test program "CRTU-II" under Windows OS. The EUT was transmitted continuously during the test.

The EUT has two modules, which are WLAN and Bluetooth. The two modules transmitted at the same time during the test. For the WLAN module, it contains 802.11b and 802.11g functions, due to the worst case output power was found in 802.11g function, we only performed the 802.11g for SAR testing.

After verifying the maximum output power, we found the maximum output power was occurred at 6Mbps data rate.

All the test data were performed under the above transmission rate.



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## 1.5 Modifications required for compliance

Intertek Testing Services implemented no modifications.

## 1.6 Additions, deviations and exclusions from standards

The phantom employed was the box phantom of 2mm thick in vertical wall.



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#### 2.0 SAR Evaluation

#### 2.1 SAR Limits

The following FCC limits for SAR apply to devices operate in General Population/Uncontrolled Exposure environment:

EXPOSURE	SAR
(General Population/Uncontrolled Exposure environment)	(W/kg)
Average over the whole body	0.08
Spatial Peak (1g)	1.60
Spatial Peak for hands, wrists, feet and ankles (10g)	4.00



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## 2.2 Configuration Photographs

## **SAR Measurement Test Setup**

## **Test System**





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# SAR Measurement Test Setup EUT top to phantom, 0 mm separation



EUT top to phantom, 0 mm separation- Zoom In





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# SAR Measurement Test Setup EUT top to phantom, 15 mm separation



EUT top to phantom, 15 mm separation - Zoom In





FCC ID: PU5MS2140BG

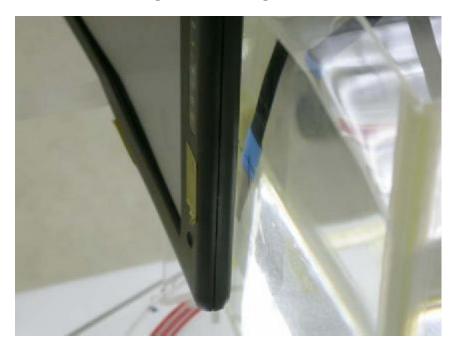
Report No.: EME-040039

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## SAR Measurement Test Setup EUT rear to phantom, 0 mm separation



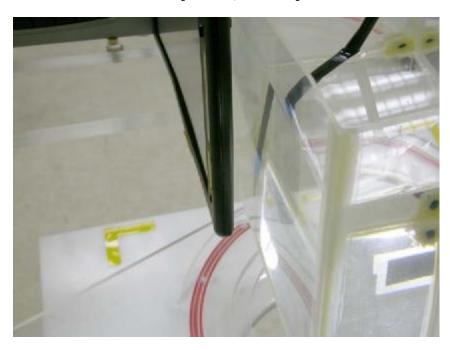
EUT rear to phantom, 0 mm separation-Zoom In



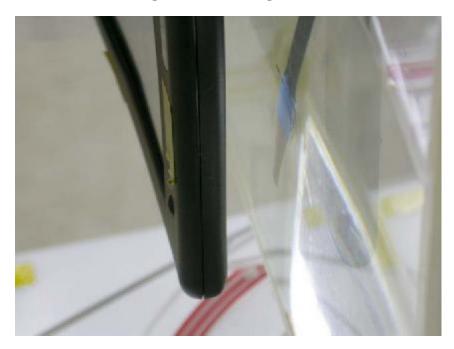


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## SAR Measurement Test Setup EUT rear to phantom, 15 mm separation



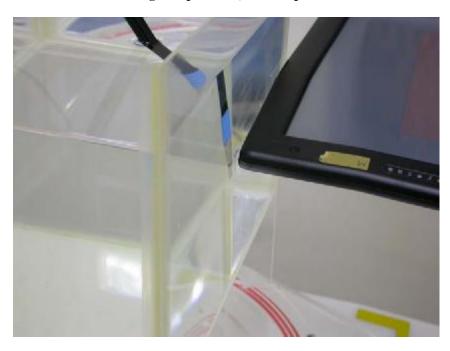
EUT rear to phantom, 15 mm separation- Zoom In



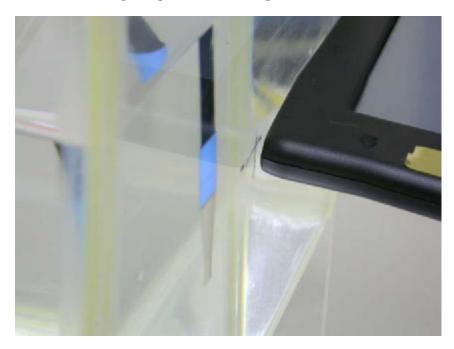


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## SAR Measurement Test Setup EUT right to phantom, 0 mm separation



EUT right to phantom, 0 mm separation-Zoom In



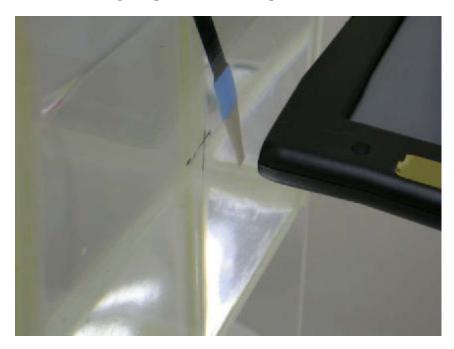


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SAR Measurement Test Setup EUT right to phantom, 15 mm separation



EUT right to phantom, 15 mm separation– Zoom In





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#### 2.3 SAR measurement system

Robot system specification

The SAR measurement system being used is the IndexSAR SARA2 system, which consists of a Mitsubishi RV-E2 6-axis robot arm and controller, IndexSAR probe and amplifier and SAM phantom Head Shape. The robot is used to articulate the probe to programmed positions inside the phantom head to obtain the SAR readings from the DUT.

The system is controlled remotely from a PC, which contains the software to control the robot and data acquisition equipment. The software also displays the data obtained from test scans.

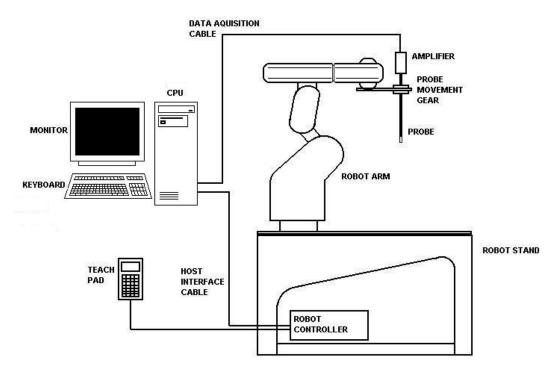


Figure 1: Schematic diagram of the SAR measurement system

The position and digitised shape of the phantom heads are made available to the software for accurate positioning of the probe and reduction of set-up time.

The SAM phantom heads are individually digitised using a mitutoyo CMM machine to a precision of 0.02mm. The data is then converted into a shape format for the software, providing an accurate description of the phantom shell. In operation, the system first does an area (2D) scan at a fixed depth within the liquid from the inside wall of the phantom. When the maximum SAR point has been found, the system will then carry out a 3D scan centred at that point to determine volume averaged SAR level.

The first 2 measurements points in a direction perpendicular to the surface of the phantom during the zoom scan and closest to the phantom surface, were only 3.5mm and the probe is kept at greater than half a diameter from the surface.



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#### 2.4 SAR measurement system validation

Prior to the assessment, the system was verified to the  $\pm 10\%$  of the specifications by using the system validation equipments. The validation was performed at 2450 MHz on the bottom side of box phantom.

#### **Procedures**

The SAR evaluation was performed with the following procedures:

- a. The SAR distribution was measured at the exposed side of the bottom of the box phantom and was measured at a distance of 8 mm from the inner surface of the shell. The feed power was 1/5W.
- b. The dimension for this cube is 32 mm x 32 mm x 34 mm was assessed by measuring 5 x 5 x 7 points. On the basis of this data set, the spatial peak SAR value was evaluated with the following procedure:
  - i) The data at the surface were extrapolated, since the center of the dipoles is 2.7 mm away from the tip of the probe and the distance between the surface and the lowest measurement point is 5 mm. The extrapolation was based on a least square algorithm. A polynomial of the fourth order was calculated through the points in Z-axes. This polynomial was then used to evaluate the points between the surface and the probe tip.
  - ii) The maximum interpolated value was searched with a straightforward algorithm. Around this maximum, the SAR values averaged over the spatial volumes (1g or 10g) were computed using the 3-D spline interpolation algorithm. The 3-D spline is composed of three one-dimensional splines with the "Not a knot" condition (in x, y and z directions). The volume was integrated with the trapezoidal algorithm. 1000 points (10 x 10 x 10) were interpolated to calculate the average.
  - iii) All neighboring volumes were evaluated until no neighboring volume with a higher average value was found.

The test scan procedure for system validation also apply to the general scan procedure except for the set-up position. For general scan, the EUT was placed at the side of phantom. For validation scan, the dipole antenna was placed at the bottom of phantom

#### 2.4.1 System Validation result

	System Validation (2450 MHz Head)				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					
2450	CW	52.4	54.688	4.37%	

Please see the plot below:



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Date:2003/10/15Position:BottomFilename:2450val10-15.txtPhantom:Box1.csvDevice Tested:SARA2 systemHead Rotation:0

Antenna: 2450dipole Test Frequency: 2450MHz
Shape File: none.csv Power Level: 24dBm/CW

.453

**Probe:** 0136

Cal File: SN0136\_2450\_CW\_HEAD

Lin

 Air
 490
 405
 405

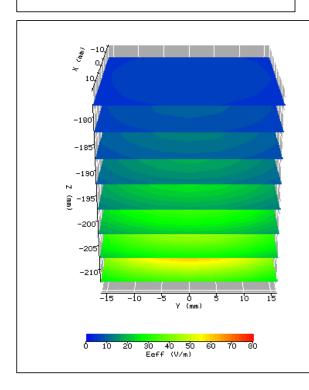
 DCP
 20
 20
 20

.453

.453

Amp Gain: 2
Averaging: 1
Batteries
Replaced:

15.5cm Liquid: 2450MHz Head Type: 1.80379 **Conductivity: Relative Permittivity:** 38.1223 23.3 Liquid Temp (deg C): 24 Ambient Temp (deg C): 50 Ambient RH (%): Density (kg/m3): 1000 **Software Version:** 0.421N



#### **ZOOM SCAN RESULTS:**

Spot SAR (W/kg): 0.896 0.889

Change during Scan (%)

Max E-field 74.25

(V/m): 74.2

` \_ \_\_\_\_ . [

Max SAR (W/kg)	1g	TUg
Wax SAK (W/Kg)	13.672	6.405

 Location of Max (mm):
 X
 Y
 Z

 -1.3
 0.0
 -220.7

Normalized to an input power of 1W Averaged over 1 cm<sup>3</sup> (1g) of tissue **54.688W/kg** 



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## 2.4.2 System Performance Check result

System performance check (2450 MHz Head)				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				
2450	CW	52.4	52.32	-0.15%

Please see the plot below:



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**Date:** 2004/1/14 **Position:** Bottom of box phantom

Filename: 2450 performance check Phantom: HeadBox1-val..csv

Device Tested:2450 performance checkHead Rotation:0Antenna:2450 dipoleTest Frequency:2450MhzShape File:none.csvPower Level:23dBm

**Probe:** 0136 **Liquid:** 15.5cm

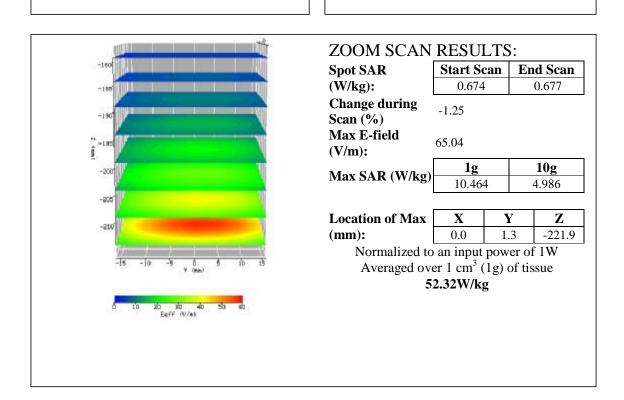
**Cal Factors:** 

Replaced:

Cal File: SN0136\_2450\_CW\_HEAD Type: 2450MHz Head

1.85153 **Conductivity:** X Y  $\mathbf{Z}$ 38.59285 **Relative Permittivity:** 490 405 405 Air **Liquid Temp (deg C):** 22.4 **DCP** 20 20 20 Ambient Temp (deg C): 23 .378 .378 .378 Lin 47 Ambient RH (%):

Amp Gain:2Ambient RH (%):47Averaging:1Density (kg/m3):1000BatteriesSoftware Version:2.1 VPM





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#### 2.5 Test Result

The results on the following page(s) were obtained when the device was tested in the condition described in this report. Detailed measurement data and plots, which reveal information about the location of the maximum SAR with respect to the device, are reported in Appendix A.

#### **Measurement Results**

Trade Name:	Wistron		Model No.:	Travel Mate	C300
Serial No.:	Not Labled		Test Engineer: Kevin Chen		
	TEST CONDITIONS				
<b>Ambient Temp</b>	erature	23 °C	Relative Humidity 50 %		50 %
Test Signal Sou	irce	Test Mode	Signal Modulation OFDM		OFDM
<b>Output Power</b>	Before	See page 6	Output Power Af	fter SAR	See page 6
SAR Test			Test		
<b>Test Duration</b>		22 min. each scan	<b>Number of Batte</b>	ry Change	1

	EUT Position										
Channel (MHz)	Operating Mode	Crest Factor	Description	Distance (mm)	Measured SAR <sub>1g</sub> (mW/g)	Plot Number					
2437	OFDM	1	Top to phantom	0	0.066	1					
2437	OFDM	1	Top to phantom	0	0.050	2					
2437	OFDM	1	Top to phantom	15	0.020	3					
2437	OFDM	1	Top to phantom	15	0.014	4					
2437	OFDM	1	Rear to phantom	0	0.126	5					
2437	OFDM	1	Rear to phantom	15	0.020	6					
2437	OFDM	1	Right to phantom	0	0.053	7					
2437	OFDM	1	Right to phantom	15	Note 1	8					

Note: 1. The measurement was only performed in Area Scan due to scanning system couldn't continue performing Zoom Scan with such a low SAR distribution.

2. Configuration at middle channel with more than –3dB of applicable limit.



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## 3.0 Test Equipment

## 3.1 Equipment List

The Specific Absorption Rate (SAR) tests were performed with the INDEXSAR SARA2 SYSTEM.

The following major equipment/components were used for the SAR evaluations:

	SAR Measurement System						
EQUIPMENT	SPECIFICATIONS	S/N #	LAST CAL. DATE				
Balanced Validation dipole	2450MHz	0048	03/26/2003				
Controller	Mitsubishi CR-E116	F1008007	N/A				
Robot	Mitsubishi RV-E2	EA009002	N/A				
	Repeatability: ± 0.04mm; Number of Axes: 6						
E-Field Probe	IXP-050	0136	09/10/2003				
	Frequency Range: Probe outer diameter: 5.2 mm; probe tip and the dipole center: 2.7 mm	Length: 350 mm;	Distance between the				
Data Acquisition	SARA2	N/A	N/A				
	Processor: Pentium 4; Clock speed: 1.5GHz; OS: Win Software: SARA2 ver. 2.0VPM	ndows XP; I/O: two	RS232;				
Phantom	2mm wall thickness box phantom	N/A	N/A				
	Shell Material: clear Perspex; Thickness: $2 \pm 0.1$ mm D) mm <sup>3</sup> ; Dielectric constant: less than 2.85 above 500		215.5 x 200 (W x L x				
Device holder	vice holder  Material: clear Perspex; Dielectric constant: less than 2.85 above 500MHz		N/A				
Simulated Tissue	Mixture	N/A	01/14/2004				
	Please see section 3.2 for details						
RF Power Meter	Boonton 4231A with 51011-EMC power sensor	79401-32482	03/21/2003				
	Frequency Range: 0.03 to 8 GHz, <24dBm						
RF Power Amplifier	INDEXSAR VTL5400	0302	01/23/2003				
	10MHz to 2.5GHz, Gain >30dB						
<b>Directional Coupler</b>	INDEXSAR VDC0830-20	0302	05/19/2003				
	0.8 to 3 GHz, Max. Power<500W						
Vector Network Analyzer	HP 8753B HP 85046A	2807J04037 2729A01958	07/04/2003				
	300k to 3GHz						
Signal Generator	R&S SMR27	100036	09/19/2003				
	10M to 27GHz, <120dBuV						
Crystal Detector	Agilent 8472B	MY42240243	N/A				
	10MHz to 18GHz						
Two Channel Digital Storage Oscilloscope	Tektronix TDS1012	C031679	08/16/2003				



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## 3.2 Tissue Simulating Liquid

#### 3.2.1 Body Tissue Simulating Liquid for evaluation test

Body Ingredients Frequency (2.45 GHz)							
DGBE (Dilethylene Glycol Butyl Ether)	26.7%						
Salt	0.04%						
Water	73.2%						

The dielectric parameters were verified prior to assessment using the HP 85046A dielectric probe kit and the HP 8753B network Analyzer. The dielectric parameters were:

Frequency (MHz)	Temp. (°C)	e r/ Relat	ve Permittivity		s / Condu	r *(kg/m <sup>3</sup> )		
2450	22.8	measured	target	Δ(±5%)	measured	target	Δ(±5%)	1000
2430	22.0	50.86	52.7	-3.49%	1.94	1.95	-0.51%	1000

<sup>\*</sup> Worst-case assumption

#### 3.2.2 Head Tissue Simulating Liquid for System performance Check test

Head Ingredients Frequency (2.45 GHz)							
DGBE (Dilethylene Glycol Butyl Ether) 53.3%							
Water	46.7%						

The dielectric parameters were verified prior to assessment using the HP 85046A dielectric probe kit and the HP 8753B network Analyzer. The dielectric parameters were:

Frequency (MHz)	Temp. (°C)	e <sub>r</sub> / <b>Relati</b>	ive Pern	nittivity	s / Condu	r *(kg/m³)		
2450	23.4	measured	target	$\Delta(\pm 5\%)$	measured	target	$\Delta(\pm 5\%)$	1000
2430	23.4	38.59	39.2	-1.56%	1.85	1.80	2.78	1000

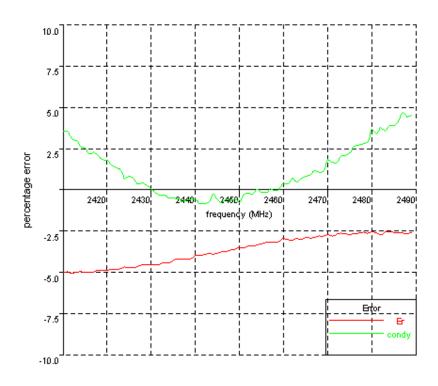
<sup>\*</sup> Worst-case assumption



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## 3.2.3 Body Liquid results

Date: 14 Jan. 2004	Temperature: 22.8°℃	Type: 2450MHz/body (FCC)	Tested by: Kevin
2410, 50.1159978554, -1.979595 2411, 50.1339191461, -1.980395 2412, 50.0949743513, -1.972910 2413, 50.1086258676, -1.971449 2414, 50.1394033587, -1.966113 2415, 50.1006186581, -1.964751 2416, 50.1142717126, -1.959073 2417, 50.1244031229, -1.962241 2418, 50.1772904504, -1.959146 2419, 50.1521541557, -1.955424 2420, 50.1703078222, -1.955684 2421, 50.2052738201, -1.951295 2422, 50.1843919119, -1.949465 2423, 50.2120975727, -1.947566 2424, 50.268192058, -1.9379761 2425, 50.2387798675, -1.932507 2426, 50.240611071, -1.9392467 2427, 50.2875110794, -1.934593 2428, 50.3388895796, -1.937383 2428, 50.3384808, -1.93821 2431, 50.328548803, -1.928175 2432, 50.356884702, -1.9267385 2433, 50.3934238784, -1.928147 2434, 50.369844054412, -1.9267385 2435, 50.4694844474, -1.925912 2436, 50.5063944412, -1.926652 2437, 50.5051057504, -1.923836 2438, 50.4999265089, -1.926507 2439, 50.525228001, -1.928911 2440, 50.6140934398, -1.927902 2441, 50.6153848382, -1.925106 2442, 50.6414825583, -1.928131 2444, 50.6595283026, -1.938133 2444, 50.6595283026, -1.938522 2445, 50.7344065674, -1.935809 2448, 50.7780035811, -1.935458	5:5264 5:2794 5:514 5:514 5:562 6:6148 6:4361 6:476 6:3072 5:5986 6:6866 6:1317 7:7825 6:8248 363 22596 2275 6:5646 3:3156 3:3944 0335 2:346 6:162 3:3944 0335 2:347 2:1153 2:1153 2:1153 2:1153 2:11602 2:2061 3:688 6:6786 6:17664 6:178 6:8835 8:8835 8:8247 8:719 1:2909	2450, 50.8582059951, -1.9353586827 2451, 50.8461944441, -1.9464119358 2452, 50.9022552645, -1.9487372676 2453, 50.8931394208, -1.9493662055 2454, 50.9402957382, -1.9564520074 2455, 50.9609265579, -1.9537441388 2456, 51.0128370336, -1.9551153561 2457, 51.0240716837, -1.9609776868 2458, 51.013833992, -1.9645281819 2460, 51.1351088475, -1.97157133 2461, 51.0935239542, -1.9726124251 2462, 51.094829542, -1.9726124251 2463, 51.1308874451, -1.9780824386 2464, 51.0935239542, -1.9726124251 2465, 51.1620671144, -1.987050944 2466, 51.1419057078, -1.9903169721 2467, 51.1481194494, -1.9970685422 2468, 51.2032067238, -1.9966782358 2470, 51.2555119728, -2.0145709638 2471, 51.1944021371, -2.0130301387 2472, 51.248978851, -2.0134288233 2473, 51.2866271604, -2.0231131979 2474, 51.2682853294, -2.0255744971 2475, 51.2365540517, -2.0300697945 2476, 51.2717025035, -2.0392325481 2477, 51.2817314477, -2.0425099052 2478, 51.3176040061, -2.0453388792 2479, 51.2771405891, -2.0489266 2480, 51.3180239613, -2.0656679909 2481, 51.2815942729, -2.06195339327 2482, 51.2268803058, -2.0758650316 2485, 51.2960274444, -2.084605512 2487, 51.2690223103, -2.0966286731 2488, 51.2609245953, -2.0928336883 2489, 51.2609245953, -2.0928336883	Tested by: Kevin
		2490, 51.2558088639, -2.1084921546	

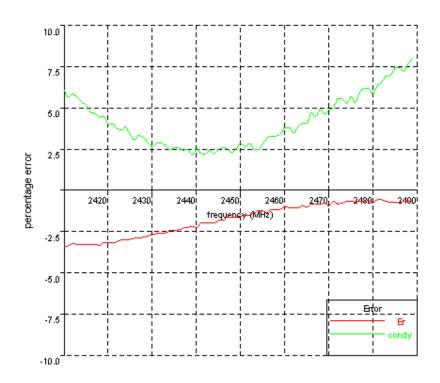




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## 3.2.4 Head Liquid results

Date: 14 Jan. 2004	Temperature: 23.4°℃	Type: 2450MHz/head (FCC)	Tested by: Kevin
2410, 37.9258334406, -1.87159; 2411, 37.9566252163, -1.86485; 2412, 37.9942737628, -1.86934; 2413, 37.9746868959, -1.86607; 2414, 37.9756558049, -1.863236; 2415, 37.9616593164, -1.860119; 2416, 37.9760647893, -1.85349; 2417, 37.9783253781, -1.85339; 2418, 37.934577754, -1.8502349; 2419, 38.0161422124, -1.85161; 2420, 38.0071636647, -1.844429; 2421, 38.0127513905, -1.84523; 2422, 38.0249120925, -1.841487; 2423, 38.0658654802, -1.841489; 2424, 38.0658654802, -1.84139; 2424, 38.0658654802, -1.84139; 2424, 38.0658654802, -1.84139; 2424, 38.0658654802, -1.84139; 2425, 38.0822537754, -1.836959; 2426, 38.1047781166, -1.833515; 2427, 38.1065837267, -1.838959; 2428, 38.1234064406, -1.837642; 2429, 38.1055837267, -1.838959; 2428, 38.1234064406, -1.833512; 2429, 38.1612204147, -1.832501; 2430, 38.192620936, -1.829424; 2431, 38.2044214104, -1.834112; 2432, 38.2728854891, -1.82993; 2435, 38.2634278939, -1.832857; 2436, 38.2845522617, -1.833400; 2447, 38.3259249511, -1.832142; 2438, 38.327644317, -1.837018; 2441, 38.434932008, -1.83263; 2442, 38.4386426484, -1.83295; 2440, 38.327644317, -1.837018; 2441, 38.4340989953, -1.83263; 2442, 38.4386426484, -1.83245; 2443, 38.4461613962, -1.837636; 2444, 38.4956776338, -1.83466; 2447, 38.57277770307, -1.84316; 2448, 38.5622614241, -1.83486; 2447, 38.5623718316, -1.844846; 2449, 38.5633718316,	5205 59389 64705 66211 55743 77069 13535 77257 1813 141692 14089 12376 1795 7046 18871 14285 7795 7046 188871 14285 17958 122506 3861 125506 3861 12589 129173 12464 129928 17061 106398 106016 13523 177571 17171 17571 1771 1771 1771 1771 1771 1771 1771 1771 1771 1771 1771 1771 1771 1771 1775 18132 14765 18528 186315 12336 13826 199317	2450, 38.5928524229, -1.8515391638 2451, 38.6009297006, -1.8480749134 2452, 38.6066047206, -1.8534319533 2453, 38.6644071537, -1.8481584642 2454, 38.7171685605, -1.8489321099 2455, 38.7038862141, -1.8569136142 2456, 38.6665569586, -1.863695346 2457, 38.7373085023, -1.8673846661 2458, 38.7216198924, -1.8684397741 2459, 38.7348544821, -1.8710334891 2460, 38.7941677517, -1.8800095671 2461, 38.7941677517, -1.880095671 2461, 38.7941677517, -1.880337501 2462, 38.76072727656, -1.8837323173 2464, 38.8231108003, -1.8892371634 2465, 38.780699656, -1.8902128651 2466, 38.8487809872, -1.9030549293 2467, 38.8512352089, -1.8998825672 2468, 38.8450988284, -1.9094375914 2469, 38.8738901015, -1.9052816735 2470, 38.8075265016, -1.9103040523 2471, 38.914193515, -1.9148527816 2472, 38.8546234171, -1.9250063069 2473, 38.8611856194, -1.9264011112 2474, 38.9089202117, -1.9228251833 2475, 38.9177926083, -1.9309618406 2476, 38.8934501924, -1.9255540585 2477, 38.9120855867, -1.9382818036 2478, 38.8938930238, -1.9446740257 2480, 38.8685800653, -1.9394834023 2481, 38.9368930238, -1.9446740257 2480, 38.8685800653, -1.9394834023 2481, 38.9361991721, -1.9549975276 2483, 38.8975399437, -1.9650380462 2485, 38.8783407137, -1.9650380462 2485, 38.8783407137, -1.9650380462 2485, 38.8783407137, -1.9650380462 2485, 38.8783407137, -1.9650380462 2487, 38.8964631827, -1.975086443 2486, 38.8975399437, -1.9650380462 2487, 38.8964631827, -1.975086443 2488, 38.9011891029, -1.9830312102 2489, 38.912606808, -1.9901837177 2490, 38.8724337747, -1.9847502555	





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## 3.3 E-Field Probe and 2450 Balanced Dipole Antenna Calibration

Probe calibration factors and dipole antenna calibration are included in Appendix C.



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## 4.0 Measurement Uncertainty

The uncertainty budget has been determined for the INDEXSAR SARA2 measurement system according to IEEE P1528 documents [3] and is given in the following table. The extended uncertainty (95% confidence level) was assessed to be 29.7 %

Table 1 Exposure Assessment Uncertainty

## Example of measurement uncertainty assessment SAR measurement

(blue entries are site-specific)

(blue entries are site-specific)											
а	b			С	d	е		f	g	h	1
Uncertainty Component	Sec.	T	ol. (+/-	)	Prob. Dist.	Divisor (descrip)			c1 (10g)	Standard Uncertainty (%) 1g	Standard Uncertainty (%) 10g
		(dB)		(%)							
Measurement System											
Probe Calibration	E2.1			2.5	Ν	1 or k	1	1	1	2.50	2.50
Axial Isotropy	E2.2	0.25	5.93	5.93	R	√3	1.73	0	0	0.00	0.00
Hemispherical Isotropy	E2.2	0.45	10.92	10.92	R	√3	1.73	1	1	6.30	6.30
Boundary effect	E2.3		4	4.00	R	√3	1.73	1	1	2.31	2.31
Linearity	E2.4	0.04	0.93	0.93	R	√3	1.73	1	1	0.53	0.53
System Detection Limits	E2.5		1	1.00	R	√3	1.73	1	1	0.58	0.58
Readout Electronics	E2.6		1	1.00	Ν	1 or k	1.00	1	1	1.00	1.00
Response time	E2.7		0	0.00	R	√3	1.73	1	1	0.00	0.00
Integration time	E2.8		1.4	1.40	R	√3	1.73	1	1	0.81	0.81
RF Ambient Conditions	E6.1		3	3.00	R	√3	1.73	1	1	1.73	1.73
Probe Positioner Mechanical Tolerance	E6.2		0.6	0.60	R	√3	1.73	1	1	0.35	0.35
Probe Position wrt. Phantom Shell	E6.3		3	3.00	R	√3	1.73	1	1	1.73	1.73
SAR Evaluation Algorithms	E5		8	8.00	R	√3	1.73	1	1	4.62	4.62
Test Sample Related											
Test Sample Positioning	E4.2		2	2.00	Z	1	1.00	1	1	2.00	2.00
Device Holder Uncertainty	E4.1		2	2.00	Ν	1	1.00	1	1	2.00	2.00
Output Power Variation	6.6.2		5	5.00	R	√3	1.73	1	1	2.89	2.89
Phantom and Tissue Parameters											
Phantom Uncertainty (shape and thickness)	E3.1		4	4.00	R	√3	1.73	1	1	2.31	2.31
Liquid conductivity (Deviation from target)	E3.2		5	5.00	R	√3	1.73	0.64	0.43	1.85	1.24
Liquid conductivity (measurement uncert.)	E3.3		1.1	1.10	Ν	1	1.00	0.64	0.43	0.70	0.47
Liquid permittivity (Deviation from target)	E3.2		5	5.00	R	√3	1.73	0.6	0.49	1.73	1.41
Liquid permittivity (measurement uncert.)	E3.3		1.1	1.10	N	1	1.00	0.6	0.49	0.66	0.54
Combined standard uncertainty					RSS					10.5	10.3
Expanded uncertainty	(95% Confidence Level)				k=2					20.6	20.3



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Table 2 System Check (Verification)

## Example of measurement uncertainty assessment for system performance check

(blue entries are site-specific)

(blue entries are site-specific)	T						•				
а	b			С	d	е		f	g	h	1
Uncertainty Component	Sec.		Tol. (+/	<b>/-</b> )	Prob. Dist.	Divisor (descrip)	Divisor (value)	c1 (1g)	c1 (10g)	Standard Uncertainty (%) 1g	Standard Uncertainty (%) 10g
		(dB)		(%)							
Measurement System											
Probe Calibration	E2.1			2.5	N	1 or k	1	1	1	2.50	2.50
Axial Isotropy	E2.2	0.25	5.93	5.93	R	√3	1.73	0	0	0.00	0.00
Hemispherical Isotropy	E2.2	0.45	10.92	10.92	R	√3	1.73	1	1	6.30	6.30
Boundary effect	E2.3		4	4.00	R	√3	1.73	1	1	2.31	2.31
Linearity	E2.4	0.04	0.93	0.93	R	√3	1.73	1	1	0.53	0.53
System Detection Limits	E2.5		1	1.00	R	√3	1.73	1	1	0.58	0.58
Readout Electronics	E2.6		1	1.00	N	1 or k	1.00	1	1	1.00	1.00
Response time	E2.7		0	0.00	R	√3	1.73	1	1	0.00	0.00
Integration time	E2.8		1.4	1.40	R	√3	1.73	1	1	0.81	0.81
RF Ambient Conditions	E6.1		3	3.00	R	√3	1.73	1	1	1.73	1.73
Probe Positioner Mechanical Tolerance	E6.2		0.6	0.60	R	√3	1.73	1	1	0.35	0.35
Probe Position wrt. Phantom Shell	E6.3		3	3.00	R	√3	1.73	1	1	1.73	1.73
SAR Evaluation Algorithms	E5		8	8.00	R	√3	1.73	1	1	4.62	4.62
Dipole											
Dipole axis to liquid distance	8, E4.2		2	2.00	N	1	1.00	1	1	2.00	2.00
Input power and SAR drift measurement	8, 6.6.2		5	5.00	R	√3	1.73	1	1	2.89	2.89
Phantom and Tissue Parameters											
Phantom Uncertainty (thickness)	E3.1		4	4.00	R	√3	1.73	1	1	2.31	2.31
Liquid conductivity (Deviation from target)	E3.2		5	5.00	R	√3	1.73	0.64	0.43	1.85	1.24
Liquid conductivity (measurement uncert.)	E3.3		1.1	1.10	N	1	1.00	0.64	0.43	0.70	0.47
Liquid permittivity (Deviation from target)	E3.2		5	5.00	R	√3	1.73	0.6	0.49	1.73	1.41
Liquid permittivity (measurement uncert.)	E3.3		1.1	1.10	N	1	1.00	0.6	0.49	0.66	0.54
Combined standard uncertainty					RSS					10.3	10.1
Expanded uncertainty	(95% Confidence Level)				k=2					20.2	19.9

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Table 3 Uncertainty assessment for waveguide probe calibration

	а		b		С	
Uncertainty Component	Tol. (+/-%)	Prob. Dist.	Divisor (descrip)	Divisor (value)	c1	Standard Uncertainty (+/- %)
Waveguide calibrations						
Incident or forward power	1	R	√3	1.73	1	0.58
Refected power	1.00	R	√3	1.73	1	0.58
Liquid conductivity	2.00	R	$\sqrt{3}$	1.73	1	1.15
Liquid permittivity	2.00	R	$\sqrt{3}$	1.73	1	1.15
Probe positioning	1.00	N	1	1.00	1	1.00
Field homogeneity	1.00	R	$\sqrt{3}$	1.73	1	0.58
Field probe positioning	2.00	R	$\sqrt{3}$	1.73	1	1.15
Field probe linearity	1.00	R	$\sqrt{3}$	1.73	1	0.58
Combined standard uncertainty		RSS				2.5
Expanded uncertainty		k=2				4.9

Table 4 Uncertainty assessment for DiLine dielectric property measurement

	а		b		С	
		Prob.	Divisor	Divisor		Standard
Uncertainty Component	Tol. (+/- %)	Dist.	(descrip)	(value)	c1	Uncertainty (+/- %)
Permittivity measurement						
Repeatability (n repeats)	1	N	1 or k	1	1	1.00
Temperature measurement	0.30	R	$\sqrt{3}$	1.73	1	0.17
VNA drift, linearity	0.50	R	$\sqrt{3}$	1.73	1	0.29
Test port cable variations	0.50	R	√3	1.73	1	0.29
Combined standard uncertainty		RSS				1.1
Expanded uncertainty		k=2				2.1

	а		b		С	
		Prob.	Divisor	Divisor		Standard
Uncertainty Component	Tol. (+/- %)	Dist.	(descrip)	(value)	c1	Uncertainty (+/- %)
Conductivity measurement						
Repeatability (n repeats)	1	Z	1 or k	1	1	1.00
Temperature measurement	0.30	R	$\sqrt{3}$	1.73	1	0.17
VNA drift, linearity	0.50	R	√3	1.73	1	0.29
Test port cable variations	0.50	R	$\sqrt{3}$	1.73	1	0.29
Combined standard uncertainty		RSS				1.1
Expanded uncertainty		k=2				2.1



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## **5.0 Measurement Traceability**

All measurements described in this report are traceable to Chinese National Laboratory Accreditation (CNLA) standards or appropriate national standards.



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## 6.0 WARNING LABEL INFORMATION - USA

See user manual.



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#### 7.0 REFERENCES

- [1] ANSI, ANSI/IEEE C95.1-1999: IEEE Standard for Safety Levels with Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 3kHz to 300 GHz, The Institute of electrical and Electronics Engineers, Inc., New York, NY 10017, 1999
- [2] Federal Communications Commission, "Evaluating Compliance with FCC Guidelines for Human Exposure to Radiofrequency Electromagnetic Fields", Supplement C to OET Bulletin 65, Washington, D.C. 20554, 1997
- [3] IEEE Standards Coordinating Committee 34, "Recommended Practice for Determining the Peak Spatial-Average Specific Absorption Rate (SAR) in the Human Head from Wireless Communications Devices: Measurement Techniques", IEEE Std 1528/D1.2, April 21, 2003



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## **8.0 DOCUMENT HISTORY**

Revision/ Job Number	Writer Initials	Date	Change
N/A	J.C.	Jan. 15, 2004	Original document



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#### **APPENDIX A - SAR Evaluation Data**

**Power drift** is the measurement of power drift of the device over one complete SAR scan.

To assess the drift of the power of the device under test, a SAR measurement was made in the middle of the zoom scan volume at the start of the scan and a measurement at this point was then also made after the measurement scan. The difference between the two measurements should be less than 5%.



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Plot #1 (1/2)

**Date / Time:** 2004/1/14 **Position:** top 0mm-1

Filename: 11g-2437top0-1.txt Phantom: HeadBox2-test.csv

**Device Tested:** C300 **Head Rotation:** 

Antenna: PIFA Test Frequency: 2437MHz
Shape File: c300-new-top.csv Power Level: 16.75dBm

**Probe:** 0136

Cal File: SN0136\_2450\_CW\_BODY

Cal Factors: X Y Z
Air 490 405 405

 DCP
 20
 20
 20

 Lin
 .405
 .405
 .405

Amp Gain: 2
Averaging: 1
Batteries

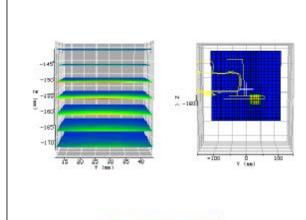
Batteries Softwa Replaced: Crest F

Liquid: 15.5cm

**Type:** 2450MHz Body

Conductivity: 1.93535
Relative Permittivity: 50.85820
Liquid Temp (deg C): 22.4
Ambient Temp (deg C): 21
Ambient RH (%): 40
Density (kg/m3): 1000
Software Version: 2.1 VPM

Crest Factor=1



0.04 0.05 SMI 18/kg8

## **ZOOM SCAN RESULTS:**

Change during Scan (%)

0.00

**Max E-field (V/m):** 6.77

Max SAR (W/kg)

1g	10g
0.066	0.034

Location of Max (mm):

X	Y	Z	
78.1	12.0	-157.0	

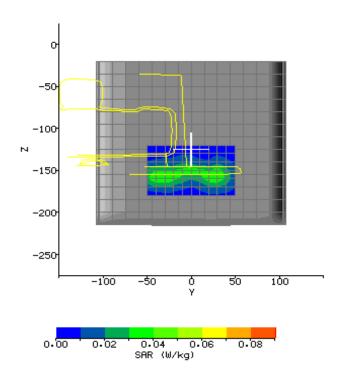


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Plot #1 (2/2)

## AREA SCAN:

		Min	Max	Steps
Scan Extent:				
Scan Latent.	Y	-50.0	50.0	10.0
	Z	-180.0	-120.0	6.0





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Plot #2 (1/2)

Date / Time: 2004/1/14 **Position:** top 0mm-2

11g-2437top0-2.txt HeadBox2-test.csv Filename: **Phantom:** 

**Device Tested:** C300 **Head Rotation:** 

**PIFA** 2437MHz Antenna: **Test Frequency:** c300-new-top.csv 16.75dBm **Shape File: Power Level:** 

**Probe:** 0136

Cal File: SN0136\_2450\_CW\_BODY

X Y  $\mathbf{Z}$ 405 490 405 Air **Cal Factors:** 

**DCP** 20 20 20 Lin .405 .405 .405

Amp Gain: 2 Averaging: 1 **Batteries** 

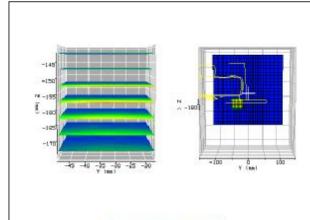
Replaced:

Liquid: 15.5cm

Type: 2450MHz Body

1.93535 **Conductivity:** 50.85820 **Relative Permittivity: Liquid Temp (deg C):** 22.4 Ambient Temp (deg C): 21 40 Ambient RH (%): 1000 Density (kg/m3): 2.1 VPM **Software Version:** 

Crest Factor=1



101 0.02 0.03 0.04 0.05 0.05 0.05 100 (M/kg)

# **ZOOM SCAN RESULTS:**

**Start Scan End Scan** Spot SAR (W/kg): 0.015 0.015

Change during Scan (%)

0.00

**Max E-field (V/m):** 5.63

Max SAR (W/kg)

1g	10g
0.050	0.028

**Location of Max** (mm):

X	Y	Z
78.1	-49.0	-157.1



Plot #2 (2/2)

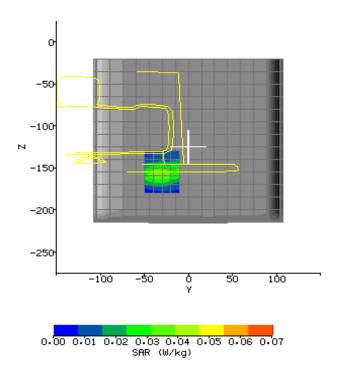
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# AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-50.0	-10.0	4.0
Z	-180.0	-130.0	5.0





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Plot #3 (1/2)

Date / Time: 2004/1/14 **Position:** top 15mm-1

11g-2437top15-1.txt HeadBox2-test.csv Filename: **Phantom: Device Tested:** C300

**Head Rotation: PIFA** 2437MHz Antenna: **Test Frequency:** 

c300-new-top.csv 16.75dBm **Shape File: Power Level:** 

**Probe:** 0136

Cal File: SN0136\_2450\_CW\_BODY

X Y  $\mathbf{Z}$ 405 490 405 Air **Cal Factors:** 

**DCP** 20 20 20 Lin .405 .405 .405

Amp Gain: 2 Averaging: 1 **Batteries** Replaced:

Liquid: 15.5cm Type: 2450MHz Body 1.93535 **Conductivity:** 50.85820 **Relative Permittivity: Liquid Temp (deg C):** 22.4 Ambient Temp (deg C): 21 40 Ambient RH (%): 1000 Density (kg/m3): 2.1 VPM **Software Version:** 

0.008

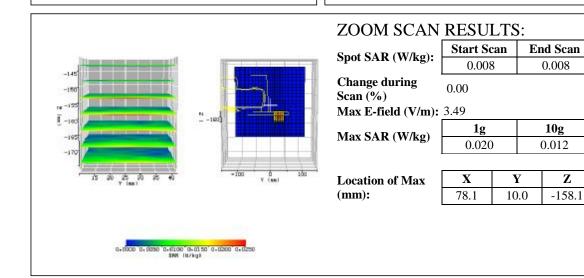
10g

0.012

 $\mathbf{Z}$ 

-158.1

Crest Factor=1





Plot #3 (2/2)

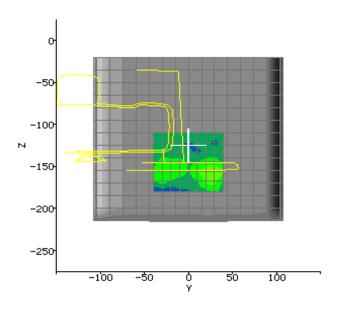
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# AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-40.0	40.0	8.0
$\mathbf{Z}$	-180.0	-110.0	6.0





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Plot #4 (1/2)

Date / Time:2004/1/14Position:top 15mm-2Filename:11g-2437top15-2.txtPhantom:HeadBox2-test.csv

**Device Tested:** C300 **Head Rotation:** C

Antenna: PIFA Test Frequency: 2437MHz
Shape File: c300-new-top.csv Power Level: 16.75dBm

**Probe:** 0136

Cal File: SN0136\_2450\_CW\_BODY

 Cal Factors:
 X
 Y
 Z

 Air
 490 405 405 

 DCP
 20 20 20 

**Lin** .405 .405 .405 **Amp Gain:** 2

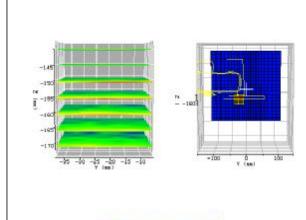
Averaging: 1
Batteries
Replaced:

Liquid: 15.5cm

**Type:** 2450MHz Body

Conductivity: 1.93535
Relative Permittivity: 50.85820
Liquid Temp (deg C): 22.4
Ambient Temp (deg C): 21
Ambient RH (%): 40
Density (kg/m3): 1000
Software Version: 2.1 VPM

Crest Factor=1



# **ZOOM SCAN RESULTS:**

Change during Scan (%)

-0.11

Max E-field (V/m): 2.92

Max SAR (W/kg)

<b>1g</b>	10g
0.014	0.010

Location of Max (mm):

X	Y	Z
78.1	-38.0	-153.3



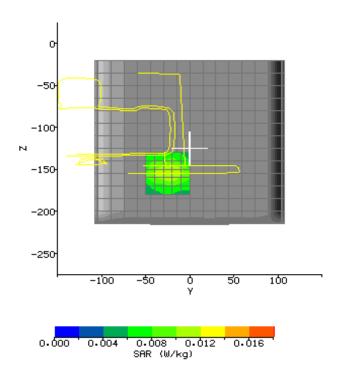
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Plot #4 (2/2)

# AREA SCAN:

**Scan Extent:** 

	Min	Max	Steps
Y	-50.0	0.0	5.0
Z	-180.0	-130.0	5.0





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**Position:** 

Plot #5 (1/2)

Date / Time: 2004/1/14

11g-2437rear0.txt HeadBox2-test.csv Filename: **Phantom:** 

**Device Tested:** C300 **Head Rotation:** 

**PIFA** 2437MHz Antenna: **Test Frequency:** c300-new-rear.csv 16.75dBm **Shape File: Power Level:** 

**Probe:** 0136

Cal File: SN0136\_2450\_CW\_BODY

X Y  $\mathbf{Z}$ 405 490 405 Air **Cal Factors: DCP** 20 20 20

Lin .405 .405 .405

Amp Gain: 2 Averaging: 1

**Batteries** Replaced: Liquid: 15.5cm

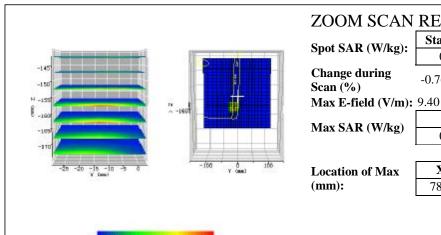
Type: 2450MHz Body

rear 0mm

1.93535 **Conductivity:** 50.85820 **Relative Permittivity: Liquid Temp (deg C):** 22.4 Ambient Temp (deg C): 21 40 Ambient RH (%):

1000 Density (kg/m3): 2.1 VPM **Software Version:** 

Crest Factor=1



# **ZOOM SCAN RESULTS:**

**Start Scan End Scan** Spot SAR (W/kg): 0.026 0.026

-0.76

1g	10g
0.126	0.062

X	Y	Z
78.0	-29.0	-158.9



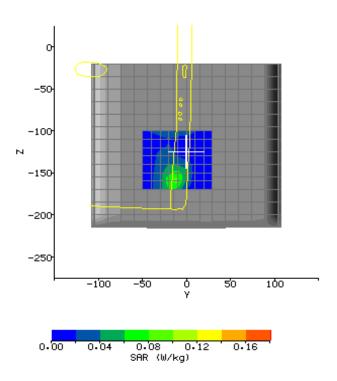
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Plot #5 (2/2)

# AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-50.0	30.0	8.0
Z	-170.0	-100.0	7.0





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Plot #6 (1/2)

**Date / Time:** 2004/1/14 **Position:** rear 15mm

Filename: 11g-2437rear15.txt Phantom: HeadBox2-test.csv

**Device Tested:** C300 **Head Rotation:** 

Antenna: PIFA Test Frequency: 2437MHz
Shape File: c300-new-rear.csv Power Level: 16.75dBm

**Probe:** 0136

Cal File: SN0136\_2450\_CW\_BODY

 Cal Factors:
 X
 Y
 Z

 Air
 490 405 405 

 DCP
 20 20 20 

**Lin** .405 .405 .405

Amp Gain: 2
Averaging: 1
Batteries
Replaced:

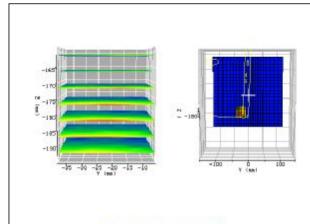
 Liquid:
 15.5cm

 Type:
 2450MHz Body

Conductivity: 1.93535
Relative Permittivity: 50.85820
Liquid Temp (deg C): 22.4
Ambient Temp (deg C): 21
Ambient RH (%): 40
Density (kg/m3): 1000

Crest Factor=1

**Software Version:** 



# **ZOOM SCAN RESULTS:**

Snot SAD (W/kg).	Start Scan	End Scan
Spot SAR (W/kg):	0.006	0.006

Change during Scan (%)

Max E-field (V/m): 3.51

Location of Max (mm):

X	Y	Z
78.1	-38.0	-180.6

2.1 VPM



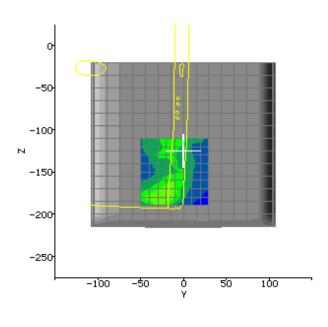
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Plot #6 (2/2)

# AREA SCAN:

Scan Extent:

	Min	Max	Steps
Y	-50.0	30.0	8.0
Z	-190.0	-110.0	8.0



0.0000'0.0050'0.0100'0.0150'0.0200'0.0250 SAR (W/kg)



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Plot #7 (1/2)

**Date / Time:** 2004/1/14 **Position:** right 0mm

Filename: 11g-2437right0.txt Phantom: HeadBox2-test.csv

**Device Tested:** C300 **Head Rotation:** 0

Antenna: PIFA Test Frequency: 2437MHz
Shape File: c300-new-right.csv Power Level: 16.75dBm

**Probe:** 0136

Cal File: SN0136\_2450\_CW\_BODY

 Cal Factors:
 X
 Y
 Z

 Air
 490 405 405 

 DCP
 20 20 20 

Lin .405 .405 .405

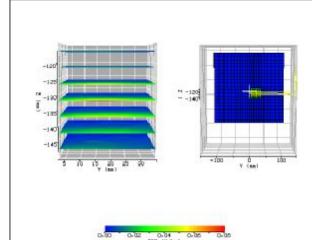
Amp Gain: 2
Averaging: 1
Batteries
Replaced:

Conductivity:1.93535Relative Permittivity:50.85820Liquid Temp (deg C):22.4Ambient Temp (deg C):21Ambient RH (%):40Density (kg/m3):1000Software Version:2.1 VPM

Crest Factor=1

Liquid:

Type:



# **ZOOM SCAN RESULTS:**

 Spot SAR (W/kg):
 Start Scan
 End Scan

 0.011
 0.011

Change during Scan (%)

0.00

**Max E-field (V/m):** 6.27

Max SAR (W/kg)

1g	10g
0.053	0.026

15.5cm

2450MHz Body

**Location of Max** (mm):

X	Y	Z	
78.1	3.0	-132.9	



Plot #7 (2/2)

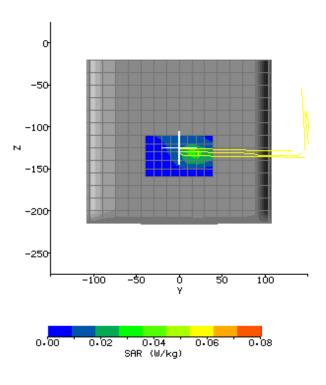
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# AREA SCAN:

**Scan Extent:** 

	Min	Max	Steps
Y	-40.0	40.0	8.0
$\mathbf{Z}$	-160.0	-110.0	5.0





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Plot #8 (1/1)

**Date / Time:** 2004/1/14 **Position:** right 15mm

Filename: 11g-2437right15a.txt Phantom: HeadBox2-test.csv

**Device Tested:** C300 **Head Rotation:** 0

Antenna: PIFA Test Frequency: 2437MHz
Shape File: c300-new-right.csv Power Level: 16.75dBm

**Probe:** 0136

Cal File: SN0136\_2450\_CW\_BODY

 Cal Factors:
 X
 Y
 Z

 DCP
 20
 405
 405

 DCP
 20
 20
 20

**Lin** .405 .405 .405

Amp Gain: 2
Averaging: 1
Batteries
Replaced:

Liquid Temp (deg C): 22.4

Ambient Temp (deg C): 21

Ambient RH (%): 40

Density (kg/m3): 1000

Software Version: 2.1 VPM

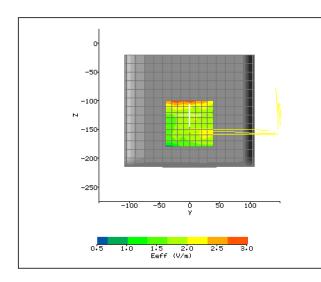
Crest Factor=1

Liquid:

**Conductivity:** 

**Relative Permittivity:** 

Type:



# AREA SCAN:

**Scan Extent:** 

	Min	Max	Steps
Y	-40.0	40.0	8.0
7.	-180.0	-100.0	8.0

15.5cm

1.93535

50.85820

2450MHz Body



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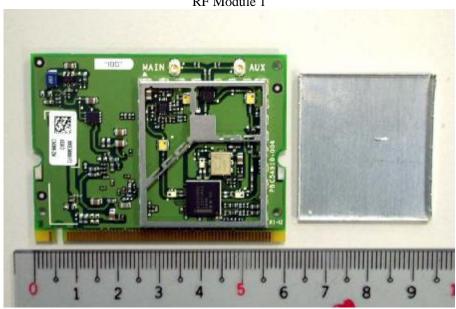
# **APPENDIX B - Photographs**





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RF Module 2





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 $\label{eq:control} \textbf{APPENDIX} \ \textbf{C} \ \textbf{-} \ \textbf{E-Field Probe} \ \textbf{and} \ \textbf{2450MHz} \ \textbf{Balanced Dipole Antenna Calibration} \\ \textbf{Data}$ 



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# **IMMERSIBLE SAR PROBE**

# **CALIBRATION REPORT**

Part Number: IXP – 050

S/N 0136

10<sup>th</sup> September 2003



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#### INTRODUCTION

This Report presents measured calibration data for a particular Indexsar SAR probe (S/N 0136) and describes the procedures used for characterisation and calibration.

Indexsar probes are characterised using procedures that, where applicable, follow the recommendations of CENELEC [1] and IEEE [2] standards. The procedures incorporate techniques for probe linearisation, isotropy assessment and determination of liquid factors (conversion factors). Calibrations are determined by comparing probe readings with analytical computations in canonical test geometries (waveguides) using normalised power inputs.

Each step of the calibration procedure and the equipment used is described in the sections below.

#### **CALIBRATION PROCEDURE**

#### 1. Equipment Used

For the first part of the characterisation procedure, the probe is placed in an isotropy measurement jig as pictured in Figure 1. In this position the probe can be rotated about its axis by a non-metallic belt driven by a stepper motor.

The probe is attached via its amplifier and an optical cable to a PC. A schematic representation of the test geometry is illustrated in Figure 2.

A balanced dipole (900 MHz) is inserted horizontally into the bracket attached to a second belt (Figure 1). The dipole can also be rotated about its axis. A cable connects the dipole to a signal generator, via a directional coupler and power meter. The signal generator feeds an RF amplifier at constant power, the output of which is monitored using the power meter. The probe is positioned so that its sensors line up with the rotation center of the source dipole. By recording output voltage measurements of each channel as both the probe and the dipole are rotated, data are obtained from which the spherical isotropy of the probe can be optimised and its magnitude determined.

The calibration process requires E-field measurements to be taken in air, in 900 MHz simulated brain liquid and at other frequencies/liquids as appropriate.

#### 2. Linearising probe output

The probe channel output signals are linearised in the manner set out in Refs [1] and [2]. The following equation is utilized for each channel:

$$U_{lin} = U_{o/p} + U_{o/p}^{2} / DCP$$
 (1)

where  $U_{lin}$  is the linearised signal,  $U_{o/p}$  is the raw output signal in voltage units and DCP is the diode compression potential in similar voltage units.

DCP is determined from fitting equation (1) to measurements of  $U_{lin}$  versus source feed power over the full dynamic range of the probe. The DCP is a characteristic of the schottky diodes used as the sensors. For the IXP-050 probes with CW signals the DCP values are typically 0.10V (or 20 in the voltage units used by Indexsar software, which are V\*200).

### 3. Selecting channel sensitivity factors to optimise isotropic response

The basic measurements obtained using the calibration jig (Fig 1) represent the output from each diode sensor as a function of the presentation angle of the source (probe and dipole rotation angles).



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The directionality of the orthogonally-arranged sensors can be checked by analysing the data using dedicated Indexsar software, which displays the data in 3D format as in Figure 3. The left-hand side of this diagram shows the individual channel outputs after linearisation (see above). The program uses these data to balance the channel outputs and then applies an optimisation process, which makes fine adjustments to the channel factors for optimum isotropic response.

The next stage of the process is to calibrate the Indexsar probe to a W&G EMR300 E-field meter in air. The principal reasons for this are to obtain conversion factors applicable should the probe be used in air and to provide an overall measure of the probe sensitivity.

A multiplier is applied to factors to bring the magnitudes of the average E-field measurements as close as possible to those of the W&G probe.

The following equation is used (where linearised output voltages are in units of V\*200):

$$E_{air}^{2} (V/m) = U_{linx} * Air Factor_{x} + U_{liny} * Air Factor_{y} + U_{linz} * Air Factor_{z}$$

$$(2)$$

It should be noted that the air factors are not separately used for normal SAR testing. The IXP-050 probes are optimised for use in tissue-simulating liquids and do not behave isotropically in air.

## 4. 900 MHz Liquid Calibration

Conversion factors for use when the probes are immersed in tissue-simulant liquids at 900 MHz are determined either using a waveguide or by comparison to a reference probe that has been calibrated by NPL. Waveguide procedures are described later. The summary sheet indicates the method used for the probe S/N 0136.

The conversion factor, referred to as the 'liquid factor' is also applied to the measurements of each channel. The following equation is used (where output voltages are in units of V\*200):

$$\begin{split} E_{liq}^{\ 2}\left(V/m\right) &= \quad U_{linx} * Air \ Factor_x * \ Liq \ Factor_x \\ &+ U_{liny} * Air \ Factor_y * \ Liq \ Factor_y \\ &+ U_{linz} * Air \ Factor_z * \ Liq \ Factor_z \end{split} \tag{3}$$

A 3D representation of the spherical isotropy for probe S/N 0136 using these factors is shown in Figure 3.

The rotational isotropy can also determined from the calibration jig measurements and is reported as the 900MHz isotropy in the summary table. Note that waveguide measurements can also be used to determine rotational isotropy (Fig. 5).

The design of the cells used for determining probe conversion factors are waveguide cells is shown in Figure 4. The cells consist of a coax to waveguide transition and an open-ended section of waveguide containing a dielectric separator. Each waveguide cell stands in the upright positition and is filled with liquid within 10 mm of the open end. The seperator provides a liquid seal and is designed for a good electrical transition from air filled guide to liquid filled guide. The choice of cell depends on the portion of the frequency band to be examined and the choice of liquid used. The depth of liquid ensures there is negligible radiation from the waveguide open top and that the probe calibration is not influenced by reflections from nearby objects. The return loss at the coaxial connector of the filled waveguide cell is measured initially using a network analyser and this information is used subsequently in the calibration procedure. The probe is positioned in the centre of the waveguide and is adjusted vertically or rotated using stepper motor arrangements. The signal generator is connected to the waveguide cell and the power is monitored with a coupler and a power meter. A fuller



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description of the waveguide method is given below.

The liquid dielectric parameters used for the probe calibrations are listed in the Tables below. The final calibration factors for the probe are listed in the summary chart.

## WAVEGUIDE MEASUREMENT PROCEDURE

The calibration method is based on setting up a calculable specific absorption rate (SAR) in a vertically-mounted WG8 (R22) waveguide section [1]. The waveguide has an air-filled, launcher section and a liquid-filled section separated by a matching window that is designed to minimise reflections at the liquid interface. A  $TE_{01}$  mode is launched into the waveguide by means of a N-type-to-waveguide adapter. The power delivered to the liquid section is calculated from the forward power and reflection coefficient measured at the input to the waveguide. At the centre of the cross-section of the waveguide, the local spot SAR in the liquid as a function of distance from the window is given by functions set out in IEEE1528 as below:

Because of the low cutoff frequency, the field inside the liquid nearly propagates as a TEM wave. The depth of the medium (greater than three penetration depths) ensures that reflections at the upper surface of the liquid are negligible. The power absorbed in the liquid is determined by measuring the waveguide forward and reflected power. Equation (4) shows the relationship between the SAR at the cross-sectional center of the lossy waveguide and the longitudinal distance (z) from the dielectric separator

$$SAR(z) = \frac{4(P_f - P_b)}{rahd}e^{-2z/d}$$
(4)

where the density r is conventionally assumed to be  $1000 \text{ kg/m}^3$ , ab is the cross-sectional area of the waveguide,  $P_f$  and  $P_b$  are the forward and reflected power inside the lossless section of the waveguide, respectively. The penetration depth d, which is the reciprocal of the waveguide-mode attenuation coefficient, is determined from a scan along the z-axis and compared with the theoretical value determined from Equation (5) using the measured dielectric properties of the lossy liquid.

$$d = \left[ \operatorname{Re} \left\{ \sqrt{\left( p / a \right)^{2} + j w m_{o} \left( s + j w e_{o} e_{r} \right)} \right\} \right]^{-1}.$$
 (5)

Table A.1 of [1] can be used for designing calibration waveguides with a return loss greater than 30 dB at the most important frequencies used for personal wireless communications. Values for the penetration depth for these specific fixtures and tissue-simulating mixtures are also listed in Table A.1.

According to [1], this calibration technique provides excellent accuracy, with standard uncertainty of less than 3.6% depending on the frequency and medium. The calibration itself is reduced to power measurements traceable to a standard calibration procedure. The practical limitation to the frequency band of 800 to 2500 MHz because of the waveguide size is not severe in the context of compliance testing.



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#### CALIBRATION FACTORS MEASURED FOR PROBE S/N 0136

The probe was calibrated at 900, 1800, 1900 and 2450MHz MHz in liquid samples representing both brain liquid and body fluid at these frequencies. The calibration was for CW signals only, and the axis of the probe was parallel to the direction of propagation of the incident field i.e. end-on to the incident radiation. The axial isotropy of the probe was measured by rotating the probe about its axis in 10 degree steps through 360 degrees in this orientation.

The reference point for the calibration is in the centre of the probe's cross-section at a distance of 2.7 m from the probe tip in the direction of the probe amplifier. A value of 2.7 mm should be used for the tip to sensor offset distance in the software.

It is important that the diode compression point and air factors used in the software are the same as those quoted in the results tables, as these are used to convert the diode output voltages to a SAR value.

# **DIELECTRIC PROPERTIES OF LIQUIDS**

The dielectric properties of the brain and body tissue-simulant liquids employed for calibration are listed in the tables below. The measurements were performed prior to each waveguide test using an Indexsar DiLine measurement kit, which uses the TEM method as recommended in [2].

#### AMBIENT CONDITIONS

Measurements were made in the open laboratory at  $22 \pm 2.0$  °C. The temperature of the liquids in the waveguide used was measured using a mercury thermometer.

## RESPONSE TO MODULATED SIGNALS

To measure the response of the probe and amplifier to modulated signals, the probe is held vertically in a liquid-filled waveguide.

An RF amplifier is allowed to warm up and stabilise before use. A spectrum analyser is used to demonstrate that the peak power of the RF amplifier for the CW signals and the pulsed signals are within 0.1dB of each other when the signal generator is switched from CW to modulated output. Subsequently, the power levels recorded are read from a power meter when a CW signal is being transmitted.

The test sequence involves manually stepping the power up in regular (e.g. 2 dB) steps from the lowest power that gives a measurable reading on the SAR probe up to the maximum that the amplifiers can deliver.

At each power level, the individual channel outputs from the SAR probe are recorded at CW and then recorded again with the modulation setting. The results are entered into a spreadsheet. Using the spreadsheets, the modulated power is calculated by applying a factor to the measured CW power (e.g. for GSM, this factor is 9.03dB). This process is repeated 3 times with the response maximised for each channel sensor in turn.



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The probe channel output signals are linearised in the manner set out in Section 1 above using equation (1) with the DCPs determined from the linearisation procedure. Calibration factors for the probe are used to determine the E-field values corresponding to the probe readings using equation (3). SAR is determined from the equation

SAR (W/kg) = 
$$E_{lig}^{2}$$
 (V/m) \*  $\sigma$ (S/m) / 1000 (6)

Where  $\sigma$  is the conductivity of the simulant liquid employed.

Using the spreadsheet data, the DCP value for linearising each of the individual channels (X, Y and Z) is assessed separately. The corresponding DCP values are listed in the summary page of the calibration factors for each probe.

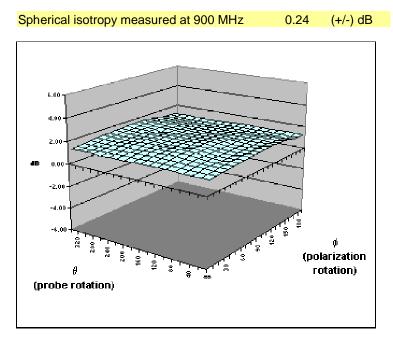
Figure 7 shows the linearised probe response to GSM signals, Figure 8 the response to GPRS signals (GSM with 2 timeslots) and Figure 9 the response to CDMA IS-95A and W-CDMA signals.

Additional tests have shown that the modulation response is similar at 1800MHz and is not affected by the orientation between the source and the probe.



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# SUMMARY OF CALIBRATION FACTORS FOR PROBE IXP-050 S/N 0136



	Χ	Υ	Z	
Air factors	490	405	405	(V*200)
DCPs	20	20	20	(V*200)
DSSS	20	20	20	(V*200)
GSM	8	9.5	11.2	(V*200)
CDMA	20	20	20	(V*200)

f (MHz)	Α	xial isot	гору	SAR conv	ersion factors	Notes
	(+	⊦/- dB)		(liq/air)		
	В	RAIN	BODY	BRAIN	BODY	
45	0					
83	5	0.05	0.04	0.257	0.272	1,2,3
90	0	0.05	0.04	0.261	0.282	1,2,3
180	0	0.06	0.06	0.315	0.339	1,2,3
190	0	0.06	0.06	0.327	0.351	1,2,3
245	0	0.05	0.10	0.378	0.405	1,2,3

Notes		
1)	Calibrations done at 22C +/- 2C	
2)	Waveguide calibration	
3)	Checked using box-phantom validation test	

(the graph shows a simple, spreadsheet representation of surface shown in 3D in Figure 3 below)



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# **ROBE SPECIFICATIONS**

Indexsar probe 0136, along with its calibration, is compared with CENELEC and IEEE standards recommendations (Refs [1] and [2]) in the Tables below. A listing of relevant specifications is contained in the tables below:

ntained in the tables below:	_	•	
Dimensions	S/N 0136	CENELEC [1]	IEEE [2]
Overall length (mm)	350		
Tip length (mm)	10		
Body diameter (mm)	12		
Tip diameter (mm)	5.2	8	8
Distance from probe tip to dipole centers (mm)	2.7		
Dynamic range	S/N 0136	CENELEC [1]	IEEE [2]
Minimum (W/kg)	0.01	< 0.02	0.01
Maximum (W/kg) N.B. only measured to 35 W/kg	>35	>100	100
Linearity of response	S/N 0136	CENELEC [1]	IEEE [2]
Over range 0.01 – 100 W/kg (+/- dB)	0.125	0.50	0.25
	1		Г
Isotropy (measured at 900MHz)	S/N 0136	CENELEC [1]	IEEE [2]
Axial rotation with probe normal to source (+/- dB) at 835, 900, 1800, 1900 and 2450 MHz	Max. 0.10 (see summary table)	0.5	0.25
Spherical isotropy covering all orientations to source (+/- dB)	0.24	1.0	0.50
Construction	sensors arrang protected again shielding, and cylindrical en are used in the materials are	Each probe contains three orthogonal dipole sensors arranged on a triangular prism core, protected against static charges by built-in shielding, and covered at the tip by PEEK cylindrical enclosure material. No adhesives are used in the immersed section. Outer case materials are PEEK and heat-shrink sleeving.	
Chemical resistance	Tested to be resistant to glycol and alcohol containing simulant liquids but probes should be removed, cleaned and dried when not in		

use.



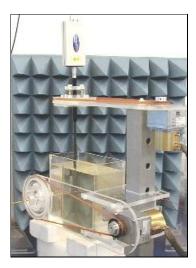
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#### **REFERENCES**

- [1] CENELEC, EN 50361, July 2001. Basic Standard for the measurement of specific absorption rate related to human exposure to electromagnetic fields from mobile phones.
- [2] IEEE 1528, Recommended practice for determining the spatial-peak specific absorption rate (SAR) in the human body due to wireless communications devices: Experimental techniques.
- [3] Calibration report on SAR probe IXP-050 S/N 0071 from National Physical Laboratory. Test Report EF07/2002/03/IndexSAR. Dated 20 February 2002.



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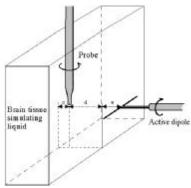


Figure 1. Spherical isotropy jig showing probe, dipole and box filled with simulated brain liquid (see Ref [2], Section A.5.2.1)

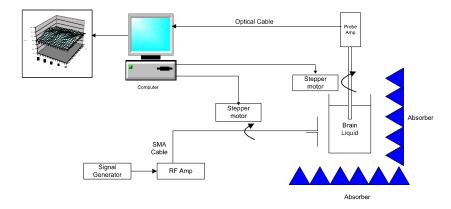


Figure 2. Schematic diagram of the test geometry used for isotropy determination



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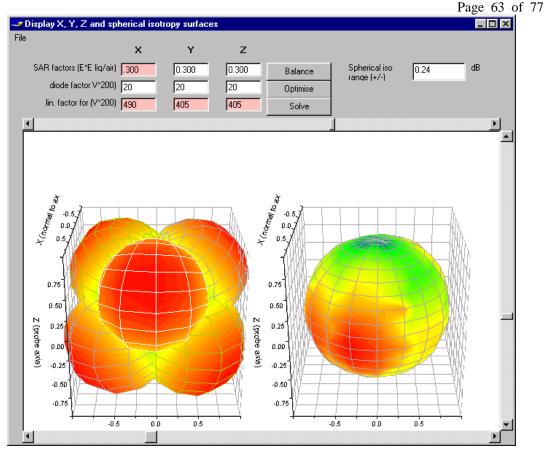


Figure 3. Graphical representation of the probe response to fields applied from each direction. The diagram on the left shows the individual response characteristics of each of the three channels and the diagram on the right shows the resulting probe sensitivity in each direction. The colour range in the figure images the lowest values as blue and the maximum values as red. For the probe S/N 0136, this range is (+/-) 0.24 dB. The probe is more sensitive to fields parallel to the axis and less sensitive to fields normal to the probe axis.

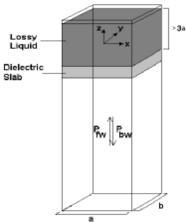


Figure 4. Geometry used for waveguide calibration (after Ref [2]. Section A.3.2.2)

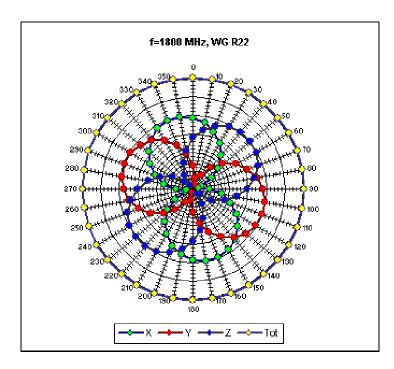


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#### IXP-050 S/N 0136

# 18-Aug-03



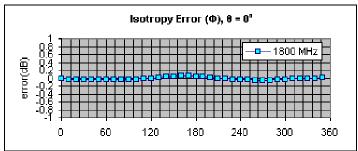
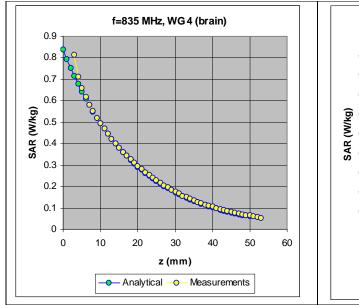


Figure 5. Example of the rotational isotropy of probe S/N 0136 obtained by rotating the probe in a liquid-filled waveguide at 2450 MHz. Similar distributions are obtained at the other test frequencies (1800 and 1900 MHz) both in brain liquids and body fluids (see summary table)



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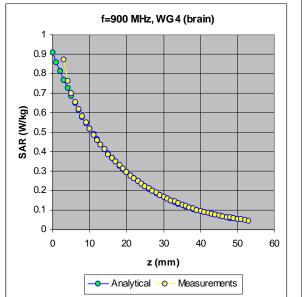


Figure 6. The measured SAR decay function along the centreline of the WG4 waveguide with conversion factors adjusted to fit to the theoretical function for the particular dimension, frequency, power and liquid properties employed.



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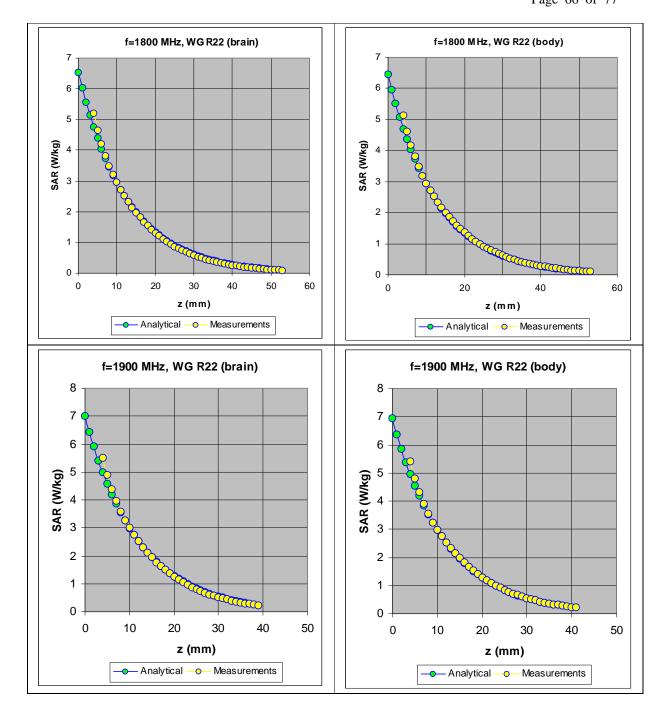


Figure 7. The measured SAR decay function along the centreline of the R22 waveguide with conversion factors adjusted to fit to the theoretical function for the particular dimension, frequency, power and liquid properties employed.



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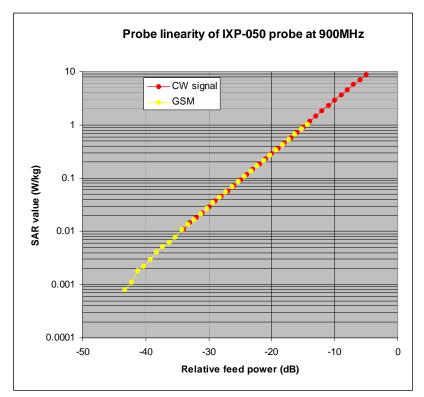


Figure 8. The GSM response of an IXP-050 probe at 900MHz.

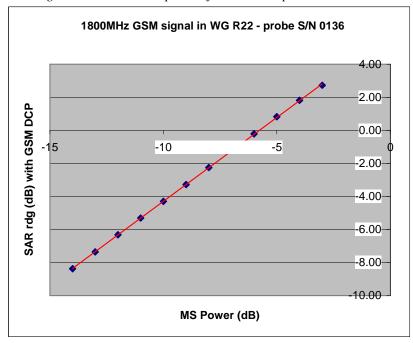


Figure 8a. The actual GSM response of IXP-050 probe S/N 0136 at 1800MHz



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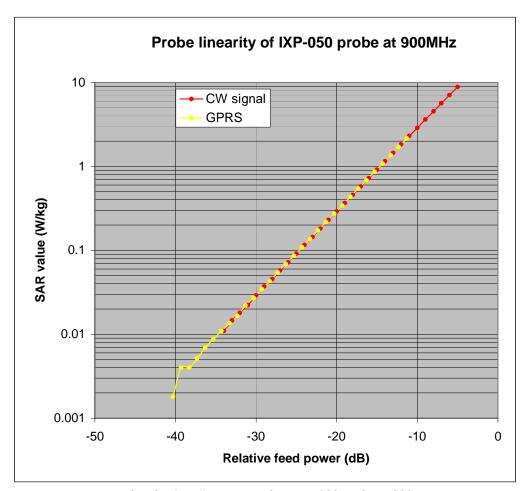
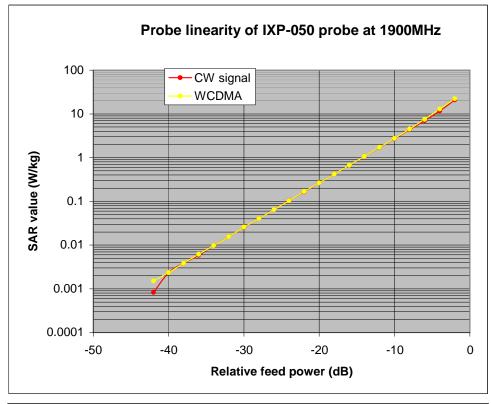


Figure 9. The GPRS response of an IXP-050 probe at 900MHz.



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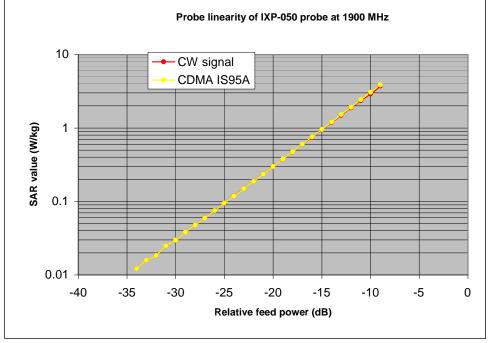


Figure 10. The CDMA response of an IXP-050 probe at 1900MHz.



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# $Table\ indicating\ the\ dielectric\ parameters\ of\ the\ liquids\ used\ for\ calibrations\ at\ each\ frequency$

Liquid used	Relative permittivity (measured)	Conductivity (S/m) (measured)
835 MHz BRAIN	43.18	0.935
835 MHz BODY	59.19	0.992
900 MHz BRAIN	42.47	0.998
900 MHz BODY	58.7	1.056
1800 MHz BRAIN	38.72	1.34
1800 MHz BODY	52.5	1.53
1900 MHz BRAIN	38.31	1.43
1900 MHz BODY	52.06	1.64
2450 MHz BRAIN	38.9	1.87
2450 MHz BODY	52.59	2.08



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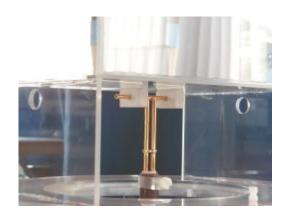


Report No. SN0048\_2450 26<sup>th</sup> March 2003

# INDEXSAR 2450MHz validation Dipole Type IXD-245 S/N 0048

#### **Performance measurements**

#### MI Manning



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# Calibration / Conformance statement Balanced Validation dipole

Type: IXD-	245 2450MHz	
Manufacturer:	IndexSAR, UK	
Serial Number:	0048	
Place of Calibration:	IndexSAR, UK	
	at the IXD series dipole named above has been checked for in the draft IEEE 1528 and CENELEC En 50361 standards on	
Date of Calibration/Check:	26 <sup>th</sup> March 2003	
	riodically re-checked using the procedures set out in the dipole that the cautions regarding handling of the dipoles (given in the	
Next Calibration Date:	March 2005	
The calibration measurements were carried out using the methods described in the calibration document. Where applicable, the standards used in the calibration process are traceable to the UK's National Physical Laboratory.		
Calibrated By:		
Approved By:	M1. Name	



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# 1. Tests on Validation Dipole

Tests have been performed on a balanced dipole made for 2450MHz application according to the construction guidelines, dimensions and tolerances given in the draft IEEE1528 standard [1]. Measurements have been made of the impedance and return loss when positioned against the liquid-filled phantom and a validation test has been performed according to the procedures set out in IEEE 1528 [1].

#### 2. Measurement Conditions

Measurements were performed using a box-shaped phantom made of PMMA with dimensions designed to meet the accuracy criteria for reasonably-sized phantoms that do not have liquid capacities substantially in excess of the volume of liquid required to fill the Indexsar upright SAM phantoms used for SAR testing of handsets against the ear.

An HP 8753B vector network analyser was used for the return loss measurements. The dipole was placed in a special holder made of low-permittivity, low-loss materials. This holder enables the dipole to be positioned accurately in the centre of the base of the Indexsar box-phantom used for flat-surface testing and validation checks.

The validation dipoles are supplied with special spacers made from a low-permittivity, low-loss foam material. These spacers are fitted to the dipole arms to ensure that, when the dipole is offered up to the phantom surface, the spacing between the dipole and the liquid surface is accurately aligned according to the guidance in the relevant standards documentation. The spacers are rectangular with a central hole equal to the dipole arm diameter and dimensioned so that the longer side can be used to ensure a spacing of 15mm from the liquid in the phantom (for tests at 900MHz and below) and the shorter side can be used for tests at 1800MHz and above to ensure a spacing of 10mm from the liquid in the phantom. The spacers are made on a CNC milling machine with an accuracy of  $1/40^{th}$  mm but they may suffer wear and tear and need to be replaced periodically. The material used is Rohacell, which has a relative permittivity of approx. 1.05 and a negligible loss tangent.

The apparatus supplied by Indexsar for dipole validation tests thus includes:

Balanced dipoles for each frequency required are dimensioned according to the guidelines given in IEEE 1528 [1]. The dipoles are made from semi-rigid 50 Ohm co-ax, which is joined by soldering and is gold-plated subsequently. The constructed dipoles are easily deformed, if mis-handled, and periodic checks need to be made of their symmetry.

Rohacell foam spacers designed for presenting the dipoles to 2mm thick PMMA box phantoms. These components also suffer wear and tear and should be replaced when the central hole is a loose-fit on the dipole arms or if the edges are too worn to ensure accurate alignment. The standard spacers are dimensioned for use with 2mm wall thickness (additional spacers are available for 4mm wall thickness).

#### 3. SAR Validation Measurement

A SAR validation check was performed with the box-phantom located on the SARA2 phantom support base on the SARA2 robot system. Tests were then conducted at a feed power level of approx. 0.25W. The actual power level was recorded and used to normalise the results obtained to the standard input power conditions of 1W (forward power). The ambient temperature was 24°C.

The phantom was filled with a 2450MHz brain liquid using a recipe from [1], which was measured using an Indexsar DiLine kit at 2450MHz. Measurements were taken at 23°C and 30°C and interpolation was used to find the properties at 24°C which were as below:

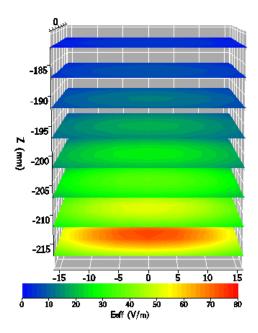


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Relative Permittivity 39.221 Conductivity 1.8714 S/m

The SARA2 software version 0.420N was used with an Indexsar probe previously calibrated using waveguide techniques.

The 3D measurement made using the dipole at the bottom of the phantom box is shown below:



The volume-averaged SAR results, normalised to an input power of 1W (forward power) are:

Averaged over 1 cm<sup>3</sup> (1g) of tissue 51.376 W/kg Averaged over 10cm<sup>3</sup> (10g) of tissue 23.888 W/kg

These results can be compared with Table 8.1 in [1]. The agreement is within 10%.

### 4. Dipole impedance and return loss

The dipoles are designed to have low return loss ONLY when presented against a lossy-phantom at the specified distance. A Vector Network Analyser (VNA) was used to perform a return loss measurement on the specific dipole when in the measurement-location against the box phantom. The distance was as specified in the standard i.e. 10mm from the liquid (for 2450MHz). The Indexsar foam spacers (described above) were used to ensure this condition during measurement.

The impedance was measured at the SMA-connector with the network analyser. The following parameters were measured:

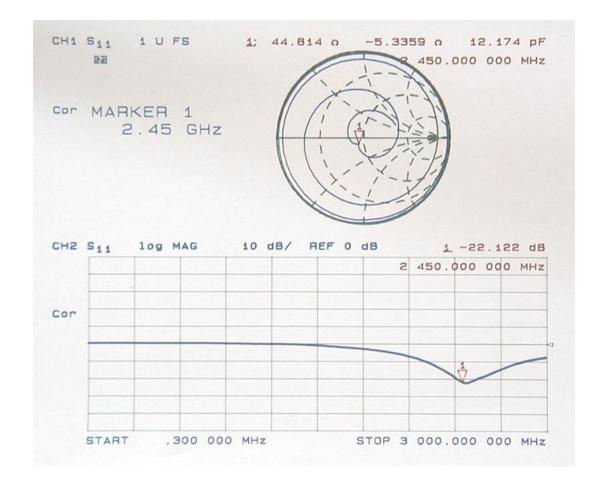
Dipole impedance at 2450 MHz Re{Z} = **44.814**  $\Omega$  Im{Z} = **-5.3359**  $\Omega$ 

Return loss at 2450MHz -22.122 dB



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#### 5. Dipole handling

The dipoles are made from standard, copper-sheathed coaxial cable. In assembly, the sections are joined using ordinary soft-soldering. This is necessary to avoid excessive heat input in manufacture, which would destroy the polythene dielectric used for the cable. The consequence of the construction material and the assembly technique is that the dipoles are fragile and can be deformed by rough handling. Conversely, they can be straightened quite easily as described in this report.

If a dipole is suspected of being deformed, a normal workshop lathe can be used as an alignment jig to restore the symmetry. To do this, the dipole is first placed in the headstock of the lathe (centred on the plastic or brass spacers) and the headstock is rotated by hand (do NOT use the motor). A marker (lathe tool or similar) is brought up close to the end of one dipole arm and then the headstock is rotated by 0.5 rev. to check the opposing arm. If they are not balanced, judicious deformation of the arms can be used to restore the symmetry.

If a dipole has a failed solder joint, the dipole can be fixed down in such a way that the arms are colinear and the joint re-soldered with a reasonably-powerful electrical soldering iron. Do not use gas soldering irons. After such a repair, electrical tests must be performed as described below.

Please note that, because of their construction, the dipoles are short-circuited for DC signals.



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# 6. Tuning the dipole

The dipole dimensions are based on calculations that assumed specific liquid dielectric properties. If the liquid dielectric properties are somewhat different, the dipole tuning will also vary. A pragmatic way of accounting for variations in liquid properties is to 'tune' the dipole (by applying minor variations to its effective length). For this purpose, Indexsar can supply short brass tube lengths to extend the length of the dipole and thus 'tune' the dipole. It cannot be made shorter without removing a bit from the arm. An alternative way to tune the dipole is to use copper shielding tape to extend the effective length of the dipole. Do both arms equally.

It should be possible to tune a dipole as described, whilst in place in the measurement position as long as the user has access to a VNA for determining the return loss.

#### 7. Reference

[1] Draft recommended practice for determining the peak spatial-average specific absorption rate (SAR) in the human body due to wireless communications devices: Measurement Techniques. Draft CD1.1 – December 29, 2002.