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## SMITH ELECTRONICS, INC. **ELECTROMAGNETIC COMPATIBILITY LABORATORIES**

## RADIO-FREQUENCY EMISSIONS TEST REPORT

FOR

HEXAGRAM, INC.

UTILITY METER TRANSMITTING UNIT (MTU) Model: 6327W FCC ID: LLB 6327W

October 20, 2003

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#### **TEST REPORT**

### **INTRODUCTION**

The Hexagram Model 6327W transmitter is a battery-powered transmitter designed to be a) mounted directly on a typical gas meter; b) connected with a utility meter by an external 12 ft wire. The transmitter provides a very short, intermittent radio frequency transmission to provide a remote reading of the meter. A microprocessor provides timing, control and data processing functions. The built in antenna is inaccessible to the user and no provision is made for an external antenna. This report describes the tests performed on the transmitter in support of both applications for certification.

### **MEASUREMENTS PERFORMED**

Power Output and Spurious Emissions	Page 3
Occupied Bandwidth	Page 13
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The microprocessor portion of the transmitter was also examined for radiated emissions per Part 15, and has been verified to comply with the appropriate sections of that part. The data used for verification of the microprocessor portion is presented in a separate report.

#### **POWER OUTPUT AND SPURIOUS EMISSIONS**

A series of measurements of three tuned frequencies and their harmonic emissions was made on the Smith Electronics, open field test site located at 8200 Snowville Road, Brecksville, OH. Data pertinent to this site is on file with the FCC. A scan of the transmitter emissions made in the shielded room showed no significant emissions other than the fundamental and its harmonics. The measurements were made using the substitution method described in TIA/EIA-603-A.

Measurements below 1000 MHz were made at a three-meter test distance with frequencies above 1000 MHz being measured at one meter. A receiver and a tuned dipole were used for receiving below 1000 MHz and a spectrum analyzer and a wave guide antenna were used above 1000 MHz.

The transmitter was placed on a remotely rotatable, non-conducting test stand. This general set up is shown in Pictorial 1. Because of the intermittent nature of the normally operating transmitter a larger, external battery pack was connected directly to the transmitter and the transmitter was forced to continually transmit for the measurements.

With the test receiver tuned to the unmodulated signal, the transmitter under test was rotated to the position of maximum signal. The receiving antenna was then varied between 1 and 4 meters in height to again maximize the signal. Measurements were made with the antennas positioned both vertically and horizontally and the maximum signal recorded.

No differences were observed with different signal detectors, so a quasi-peak detector was used for the signals below 1000 MHz and average detection above 1000 MHz.

After the maximum received meter readings were obtained for each frequency and polarity, the meter under test was removed from the area and replaced by a signal generator and transmitting antenna. With the transmit antenna placed as close as possible to the position of the test unit, the signal generator was activated at a test frequency. With the signal detected, the transmit antenna was rotated slightly to maximize the reading. The receive antenna was also positioned for maximum reception. The signal generator output was then adjusted until the received signal was equal to the received signal from the unit under test. These measurements were repeated for each frequency and antenna orientation and the maximum values obtained are noted in Tables 1a – 1c. Transmitting antenna gain and coax loss figures are also included in the tables.

In order to convert the signal generator output value to equivalent radiated power from a dipole, the following equation is used:

$$P_d = P_g - cable loss(dB) + antenna gain(dB_d)$$

where:

 $P_d$  is the dipole equivalent power,  $P_g$  is the generator output into the substitution antenna and "antenna gain" is the gain of the substitution antenna with respect to a dipole.

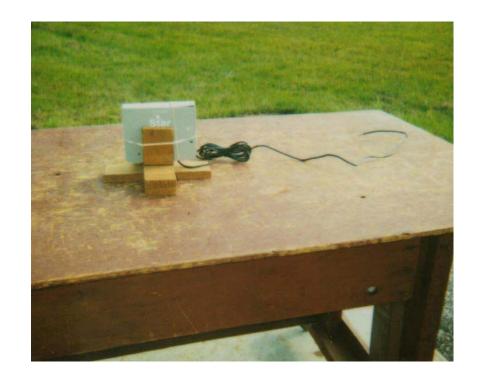
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According to 90.210(d)(3) all emissions greater than 12.5 kHz from the center of the authorized band shall be attenuated below the unmodulated carrier by  $50 + 10\log(P)$ . The determined power outputs, the required harmonic attenuation as well as the attenuation for each harmonic are found in Tables 1a - 1c, and, 2a - 2c.



PICTORIAL 1
HEXAGRAM GAS METER TRANSMITTING UNIT
MODEL 6327W, no external wiring
OUTPUT POWER AND SPURIOUS EMISSIONS
TEST SETUP

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PICTORIAL 2
HEXAGRAM GAS METER TRANSMITTING UNIT
MODEL 6327W with external wiring
OUTPUT POWER AND SPURIOUS EMISSIONS
TEST SETUP

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# TABLE 1a HEXAGRAM MODEL 6327W TRANSMITTER WITHOUT EXTERNAL WIRING SUBSTITUTION METHOD

3 meter measurement using tuned dipole antenna

			110 0151115 CO1110 CO	I	
Frequency	Gen. Output	Coax Loss	Ant. Gain	Dipole Eq.	Difference
(MHz)	(dB)	(dB)	(dBd)	Power	(dB)
				(dBm)	
450	14.8	0.3	0	14.5	-
900	-32.0	0.5	0	-32.5	-47.0

1 meter measurement using horn antenna

		l	Inchi ushig in		
Frequency	Gen. Output	Coax Loss	Ant. Gain	Dipole Eq.	Difference
(MHz)	(dBm)	(dB)	(dBd)	Power	(dB)
	, , ,		, , ,	(dBm)	, ,
1350	-52.3	0.7	3.1	-49.9	-64.4
1800	-51.0	0.8	4.9	-46.9	-61.4
2250	-45.7	0.9	5.6	-41.0	-55.5
2700	-50.0	1.1	6.2	-44.9	-59.4
3150	-46.0	1.2	6.7	-40.5	-55.0
3600	-42.2	1.3	6.6	-36.9	-51.4
4050	-47.0	1.4	6.5	-41.9	-56.4
4500	-54.8	1.5	7.2	-49.1	-63.6
		,-	· ,—		

14.5 dBm = 28.2 mW or 0.0282 WRequired attenuation for harmonics is  $50 + \log (.0282) = 34.5 \text{ dBm}$ 

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# TABLE 1b HEXAGRAM MODEL 6327W TRANSMITTER WITHOUT EXTERNAL WIRING SUBSTITUTION METHOD

3 meter measurement using tuned dipole antenna

	1	1		, 1	
Frequency	Gen. Output	Coax Loss	Ant. Gain	Dipole Eq.	Difference
(MHz)	(dB)	(dB)	(dBd)	Power	(dB)
	` '	, ,	, ,	(dBm)	, ,
460	19.0	0.3	0	18.7	-
920	-28.0	0.5	0	-27.5	-46.2

1 meter measurement using horn antenna

_		1	inent using n		D:00
Frequency	Gen. Output	Coax Loss	Ant. Gain	Dipole Eq.	Difference
(MHz)	(dBm)	(dB)	(dBd)	Power	(dB)
	,	, ,	,	(dBm)	,
1380	-54.0	0.7	3.1	-51.6	-70.3
1360	-34.0	0.7	3.1	-31.0	-70.3
1840	-50.8	0.8	4.9	-46.7	-65.4
2300	-49.0	0.9	5.6	-44.3	-63.0
2500	-47.0	0.7	3.0	-44.5	-05.0
2760	-50.7	1.1	6.2	-45.6	-64.3
3220	-44.7	1.2	6.7	-39.2	-57.9
5220	,	1	0.7	<i>53.</i> 2	67.5
2600	44.1	1.2	( (	20.0	57.5
3680	-44.1	1.3	6.6	-38.8	-57.5
4140	-52.0	1.4	6.5	-46.9	-65.6
4600	-39.7	1.5	7.2	-34.0	-52.7
4000	-37.1	1.3	1.4	-34.0	-34.1

18.7 dBm = 74.1 mW or 0.0741 W Required attenuation for harmonics is  $50 + \log (.0741) = 38.7$  dBm

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# TABLE 1c HEXAGRAM MODEL 6327W TRANSMITTER WITHOUT EXTERNAL WIRING SUBSTITUTION METHOD

3 meter measurement using tuned dipole antenna

Frequency	Gen. Output	Coax Loss	Ant. Gain	Dipole Eq.	Difference
(MHz)	(dB)	(dB)	(dBd)	Power (dBm)	(dB)
469.15	20.9	0.3	0	20.6	-
938.3	-22.0	0.5	0	-22.5	-43.1

1 meter measurement using horn antenna

Frequency	Gen. Output	Coax Loss	Ant. Gain	Dipole Eq.	Difference
(MHz)	(dBm)	(dB)	(dBd)	Power	(dB)
			,	(dBm)	
1407.45	-55.8	0.7	3.1	-53.4	-72.5
1876.6	-54.8	0.8	4.9	-50.4	-69.5
	10.0				5.1.5
2345.75	-49.8	0.9	5.6	-45.1	-64.2
20140	52.0			47.0	66.0
2814.9	-52.9	1.1	6.2	-47.8	-66.9
2204.05	47.0	1.2	(7	41.5	(0.6
3284.05	-47.0	1.2	6.7	-41.5	-60.6
3753.2	-42.0	1.3	6.6	-36.7	-55.8
3/33.2	-42.0	1.3	0.0	-30.7	-33.8
4222.35	-51.5	1.4	6.5	-46.4	-65.5
7222.33	-31.3	1.4	0.5	-40.4	-03.3
4691.5	-46.3	1.5	7.2	-40.6	-59.7
1071.5	10.5	1.5	, .2	10.0	37.1
<u> </u>	l .	l .		l .	l

20.6 dBm = 114.8 mW or 0.1148 W Required attenuation for harmonics is  $50 + \log (.1148) = 40.6$  dBm

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## TABLE 2a HEXAGRAM MODEL 6327W TRANSMITTER WITH EXTERNAL WIRING SUBSTITUTION METHOD

3 meter measurement using tuned dipole antenna

Frequency	Gen. Output	Coax Loss	Ant. Gain	Dipole Eq.	Difference
(MHz)	(dB)	(dB)	(dBd)	Power	(dB)
				(dBm)	
450	21.2	0.3	0	20.9	
900	-37.0	0.5	0	-37.5	-58.4

1 meter measurement using horn antenna

Б			thient using no	1	D:00
Frequency	Gen. Output	Coax Loss	Ant. Gain	Dipole Eq.	Difference
(MHz)	(dBm)	(dB)	(dBd)	Power	(dB)
	` ,		, ,	(Dbm)	` ,
1350	-50.0	0.7	3.1	-47.6	-68.5
1550	-30.0	0.7	5.1	-47.0	-00.5
1800	-58.1	0.8	4.9	-54.0	-74.9
2250	-37.0	0.9	5.6	-32.3	-53.2
2200	37.0	0.5	5.0	32.3	03.2
2700	46.0	1.1	( 2	40.0	(1.0
2700	-46.0	1.1	6.2	-40.9	-61.8
3150	-46.4	1.2	6.7	-40.9	-61.8
3600	-42.4	1.3	6.6	-37.1	-58.0
3000	<b>-</b> 4∠.4	1.3	0.0	-37.1	-38.0
4050	-54.8	1.4	6.5	-49.7	-70.6
4500	-45.2	1.5	7.2	-39.5	-60.4
7500	-73.2	1.5	1.4	-57.5	-00.7

20.9 dBm = 123.0 mW or 0.123 W Required attenuation for harmonics is  $50 + \log (.123) = 40.9$ dB

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# TABLE 2b HEXAGRAM MODEL 6327W TRANSMITTER WITH EXTERNAL WIRING SUBSTITUTION METHOD

3 meter measurement using tuned dipole antenna

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Frequency	Gen. Output	Coax Loss	Ant. Gain	Dipole Eq.	Difference
(MHz)	(dB)	(dB)	(dBd)	Power	(dB)
				(dBm)	
460	20.8	0.3	0	20.5	-
920	-31.2	0.5	0	-31.7	-52.2

1 meter measurement using horn antenna

	I meter measurement using norn antenna					
Frequency	Gen. Output	Coax Loss	Ant. Gain	Dipole Eq.	Difference	
(MHz)	(dBm)	(dB)	(dBd)	Power	(dB)	
				(Dbm)		
1380	-48.4	0.7	3.1	-46.0	-66.5	
1840	-50.2	0.8	4.9	-46.1	-66.6	
2300	-41.0	0.9	5.6	-36.3	-56.8	
2760	-48.1	1.1	6.2	-43.0	-63.5	
3220	-44.5	1.2	6.7	-39.0	-59.5	
3680	-39.5	1.3	6.6	-34.2	-54.7	
4140	-52.2	1.4	6.5	-47.1	-67.6	
4600	-52.8	1.5	7.2	-47.1	-67.6	

20.5dBm = 112.2 mW or 0.112 W Required attenuation for harmonics is  $50 + \log (.112) = 40.5$ dB

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## TABLE 2c HEXAGRAM MODEL 6327W TRANSMITTER WITH EXTERNAL WIRING SUBSTITUTION METHOD

3 meter measurement using tuned dipole antenna

Frequency	Gen. Output	Coax Loss	Ant. Gain	Dipole Eq.	Difference
(MHz)	(dB)	(dB)	(dBd)	Power	(dB)
				(dBm)	
470	20.0	0.3	0	19.7	-
940	-26.0	0.5	0	-26.5	-46.2

1 meter measurement using horn antenna

C 0 4 4	$\alpha$ $\tau$	A 4 C .	D' 1 E	D.CC
			1 1	Difference
(dBm)	(dB)	(dBd)	Power	(dB)
	, , ,		(Dbm)	
-52.0	0.7	3.1	-49.6	-69.3
-51.9	0.8	4.9	-47.8	-67.5
-48.0	0.9	5.6	-43.3	-63.0
-49.4	1.1	6.2	-44.3	-64.0
-43.8	1.2	6.7	-38.3	-58.0
-42.0	1.3	6.6	-36.7	-56.4
-51.8	1.4	6.5	-46.7	-66.4
-52.8	1.5	7.2	-47.1	-66.8
	-51.9 -48.0 -49.4 -43.8 -42.0	(dBm) (dB)  -52.0 0.7  -51.9 0.8  -48.0 0.9  -49.4 1.1  -43.8 1.2  -42.0 1.3  -51.8 1.4	(dBm)     (dB)     (dBd)       -52.0     0.7     3.1       -51.9     0.8     4.9       -48.0     0.9     5.6       -49.4     1.1     6.2       -43.8     1.2     6.7       -42.0     1.3     6.6       -51.8     1.4     6.5	(dBm)         (dB)         (dBd)         Power (Dbm)           -52.0         0.7         3.1         -49.6           -51.9         0.8         4.9         -47.8           -48.0         0.9         5.6         -43.3           -49.4         1.1         6.2         -44.3           -43.8         1.2         6.7         -38.3           -42.0         1.3         6.6         -36.7           -51.8         1.4         6.5         -46.7

19.7 dBm = 93.3 mW or 0.0933 W.Required attenuation for harmonics is  $50 + \log (.0933) = 39.7 \text{ dB}$ 

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#### TEST EQUIPMENT USED

Meters & Analyzers Singer-Stoddart EMI Field Intensity Meter

Model NM 37/57 S/N 0366-06168

Calibrated 6/03

Hewlett-Packard Spectrum Analyzer Model 8593EM S/N 3536A00147

Calibrated 6/00

Antennas (2x) Stoddart 91598-2 Tuned Dipole

Frequency Range 400 – 1000 MHz

EMCO 3115 Double Ridged Guide Horn Frequency Range 1 – 18 GHz (Rcv)

Eaton Model 96001 Double Ridged Guide Horn

Frequency Range 1 - 18 GHz (Xmt)

Signal Generator Hewlett-Packard Model 8340B, S/N 3010A01889

Calibrated 1/03

Miscellaneous 12.2 m RG-214/U coaxial cable

6.1 m RG-214/U coaxial cable

(2x) 1.8 m RG-214/U coaxial cable

#### **OCCUPIED BANDWIDTH**

The emissions close to the center of the specified channel are limited by the emissions masks described in 90.210. For the frequency range of the MTU transmitter, Mask D is specified. From the center frequency of the band  $\pm 5.625$  kHz, 0 dB of attenuation is required. From 5.625 kHz to 12.5 kHz from the center frequency, attenuation must be at least  $7.27(f_d-2.88 \text{ kHz})$  dB, where  $f_d$  is the displacement frequency from the center of the band in kHz.

At more than 12.5 kHz from the band center, the attenuation must be 70 dB or  $50 + 10 \log(P)$ , whichever is less. Since maximum P was determined to be 0.1148 W (application without external wires), and 0.123 W (with external wires),  $50 + 10 \log(0.1148)$  equals 40.6 dB (without external wires) and 40.9 dB (at application with external wires).

The short transmission was caught by the Real-Time-Spectrum-Analyzer and stored to disk for evaluation.

The plots of Fig. 3a and 4a shows the unmodulated carrier, while Fig. 3b and 4b shows the modulated signal.

Both Figs. have Mask D superimposed on the plot. The plots indicate that the modulated emission does appear to comply with the requirement for occupied bandwidth as found in 90.210. For clearer view of plots see Appendix 1.

For purposes of this test, the transmitter was FSK modulated with a continuous sequence of Manchester encoded 1's at the specified 1200 bits per second data rate. The Manchester encoding scheme forces a mid-bit transition for an encoded "1". Therefore, the sequence of continuous 1's sends the highest frequency waveform to the modulator circuit.

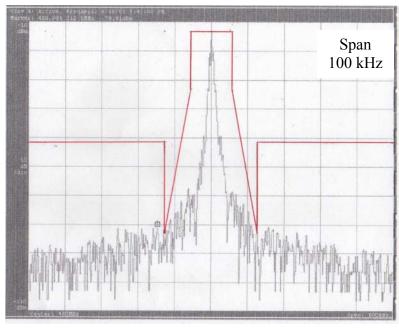


Fig. 3a Hexagram Model LLB 6327W (w/o external wire) Unmodulated Emissions Mask

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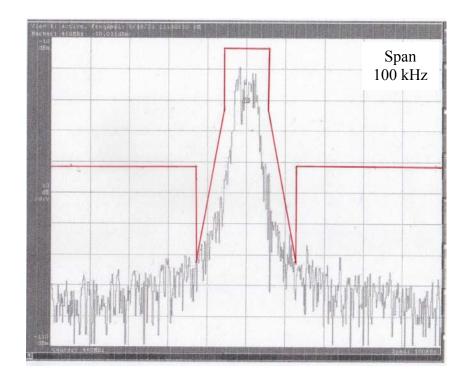


Fig. 3b Hexagram LLB 6327W w/o external wire Modulated Emissions Mask

LLB 6327W w/o Wire August 18, 2003

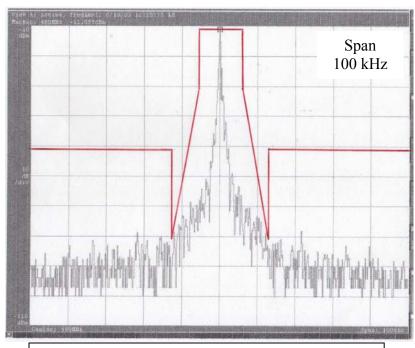


Fig. 4a Hexagram LLB 6327W MTU with external Wire Unmodulated Emissions Mask

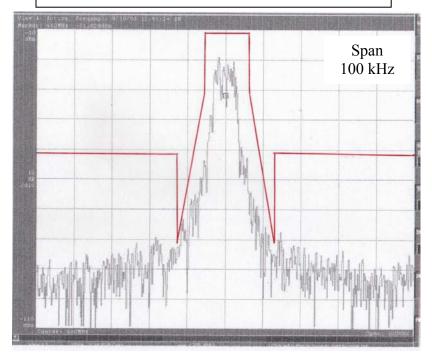


Fig. 4b Hexagram LLB 6327W MTU with external Wire Modulated Emissions Mask

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## **TEST EQUIPMENT USED**

Real-Time Spectrum Analyzer Tektronix/Sony Model 3086

Tektronix/Sony Model 3086 S/N J300195 Calibration 12/02

Antenna EMCO Model 3146 Log Periodic

Frequency Range 200 MHz – 1000 MHz

For clearer view of above shown plots see Appendix 1.

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#### FREQUENCY STABILITY VS. TEMPERATURE

The temperature stability of the frequency generating components of the transmitter was observed. The transmitter was placed in a temperature chamber. The battery powered meter was set to transmit at intervals of about 40 seconds. A receiving antenna outside the chamber picked up the transmitted signal which was fed to the real-time spectrum analyzer.

With the transmitter programmed to transmit at 460.025000 MHz, the chamber temperature was set to 70° C. After reaching the set temperature, the transmitter was allowed to stabilize for about 10 minutes or more. The transmission signal was captured by the real-time spectrum analyzer and the frequency was determined and compared to the expected 460.025000 MHz. The temperature in the chamber was then decreased in 10° C increments. At each new temperature, time was allowed for stabilization of the transmitter, a transmission was made and the frequency determined. The temperature was decreased by the 10° C increments, stabilizing and checking the frequency at each point, until a temperature of -30° C was reached. The frequency at each temperature was recorded and is found in Table 3 (this is the worst case for both: MTUs with and without external wires). It can be seen from the table that all readings are exactly on frequency with no deviation.

TABLE 3

## FREQUENCY STABILITY

## VS. TEMPERATURE

Temperature ° C	Measured Frequency MHz	Dev. Hz	Dev. ppm
	Expected = 460.025000		
+70	460.025000	0	0
+60	460.025000	0	0
+50	460.025000	0	0
+40	460.025000	0	0
+30	460.025000	0	0
+20	460.025000	0	0
+10	460.025000	0	0
0	460.025000	0	0
-10	460.025000	0	0
-20	460.025000	0	0
-30	460.025000	0	0

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### FREQUENCY STABILITY VS. SUPPLY VOLTAGE

The frequency stability was also determined as a function of the DC battery voltage. A variable DC power supply was used to set the voltage between about 85% and 115% of the nominal 3.60 VDC input. Measurements were made at 3.60 V, 3.06 V and 4.14 V. With the voltage set to a measurement point, the transmitted signal was captured by the real-time spectrum analyzer and the frequency value determined. The data for these measurements are found in Table 3 (this is the worst case for both: MTUs with and without external wires). Again, it can be seen that all values obtained are exactly on frequency.

### TABLE 4

## FREQUENCY STABILITY

## VS. SUPPLY VOLTAGE

INPUT DC Volts	Measured Frequency MHz	Dev. Hz	Dev. ppm
	Expected = 460.028125		
3.06	460.028125	0	0
3.60	460.028125	0	0
4.14	460.028125	0	0

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**TEST EQUIPMENT USED** 

Real-Time Spectrum Analyzer Tektronix/Sony Model 3086

S/N J300195 Calibration 12/02

Antenna EMCO Model 3146 Log Periodic

Frequency Range 200 MHz – 1000 MHz

**DC Power Supply** Harrison Laboratories, Inc. Model 8028

Twin Low Voltage Power Supply

<u>Thermometer</u> Radio Shack 63-1011 Digital Thermometer

<u>Digital Volt Meter</u> Fluke Model 23

<u>Temperature Chamber</u> Standard Environmental Systems, Inc.

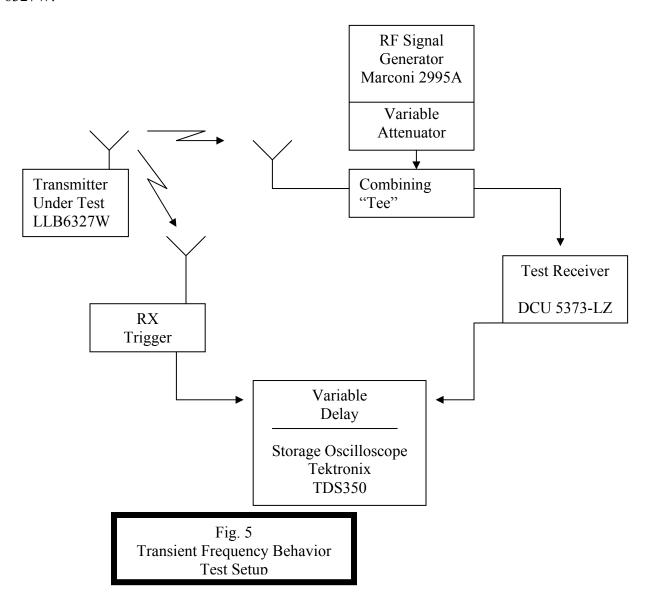
Model TK/5

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#### **TRANSIENT STABILITY**

The transient stability measurements indicate the variation in tuned frequency during the brief interval of time during the start of the transmission and the end of the transmission.

The LLB 6327W transmitter was tested for transient frequency behavior using the test method TIA/EIA-603. A block diagram of the test setup is seen in Fig. 5. A model DCU-1 receiver with an audio bandwidth of 16 kHz (low Pass) was used. The storage oscilloscope was triggered by the radiated signal from the transmitter. Appropriate delay was provided by the digital delay circuitry of the oscilloscope. The 1 kHz test signal was provided by the Marconi signal generator. The generator's output control was used to insure that the signal was at least 50 dB below the received signal level from the LLB 6327W.



### **Test Requirements**

The test requirements per 90.214 are:

- 1. Frequency deviation during  $t_1$  (10 ms duration after  $t_{on}$ ) may be greater than  $\pm 12,5$  kHz because the output power is less than 6 Watts.
- 2. Frequency deviation during t<sub>2</sub> (25 ms duration after t<sub>1</sub>) must be less than ±6.25 kHz.
- 3. Frequency deviation after  $t_2$  must be less the  $\pm 2.5$  ppm. or  $\pm 1150$  Hz.
- 4. Frequency deviation during  $t_3$  (10 ms duration after transmitter is turned off) may exceed  $\pm 12.5$  kHz because output power is less than 6 Watts.

Both transmitters (with and without external wires) are tested, and, the worst case is represented in the following oscilloscope snaps.

#### **Test Data**

Figures 6 through 10 show the LLB 6327W's transient frequency characteristics. The limit masks are overlaid or indicated on each of the figures.

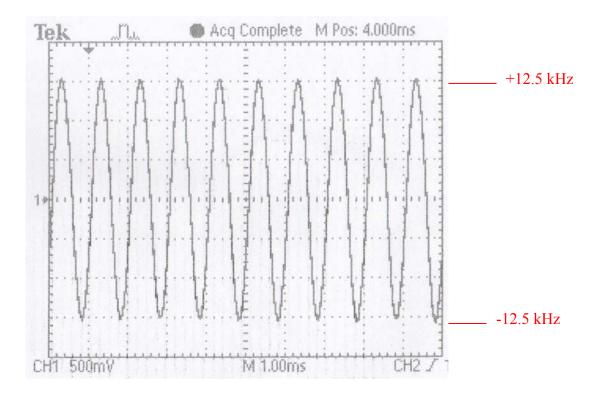
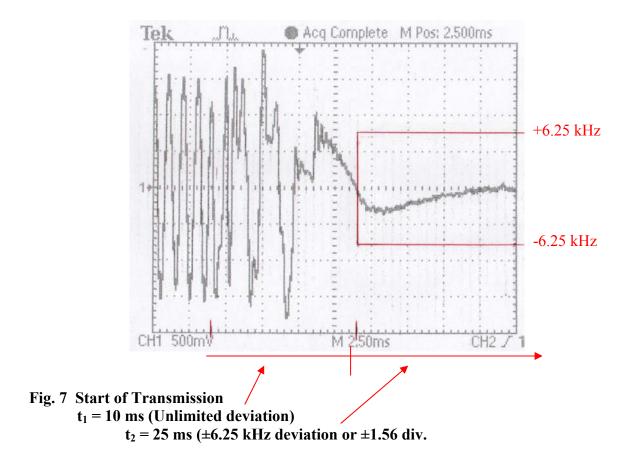
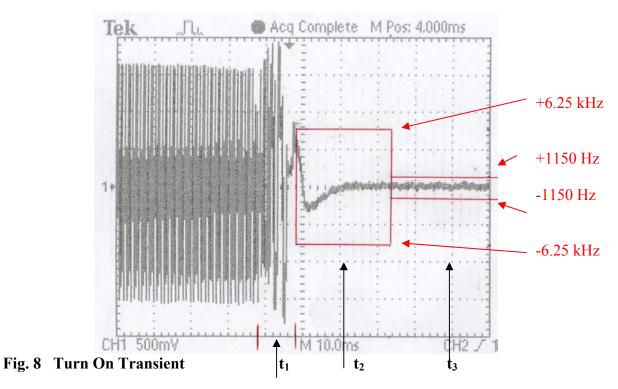


Fig. 6  $\pm 12.5$  kHz modulated test signal 25 kHz/6.2 div. = 4 kHz/div.





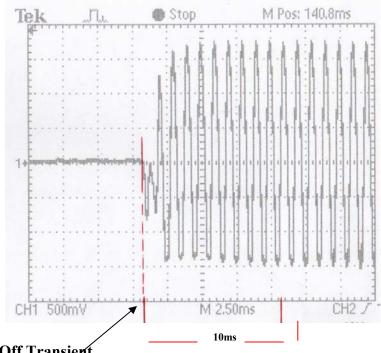
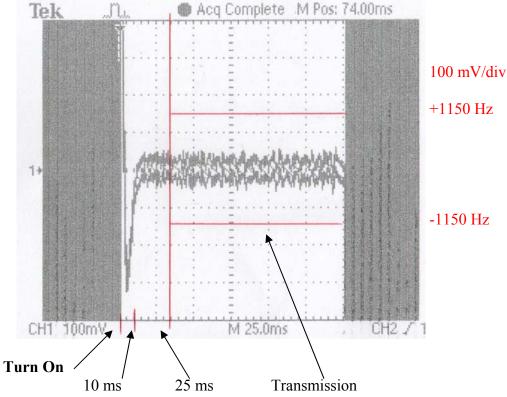


Fig. 9 Turn Off Transient
Turn Off

Modulated signal appears well within the allowed 10 ms and does not exceed  $\pm 12.5$  kHz.



**Fig. 10 Complete Transmission** MTU 6327W w/o Wire, August 20, 2003

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## **TEST EQUIPMENT USED**

Marconi Model 2955A
Signal Generator

Marconi Model 2955A
Calibration 10/02

Hexagram DCU-1 (Modified)

Test Receiver

Tektronix Model TDS 1002

Oscilloscope S/N CO15640 Calibration 10/02

Hewlett-Packard Thinkjet

Printer

RF Trigger

Hexagram Detector Circuit

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#### **TEST INFORMATION**

### **SUMMARY**

The Hexagram Meter Transmitting Unit transmitter, LLB 6327W, has been shown to be capable of complying with those requirements of the Federal Communications Commission for a Part 90 transmitter that are covered by this report.

**EQUIPMENT UNDER TEST** MTU Transmitter, LLB 6327W

MANUFACTURER Hexagram, Inc.

23905 Mercantile Cleveland, OH 44122

**TEST DATES** August 4 – September 24, 2003

**TEST LABORATORY** Smith Electronics, Inc.

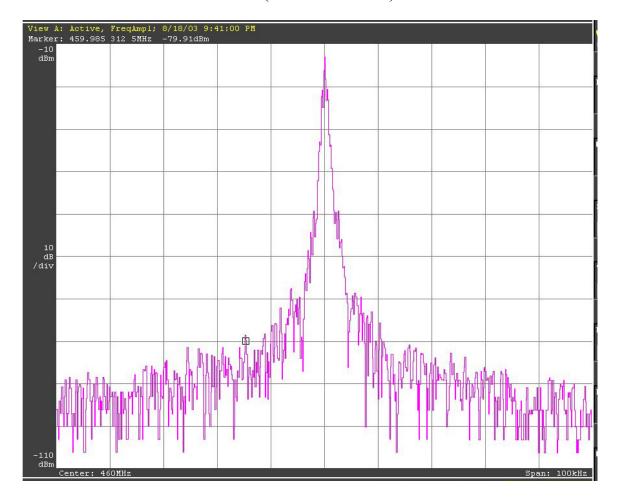
8200 Snowville Road Cleveland, OH 44141

(440)526-4386

## **APPENDIX**

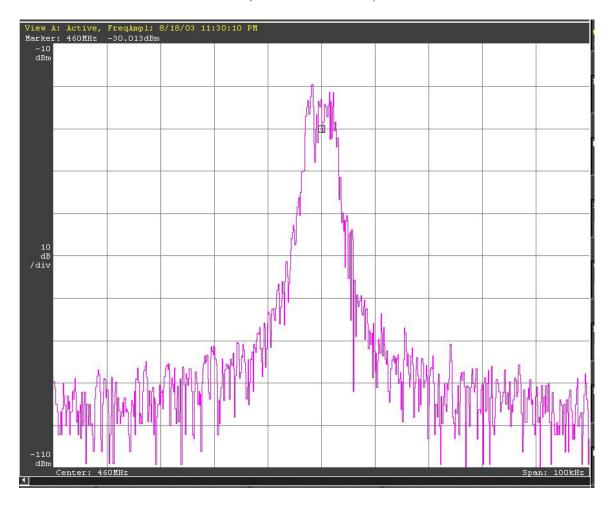
## **APPENDIX**

Unmodulated transmission w/o mask (Unit without wires)

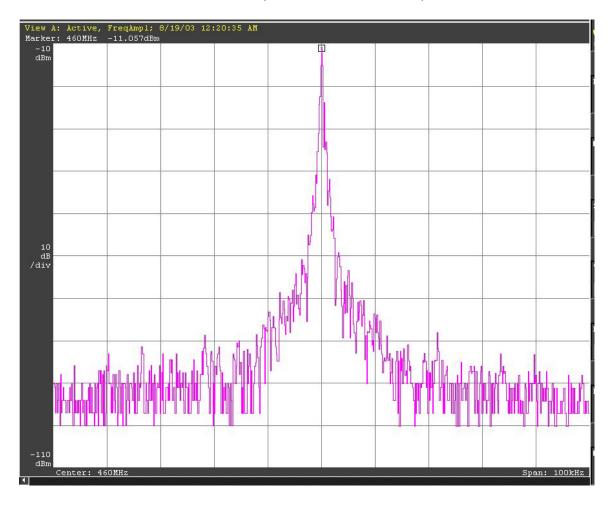


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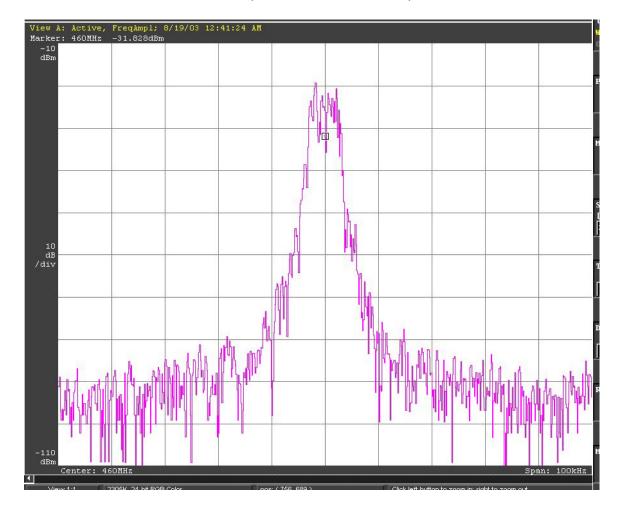
## Modulated transmission w/o mask. (Unit without wires)



Unmodulated transmission w/o mask (Unit with external wires).



Modulated transmission w/o mask (Unit with external wires).



END.