

Specific Absorption Rate (SAR) Test Report
for
BENQ Corporation
on the
Mobile Phone

Report No. : O461002-1-2-02
Trade Name : BenQ
Model Name : M100(56F52)
FCC ID : JVPM100
Date of Testing : June 14~15, 2004
Date of Report. : June 17, 2004
Date of Review : June 18, 2004

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1. Statement of Compliance

The Specific Absorption Rate (SAR) maximum results found during testing for the **BENQ Corporation Mobile Phone M100 (56F52)** are **0.683 W/Kg for PCS head SAR and 1.13 W/Kg for PCS body SAR** with expanded uncertainty 20.6%. They are in compliance with Specific Absorption Rate (SAR) for general population/uncontrolled exposure limits specified in FCC 47 CFR part 2 (2.1093) and ANSI/IEEE C95.1-1999 and had been tested in accordance with the measurement methods and procedures specified in OET Bulletin 65 Supplement C (Edition 01-01).

Tested by

Approved by

Phillip Lin

Phillip Lin
Project Leader

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SAR Lab. Manager



2. Administration Data

2.1 Testing Laboratory

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2.2 Detail of Applicant

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2.3 Detail of Manufacturer

Company Name : BenQ Corporation
Address : 157 Shan-Ying Road, Gueishan, Taoyuan 333, Taiwan R.O.C.

2.4 Application Detail

Date of reception of application: June 10, 2004
Start of test : June 14, 2004
End of test : June 15, 2004



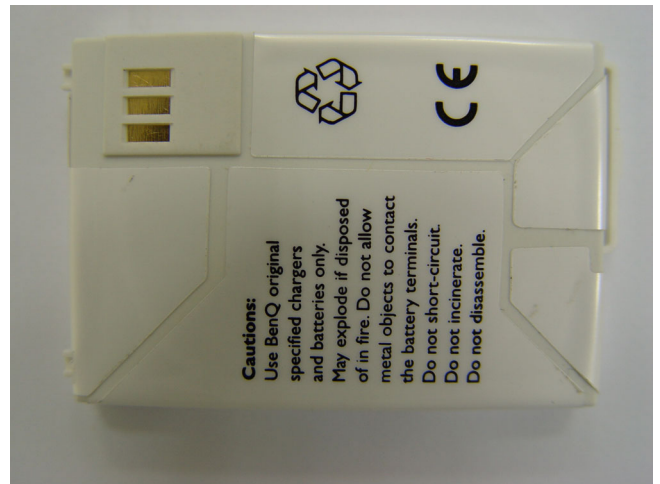
3. General Information

3.1 Description of Device Under Test (DUT)

DUT Type :	Mobile Phone
Trade Name :	BenQ
Model Name :	M100 (56F52)
FCC ID :	JVPM100
Tx Frequency :	1850-1910 MHz (PCS)
Rx Frequency :	1930-1990MHz (PCS)
Antenna Type :	Fixed Internal
Maximum Power Rating :	30.32 dBm
HW Version:	LPR3
SW Version:	0.15
Type of Modulation :	GMSK
DUT Stage:	Identical Prototype
Application Type :	Certification



3.2 Product Photo





3.2 Applied Standards:

The Specific Absorption Rate (SAR) testing specification, method and procedure for this Mobile Phone is in accordance with the following standards:

47 CFR Part 2 (2.1093),
IEEE C95.1-1999,
IEEE C95.3-1991,
IEEE P1528 -200X, and
OET Bulletin 65 Supplement C (Edition 01-01)



3.3 Device Category and SAR Limits

This device belongs to portable device category because its radiating structure is allowed to be used within 20 centimeters of the body of the user.

Limit for General Population/Uncontrolled exposure should be applied for this device, it is 1.6 W/kg as averaged over any 1 gram of tissue.

3.4 Test Conditions:

3.4.1 Ambient Condition

Item	Head	Body
Ambient Temperature (°C)	20-24°C	
Tissue simulating liquid temperature (°C)	22.2°C	21.9°C
Humidity (%)	<60%	

3.4.2 Test Configuration

The device was controlled by using a base station emulator CMU 200. Communication between the device and the emulator was established by air link. The distance between the DUT and the antenna of the emulator is larger than 50 cm and the output power radiated from the emulator antenna is at least 30 dB smaller than the output power of DUT.

Measurements were performed on the lowest, middle , and highest channel for each testing position for head SAR testing. Measurements were performed only on the middle channel if the SAR is below 3 dB of limit for body SAR testing.

The DUT was set from the emulator to radiate maximum output power during all testing.

For head and body SAR testing, EUT is in GSM link mode, and its crest factor is 8.3.



4. Specific Absorption Rate (SAR)

4.1 Introduction

SAR is related to the rate at which energy is absorbed per unit mass in an object exposed to a radio field. The SAR distribution in a biological body is complicated and is usually carried out by experimental techniques or numerical modeling. The standard recommends limits for two tiers of groups, occupational/controlled and general population/uncontrolled, based on a person's awareness and ability to exercise control over his or her exposure. In general, occupational/controlled exposure limits are higher than the limits for general population/uncontrolled.

4.2. SAR Definition

The SAR definition is the time derivative (rate) of the incremental energy (dW) absorbed by (dissipated in) an incremental mass (dm) contained in a volume element (dv) of a given density.

ρ). The equation description is as below:

$$\mathbf{SAR} = \frac{d}{dt} \left(\frac{dW}{dm} \right) = \frac{d}{dt} \left(\frac{dW}{\rho dv} \right)$$

SAR is expressed in units of Watts per kilogram (W/kg)

SAR measurement can be either related to the temperature elevation in tissue by

$$\mathbf{SAR} = C \frac{\delta T}{\delta t}$$

, where C is the specific heat capacity, δT is the temperature rise and δt the exposure duration,

or related to the electrical field in the tissue by

$$\mathbf{SAR} = \frac{\sigma |E|^2}{\rho}$$

, where σ is the conductivity of the tissue, ρ is the mass density of the tissue and E is the rms electrical field strength.

However for evaluating SAR of low power transmitter, electrical field measurement is typically applied.

5. SAR Measurement Setup

Remote Control Box

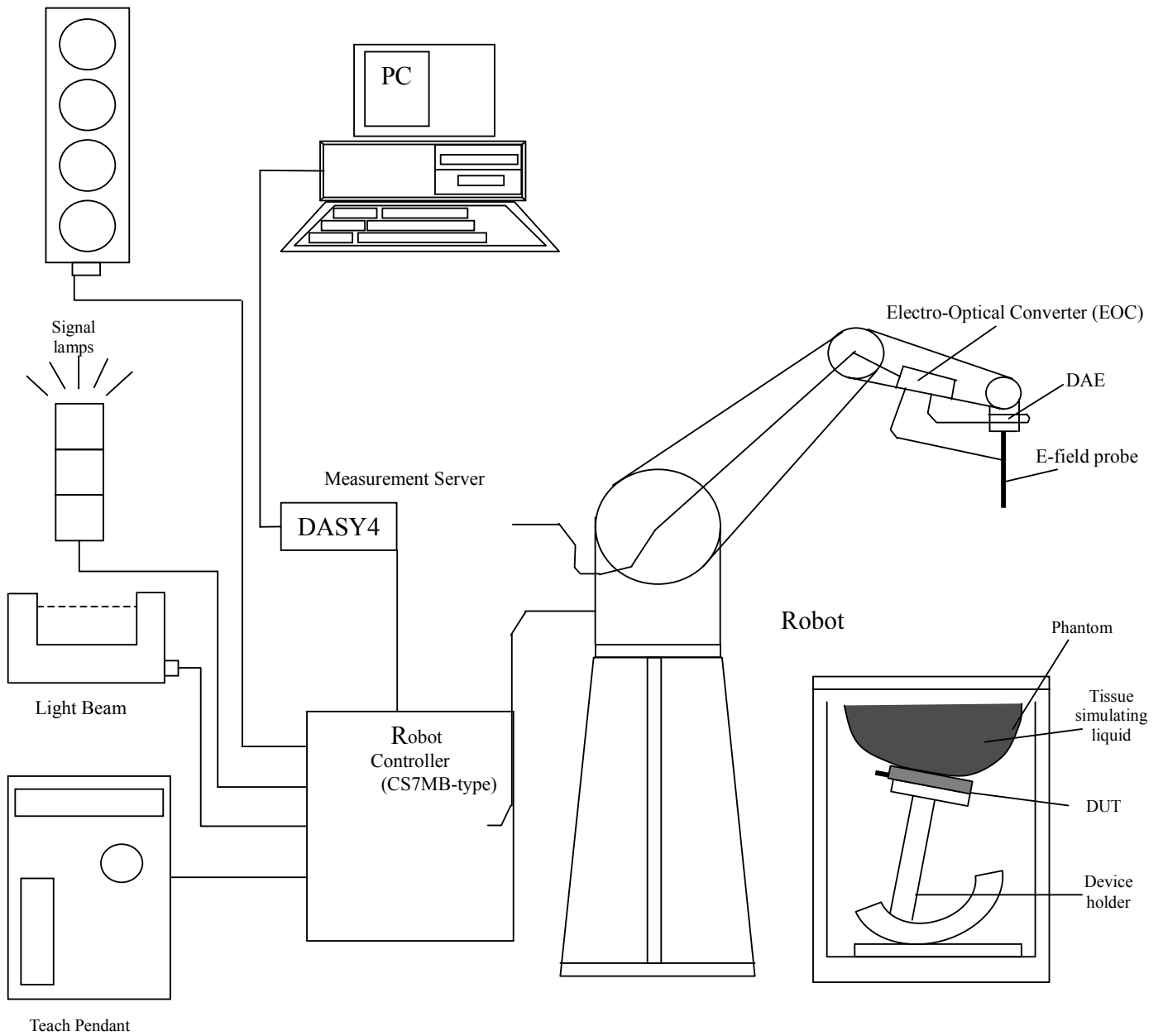


Fig. 5.1 DASY4 system



The DASY4 system for performance compliance tests is illustrated above graphically. This system consists of the following items:

- A standard high precision 6-axis robot with controller, a teach pendant and software
- A data acquisition electronic (DAE) attached to the robot arm extension
- A dosimetric probe equipped with an optical surface detector system
- The electro-optical converter (ECO) performs the conversion between optical and electrical signals
- A measurement server performs the time critical tasks such as signal filtering, control of the robot operation and fast movement interrupts.
- A probe alignment unit which improves the accuracy of the probe positioning
- A computer operating Windows XP
- DASY4 software
- Remote control with teach pendant and additional circuitry for robot safety such as warning lamps, etc.
- The SAM twin phantom
- A device holder
- Tissue simulating liquid
- Dipole for evaluating the proper functioning of the system

Some of the components are described in details in the following sub-sections.

5.1.DASY4 E-Field Probe System

The SAR measurement is conducted with the dosimetric probe ET3DV6 (manufactured by SPEAG). The probe is specially designed and calibrated for use in liquid with high permittivity. The dosimetric probe has special calibration in liquid at different frequency. This probe has a built in optical surface detection system to prevent from collision with phantom.

Calibration: Required once a year.



5.1.1.ET3DV6 E-Field Probe Specification

Construction	Symmetrical design with triangular core Built-in optical fiber for surface detection system Built-in shielding against static charges PEEK enclosure material (resistant to organic solvents)
Calibration	Simulating tissue at frequencies of 900MHz, 1.8GHz and 2.45GHz for brain and muscle (accuracy $\pm 8\%$)
Frequency	10 MHz to > 3 GHz
Directivity	± 0.2 dB in brain tissue (rotation around probe axis) ± 0.4 dB in brain tissue (rotation perpendicular to probe axis)
Dynamic Range	5μ W/g to > 100mW/g; Linearity: ± 0.2 dB
Surface Detection	± 0.2 mm repeatability in air and clear liquids on reflecting surface
Dimensions	Overall length: 330mm Tip length: 16mm Body diameter: 12mm Tip diameter: 6.8mm Distance from probe tip to dipole centers: 2.7mm
Application	General dosimetry up to 3GHz Compliance tests for mobile phones and Wireless LAN Fast automatic scanning in arbitrary phantoms



Fig. 5.2 Probe setup on robot

5.1.2 ET3DV6 E-Field Probe Calibration

Each probe needs to be calibrated according to a dosimetric assessment procedure with accuracy better than $\pm 10\%$. The spherical isotropy shall be evaluated and within ± 0.25 dB. The sensitivity parameters (NormX, NormY, and NormZ), the diode compression parameter (DCP) and the conversion factor (ConvF) of the probe are tested. The calibration data are as below:



Sensitivity	X axis : 1.68 μ V	Y axis : 1.62 μ V	Z axis : 1.71 μ V	
Diode compression point	X axis : 95 mV	Y axis : 95 mV	Z axis : 95 mV	
Conversion factor (Head/Body)	Frequency (MHz)	X axis	Y axis	Z axis
	800~1000	6.6/6.5	6.6/6.5	6.6/6.5
	1710~1990	5.3/5.0	5.3/5.0	5.3/5.0
Boundary effect (Head/Body)	Frequency (MHz)	Alpha	Depth	
	800~1000	0.34/0.31	2.48/2.92	
	1710~1990	0.43/0.51	2.80/2.78	

NOTE:

- The probe parameters have been calibrated by the SPEAG.

5.2 DATA Acquisition Electronics (DAE)

The data acquisition electronics (DAE4) consists of a highly sensitive electrometer-grade preamplifier with auto-zeroing, a channel and gain-switching multiplexer, a fast 16 bit AD-converter and a command decoder and control logic unit. Transmission to the measurement server is accomplished through an optical downlink for data and status information as well as an optical uplink for commands and the clock.

The mechanical probe mounting device includes two different sensor systems for frontal and sideways probe contacts. They are used for mechanical surface detection and probe collision detection.

The input impedance of the DAE4 is 200M Ohm; the inputs are symmetrical and floating. Common mode rejection is above 80dB.

Calibration: Required once a year.



5.3 Robot

The DASY4 system uses the high precision robots RX90BL type out of the newer series from Stäubli SA (France). For the 6-axis controller DASY4 system, the CS7MB robot controller version from Stäubli is used. The RX robot series have many features that are important for our application:

- High precision (repeatability 0.02 mm)
- High reliability (industrial design)
- Jerk-free straight movements
- Low ELF interference (the closed metallic construction shields against motor control fields)
- 6-axis controller

5.4 Measurement Server

The DASY4 measurement server is based on a PC/104 CPU board with
166 MHz CPU
32 MB chipset and
64 MB RAM.

Communication with
the DAE4 electronic box
the 16-bit AD-converter system for optical detection and digital I/O interface.

The measurement server performs all the real-time data evaluation for field measurements and surface detection, controls robot movements and handles safety operations.

Calibration: No calibration required.

5.5 SAM Twin Phantom

The SAM twin phantom is a fiberglass shell phantom with 2mm shell thickness (except the ear region where shell thickness increases to 6mm). It has three measurement areas:

- Left head
- Right head
- Flat phantom

The bottom plate contains three pair of bolts for locking the device holder. The device holder positions are adjusted to the standard measurement positions in the three sections.



A white cover is provided to tap the phantom during off-periods to prevent water evaporation and changes in the liquid parameters.

On the phantom top, three reference markers are provided to identify the phantom position with respect to the robot.

The phantom can be used with the following tissue simulating liquids:

- *Water-sugar based liquid
- *Glycol based liquids

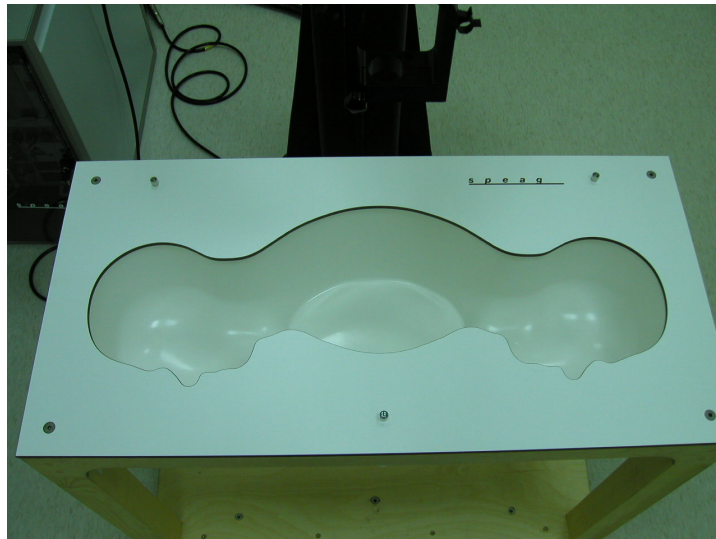


Fig. 5.3 Top view of twin phantom



Fig. 5.4 Bottom view of twin phantom

5.6. Device Holder for SAM Twin Phantom

The SAR in the Phantom is approximately inversely proportional to the square of the distance between the source and the liquid surface. For a source in 5 mm distance, a positioning uncertainty of $\pm 0.5\text{mm}$ would produce a SAR uncertainty of $\pm 20\%$. An accurate device position is therefore crucial for accurate and repeatable measurement. The position in which the devices must be measured, are defined by the standards.

The DASY device holder is designed to cope with different positions given in the standard. It has two scales for the device rotation (with respect to the body axis) and the device inclination (with respect to the line between the ear reference points). The rotation centers for both scales is the ear reference point (EPR). Thus the device needs no repositioning when changing the angles.

The DASY device holder has been made out of low-loss POM material having the following dielectric parameters: relative permittivity $\epsilon_r=3$ and loss tangent $\delta = 0.02$. The amount of dielectric material has been reduced in the closest vicinity of the device, since measurements have suggested that the influence of the clamp on the test results could thus be lowered.



Fig. 5.5 Device Holder



5.7 Data Storage and Evaluation

5.7.1 Data Storage

The DASY4 software stores the assessed data from the data acquisition electronics as raw data (in microvolt readings from the probe sensors), together with all the necessary software parameters for the data evaluation (probe calibration data, liquid parameters and device frequency and modulation data) in measurement files with the extension .DA4. The postprocessing software evaluates the desired unit and format for output each time the data is visualized or exported. This allows verification of the complete software setup even after the measurement and allows correction of erroneous parameter settings. For example, if a measurement has been performed with an incorrect crest factor parameter in the device setup, the parameter can be corrected afterwards and the data can be reevaluated.

The measured data can be visualized or exported in different units or formats, depending on the selected probe type (e.g., [V/m], [A/m], [mW/g]). Some of these units are not available in certain situations or give meaningless results, e.g., a SAR-output in a loseless media, will always be zero. Raw data can also be exported to perform the evaluation with other software packages.

5.7.2 Data Evaluation

The DASY4 postprocessing software (SEMCAD) automatically executes the following procedures to calculate the field units from the microvolt readings at the probe connector. The parameters used in the evaluation are stored in the configuration modules of the software :

Probe parameters :	- Sensitivity	$Norm_i, a_{i,0}, a_{i,1}, a_{i,2}$
	- Conversion factor	$ConvF_i$
	- Diode compression point	dcp_i
Device parameters :	- Frequency	f
	- Crest factor	cf
Media parameters :	- Conductivity	σ
	- Density	ρ

These parameters must be set correctly in the software. They can be found in the component documents or they can be imported into the software from the configuration files issued for the DASY components. In the direct measuring mode of the multimeter option, the parameters of the actual system setup are used. In the scan visualization and export modes, the parameters stored in the corresponding document files are used.

The first step of the evaluation is a linearization of the filtered input signal to account for the compression characteristics of the detector diode. The compensation depends on the input signal, the diode type and the DC-transmission factor from the diode to the evaluation electronics. If the exciting field is pulsed, the crest



factor of the signal must be known to correctly compensate for peak power. The formula for each channel can be given as :

$$V_i = U_i + U_i^2 \cdot \frac{cf}{dcp_i}$$

with $V_i =$ compensated signal of channel i ($i = x, y, z$)
 $U_i =$ input signal of channel i ($i = x, y, z$)
 $cf =$ crest factor of exciting field (DASY parameter)
 $dcp_i =$ diode compression point (DASY parameter)

From the compensated input signals, the primary field data for each channel can be evaluated :

$$\text{E-field probes : } E_i = \sqrt{\frac{V_i}{Norm_i ConvF}}$$

$$\text{H-field probes : } H_i = \sqrt{V_i \frac{a_{i0} + a_{i1}f + a_{i2}f^2}{f}}$$

with $V_i =$ compensated signal of channel i ($i = x, y, z$)
 $Norm_i =$ sensor sensitivity of channel i ($i = x, y, z$)
 $\mu V/(V/m)^2$ for E-field Probes
 $ConvF =$ sensitivity enhancement in solution
 $a_{ij} =$ sensor sensitivity factors for H-field probes
 $f =$ carrier frequency [GHz]
 $E_i =$ electric field strength of channel i in V/m
 $H_i =$ magnetic field strength of channel i in A/m

The RSS value of the field components gives the total field strength (Hermitian magnitude) :

$$E_{tot} = \sqrt{E_x^2 + E_y^2 + E_z^2}$$

The primary field data are used to calculate the derived field units.

$$SAR = E_{tot}^2 \cdot \frac{\sigma}{\rho \cdot 1000}$$

with $SAR =$ local specific absorption rate in mW/g
 $E_{tot} =$ total field strength in V/m
 $\sigma =$ conductivity in [mho/m] or [Siemens/m]



ρ = equivalent tissue density in g/cm³

*Note that the density is set to 1, to account for actual head tissue density rather than the density of the tissue simulating liquid.

The power flow density is calculated assuming the excitation field to be a free space field.

$$P_{pwe} = \frac{E_{tot}^2}{3770} \quad \text{or} \quad P_{pwe} = H_{tot}^2 \cdot 37.7$$

with P_{pwe} = equivalent power density of a plane wave in mW/cm²
 E_{tot} = total electric field strength in V/m
 H_{tot} = total magnetic field strength in A/m



5.8. Test Equipment List

Manufacture	Name of Equipment	Type/Model	Serial Number	Calibration	
				Last Cal.	Due Date
SPEAG	Dosimetric E-Filed Probe	ET3DV6	1788	Aug. 29, 2003	Aug. 29, 2004
SPEAG	835MHz System Validation Kit	D835V2	499	Feb. 12, 2004	Feb. 12, 2005
SPEAG	900MHz System Validation Kit	D900V2	190	July 17, 2003	July 17, 2004
SPEAG	1800MHz System Validation Kit	D1800V2	2d076	July 16, 2003	July 16, 2004
SPEAG	1900MHz System Validation Kit	D1900V2	5d041	Feb. 17, 2004	Feb. 17, 2005
SPEAG	2450MHz System Validation Kit	D2450V2	736	Aug. 26, 2003	Aug. 26, 2004
SPEAG	Data Acquisition Electronics	DAE3	577	Nov. 21, 2003	Nov. 21, 2004
SPEAG	Device Holder	N/A	N/A	NCR	NCR
SPEAG	Phantom	QD 000 P40 C	TP-1150	NCR	NCR
SPEAG	Robot	Staubli RX90BL	F03/5W15A1/A/01	NCR	NCR
SPEAG	Software	DASY4 V4.1 Build 47	N/A	NCR	NCR
SPEAG	Software	SEMCAD V1.6 Build 116	N/A	NCR	NCR
SPEAG	Measurement Server	SE UMS 001 BA	1021	NCR	NCR
Agilent	S-Parameter Network Analyzer (PNA)	E8358A	US40260131	Oct. 17, 2003	Oct. 17, 2004
Agilent	Dielectric Probe Kit	85070D	US01440205	NCR	NCR
Agilent	Dual Directional Coupler	778D	50422	NCR	NCR
Agilent	Power Amplifier	8449B	3008A01917	Sep. 16, 2003	Sep. 16, 2004
R & S	Radio Communication Tester	CMU200	103937	Oct. 20, 2003	Oct. 20, 2004
Agilent	Power Meter	E4416A	GB41292344	Feb. 12, 2004	Feb. 12, 2005
Agilent	Signal Generator	E8247C	MY43320596	Feb. 10, 2004	Feb. 10, 2005
Agilent	Base Station Emulator	E5515C	GB43460754	Jan. 12, 2004	Jan. 12, 2005

Table 5.1 Test Equipment List



6. Tissue Simulating Liquids

For the measurement of the field distribution inside the SAM phantom with DASY4, the phantom must be filled with around 25 liters of homogeneous tissue simulating liquid. The liquid height from the ear reference point (ERP) of the phantom to the liquid top surface is (head SAR) or from the flat phantom to the liquid top surface (body SAR) is 15.2cm.

The following ingredients for tissue simulating liquid are used:

- **Water:** deionized water (pure H₂O), resistivity $\geq 16M\Omega$ - as basis for the liquid
- **Sugar:** refined sugar in crystals, as available in food shops – to reduce relative permittivity
- **Salt:** pure NaCl – to increase conductivity
- **Cellulose:** Hydroxyethyl-cellulose, medium viscosity (75-125 mPa.s, 2% in water, 20°C), CAS#54290-to increase viscosity and to keep sugar in solution.
- **Preservative:** Preventol D-7 Bayer AG, D-51368 Leverkusen, CAS#55965-84-9- to prevent the spread of bacteria and molds.
- **DGMBE:** Deithlenglycol-monobuthyl ether (DGMBE), Fluka Chemie GmbH, CAS#112-34-5 – to reduce relative permittivity.

Table 6.1 gives the recipes for one liter of head and body tissue simulating liquid for frequency band 1900 MHz.

Ingredient	HSL-1900	MSL-1900
Water	552.42 g	716.56 g
Cellulose	0 g	0 g
Salt	3.06 g	4.0 g
Preventol D-7	0 g	0 g
Sugar	0 g	0 g
DGMBE	444.52 g	300.67 g
Total amount	1 liter (1.0 kg)	1 liter (1.0 kg)
Dielectric Parameters at 22°	f= 1900 MHz $\epsilon_r = 40.0 \pm 5\%$, $\sigma = 1.4 \pm 5\%$ S/m	f= 1900 MHz $\epsilon_r = 53.3 \pm 5\%$, $\sigma = 1.52 \pm 5\%$ S/m

Table 6.1

The dielectric parameters of the liquids were verified prior to the SAR evaluation using an Agilent 85070D Dielectric Probe Kit and an Agilent E8358A Network Analyzer.



Table 6.2 shows the measuring results for head and muscle simulating liquid.

	Bands	Frequency(MHz)	Permittivity (ϵ_r)	Conductivity (σ)	Measurement Date
Head	PCS band (1850 ~ 1910 MHz)	1850.2	39.3	1.38	June 15, 2004
		1880.0	39.3	1.41	
		1909.8	39.2	1.44	
Body	PCS band (1850 ~ 1910 MHz)	1850.2	52.3	1.49	June 14, 2004
		1880.0	52.2	1.52	
		1909.8	52	1.55	

Table 6.2

The measuring data are consistent with $\epsilon_r = 40.0 \pm 5\%$ and $\sigma = 1.4 \pm 5\%$ for head PCS band and $\epsilon_r = 53.3 \pm 5\%$ and $\sigma = 1.52 \pm 5\%$ for body PCS band.



7. Uncertainty Assessment

The component of uncertainty may generally be categorized according to the methods used to evaluate them. The evaluation of uncertainty by the statistical analysis of a series of observations is termed a Type A evaluation of uncertainty. The evaluation of uncertainty by means other than the statistical analysis of a series of observation is termed a Type B evaluation of uncertainty. Each component of uncertainty, however evaluated, is represented by an estimated standard deviation, termed standard uncertainty, which is determined by the positive square root of the estimated variance.

A Type A evaluation of standard uncertainty may be based on any valid statistical method for treating data. This includes calculating the standard deviation of the mean of a series of independent observations; using the method of least squares to fit a curve to the data in order to estimate the parameter of the curve and their standard deviations; or carrying out an analysis of variance in order to identify and quantify random effects in certain kinds of measurement.

A type B evaluation of standard uncertainty is typically based on scientific judgment using all of the relevant information available. These may include previous measurement data, experience and knowledge of the behavior and properties of relevant materials and instruments, manufacture’s specification, data provided in calibration reports and uncertainties assigned to reference data taken from handbooks. Broadly speaking, the uncertainty is either obtained from an outdoor source or obtained from an assumed distribution, such as the normal distribution, rectangular or triangular distributions indicated in Table 7.1

Uncertainty Distributions	Normal	Rectangular	Triangular	U-shape
Multiplying factor ^(a)	1/k (b)	1/√3	1/√6	1/√2

(a) standard uncertainty is determined as the product of the multiplying factor and the estimated range of variations in the measured quantity

(b) k is the coverage factor

Table 7.1

The combined standard uncertainty of the measurement result represents the estimated standard deviation of the result. It is obtained by combining the individual standard uncertainties of both Type A and Type B evaluation using the usual “root-sum-squares” (RSS) methods of combining standard deviations by taking the positive square root of the estimated variances.

Expanded uncertainty is a measure of uncertainty that defines an interval about the measurement result within which the measured value is confidently believed to lie. It is obtained by multiplying the combined standard uncertainty by a coverage factor. Typically, the coverage factor ranges from 2 to 3. Using a coverage factor allows the true value of a measured quantity to be specified with a defined probability within the specified uncertainty range. For purpose of this document, a coverage factor two is used, which corresponds to confidence interval of about 95 %. The DASY4 uncertainty Budget is showed in



Table 7.2.

Error Description	Uncertainty Value \pm %	Probability Distribution	Divisor	C_i $1g$	Standard Unc. (1-g)	v_i or V_{eff}
Measurement System						
Probe Calibration	± 4.8	Normal	1	1	± 4.8	∞
Axial Isotropy	± 4.7	Rectangular	$\sqrt{3}$	$(1-C_p)^{1/2}$	± 1.9	∞
Hemispherical Isotropy	± 9.6	Rectangular	$\sqrt{3}$	$(C_p)^{1/2}$	± 3.9	∞
Boundary Effect	± 1.0	Rectangular	$\sqrt{3}$	1	± 0.6	∞
Linearity	± 4.7	Rectangular	$\sqrt{3}$	1	± 2.7	∞
System Detection Limit	± 1.0	Rectangular	$\sqrt{3}$	1	± 0.6	∞
Readout Electronics	± 1.0	Rectangular	1	1	± 1.0	∞
Response Time	± 0.8	Normal	$\sqrt{3}$	1	± 0.5	∞
Integration time	± 2.6	Rectangular	$\sqrt{3}$	1	± 1.5	∞
RF Ambient Conditions	± 3.0	Rectangular	$\sqrt{3}$	1	± 1.7	∞
Probe Positioner Mech. Tolerance	± 0.4	Rectangular	$\sqrt{3}$	1	± 0.2	∞
Probe Positioning with respect to Phantom Shell	± 2.9	Rectangular	$\sqrt{3}$	1	± 1.7	∞
Extrapolation and Interpolation Algorithms for Max. SAR Evaluation	± 1.0	Rectangular	$\sqrt{3}$	1	± 0.6	∞
Test sample Related						
Test sample Positioning	± 2.9	Normal	1	1	± 2.9	145
Device Holder Uncertainty	± 3.6	Normal	1	1	± 3.6	5
Output Power Variation-SAR drift measurement	± 2.5	Rectangular	$\sqrt{3}$	1	± 1.4	∞
Phantom and Tissue parameters						
Phantom uncertainty(Including shape and thickness tolerances)	± 4.0	Rectangular	$\sqrt{3}$	1	± 2.3	∞
Liquid Conductivity Target tolerance	± 5.0	Rectangular	$\sqrt{3}$	0.64	± 1.8	∞
Liquid Conductivity measurement uncertainty	± 2.5	Normal	1	0.64	± 1.6	∞
Liquid Permittivity Target tolerance	± 5.0	Rectangular	$\sqrt{3}$	0.6	± 1.7	∞
Liquid Permittivity measurement uncertainty	± 2.0	Normal	1	0.6	± 1.2	∞
Combined standard uncertainty					± 10.3	330
Coverage Factor for 95 %		K=2				
Expanded uncertainty (Coverage factor = 2)					± 20.6	



Table 7.2. Uncertainty Budget of DASYS

8. SAR Measurement Evaluation

Each DASYS system is equipped with one or more system validation kits. These units, together with the predefined measurement procedures within the DASYS software, enable the user to conduct the system performance check and system validation. System validation kit includes a dipole, tripod holder to fix it underneath the flat phantom and a corresponding distance holder.

8.1 Purpose of System Performance check

The system performance check verifies that the system operates within its specifications. System and operator errors can be detected and corrected. It is recommended that the system performance check be performed prior to any usage of the system in order to guarantee reproducible results. The system performance check uses normal SAR measurements in a simplified setup with a well characterized source. This setup was selected to give a high sensitivity to all parameters that might fail or vary over time. The system check does not intend to replace the calibration of the components, but indicates situations where the system uncertainty is exceeded due to drift or failure.

8.2 System Setup

In the simplified setup for system evaluation, the DUT is replaced by a calibrated dipole and the power source is replaced by a continuous wave which comes from a signal generator at frequency 1900 MHz. The calibrated dipole must be placed beneath the flat phantom section of the SAM twin phantom with the correct distance holder. The distance holder should touch the phantom surface with a light pressure at the reference marking and be oriented parallel to the long side of the phantom. The equipment setup is shown below:

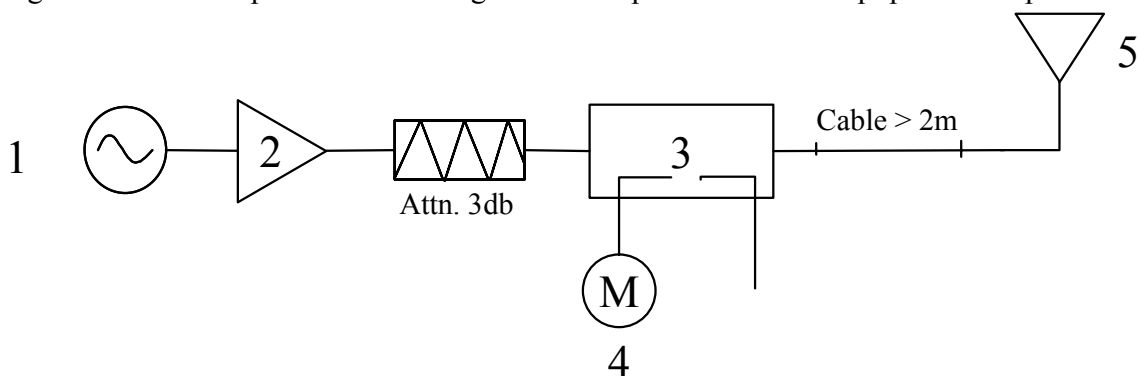


Fig. 8.1



1. Signal Generator
2. Amplifier
3. Directional Coupler
4. Power Meter
5. 1900 MHz Dipole

The output power on dipole port must be calibrated to 20dBm (100mW) before dipole is connected.

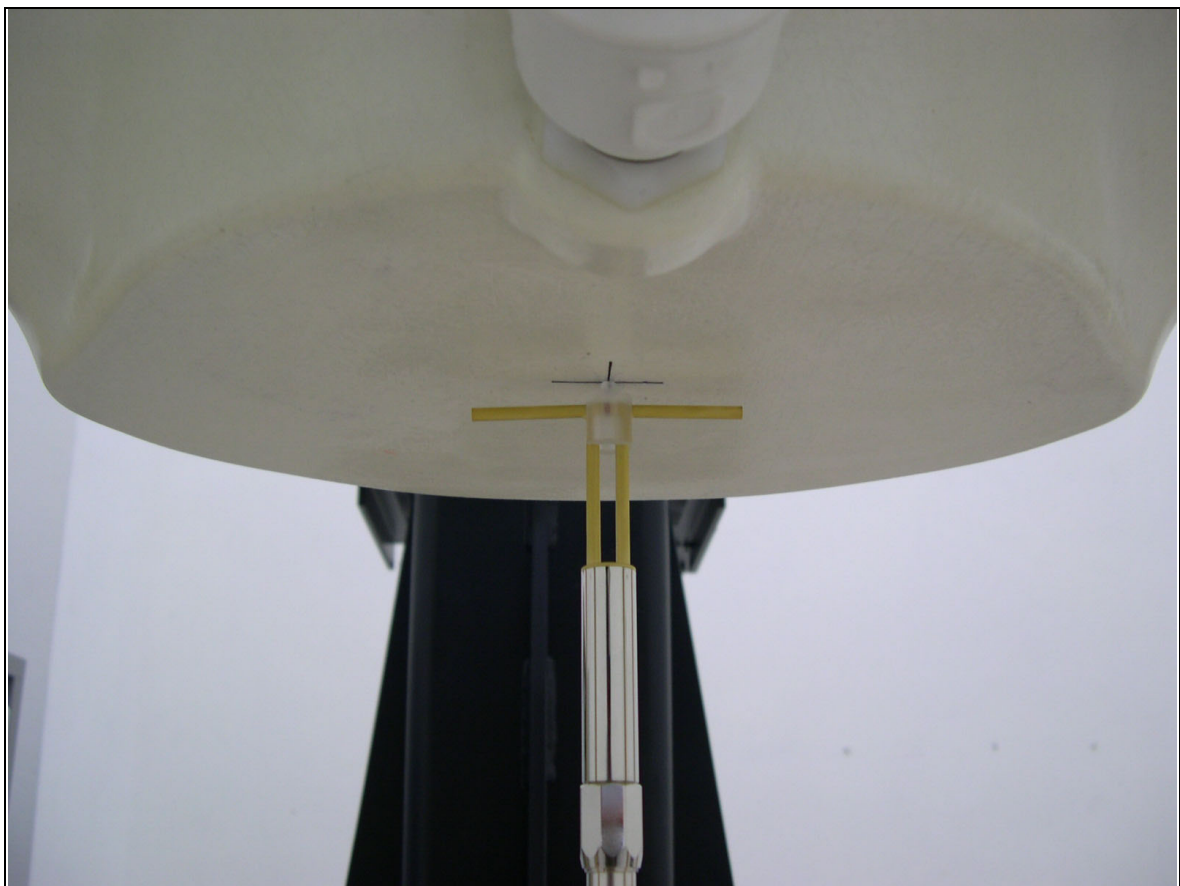


Fig 8.2 Dipole Setup



8.3 Validation Results

Comparing to the original SAR value provided by Speag, the validation data should be within its specification of 10 %. Table 8.1 shows the target SAR and measured SAR after normalized to 1W input power.

		Target (W/kg)	Measurement data (W/kg)	Variation
PCS band (1900MHz) for head	SAR (1g)	41.6	39.8	-4.3 %
	SAR (10g)	21.6	21	-2.8 %
PCS band (1900MHz) for body	SAR (1g)	42	39.9	-5.0 %
	SAR (10g)	22	21.4	-2.7 %

Table 8.3

The table above indicates the system performance check can meet the variation criterion.



9. Description for DUT Testing Position

This DUT was tested in 6 different positions. They are left cheek, left tilted, right cheek, right tilted, body worn with keypad up and body worn with keypad down as illustrated below:

- 1) “Cheek Position”
 - i) To position the device with the vertical center line of the body of the device and the horizontal line crossing the center piece in a plane parallel to the sagittal plane of the phantom. While maintaining the device in this plane, align the vertical center line with the reference plane containing the three ear and mouth reference point (M, RE and LE) and align the center of the ear piece with the line RE-LE.
 - ii) To move the device towards the phantom with the ear piece aligned with the line LE-RE until the phone touched the ear. While maintaining the device in the reference plane and maintaining the phone contact with the ear, move the bottom of the phone until any point on the front side is in contact with the cheek of the phantom or until contact with the ear is lost (see Fig. 9.1).

- 2) “Tilted Position”
 - i) To position the device in the “cheek” position described above
 - ii) While maintaining the device the reference plane described above and pivoting against the ear, move it outward away from the mouth by an angle of 15 degrees or until contact with the ear is lost (see Fig. 9.2).

- 3) “Body Worn”
 - i) To position the device parallel to the phantom surface with either keypad up or down
 - ii) To adjust the phone parallel to the flat phantom
 - iii) To adjust the distance between the phone top/bottom surface and the flat phantom to 1.5 cm

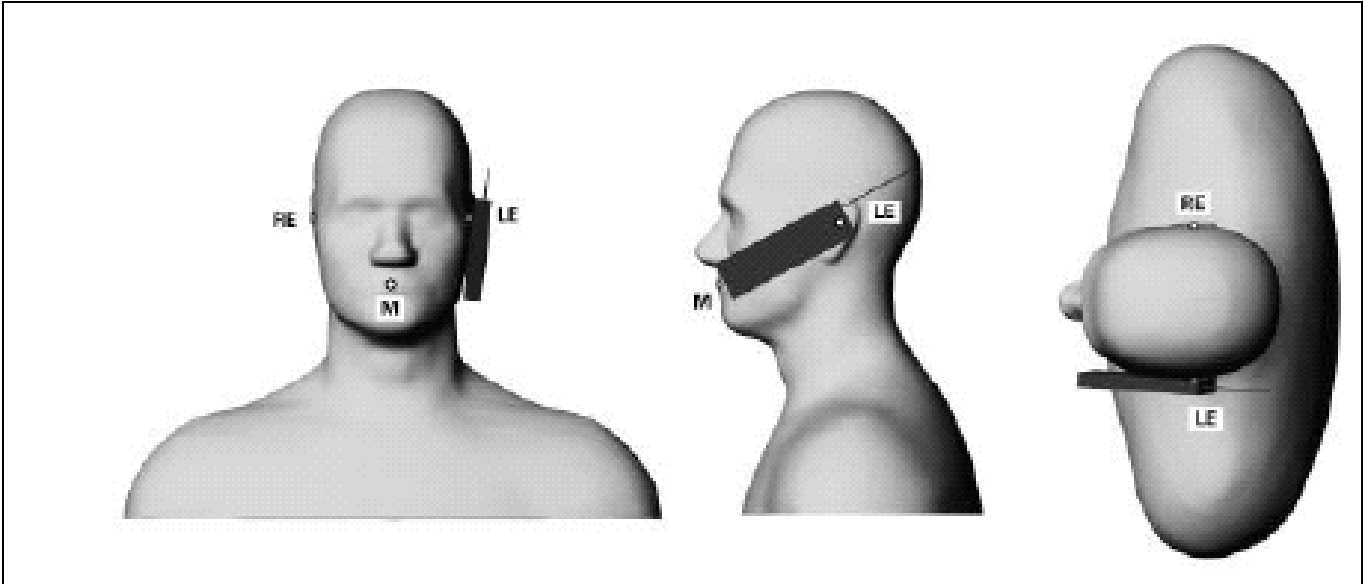


Fig. 9.1 Phone Position 1, “Cheek” or “Touch” Position. The reference points for the right ear (RE), left ear (LE) and mouth (M), which define the plane for phone positioning, are indicated.

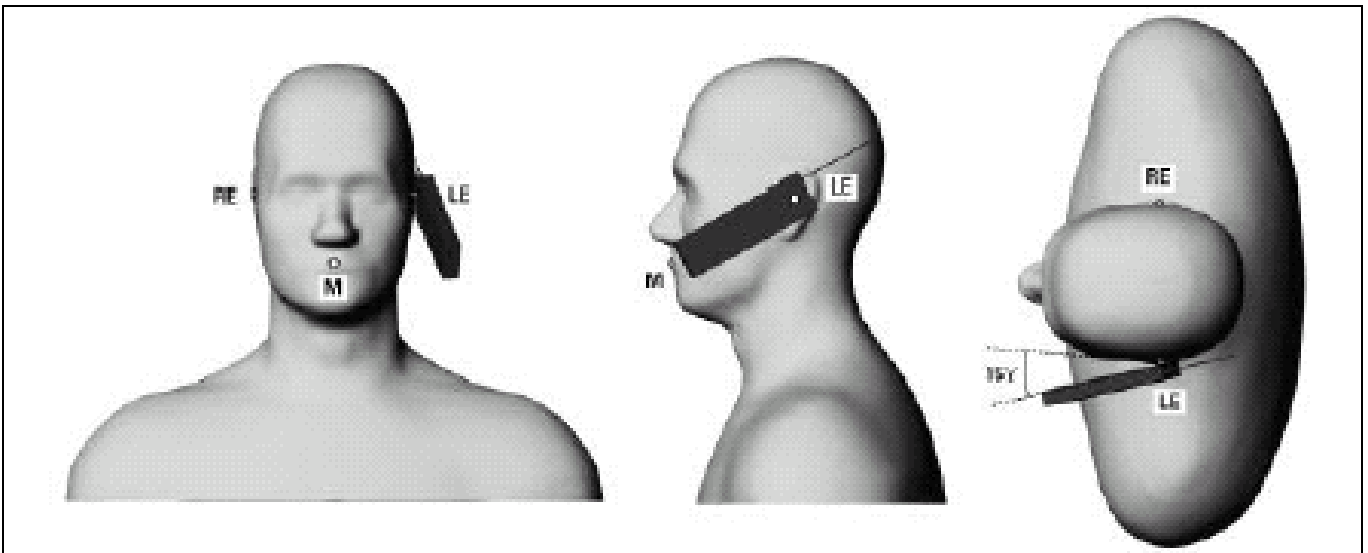


Fig. 9.2 Phone Position 2, “Tilted Position”. The reference point for the right ear (RE), left ear (LE) and mouth (M), which define the plane for phone positioning, are indicated.

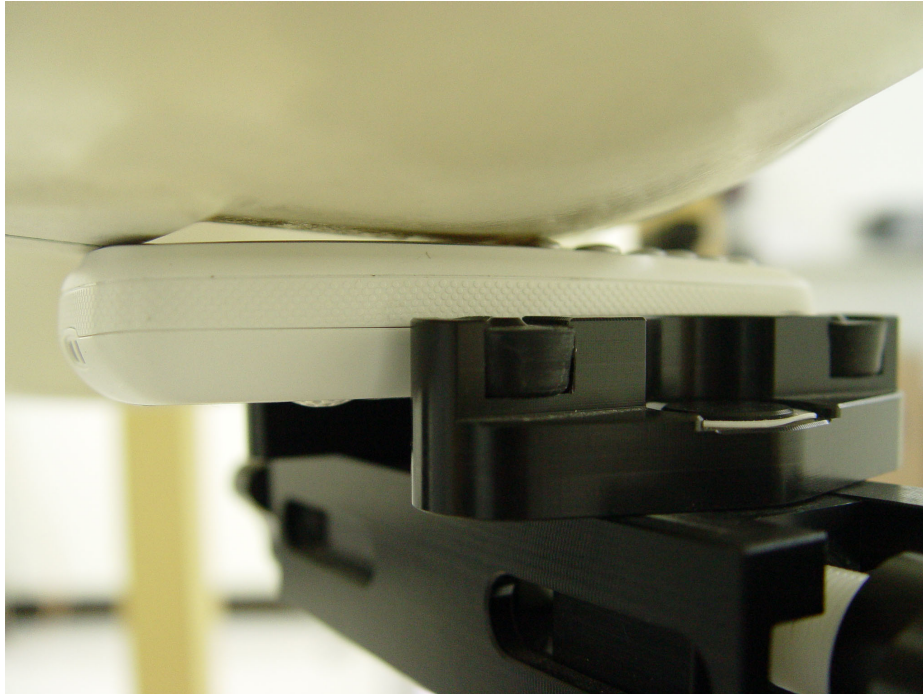


Fig. 9.3 Right Check

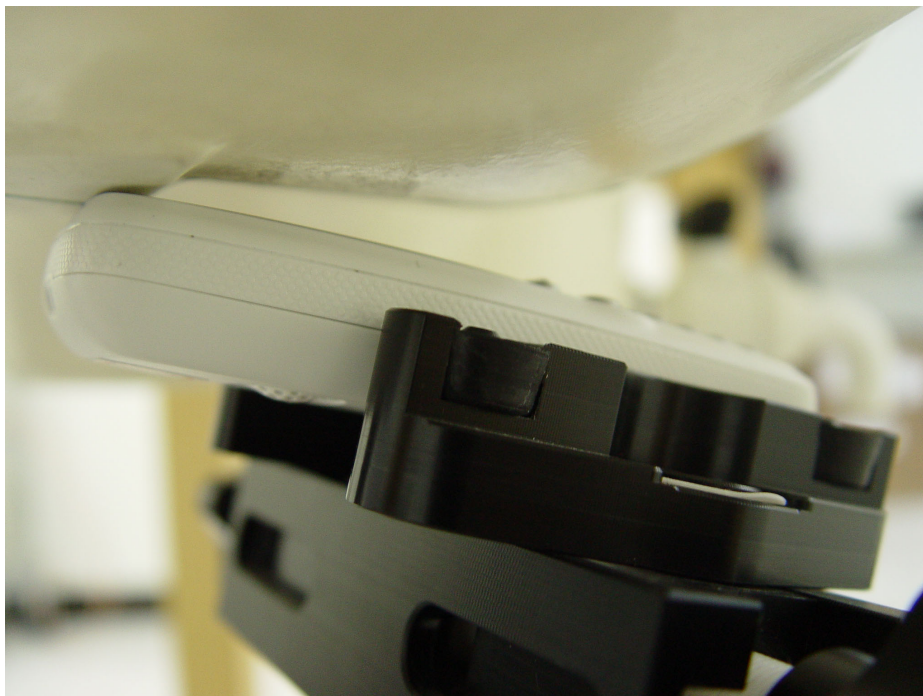


Fig. 9.4 Right Tilted

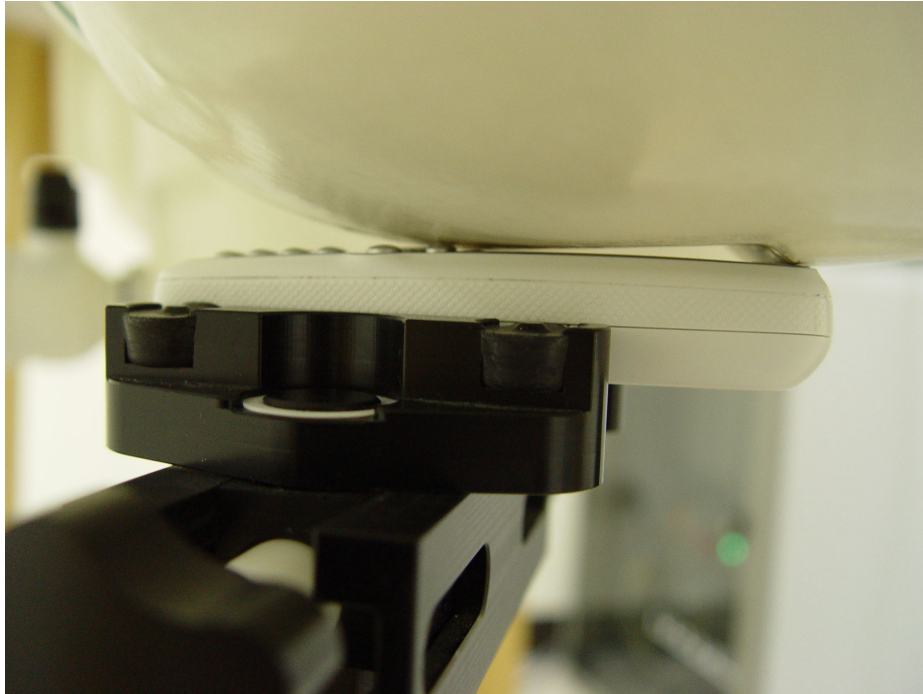


Fig. 9.5 Left Cheek

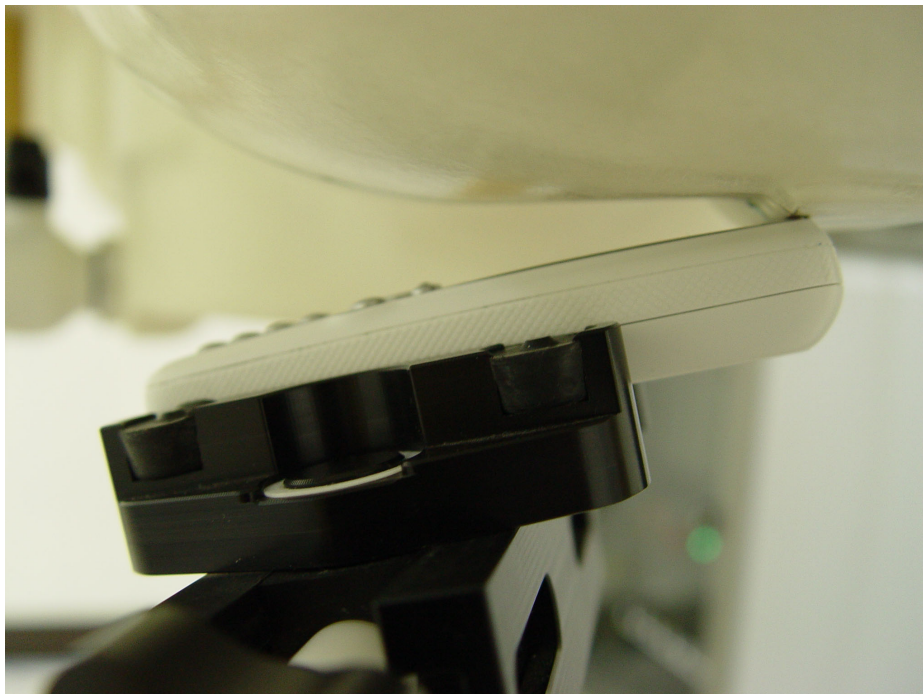


Fig. 9.6 Left Tilted