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FCC Part 90 Certification Application

FCC Form 731

For The

**IntegraTR
UHF RADIO MODEM**

FCC ID: NP44048350

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NAME OF TEST: Transmitter Rated Power Output

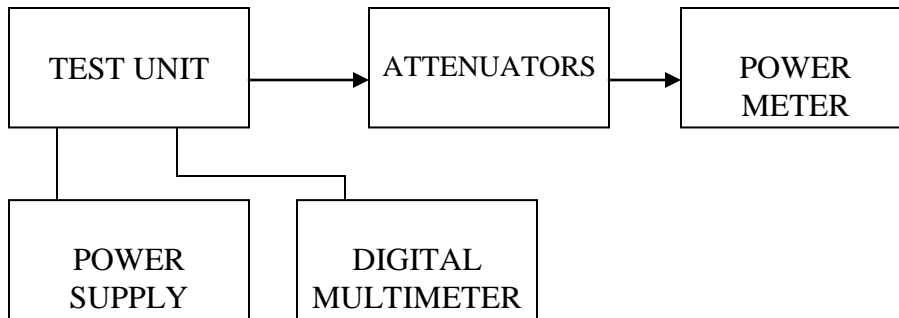
RULE PART NUMBER: 2.1046 (a) (c)

TEST RESULTS: See results below

TEST CONDITIONS: Standard Test Conditions

TEST EQUIPMENT: 50-Ohm Attenuator, Aeroflex/Weinschel 56-6-34 (6 dB / 250W)
 Bird Elec. Corp. 50-A-FFN-20 (20 db / 50 Watt)
 Power Supply, HP 6653A
 Digital Multimeter, Instek GDM-8245
 Power Meter, Model HP 437B

TEST SET-UP:



TEST RESULTS:

Frequency (MHz)	DC Voltage at Final (Vdc)	DC Current into Final (Adc)	DC Power into Final (W)	RF Power Output (W)
458.1	13.3	1.660	22.078	4.948

NAME OF TEST: Transmitter Spurious and Harmonic Outputs

RULE PART NUMBER: 2.1051, 90.210 (c,3)(d,3)(e,3)

MINIMUM STANDARDS: For 5 Watts: $50+10\text{Log}_{10}(5 \text{ Watts}) = -57.0 \text{ dBc}$
or -65dBc , whichever is the lesser attenuation.

For 1 Watt: $50+10\text{Log}_{10}(1 \text{ Watt}) = -50 \text{ dBc}$
or -70 dBc , whichever is the lesser attenuation.

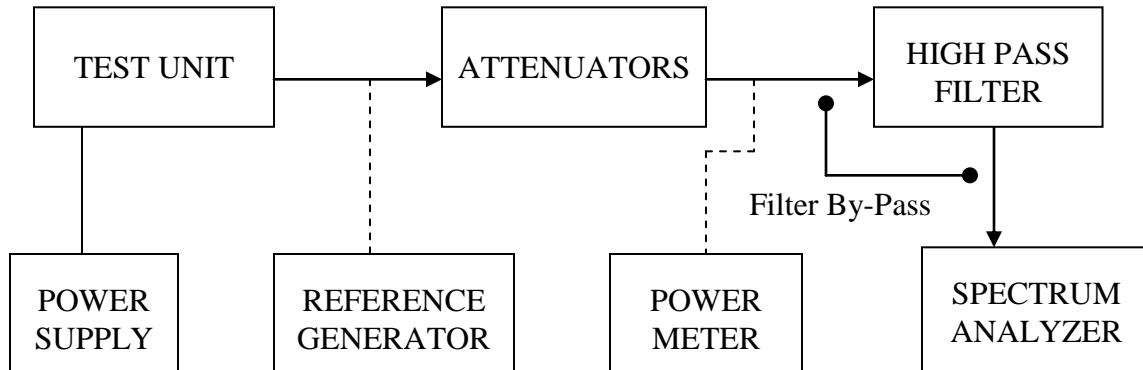
TEST RESULTS: Meets minimum standards (see data on following pages)

TEST CONDITIONS: Standard Test Conditions, 25 C
RF Voltage measured at antenna terminals

TEST PROCEDURE: TIA/EIA – 603-C

TEST EQUIPMENT: 50-Ohm Attenuator, Aeroflex/Weinschel 56-6-34 (6 dB / 250W)
Power Supply, HP 6653A
Spectrum Analyzer, HP-8563E
Reference Generator, Agilent E8257D
High Pass Filter, Mini Circuits VHF-740, $F_c = 740 \text{ MHz}$

TEST SET-UP:



MEASUREMENT PROCEDURE:

1. The transmitter carrier output frequency are 406.1, 439.8, 440.1, and 475.8. The reference oscillator frequency is 14.40 MHz. The power amplifier has voltage levels at 13.3 Volts for 5 watts.
2. The carrier reference was established on the spectrum analyzer with the filter by-pass in place. Then the spectrum was scanned from DC to $2 F_c$. Finally, the high pass filter was inserted to null the carrier fundamental and extend the range of the spectrum analyzer for harmonic measurements above $2 F_c$.
3. At each spurious frequency, generation substitution was used to establish the true spurious level.
4. The spectrum was scanned to the 10th harmonic of the highest internally generated frequency.

Tuned Frequency	406.1 MHz	
Power	5 Watts	
	37 dBm	
Min. Specification	-57.0 dBc	
Worse Case	-89.28 dBc	
<u>Spurious Frequency (MHz)</u>	<u>Relation to Carrier</u>	<u>Relative to Carrier (dBc)</u>
812.2	2 fo	-89.28
1218.3	3 fo	-104.28
1624.4	4 fo	-127.20
2030.5	5 fo	-124.60
2436.6	6 fo	-126.96
2842.7	7 fo	-137.00
3248.8	8 fo	-130.70
3654.9	9 fo	-113.20
4061.0	10 fo	-127.70

Tuned Frequency	406.1 MHz	
Power	1 Watt	
	30.0 dBm	
Min. Specification	-50.0 dBc	
Worse Case	-85.40 dBc	
<u>Spurious Frequency (MHz)</u>	<u>Relation to Carrier</u>	<u>Relative to Carrier (dBc)</u>
812.2	2 fo	-85.40
1218.3	3 fo	-111.10
1624.4	4 fo	-136.00
2030.5	5 fo	-123.00
2436.6	6 fo	-125.00
2842.7	7 fo	-138.00
3248.8	8 fo	-138.00
3654.9	9 fo	-116.00
4061.0	10 fo	-134.00

Tuned Frequency	439.8 MHz	Tuned Frequency	439.8 MHz		
Power	5 Watts	Power	1 Watt		
	37 dBm		30.0 dBm		
Min. Specification	-57.0 dBc	Min. Specification	-50.0 dBc		
Worse Case	-103.92 dBc	Worse Case	-99.38 dBc		
<u>Spurious</u>	<u>Relation to</u>	<u>Relative to</u>	<u>Spurious</u>	<u>Relation to</u>	<u>Relative to</u>
<u>Frequency (MHz)</u>	<u>Carrier</u>	<u>Carrier (dBc)</u>	<u>Frequency (MHz)</u>	<u>Carrier</u>	<u>Carrier (dBc)</u>
879.6	2 fo	-103.92	879.6	2 fo	-99.38
1319.4	3 fo	-112.10	1319.4	3 fo	-119.66
1759.2	4 fo	-123.00	1759.2	4 fo	-126.98
2199.0	5 fo	-123.00	2199	5 fo	-128.66
2638.8	6 fo	-120.50	2638.8	6 fo	-138.00
3078.6	7 fo	-128.30	3078.6	7 fo	-138.00
3518.4	8 fo	-122.30	3518.4	8 fo	-138.00
3958.2	9 fo	-104.50	3958.2	9 fo	-138.00
4398.0	10 fo	-121.00	4398	10 fo	-103.60

Tuned Frequency	440.1 MHz		
Power	5 Watts 37 dBm		
Min. Specification	-57.0 dBc		
Worse Case	-85.70 dBc		
	Spurious	Relation to	
	<u>Frequency (MHz)</u>	<u>Carrier</u>	
		<u>Relative to</u>	
		<u>Carrier (dBc)</u>	
	880.2	2 fo	-108.92
	1320.3	3 fo	-115.00
	1760.4	4 fo	-121.20
	2200.5	5 fo	-85.70
	2640.6	6 fo	-116.00
	3080.7	7 fo	-127.00
	3520.8	8 fo	-106.50
	3960.9	9 fo	-103.00
	4401.0	10 fo	-91.80

Tuned Frequency	440.1 MHz		
Power	1 Watt 30.0 dBm		
Min. Specification	-50.0 dBc		
Worse Case	-94.4 dBc		
	Spurious	Relation to	
	<u>Frequency (MHz)</u>	<u>Carrier</u>	
		<u>Relative to</u>	
		<u>Carrier (dBc)</u>	
	880.2	2 fo	-101.54
	1320.3	3 fo	-94.40
	1760.4	4 fo	-122.70
	2200.5	5 fo	-126.00
	2640.6	6 fo	-138.80
	3080.7	7 fo	-133.70
	3520.8	8 fo	-133.60
	3960.9	9 fo	-122.80
	4401.0	10 fo	-116.80

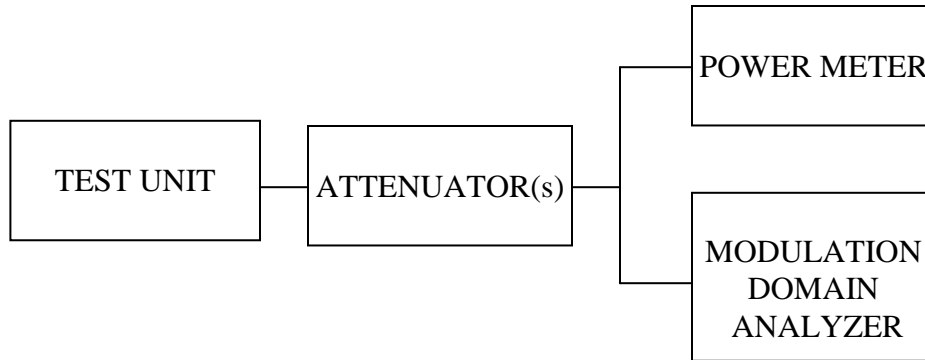
Tuned Frequency	475.8 MHz		Tuned Frequency	475.8 MHz	
Power	5 Watts		Power	1 Watt	
	37 dBm			30.0 dBm	
Min. Specification	-57.0 dBc		Min. Specification	-50.0 dBc	
Worse Case	-92.9 dBc		Worse Case	-107.6 dBc	
<u>Spurious</u>	<u>Relation to</u>	<u>Relative to</u>	<u>Spurious</u>	<u>Relation to</u>	<u>Relative to</u>
<u>Frequency (MHz)</u>	<u>Carrier</u>	<u>Carrier (dBc)</u>	<u>Frequency (MHz)</u>	<u>Carrier</u>	<u>Carrier (dBc)</u>
951.6	2 fo	-103.00	951.6	2 fo	-107.60
1427.4	3 fo	-107.30	1427.4	3 fo	-116.10
1903.2	4 fo	-115.50	1903.2	4 fo	-124.60
2379.0	5 fo	-110.60	2379.0	5 fo	-128.20
2854.8	6 fo	-99.50	2854.8	6 fo	-135.00
3330.6	7 fo	-123.00	3330.6	7 fo	-130.00
3806.4	8 fo	-111.90	3806.4	8 fo	-127.50
4282.2	9 fo	-97.00	4282.2	9 fo	-119.12
4758.0	10 fo	-92.90	4758.0	10 fo	-117.78

NAME OF TEST: Transient Frequency Behavior

RULE PART NUMBER: 90.214

MINIMUM STANDARD: ± 12.5 kHz channel (used worst case numbers from 406.1 to 476 MHz)

<u>TIME INTERVAL</u>	<u>MAXIMUM FREQUENCY DIFFERENCE (kHz)</u>	<u>TIME (ms)</u>
T1	± 12.5	10
T2	± 6.25	25
T3	± 12.5	10



TEST RESULTS: Meets minimum standards, see data on following pages

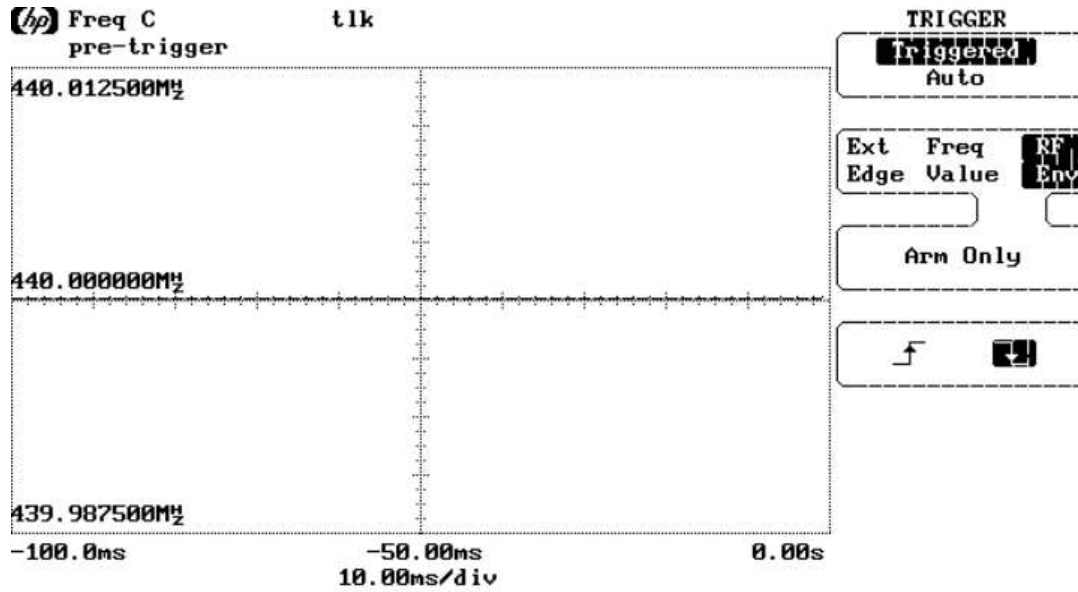
TEST CONDITIONS: RF Power Level = 5.0 Watts and 1.0 Watt
Standard Test Conditions, 25 C

TEST PROCEDURE: TIA/EIA – 603-C

TEST EQUIPMENT: 50-Ohm Attenuator, Aeroflex Model 58-10-34 (10dB, 50W)
50-Ohm Attenuator, Mini-Circuits Model CAT-20 (20dB)
50-Ohm Attenuator, Mini-Circuits Model CAT-10 (10dB)
Power Supply, Agilent 6654A
Modulation Domain Analyzer, HP-53310A
Power Meter, Model HP 437B

Frequency : 440.00000 MHz
Power: 5 W

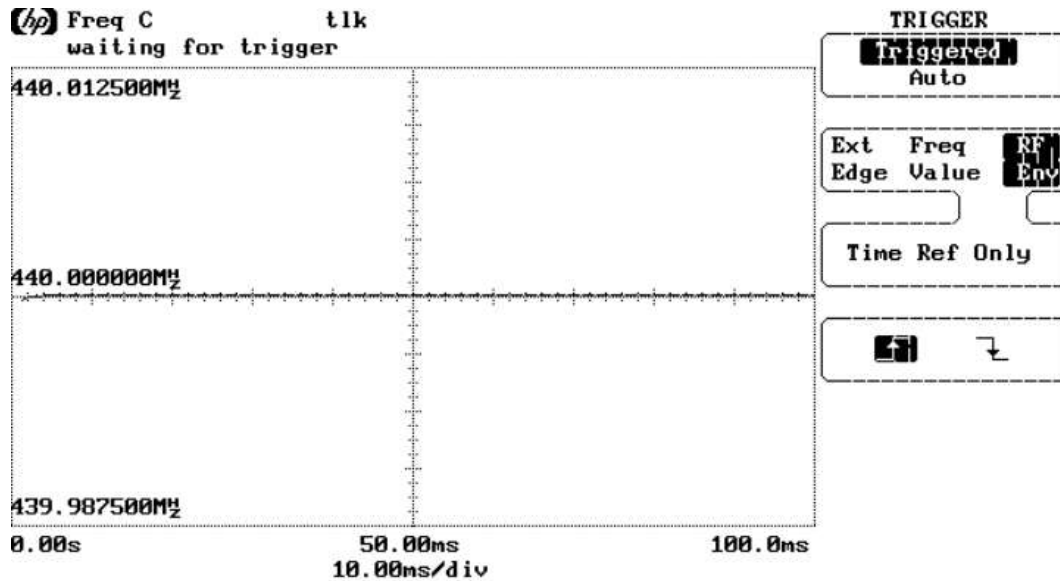
Key-Down



Settling Time -----

ref int

Key-up

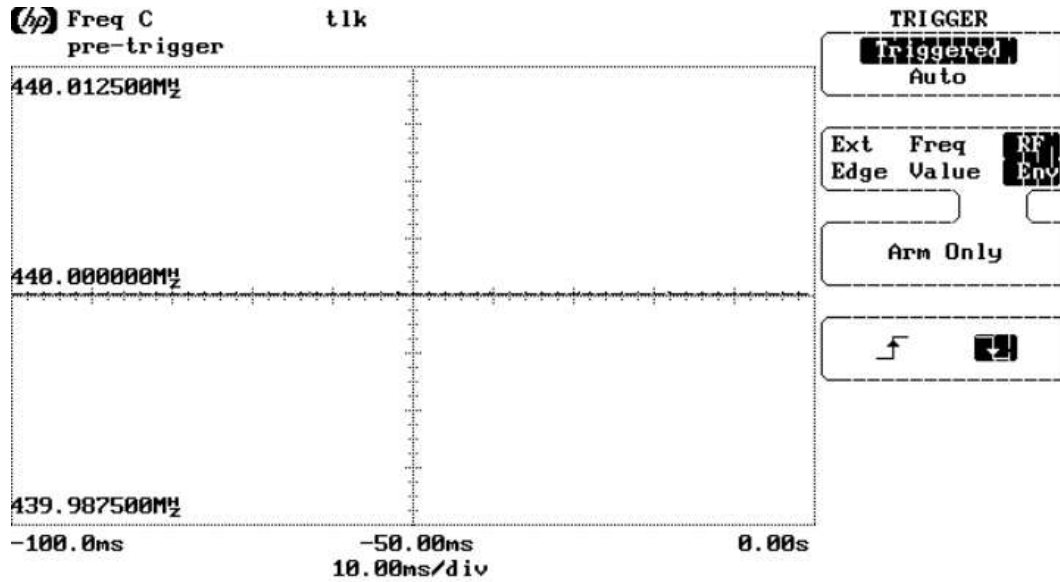


Settling Time -----

ref int

Frequency : 440.00000 MHz
Power: 1.0 W

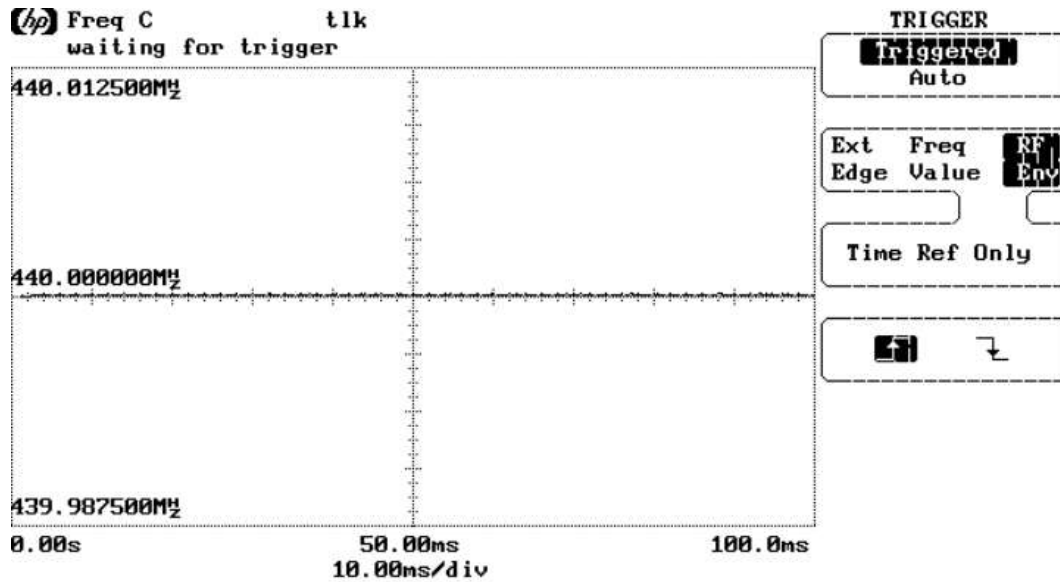
Key-Down



Settling Time -----

ref int

Key-up



Settling Time -----

ref int

NAME OF TEST: Frequency Stability with Variation in Supply Voltage

RULE PART NUMBER: 2.1055 (d)(1), 90.213 (a)

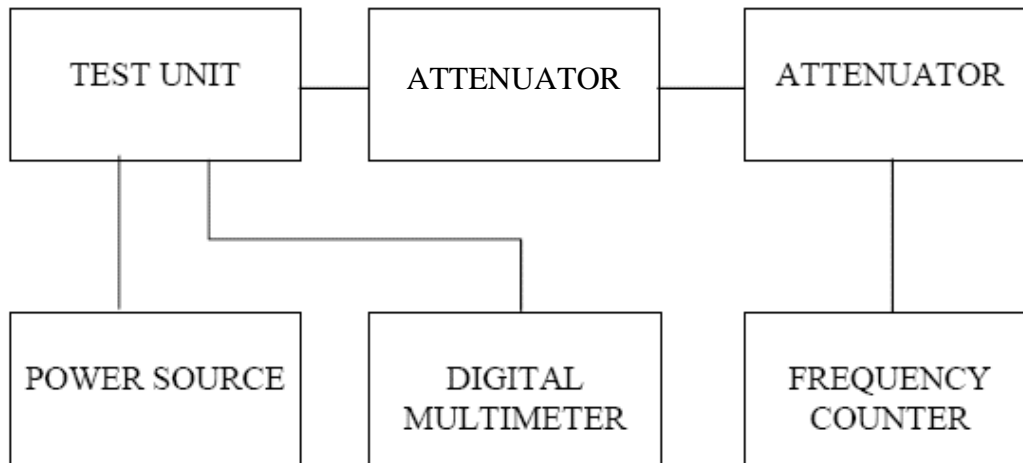
MINIMUM STANDARD: Shall not exceed ± 1.50 ppm.

TEST RESULTS: Meets minimum standard, see data on following page

TEST CONDITIONS: Standard Test Conditions, 25 C

TEST EQUIPMENT: Frequency Counter, HP 8901A Modulation Analyzer
 DC Power Supply, HP 6653A
 Digital Voltmeter, Instek GDM-8245
 50-Ohm Attenuator, AeroFlex/Weinschel 56-6-34 (6Db / 250W)
 Bird Elec. Corp. 50-A-FFN-20 (20 db / 50 Watt)

TEST SET-UP:



TEST SET-UP

Channel Frequency: 458.1000 MHz
Tolerance Requirements: ± 1.5 ppm
Highest Variation: 0.31 ppm
Power Output: 5 Watts

Input Voltage (Vdc)	Frequency (MHz)	Frequency Error (Hz)	Frequency Error (ppm)
10	458.100140	140	0.31
13.3	458.100120	120	0.26
16	458.100130	130	0.28

NAME OF TEST: Frequency Stability with Variation in Ambient Temperature

RULE PART NUMBER: 2.1055 (a) (b), 90.213 (a)

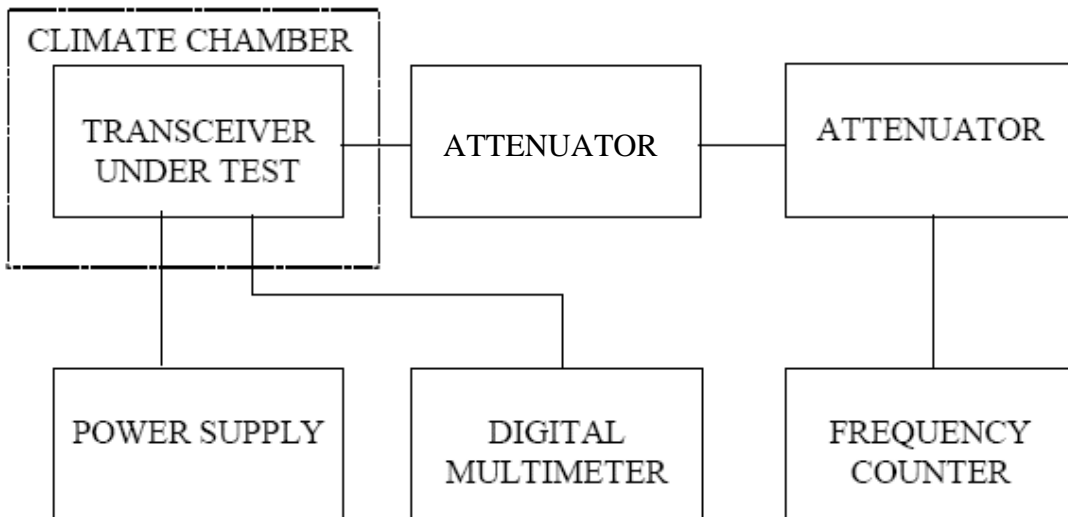
MINIMUM STANDARD: Shall not exceed ± 1.50 ppm from test frequency

TEST RESULTS: Meets minimum standard, see data on following page

TEST CONDITIONS: Standard Test Conditions

TEST EQUIPMENT: Frequency Counter, 8901A Modulation Analyzer
 DC Power Supply, HP 6653A
 Digital Voltmeter, Instek GDM-8245
 50-Ohm Attenuator, AeroFlex/Weinschel 56-6-34 (6dB,250W)
 Bird Elec. Corp. 50-A-FFN-20 (20 db / 50 Watt)
 Climate Chamber, Test Equity Half Cube Model 105

TEST SET-UP:



Channel Frequency: 458.10000 MHz
 Voltage & Power Level: 13.3 Volts @ 5 Watts
 Highest Variation: 0.48 ppm

Temperature (Deg C)	Measured Frequency (MHz)	Frequency Error (Hz)	Frequency Error (ppm)
-30	458.10025	200	0.44
-20	458.10011	110	0.24
-10	458.10020	200	0.44
0	458.10018	180	0.39
10	458.10018	180	0.39
20	458.10022	220	0.48
30	458.10012	120	0.26
40	458.10005	50	0.11
50	458.10010	100	0.22
60	458.10013	130	0.28

Channel Frequency: 458.10000 MHz
 Voltage & Power Level: 13.3 Volts @ 1.0 Watts
 Highest Variation: 0.44 ppm

Temperature (Deg C)	Measured Frequency (MHz)	Frequency Error (Hz)	Frequency Error (ppm)
-30	458.10020	200	0.44
-20	458.10013	130	0.28
-10	458.10018	180	0.39
0	458.10019	190	0.41
10	458.10017	170	0.37
20	458.10015	150	0.33
30	458.10008	80	0.17
40	458.10002	20	0.04
50	458.10011	110	0.24
60	458.10016	160	0.35

NAME OF TEST: Transmitter Occupied Bandwidth

RULE PART NUMBER: 2.201, 2.202, 2.1033 (c)(14), 2.1049 (h), 2.1041;90.203(j)(3)

Necessary Bandwidth Measurement

This radio modem uses digital modulation signals, passing through a linear 8th order low-pass filter (Raise-Cosine alpha 1 approximation), to an FM transceiver. The necessary bandwidth calculation for this type of modulation (DRCMSK) is not covered by paragraphs (1), (2) or (3) from 2.202(c). Therefore, the approach outlined in (2.202(c)(4)) is applicable in this case.

The measurement explanations are provided in “Annex” (following pages)

Necessary Bandwidth Measurement:

Peak deviation = ±4 kHz

Modulator signal bit rate 19200 bps,

Bn=15260 Hz

The corresponding emission designator prefix for necessary bandwidth = 15K3

Table 1 - Measurements results for the INTEGRATR unit , 9600 bps BT.3 and 19200 bps BT.3 and frequency deviations set to obtain specified values .

unit's software settings	measured data (kHz)		Emission designator
	freq. dev	99% occupied BW	
9600 BT.3	3.0	9.24	9K30
19200 BT.3	4.0	15.26	15K3

Also, Spectrum Efficiency (90.203 (j)(3)) requirement: 4800 bits per second per 6.25 kHz of channel bandwidth.

19200bps=4*4800bps so it is efficient for 25 kHz channel

9600bps=2*4800bps so it is efficient for 12.5 kHz channel

ANNEX

Theory of Measurement

The way to define the **Occupied Bandwidth** is “the frequency bandwidth such that, below its lower and above its upper frequency limits, the mean powers radiated are each equal to 0.5 percent of the total mean power radiated by a given emission” (FCC 2.202), the mathematics are as follows:

$$0.005*TP=P_{(f1)}=\int_0^{f1} PSD_{(f)}df$$

$$0.995*TP=P_{(f2)}=\int_0^{f2} PSD_{(f)}df$$

$$OBW=f2-f1$$

where TP (total mean power) is

$$TP=\int_0^{+\infty} PSD_{(f)}df=(1/t)\int_{-\infty}^{+\infty} |z_{(t)}|^2 dt$$

and PSD (power spectral distribution) is

$$PSD_{(f)}=|Z_{(f)}|^2+|Z_{(-f)}|^2 \quad 0\leq f<4$$

and expresses the positive frequency representation of the transmitter output power for z(t) signal.

By applying these mathematics to the measurements, it is possible to measure the Occupied Bandwidth using the RF signal's trace provided by a digital spectrum analyzer and processed further by computational methods.

The Occupied Bandwidth measurement is in two parts relatively independent of each other. The first gives the RF spectrum profile, and the second calculates the frequency limits and they result in the Occupied bandwidth. While the first involves RF measurement instrumentation, the second is strictly a computational part related to measured trace.

Getting an equally-sampled RF power spectrum profile requires a Digital Spectrum Analyzer. In addition to the instrument's usual requirements, a special attention must be paid to the analyzer's span (bandwidth to be investigated).

This bandwidth must be large enough to contain all the power spectral components created by the transmitter. The frequency step, where the samples are picked, is directly dependent on the span's value.

$$\Delta f= \text{span}/\text{number of points displayed}$$

The frequency resolution will determine the measurement accuracy. So for greater accuracy, less bandwidth will give better values because of the constant number of points that can be displayed. Taking into account the purpose of transmitter, an acceptable balance can be set. For channel-limited transmitters all the power spectral components can be found in main channel and a number of adjacent channels, upper and lower, from the main channel. The relation between these two requirements, number of channels and accuracy, is depicted by:

$$a(\%) \cong (2*k*n/N)*100,$$

where a is desired accuracy, in percentage units, n is the number of channels in span, including main channel, N is displayed number of points and k= (authorized bandwidth) /channel bandwidth.

For usual spectrum analyzers $N\cong 500$, $k=0.8$ (20/25) for 25kHz channel transmitters or $k=0.9$ (11.25/12.5) for 12.5kHz channel transmitters, so $a \cong n/2.5$ (%) can estimate the expected precision for measurement.

All other requirements for spectrum analyzer are the same as they are for mask compliance determination.

The second part has computational requirements related to the trace's values processing.

The following operations must be performed over the trace's (x,y) points:

1. convert y value in dBm (or the analyzer's display y units) units power sample
2. convert y value in W units power sample,
3. add to total power every power sample and get total power value (W units for total power)
4. set low level (0.5%*total power)
5. detect x1-sample which pass low level (convert f1 integrals to sample summing)
6. convert (x1-1)-sample value in frequency units (the x-sample is already in occupied bandwidth),
7. store first frequency correspondent to (x1-1)-sample
8. set up level (99.5%*total power)
9. detect x2-sample which pass up level (convert f2 integrals to sample summing)
10. convert (x2)-sample value in frequency units (the x-sample is now out of occupied bandwidth),
11. store second frequency correspondent to (x2)-sample
12. read the frequency difference , this is **Occupied Bandwidth**, and display the result.

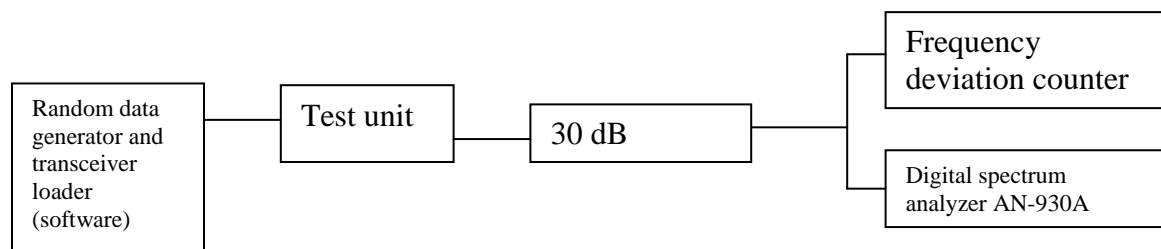
Standard calculation precision is all that is required. The main error factor being the y display resolution is covering calculation precision.

The absolute error for this measurement is $-0/+2*f$. It is not possible to decrease span bandwidth under 2 channels bandwidth because this will affect the significance of result by cutting off the power's spectral distribution edges.

Measurement Set-Up

For the above requirements, the occupied bandwidth of a transmitter was measured using an IFR AN930 A spectrum analyzer having adequate macrofunction to perform computational part. The number of power spectrum samples (N) is 500. Because in test results frequency deviation was also a parameter, measurement instruments were completed with an IFR COM-120 B for frequency deviation determination.

The measurement set-up is:



The AN-930 A spectrum analyzer's parameters are adjusted as follow:

-total span is adjusted at $2.8 \times$ channel space this means 70 kHz for 25 kHz channel and 35 kHz for 12.5 kHz channel. This setting will result in frequency sample step (f) of 140 Hz for 25 kHz channel and 70 Hz for 12.5 kHz channel.

-RBW is set to 300 Hz, this is better than 1% of total span bandwidth.

-video filter is set to 1Khz;

-all other parameter of the instrument are automatically adjusted to obtain calibrated measurements (sweep time 4s).

-central frequency and reference level are adjusted to the unmodulated carrier frequency and level.

The AN 930 A spectrum analyzer's Occupied Bandwidth macrofunction input parameters are:

-central frequency, same as above, the unmodulated carrier frequency.

-channel spacing, 25 kHz or 12.5 kHz according to the signal,

-percentage of Occupied Bandwidth 99%.

The macro operations are:

-the trace is read;

-follow all the computational steps required.

Each sample is converted from dBm to mW and add to total power (tpow) variable. Then are computed the limits of 0.5% and 99.5% by using variable remaining percent (RemPer), and in same time are stored sample number where these two percentage meet. Then are assigned to the markers the correspondent frequencies of numbers.

- Occupied Bandwidth is then displayed as Delta mode marker (difference between markers).

-return to operational mode.

NOTE 1: The computational part could be performed on every device featured with data acquisition.

NOTE 2: An approximation of the occupied bandwidth calculation can be performed by measuring at the points at which the spectrum, measured with a spectrum analyzer of 300 Hz resolution bandwidth, is 25dB down relative to the unmodulated carrier reference level.

NAME OF TEST: Transmitter Occupied Bandwidth for Emission Designators
9K30 F1D

RULE PART NUMBER: 2.202, 90.209 (b)(5), 90.210(e), 2.1049 (c) (1)

MINIMUM STANDARDS: Mask D
Sidebands and Spurious [Rule 90.210 (d), P = 5 Watts]
Authorized Bandwidth = 11.25 kHz [Rule 90.209(b) (5)]
From Fo to 5.625 kHz, down 0 dB. Greater than 5.625 kHz to 12.5 kHz, down 7.27($f_d - 2.88\text{kHz}$) dB. Greater than 12.5 kHz, at least $50 + 10\log_{10}(P)$ or 70 dB, whichever is the lesser of the attenuation.

Attenuation = 0 dB at Fo to 5.625 kHz
Attenuation = 20 dB at 5.625 kHz and 70 dB at 12.5 kHz
Attenuation = 57 dB at > 12.5 kHz

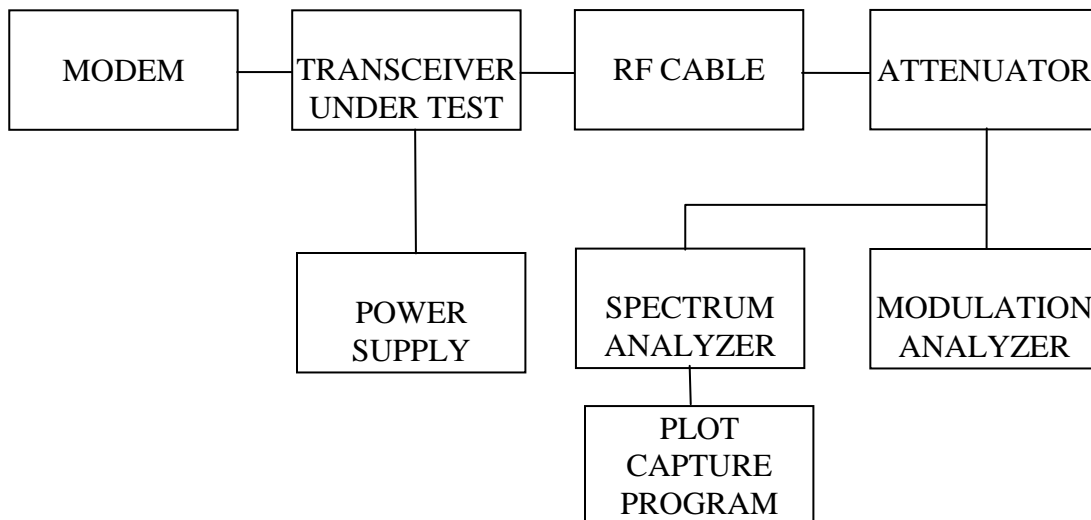
TEST RESULTS: Meets minimum standards (see data on following page)

TEST CONDITIONS: Standard Test Conditions, 25 C
RF Power Level = 1 Watt and 5 Watts
Voltage = 13.3VDC

TEST PROCEDURE: TIA/EIA – 603-C

TEST EQUIPMENT: 50-Ohm Attenuator, Bird Electronics 50-A-FFN-20 (20dB, 50W)
Power Supply, Agilent 6654A
Spectrum Analyzer, Hewlett Packard Model HP8563E
Modulation Analyzer, Hewlett Packard Model HP8901A

TEST SET-UP:



MODULATION SOURCE DESCRIPTION:

The digital modulation type used in the IntegraTR is DRCMSK (Differential Raised Cosine Minimum Shift Keying). A modem using such type of modulation is divided into three main functional units in a CPLD chip:

1. Scrambler:

The scrambler converts the data stream to a new data stream more suitable for FM transmission.

-It randomizes the data to avoid predictable patterns: 00000000, 11111111, 01010101, 00110011, etc.

-It keeps the power spectrum more compact by avoiding sequences like 01010101...

The scrambler is made with a serial shift register and 2 exclusive OR gates which implement the polynomial form X^7+X^5-1 . For the receiver side, a similar circuit performs the descrambling function to decode the received scrambled data.

2. Differential encoder:

After data is scrambled, we encode the data with a differential encoder. The differential encoder XOR's the current input bit with the previous bit. The differential encoder is used to make the modem insensitive to audio polarity inversion of the FM radio system.

3. Waveshape generator:

The waveshape generator converts the processed data bits (scrambled and differentially encoded for DRCMSK) to the DRCMSK audio signal. This audio signal is passed through a low-pass filter before modulating the RF transmitter.

TRANSMISSION PREAMBLE:

Each data transmission begins by sending a 15 millisecond preamble of sinewave (101010...). This is to synchronize the digital phase locked loop of the receiver modem.

TEST PATTERN GENERATOR:

A 30 s test pattern sequence is generated by the test software when the "test data" button is clicked. The highest resulting modulating frequency is (baud rate)/2 Hz. The following pseudo random test pattern was used to modulate the transmitter:

```
###ABCDEFGHIJKLMNQRSTUvwxyz0123456789\r\n,
```

In this pattern ### is replaced by the number of replays, \r is a carriage return and \n is a linefeed. The data is fed to the RS232 interface IC and processed as described above. The async-to-sync conversion, scrambler and differential encoder make the ABCDE... pattern appear random over the air.

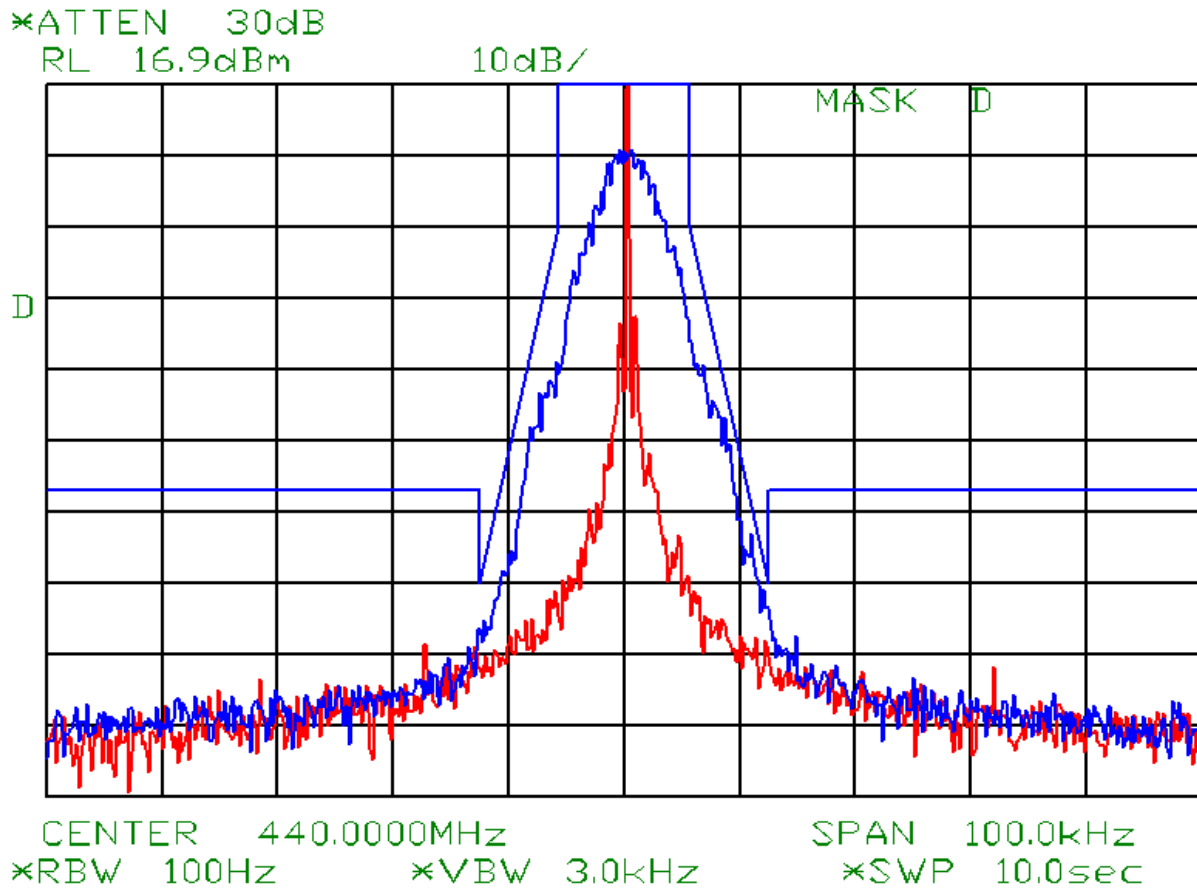
NECESSARY BANDWIDTH (Bn) CALCULATION

See page 15 for Emission Designator determination.

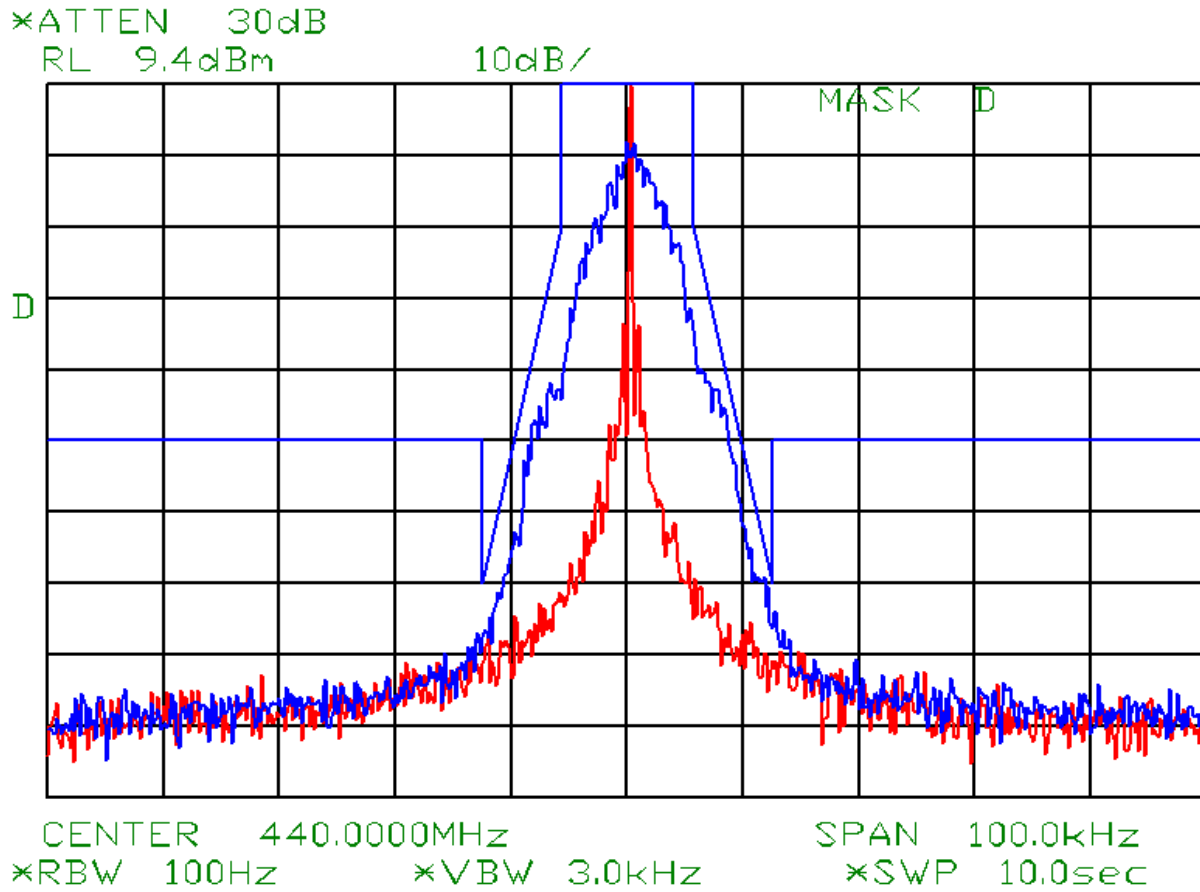
The corresponding emission designator prefix for necessary bandwidth = **9K30**

TEST DATA: Refer to the following graphs:

MASK: D for 5W
SPECTRUM FOR EMISSION 9K30F1D
OUTPUT POWER: 5 Watts
9600 bps
PEAK DEVIATION = 2500 Hz
SPAN = 100 kHz



MASK: D for 1W
SPECTRUM FOR EMISSION 9K30F1D
OUTPUT POWER: 1 Watt
9600 bps
PEAK DEVIATION = 2500 Hz
SPAN = 100 kHz

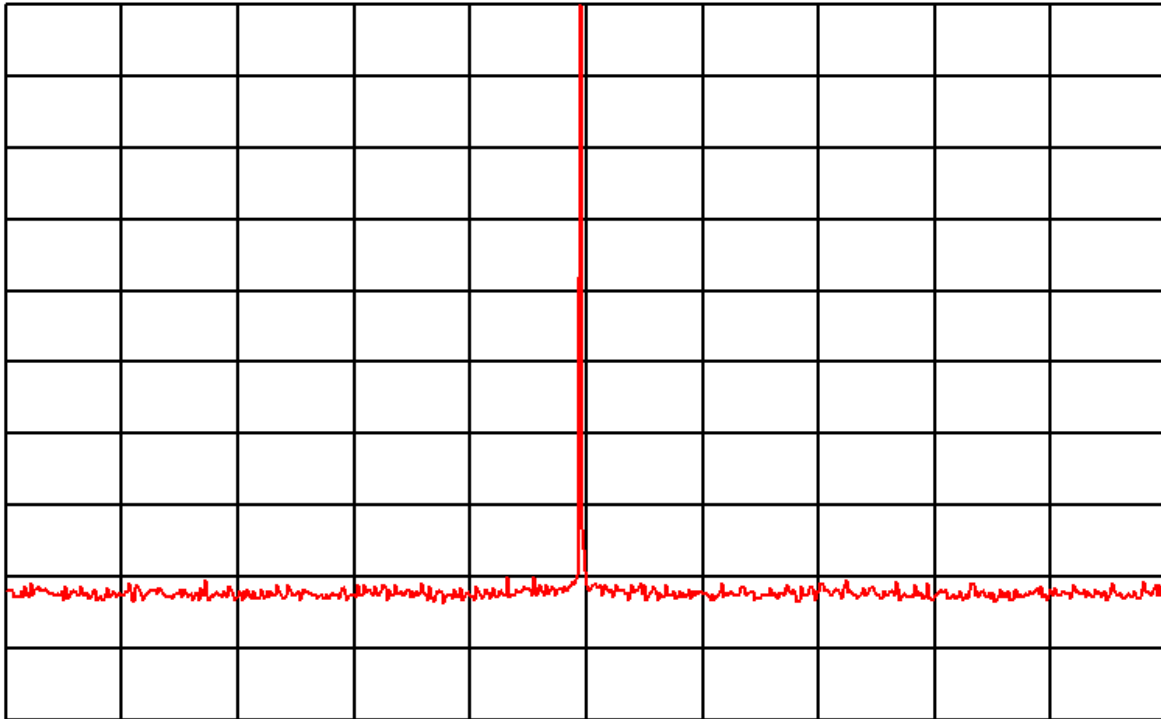


WIDE SPAN = 100 MHz
OUTPUT POWER: 5 Watts

*ATTEN 30dB
RL 16.9dBm

10dB/

D



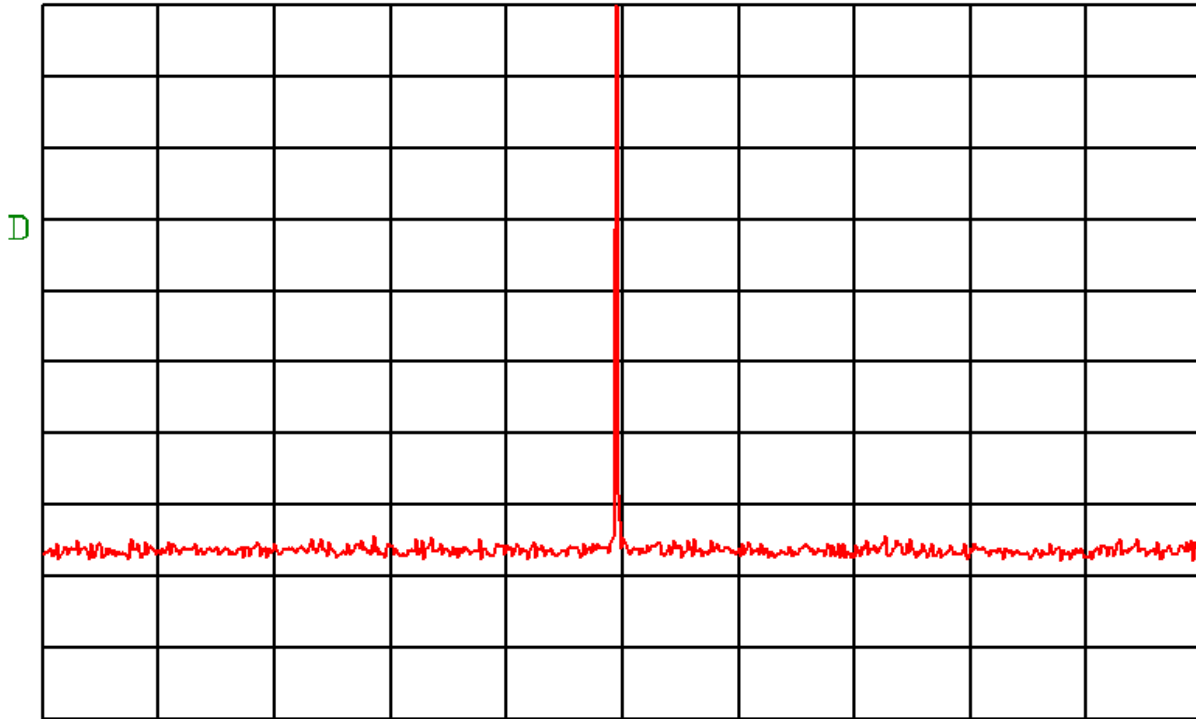
CENTER 440.0MHz
*RBW 10kHz *VBW 10kHz

SPAN 100.0MHz
*SWP 2.50sec

WIDE SPAN = 100 MHz
OUTPUT POWER: 1 Watt

*ATTEN 30dB
RL 9.4dBm

10dB/



CENTER 440.0MHz
*RBW 10kHz *VBW 10kHz

SPAN 100.0MHz
*SWP 2.50sec

NAME OF TEST: Transmitter Occupied Bandwidth for Emission Designators
15K3 F1D

RULE PART NUMBER: 2.201, 2.202, 2.1033 (c)(14), 2.1049(h), 2.1041, 90.209(b)(5), 90.210 (b)

MINIMUM STANDARD: Mask B
Sidebands and Spurious [Rule 90.210 (b), P = 5 Watts]
Authorized Bandwidth = 20 kHz [Rule 90.209(b) (5)]
From Fo to 50% of Authorized BW Removed from Fo, down 0 dB.
From 50% to 100% removed, at least 25 dB.
From 100% to 250% removed, at least 35 dB.
Greater than 250% remove, at least 43 + 10log₁₀(P) dB.

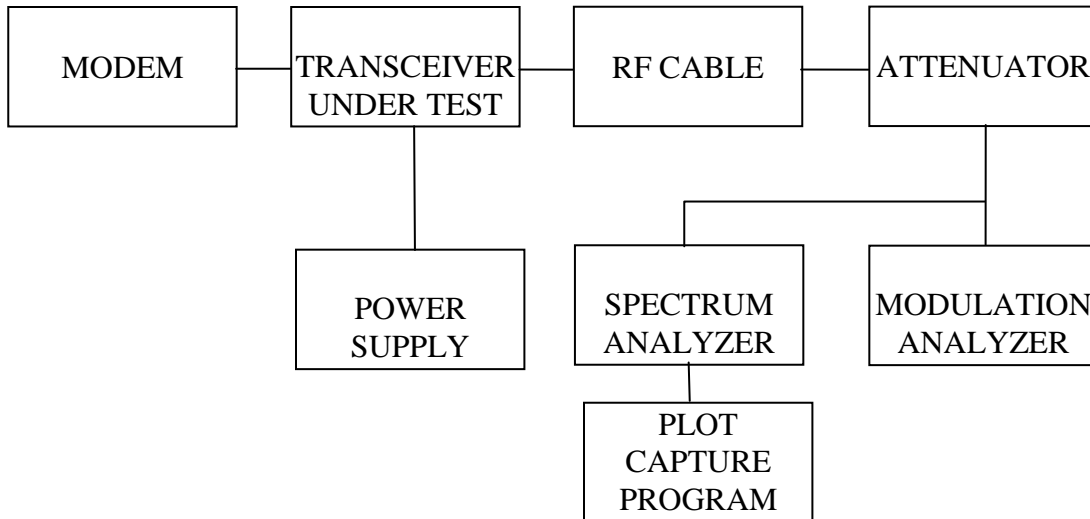
Fo to 10 kHz Attenuation = 0 dB
10 kHz to 20 kHz, Attenuation = 25 dB minimum
20 kHz to 50 kHz, Attenuation = 35 dB minimum
> 50 kHz, Attenuation = 50 dB minimum (5 watts)
> 50 kHz, Attenuation = 43 dB minimum (1 watt)

TEST RESULTS: Meets minimum standard (see data on the following pages)

TEST CONDITIONS: Standard Test Conditions, 25 C

TEST EQUIPMENT: 50-Ohm Attenuator, Bird Electronics 50-A-FFN-20 (20dB, 50W)
Power Supply, Agilent 6654A
Spectrum Analyzer, Hewlett Packard Model HP8563E
Modulation Analyzer, Hewlett Packard Model HP8901A

TEST SET-UP:



MODULATION SOURCE DESCRIPTION:

The digital modulation type used in the INTEGRA is DRCMSK (Differential Raised Cosine Minimum Shift Keying). A modem using such type of modulation is divided into three main functional units in a CPLD chip:

1. Scrambler:

The scrambler converts the data stream to a new data stream more suitable for FM transmission.

-It randomizes the data to avoid predictable patterns: 00000000, 11111111, 01010101, 00110011, etc.

-It keeps the power spectrum more compact by avoiding sequences like 01010101...

The scrambler is made with a serial shift register and 2 exclusive OR gates which implement the polynomial form X^7+X^5-1 . For the receiver side, a similar circuit performs the descrambling function to decode the received scrambled data.

2. Differential encoder:

After data is scrambled, we encode the data with a differential encoder. The differential encoder XOR's the current input bit with the previous bit. The differential encoder is used to make the modem insensitive to audio polarity inversion of the FM radio system.

3. Waveshape generator:

The waveshape generator converts the processed data bits (scrambled and differentially encoded for DRCMSK) to the DRCMSK audio signal. This audio signal is passed through a low-pass filter before modulating the RF transmitter.

TRANSMISSION PREAMBLE:

Each data transmission begins by sending a 15 millisecond preamble of sinewave (101010...). This is to synchronize the digital phase locked loop of the receiver modem.

TEST PATTERN GENERATOR:

A 30 s test pattern sequence is generated by the test software when the "test data" button is clicked. The highest resulting modulating frequency is (baud rate)/2 Hz. The following pseudo random test pattern was used to modulate the transmitter:

```
###ABCDEFGHIJKLMNQRSTUvwxyz0123456789\r\n,
```

In this pattern ### is replaced by the number of replays, \r is a carriage return and \n is a linefeed. The data is fed to the RS232 interface IC and processed as described above. The async-to-sync conversion, scrambler and differential encoder make the ABCDE... pattern appear random over the air.

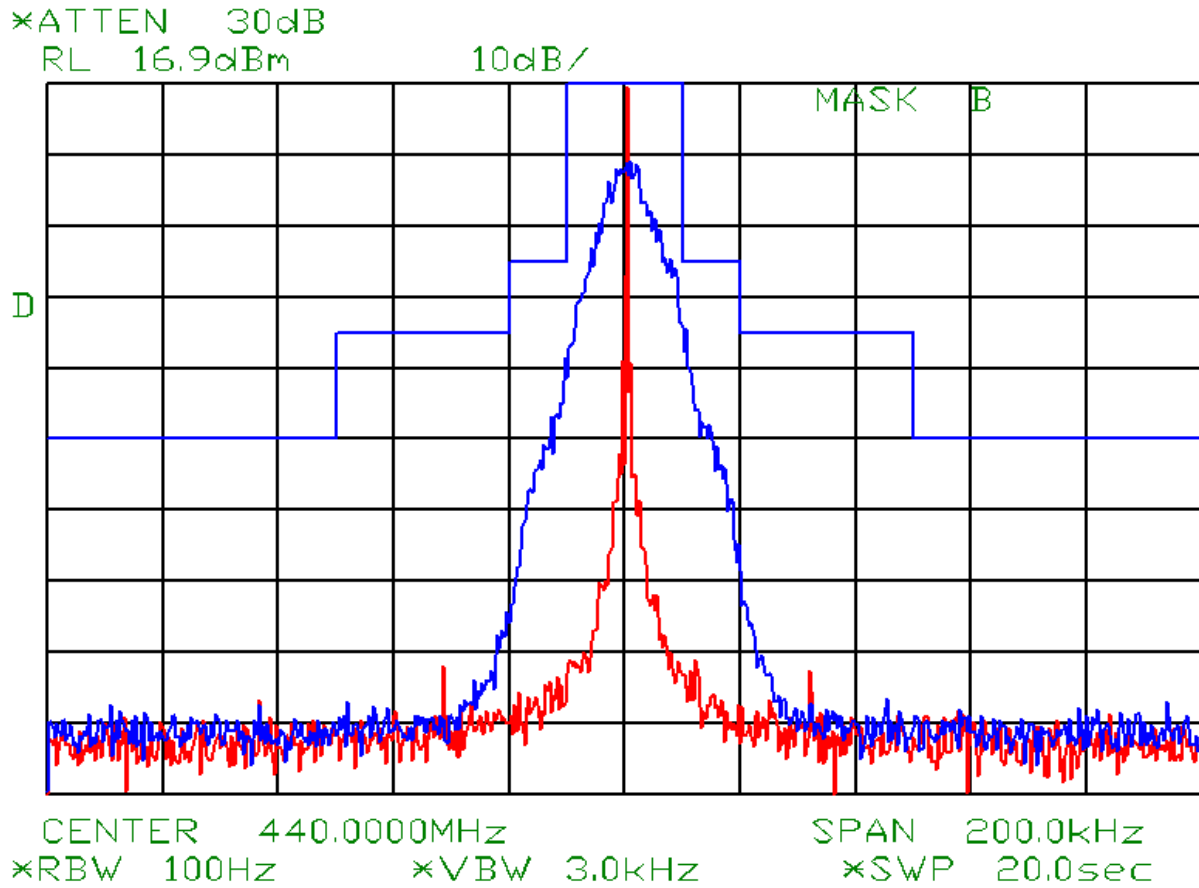
NECESSARY BANDWIDTH (Bn) CALCULATION

See page 15 for Emission Designator determination.

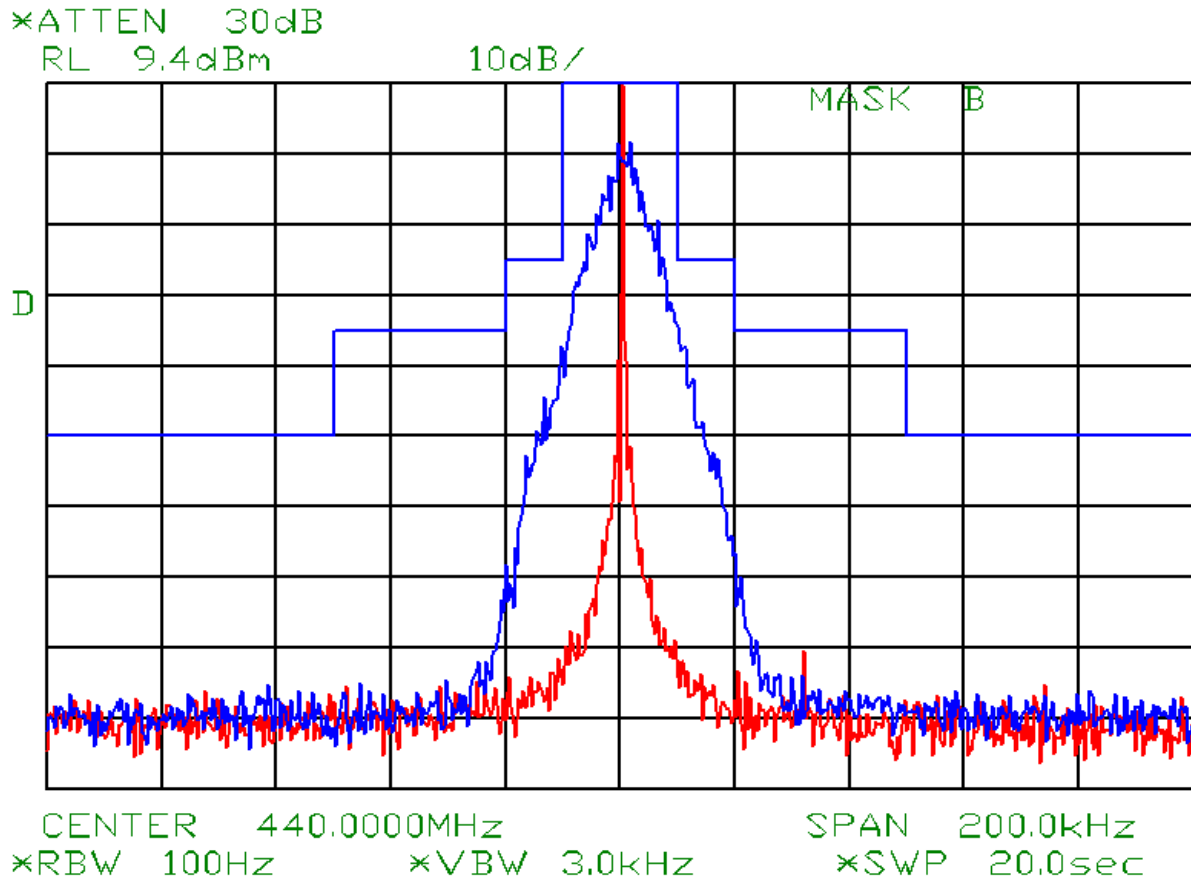
The corresponding emission designator prefix for necessary bandwidth = **15K3**

TEST DATA: Refer to the following graphs:

MASK: B for 5W
SPECTRUM FOR EMISSION **15K3 F1D**
OUTPUT POWER: 5 Watts
19200 bps
PEAK DEVIATION = 4000 Hz
SPAN = 200 kHz



MASK: B for 1W
SPECTRUM FOR EMISSION **15K3 F1D**
OUTPUT POWER: 1 Watts
19200 bps
PEAK DEVIATION = 4000 Hz
SPAN = 200 kHz



NAME OF TEST: Field Strength of Spurious Radiation

RULE PART NUMBER: 2.1053, 90.210 (b,3)(d,3)

MINIMUM STANDARDS: For 5 Watts: $50+10\text{Log}_{10}(5 \text{ Watts}) = -57.0 \text{ dBc}$
or -65dBc , whichever is the lesser attenuation.

For 1 Watt: $50+10\text{Log}_{10}(1 \text{ Watt}) = -50.0 \text{ dBc}$
or -70 dBc , whichever is the lesser attenuation.

TEST RESULTS: Meets minimum standards (see data on following page)

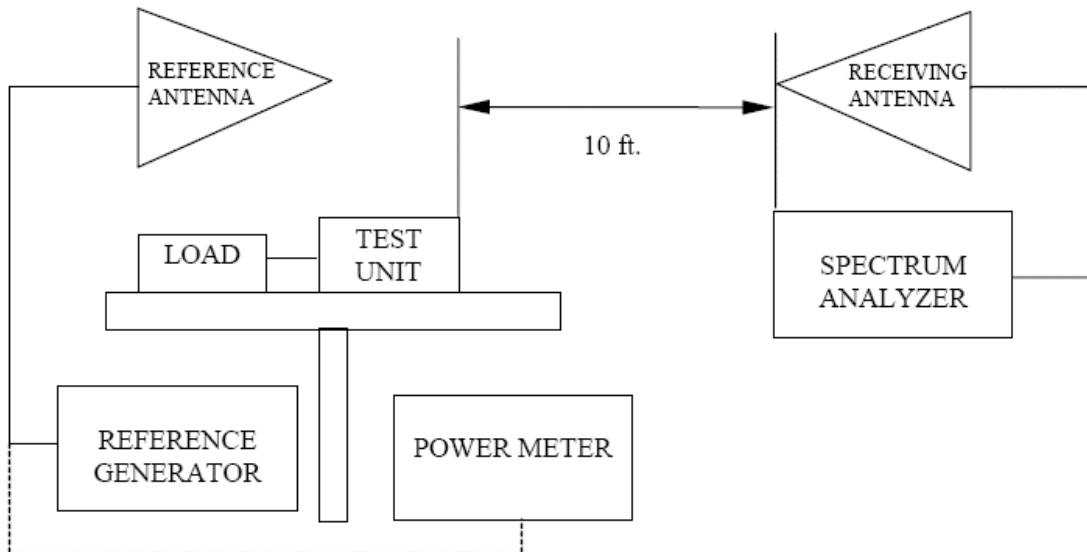
TEST CONDITIONS: Standard Test Conditions, 25 C
RF Power Level = 1 Watt and 5 Watts
Voltage = 13VDC

TEST PROCEDURE: TIA/EIA – 603-C

TEST EQUIPMENT: Waveguide Horn Antenna, EMCO Model 3115
Waveguide Horn Antenna, Electro-Metrics EM-6961
Bilog Antenna, Chase Model CBL6111B
Dipole Antenna, Electro-Metrics Model EM-6924
Power Supply, Model Instek GPS-3303
Spectrum Analyzer, Model HP-8563E
Reference Generator, Agilent Model E82570
Power Meter, Model HP 437B
50-Ohm Attenuator, Bird Electronics 50-A-FFN-20 (20dB, 50W)

MEASUREMENT PROCEDURE: Measurements were made from the lowest radio frequency generated in the equipment to the tenth harmonic of the carrier.

TEST SET-UP:



Integra-TR Low
Band

Frequency: 406.1 MHz Spec = -57.0 dBc
 Highest
 Power: 5 Watts Spur = -62.1 dBc
 37.0 dBm

Spurious Frequency (MHz)	Polarization (Horz/Vert)	Spurious Level (dBm)	Substitution Generator (dBm)	Cable Loss (dB)	Antenna Gain (dBd)	Spurious Attenuation (dBc)
812.2	H	-76.7	-27.7	-3.00	-0.49	-62.1
	V	-78.2	-44.0	-3.00	-0.49	-78.5
1218.3	H	-95.3	-58.0	-3.67	2.75	-88.5
	V	-102.5	-67.5	-3.67	2.75	-98.1
1624.4	H	-108.5	-70.2	-4.67	4.75	-97.7
	V	-107.5	-71.2	-4.67	4.75	-98.7
2030.5	H	-95.3	-54.7	-5.50	4.95	-81.2
	V	-85.3	-44.8	-5.50	4.95	-71.4
2436.6	H	-101.8	-59.5	-6.50	5.55	-84.4
	V	-98.3	-54.7	-6.50	5.55	-79.6
2842.7	H	-99.8	-54.8	-6.83	5.75	-79.2
	V	-98.3	-54.0	-6.83	5.75	-78.4
3248.8	H	-112.0	-61.7	-11.50	5.75	-81.4
	V	-110.8	-60.8	-11.50	5.75	-80.5
3654.9	H	-112.0	-57.7	-10.50	5.95	-78.2
	V	-112.0	-59.8	-10.50	5.95	-80.4
4061	H	-112.0	-56.5	-11.17	5.95	-76.4
	V	-112.0	-58.7	-11.17	5.95	-78.5

Frequency: 406.1 MHz Spec = -50.0 dBc
 Highest
 Power: 1 Watts Spur = -61.8 dBc
 30.0 dBm

Spurious Frequency (MHz)	Polarization (Horz/Vert)	Spurious Level (dBm)	Substitution Generator (dBm)	Cable Loss (dB)	Antenna Gain (dBd)	Spurious Attenuation dBc
812.2	H	-83.3	-34.3	-3.00	-0.49	-61.8
	V	-84.6	-50.5	-3.00	-0.49	-77.9
1218.3	H	-88.0	-50.7	-3.67	2.75	-74.3
	V	-92.8	-57.8	-3.67	2.75	-81.4
1624.4	H	-108.5	-70.2	-4.67	4.75	-90.8
	V	-107.5	-71.2	-4.67	4.75	-91.8
2030.5	H	-99.2	-58.5	-5.50	4.95	-78.1
	V	-90.0	-49.5	-5.50	4.95	-69.1
2436.6	H	-104.8	-62.5	-6.50	5.55	-80.4
	V	-101.0	-57.3	-6.50	5.55	-75.3
2842.7	H	-99.8	-54.8	-6.83	5.75	-72.3
	V	-103.8	-59.5	-6.83	5.75	-76.9
3248.8	H	-112.0	-61.7	-11.50	5.75	-74.4
	V	-112.0	-62.0	-11.50	5.75	-74.8
3654.9	H	-112.0	-57.7	-10.50	5.95	-71.2
	V	-112.0	-59.8	-10.50	5.95	-73.4
4061	H	-112.0	-56.5	-11.17	5.95	-69.4
	V	-112.0	-58.7	-11.17	5.95	-71.6

Integra-TR Low
Band

Frequency: 440 MHz Spec = -57.0 dBc
 Highest
 Power: 5 Watts Spur = -67.3 dBc
 37.0 dBm

Spurious Frequency (MHz)	Polarization (Horz/Vert)	Spurious Level (dBm)	Substitution Generator (dBm)	Cable Loss (dB)	Antenna Gain (dBd)	Spurious Attenuation (dBc)
880	H	-71.5	-34.8	-3.17	-0.46	-69.1
	V	-70.7	-33.0	-3.17	-0.46	-67.3
1320	H	-83.8	-44.0	-4.00	4.75	-72.2
	V	-86.7	-50.8	-4.00	4.75	-79.1
1760	H	-90.7	-50.5	-4.67	4.95	-77.9
	V	-91.3	-51.0	-4.67	4.95	-78.4
2200	H	-96.5	-55.2	-5.83	4.95	-81.4
	V	-84.8	-42.2	-5.83	4.95	-68.4
2640	H	-92.0	-46.3	-6.50	5.55	-71.3
	V	-89.7	-43.2	-6.50	5.55	-68.1
3080	H	-106.2	-57.2	-10.00	5.75	-78.4
	V	-101.8	-52.3	-10.00	5.75	-73.5
3520	H	-112.0	-61.2	-10.17	5.95	-82.0
	V	-110.5	-59.2	-10.17	5.95	-80.0
3960	H	-108.7	-55.5	-9.83	5.95	-76.7
	V	-112.7	-59.7	-9.83	5.95	-80.9
4400	H	-107.7	-54.4	-11.00	7.05	-73.3
	V	-107.0	-53.8	-11.00	7.05	-72.8

Frequency: 440 MHz Spec = -50.0 dBc
 Highest
 Power: 1 Watts Spur = -62.4 dBc
 30.0 dBm

Spurious Frequency (MHz)	Polarization (Horz/Vert)	Spurious Level (dBm)	Substitution Generator (dBm)	Cable Loss (dB)	Antenna Gain (dBd)	Spurious Attenuation dBc
880	H	-80.8	-44.2	-3.17	-0.46	-71.5
	V	-79.0	-41.3	-3.17	-0.46	-68.6
1320	H	-82.7	-42.8	-4.00	4.75	-64.1
	V	-106.0	-70.2	-4.00	4.75	-91.4
1760	H	-103.5	-63.3	-4.67	4.95	-83.7
	V	-102.3	-62.0	-4.67	4.95	-82.4
2200	H	-94.8	-53.5	-5.83	4.95	-72.7
	V	-85.8	-43.2	-5.83	4.95	-62.4
2640	H	-93.3	-47.7	-6.50	5.55	-65.6
	V	-99.2	-52.7	-6.50	5.55	-70.6
3080	H	-99.2	-50.2	-10.00	5.75	-64.4
	V	-107.7	-58.2	-10.00	5.75	-72.5
3520	H	-112.0	-61.2	-10.17	5.95	-75.1
	V	-110.5	-59.2	-10.17	5.95	-73.1
3960	H	-112.0	-58.8	-9.83	5.95	-73.1
	V	-112.7	-59.7	-9.83	5.95	-73.9
4400	H	-107.7	-54.4	-11.00	7.05	-66.3
	V	-106.7	-53.5	-11.00	7.05	-65.5

Integra-TR High
Band

Frequency: 440 MHz Spec = -57.0 dBc
 Highest
 Power: 5 Watts Spur = -62.4 dBc
 37.0 dBm

Spurious Frequency (MHz)	Polarization (Horz/Vert)	Spurious Level (dBm)	Substitution Generator (dBm)	Cable Loss (dB)	Antenna Gain (dBd)	Spurious Attenuation dBc
880	H	-80.5	-43.8	-3.17	-0.46	-78.1
	V	-87.7	-50.0	-3.17	-0.46	-84.3
1320	H	-85.0	-45.2	-4.00	4.75	-73.4
	V	-89.2	-53.3	-4.00	4.75	-81.6
1760	H	-96.5	-56.3	-4.67	4.95	-83.7
	V	-86.3	-46.0	-4.67	4.95	-73.4
2200	H	-88.0	-46.7	-5.83	4.95	-72.9
	V	-84.0	-41.3	-5.83	4.95	-67.5
2640	H	-83.2	-37.5	-6.50	5.55	-62.4
	V	-85.3	-38.8	-6.50	5.55	-63.8
3080	H	-95.0	-46.0	-10.00	5.75	-67.2
	V	-93.3	-43.8	-10.00	5.75	-65.1
3520	H	-104.7	-53.9	-10.17	5.95	-74.7
	V	-102.5	-51.2	-10.17	5.95	-72.0
3960	H	-100.2	-47.0	-9.83	5.95	-68.2
	V	-104.0	-51.0	-9.83	5.95	-72.2
4400	H	-100.0	-46.7	-11.00	7.05	-65.6
	V	-97.3	-44.2	-11.00	7.05	-63.1

Frequency: 440 MHz Spec = -50.0 dBc
 Highest
 Power: 1 Watts Spur = -66.3 dBc
 30.0 dBm

Spurious Frequency (MHz)	Polarization (Horz/Vert)	Spurious Level (dBm)	Substitution Generator (dBm)	Cable Loss (dB)	Antenna Gain (dBd)	Spurious Attenuation (dBc)
880	H	-85.8	-49.2	-3.17	-0.46	-76.5
	V	-90.2	-52.5	-3.17	-0.46	-79.8
1320	H	-84.8	-45.0	-4.00	4.75	-66.3
	V	-87.7	-51.8	-4.00	4.75	-73.1
1760	H	-103.5	-63.3	-4.67	4.95	-83.7
	V	-103.3	-63.0	-4.67	4.95	-83.4
2200	H	-101.8	-60.5	-5.83	4.95	-79.7
	V	-99.3	-56.7	-5.83	4.95	-75.9
2640	H	-98.8	-53.2	-6.50	5.55	-71.1
	V	-100.0	-53.5	-6.50	5.55	-71.5
3080	H	-111.5	-62.5	-10.00	5.75	-76.8
	V	-110.8	-61.3	-10.00	5.75	-75.6
3520	H	-111.5	-60.7	-10.17	5.95	-74.6
	V	-110.8	-59.5	-10.17	5.95	-73.4
3960	H	-110.7	-57.5	-9.83	5.95	-71.8
	V	-111.3	-58.3	-9.83	5.95	-72.5
4400	H	-108.3	-55.0	-11.00	7.05	-66.9
	V	-107.5	-54.3	-11.00	7.05	-66.3

Integra-TR High
Band

Frequency: 476 MHz Spec = -57.0 dBc
 Highest
 Power: 5 Watts Spur = -61.7 dBc
 37.0 dBm

Spurious Frequency (MHz)	Polarization (Horz/Vert)	Spurious Level (dBm)	Substitution Generator (dBm)	Cable Loss (dB)	Antenna Gain (dBd)	Spurious Attenuation dBc
952	H	-84.0	-49.3	-3.17	-0.54	-83.7
	V	-90.0	-43.7	-3.17	-0.54	-78.0
1428	H	-85.3	-50.0	-4.17	4.75	-78.1
	V	-86.0	-45.8	-4.17	4.75	-73.9
1904	H	-83.8	-42.2	-5.00	4.95	-69.2
	V	-76.0	-34.7	-5.00	4.95	-61.7
2380	H	-83.2	-38.7	-5.67	5.55	-64.4
	V	-88.3	-44.7	-5.67	5.55	-70.4
2856	H	-104.5	-59.5	-6.83	5.75	-83.9
	V	-104.5	-60.2	-6.83	5.75	-84.6
3332	H	-108.2	-59.2	-10.33	5.95	-79.9
	V	-107.7	-57.2	-10.33	5.95	-77.9
3808	H	-108.5	-58.0	-9.67	5.95	-79.4
	V	-110.5	-57.3	-9.67	5.95	-78.7
4284	H	-101.3	-48.8	-10.83	7.05	-67.9
	V	-102.8	-48.5	-10.83	7.05	-67.6
4760	H	-106.2	-52.4	-11.33	6.75	-71.3
	V	-104.8	-49.1	-11.33	6.75	-68.0

Frequency: 476 MHz Spec = -50.0 dBc
Highest
Power: 1 Watts Spur = -63.0 dBc
30.0 dBm

Spurious Frequency (MHz)	Polarization (Horz/Vert)	Spurious Level (dBm)	Substitution Generator (dBm)	Cable Loss (dB)	Antenna Gain (dBd)	Spurious Attenuation dBc
952	H	-83.7	-49.0	-3.17	-0.54	-76.4
	V	-90.5	-44.2	-3.17	-0.54	-71.5
1428	H	-81.3	-46.0	-4.17	4.75	-67.1
	V	-86.0	-45.8	-4.17	4.75	-66.9
1904	H	-102.2	-60.5	-5.00	4.95	-80.6
	V	-99.2	-57.8	-5.00	4.95	-77.9
2380	H	-94.0	-49.5	-5.67	5.55	-68.3
	V	-97.8	-54.2	-5.67	5.55	-72.9
2856	H	-104.5	-59.5	-6.83	5.75	-76.9
	V	-108.0	-63.7	-6.83	5.75	-81.1
3332	H	-111.3	-62.3	-10.33	5.95	-76.0
	V	-111.2	-60.7	-10.33	5.95	-74.4
3808	H	-107.0	-56.5	-9.67	5.95	-70.9
	V	-110.5	-57.3	-9.67	5.95	-71.7
4284	H	-107.0	-54.5	-10.83	7.05	-66.6
	V	-108.0	-53.7	-10.83	7.05	-65.8
4760	H	-108.7	-54.9	-11.33	6.75	-66.8
	V	-106.7	-51.0	-11.33	6.75	-63.0

Equipment Calibration Information

Equipment	Serial Number	Cal Date	Cal Due
HP 8563E Spectrum Analyzer	3221A00149	4/15/2010	4/15/2012
Agilent E8257D Signal Generator	MY44320507	4/20/2010	4/20/2012
HP 8901A Modulation Analyzer	2950A05551	4/12/2010	4/12/2012
HP 437B Power Meter	3125U13882	4/12/2010	4/12/2012

Instruments have been calibrated using standards with accuracies traceable to NIST standards.