## TEST REPORT

| EUT Description | 2x2 Wi-Fi and BT, M.2 1216 adapter card |
| :--- | :--- |
| Brand Name | Intel® BE200D2W |
| Model Name | BE200D2W |
| FCC ID | PD9BE200D2 |
| Date of Test Start/End | $2023-08-21 / 2023-09-26$ |
| Features | 2x2 Wi-Fi - IEEE 802.11be - Bluetooth $®$ <br> (see section 5) |
| Description | Modular sample + Tri-band antenna |


| Applicant | Intel Corporation SAS |
| :--- | :--- |
| Address | $\mathbf{4 2 5}$ Rue de Goa - Le Cargo B6 - 06600 Antibes, FRANCE |
| Contact Person | Benjamin Lavenant |
| Telephone/Fax/ Email | Benjamin.lavenant@intel.com |


| Reference Standards | FCC 47 CFR Part §2.1093 (see section 1) |  |
| :---: | :---: | :---: |
| RF Exposure Environment | Portable devices - General population/uncontrolled exposure |  |
|  | Testing Result | Limit |
| Maximum Power Density Result \& Limit | 9.90 W/m ${ }^{\mathbf{2}}\left(4 \mathrm{~cm}^{2}\right)$ | $10 \mathrm{~W} / \mathrm{m}^{2}\left(4 \mathrm{~cm}^{2}\right)$ |
| Maximum SAR Result \& Limit | 0.79 W/kg (1g) | 1.6 W/kg (1g) |
| Min. test separation distance | 11 mm to phantom, 11 mm to probe tip (PD) |  |


| Test Report identification | $230526-09$. TR66 |
| :--- | :--- |
| Revision Control | Rev. 00 <br> This test report revision replaces any previous test report revision <br> (see section 8) |

The test results relate only to the samples tested.

Issued by


Yamine HADDAD (SAR Test Engineer)
Reviewed by


Adel LOUNES
(SAR Test Lead Engineer)

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## 1. Standards, reference documents and applicable test methods

1. FCC 47 CFR Part $\S 2.1093$ - Radiofrequency radiation exposure evaluation: portable devices. 2021-1001 Edition
2. FCC 47 CFR Part $\S 1.1310$ - Radiofrequency radiation exposure limits. Edition October 2021
3. FCC OET KDB 248227 D01 v02r02 - SAR guidance for IEEE 802.11 (Wi-Fi) transmitters.
4. FCC OET KDB 447498 D04 v01 General RF Exposure Guidance v01- RF Exposure Procedures and Equipment Authorization Policies for Mobile and Portable Devices
5. FCC OET KDB 616217 D04 v01r02 - SAR Evaluation Considerations for Laptop, Notebook, Netbook and Tablet Computers.
6. FCC OET KDB 865664 D01 v01r04 - SAR Measurement Requirements for 100 MHz to 6 GHz .
7. FCC OET KDB 865664 D02 v01r02 - RF Exposure Compliance Reporting and Documentation Considerations.
FCC
8. IEEE Std 1528-2013 - IEEE Recommended Practice Determining the Peak Spatial-Average Specific Absorption Rate (SAR) in the Human Head from Wireless Communication Devices: Measurement Techniques...
9. RF Exposure Policies and Procedures: TCB Workshop - October 2020
10. IEC/IEEE 62209-1528:2020 Measurement procedure for the assessment of specific absorption rate of human exposure to radio frequency fields from hand-held and body-mounted wireless communication devices - Part 1528: Human models, instrumentation, and procedures (Frequency range of 4 MHz to $10 \mathrm{GHz})$
11. 987594 D04 UN6GHZ Pre-Approval Guidance Checklist v01
12. SPEAG Application Note - 5G Compliance Testing with DASY6 (5GModule V1.0Beta)
13. SPEAG Application Note - 5G Compliance Testing with DASY6/8 (5GModule V5.0)

## 2. General conditions, competences and guarantees

$\checkmark$ Intel Corporation SAS Wireless RF Lab (Intel WRF Lab) is an Accredited Test Firm recognized by the FCC, with Designation Number FR0011.
$\checkmark$ Intel WRF Lab only provides testing services and is committed to providing reliable, unbiased test results and interpretations.
$\checkmark$ Intel WRF Lab is liable to the client for the maintenance of the confidentiality of all information related to the item under test and the results of the test.
$\checkmark$ Intel WRF Lab has developed calibration and proficiency programs for its measurement equipment to ensure correlated and reliable results to its customers.
$\checkmark$ This report is only referred to the item that has undergone the test.
$\checkmark$ This report does not imply an approval of the product by the Certification Bodies or competent Authorities.

## 3. Environmental Conditions

$\checkmark$ At the site where the measurements were performed the following limits were not exceeded during the tests:

| Temperature | $21.4^{\circ} \mathrm{C} \pm 1.2^{\circ} \mathrm{C}$ |
| :---: | :---: |
| Humidity | $46.1 \% \pm 18.4 \%$ |
| Liquid Temperature | $22.2^{\circ} \mathrm{C} \pm 1.2^{\circ} \mathrm{C}$ |

## 4. Test samples

| Sample | Control \# | Description | Model | Serial \# | Date of receipt | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \#01 | 230526-09.S31 | 2x2 Wi-Fi and BT, M. 21216 adapter card | BE200D2W+Engineering sample | 743AF406E16D | 2023-08-06 | - |
|  | 230724-02.S16 | 2x2 Wi-Fi and BT, M. 21216 adapter card | BE200D2W Engineering sample | 04E8B963C28E | 2023-07-24 | - |
|  | 180001-01.S16 | Socket | - | - | 2018-12-18 | - |
|  | 180001-01.S17 | Socket | Extender board | $\begin{gathered} \hline \text { ASS0495-001, } \\ 4950414-019 \\ \hline \end{gathered}$ | 2015-05-12 | - |
|  | 230306-01.S01 | Antenna | Tri-band | - | 2023-07-03 | - |
|  | 230306-01.S03 | Antenna | Tri-band | - | 2023-07-03 | - |
|  | 200904-01.S09 | Computer | Opel (HSN-I42C) | 000075059H | 2021-09-21 | - |

## 5. EUT Features

The herein information is provided by the customer
Intel WRF Lab declines any responsibility for the accuracy of the stated customer provided information, especially if it has any impact on the correctness of test results presented in this report.

| Brand Name | Intel® BE200D2W |  |  |
| :---: | :---: | :---: | :---: |
| Model Name | BE200D2W |  |  |
| Software Version | DRTU.04696.99.0.81 |  |  |
| Driver Version | 99.0.81.11 |  |  |
| Prototype / Production | Production |  |  |
| Host Identification | Engineering sample |  |  |
| Supported Radios | $802.11 \mathrm{~b} / \mathrm{g} / \mathrm{h} / \mathrm{ax} / \mathrm{be}$ 802.11a/n/ac/ax/be <br> 802.11ax/be Bluetooth | 2.4GHz (2400.0-2483.5 MHz) <br> $5.2 \mathrm{GHz}(5150.0-5350.0 \mathrm{MHz})$ <br> $5.6 \mathrm{GHz}(5470.0-5725.0 \mathrm{MHz})$ <br> $5.8 \mathrm{GHz}(5725.0-5850.0 \mathrm{MHz})$ <br> $5.9 \mathrm{GHz}(5850.0-5895.0 \mathrm{MHz})$ <br> $6.0 \mathrm{GHz}(5925.0-6425.0 \mathrm{MHz}$ ) * <br> $2.4 \mathrm{GHz}(2400.0-2483.5 \mathrm{MHz})$ |  |
| Antenna Information | Transmitter | Main / Chain B / Tx2 | Aux / Chain A / Tx 1 |
|  | Manufacturer | Intel | Intel |
|  | Antenna type | Tri-band | Tri-band |
|  | Part number | 01 | 03 |
|  | See Annex $G$ for more details on antennas location. |  |  |
| Simultaneous Transmission Configurations | WLAN 6GHz Main + BT Aux* <br> WLAN 6GHz Main + WLAN 6GHz Aux* <br> WLAN 6GHz Main + WLAN 6GHz Aux + BT Aux* <br> WLAN 2.4GHz Main + BT Aux <br> WLAN 2.4GHz Main + WLAN 2.4GHz Aux <br> WLAN 5GHz Main + BT Aux <br> WLAN 5GHz Main + WLAN 5GHz Aux <br> WLAN 5GHz Main + WLAN 5GHz Aux + BT Aux |  |  |
| Additional Information | No WWAN transmitter is considered in this report |  |  |
|  | $5.60-5.65 \mathrm{GHz}$ band (TDWR) is supported by the device |  |  |
|  | Band gap is supported by the device |  |  |

*Only these combinations are treated on this document since this report is limited to WiFi 6E capabilities

## Supported Radios

| Mode | Duty Cycle | Modulation | Band | UL Freq Range (MHz) | Measured Max Conducted Power (dBm) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 802.11ax/be | 100\% | $\begin{gathered} \text { BPSK } \\ \text { QPSK } \\ \text { 16QAM } \\ \text { 64QAM } \\ \text { 256QAM } \end{gathered}$ | 6.2GHz | 5955-6415 | 18.95 |
| 802.11ax/be | 100\% | $\begin{gathered} \hline \text { BPSK } \\ \text { QPSK } \\ \text { 16QAM } \\ \text { 64QAM } \\ \text { 256QAM } \end{gathered}$ | 6.5 GHz | 6435-6515 | 14.72 |
| 802.11ax/be | 100\% | $\begin{gathered} \hline \text { BPSK } \\ \text { QPSK } \\ \text { 16QAM } \\ \text { 64QAM } \\ \text { 256QAM } \end{gathered}$ | 6.7 GHz | 6535-6855 | 18.99 |
| 802.11ax/be | 100\% | BPSK QPSK 16QAM 64QAM 256QAM | 7.0GHz | 6875-7125 | 17.12 |

NM: Not Measured

Maximum Output power specification + Tune up tolerance limit, as specified by the client

|  |  |  | SISO mode |  |
| :---: | :---: | :---: | :---: | :---: |
| Equipment Class | Mode | BW (MHz) | Main/Tx2 (dBm) | Aux/Tx1 (dBm) |
|  |  | 20 | 19.00 | 19.00 |
|  | 8 | 40 | 19.00 | 19.00 |
| U-NII-5 | 802.11ax/be | 80 | 19.00 | 19.00 |
|  |  | 160 | 19.00 | 19.00 |
|  | 802.11 be | 320 | 18.25 | 18.50 |
|  |  | 20 | 5.50 | 5.75 |
| -NII-6 | 802.11ax/be | 40 | 8.75 | 8.75 |
| U-Nil-6 | 802.11ax/be | 80 | 11.75 | 11.75 |
|  |  | 160 | 14.75 | 14.75 |
|  |  | 20 | 19.00 | 19.00 |
|  | $802.11 \mathrm{ax} / \mathrm{be}$ | 40 | 19.00 | 19.00 |
| U-NII-7 | 802.11ax/be | 80 | 19.00 | 19.00 |
|  |  | 160 | 19.00 | 19.00 |
|  | 802.11 be | 320 | 17.25 | 17.25 |
|  |  | 20 | 5.75 | 5.75 |
|  | $802.11 \mathrm{ax} / \mathrm{be}$ | 40 | 8.75 | 8.75 |
| U-NII-8 | 802.11ax/be | 80 | 11.75 | 11.75 |
|  |  | 160 | 14.75 | 14.75 |
|  | 802.11be | 320 | 17.00 | 17.25 |

## 6. Remarks and comments

1. Only the plots for the test positions with the highest measured SAR/PD per band/mode are included in Annex $C$

## 7. Test Verdicts summary

The statement of conformity to applicable standards in the table below are based on the measured values, without taking into account the measurement uncertainties.

| Standard | Band | Highest Reported PS $_{\text {tot }}$ avg $\left[\mathrm{W} / \mathrm{m}^{2}\right] 4 \mathrm{~cm}^{2}$ | Verdict |
| :---: | :---: | :---: | :---: |
| $802.11 \mathrm{ax} / \mathrm{be}$ | 6.2 GHz | 9.90 | Pass |
| $802.11 \mathrm{ax} / \mathrm{be}$ | 6.5 GHz | 3.52 | Pass |
| $802.11 \mathrm{ax} / \mathrm{be}$ | 6.7 GHz | 8.57 | Pass |
| $802.11 \mathrm{ax} / \mathrm{be}$ | 7.0 GHz | 9.30 | Pass |


| Standard | Band | Highest Reported SAR [W/kg] | Verdict |
| :---: | :---: | :---: | :---: |
| $802.11 \mathrm{ax} / \mathrm{be}$ | 6.2 GHz | 0.79 | Pass |
| $802.11 \mathrm{ax} / \mathrm{be}$ | 6.5 GHz | 0.25 | Pass |
| $802.11 \mathrm{ax} / \mathrm{be}$ | 6.7 GHz | 0.79 | Pass |
| $802.11 \mathrm{ax} / \mathrm{be}$ | 7.0 GHz | 0.62 | Pass |

P: Pass
F: Fail
NM: Not Measured
NA: Not Applicable

According to the FCC OET KDB 690783 D01, this is the summary of the values for the Grant Listing:

| Highest Reported SAR (1g) (W/kg) |  |  |
| :---: | :---: | :---: |
| Exposure Condition | Equipment Class |  |
|  | DSS | U-NII |
| Body Worn | 0.31 | 0.79 |
| Simultaneous Tx | Sum-SAR: 0.95 | Sum-SAR: 0.95 |
|  | SPLSR: NA | SPLSR: NA |

Considering the results of the performed test according to FCC 47CFR Part 2.1093 the item under test is IN COMPLIANCE with the requested specifications specified in Section1. Standards, reference documents and applicable test methods

## 8. Document Revision History

| Revision \# | Modified by | Revision Details |
| :---: | :--- | :--- |
| Rev. 00 | Y.HADDAD | First Issue |

## Annex A. PD Test \& System Description

## A. 1 Power Density Definition

The power density for an electromagnetic field represents the rate of energy transfer per unit area.
The local power density (i.e. Poynting vector) at a given spatial point is deduced from electromagnetic fields by the following formula:

$$
\overrightarrow{P_{\text {local }}}=\frac{1}{2} \operatorname{Re}\left(\vec{E} \times \vec{H}^{*}\right)
$$

Where $\vec{E}$ is the complex electric field peak phasor and $\vec{H}^{*}$ is the complex conjugate magnetic field peak phasor. This power density is also called "single-point" or "spot power density". Considering that the FCC's Maximum Permissible Exposure (MPE) limit is applicable on the average power density inside $1 \mathrm{~cm}^{2}$ area, the single point power densities in the evaluation plane should be averaged inside the $1 \mathrm{~cm}^{2}$ area.

## A. 2 SPEAG free space Measurement System

## A.2.1 Measurement Setup

The DASY6 system for performing compliance tests consists of the following items:

$\checkmark$ A standard high precision 6-axis robot (Staübli TX/RX family) with controller, teach pendant and software. It includes an arm extension for accommodating the data acquisition electronics (DAE)
$\checkmark$ An mm-wave E-field probe optimized and calibrated for the targeted measurements.
$\checkmark$ A data acquisition electronics (DAE) which performs the signal amplification, signal multiplexing, AD-conversion, offset measurements, mechanical surface detection, collision detection, etc. The signal is optically transmitted to the EOC.
$\checkmark$ The Electro-optical Converter (EOC) performs the conversion from optical to electrical signals for the digital communication to the DAE. The EOC signal is transmitted to the measurement server.
$\checkmark$ The function of the measurement server is to perform the time critical tasks such as signal filtering, control of the robot operation and fast movements interrupts.
$\checkmark$ The Light Beam used is for probe alignment. This improves the (absolute) accuracy of the probe positioning.
$\checkmark$ A computer running Windows professional operating system and the cDASY6 software.
$\checkmark$ Remote control and teach pendant as well as additional circuitry for robot safety such as warning lamps, etc.

## A.2.2 E-Field Measurement Probe

The probe consists of two dipoles ( 0.8 mm length) optimally arranged with different angles ( $\gamma_{1}$ and $\gamma_{2}$ ) to obtain pseudovector information, printed on glass substrate protected by high density foam that allows low perturbation of the measured field.
Three or more measurements are taken for different probe rotational angles, deriving the amplitude and polarization information.
The probe's characteristics are:

| Frequency Range | $750 \mathrm{MHz}-110 \mathrm{GHz}$ |
| :--- | :---: |
| Length | 320 mm |
| Probe tip external diameter | 8 mm |
| Probe's two dipoles length | Quartz $0.9 \times 20 \times 0.111 \mathrm{~mm}$ <br> $(\varepsilon r=3.8)$ |
| Probe's substrate | 1.5 mm |
| Distance between diode sensors <br> and probe's tip | $\pm 0.6 \mathrm{~dB}$ |
| Axial Isotropy | $3000 \mathrm{~V} / \mathrm{m}$ |
| Maximum operating E-field | $5 \mathrm{~V} / \mathrm{m} @ 60 \mathrm{GHz}$ |
| Lower E-field detection threshold | 0.11 mm |
| Minimum Mechanical separation <br> between probe tip and a Surface | Diode Sensor |
| Calibration reference point |  |



## A.2.3 Worst Case Linearization Error

For continuously transmitting signals ( $100 \%$ duty cycle), the worst case linearization error is given by the difference between non linearized voltage and linearized voltage using CW parameters. The error is increasing with the voltage levels. In our particular case, the measured voltages averaged over the signal period are below 1 mV . We use 1 mV in the below calculation to have the worst case condition. The signal PAR (Peak to Average Ratio) is 6dB and the diode compression point 100 mV .

The maximum voltage through the diode is given by:

$$
\begin{gathered}
\text { vpeak }=\text { vmeas avg } \times \text { PARlinear } \\
\text { vpeak }=1 * 4=4 \mathrm{mV}
\end{gathered}
$$

The linearized voltage using CW parameter is given by:

$$
\begin{gathered}
\text { vlin peak }=\text { vpeak }+\frac{v_{\text {peak }}^{2}}{\text { diode compression point }} \\
\qquad \text { vlin peak }=4+\frac{4^{2}}{100}=4.16 \mathrm{mV}
\end{gathered}
$$

The worst case linearization error is:

$$
\text { lin error }=\frac{\text { vlin peak }}{\text { v peak }}=\frac{4.16}{4}=1.04=4 \%
$$

## A.2.4 Data Evaluation

## A.2.4.1 Scan

The scan involves the measurement of two planes with three different probe rotations. The grid steps are optimized by the software based on the test frequency. The location of the lowest measurement plane is defined by the distance of first measurement layer from device under test (DUT) entered by the user. The DUT location settings can be used to offset the center of the grid.

## A.2.4.2 Total Field and Power Flux Density Reconstruction

Computation of the power density in general requires knowledge of the electric ( $\mathrm{E}-$ ) and magnetic ( $\mathrm{H}-$ ) field amplitudes and phases in the plane of incidence. Reconstruction of these quantities from pseudo-vector E-field measurements is feasible, as they are constrained by Maxwell's equations.
The reconstruction algorithm developed by the system manufacturer, together with the ability of the probe to measure extremely close to the source without perturbing the field, permits reconstruction of the E - and H -fields, as well as of the power density, on measurement planes located as near as 0.11 mm away in the frequency band of 60 GHz .

The average of the reconstructed power density is evaluated over a circular area in each measurement plane. The area of the circle is defined by the user; the default is $1 \mathrm{~cm}^{2}$.

## A. 3 System Check

The system performance check verifies that the system operates within its specifications. It is recommended that the system performance check be performed prior to any usage of the system in order to guarantee reproducible results. The system performance check uses normal E-field measurements in a simplified setup with a well characterized source. This setup was selected to give a high sensitivity to all parameters that might fail or vary over time. The system check does not intend to replace the calibration of the components, but indicates situations where the system uncertainty is exceeded due to drift or failure.
In the simplified setup for system check, the EUT is replaced by a calibrated source and the power source is replaced by a controlled continuous wave generated by a signal generator. The calibrated source must be placed at the correct distance from the E-field probe according to the calibration certificate.


First, the power meter is connected to the output of the signal generator to measure the forward power at the location of the connector to the system check source. The signal generator is adjusted for the desired forward power to match the system check source calibration setup at the connector as read by power meter. Then the power meter is replaced by the system check source.


The output power on the reference source is set to $10.0 \mathrm{dBm}(10 \mathrm{~mW})$ and the measurement results $\mathrm{E}, \mathrm{H}$ and Avg PD are compared with the Numerical modeling.

## A. 4 Test Equipment List

SAR system \#4

| ID \# | Device | Type/Model | Serial Number | Manufacturer | Cal. Date | Cal. Due Date |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $002-014$ | E-Field probe <br> $750 M H z-110 G H z$ | EUmmWV3 | 9594 | SPEAG | $2022-09-20$ | $2023-09-20$ |
| $003-016$ | Data Acquisition <br> Electronics | DAEip | 1705 | SPEAG | $2023-04-18$ | $2024-04-18$ |
| $004-000$ | 6-axis Robot | TX90 XL | F11/5JL2A1/A/01 | STAÜBLI | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ |
| $004-001$ | Robot Controller | CS8C | F11/5JL2A1/C/01 | STAÜBLI | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ |
| $004-005$ | Measurement Server | DASY6 <br> P/N: SE UMS 028 BB | - | SPEAG | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ |
| $004-004$ | Light Beam Unit | SE UKS 030 AA | 1030 | Di-soric | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ |
| $003-002$ | 5G Phantom | mmWave | NA | SPEAG | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ |
| $003-006$ | Measurement <br> Software | DASYmmW v3.0 | $9-5 E D 1 A C 01$ | SPEAG | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ |
| $004-010$ | Laptop Holder | P/N SM LH1 001 CD | - | SPEAG | $\mathrm{n} / \mathrm{a}$ | $\mathrm{n} / \mathrm{a}$ |

Shared equipment

| ID \# | Device | Type/Model | Serial Number | Manufacture <br> $r$ | Cal. Date | Cal. Due Date |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $017-001$ | USB Power Sensor | NRP-Z57 | 101486 | R\&S | $2022-03-15$ | $2024-03-15$ |
| $008-025$ | USB Power Sensor | NRP-Z57 | 101280 | R\&S | $2022-04-22$ | $2024-04-22$ |
| $151-000$ | USB Power Sensor | NRP-Z58 | 100972 | R\&S | $2022-03-29$ | $2024-03-29$ |
| $008-025$ | USB Power Sensor | NRP-Z57 | 101280 | R\&S | $2022-04-22$ | $2024-04-22$ |
| $077-000$ | Coupler | CD0.5-8-20-30 | $1251-002$ | Amd-group | $2023-02-20$ | $2024-02-20$ |
| $079-001$ | RF Cable | ST-18/SMAm/SMAm/48 | - |  <br> Suhner | $2023-02-20$ | $2024-02-20$ |
| $078-000$ | RF Cable | ST-18/SMAm/SMAm/48 | - |  <br> Suhner | $2023-02-20$ | $2024-02-20$ |
| $141-000$ | USB Power Sensor | NRP-Z81 | 104381 | R\&S | $2022-05-18$ | $2024-05-18$ |
| $327-000$ | Temp \& Humidity <br> Logger | RA32E-TH1-RAS | RA32-F0DED9 | AVTECH | $2023-07-12$ | $2025-07-12$ |
| $129-000$ | Signal Generator | SMB100A | 178212 | R\&S | $2022-12-19$ | $2024-12-19$ |
| $198-000$ | 0.8-21GHz RF <br> amplifier | TVA-82-213A+ | 2004003 | Mini-Circuits | $2023-02-20$ | $2024-02-20$ |
| $008-081$ | Horn reference <br> antenna | PE9859/SF-15 | - | PAsternack | NA | NA |
| $458-000$ | Measurement <br> Software | SARA V2.3 | NA | Intel | NA | NA |

## A. 5 Measurement Uncertainty Evaluation

The system uncertainty evaluation is shown in the table below with a coverage factor of $k=2$ to indicate a $95 \%$ level of confidence:

Table 1: DASY6 Uncertainty Budget in Compliance with IEC/IEEE 63195-1 for the cases indicated in the REFERENCE TABLE

| Error Description | Uncertainty Value ( $\pm \mathrm{dB}$ ) | Probability Distribution | Div. | (c) | Std. Unc. $( \pm \mathrm{dB})$ | $\begin{aligned} & \left(v_{i}\right) \\ & \text { Veff } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Measurement System |  |  |  |  |  |  |
| Probe calibration Hemispherical Isotropy Linearity <br> System Detection Limits | 0.49 | N | 1 | 1 | 0.49 | $\infty$ |
|  | 0.50 | R | $\sqrt{3}$ | 1 | 0.29 | $\infty$ |
|  | 0.20 | R | $\sqrt{ } 3$ | 1 | 0.12 | $\infty$ |
|  | 0.04 | R | $\sqrt{3}$ | 1 | 0.02 | $\infty$ |
| Data acquisition <br> Field reconstruction Probe Positioning Repeatability | 0.03 | N | 1 | 1 | 0.03 | $\infty$ |
|  | 0.60 | R | $\sqrt{3}$ | 1 | 0.35 | $\infty$ |
|  | 0.04 | R | $\sqrt{ } 3$ | 1 | 0.02 | $\infty$ |
| Probe Positioning offset Amplitude and Phase Noise | 0.30 | R | $\sqrt{3}$ | 1 | 0.17 | $\infty$ |
|  | 0.04 | R | $\sqrt{3}$ | 1 | 0.02 | $\infty$ |
| Spatial Averaging | 0.1 | R | $\sqrt{3}$ | 1 | 0.06 | $\infty$ |
| Frequency Response | 0.2 | R | $\sqrt{ } 3$ | 1 | 0.12 | $\infty$ |
| Test Sample Related |  |  |  |  |  |  |
| Power Drift <br> Modulation response | 0.21 | R | $\sqrt{ } 3$ | 1 | 0.12 | $\infty$ |
|  | 0.40 | R | $\sqrt{3}$ | 1 | 0.23 | $\infty$ |
| Device holder influence RF Ambient Noise RF Ambient Reflections | 0.1 | R | $\sqrt{ } 3$ | 1 | 0.06 | $\infty$ |
|  | 0.04 | R | $\sqrt{3}$ | 1 | 0.02 | $\infty$ |
|  | 0.04 | R | $\sqrt{3}$ | 1 | 0.02 | $\infty$ |
| Combined Std. Uncertaintv <br> Expanded Std. Uncertainty 95\% |  |  |  |  | 0.76 dB | $\infty$ |
|  |  |  |  |  | 1.53 dB |  |

## A. 6 RF Exposure Limits

Power density assessments have been made in line with the requirements of FCC 47CFR Part 2.1093, in particular chapter 1.1310 specifying the MPE limits, on the limitation of exposure of the general population / uncontrolled exposure for portable devices.

| Exposure Type | Power density (S) |
| :--- | :---: |
| Limits for Occupational/Controlled Exposure. $50.0 \mathrm{~W} / \mathrm{m}^{2}$ <br> $1.5 \mathrm{GHz}-100 \mathrm{GHz}$ $10.0 \mathrm{~W} / \mathrm{m}^{2}$ <br> Limits for General Population/ Uncontrolled Exposure. <br> $1.5 \mathrm{GHz}-100 \mathrm{GHz}$  l |  |

## Annex B. SAR Test \& System Description

## B. 1 SAR Definition

Specific Absorption rate is defined as the time derivative of the incremental energy (dW) absorbed by (dissipated in) and incremental mass (dm) contained in a volume element ( dV ) of a given density ( $\rho$ ).

$$
S A R=\frac{d}{d t} \cdot\left(\frac{d W}{d m}\right)=\frac{d}{d t} \cdot\left(\frac{d W}{\rho \cdot d V}\right)
$$

SAR is expressed in units of watts per kilogram (W/kg). SAR can be related to the electric field at a point by

$$
S A R=\frac{\sigma|E|^{2}}{\rho}
$$

Where:
$\sigma=$ Conductivity of the tissue ( $\mathrm{S} / \mathrm{m}$ )
$\rho=$ Mass density of the tissue (kg/m3)
$E=R M S$ electric field strength $(\mathrm{V} / \mathrm{m})$

## B. 2 SPEAG SAR Measurement System

## B.2.1 SAR Measurement Setup

The DASY6 system for performing compliance tests consists of the following items:

$\checkmark$ A standard high precision 6-axis robot (Staübli TX/RX family) with controller, teach pendant and software. It includes an arm extension for accommodating the data acquisition electronics (DAE)
$\checkmark$ An isotropic field probe optimized and calibrated for the targeted measurements.
$\checkmark$ A data acquisition electronics (DAE) which performs the signal amplification, signal multiplexing, AD-conversion, offset measurements, mechanical surface detection, collision detection, etc. The signal is optically transmitted to the EOC.
$\checkmark$ The Electro-optical Converter (EOC) performs the conversion from optical to electrical signals for the digital communication to the DAE. The EOC signal is transmitted to the measurement server.
$\checkmark$ The function of the measurement server is to perform the time critical tasks such as signal filtering, control of the robot operation and fast movements interrupts.
$\checkmark$ The Light Beam used is for probe alignment. This improves the (absolute) accuracy of the probe positioning.
$\checkmark$ A computer running Windows professional operating system and the DASY6 software.
$\checkmark$ Remote control and teach pendant as well as additional circuitry for robot safety such as warning lamps, etc.
$\checkmark$ The phantom, the device holder and other accessories according to the targeted measurement.
$\checkmark$ MAIA is a hardware interface (Antenna) used to evaluate the modulation and audio interference characteristics of RF signals.
$\checkmark \quad$ ANT is an ultra-wideband antenna for use with the base station simulators over 698 MHz to 6 GHz for SAR cellular testing (not used for WLAN testing).
$\checkmark$ The base station simulator is an equipment used for SAR cellular tests in order to emulate the cellular signals characteristics and behavior between a regular base station and the equipment under test.
$\checkmark$ Tissue simulating liquid.
$\checkmark$ System Validation dipoles.
$\checkmark$ Network emulator or RF test tool

## B.2.2 E-Field Measurement Probe

The probe is constructed using three orthogonal dipole sensors arranged on an interlocking, triangular prism core. The probe has built-in shielding against static charges and is contained within a PEEK cylindrical enclosure material at the tip.


The probe's characteristics are:

| Frequency Range | $30 \mathrm{MHz}-10 \mathrm{GHz}$ |
| :--- | :---: |
| Length | 337 mm |
| Probe tip external diameter | 2.5 mm |
| Typical distance between dipoles and the probe tip | 1 mm |
| Axial Isotropy (in human-equivalent liquids) | $\pm 0.3 \mathrm{~dB}$ |
| Hemispherical Isotropy (in human-equivalent liquids) | $\pm 0.5 \mathrm{~dB}$ |
| Linearity | $\pm 0.2 \mathrm{~dB}$ |
| Maximum operating SAR | $100 \mathrm{~W} / \mathrm{kg}$ |
| Lower SAR detection threshold | $0.001 \mathrm{~W} / \mathrm{kg}$ |

## B.2.3 Flat Phantom

Phantom for compliance testing of handheld and body-mounted wireless devices in the frequency range of 30 MHz to 6 GHz . ELI is fully compatible with the IEC 62209-2 standard and all known tissue simulating liquids. ELI has been optimized regarding its performance and can be integrated into our standard phantom tables. A cover prevents evaporation of the liquid. Reference markings on the phantom allow installation of the complete setup, including all predefined phantom positions and measurement grids, by teaching three points. The phantom is compatible with all SPEAG dosimetric probes and dipoles.
The phantom's characteristics are:

| Material | Vinylester, glass fiber reinforced (VE-GF) |
| :--- | :--- |
| Shell thickness | $2 \mathrm{~mm} \pm 0.2 \mathrm{~mm}$ |
| Filling volume | 30 Liters approx. |
| Dimensions | Major axis: $600 \mathrm{~mm} /$ Minor axis: 400 mm |



## B.2.4 Device Positioner

The SAR in the phantom is approximately inversely proportional to the square of the distance between the source and the liquid surface. For a source at 5 mm distance, a positioning uncertainty of 0.5 mm would produce a SAR uncertainty of $20 \%$. Accurate device positioning is therefore crucial for accurate and repeatable measurements. The positions in which the devices must be measured are defined by the standards.


The DASY device holder is designed to cope with the different positions given in the standard. It has two scales for device rotation (with respect to the body axis) and device inclination (with respect to the line between the ear reference points). The rotation center for both scales is the ear reference point (ERP). Thus the device needs no repositioning when changing the angles.
The DASY device holder is constructed of low-loss POM material having the following dielectric parameters: relative permittivity $\varepsilon=3$ and loss tangent $\delta=0.02$. The amount of dielectric material has been reduced in the closest vicinity of the device, since measurements have suggested that the influence of the clamp on the test results could thus be lowered.

A simple but effective and easy-to-use extension for the Mounting Device; facilitates testing of larger devices according to IEC 62209-2 (e.g., laptops, cameras, etc.); lightweight and fits easily on the upper part of the Mounting Device in place of the phone positioner. The extension is fully compatible with the Twin SAM, ELI and other Flat Phantoms.

## B. 3 Data Evaluation

## - Power Reference measurement

The robot measures the E field in a specified reference position that can be either the selected section's grid reference point or a user point in this section at 4 mm of the inner surface of the phantom, 2 mm for frequencies above 3 GHz .

## - Area Scan

Measurement procedures for evaluating SAR from wireless handsets typically start with a coarse measurement grid to determine the approximate location of the local peak SAR values. This is known as the area-scan procedure. The SAR distribution is scanned along the inside surface of one side of the phantom head, at least for an area larger than the projection of the handset and antenna. The distance between the measured points and phantom surface should be less than 8 mm , and should remain constant (with variation less than $\pm 1 \mathrm{~mm}$ ) during the entire scan in order to determine the locations of the local peak SAR with sufficient accuracy. The angle between the probe axis and the surface normal line is recommended but not required to be less than $30^{\circ}$. If this angle is larger than $30^{\circ}$ and the closest point on the probe-tip housing to the phantom surface is closer than a probe diameter, the boundary effect may become larger and polarization dependent. This additional uncertainty needs to be analyzed and accounted for. To achieve this, modified test procedures and additional uncertainty analyses not described in this recommended practice may be required. The measurement and interpolation point spacing should be chosen such as to allow identification of the local peak locations to within one-half of the linear dimension of a side of the zoom-scan volume. Because a local peak having specific amplitude and steep gradients may produce a lower peak spatial-average SAR compared to peaks with slightly lower amplitude and less steep gradients, it is necessary to evaluate these other peaks as well. However, since the spatial gradients of local SAR peaks are a function of the wavelength inside the tissue-equivalent liquid and the incident magnetic field strength, it is not necessary to evaluate local peaks that are less than 2 dB or more below the global maximum peak. Two-dimensional spline algorithms (Brishoual et al. 2001; Press et al., 1996) are typically used to determine the peaks and gradients within the scanned area. If a peak is found at a distance from the scan border of less than one-half the edge dimension of the desired 1 g or 10 g cube, the measurement area should be enlarged if possible.

## - Zoom Scan

To evaluate the peak spatial-average SAR values for 1 g or 10 g cubes, fine resolution volume scans, called zoom scans, are performed at the peak SAR locations identified during the area scan. The minimum zoom scan volume size should extend at least 1.5 times the edge dimension of a 1 g cube in all directions from the center of the scan volume, for both 1 g and 10 g peak spatial-average SAR evaluations. Along the phantom curved surfaces, the front face of the volume facing the tissue/liquid interface conforms to the curved boundary, to ensure that all SAR peaks are captured. The back face should be equally distorted to maintain the correct averaging mass. The flatness and orientation of the four side faces are unchanged from that of a cube whose orientation is within $\pm 30^{\circ}$ of the line normal to the phantom at the center of the cube face next to the phantom surface. The peak local SAR locations that were determined in the area scan (interpolated values) should be used for the centers of the zoom scans. If a scan volume cannot be centered due to proximity of a phantom shape feature, the probe should be tilted to allow scan volume enlargement. If probe tilt is not feasible, the zoom-scan origin may be shifted, but not by more than half of the 1 g or 10 g cube edge dimension.
After the zoom-scan measurement, extrapolations from the closest measured points to the surface, for example along lines parallel to the zoom-scan centerline, and interpolations to a finer resolution between all measured and extrapolated points are performed. Extrapolation algorithm considerations are described in 6.5.3, and 3-D spline methods (Brishoual et al., 2001; Kreyszig, 1983; Press et al., 1996) can be used for interpolation. The peak spatial-average SAR is finally determined by a numerical averaging of the local SAR values in the interpolation grid, using for example a trapezoidal algorithm for the integration (averaging).
In some areas of the phantom, such as the jaw and upper head regions, the angle of the probe with respect to the line normal to the surface may be relatively large, e.g., greater than $\pm 30^{\circ}$, which could increase the boundary effect error to a larger level. In these cases, during the zoom scan a change in the orientation of the probe, the phantom, or both is recommended but not required for the duration of the zoom scan, so that the angle between the probe axis and the line normal to the surface is within $30^{\circ}$ for all measurement points.

## - Power Drift measurement

The robot re-measures the E-Field in the same reference location measured at the Power Reference. The drift measurement gives the field difference in dB from the first to the last reference reading. This allows a user to monitor the power drift of the device under test that must remain within a maximum variation of $\pm 5 \%$.

## - Post-processing

The procedure for spatial peak SAR evaluation has been implemented according to the IEEE1528 and IEC 62209-1/2 standards. It can be conducted for 1 g and 10 g .

The software allows evaluations that combine measured data and robot positions, such as:
$\checkmark$ Maximum search
$\checkmark$ Extrapolation
$\checkmark$ Boundary correction
$\checkmark$ Peak search for averaged SAR
Interpolation between the measured points is performed when the resolution of the grid is not fine enough to compute the average SAR over a given mass.

Extrapolation routines are used to obtain SAR values between the lowest measurement points and the inner phantom surface. The extrapolation is determined by the surface detection distance and the probe sensor offset. Several measurements at different distances are necessary for the extrapolation.

## B. 4 System and Liquid Check

## B.4.1 System Check

The system performance check verifies that the system operates within its specifications. System and operator errors can be detected and corrected. It is recommended that the system performance check be performed prior to any usage of the system in order to guarantee reproducible results.

The system performance check uses normal SAR measurements in a simplified setup with a well characterized source. This setup was selected to give a high sensitivity to all parameters that might fail or vary over time. The system check does not intend to replace the calibration of the components, but indicates situations where the system uncertainty is exceeded due to drift or failure.

In the simplified setup for system check, the EUT is replaced by a calibrated dipole and the power source is replaced by a controlled continuous wave generated by a signal generator. The calibrated dipole must be placed beneath the flat phantom section of the phantom at the correct distance.


The equipment setup is shown below:
$\checkmark$ Signal Generator
$\checkmark$ Amplifier
$\checkmark$ Directional coupler
$\checkmark$ Power meter
$\checkmark$ Calibrated dipole

First, the power meter PM1 (including attenuator Att1) is connected to the cable to measure the forward power at the location of the connector (x) to the system check source. The signal generator is adjusted for the desired forward power at the connector as read by power meter PM1 after attenuation Att1 and also as coupled through Att2 to PM2. After connecting the cable to the source, the signal generator is readjusted for the same reading at power meter PM2.

SAR results are normalized to a forward power of 1 W to compare the values with the calibration reports results as described at IEC/IEEE 62209-1528:2020 standards.

## B.4.2 Liquid Check

The dielectric parameters check is done prior to the use of the tissue simulating liquid. The verification is made by comparing the relative permittivity and conductivity to the values recommended by the applicable standards.
The liquid verification was performed using the following test setup:

```
V VNA (Vector Network Analyzer)
\checkmark Open-Short-Load calibration kit
\checkmark ~ R F ~ C a b l e
\checkmark ~ O p e n - E n d e d ~ C o a x i a l ~ p r o b e
\checkmark ~ D A K ~ s o f t w a r e ~ t o o l
\checkmark ~ S A R ~ L i q u i d
\checkmark ~ D e - i o n i z e d ~ w a t e r ~
\checkmark ~ T h e r m o m e t e r ~
```

These are the target dielectric properties of the tissue-equivalent liquid material according to the manufacturer's datasheet:

| Frequency | Head Tissue Simulating <br> Media |  |
| :---: | :---: | :---: |
| $(\mathrm{MHz})$ | $\varepsilon_{\mathrm{r}}(\mathrm{F} / \mathrm{m})$ | $\sigma(\mathrm{S} / \mathrm{m})$ |
| 6000 | 35.07 | 5.48 |
| 6500 | 34.46 | 6.07 |
| 7000 | 33.88 | 6.65 |

( $\varepsilon_{\mathrm{r}}=$ relative permittivity, $\sigma=$ conductivity and $\rho=1000 \mathrm{~kg} / \mathrm{m} 3$ )

The measurement system implements a SAR error compensation algorithm as documented IEC/IEEE 62209-1528:2020 to automatically compensate the measured SAR results for deviations between the measured and required tissue dielectric parameters (applied to only scale up the measured SAR, and not downward) so, according to FCC OET KDB 865664 D01, the tolerance for $\varepsilon_{r}$ and $\sigma$ may be relaxed to $\pm 10 \%$.

## B. 5 Test Equipment List

SAR system \#2

| ID \# | Device | Type/Model | Serial Number | Manufacturer | Cal. Date | Cal. Due Date |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $002-000$ | 6-Axis Robot | TX60 Lspeag | F16/55FXA1/A/01 | STAÜBLI | NA | NA |
| $002-001$ | Robot Controller | CS8C | F16/55FXA1/C/01 | STAÜBLI | NA | NA |
| $002-002$ | Measurement Server | DASY6 | 1489 | SPEAG | NA |  |
| $002-003$ | Electro Optical Converter | EOC60 | 1098 | SPEAG | NA | NA |
| $002-004$ | Light Beam Unit | SE UKS 030 AA | N/A | Di-soric | NA | NA |
| $002-005 ~$ | Oval Flat Phantom | ELI V8.0 | 2048 | SPEAG | NA | NA |
| $002-006$ | Laptop Holder |  | N/A | SPEAG | NA | NA |
| $002-007$ | Measurement Software | DASY6 v16.0.0.116 | $9-5 D E E 27 C 2$ | SPEAG | NA | NA |
| $001-017$ | Data Acquisition Electronics | DAEip | 1703 | SPEAG | $2023-04-18$ | $2024-04-18$ |
| $086-000$ | Dosimetric E-Field probe | EX3DV4 | 7455 | SPEAG | $2023-03-16$ | $2024-03-16$ |

Shared equipment

| ID \# | Device | Type/Model | Serial Number | Manufacturer | Cal. Date | Cal. Due Date |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $123-000$ | USB Power Sensor | NRP-Z81 | 102278 | R\&S | $2023-04-18$ | $2025-04-18$ |
| $124-000$ | USB Power Sensor | NRP-Z81 | 102279 | R\&S | $2023-04-18$ | $2025-04-18$ |
| $077-000$ | Coupler | CD0.5-8-20-30 | $1251-002$ | Amd-group | $2023-02-20$ | $2024-02-20$ |
| $079-001$ | RF Cable | CBL-0.5M- <br> SMSM | 226527 | Mini-Circuits | $2023-02-20$ | $2024-02-20$ |
| $167-001$ | RF Cable | CBL-2M-SMSM+ | 233846 | Mini-Circuits | $2023-02-20$ | $2024-02-20$ |
| $198-000$ | $0.8-21 G H z ~ R F ~$ <br> amplifier | TVA-82-213A+ | 2004003 | Mini-Circuits | $2023-02-20$ | $2024-02-20$ |
| $129-000$ | Signal Generator <br> $094-000$ | Temp \& Humidity <br> Logger | RA32E-TH1-RAS | RA32-FBFD5A | AVTECH | $2023-02-20$ |
| $099-000$ | Liquid measurement <br> SW | DAK-3.5 <br> V3.0.2.3 | $9-2687 B 491$ | SPEAG | NA | NA |
| $369-000$ | Dielectric Probe Kit | DAK-3.5 | 1309 | SPEAG | $2023-03-13$ | $2025-03-13$ |
| $089-000$ | Vector <br> Reflectometer R140 | PLANAR R140 | 0190616 | Copper <br> mountain | $2021-09-02$ | $2023-09-02$ |
| $097-000$ | System Validation <br> Dipole 7000MHz | D7GHzV2 | 1008 | SPEAG | $2023-08-24$ | $2024-08-24$ |
| $458-000$ | Measurement <br> Software | SARA V2.3 | NA | Intel | NA | NA |

## B.5.1 Tissue Simulant Liquid

| TSL | Manufacturer / Model | Freq Range <br> $(\mathrm{MHz})$ | Main Ingredients |
| :---: | :---: | :---: | :---: |
| Head WideBand | SPEAG HBBL600-10000 <br> Batch 210331-1 | $600-10000$ | Ethanediol, Sodium petroleum sulfonate, <br> Hexylene Glycol / 2-Methyl-pentane-2.4- <br> diol, Alkoxylated alcohol |

## B. 6 Measurement Uncertainty Evaluation

The system uncertainty evaluation is shown in the table below with a coverage factor of $k=2$ to indicate a $95 \%$ level of confidence:

| SPEAG DASY6 Uncertainty Budget According to IEC/IEEE 62209-1528 ( 6 GHz - 10 GHz ) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Symbol | Error Description | Uncert. Value | Prob Dist. | Div. | $\begin{array}{\|l} \hline \text { (ci) } \\ 1 \mathrm{~g} \\ \hline \end{array}$ | $\begin{aligned} & \text { (ci) } \\ & 10 \mathrm{~g} \end{aligned}$ | Std Unc. <br> (1g) | Std Unc. $(10 \mathrm{~g})$ |
| Measurement System Errors |  |  |  |  |  |  |  |  |
| CF | Probe Calibration | $\pm 18.6$ \% | N | 2 | 1 | 1 | $\pm 9.3$ \% | $\pm 9.3$ \% |
| CFonft | Probe Calibration Drift | $\pm 1.0 \%$ | N | 1 | 1 | 1 | $\pm 1.0$ \% | $\pm 1.0$ \% |
| LIN | Probe Linearity | $\pm 4.7$ \% | R | $\sqrt{3}$ | 1 | 1 | $\pm 2.7$ \% | $\pm 2.7$ \% |
| BBS | Broadband Signal | $\pm 3.0 \%$ | N | 2 | 1 | 1 | $\pm 1.5$ \% | $\pm 1.5$ \% |
| ISO | Axial Isotropy | $\pm 4.7$ \% | R | $\sqrt{3}$ | 0.5 | 0.5 | $\pm 1.4$ \% | $\pm 1.4$ \% |
| ISO | Hemspherical Isotropy | $\pm 9.6$ \% | R | $\sqrt{3}$ | 0.5 | 0.5 | $\pm 2.8$ \% | $\pm 2.8$ \% |
| DAE | Data Acquisition | $\pm 0.3$ \% | N | 1 | 1 | 1 | $\pm 0.3$ \% | $\pm 0.3$ \% |
| AMB | RF Ambient | $\pm 1.8$ \% | N | 1 | 1 | 1 | $\pm 1.8$ \% | $\pm 1.8$ \% |
| $\begin{array}{\|l\|l} \Delta y s \\ s y s \end{array}$ | Probe Positioning | $\pm 0.2$ \% | N | 1 | 0.33 | 0.33 | $\pm 0.1$ \% | $\pm 0.1$ \% |
| DAT | Data Processing | $\pm 3.5$ \% | N | 1 | 1 | 1 | $\pm 3.5$ \% | $\pm 3.5$ \% |

## Phantom and Device Errors

| LIQ $(\sigma)$ | Conductivity (meas.) DAK | $\pm 2.5$ \% | N | 1 | 0.78 | 0.71 | $\pm 2.0$ \% | $\pm 1.8$ \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LIQ ( $\mathrm{T}_{\mathrm{\sigma}}$ ) | Conductivity (temp.) 88 | $\pm 2.4$ \% | R | $\sqrt{3}$ | 0.78 | 0.71 | $\pm 1.1$ \% | $\pm 1.0 \%$ |
| EPS | Phantom Permittivity | $\pm 14.0$ \% | R | $\sqrt{3}$ | 0.5 | 0.5 | $\pm 4.0$ \% | $\pm 4.0$ \% |
| DAS | Distance DUT - TSL | $\pm 2.0$ \% | N | 1 | 2 | 2 | $\pm 4.0$ \% | $\pm 4.0$ \% |
| H | Device Holder | $\pm 3.6$ \% | N | 1 | 1 | 1 | $\pm 3.6$ \% | $\pm 3.6$ \% |
| MOD | DUT Modulationm | $\pm 2.4$ \% | R | $\sqrt{3}$ | 1 | 1 | $\pm 1.4$ \% | $\pm 1.4$ \% |
| TAS | Time-average SAR | $\pm 2.6$ \% | R | $\sqrt{3}$ | 1 | 1 | $\pm 1.5$ \% | $\pm 1.5$ \% |
| RF ${ }_{\text {dinf }}$ t | DUT drift | $\pm 5.0$ \% | N | 1 | 1 | 1 | $\pm 2.9$ \% | $\pm 2.9$ \% |

Correction to the SAR results

| $\mathrm{C}(\varepsilon, \sigma)$ | Deviation to Target | $\pm 1.9 \%$ | N | 1 | 1 | 0.84 | $\pm 1.9 \%$ | $\pm 1.6 \%$ |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{C}(\mathrm{R})$ | SAR scalingo | $\pm 0 \%$ | R | $\sqrt{ } 3$ | 1 | 1 | $\pm 0 \%$ | $\pm 0 \%$ |
| Combined Std. Uncertainty |  |  |  |  |  |  | $\pm 13.7 \%$ | $\pm 13.7 \%$ |
| Expanded STD Uncertainty |  |  |  |  |  | $\pm 27.5 \%$ | $\pm 27.3 \%$ |  |

## B. 7 RF Exposure Limits

SAR assessments have been made in line with the requirements of FCC 47CFR Part 2.1093 on the limitation of exposure of the general population / uncontrolled exposure for portable devices.

| Exposure Type | General Population / <br> Uncontrolled Environment |
| :--- | :---: |
| Peak spatial-average SAR <br> (averaged over any 1 gram of tissue) | $\mathbf{1 . 6 ~ W / k g ~}$ |
| Whole body average SAR | $\mathbf{0 . 0 8} \mathbf{~ W / k g ~}$ |
| Peak spatial-average SAR (extremities) <br> (averaged over any 10 grams of tissue) | $\mathbf{4 . 0 ~ W / k g ~}$ |

## Annex C. Test Results

The herein test results were performed by:

| Test case measurement | Test Personnel |
| :--- | :---: |
| Conducted measurement | F. Heurtematte |
| SAR/PD measurement | Y.HADDAD |

## C. 1 Test Conditions

## C.1.1 Test positions relative to the phantom

The device under test was an Intel $®$ BE200D2W card using a Tri band Electronics antenna as reference. The card was operated utilizing proprietary software (DRTU version DRTU.04696.99.0.81) and each channel was measured using a broadband power meter to determine the maximum average power.

As per the Interim Procedures for UNII 6-7GHz RF Exposure, explained in RF Exposure Policies and Procedures: TCB Workshop - October 2020, the testing has been performed on SAR following IEC/IEEE 62209-1528:2020 and then on Power Density for the highest SAR test configurations.

All sides of the antenna were tested for SAR compliance with the antenna placed at 11 mm beneath the phantom. The adjacent edges of the antenna were positioned perpendicular to the phantom.

Considering the antenna location diagrams in Annex $G$ and the test exclusions described before, the surfaces/edges to be measured for each antenna are:

| Antenna | Aux |  | Main |  |
| :---: | :--- | :--- | :--- | :--- |
| Position | $\bullet$ | Front face | $\bullet$ | Front face |
|  | $\bullet$ | Back Face | $\bullet$ | Back Face |
|  | $\bullet$ | Top edge | $\bullet$ | Top edge |
|  | $\bullet$ | Left edge | $\bullet$ | Left edge |
|  | $\bullet$ | Right edge | $\bullet$ | Right edge |

See G. 2 SAR/PD Test positions section for more information on the tested positions.

## C.1.2 Test signal, Output power and Test Frequencies

For 802.11 transmission modes the device was put into operation by using an own control software to program the test mode required to select the continuous transmission with $100 \%$ duty cycle.

The output power of the device was set to transmit at maximum power for all tests.

## C.1.3 Evaluation Exclusion and Test Reductions

The SAR Test Exclusion Threshold in FCC OET KDB 447498 can be applied to determine SAR test exclusion for adjacent edge configurations. For 100 MHz to 6 GHz and test separation distances $\leq 50 \mathrm{~mm}$, the $1-\mathrm{g}$ and $10-\mathrm{g}$ SAR test exclusion thresholds are determined by the following formula:
[(max. power of channel, including tune - up tolerance, mW$) /($ min. test separation distance, mm$)] \cdot\left[\sqrt{f_{(G H z)}}\right]$
$\leq 3.0$ for $1 g S A R$, and $\leq 7.5$ for $10 g$ extremity $S A R$
Where:

- $\mathrm{f}(\mathrm{GHz})$ is the RF channel transmit frequency in GHz
- Power and distance are rounded to the nearest mW and mm before calculation
- The result is rounded to one decimal place for comparison
- The values 3.0 and 7.5 are referred to as numeric thresholds

The test exclusions are applicable only when the minimum test separation distance is $\leq 50 \mathrm{~mm}$, and for transmission frequencies between 100 MHz and 6 GHz . When the minimum test separation distance is < 5 mm , a distance of 5 mm is applied to determine SAR test exclusion.

For test separation distances $>50 \mathrm{~mm}$, the $1-\mathrm{g}$ and $10-\mathrm{g}$ SAR test exclusion thresholds are determined using the following formulas:
$\left\langle(\right.$ Power allowed at numeric threshold for 50 mm in (1)) + (test separation distance $\left.-50 \mathrm{~mm}) \cdot\left(f_{M H Z} / 150\right)\right\rangle \mathrm{mW}$,
for 100 MHz to 1500 MHz
$\langle($ Power allowed at numeric threshold for 50 mm in (1)) + (test separation distance $-50 \mathrm{~mm}) \cdot 10)\rangle \mathrm{mW}$,
for 1500 MHz and $\leq 6 \mathrm{GHz}$

| WLAN <br> Antenna | Band <br> Name | Output power |  |  | $\begin{aligned} & -1 \\ & \hline-8 \\ & \text { ㅇ } \\ & \stackrel{\circ}{0} \end{aligned}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { 을 } \\ & \frac{\mathbf{B}}{3} \end{aligned}$ | $\underset{k}{3}$ |  |  |  |  |  |
| WLAN <br> Main | U-NII-5 | 19.00 | 79.43 | <50 | <50 | <50 | <50 | <50 |
|  | U-NII-6 | 14.75 | 29.85 | <50 | <50 | <50 | <50 | <50 |
|  | U-NII-7 | 19.00 | 79.43 | <50 | <50 | <50 | <50 | <50 |
|  | U-NII-8 | 17.00 | 50.12 | <50 | <50 | <50 | <50 | <50 |
| WLAN Aux | U-NII-5 | 19.00 | 79.43 | <50 | <50 | <50 | <50 | <50 |
|  | U-NII-6 | 14.75 | 29.85 | <50 | <50 | <50 | <50 | <50 |
|  | U-NII-7 | 19.00 | 79.43 | <50 | <50 | <50 | <50 | <50 |
|  | U-NII-8 | 17.25 | 53.09 | <50 | <50 | <50 | <50 | <50 |


| $\begin{aligned} & \text { س } \\ & 0 \\ & \tilde{N} \\ & \text { N } \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & -1 \\ & \text { 웅 } \\ & \text { M } \\ & \text { O} \end{aligned}$ |  | $\begin{aligned} & \text { } \\ & \stackrel{D}{7} \\ & \Pi \\ & \stackrel{O}{0} \\ & \stackrel{Q}{D} \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: |
| T | T | T | T | T |
| T | T | T | T | T |
| T | T | T | T | T |
| T | T | T | T | T |
| T | T | T | T | T |
| T | T | T | T | T |
| T | T | T | T | T |
| T | T | T | T | T |

T: Tested position
R: Reduced
See Annex $G$ for a more detailed explanation of the separation distance related to the platform.

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## C. 2 Conducted Power Measurements

## C.2.1 WLAN 6-7GHz (U-NII)

## C.2.1.1 6.2GHz (U-NII-5)

|  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Band | Mode | Data <br> Rate | Ch \# | Freq (MHz) | Avg Pwr (dBm) | Declared Max Power (dBm) | Avg Pwr (dBm) | Declared Max Power (dBm) |
| $\begin{aligned} & \stackrel{0}{\mathrm{O}} \\ & \frac{1}{N} \end{aligned}$ | 802.11ax20/be20 | MCSO | 1 | 5955 | $N R^{1}$ | 19.00 | $N R^{1}$ | 19.00 |
|  |  |  | 49 | 6195 |  | 19.00 |  | 19.00 |
|  |  |  | 93 | 6415 |  | 19.00 |  | 19.00 |
|  |  |  | 3 | 5965 |  | 19.00 |  | 19.00 |
|  | 802.11ax40/be40 |  | 43 | 6165 |  | 19.00 |  | 19.00 |
|  |  |  | 91 | 6405 |  | 19.00 |  | 19.00 |
|  |  |  | 7 | 5985 |  | 19.00 |  | 19.00 |
|  | 802.11ax80/be80 |  | 39 | 6145 |  | 19.00 |  | 19.00 |
|  |  |  | 87 | 6385 |  | 19.00 |  | 19.00 |
|  |  |  | 15 | 6025 | 18.91 | 19.00 | 18.95 | 19.00 |
|  | 802.11ax160/be160 |  | 47 | 6185 | 18.82 | 19.00 | 18.88 | 19.00 |
|  |  |  | 79 | 6345 | 18.93 | 19.00 | 18.90 | 19.00 |
|  | 802.11ax160/be160 |  | 15 | 6025 | 15.91 | 16.00 | 15.95 | 16.00 |
|  | MIMO |  | 79 | 6345 | 15.93 | 16.00 | 15.90 | 16.00 |
|  | 802.11be320 |  | 31 | 6105 | NR ${ }^{1}$ | 18.25 | $N R^{1}$ | 18.50 |
|  |  |  | 63 | 6265 |  | 16.25 |  | 16.25 |
|  |  |  | 95 | 6425 |  | 16.25 |  | 16.25 |

Initial test configuration

1. NR: Not Required

## C.2.1.2 6.5GHz (U-NII-6)

Initial test configuration

1. NR: Not Required

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## C.2.1.3 6.7GHz (U-NII-7)

|  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Band | Mode | Data Rate | Ch \# | Freq (MHz) | Avg Pwr (dBm) | Declared Max Power (dBm) | Avg Pwr (dBm) | Declared Max Power (dBm) |
| $\begin{aligned} & \text { op } \\ & \frac{1}{N} \end{aligned}$ | 802.11ax20/be20 | MCS0 | 117 | 6535 | $N R^{1}$ | 19.00 | $N R^{1}$ | 19.00 |
|  |  |  | 149 | 6695 |  | 19.00 |  | 19.00 |
|  |  |  | 181 | 6855 |  | 19.00 |  | 19.00 |
|  | 802.11ax40/be40 |  | 115 | 6525 |  | 19.00 |  | 19.00 |
|  |  |  | 147 | 6685 |  | 19.00 |  | 19.00 |
|  |  |  | 179 | 6845 |  | 19.00 |  | 19.00 |
|  | 802.11ax80/be80 |  | 135 | 6625 |  | 19.00 |  | 19.00 |
|  |  |  | 151 | 6705 |  | 19.00 |  | 19.00 |
|  |  |  | 167 | 6785 |  | 19.00 |  | 19.00 |
|  | 802.11ax160/be160 |  | 143 | 6665 | 18.99 | 19.00 | 18.92 | 19.00 |
|  |  |  | 175 | 6825 | 14.43 | 14.50 | 14.30 | 14.50 |
|  | 802.11 be320 |  | 127 | 6585 | $N R^{1}$ | 16.75 | $N R^{1}$ | 17.00 |
|  |  |  | 159 | 6745 |  | 17.25 |  | 17.25 |

Initial test configuration

1. NR: Not Required

## C.2.1.4 7.0GHz (U-NII-8)

|  |  |  |  |  | Main |  | Aux |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Band | Mode | Data Rate | Ch \# | Freq (MHz) | Avg Pwr (dBm) | Declared Max Power (dBm) | Avg Pwr (dBm) | Declared Max Power (dBm) |
| $\begin{aligned} & \text { on } \\ & \frac{1}{N} \end{aligned}$ | 802.11ax20/be20 | MCS0 | 185 | 6875 | $N R^{1}$ | 5.50 | NR ${ }^{1}$ | 5.50 |
|  |  |  | 209 | 6995 |  | 5.75 |  | 5.75 |
|  |  |  | 233 | 7115 |  | 0.50 |  | 0.50 |
|  | 802.11ax40/be40 |  | 187 | 6885 |  | 8.75 |  | 8.75 |
|  |  |  | 211 | 7005 |  | 8.75 |  | 8.75 |
|  |  |  | 227 | 7085 |  | 8.75 |  | 8.75 |
|  | 802.11ax80/be80 |  | 183 | 6865 |  | 11.50 |  | 11.50 |
|  |  |  | 199 | 6945 |  | 11.75 |  | 11.75 |
|  |  |  | 215 | 7025 |  | 12.00 |  | 12.00 |
|  | 802.11ax160/be160 |  | 207 | 6985 |  | 14.75 |  | 14.75 |
|  | 802.11be320 |  | 191 | 6905 | 16.65 | 17.00 | 17.12 | 17.25 |

[^0]1. NR: Not Required

## C. 3 Tissue Parameters Measurement

Head TSL

| Freq. <br> $(\mathrm{MHz})$ | Target Parameters |  | Measured TSL <br> Parameters |  | Deviation (\%) |  | Date |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\varepsilon^{\prime}(\mathrm{F} / \mathrm{m})$ | $\sigma(\mathrm{S} / \mathrm{m})$ | $\varepsilon^{\prime}(\mathrm{F} / \mathrm{m})$ | $\sigma(\mathrm{S} / \mathrm{m})$ | $\varepsilon^{\prime}$ | $\sigma$ |  |
| 7000.0 | 33.88 | 6.65 | 33.38 | 7.09 | -1.48 | 6.62 | $2023-08-28$ |

See Annex E for more details.

## C. 4 System Check Measurements

## C.4.1 E-Field

| Frequency | Signal Type | Target <br> E-field <br> $(\mathrm{V} / \mathrm{m})$ | Measured <br> E-field <br> $(\mathrm{V} / \mathrm{m})$ | Deviation <br> $(\%)$ | Date |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 6.5 GHz | Continuous <br> Wave | 60.59 | 62.08 | 2.44 | $2023-08-30$ |

The E-fields presented in the System Check Measurements table are Peak values. The target E-field value is obtained by simulation. The maximum target E-field value at 10 mm with $10 \mathrm{dBm}(10 \mathrm{~mW})$ source power is $60.59 \mathrm{~V} / \mathrm{m}$. The maximum measured E-field value at 10 mm with $10 \mathrm{dBm}(10 \mathrm{~mW})$ is $62.08 \mathrm{~V} / \mathrm{m}$.

## C.4.2 H-Field

| Frequency | Signal Type | Target <br> H-field <br> $(\mathrm{A} / \mathrm{m})$ | Measured <br> H-field <br> $(\mathrm{A} / \mathrm{m})$ | Deviation <br> $(\%)$ | Date |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 6.5 GHz | Continuous <br> Wave | 0.17 | 0.16 | -5.88 | $2023-08-30$ |

The H -fields presented in the System Check Measurements table are Peak values. The target H -field value is obtained by simulation. The maximum target H -field value at 10 mm with $10 \mathrm{dBm}(10 \mathrm{~mW})$ source power is $0.17 \mathrm{~A} / \mathrm{m}$. The maximum measured E-field value at 10 mm with $10 \mathrm{dBm}(10 \mathrm{~mW})$ is $0.16 \mathrm{~A} / \mathrm{m}$.

## C.4.3 Local Power Density

| Frequency | Signal Type | Target Local <br> Power Density <br> $(\mathrm{W} / \mathrm{m} 2)$ | Measured Local <br> Power Density <br> $(\mathrm{W} / \mathrm{m} 2)$ | Deviation <br> $(\%)$ | Date |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 6.5 GHz | Continuous <br> Wave | 5.12 | 4.98 | 4.27 | $2023-08-30$ |

The Local Power Density presented in the System Check Measurements table are Peak values. The target Local Power Density value is obtained by simulation. The maximum target Local Power Density value at 10 mm with 10 dBm ( 10 mW ) source power is $5.12 \mathrm{~W} / \mathrm{m}^{2}$. The maximum measured E -field value at 10 mm with $10 \mathrm{dBm}(10 \mathrm{~mW})$ is $4.98 \mathrm{~W} / \mathrm{m}^{2}$.

## C.4.4 Averaged Power Density

| Frequency | Signal Type | Target Spatially <br> Averaged Power <br> Density <br> (W/m2) | Measured Spatially <br> Averaged Power <br> Density <br> (W/m2) | Deviation <br> $(\%)$ | Date |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 6.5 GHz | Continuous <br> Wave | 4.93 | 4.75 | -3.65 | $2023-08-30$ |

The Spatially Averaged Power Density presented in the System Check Measurements table are Peak values. The target Spatially Averaged Power Density value is obtained by simulation. The maximum target Spatially Averaged Power Density value at 10 mm with $10 \mathrm{dBm}(10 \mathrm{~mW})$ source power is $4.93 \mathrm{~W} / \mathrm{m}^{2}$. The maximum measured Spatially Averaged Power Density value at 10 mm with $10 \mathrm{dBm}(10 \mathrm{~mW})$ is $4.75 \mathrm{~W} / \mathrm{m}^{2}$.

## C.4.5 SAR

Head Measurements

| Frequency $(\mathrm{MHz})$ | Average | Target SAR (W/kg) | Measured SAR (W/kg) | Forwarded Power (mW) | Deviation to target (\%) | Limit (\%) | Date |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7000 | 1 g | 278.0 | 300.40 | 25.10 | 8.06 | $\pm 10$ | 2023-08-28 |
|  | 10 g | 48.70 | 52.99 |  | 8.81 |  |  |
| 7000 | 1 g | 278.0 | 298.01 | 25.10 | 7.20 | $\pm 10$ | 2023-08-30 |
|  | 10 g | 48.70 | 52.99 |  | 8.81 |  |  |

## C. 5 Test Results

## C.5.1 SAR - 802.11ax/be-6.2 GHz - U-NII-5

| Mode Data Rate | $\begin{gathered} \mathrm{BW} \\ (\mathrm{MH} \\ \mathrm{z}) \end{gathered}$ | Chann el Numbe r | Freq <br> (MH <br> z) | Test position mode | Ant | Scali <br> ng <br> Fact or (dB). | Measured SAR 1 g . (W/kg) | Reported SAR 1 g (W/kg) | Measured SAR 10 g (W/kg) | Estimated epithelial PD $\left(\mathrm{W} / \mathrm{m}^{2}\right)^{*}$ |  | No Plot |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  | $\underset{2}{1 \mathrm{~cm}}$ | $4 \mathrm{~cm}^{2}$ |  |
| 802.11 ax/be MCSO | 160 | 15 | 6025 | Front face | Main | 0.09 | 0.69 | 0.70 | 0.27 |  |  |  |
|  |  | 15 | 6025 | Back face |  | 0.09 | 0.59 | 0.60 | 0.23 |  |  |  |
|  |  | 15 | 6025 | Top edge |  | 0.09 | 0.28 | 0.29 | 0.12 |  |  |  |
|  |  | 15 | 6025 | Right edge |  | 0.09 | 0.46 | 0.46 | 0.18 |  |  |  |
|  |  | 15 | 6025 | Left edge |  | 0.09 | 0.14 | 0.14 | 0.06 |  |  |  |
| $\begin{gathered} 802.11 \\ \text { ax/be } \\ \text { MCS0 } \\ \text { MIMO } \end{gathered}$ |  | 15 | 6025 | Back face |  | 0.09 | 0.21 | 0.22 | 0.08 |  |  |  |
| 802.11 ax/be MCSO | 160 | 15 | 6025 | Front face | Aux | 0.05 | 0.72 | 0.73 | 0.29 |  |  |  |
|  |  | 15 | 6025 | Back face |  | 0.05 | 0.72 | 0.73 | 0.28 |  |  |  |
|  |  | 15 | 6025 | Top edge |  | 0.05 | 0.29 | 0.29 | 0.13 |  |  |  |
|  |  | 15 | 6025 | Right edge |  | 0.05 | 0.46 | 0.46 | 0.19 |  |  |  |
|  |  | 15 | 6025 | Left edge |  | 0.05 | 0.15 | 0.15 | 0.07 |  |  |  |
| $\begin{gathered} 802.11 \\ \text { ax/be } \\ \text { MCS0 } \\ \text { MIMO } \end{gathered}$ |  | 15 | 6025 | Back face |  | 0.05 | 0.26 | 0.27 | 0.10 |  |  |  |
| 802.11 ax/be MCSO | 160 | 79 | 6345 | Front face | Main | 0.07 | 0.72 | 0.73 | 0.27 |  |  |  |
|  |  | 79 | 6345 | Back face |  | 0.07 | 0.60 | 0.61 | 0.23 |  |  |  |
|  |  | 79 | 6345 | Top edge |  | 0.07 | 0.31 | 0.32 | 0.13 |  |  |  |
|  |  | 79 | 6345 | Right edge |  | 0.07 | 0.38 | 0.39 | 0.16 |  |  |  |
|  |  | 79 | 6345 | Left edge |  | 0.07 | 0.08 | 0.08 | 0.04 |  |  |  |
| 802.11 <br> ax/be <br> MCSO <br> MIMO |  | 79 | 6345 | Front face |  | 0.07 | 0.27 | 0.27 | 0.10 |  |  |  |
|  |  | 79 | 6345 | Back Face |  | 0.07 | 0.23 | 0.24 | 0.09 |  |  |  |
| 802.11 ax/be MCSO | 160 | 79 | 6345 | Front face | Aux | 0.10 | 0.77 | 0.79 | 0.28 | 7.69 | 6.26 | 1 |
|  |  | 79 | 6345 | Back face |  | 0.10 | 0.66 | 0.68 | 0.25 |  |  |  |
|  |  | 79 | 6345 | Top edge |  | 0.10 | 0.32 | 0.33 | 0.14 |  |  |  |
|  |  | 79 | 6345 | Right edge |  | 0.10 | 0.33 | 0.34 | 0.14 |  |  |  |
|  |  | 79 | 6345 | Left edge |  | 0.10 | 0.08 | 0.08 | 0.03 |  |  |  |
| 802.11 <br> ax/be <br> MCSO <br> MIMO |  | 79 | 6345 | Front face |  | 0.10 | 0.29 | 0.30 | 0.11 |  |  |  |
|  |  | 79 | 6345 | Back Face |  | 0.10 | 0.26 | 0.27 | 0.10 |  |  |  |

* For reference purposes only, not specifically for compliance, the estimated absorbed (epithelial) power density derived from the measured SAR is shown


## C.5.2 SAR - 802.11ax/be - 6.5 GHz - U-NII-6

| Mode Data Rate | $\begin{gathered} \mathrm{BW} \\ (\mathrm{MH} \\ \mathrm{z}) \end{gathered}$ | Chann <br> el <br> Numb er | $\begin{gathered} \text { Freq } \\ (\mathrm{MHz}) \end{gathered}$ | Test position mode | Ant | Scaling Factor (dB). | Measure d SAR 1 g. (W/kg) | Reported SAR 1 g (W/kg) | Measured SAR 10 g (W/kg) | Estimated epithelial PD ( $\mathrm{W} / \mathrm{m}^{2}$ ) |  | $\begin{gathered} \text { No } \\ \text { Plo } \\ \text { t } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  | $1 \mathrm{~cm}^{2}$ | $4 \mathrm{~cm}^{2}$ |  |
| $\begin{gathered} \text { 802.11ax } \\ \text { /be } \\ \text { MCSO } \end{gathered}$ | 160 | 111 | 6505 | Front face | MAIN | 0.03 | 0.23 | 0.23 | 0.08 |  |  |  |
|  |  | 111 | 6505 | Back face |  | 0.03 | 0.19 | 0.19 | 0.07 |  |  |  |
|  |  | 111 | 6505 | Top edge |  | 0.03 | 0.11 | 0.11 | 0.04 |  |  |  |
|  |  | 111 | 6505 | Right edge |  | 0.03 | 0.10 | 0.10 | 0.04 |  |  |  |
|  |  | 111 | 6505 | Left edge |  | 0.03 | 0.02 | 0.02 | 0.01 |  |  |  |
| $\begin{gathered} \text { 802.11ax } \\ \text { /be } \\ \text { MCS0 } \end{gathered}$ | 160 | 111 | 6505 | Front face | AUX | 0.28 | 0.23 | 0.25 | 0.09 | 2.34 | 1.87 | 2 |
|  |  | 111 | 6505 | Back face |  | 0.28 | 0.19 | 0.20 | 0.08 |  |  |  |
|  |  | 111 | 6505 | Top edge |  | 0.28 | 0.09 | 0.10 | 0.04 |  |  |  |
|  |  | 111 | 6505 | Right edge |  | 0.28 | 0.23 | 0.24 | 0.26 |  |  |  |
|  |  | 111 | 6505 | Left edge |  | 0.28 | 0.03 | 0.04 | 0.02 |  |  |  |

* For reference purposes only, not specifically for compliance, the estimated absorbed (epithelial) power density derived from the measured SAR is shown


## C.5.3 SAR - 802.11ax/be-6.7 GHz - U-NII-7

| Mode | $\begin{gathered} \mathrm{BW} \\ (\mathrm{MHz}) \end{gathered}$ | Channel Number | $\begin{gathered} \text { Freq } \\ (\mathrm{MHz}) \end{gathered}$ | Test position mode | Ant | Scaling Factor (dB). | Measured SAR 1 g . (W/kg) | Reported SAR 1 g (W/kg) | Measured SAR 10 g (W/kg) | Estimated epithelial PD (W/m) |  | No Plot |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  | $1 \mathrm{~cm}^{2}$ | $4 \mathrm{~cm}^{2}$ |  |
| 802.11ax/be MCSO | 160 | 143 | 6665 | Front face | MAIN | 0.01 | 0.70 | 0.70 | 0.29 |  |  |  |
|  |  | 143 | 6665 | Back face |  | 0.01 | 0.55 | 0.55 | 0.21 |  |  |  |
|  |  | 143 | 6665 | Top edge |  | 0.01 | 0.25 | 0.25 | 0.11 |  |  |  |
|  |  | 143 | 6665 | Right edge |  | 0.01 | 0.28 | 0.28 | 0.12 |  |  |  |
|  |  | 143 | 6665 | Left edge |  | 0.01 | 0.05 | 0.05 | 0.02 |  |  |  |
| 802.11ax/be MCS0 | 160 | 143 | 6665 | Front face | AUX | 0.08 | 0.78 | 0.79 | 0.29 | 7.77 | 6.38 | 3 |
|  |  | 143 | 6665 | Back face |  | 0.08 | 0.57 | 0.58 | 0.22 |  |  |  |
|  |  | 143 | 6665 | Top edge |  | 0.08 | 0.22 | 0.22 | 0.10 |  |  |  |
|  |  | 143 | 6665 | Right edge |  | 0.08 | 0.22 | 0.22 | 0.09 |  |  |  |
|  |  | 143 | 6665 | Left edge |  | 0.08 | 0.05 | 0.05 | 0.02 |  |  |  |

* For reference purposes only, not specifically for compliance, the estimated absorbed (epithelial) power density derived from the measured SAR is shown


## C.5.4 SAR - 802.11ax/be - 7.0 GHz - U-NII-8

| Mode | $\begin{gathered} \mathrm{BW} \\ (\mathrm{MHz}) \end{gathered}$ | Channel Number | $\begin{gathered} \text { Freq } \\ (\mathrm{MHz}) \end{gathered}$ | Test position mode | Ant | Scaling Factor (dB). | Measured SAR 1 g . (W/kg) | Reported SAR 1 g (W/kg) | Measured SAR 10 g (W/kg) | Estimated epithelial PD ( $\mathrm{W} / \mathrm{m}^{2}$ ) |  | No Plot |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  | $1 \mathrm{~cm}^{2}$ | $4 \mathrm{~cm}^{2}$ |  |
| $\begin{aligned} & \text { 802.11be } \\ & \text { MCS0 } \end{aligned}$ | 320 | 191 | 6905 | Front face | MAIN | 0.35 | 0.57 | 0.62 | 0.22 | 5.68 | 4.60 | 4 |
|  |  | 191 | 6905 | Back face |  | 0.35 | 0.55 | 0.60 | 0.20 |  |  |  |
|  |  | 191 | 6905 | Top edge |  | 0.35 | 0.22 | 0.24 | 0.09 |  |  |  |
|  |  | 191 | 6905 | Right edge |  | 0.35 | 0.27 | 0.29 | 0.11 |  |  |  |
|  |  | 191 | 6905 | Left edge |  | 0.35 | 0.05 | 0.05 | 0.02 |  |  |  |
| $\begin{aligned} & \text { 802.11be } \\ & \text { MCS0 } \end{aligned}$ | 320 | 191 | 6905 | Front face | AUX | 0.13 | 0.57 | 0.59 | 0.21 |  |  |  |
|  |  | 191 | 6905 | Back face |  | 0.13 | 0.47 | 0.48 | 0.17 |  |  |  |
|  |  | 191 | 6905 | Top edge |  | 0.13 | 0.20 | 0.21 | 0.08 |  |  |  |
|  |  | 191 | 6905 | Right edge |  | 0.13 | 0.13 | 0.13 | 0.05 |  |  |  |
|  |  | 191 | 6905 | Left edge |  | 0.13 | 0.06 | 0.06 | 0.03 |  |  |  |

[^1]
## C.5.5 Power Density - 802.11ax/be - 6.2 GHz - U-NII-5

| Ant. | Mode <br> Data <br> rate | $\begin{gathered} \mathrm{BW} \\ (\mathrm{MHz}) \end{gathered}$ | Ch \# | $\begin{gathered} \text { Freq } \\ (\mathrm{MHz}) \end{gathered}$ | Positi on | $\begin{gathered} \text { PStot } \\ \text { avg } \\ {\left[\mathrm{W} / \mathrm{m}^{2}\right]} \\ 1 \mathrm{~cm}^{2} \end{gathered}$ | PStot avg [W/m²] $4 \mathrm{~cm}^{2}$ | $\begin{aligned} & \mathrm{EM} \mathrm{E} \\ & {[\mathrm{~V} / \mathrm{m}]} \end{aligned}$ | $\begin{aligned} & \mathrm{EM} \mathrm{H} \\ & {[\mathrm{~A} / \mathrm{m}]} \end{aligned}$ | $\begin{gathered} \text { Plot } \\ \# \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Aux | $\begin{gathered} 802.11 \\ \text { ax/be } \end{gathered}$ | 160 | 15 | 6025 | Front face | 9.46 | 8.56 | 86.90 | 0.26 |  |
|  |  | 160 | 79 | 6345 |  | 10.90 | 9.90 | 97.00 | 0.27 | 5 |

C.5.6 Power Density - 802.11ax/be - 6.5 GHz - U-NII-6

| Ant. | Mode <br> Data <br> rate | BW <br> $(\mathrm{MHz})$ | Ch \# | Freq <br> $(\mathrm{MHz})$ | Positi <br> on | PStot <br> avg <br> $\left[\mathrm{W} / \mathrm{m}^{2}\right]$ <br> $1 \mathrm{~cm}^{2}$ | PStot <br> avg <br> $\left[\mathrm{W} / \mathrm{m}^{2}\right]$ <br> $4 \mathrm{~cm}^{2}$ | EM E <br> $[\mathrm{V} / \mathrm{m}]$ | EM H <br> $[\mathrm{A} / \mathrm{m}]$ | Plot <br> $\#$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Aux | 802.11 <br> ax/be | 160 | 111 | 6505 | Front <br> face | 3.77 | 3.52 | 57.60 | 0.17 | 6 |

C.5.7 Power Density - 802.11ax/be - 6.7 GHz - U-NII-7

| Ant. | Mode <br> Data <br> rate | BW <br> $(\mathrm{MHz}$ <br> $)$ | Ch \# | Freq <br> $(\mathrm{MHz})$ | Positio <br> n | PStot <br> avg <br> $\left[\mathrm{W} / \mathrm{m}^{2}\right.$ <br> $]$ <br> $1 \mathrm{~cm}^{2}$ | PStot <br> avg <br> $\left[\mathrm{W} / \mathrm{m}^{2}\right]$ <br> $4 \mathrm{~cm}^{2}$ | EM E <br> $[\mathrm{V} / \mathrm{m}]$ | EM H <br> $[\mathrm{A} / \mathrm{m}]$ | Plot <br> $\#$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Aux | 802.11 ax <br> /be | 160 | 143 | 6665 | Front <br> face | 9.23 | 8.57 | 87.50 | 0.25 | $\mathbf{7}$ |

## C.5.8 Power Density - 802.11ax/be - 7.0 GHz - U-NII-8

| Ant. | Mode <br> Data <br> rate | BW <br> $(\mathrm{MHz}$ <br> $)$ | $\mathrm{Ch} \#$ | Freq <br> $(\mathrm{MHz})$ | Positio <br> n | PStot <br> avg <br> $\left[\mathrm{W} / \mathrm{m}^{2}\right]$ <br> $1 \mathrm{~cm}^{2}$ | PStot <br> avg <br> $\left[\mathrm{W} / \mathrm{m}^{2}\right]$ <br> $4 \mathrm{~cm}^{2}$ | EM E <br> $[\mathrm{V} / \mathrm{m}]$ | EM H <br> $[\mathrm{A} / \mathrm{m}]$ | Plot <br> $\#$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Aux | 802.1 be | 320 | 191 | 6905 | Front <br> face | 11.80 | 9.30 | 93.70 | 0.39 | $\mathbf{8}$ |

## C.5.9 Measurement Variability

According to FCC OET KDB 865664, SAR Measurement variability is assessed when the maximum initial measured SAR is $>=0.8 \mathrm{~W} / \mathrm{kg}$ for a certain band $/$ mode .

As all measured values are under both limits, no variability is required.

## C.5.10Simultaneous Transmission Evaluation - SAR

According to FCC OET KDB 447498, when the sum of 1 g SAR for all simultaneously transmitting antennas in an operating mode and exposure condition combination is within the SAR limit, SAR test exclusion applies to that simultaneous transmission configuration.

All the values stated in the table below are the worst case found for standalone measurement with disregard of the transmission mode or channel where the worst case was found.

| Antenna | Position | Highest Reported SAR (1g) (W/kg) |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Bluetooth* |
| Chain A | Front face | 0.79** | 0.30*** | 0.31 |
| Chain B |  | 0.73** | $0.27^{* * *}$ |  |
| Chain A | Back face | 0.73** | 0.27*** | 0.28 |
| Chain B |  | 0.61** | 0.24*** |  |
| Chain A | Top edge | 0.33 |  | 0.02 |
| Chain B |  | 0.32 |  |  |
| Chain A | Right edge | 0.46 |  | 0.03 |
| Chain B |  | 0.46 |  |  |
| Chain A | Left edge | 0.15 |  | 0.01 |
| Chain B |  | 0.14 |  |  |

* For Bluetooth values refer to test report 230526-09.TR72
${ }^{* *} \mathrm{CH} 15$ and CH 79 was considered for Front and Back positions as the highest standalone measurement on UNII-5 for Aux and Main transmitters for the simultaneous transmission with MIMO power.
****This combination requires SISO value for simultaneous considerations.

| Position | Simultaneous Tx Antenna Combination |  | $\Sigma$ SAR $1 \mathrm{~g}(\mathrm{~W} / \mathrm{kg})$ | Limit (W/kg) |
| :---: | :---: | :---: | :---: | :---: |
|  | Chain A | Chain B |  |  |
| Front Face | WLAN 6GHz | WLAN 6GHz | 0.57 | 1.6 |
|  | WLAN 6GHz + BT | WLAN 6GHz | 0.88 |  |
|  | BT | WLAN 6GHz | 0.58 |  |
| Back face | WLAN 6GHz | WLAN 6GHz | 0.51 |  |
|  | WLAN 6GHz + BT | WLAN 6GHz | 0.79 |  |
|  | BT | WLAN 6GHz | 0.52 |  |
| Top edge | WLAN 6GHz | WLAN 6GHz | 0.65 |  |
|  | WLAN 6GHz + BT | WLAN 6GHz | 0.67 |  |
|  | BT | WLAN 6GHz | 0.34 |  |
| Right edge | WLAN 6GHz | WLAN 6GHz | 0.92 |  |
|  | WLAN 6GHz + BT | WLAN 6GHz | 0.95 |  |
|  | BT | WLAN 6GHz | 0.49 |  |
| Left edge | WLAN 6GHz | WLAN 6GHz | 0.29 |  |
|  | WLAN 6GHz + BT | WLAN 6GHz | 0.30 |  |
|  | BT | WLAN 6GHz | 0.15 |  |

Considering the results described above and according to the simultaneous transmission SAR test exclusion considerations described in FCC OET KDB 447498, no SAR to Peak Location Separation Ratio is required.

## Annex D. Test System Plots

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## 1. U-NII-5-802.11ax160/be160, CH79, Aux - Front face

## Device under Test Properties

| Model, Manufacturer | Dimensions $[\mathrm{mm}]$ | IMEI | DUT Type |
| :---: | :---: | :--- | :--- |
| BE200D2W | $37.0 \times 62.0 \times 2.0$ | 04E8B963C28E | WLAN module + Reference antenna |

## Exposure Conditions

| Phantom Section, TSL | Position, Test Distance [mm] | Band | Group, UID | Frequency [MHz], Channel Number | Conversion Factor | TSL Conductivity [S/m] | TSL Permittivity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Flat, HSL | $\begin{aligned} & \text { FRONT, } \\ & 11.00 \end{aligned}$ | U-NII-5 | WLAN, 10707-AAC | $\begin{aligned} & 6345.0, \\ & 6345000 \end{aligned}$ | 5.25 | 6.20 | 34.6 |

## Hardware Setup

| Phantom | TSL, Measured Date |  | Probe, Calibration Date DA |  | DAE, Calibration Date |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ELI V8.0 (20deg probe tilt) | ) HBBL-600- | 00,2023-Aug-28 | EX3DV4-SN7455, | 23-03-16 DA | n1703, 2023-04-18 |
| Scan Setup |  |  | Measurement Results |  |  |
|  | Area Scan | Zoom Scan |  | Area Scan | Zoom Scan |
| Grid Extents [mm] | $160.0 \times 160.0$ | $22.0 \times 22.0 \times 22.0$ | Date | 2023-08-28, 16:14 | 2023-08-28, 16:24 |
| Grid Steps [mm] | $10.0 \times 10.0$ | $3.4 \times 3.4 \times 1.4$ | psSAR1g [W/kg] | 0.729 | 0.769 |
| Sensor Surface | 3.0 | 1.4 | psSAR10g | 0.275 | 0.278 |
| [mm] |  |  | [W/kg] |  |  |
| Graded Grid | Yes | Yes | Power Drift [dB] | -0.05 | 0.21 |
| Grading Ratio | 1.5 | 1.4 | Power Scaling | Disabled | Disabled |
| MAIA | Confirmed by Maia | Confirmed by Maia | Scaling Factor |  |  |
| Surface Detection | VMS $+6 p$ | VMS $+6 p$ | [dB] |  |  |
| Scan Method | Measured | Measured | TSL Correction | Positive only | Positive only |
|  |  |  | M2/M1 [\%] |  | 55.3 |
|  |  |  | Dist 3dB Peak |  | 11.0 |



## 2. U-NII-6-802.11ax160/be160, CH111, Aux - Front face

## Device under Test Properties

| Model, Manufactu |  | Dimensions [mm] |  | IMEI | DUT Type |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| BE200D2W |  | $37.0 \times 62.0 \times 2.0$ |  | 04E8B963C28E | WLAN module + Reference antenna |  |  |
| Exposure Conditions |  |  |  |  |  |  |  |
| Phantom <br> Section, TSL | Position, Test Distance [mm] | Band | Group, UID | Frequency [MHz], Channel Number | Conversion Factor | TSL Conductivity [S/m] | TSL Permittivity |
| Flat, HSL | $\begin{aligned} & \text { FRONT, } \\ & 11.00 \end{aligned}$ | U-NII-6 | WLAN, 10755-AAC | $\begin{aligned} & 6505.0 \\ & 111 \end{aligned}$ | 5.25 | 6.45 | 34.2 |

## Hardware Setup

| Phantom | TSL, Measured Date |  | Probe, Calibration Date D |  | DAE, Calibration Date |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ELI V8.0 (20deg probe tilt) | ) HBBL-600- | 00,2023-Aug-28 | EX3DV4-SN7455, | 23-03-16 DA | 1703, 2023-04-18 |
| Scan Setup |  |  | Measurement Results |  |  |
|  | Area Scan | Zoom Scan |  | Area Scan | Zoom Scan |
| Grid Extents [mm] | $180.0 \times 180.0$ | $22.0 \times 22.0 \times 22.0$ | Date | 2023-08-28, 13:25 | 2023-08-28, 13:44 |
| Grid Steps [mm] | $10.0 \times 10.0$ | $3.4 \times 3.4 \times 1.4$ | psSAR1g [W/kg] | 0.243 | 0.234 |
| Sensor Surface | 3.0 | 1.4 | psSAR10g | 0.093 | 0.083 |
| [mm] |  |  | [W/kg] |  |  |
| Graded Grid | Yes | Yes | Power Drift [dB] | 0.14 | -0.21 |
| Grading Ratio | 1.5 | 1.4 | Power Scaling | Disabled | Disabled |
| MAIA | Confirmed by Maia | Confirmed by Maia | Scaling Factor |  |  |
| Surface Detection | VMS $+6 p$ | VMS $+6 p$ | [dB] |  |  |
| Scan Method | Measured | Measured | TSL Correction | Positive only | Positive only |
|  |  |  | M2/M1 [\%] |  | 41.5 |
|  |  |  | Dist 3dB Peak [mm] |  | 19.7 |



## 3. U-NII-7-802.11ax160/be160, CH143, Aux - Front face

## Device under Test Properties

| Model, Manufacturer | Dimensions $[\mathrm{mm}]$ | IMEI | DUT Type |
| :--- | :--- | :--- | :--- |
| BE200D2W | $37.0 \times 62.0 \times 2.0$ | 04E8B963C28E | WLAN module + Reference antenna |

## Exposure Conditions

| Phantom Section, TSL | Position, Test Distance [mm] | Band | Group, UID | Frequency [MHz], Channel Number | Conversion Factor | TSL Conductivity [S/m] | TSL Permittivity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Flat, HSL | $\begin{aligned} & \text { FRONT, } \\ & 11.00 \end{aligned}$ | U-NII-7 | WLAN, 10707-AAC | $\begin{aligned} & 6665.0 \\ & 143 \end{aligned}$ | 5.25 | 6.69 | 33.8 |

## Hardware Setup

| Phantom | TSL, Measured Date |  | Probe, Calibration Date D |  | DAE, Calibration Date |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ELI V8.0 (20deg probe tilt) | ) HBBL-600- | 00,2023-Aug-28 | EX3DV4-SN7455, | 23-03-16 DA | 1703, 2023-04-18 |
| Scan Setup |  |  | Measurement Results |  |  |
|  | Area Scan | Zoom Scan |  | Area Scan | Zoom Scan |
| Grid Extents [mm] | $160.0 \times 160.0$ | $22.0 \times 22.0 \times 22.0$ | Date | 2023-08-30, 14:44 | 2023-08-30, 14:53 |
| Grid Steps [mm] | $10.0 \times 10.0$ | $3.4 \times 3.4 \times 1.4$ | psSAR1g [W/kg] | 0.768 | 0.777 |
| Sensor Surface | 3.0 | 1.4 | psSAR10g | 0.290 | 0.285 |
| [mm] |  |  | [W/kg] |  |  |
| Graded Grid | Yes | Yes | Power Drift [dB] | 0.09 | -0.12 |
| Grading Ratio | 1.5 | 1.4 | Power Scaling | Disabled | Disabled |
| MAIA Con | Confirmed by Maia | Confirmed by Maia | Scaling Factor |  |  |
| Surface Detection | VMS + 6p | VMS + 6p | [dB] |  |  |
| Scan Method | Measured | Measured | TSL Correction | Positive only | Positive only |
|  |  |  | M2/M1 [\%] |  | 52.3 |
|  |  |  | Dist 3dB Peak |  | 11.0 |



## 4. U-NII-8-802.11be320, CH191, Main - Front face

## Device under Test Properties

| Model, Manufacturer | Dimensions $[\mathrm{mm}]$ | IMEI | DUT Type |
| :--- | :--- | :--- | :--- |
| BE200D2W | $37.0 \times 62.0 \times 2.0$ | 04E8B963C28E | WLAN module + Reference antenna |

## Exposure Conditions

| Phantom Section, TSL | Position, Test Distance [mm] | Band | Group, UID | Frequency [MHz], Channel Number | Conversion Factor | TSL Conductivity [S/m] | TSL <br> Permittivity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Flat, HSL | $\begin{aligned} & \text { FRONT, } \\ & 11.00 \end{aligned}$ | Custom Band | $\begin{aligned} & \text { CW, } \\ & \text { 10554-AAD } \end{aligned}$ | $\begin{aligned} & 6905.0, \\ & 6905000 \end{aligned}$ | 5.25 | 6.99 | 33.5 |

## Hardware Setup

| Phantom | TSL, Measured Date |  | Probe, Calibration Date <br> EX3DV4 - SN7455, 2023-03-16 |  | DAE, Calibration Date |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ELI V8.0 (20deg probe tilt | it HBBL-600-1 | 00,2023-Aug-28 |  |  | n1703, 2023-04-18 |
| Scan Setup | Area Scan | Zoom Scan | Measurement Results |  | Zoom Scan |
|  |  |  | Area Scan |  |  |
| Grid Extents [mm] | $102.0 \times 102.0$ | $22.0 \times 22.0 \times 22.0$ | Date | 2023-08-28, 10:08 | 2023-08-28, 10:17 |
| Grid Steps [mm] | $8.5 \times 8.5$ | $3.4 \times 3.4 \times 1.4$ | psSAR1g [W/kg] | 0.575 | 0.568 |
| Sensor Surface | 3.0 | 1.4 | psSAR10g | 0.215 | 0.205 |
| [mm] |  |  | [W/kg] |  |  |
| Graded Grid | Yes | Yes | Power Drift [dB] | 0.09 | -0.06 |
| Grading Ratio | 1.5 | 1.4 | Power Scaling | Disabled | Disabled |
| MAIA | Confirmed by MAIA | Confirmed by MAIA | Scaling Factor |  |  |
| Surface Detection | VMS +6 p | VMS + 6 p | [dB] |  |  |
| Scan Method | Measured | Measured | TSL Correction | Positive only | Positive only |
|  |  |  | M2/M1 [\%] |  | 46.8 |
|  |  |  | Dist 3dB Peak |  | 11.0 |
|  |  |  | [mm] |  |  |



## 5. U-NII-5-802.11ax160/be160, CH79, Aux - Front face

DUT: Engineering sample BE200D2W; Type: 03
Signal Source: modulation Custom Channel for $802.11 \mathrm{ax} / \mathrm{be}$, level 19.00 dBm .
Medium parameters used: $\sigma=0 \mathrm{~S} / \mathrm{m}, \varepsilon r=1 ; \rho=0 \mathrm{~kg} / \mathrm{m} 3$
Phantom section: Table Section
Measurement Standard: DASY6 (IEEE/IEC/ANSI C63.19-2011)
DASY Configuration:

- Probe: EUmmW - SN9594; ConvF(1, 1, 1); Calibrated: 20-09-2022;
- Modulation Compensation:
- Sensor-Surface : Omm (Fix Surface), z = 11 mm
- Electronics: DAE4 Sn1705; Calibrated: 18-04-2023
- Phantom: Cover; Type: SPEAG Phantom Cover
- cDASY6 5G Module v3.0
- Test Date: 2023-08-31


## Distance-11mm:

Measurement Resolution $=\lambda / 8 \mathrm{~mm}$
Measurement Scan area $=120 \mathrm{~mm} \times 120 \mathrm{~mm}$
The plots below show the average PStot $\left(1 \mathrm{~cm}^{2}\right)$, PStot $\left(4 \mathrm{~cm}^{2}\right)$ the E-field and the H Field


## 6. U-NII-6-802.11ax160/be160, CH111, Aux - Front face

## DUT: Engineering sample BE200D2W; Type: 03

Signal Source: modulation Custom Channel for 802.11ax/be, level 14.75 dBm .
Medium parameters used: $\sigma=0 \mathrm{~S} / \mathrm{m}, \varepsilon r=1 ; \rho=0 \mathrm{~kg} / \mathrm{m} 3$
Phantom section: Table Section
Measurement Standard: DASY6 (IEEE/IEC/ANSI C63.19-2011)
DASY Configuration:

- Probe: EUmmW - SN9594; ConvF(1, 1, 1); Calibrated: 20-09-2022;
- Modulation Compensation:
- Sensor-Surface : Omm (Fix Surface), z = 11 mm
- Electronics: DAE4 Sn1705; Calibrated: 18-04-2023
- Phantom: Cover; Type: SPEAG Phantom Cover
- cDASY6 5G Module v3.0
- Test Date: 2023-08-31


## Distance-11mm:

Measurement Resolution $=\lambda / 8 \mathrm{~mm}$
Measurement Scan area $=120 \mathrm{~mm} \times 120 \mathrm{~mm}$
The plots below show the average PStot $\left(1 \mathrm{~cm}^{2}\right)$, PStot $\left(4 \mathrm{~cm}^{2}\right)$ the E-field and the H Field


## 7. U-NII-7-802.11ax160/be160, CH143, Aux - Front face

DUT: Engineering sample BE200D2W; Type: 03
Signal Source: modulation Custom Channel for 802.11ax/be, level 19.00dBm.
Medium parameters used: $\sigma=0 \mathrm{~S} / \mathrm{m}, \varepsilon r=1 ; \rho=0 \mathrm{~kg} / \mathrm{m} 3$
Phantom section: Table Section
Measurement Standard: DASY6 (IEEE/IEC/ANSI C63.19-2011)
DASY Configuration:

- Probe: EUmmW - SN9594; ConvF(1, 1, 1); Calibrated: 20-09-2022;
- Modulation Compensation:
- Sensor-Surface : Omm (Fix Surface), z = 11 mm
- Electronics: DAE4 Sn1705; Calibrated: 18-04-2023
- Phantom: Cover; Type: SPEAG Phantom Cover
- cDASY6 5G Module v3.0
- Test Date: 2023-08-31


## Distance-11mm:

Measurement Resolution $=\lambda / 8 \mathrm{~mm}$
Measurement Scan area $=120 \mathrm{~mm} \times 120 \mathrm{~mm}$
The plots below show the average PStot $\left(1 \mathrm{~cm}^{2}\right)$, PStot $\left(4 \mathrm{~cm}^{2}\right)$ the E-field and the H Field

\begin{tabular}{|c|c|}
\hline \multicolumn{2}{|c|}{Measurement Results} \\
\hline \begin{tabular}{l}
\|spotokt ( 1 acma, circ)\| \\
[W/m^2]
9.25
0
\end{tabular} \& \begin{tabular}{l}
\|sprotat+ (4.90mzi cric)\| [W/m^2] \\
8.57
\end{tabular} \\
\hline \begin{tabular}{l}
\|EM \(E(x, y, z, f 0) \|\) \\
[ \(\mathrm{V} / \mathrm{m}\) ] \\
87.5
\end{tabular} \& \(\| E M M\left(x_{2} y_{2} z n y\right) \mid\) fato zastinli

$$
0 .
$$

$$
1 \pi
$$ <br>

\hline
\end{tabular}

## 8. U-NII-8-802.11be320, CH191, Aux- Front face

DUT: Engineering sample BE200D2W; Type: 03
Signal Source: modulation Custom Channel for 802.11 be , level 17.25 dBm .
Medium parameters used: $\sigma=0 \mathrm{~S} / \mathrm{m}, \varepsilon r=1 ; \rho=0 \mathrm{~kg} / \mathrm{m} 3$
Phantom section: Table Section
Measurement Standard: DASY6 (IEEE/IEC/ANSI C63.19-2011)
DASY Configuration:

- Probe: EUmmW - SN9594; ConvF(1, 1, 1); Calibrated: 20-09-2022;
- Modulation Compensation:
- Sensor-Surface : Omm (Fix Surface), z = 11 mm
- Electronics: DAE4 Sn1705; Calibrated: 18-04-2023
- Phantom: Cover; Type: SPEAG Phantom Cover
- cDASY6 5G Module v3.0
- Test Date: 2023-08-30


## Distance-11mm:

Measurement Resolution $=\lambda / 8 \mathrm{~mm}$
Measurement Scan area $=120 \mathrm{~mm} \times 120 \mathrm{~mm}$
The plots below show the average PStot $\left(1 \mathrm{~cm}^{2}\right)$, PStot $\left(4 \mathrm{~cm}^{2}\right)$ the E-field and the H Field


## 9. Power Density System Check From 6500MHz- 2023-08-30

DUT: Horn reference source; Type: PE9859/SF-15
Signal Source: modulation CW, level 10 dBm .
Medium parameters used: $\sigma=0 \mathrm{~S} / \mathrm{m}, \varepsilon r=1 ; \rho=0 \mathrm{~kg} / \mathrm{m} 3$
Phantom section: Table Section
Measurement Standard: DASY6 (IEEE/IEC/ANSI C63.19-2011)
DASY Configuration:

- Probe: EUmmW - SN9594; ConvF(1, 1, 1); Calibrated: 20-09-2022;
- Modulation Compensation:
- Sensor-Surface : Omm (Fix Surface), z = 10 mm
- Electronics: DAE4 Sn1705; Calibrated: 18-04-2023
- Phantom: Cover; Type: SPEAG Phantom Cover
- cDASY6 5G Module v3.0
- Test Date: 2023-08-30

Distance-10mm/Measure Horn reference source (86.9x63.5):
Measurement Resolution $=\lambda / 4 \mathrm{~mm}$
Measurement Scan area $=200 \mathrm{~mm} \times 200 \mathrm{~mm}$

The plots below show the comparison between the Numerical Modeling results and the system check measurement results in terms of E-field, H Field, single point power density and Avg Power density $1 \mathrm{~cm}^{2}$.


The plots below show the comparison between the numerical modeling and the system check results in terms of normalized E-field distribution and the 1D variation along the two axis of the maximum.

| Numerical Modeling Results <br> scan area: 200 mm x 200 mm Resolution: 0.5 mm |  |  |  |  | System Check Measurement Results <br> scan area: $200 \mathrm{~mm} \times 200 \mathrm{~mm}$ <br> - Resolution: N/4 mm |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Field variation through the maximum along the E-field polarizatio |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Field variation through the maximum along the H-field polarization |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |

## 10.SAR System Check From 7000MHz 2023-08-28

## Device under Test Properties

| Model, Manufacturer | Dimensions $[\mathrm{mm}]$ | IMEI | DUT Type |
| :--- | :---: | :---: | :--- |
| D7.0GHzV2, Speag | $50.0 \times 10.0 \times 8.0$ | 1008 | Validation Dipole |

## Exposure Conditions

| Phantom Section, TSL | Position, Test Distance [mm] | Band | Group, UID | Frequency [MHz], <br> Channel Number | Conversion Factor | TSL Conductivity [S/m] | TSL Permittivity |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Flat, HSL | , |  | ' | $\begin{aligned} & 7000.0 \\ & 0 \end{aligned}$ | 5.25 | 7.09 | 33.4 |

## Hardware Setup

| PhantomELI V8.0 (20deg probe tilt) | TSL, Measured Date |  | Probe, Calibration Date D |  | DAE, Calibration Date |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | t) HBBL-600- | 00,2023-Aug-28 | EX3DV4-SN7455, | 23-03-16 DA | n1703, 2023-04-18 |
| Scan Setup |  |  | Measurement Results |  |  |
|  | Area Scan | Zoom Scan |  | Area Scan | Zoom Scan |
| Grid Extents [mm] | $45.0 \times 90.0$ | $22.0 \times 22.0 \times 22.0$ | Date | 2023-08-28, 08:43 | 2023-08-28, 08:53 |
| Grid Steps [mm] | $7.5 \times 7.5$ | $3.0 \times 3.0 \times 1.4$ | psSAR1g [W/kg] | 6.51 | 7.54 |
| Sensor Surface | 3.0 | 1.4 | psSAR10g | 1.28 | 1.33 |
| [mm] |  |  | [W/kg] ${ }^{\text {P }}$ |  |  |
| Graded Grid | Yes | Yes | Power Drift [dB] | -0.12 | -0.06 |
| Grading Ratio | 1.5 | 1.4 |  |  |  |
| MAIA Con | Confirmed by MAIA | Confirmed by MAIA | Power Scaling | Disabled | Disabled |
| Surface Detection | VMS $+6 p$ | VMS $+6 p$ | Scaling Factor |  |  |
| Scan Method | Measured | Measured | [dB] |  |  |
|  |  |  | TSL Correction | Positive Only | Positive Only |
|  |  |  | M2/M1 [\%] |  | 47.3 |
|  |  |  | Dist 3dB Peak [mm] |  | 4.6 |



## 11.SAR System Check From 7000MHz 2023-08-30



| Hardware Setup |  |  |
| :---: | :---: | :---: |
| Phantom | TSL, Measured Date |  |
| ELI V8.0 (20deg probe tilt) | ) HBBL-600-10000, 2023-Aug-28 |  |
| Scan Setup |  |  |
|  | Area Scan | Zoom Scan |
| Grid Extents [mm] | $45.0 \times 90.0$ | $22.0 \times 22.0 \times 22.0$ |
| Grid Steps [mm] | $7.5 \times 7.5$ | $3.0 \times 3.0 \times 1.4$ |
| Sensor Surface | 3.0 | 1.4 |
| [mm] |  |  |
| Graded Grid | Yes | Yes |
| Grading Ratio | 1.5 | 1.4 |
| MAIA | Confirmed by MAIA | Confirmed by MAIA |
| Surface Detection | VMS + 6 p | VMS +6 p |
| Scan Method | Measured | Measured |


| Probe, Calibration Date <br> EX3DV4 - SN3978, 2023-04-19 |  | DAE, Calibration Date |
| :---: | :---: | :---: |
|  |  | n1704, 2023-04-18 |
| Measurement Results |  |  |
| Area Scan |  | Zoom Scan |
| Date psSAR1g [W/kg] | 2023-08-30, 15:36 | 2023-08-30, 15:46 |
|  | 6.66 | 7.48 |
| psSAR10g | 1.27 | 1.33 |
| [W/kg] |  |  |
| Power Drift [dB] | -0.00 | -0.01 |
| APD (W/m2) |  |  |
| Power Scaling | Disabled | Disabled |
| Scaling Factor [dB] |  |  |
| TSL Correction | Positive Only | Positive Only |
| M2/M1 [\%] |  | 47.0 |
| Dist 3dB Peak |  | 4.7 |



## Annex E. TSL Dielectric Parameters

## E. 1 Head WiFi 6E 7000MHz

| Freq.(MHz) | Target |  | 2023-08-28 |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\varepsilon^{\prime}(\mathrm{F} / \mathrm{m})$ | $\sigma(\mathrm{S} / \mathrm{m})$ | $\varepsilon^{\prime} 1(\mathrm{~F} / \mathrm{m})$ | $\varepsilon^{\prime} 1(\mathrm{~F} / \mathrm{m})$ |
| 6000.0 | 35.07 | 5.48 | 34.95 | 5.77 |
| 6050.0 | 35.01 | 5.54 | 34.95 | 5.84 |
| 6100.0 | 34.95 | 5.59 | 34.95 | 5.9 |
| 6150.0 | 34.89 | 5.65 | 34.93 | 5.96 |
| 6200.0 | 34.83 | 5.71 | 34.89 | 6.03 |
| 6250.0 | 34.77 | 5.77 | 34.82 | 6.09 |
| 6300.0 | 34.70 | 5.83 | 34.72 | 6.16 |
| 6350.0 | 34.64 | 5.89 | 34.60 | 6.23 |
| 6400.0 | 34.58 | 5.95 | 34.46 | 6.30 |
| 6450.0 | 34.52 | 6.01 | 34.33 | 6.37 |
| 6500.0 | 34.46 | 6.07 | 34.19 | 6.44 |
| 6550.0 | 34.40 | 6.13 | 34.07 | 6.51 |
| 6600.0 | 34.34 | 6.19 | 33.94 | 6.58 |
| 6650.0 | 34.29 | 6.25 | 33.82 | 6.65 |
| 6700.0 | 34.23 | 6.30 | 33.73 | 6.72 |
| 6750.0 | 34.17 | 6.36 | 33.65 | 6.79 |
| 6800.0 | 34.11 | 6.42 | 33.57 | 6.86 |
| 6850.0 | 34.05 | 6.48 | 33.51 | 6.93 |
| 6900.0 | 33.99 | 6.53 | 33.46 | 6.98 |
| 6950.0 | 33.94 | 6.59 | 33.41 | 7.04 |
| 7000.0 | 33.88 | 6.65 | 33.38 | 7.09 |




[^0]:    Initial test configuration

[^1]:    * For reference purposes only, not specifically for compliance, the estimated absorbed (epithelial) power density derived from the measured SAR is shown

