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# **CERTIFICATE OF COMPLIANCE (SAR EVALUATION)**

**Vertex Standard Co., Ltd. Dates of Tests: December 11-12, 2000 4-8-8 Nakameguro, Meguro-Ku, Test Report S/N: SAR.201208627.K66 Tokyo, 153-8644 Test Site: PCTEST Lab, Columbia MD Attn: Tomiro Ohmoto, Export Manager**

# **FCC ID K66VX-900U**

**APPLICANT VERTEX STANDARD CO., LTD.**



**This wireless portable device has been shown to be capable of compliance for localized specific absorption rate (SAR) for Controlled Environment/Occupational exposure limits specified in ANSI/IEEE Std. C95.1- 1992 and had been tested in accordance with the measurement procedures specified in ANSI/IEEE Std. C95.3-1992. (See Test Report).**

**I attest to the accuracy of data. All measurements reported herein were performed by me or were made under my supervision and are correct to the best of my knowledge and belief. I assume full responsibility for the completeness of these measurements and vouch for the qualifications of all persons taking them.**

*NVLAP accreditation does not constitute any product endorsement by NVLAP or any agency of the United States Government.*

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*PCTEST certifies that no party to this application has been denied the FCC benefits pursuant to Section 5301 of the Anti-Drug Abuse Act of 1988, 21 U.S.C. 853(a).*

**Randy Ortanez** President & Chief Engineer



# **Table of Contents**



# **SAR MEASUREMENT REPORT**

### **1.1 Scope**

*Environmental evaluation measurements of specific absorption rate<sup>1</sup> (SAR) distributions in simulated human tissues exposed to radiofrequency (RF) radiation from wireless portable devices for compliance with the rules and regulations of the U.S. Federal Communications Commission (FCC).<sup>2</sup>*



- EUT Type: UHF Mobile Radio
	- Trade Name: *Vertex Standard*
- Model(s): *VX-900U*
- FCC IDENTIFIER: **K66VX-900U**
- S/N: Pre-production

• Tx Frequency: 450.025MHz – 484.975MHz

- Rx Frequency : 450.025MHz 484.975MHz
- Application Type: Certification
- FCC Classification: Licensed Non-Broadcast Transmitter Held to Face (TNF)
	- Modulation(s): FM
	- FCC Rule Part(s): § 2.1093, Docket 96-326
- Max. Conducted Power: 5.0 Watts
- Dates of Tests: December 11-12, 2000
- Place of Tests: PCTEST Engineering Lab.
- Report Serial No.: SAR.201208627.K66



**Fig. 1 SAR Test Setup**



Columbia, MD, U.S.A.

1

*<sup>1</sup> Specific Absorption Rate (SAR) is a measure of the rate of energy absorption due to exposure to an RF transmitting source (wireless portable device).*

*<sup>2</sup> IEEE/ANSI Std. C95.1-1992 limits are used to determine compliance with FCC ET Docket 93-62.*

# **2.1 INTRODUCTION**

The FCC has adopted the guidelines for evaluating the environmental effects of radiofrequency radiation in ET Docket 93-62 on Aug. 6, 1996 to protect the public and workers from the potential hazards of RF emissions due to FCC-regulated portable devices.[1]

The safety limits used for the environmental evaluation measurements are based on the criteria published by the American National Standards Institute (ANSI) for localized specific absorption rate (SAR) in *IEEE/ANSI C95.1-1992 Standard for Safety Levels with Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 3 kHz to 300 GHz*. (c) 1992 by the Institute of Electrical and Electronics Engineers, Inc., New York, New York 10017.[2] The measurement procedure described in *IEEE/ANSI C95.3-1992 Recommended Practice for the Measurement of Potentially Hazardous Electromagnetic Fields - RF and Microwave*[3] is used for guidance in measuring SAR due to the RF radiation exposure from the Equipment Under Test (EUT). These criteria for SAR evaluation are similar to those recommended by the National Council on Radiation Protection and Measurements (NCRP) in *Biological Effects and Exposure Criteria for Radiofrequency Electromagnetic Fields,"* NCRP Report No. 86 (c) NCRP, 1986, Bethesda, MD 20814.[4] SAR is a measure of the rate of energy absorption due to exposure to an RF transmitting source. SAR values have been related to threshold levels for potential biological hazards.

### **2.2 SAR Definition**

Specific Absorption Rate (SAR) is defined as the time derivative (rate) of the incremental energy (*dU*) absorbed by (dissipated in) an incremental mass (*dm*) contained in a volume element (*dV*) of a given density (*r*). It is also defined as the rate of RF energy absorption per unit mass at a point in an absorbing body (see Fig. 2).





*SAR is expressed in units of Watts per Kilogram (W/kg).* 

 $SAR = S E^2 / r$ 

where:

- *s* = conductivity of the tissue-simulant material (S/m)
- $r =$  mass density of the tissue-simulant material (kg/m<sup>3</sup>)
- $\vec{E}$  = Total RMS electric field strength (V/m)

NOTE: The primary factors that control rate of energy absorption were found to be the wavelength of the incident field in relations to the dimensions and geometry of the irradiated organism, the orientation of the organism in relation to the polarity of field vectors, the presence of reflecting surfaces, and whether conductive contact is made by the organism with a ground plane.[4]

# **3.1 SAR MEASUREMENT SET-UP**

These measurements are performed using the DASY3 automated dosimetric assessment system. It is made by Schmid & Partner Engineering AG (SPEAG) in Zurich, Switzerland. It consists of high precision robotics system (Staubli), robot controller, Pentium III computer, near-field probe, probe alignment sensor, and the generic twin phantom containing the brain or muscle equivalent material. The robot is a six-axis industrial robot performing precise movements to position the probe to the location (points) of maximum electromagnetic field (EMF) (see Fig. 2).

A cell controller system contains the power supply, robot controller, teach pendant (Joystick), and remote control, is used to drive the robot motors. The PC consists of the Micron Pentium III 500 MHz computer with Windows NT system and SAR Measurement Software DASY3, A/D interface card, monitor, mouse, and keyboard. The Staubli Robot is connected to the cell controller to allow software manipulation of the robot. A data acquisition electronic (DAE) circuit performs the signal amplification, signal multiplexing, AD-conversion, offset measurements, mechanical surface detection, collision detection, etc. is connected to the Electro-optical coupler (EOC). The EOC performs the conversion from the optical into digital electric signal of the DAE and transfers data to the PC plug-in card. The DAE3 consists of a



**Figure 3. PCTEST SAR Lab II Test Measurement Set-up**

highly sensitive electrometer-grade preamplifier with auto-zeroing, a channel and gainswitching multiplexer, a fast 16 bit AD-converter and a command decoder and control logic unit. Transmission to the PC-card is accomplished through an optical downlink for data and status information and an optical uplink for commands and clock lines. The mechanical probe mounting device includes two different sensor systems for frontal and sidewise probe contacts. They are also used for mechanical surface detection and probe collision detection. The robot uses its own controller with a built in VME-bus computer. The system is described in detail in [5].

# **4.1 DASY3 E-FIELD PROBE SYSTEM**

# **4.2 ET3DV5 Probe Specification**



Fast automatic scanning in arbitrary phantoms



**Figure 4. Photograph of the Probe and the Phantom**



**Fig. 5. ET3DV5 E-field Probe**

The SAR measurements were conducted with the dosimetric probe ET3DV5, designed in the classical triangular configuration [5] and optimized for dosimetric evaluation. The probe is constructed using the thick film technique; with printed resistive lines on ceramic substrates. The probe is equipped with an optical multifiber line ending at the front of the probe tip. It is connected to the EOC box on the robot arm and provides an automatic detection of the phantom surface. Half of the fibers are connected to a pulsed infrared transmitter, the other half to a synchronized receiver. As the probe approaches the surface, the reflection from the surface produces a coupling from the transmitting to the receiving fibers. This reflection increases first during the approach, reaches a maximum and then decreases. If the probe is flatly touching the surface, the coupling is zero. The distance of the coupling maximum to the surface is independent of the surface reflectivity and largely independent of the surface to probe angle. The DASY3 software reads the reflection during a software approach and looks for the maximum using a  $2^{nd}$  order fitting. The approach is stopped at reaching the maximum.

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# **5.1 E-FIELD PROBE CALIBRATION PROCESS**

# **5.2 E-Probe Calibration**

Each probe is calibrated according to a dosimetric assessment procedure described in [6] with an accuracy better than +/- 10%. The spherical isotropy was evaluated with the procedure described in [7] and found to be better than +/-0.25dB. The sensitivity parameters (NormX, NormY, NormZ), the diode compression parameter (DCP) and the conversion factor (ConvF) of the probe is tested.

The free space E-field from amplified probe outputs is determined in a test chamber. This is performed in a TEM cell for frequencies bellow 1 GHz, and in a waveguide above 1 GHz for free space. For the free space calibration, the probe is placed in the volumetric center of the cavity and at the proper orientation with the field. The probe is then rotated 360 degrees.

E-field temperature correlation calibration is performed in a flat phantom filled with the appropriate simulating tissue. The measured free space E-field in the medium correlates to temperature rise in a dielectric medium. For temperature correlation calibration a RF transparent thermistor-based temperature probe is used in conjunction with the E-field probe.

$$
\text{SAR} = C \frac{\Delta T}{\Delta t}
$$

where:

 $\Delta t$  = exposure time (30 seconds),

 $C =$  heat capacity of tissue (brain or muscle),

 $\Delta T$  = temperature increase due to RF exposure.

SAR is proportional to  $\Delta T / \Delta t$ , the initial rate of tissue heating, before thermal diffusion takes place. Now it's possible to quantify the electric field in the simulated tissue by equating the thermally derived SAR to the E- field;





$$
SAR = \frac{|E|^2 \cdot s}{r}
$$

where:

 $\sigma$  = simulated tissue conductivity,

$$
\rho = \text{Tissue density (1.25 g/cm}^3 \text{ for brain tissue)}
$$



**Figure 7. E-Field and temperature measurements at 1.8GHz [5]**

### **5.3 Data Extrapolation**

The DASY3 software automatically executes the following procedures to calculate the field units from the microvolt readings at the probe connector. The first step of the evaluation is a linearization of the filtered input signal to account for the compression characteristics of the detector diode. The compensation depends on the input signal, the diode type and the DC-transmission factor from the diode to the evaluation electronics. If the exciting field is pulsed, the crest factor of the signal must be known to correctly compensate for peak power. The formula for each channel can be given as [8]:

$V_i = U_i + U_i^2 \cdot \frac{cf}{dep_i}$	with	$V_i$ = compensated signal of channel i	(i=x,y,z)
$U_i$ = input signal of channel i	(i=x,y,z)		
$G = \text{crest factor of exciting field}$	(DASY parameter)		
$dcp_i = \text{diode compression point}$	(DASY parameter)		

From the compensated input signals the primary field data for each channel can be evaluated:

E-field probes: *Norm ConvF V E i i i* ⋅ = with V<sup>i</sup> = compensated signal of channel i (i = x,y,z) Norm<sup>i</sup> = sensor sensitivity of channel i (i = x,y,z) μV/(V/m)<sup>2</sup> for E-field probes ConvF = sensitivity of enhancement in solution E<sup>i</sup> = electric field strength of channel i in V/m

The RSS value of the field components gives the total field strength (Hermetian magnitude):

$$
E_{\text{tot}} = \sqrt{E_x^2 + E_y^2 + E_z^2}
$$

The primary field data are used to calculate the derived field units.



The power flow density is calculated assuming the excitation field to be a free space field.

$$
P_{\text{pwe}} = \frac{E_{\text{tot}}^2}{3770}
$$
 with 
$$
P_{\text{pwe}} = \text{equivalent power density of a plane wave in W/cm}^2
$$

$$
E_{\text{tot}} = \text{total electric field strength in V/m}
$$

# **6.1 PHANTOM, HOLDER AND THE EQUIVALENT TISSUES**

### **6.2 Generic Twin Phantom**

The Generic Twin Phantom is constructed of a fiberglass shell integrated in a wooden table. The shape of the shell is based on data from an anatomical study designed to determine the maximum exposure in at least 90% of all users [9][10]. It enables the dosimetric evaluation of left and right hand phone usage as well as body mounted usage at the flat phantom region. A cover prevents the evaporation of the liquid. Reference markings on the Phantom allow the complete setup of all predefined phantom positions and measurement grids by manually teaching three points in the robot. See Figure 8.



**Fig. 8 Generic Twin Phantom**

Shell Thickness  $2 \pm 0.1$  mm

Filling Volume Volume Approx. 20 liters Dimensions 810 x 1000 x 500 mm (H x L x W)

### **6.3 Tissue Simulating Mixture Characterization**

The mixtures consist of a viscous gel using hydroxethylcellullose (HEC) gelling agent and saline solution (see Table 1). Preservation with a bacteriacide is added and visual inspection is made to make sure air bubbles are not trapped during the mixing process. The mixture is calibrated to obtain proper dielectric constant (permittivity) and conductivity of brain or muscle tissue. The mixture characterizations used for the tissue simulating liquids are according to the data by C. Gabriel and G. Hartsgrove [11].



**Table 1. Composition of the Tissue Equivalent Matters**

### **6.4 Device Holder for Transmitters**

In combination with the Generic Twin Phantom V3.0, the Mounting Device (POM) enables the rotation of the mounted transmitter in spherical coordinates whereby the rotation points is the ear opening. The devices can be easily, accurately, and repeatably positioned according to the FCC and CENELEC specifications. The device holder can be locked at different phantom locations (left head, right head, flat phantom).



**Fig. 9. Device Holder**

\* Note: A simulating human hand is not used due to the complex anatomical and geometrical structure of the hand that may produced infinite number of configurations [10]. To produce the worst-case condition (the hand absorbs antenna output power), the hand is omitted during the tests.

# **7.1 SYSTEM SPECIFICATIONS**

### **7.2 Robotic System Specifications**

### **Specifications**



### **Data Acquisition Electronic (DAE) System**



### **PC Interface Card**

**Function:** 24 bit (64 MHz) DSP for real time processing Link to DAE3 16 bit A/D converter for surface detection system serial link to robot direct emergency stop output for robot

### **E-Field Probes**



### **Phantom**





# **8.1 MEASUREMENT PROCESS**

# **8.2 System Verification**

Prior to assessment, the system is verified to the ±5% of the specifications by using the system validation kit. (Graphics plots attached)



# **8.3 Dosimetric Assessment Setup**

The evaluation was performed with the following procedure:

- 1. The SAR value at a fixed location above the ear point was measured and was used as a reference value for assessing the power drop.
- 2. The SAR distribution at the exposed side of the head was measured at a distance of 3.9mm from the inner surface of the shell. The area covered the entire dimension of the head and the horizontal grid spacing was 20mm x 20mm. Based on this data, the area of the maximum absorption was determined by spline interpolation.
- 3. Around this point, a volume of 32mm x 32mm x 34mm was assessed by measuring 5 x 5 x 7 points. On this basis of this data set, the spatial peak SAR value was evaluated with the following procedure:
	- a. The data at the surface were extrapolated, since the center of the dipoles is 2.7mm away from the tip of the probe and the distance between the surface and the lowest measuring point is 1.2mm. The extrapolation was based on a least square algorithm [13]. A polynomial of the fourth order was calculated through the points in z-axes. This polynomial was then used to evaluate the points between the surface and the probe tip.
	- b. The maximum interpolated value was searched with a straight-forward algorithm. Around this maximum the SAR values averaged over the spatial volumes (1g or 10g) were computed using the 3D-Spline interpolation algorithm. The 3D-spline is composed of three one-dimensional splines with the "Not a knot" condition (in x,y, and z directions) [13][14]. The volume was integrated with the trapezoidal algorithm. One thousand points (10 x 10 x 10) were interpolated to calculate the average.
	- c. All neighboring volumes were evaluated until no neighboring volume with a higher average value was found.

4. The SAR value, at the same location as procedure #1, was re-measured. If the value changed by more than 5%, the evaluation is repeated.



**Fig 10. SAR Measurement Points in Area Scan**

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# **9.1 TEST POSITION OF THE RADIO**

# **9.2 FACE-HELD TEST SETUP**

The radio was placed in a normal operating position with the center of the mouthpiece aligned with the mouth and parallel to the face of the phantom (See figure 8.) Testing is performed with the use of a head/torso, or flat phantom, as applicable, filled with a muscle equivalent tissue. SAR test is then performed in antenna in and out (if applicable), or fixed antenna position using the low, middle and high channels.



**Figure 11. Diagram showing typical alignment of radio held to face.**

# **10.1 BODY-WORN CONFIGURATION TEST SETUP**

### **10.2 Ear-Microphone Jack**

Portable transmitting devices which have an Ear-Microphone jack must be evaluated for RF exposure in a body-worn configuration. The testing is performed with the use of a torso phantom filled with muscle equivalent tissue. The EUT is positioned with the keypad facing away from the phantom, and the Ear-Microphone wire attached to the phone jack, simulating the device placed in a shirt pocket or attached to a body holster. The SAR tests are then performed in both the antenna in and antenna out positions using the low, middle, and high channels to investigate the worst case SAR value (see Figure 12). Please note that body-worn configurations which have not been SAR tested may result in operating conditions that could exceed FCC RF exposure limits, therefore, users are cautioned to use tested and/or approved accessories.

### **A. Shirt Pocket Configuration**

The shirt pocket configuration is used for devices designed to be body-worn, and small enough to be placed inside a shirt pocket. To simulate the worstcase configuration, the EUT is placed in a torso position on the phantom with the keypad facing away from the phantom, and the Ear-Microphone wire connected to the phone to simulate hands-free operation in a shirt-pocket configuration (see Figure 13).

### **B. Body Holster Configuration**

The body holster configuration is used for body-worn devices which have a body holster accessory. Typically, a holster or carrying case is provided or available as an accessory item for supporting headset and body-worn operations. SAR may vary depending on the body separation distance provided by the type of holster and batteries supplied for a phone. In most cases, the antenna may become closer to the user's body than next to the head. The design of the holster permits the phone to be positioned only with the keypad facing away from the phantom. Proper usage of the holster restricts the antenna to a specified distance away from the surface of the body. For this test the EUT is placed into the holster and the holster is positioned against the torso of the phantom in a normal operating position. The Ear-Microphone wire is then connected to the phone to simulate handsfree operation in a body holster configuration (see Figure 14).

### **C. Other Configurations**

If other operating configurations are possible (i.e.: pants pocket, car adapter kit, etc), it will be indicated to users in the instruction manual about untested conditions and the possibility of exceeding FCC RF exposure limits for such use or the use of third-party accessories. If there is a high potential for exceeding limits in certain unintended configurations, a warning statement will be included in the manual, warning the user to avoid such operating conditions.



**Figure 12. Ear-Microphone Jack**



**Figure 13. Shirt Pocket Configuration**



**Figure 14. Body Holster Configuration**

# **11.1 ANSI/IEEE C95.1 - 1992 RF EXPOSURE LIMITS**



### **Table 2. Safety Limits for Partial Body Exposure [2]**

### **NOTES:**

- *\** The Spatial Peak value of the SAR averaged over any 1 gram of tissue (defined as a tissue volume in the shape of a cube) and over the appropriate averaging time.
- \*\* The Spatial Average value of the SAR averaged over the whole-body.
- **\*\*\*** The Spatial Peak value of the SAR averaged over any 10 grams of tissue (defined as a tissue volume in the shape of a cube) and over the appropriate averaging time.

**Uncontrolled Environments** are defined as locations where there is the exposure of individuals who have no knowledge or control of their exposure.

**Controlled Environments** are defined as locations where there is exposure that may be incurred by persons who are aware of the potential for exposure, (i.e. as a result of employment or occupation).

# **12.1 MEASUREMENT UNCERTAINTIES**

Measurement uncertainties in SAR measurements are difficult to quantify due to several variables including biological, physiological, and environmental. However, we estimate the measurement uncertainties in SAR to be less than 15-25 % [16].

According to ANSI/IEEE C95.3, the overall uncertainties are difficult to assess and will vary with the type of meter and usage situation. However, accuracy's of  $\pm$  1 to 3 dB can be expected in practice, with greater uncertainties in near-field situations and at higher frequencies (shorter wavelengths), or areas where large reflecting objects are present. Under optimum measurement conditions, SAR measurement uncertainties of at least  $\pm$  2dB can be expected.[3]

According to CENELEC [17], typical worst-case uncertainty of field measurements is  $\pm$  5 dB. For well-defined modulation characteristics the uncertainty can be reduced to  $\pm$  3 dB.



**Table 3. Breakdown of Errors [18]**

# **13.1 SAR TEST DATA SUMMARY**



# **13.2 Measurement Results (Mouth SAR including 50% Duty Cycle)**



### NOTES:

- 1. All modes of operation were investigated and the worst-case are reported.
- 2. Battery condition is fully charged for all readings.
- 
- 
- 3. Battery **X** Standard **D** Extended 4. \*Power Measured **X** Conducted **D** EIRP
- Frank and THE Conducted A EIRP OF ERP<br>
4. \*Power Measurement System **EXPEAG** OF IDX
- 5. SAR Measurement System x SPEAG o IDX
	-
- 
- 6. SAR Configuration **X** Mouth **O** Body **O** Hand
- 
- -
- 7. \*\*SAR Test Data includes a 50% Duty Cycle

**Randy Ortanez** President & Chief Engineer



**Figure 15. MOUTH SAR Test Setup**

# **13.1 SAR TEST DATA SUMMARY**



# **13.3 Measurement Results (Body SAR including 50% Duty Cycle)**



### NOTES:

- 1. All modes of operation were investigated and the worst-case are reported.
- 2. Battery condition is fully charged for all readings.<br>3. Battery Type  $\boxtimes$  Standard
- 
- 3. Battery Type **X** Standard **D** Extended 4. \* Power Measured **X** Conducted **D** EIRP
	-
- 4. \* Power Measured **X** Conducted **D** EIRP **D** ERP<br>5. SAR Measurement System **X** SPEAG **D** IDX 5. SAR Measurement System ⊠ SPEAG D IDX<br>5. SAR Configuration D Mouth ⊠ Body
- 6. SAR Configuration  $\Box$  Mouth  $\boxtimes$  Body  $\Box$  Hand 7. \*\* Test Configuration  $\boxtimes$  Belt Clip  $\Box$  Without Belt Clip
	-
- 7. \*\* Test Configuration
- 
- 
- 
- 
- 
- 8. \*\*\* SAR Test Data includes a 50% Duty Cycle

Randy Ortanez President & Chief Engineer



**Figure 16. BODY SAR Test Setup w/ Belt Clip**

# **14.1 SAR TEST EQUIPMENT**



### NOTE:

The E-field probe was calibrated by SPEAG. The SAR calibration of the E-field probe is performed by temperature measurement procedure. A TEM cell is used for the free space calibration of the probe. The tissue simulating material is calibrated by PCTEST using the dielectric probe system and network analyzer to determine the conductivity and permittivity (dielectric constant) of the desired equivalent material.

The following list of equipment was used to calibrate the equivalent materials:



# **15.1 CONCLUSION**

The SAR measurement indicates that the EUT complies with the RF radiation exposure limits of the FCC. These measurements are taken to simulate the RF effects exposure under worst-case conditions. Precise laboratory measures were taken to assure repeatability of the tests.

Please note that the absorption and distribution of electromagnetic energy in the body are very complex phenomena that depend on the mass, shape, and size of the body, the orientation of the body with respect to the field vectors, and the electrical properties of both the body and the environment. Other variables that may play a substantial role in possible biological effects are those that characterize the environment (e.g. ambient temperature, air velocity, relative humidity, and body insulation) and those that characterize the individual (e.g. age, gender, activity level, debilitation, or disease). Because innumerable factors may interact to determine the specific biological outcome of an exposure to electromagnetic fields, any protection guide shall consider maximal amplification of biological effects as a result of field-body interactions, environmental conditions, and physiological variables.[3]

# **16.1 REFERENCES:**

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[18] Prof. Dr. Niels Kuster, ETH, Eidgenössische Technische Hoschschule Zürich, *Dosimetric Evaluation of the Cellular Phone*.

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# **APPENDIX A – SAR TEST PLOTS**





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2.39E+0

1.19E+0

3.98E-1



Med. Parameters 450 MHz Muscle:  $\sigma = 0.82$  mho/m  $\epsilon_r = 57.5 \rho = 1.00$  g/cm<sup>3</sup>; Antenna Position -- Out; Crest Factor 1.0<br>**SAR** (1g): 11.2 mW/g, SAR (10g): 8.10 mW/g  $=$  57.5  $\rho = 1.00$  g/cm<sup>3</sup>; Antenna Position -- Out; Crest Factor 1.0 Generic Twin Phantom; Flat Section; Probe: ET3DV5 - SN1370 -- Probe Cal Date 02/00 Generic Twin Phantom; Flat Section; Probe: ET3DV5 - SN1370 -- Probe Cal Date 02/00 **SAR (1g): 11.2 mW/g,** SAR (10g): 8.10 mW/g Med. Parameters 450 MHz Muscle:  $\sigma = 0.82$  mho/m  $\varepsilon_r$ 

High Conducted Power = 5 Watts; Spacing = 1.5cm from flat phantom to radio back, w/Beltclip High Conducted Power = 5 Watts; Spacing = 1.5cm from flat phantom to radio back, w/Beltclip Vertex Standard Portable Radio Model: VX-900U Vertex Standard Portable Radio Model:VX-900U FM Low Channel 450.025MHz FM Low Channel 450.025MHz Test Date -- 12-11-200 Test Date -- 12-11-200









# **APPENDIX B – SAR TEST SETUP PHOTOGRAPHS**













# **APPENDIX C – DIPOLE VALIDATION DATA**



Med. Parameters 835 MHz Muscle:  $\sigma$  = 0.95 mho/m  $\varepsilon$ <sub>r</sub> = 56.2  $\rho$  = 1.00 g/cm<sup>3</sup>; Antenna Position -- Out; Crest Factor 1.0  $=$  56.2  $\rho = 1.00$  g/cm<sup>3</sup>; Antenna Position -- Out; Crest Factor 1.0 Generic Twin Phantom; Flat Section; Probe: ET3DV5 - SN1370 -- Probe Cal Date 02/00 Generic Twin Phantom; Flat Section; Probe: ET3DV5 - SN1370 -- Probe Cal Date 02/00 SAR (1g): 2.19 mW/g, SAR (10g): 1.44 mW/g SAR (1g): 2.19 mW/g, SAR (10g): 1.44 mW/g Med. Parameters 835 MHz Muscle:  $\sigma = 0.95$  mho/m  $\varepsilon_r$ 

835MHz Muscle Dipole Validation (D835V2 S/N: 406) 835MHz Muscle Dipole Validation (D835V2 S/N: 406) Frequency: 835 MHz; Antenna Input Power: 250 [mW] Frequency: 835 MHz; Antenna Input Power: 250 [mW] PCTEST Muscle Tissue Simulating Liquid PCTEST Muscle Tissue Simulating Liquid



# **APPENDIX D – PROBE CALIBRATION DATA**

# Probe ET3DV5

# SN:1370

Manufactured: February 1999 Calibrated: February 2000

Calibrated for System DASY3

### **ET3DV5 SN:1370**

# **Introduction**

The performance of all probes is measured before delivery. This includes an assessment of the characteristic parameters, receiving patterns as a function of frequency, frequency response and relative accuracy. Furthermore, each probe is tested in use according to a dosimetric assessment protocol. The sensitivity parameters (NormX, NormY, NormZ), the diode compresion parameter (DCP) and the conversion factor (ConvF) of the probe and some of the measurement diagrams are given in the following.

The performance of the individual probes varies slightly due to tolerances arising from the manufacturing process. Since the lines are highly resistive (several MOhms), the offset and noise problem is greatly increased if signals in the low µV range are measured. Accurate measurement below 10  $\mu$ W/g are possible if the following precautions are taken. 1) check the current grounding with the *multimeter*<sup>1</sup>, i.e., low noise levels, 2) compensate the current *offset*<sup>1</sup>, 3) use long integration time (approx. 10 seconds), 4) *calibrate*<sup> $I$ </sup> before each measurement, 5) persons should avoid moving around the lab while measuring.

Since the field distortion caused by the supporting material and the sheath is quite high in the  $\theta$  direction, the receiving pattern is poor in air. However, the distortion in tissue equivalent material is much less because of its high dielectricity. In addition, the fields induced in the phantoms by dipole structures close to



Fig 1: Due to the field distortion caused by the supporting material, the probe has two characteristic directions, referred to as angle  $ψ$  and  $θ$ .

the body are dominently parallel to the surface. Thus, the error due to non-isotropy is much better than 1 dB for dosimetric assessments.

The probes are calibrated in the TEM cell ifi 110 although the field distribution in the cell is not very uniform and the frequency response is not very flat. To ensure consistency, a strict protocol is followed. The conversion factor (ConF) between this calibration and the measurement in the tissue simulation solution is performed by comparison with temperature measurements and computer simulations. This conversion factor is only valid for the specified tissue simulating liquids at the specified frequencies. If measurements have to be performed in solutions with other electrical properties or at other frequencies, the conversion factor has to be assessed by the same procedure.

As the probes have been constructed with printed resistive lines on ceramic substrates (thick film technique), the probe is very delicate with respect to mechanical shocks.

### **Attention:**

**Do not drop the probe or let the probe collide with any solid object. Never let the robot move without first activating the emergency stop feature (i.e., without first turning the data acquisition electronics on).**

<sup>1</sup> Feature of the DASY Software Tool.

**ET3DV5 SN:1370**

# **DASY3 - Parameters of Probe: ET3DV5 SN:1370**

# Sensitivity in Free Space



# Diode Compression



# Sensitivity in Tissue Simulating Liquid



# Sensor Offset





# **Receiving Pattern (**φ)**,** θ **= 0°**



**Isotropy Error (**φ**),** θ **= 0°**



# **Frequency Response of E-Field**

**( TEM-Cell:ifi110, Waveguide R22, R26 )**



# **Dynamic Range f(SAR<sub>brain</sub>)**

**( TEM-Cell:ifi110 )**







# **Conversion Factor Assessment**

# **Receiving Pattern (**φ**)**

**( in brain tissue, z = 5 mm )**



# **APPENDIX E – EUT EXTERNAL PHOTOGRAPHS**











