Measurement of Processing Gain of the JX-4000F

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Wireless LAN Division

Clarion Corp. of America

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1. A GENERAL DEFINITION OF THE PROCESSING GAIN

The nominal processing gain for a direct-sequence spread-spectrum system is simply the number of chips $N_{\rm e}$ in the symbol waveform; it represents the theoretical rejection of a center-band narrowband interferer, averaged over all chip-code patterns. The practical processing gain of the system must also take into account the SNR (Signal to Noise Ratio) required for adequately low demodulation errors and the system implementation losses. The practical processing gain Gp is defined by 1

$$Gp = (S/N)_{reg} + Mj + Lsys$$
 (1)

(all in dB) where

- (S/N) req is the minimum signal-to-noise ratio after despreading at which the given modulation can provide adequate error performance,
- Mj is the maximum ratio of interference power to the signal power, measured at the system input, for which the system can provide the adequate error performance,
- Lsys is the system implementation losses in SNR due to practical implementation limitations.

2. CONSIDERATION OF ACTUAL PROCESSING GAIN

First, the values used for S/N and Lsys will be discussed, then the measured values of Mj will be presented.

2.1.REQUIRED SNR

The data modulation employed is a form of bi-orthogonal signaling in which transmission of one of 32 waveforms, these differing in the spreading code pattern, conveys five bits of information during each 16-chip data symbol. The theoretical coherent S/N performance in terms of probability of symbol error (P_{SE}) can be seen in the graph on page 259 in a book of Wozencraft and Jacobs². This analysis is appended on page 263 of the book, which shows that the 32 channel bi-orthogonal performance is approximately equal to the 16 channel orthogonal performance shown on page 259. The JX-4000F, applying to the FCC, processes In-phase and Quadrature-phase correlation channels, and then noncoherently combines the results; thus, it would be expected to perform a fraction of a dB worse (at good S/N) than the fully coherent (recovered carrier) case shown in the book. In fact, the manufacturer has performed simulation, numerical computation, and experimentation (using unfiltered, perfectly timed received waveforms) to verify this performance. The results of the numerical computation are shown in Figure 1.

¹ Dixon, R, Spread Spectrum Systems, Chapter 1 (New York: Wiley, 1994)

² Wozencraft and Jacobs, Principles of Communication Engineering, John Wiley & Sons, Inc., New York, 1965

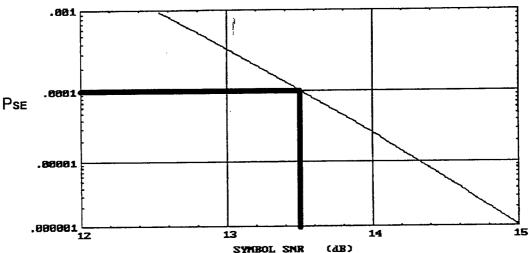


Figure 1

As expected, at low P_{SE} , these results are within 0.5 dB of the coherent performance expected from the theoretical analysis described above. It is the manufacturers view that adequate system performance is still achieved when the JX-4000F has degraded to 75% of its maximum throughput. As will be shown by calculation in the next section, this level of throughput results for a P_{SE} of 10^{-4} (recall that each symbol consists of 5 data bits), resulting in an operating point output SNR = 13.5 dB.

The processing gain does not change rapidly with operating point. The 75% point of its maximum throughput (a loss of approximately 160 frames/sec out of 640 frames/sec) results in good measurement accuracy; Effects of the computer interface and long time averaging are minimized. Because of the proprietary re-transmission protocol that can be enabled in the JX-4000F, this level of frame loss does not render the link ineffective.

2.2. ANTICIPATED SYSTEM LOSS

System loss is due to a multitude of effects which include various filters, signal quantization, computation errors, timing misalignment, etc. The very tight filtering required to conform to FCC part 15 regulations (the 2400-to-2483.5-MHz band resides between two protected bands which constrain the absolute levels of signal power which may be produced, unlike the relative-power-level constraint of the part 15.247 alone) causes mismatch between the transmitted waveform and the much-less-filtered reference waveforms in the correlator bank. This causes a loss of approximately 0.8 dB loss. Signal quantization as well as round-off and truncation within the digital correlation subsystem result in approximately 0.45 dB departure from ideal. Timing error in the placement of the correlation processor relative to the received signal results in an average loss of 0.25 dB. The total implementation loss is consequently 1.5 dB.

MICRILOR/CLARION PROPRIETABY 3. MEASUREMENT PROCEDURE OF THE PROCESSING GAIN

The practical processing gain may be measured using the CW jamming margin method. Figure 2 shows the test configuration. The actual test site is shown in Appendix-A.

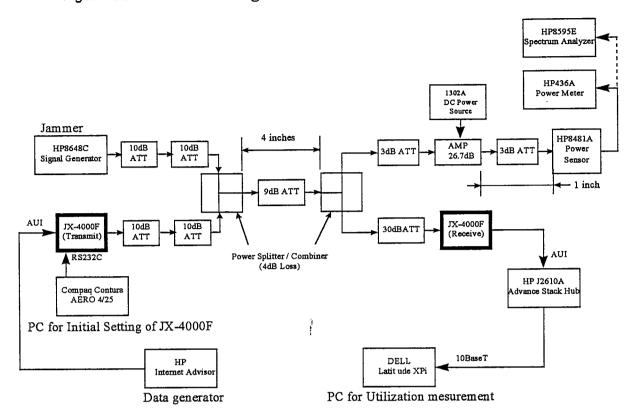


Figure 2

The "HP Internet advisor", a data generator, is the source of continuous Ethernet frames. The rate of frame sourcing and all frame parameters can be set. The output of the "HP Internet Advisor" is fed to the Ethernet MAU port on the JX-4000F (Transmit). A "Compaq Contura" PC is used on a local RS-232 control port on the JX-4000F for the initial setting of the transmitter. An "HP8648C" signal generator is used as a jammer (causes CW interference). The desired signal and CW jamming signal are combined and then split for observation of power and for feeding to the JX-4000F (Receive).

The Jammer-to-Signal (J/S) ratio is measured using HP 436A power meter. The power meter readout of the desired signal must be compensated using the transmit stream duty factor of the desired signal frames. The detailed compensation procedure is described in Appendix-B. The spectrum analyzer is exchanged with the power meter only to verify that operation is normal and all spectra are as anticipated.

The output signal of the receiving JX-4000F is a stream of Ethernet frames that is fed through the "HPJ2610A Stack Hub" for conversion of interface from AUI to 10BaseT because no AUI connectors are provided on the "DELL Latitude Xpi" Ethernet card. The "DELL Latitude Xpi" is running "Lanalyzer", a LAN monitoring software package supplied by Novell, used for measuring the rate of frames that are received without any errors (i.e. passed a 32-bit CRC check by the JX-4000F).

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Although the data rate is actually 10 Mbps, the software that assigns frame buffers in the JX-4000F limits the overall throughput. It should be noted that all re-transmission protocol, acknowledgment protocol and error-correction coding are shut off for this measurement. The "HP Internet Advisor" is set to generate Ethernet frames at the maximum rate and maximum length that the JX-4000F will accept them. In this case, a utilization of 82% can be observed at the output without any interference. The JX-4000F will only download frames to the MAU port if the 32-bit CRC has passed. Therefore, only the percentage utilization need be noted on the "Lanalyzer." A measured J/S (equal to jamming margin Mj) at the input of the receiving JX-4000F which results in 61.5% utilization (75% of the maximum utilization of the JX-4000F), corresponds to symbol error rate of 10⁻⁴.

3.1. DETAIL PROCEDURE OF THE MEASUREMENT

The processing gain Gp can be calculated by applying the system loss Lsys of 1.5 dB described above and the measured jamming margin Mj to Equation 1. The processing gain is measured across the band in the steps shown in Table 1.

Table 1

Brequency Range (MHz)	Frequency Step
2400.536 - 2425.536	1 MHz
2425.636 - 2431.036	100 kHz
2431.086 - 2441.136	50 kHz
2441.236 - 2446.536	100 kHz
2447.536 - 2483.536	1 MHz

The output level of the signal generator (HP8648C) is adjusted in 0.1 dB steps. The CW source is shut off to measure the signal power with the "RF OFF" switch on the front panel of the signal generator. This is done after each measurement to account for any time variation of the power level. The signal source is shut off to measure the CW power through the RS-232 control port on the transmitting JX-4000F. This is done after each measurement to account for any variation of the CW source power at each new frequency sample. At each frequency step, the CW source power is varied with 0.1 dB resolution in order to achieve a reading of approximately 62% on the utilization meter. After each measurement, when turning off the CW, the utilization is verified to go back up to 82%. For the band edge measurements, additional padding is inserted in the signal line in order to preserve the accuracy of the relative-power measurements on the power meter for the high J/S values. In the case of any mechanical change to the test setup, the spectra are re-verified on the spectrum analyzer.

The detail of test equipment is described below.:

■ Signal generator (Jammer) : HP 8640C

■ Data generator : HP Internet Advisor, J2522B

■ Transmitter : Spread Spectrum Transceiver, JX-4000F

(Equipment under test)

■ Receiver : Spread Spectrum Transceiver, JX-4000F

(Equipment under test)

■ RF Amplifier : Mini-circuit ZHL1042J, Gain 26.7dB

■ Power meter : HP426A

■ Power Sensor : HP8481A

■ Hub HP J2610A, Advance Stack Hub

Computers : Dell Latitude Xpi and Compaq Contura

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■ Spectrum analyzer : HP 8595E

Power Splitter/Combiner: Mini-circuit 15542 ZFSC-2-2500

4. TEST RESULT

Figure 3 shows actually measured and calculated result of the processing gain of the JX-4000F against CW jammer through entire frequency range of 2400.536MHz to 2483.536MHz. A table of numerical value is shown in Appendix-C.

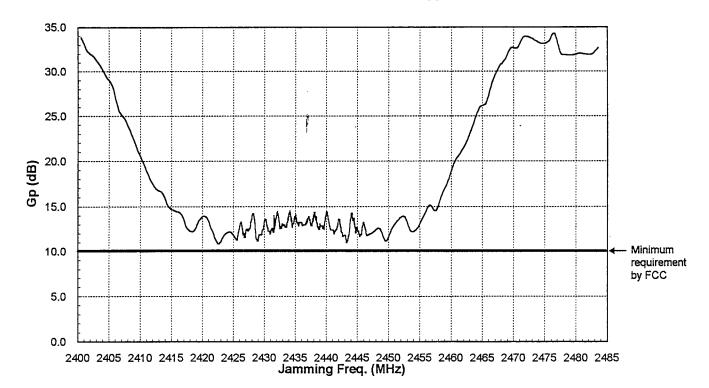


Figure 3

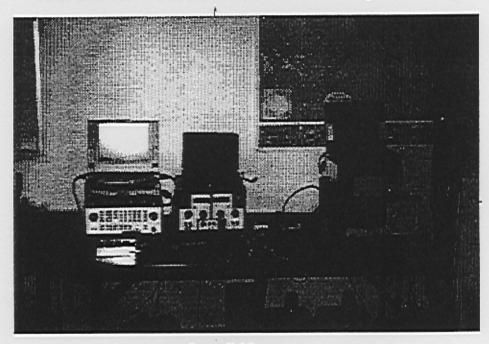
5. CONCLUSION

The processing gain of the JX-4000F has been measured using CW jamming margin method. The result shows that the actual processing gain of the JX-4000F exceeds 10 dB throughout the entire bandwidth of the JX-4000F. This means that the JX-4000F

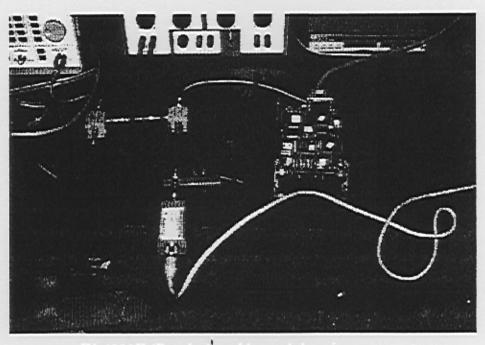
conforms to FCC regulation 15.247(e) prescribes that the processing gain of a direct sequence system shall be at least 10 dB.

Appendix-A

Test Site for Measurement of Processing Gain



Overall View



JX-4000F (Receive) and its peripheral components

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Appendix-B

Compensation Procedure of Power for Desired Signal

Readout of the power meter against desired signal should be compensated to continuous power because

- the power meter responds to average power,
- the JX-4000F transmits burst streams.

Compensation can be done using Equation A1.

$$P_{CONT} = P_{READ} / F_D \tag{A1}$$

where

 P_{CONT} : Continuous transmission power (W) P_{READ} : Readout of the power meter (W)

 F_D : Duty factor of the desired signal (sec/sec).

The duty factor F_D is defined as Equation A2.

$$F_D = D_T / (D_T + D_R) \quad (\text{sec/sec}) \tag{A2}$$

where

 D_T : Duration of transmission (sec)

 D_R : Duration of receive (sec).

Figure A1 shows measurement result of D_T of 1.260 ms under the same condition as processing gain measurement. Figure A2 and Figure A3 show measurement result of D_R under the same condition as processing gain measurement. Two different D_R of 182 μ s and 282 μ s are observed. This flicker of D_R is caused by uncertainty of task duration of a microprocessor. Accordingly, averaged value of 232 μ s may be used because probability of appearance of each value can be considered as equal throughout the response time of the power meter. F_D of the system can be obtained as 0.8445 (-0.73 dB) by applying these values to Equation A2. The readout of the power meter against desired signal can be compensated by applying F_D of this value to Equation A1.

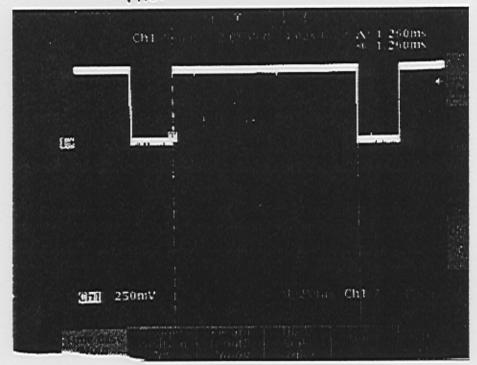


Figure A1

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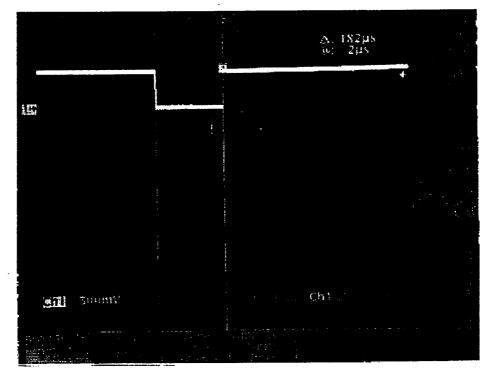


Figure A2

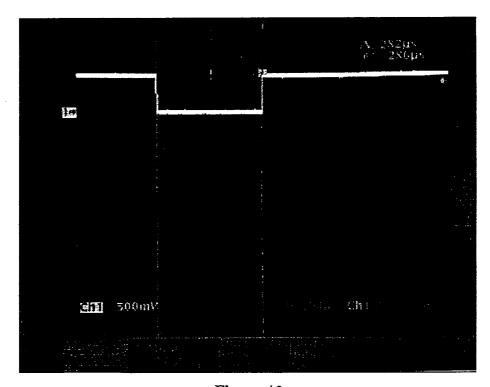


Figure A3

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Appendix-C

Numerical Value of Measured Processing Gain

Jamming	J/S	Gp	Jamming	J/S	Gp	Jamming	J/S	Gp	Jamming	J/S	Gp
frequency (MHz)	(dB)	(dB)	frequency (MHz)	(dB)	(dB)	frequency (MHz)	(dB)	(dB)	frequency (MHz)	(dB)	(dB)
2400.536	18.8	33.8	2427.736	-1.7	13.3	2431.736	-2.1	12.9	2434.086	-0.6	14.4
2401.536	17.3	32.3	2427.836	-1.6	13.4	2431.786		13.5	2434.136	141-1414-1414-1414-1414-141	14.6
2402.536	16.7	31.7	2427.936	-1.3	13.7	2431.836		13.7	2434,186		14.0
2403.536	15.7	30.7	2428.036	-0.8	14.2	2431.886		13.7	2434.236		14.1
2404.536	14.4	29.4	2428.136	-0.8	14.2	2431.936		13.9	2434.286	0.0000000000000000000000000000000000000	13.4
2405.536	13.3	28.3	2428,236	-0.8	14.2	2431.986		14.3	2434.336		13.8
2406.536	10.6	25.6	2428.336	-1.3	13.7	2432.036		14.3	2434.386		13.3
2407.536	9.6	24.6	2428.436	-1.9	13.1	2432.086		14.5	2434.436	3333533333333333	13.3
2408.536	8.0	23.0	2428.536	-2.7	12.3	2432.136		14.4	2434.486		12.7
2409.536	6.2	21.2	2428.636	000000000000000000000000000000000000000	11.5	2432.186		14.1	2434.536	***********	13.1
2410.536	4.7	19.7	2428.736	*****	11.4	2432.236		14.2	2434.586	*****	13.1
2411.536	3.0	18.0	2428.836		11.2	2432.286		13.6	2434.636	*************	13.1
2412.536	1.9	16.9	2428.936	-3.8	11.2	2432.336		13.7	2434.686		13.1
2413.536	1.5	16.5	2429.036	-3.4	11.6	2432.386		13.3	2434,736	Mark 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	13.4
2414.536	0.0	15.0	2429 136	000000000000000000000000000000000000000	11.9	2432.436		13.3	2434.786		13.4
2415.536	-0.4	14.6	2429,236		11.9	2432.486		12.6	2434.836		13.9
2416.536	-0.8	14.2	2429,336		11.9	2432.536		12.8	2434.886		13.6
2417.536	-2.4	12.6	2429.436		11.9	2432.586	i .	12.7	2434.936		13.8
2418.536	-2.7 -2.7	12.3	2429.536	-3.1	11.9	2432.636		12.8	2434.986		13.8
2419.536	-1.4	13.6	2429.636		12.4	2432.686	l	12.6	2435.036		14.1
2419.536	-1. 1	13.9	2429.736		12.4	2432.736		12.6	2435.086		13.7
2420.536	-2.6	12.4	2429.836		12.9	2432.786		12.6	2435.136		13.7
2421.536	-2.0 -4.1	10.9	2429.936	-2.1 -2.1	12.9	2432.760		13.1	2435.186		13.5
2422.536	-3.1	11.9	2429.936		13.6	2432.886	i	13.1	2435,236		13.2
2423.536	-3.1 -2.8	12.2	2430.036		13.6	2432.936		13.1	2435,286		13.2
2424.536	-2.0 -3.7	11.3	2430.136	-1.4 -1.4	13.6	2432.986		12.9	2435,336		13.2
2425.636	-3.7 -3.3	11.7	2430.236	-1. 1	13.2	2432.960		13.0	2435.386		13.2
2425.736	-3.3 -3.1	11.9	2430.336	-1.0 -2.2	12.8	2433.086		13.0	2435,436		12.9
2425.736	-3.1 -2.7	12.3	2430.436	-2.2 -2.5	12.5	2433.080		13.0	2435.486		12.9
2425.936	-2.1 -2.4	12.5	2430,636		12.3	2433.186		13.0	2435.536	300000000000000000000000000000000000000	12.9
2425.936		13.0	2430,736	-2.7 -2.7	12.3	2433.186		13.0	2435.586		13.3
	-2.0	13.0	2430.736	-2.7 -2.8	12.3	2433.286	-2.0	13.0	2435.636		13.3
2426.136 2426.236	-1.8	ł .	2430.936		12.2	2433.266	-2.0 -2.3	12.7	2435.686		13.3
	-1.7	13.3						i .			
2426.336	-2.2	12.8	2431.036		12.4	2433.386		12.7	2435.736		
2426.436			2431.086		100000000000000000000000000000000000000			1	and the second of the second o		
2426.536		11.9	2431.136			2433.486		12.7			
2426.636		1	2431.186		*******	2433.536		12.7			
2426.736			2431,236			2433.586		12.7			
2426.836		11.6	2431,286	A.C	100000000000000000000000000000000000000	2433.636		13.2	2435.986 2436.036		13.2 13.2
2426.936		12.1	2431.336			2433.686		13.3			
2427.036		12.5	2431.386			2433.736		13.5	2436.086		12.9
2427.136		12.5	2431.436			2433.786		13.8	2436.136		12.9
2427.236		12.5	2431.486			2433.836		13.5	\$200,000 particular and the second		13.0
2427.336		12.3	2431.536	A 100 CONTRACTOR 1		2433.886		14.2	2436.236		13.0
2427.436		12.4	2431.586		200000000000000000000000000000000000000	2433.936		13.9			13.0
2427.536			2431.636	4444	*******	2433.986		14.4	 A. Marian, Physics and Physics and Physics 	40.000.000.000.000.000	13,0
2427.636	-2.4	12.6	2431.686	-2.0	13.0	2434.036	-0.6	14.4	2436,386	-2.0	13

PROPRIETARY											
Jamming	J/S	Gp	Jamming	J/S	Gp	Jamming	J/S	Gp	Jamming	J/S	Gp
frequency	(dB)	(dB)	frequency	(dB)	(dB)	frequency	(dB)	(dB)	frequency	(dB)	(dB)
(MHz)	(db)	(מם	(MHz)	(00)	(0.5)	(MHz)			(MHz)		
2436.436	-2.0	13.0	2438.786	-2.5	12.5	2441.136	-2.7	12.3	2445.836		12.9
2436,486	-2.0	13.0	2438,836	-2.5	12.5	2441.236		12.0	2445.936	200000000000000000000000000000000000000	13.3
2436.536	-2.0	13.0	2438.886	-2.5	12.5	2441.336		12.2	2446,036		13.0
2436.586	-2.0	13.0	2438.936		13.1	2441.436		12.3	2446,136		13.0
2436.636	-1.9	13.1	2438,986	(0.000)	12.9	2441.536		12.4	2446.236		12.6
2436.686	-1.9	13.1	2439.036		12.9	2441.636		12.5	2446.336		12.4
2436.736	-1.6	13.4	2439.086		12.9	2441.736		12.8	2446.436		11.9
2436.786	-1.9	13.1	2439,136		12.9	2441.836		13.2	2446.536		11.8
2436.836	-1.4	13.6	2439,186	-2.1	12.9	2441.936	Ï	13.6	2447.536		12.2
2436.886	-1.7	13.3	2439.236	-2.1	12.9	2442.036	-1.4	13.6	2448.536		12.6
2436.936	-1.3	13.7	2439.286	-2.1	12.9	2442.136	-1.4	13.6	2449.536		11.2
2436.986	-1.3	13.7	2439,336	-2.2	12.8	2442.236	-2.1	12.9	2450,536		12.6
2437.036	-1.3	13.7	2439,386	-2.2	12.8	2442.336	-2.3	12.7	2451,536	-1.4	13.6
2437.086	-1.1	13.9	2439.436	-2.4	12.6	2442.436	-2.9	12.1	2452.536	-1.1	13.9
2437.136	-1.1	13.9	2439,486	-2.2	12.8	2442.536	-2.9	12.1	2453.536	-2.7	12.3
2437.186	-1.1	13.9	2439,536	-2,2	12.8	2442.636	-3.3	11.7	2454.536	-2.4	12.6
2437.236	-1.5	13.5	2439.586	-2,2	12.8	2442.736	-3.2	11.8	2455,536	-1.1	13.9
2437.286	-1.4	13.6	2439.636	-2.5	12.5	2442.836	-3.2	11.8	2456.536	0.2	15.2
2437.336	-1.6	13.4	2439.686	-1.7	13.3	2442.936	-3.2	11.8	2457,536	-0.4	14.6
2437.386	-1.6	13.4	2439.736	-1.7	13.3	2443.036	-3.2	11.8	2458.536	1.4	16.4
2437.436	-2.1	12.9	2439.786	-1.2	13.8	2443.136	-3.6	11.4	2459,536	2,9	17.9
2437.486	-1.9	13.1	2439.836	-1.4	13.6	2443.236	-4.0	11.0	2460.536	5.0	20.0
2437.536	-2.1	12.9	2439.886	-0.9	14.1	2443.336	-3.8	11.2	2461.536	6.0	21.0
2437.586	-2.1	12.9	2439,936	-0.9	14.1	2443.436	-3.8	11.2	2462.536	7.3	22.3
2437.636	-2.1	12.9	2439.986	-0.5	14.5	2443.536	-3.3	11.7	2463,536	9.2	24.2
2437.686	-1.8	13.2	2440.036	-0.5	14.5	2443.636	-3.1	11.9	2464,536	11,0	26.0
2437.736	-1.8	13.2	2440,086	-0,6	14.4	2443.736	-2.5	12.5	2465.536	11.5	26.5
2437.786	-1.3	13.7	2440.136	-0.6	14.4	2443.836	-1.5	13.5	2466,536	13.8	28.8
2437.836	-1.6	13.4	2440.186	-0.9	14.1	2443.936	-1.0	14.0	2467.536	15.5	30.5
2437.886	-0.9	14.1	2440.236	-1.1	13.9	2444.036	-0.7	14.3	2468,536	16.4	31.4
2437.936	-1.2	13.8	2440.286	-1,4	13.6	2444.136	-0.7	14.3	2469.536	17.7	32.7
2437.986	-0.6	14.4	2440.336	-1.4	13.6	2444.236	-1.5	13.5	2470.536	17.7	32.7
2438.036		14.4	2440.386	-1.5	13.5	2444.336	-1.5	13.5	2471.536	18.9	33.9
2438.086	-0.6	14.4	2440.436	000000000000000000000000000000000000000	13.0	2444.436	-1.3	13.7	2472.536	18.9	33.9
2438.136	1	14.4	2440,486	-2.0	13.0	2444.536	-2.1	12.9	2473.536	18.5	33.5
2438.186		13.8	2440.536		12.9	2444.636		12.6	2474.536		33,2
2438.236		13.9	2440,586	000000000000000000000000000000000000000	12.7	2444.736	į į	12.1	2475.536	100000000000000000000000000000000000000	33.4
2438.286		13.5	2440.636	-2.4	12.6	2444.836		12.7	2476.536	19.3	34.3
2438.336		13.9	2440.686		12.4	2444.936		12.7	2477.536		32.1
2438.386	-1.5	13.5	2440.736		12.4	2445.036		12.3	2478.536		31.9
2438.436	-1.8	13.2	2440.786		12.4	2445.136		12.3	2479.536		31.9
2438.486		13.2	2440.836		12.4	2445.236		12.0	2480.536	30000000000000000000000000000000000000	32.1
2438.536		12.8	2440,886	**********		2445.336		11.7	2481.536		32.0
2438.586		12.8	2440,936	***********	12.4	2445.436		11.9	2482.536		32.0
2438.636	-2.2	12.8	2440.986		200000000000000000000000000000000000000	2445.536		11.9	2483.536		***********
2438.686		12.5	2441.036		12.4	2445.636		11.9			
2438.736		12.8	2441.086			2445.736		12.7			

MICRILOR/CLARION PROPRIETARY