

SAR TEST REPORT

Test item	:	Mobile Phone
Model No.	;	KCMH01
Order No.	:	DEMC1303-00991
Date of receipt	:	2013-03-15
Test duration	:	2013-04-08
Date of issue	:	2013-04-09
Use of report	:	FCC Original Grant

Applicant : KYOCERA Corporation 2-1-1 Kagahara, Tsuzuki-ku, Yokohama-Shi, Kanagawa 224-8502, Japan

Test laboratory : Digital EMC Co., Ltd. 683-3, Yubang-Dong, Cheoin-Gu, Yongin-Si, Gyeonggi-Do, 449-080, Korea

Test specification	:	§2.1093, FCC/OET E	Bulletin 65 Supplement C[July 2001]
Test environment	:	See appended test r	eport
Test result	:	🛛 Pass	🗌 Fail

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Test Report Version

Test Report No.	Date	Description
DRTFCC1304-0338	Apr. 09, 2013	Final version for approval

1. DESCRIPTION OF DEVICE

Environmental evaluation measurements of specific absorption rate (SAR) distributions in emulated human head and body tissues exposed to radio frequency (RF) radiation from wireless portable devices for compliance with the rules and regulations of the U.S. Federal Communications Commission (FCC).

General Information

Equipment type	Mobile Phone						
FCC ID	JOYKCMH01						
Equipment model name	KCMH01						
Equipment add model name	N/A						
Equipment serial no.	Identical prototype						
Mode(s) of Operation	CDMA Cellular						
TX Frequency Range	824.70 ~ 848.31 MHz (CDMA Cellular)						
RX Frequency Range	869.70 ~ 893.31 MHz (CDMA Cellular)						
_		Measured	S	AR			
Equipment Class	Band & Mode	Conducted	1g SAI	g SAR (W/kg)			
		Power [dBm]	Head	Body-worn			
PCE	Cell. CDMA	21.48	1.19	0.46			
DSS	Bluetooth -3.206 -						
		0.200		s SAR per KDB 690783 D01v01r02 - 0.47			
	s SAR per KDB 690783 D01v(-	0.47			
	s SAR per KDB 690783 D01v0 Licensed Portable Transmi	01r02	-	0.47			
Simultaneou	-	01r02	-	0.47			
Simultaneous FCC Equipment Class	Licensed Portable Transmi	01r02	-	0.47			

1.1 Guidance Applied

- FCC OET Bullentin 65 Supplement C [June 2001]
- IEEE 1528-2003
- FCC KDB Publication 941225 D01-D06 (2G/3G and Hotspot)
- FCC KDB Publication 447498 D01 v05 (General SAR Guidance)
- FCC KDB Publication 865664 D01-D02 (SAR Measurements up to 6 GHz)
- October 2012 TCB Workshop Notes (1x Advanced)

1.2 Device Overview

Band & Mode	Operating Modes	Tx Frequency
Cell. CDMA	Voice/Data	824.70 ~ 848.31 MHz
Bluetooth	Data	2402 ~ 2480 MHz

1.3 Nominal and Maximum Output Power Specifications

This device operates using the following maximum and nominal output power specifications. SAR values were scaled to the maximum allowed power to determine compliance per KDB Publication 447498 D01v05.

Mode / Band		Modulated Average [dBm]
Cell. CDMA	Maximum	22.5
Cell. CDMA	Nominal	21.5
Mode / Band		
Мо	de / Band	Modulated Average [dBm]
Bluetooth	de / Band Maximum	Modulated Average [dBm] -2.20

1.4 DUT Antenna Locations & SAR Test Configurations

DUT Antenna Locations (Front Side View)

	Bluetooth antenna	
-		
	Front	
5	5 mm	
-		
	<u> </u>	/

Note: Specific antenna dimensions and separation distances are shown in the antenna distance document.

1.5 SAR Test Exclusions Applied

(A) Bluetooth

Per FCC KDB 447498 D01v05, **Bluetooth SAR was not required** based on the maximum conducted power and the Bluetooth antenna to user separation distance.

Per FCC KDB 447498 D01v05, the SAR exclusion threshold for distances < 50 mm is defined by the following equation:

 $\frac{Max Power of Channel (mW)}{Test Separation Dist (mm)} * \sqrt{Frequency(GHz)} \le 3.0$

Based on the maximum conducted power of Bluetooth and the antenna to use separation distance, Bluetooth SAR was not required; $(0.603 / 15) * \sqrt{2.402} = 0.1 < 3.0$.

1.6 Device Serial Numbers

Band & Mode	Serial Number
Cell. CDMA	SAR #1

2. INTROCUCTION

The FCC and Industry Canada have adopted the guidelines for evaluating the environmental effects of radio frequency (RF) radiation in ET Docket 93-62 on Aug. 6, 1996 and Health Canada Safety Code 6 to protect the public and workers from the potential hazards of RF emissions due to FCC-regulated portable devices.

The FCC has adopted the guidelines for evaluating the environmental effects of radio frequency radiation in ET Docket 93-62 on Aug. 6, 1996 to protect the public and workers from the potential hazards of RF emissions due to FCC-regulated portable devices. The safety limits used for the environmental evaluation measurements are based on the criteria published by the American National Standards Institute (ANSI) for localized specific absorption rate (SAR) in IEEE/ANSI C95*.1-2005 Standard for Safety Levels with Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 3 kHz to 300 GHz. 1992 by the Institute of Electrical and Electronics Engineers, Inc., New York, New York 10017. The measurement procedure described in IEEE/ANSI C95.3-1992 Recommended Practice for the Measurement of Potentially Hazardous Electromagnetic Fields - RF and Microwave is used for guidance in measuring SAR due to the RF radiation exposure from the Equipment Under Test (EUT). These criteria for SAR evaluation are similar to those recommended by the National Council on Radiation Protection and Measurements (NCRP) in Biological Effects and Exposure Criteria for Radio frequency Electromagnetic Fields," NCRP Report No. 86 NCRP, 1986, Bethesda, MD 20814. SAR is a measure of the rate of energy absorption due to exposure to an RF transmitting source. SAR values have been related to threshold levels for potential biological hazards.

SAR Definition

Specific Absorption Rate (SAR) is defined as the time derivative (rate) of the incremental energy (dU)absorbed by (dissipated in) an incremental mass (dm) contained in a volume element (dV) of a given density (p) It is also defined as the rate of RF energy absorption per unit mass at a point in an absorbing body (see Fig. 1.1)

$$SAR = \frac{d}{dt} \left(\frac{dU}{dm} \right) = \frac{d}{dt} \left(\frac{dU}{\rho dv} \right)$$

Fig. 1.1 SAR Mathematical Equation

SAR is expressed in units of Watts per Kilogram (W/kg).

$$SAR = \frac{\sigma \cdot E^2}{\rho}$$

where:

 σ = conductivity of the tissue-simulating material (S/m)

- ρ = mass density of the tissue-simulating material (kg/m³)
- E = Total RMS electric field strength (V/m)

NOTE: The primary factors that control rate of energy absorption were found to be the wavelength of the incident field in relations to the dimensions and geometry of the irradiated organism, the orientation of the organism in relation to the polarity of field vectors, the presence of reflecting surfaces, and whether conductive contact is made by the organism with a ground plane.

3. DESCRIPTION OF TEST EQUIPMENT

3.1 SAR MEASUREMENT SETUP

Measurements are performed using the DASY4 automated dosimetric assessment system. The DASY4 is made by Schmid & Partner Engineering AG (SPEAG) in Zurich, Switzerland and consists of high precision robotics system (Staubli), robot controller, desktop computer, near-field probe, probe alignment sensor, and the generic twin phantom containing the brain equivalent material. The robot is a six-axis industrial robot performing precise movements to position the probe to the location (points) of maximum electromagnetic field (EMF) (see Fig. 3.1).

A cell controller system contains the power supply, robot controller teach pendant (Joystick), and a remote control used to drive the robot motors. The PC consists of the Intel Core i5-2500 3.31GHz desktop computer with Windows NT system and SAR Measurement Software DASY4,, A/D interface card, monitor, mouse, and keyboard. The Staubli Robot is connected to the cell controller to allow software manipulation of the robot. A data acquisition electronic (DAE) circuit that performs the signal amplification, signal multiplexing, AD-conversion, offset measurements, mechanical surface detection, collision detection, etc. is connected to the Electro-optical coupler (EOC). The EOC performs the conversion from the optical into digital electric signal of the DAE and transfers data to the PC plug-in card.

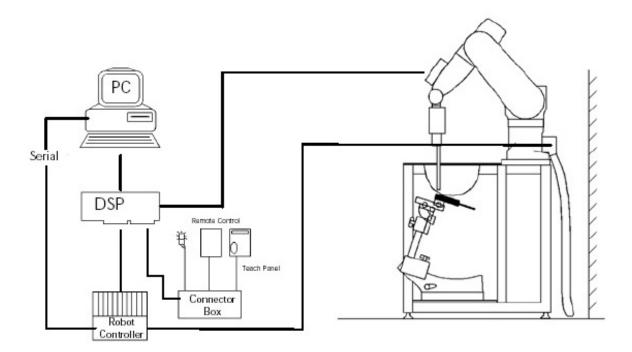


Figure 3.1 SAR Measurement System Setup

The DAE3 consists of a highly sensitive electrometer-grade preamplifier with auto-zeroing, a channel and gainswitching multiplexer, a fast 16 bit AD-converter and a command decoder and control logic unit. Transmission to the PC-card is accomplished through an optical downlink for data and status information and an optical uplink for commands and clock lines. The mechanical probe mounting device includes two different sensor systems for frontal and sidewise probe contacts. They are also used for mechanical surface detection and probe collision detection. The robot uses its own controller with a built in VME-bus computer. The system is described in detail.

3.2 EX3DV4 Probe Specification

CalibrationIn air from 10 MHz to 6 GHzIn brain and muscle simulating tissue at Frequencies of450 MHz, 750 MHz, 835 MHz, 900 MHz, 1750 MHz, 1900 MHz, 2300 MHz, 2450 MHz2600 MHz, 3500 MHz, 5200 MHz, 5300 MHz, 5500 MHz, 5600 MHz, 5800 MHz

Frequency	10 MHz to 6 GHz
-----------	-----------------

- Linearity± 0.2 dB(30 MHz to 6 GHz)
- **Dynamic** $5 \mu W/g \text{ to } > 100 \text{ mW/g}$

RangeLinearity :± 0.2 dB

Dimensions Overall length : 330 mm

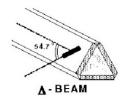
Tip length 20 mm

Body diameter 12 mm

Tip diameter 2.5 mm

Distance from probe tip to sensor center 1.0 mm

ApplicationSAR Dosimetry Testing
Compliance tests of mobile phones



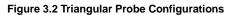




Figure 3.3 Probe Thick-Film Technique



DAE System

The SAR measurements were conducted with the dosimetric probe EX3DV4, designed in the classical triangular configuration (see Fig. 3.2) and optimized for dosimetric evaluation. The probe is constructed using the thick film technique; with printed resistive lines on ceramic substrates. The probe is equipped with an optical multi fiber line ending at the front of the probe tip (see Fig. 3.3). It is connected to the EOC box on the robot arm and provides an automatic detection of the phantom surface. Half of the fibers are connected to a pulsed infrared transmitter, the other half to a synchronized receiver. As the probe approaches the surface, the reflection from the surface produces a coupling from the transmitting to the receiving fibers. This reflection increases first during the approach, reaches maximum and then decreases. If the probe is flatly touching the surface, the coupling is zero. The distance of the coupling maximum to the surface is independent of the surface reflectivity and largely independent of the surface to probe angle. The DASY software reads the reflection during a software approach and looks for the maximum using a 2nd order fitting. The approach is stopped at reaching the maximum.

3.3 Probe Calibration Process

3.3.1 E-Probe Calibration

Dosimetric Assessment Procedure

Each probe is calibrated according to a dosimetric assessment procedure with accuracy better than +/- 10%. The spherical isotropy was evaluated with the procedure and found to be better than +/-0.25dB. The sensitivity parameters (NormX, NormY, NormZ), the diode compression parameter (DCP) and the conversion factor (ConvF) of the probe is tested.

Free Space Assessment

The free space E-field from amplified probe outputs is determined in a test chamber. This is performed in a TEM cell for frequencies below 1 GHz, and in a waveguide above 1GHz for free space. For the free space calibration, the probe is placed in the volumetric center of the cavity at the proper orientation with the field. The probe is then rotated 360 degrees.

Temperature Assessment *

E-field temperature correlation calibration is performed in a flat phantom filled with the appropriate simulated brain tissue. The measured free space E-field in the medium, correlates to temperature rise in a dielectric medium. For temperature correlation calibration a RF transparent the rmist or based temperature probe is used in conjunction with the E-field probe.

$$SAR = C \frac{\Delta T}{\Delta t}$$

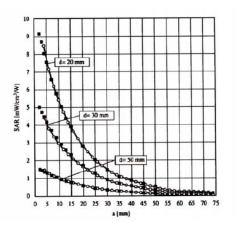
where:

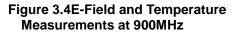
 Δt = exposure time (30 seconds),

C = heat capacity of tissue (brain or muscle),

 ΔT = temperature increase due to RF exposure.

SAR is proportional to $\Delta T / \Delta t$, the initial rate of tissue heating, before thermal diffusion takes place. Now it's possible to quantify the electric field in the simulated tissue by equating the thermally derived SAR to the E- field;





$$\mathsf{SAR} = \frac{\left|\mathsf{E}\right|^2 \cdot \sigma}{\rho}$$

where:

 σ = simulated tissue conductivity,

 ρ = **Tissue** density (1.25 g/cm³ for brain tissue)

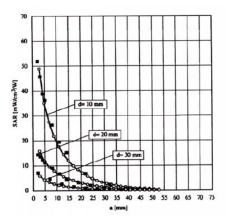


Figure 3.5 E-Field and Temperature Measurements at 1800MHz

3.4 Data Extrapolation

The DASY software automatically executes the following procedures to calculate the field units from the microvolt readings at the probe connector. The first step of the evaluation is a linearization of the filtered input signal to account for the compression characteristics of the detector diode. The compensation depends on the input signal, the diode type and the DC-transmission factor from the diode to the evaluation electronics. If the exciting field is pulsed, the crest factor of the signal must be known to correctly compensate for peak power. The formula for each channel can be given like below;

$$V_{i} = U_{i} + U_{i}^{2} \cdot \frac{cf}{dcp_{i}}$$
with V_{i} = compensated signal of channel i (i=x,y,z)
 U_{i} = input signal of channel i (i=x,y,z)
 cf = crest factor of exciting field (DASY parameter)
 dcp_{i} = diode compression point (DASY parameter)

From the compensated input signals the primary field data for each channel can be evaluated:

E-field probes:	with	V _i Norm _i	 = compensated signal of channel i (i = x,y,z) = sensor sensitivity of channel i (i = x,y,z)
$E_i = \sqrt{\frac{V_i}{Norm_i \cdot ConvF}}$		ConvF E _i	μV/(V/m) ² for E-field probes = sensitivity of enhancement in solution = electric field strength of channel i in V/m

The RSS value of the field components gives the total field strength (Hermetian magnitude):

$$E_{tot} = \sqrt{E_x^2 + E_y^2 + E_z^2}$$

The primary field data are used to calculate the derived field units.

$SAR = E_{tot}^2 \cdot \frac{\sigma}{\rho \cdot 1000}$	with	SAR Ε _{τοτ} σ	 = local specific absorption rate in W/g = total field strength in V/m = conductivity in [mho/m] or [Siemens/m] = equivalent tissue density in g/cm³
		Ρ	= equivalent tissue density in grein

The power flow density is calculated assuming the excitation field to be a free space field.

$$P_{pure} = \frac{E_{tot}^{2}}{3770}$$
 with P_{pwe} = equivalent power density of a plane wave in W/cm²
= total electric field strength in V/m

3.5 SAM Twin PHANTOM

The SAM Twin Phantom V4.0 is constructed of a fiberglass shell integrated in a wooden table. The shape of the shell is based on data from an anatomical study designed to determine the maximum exposure in at least 90% of all users. It enables the dosimetric evaluation of left and right hand phone usage as well as body mounted usage at the flat phantom region. A cover prevents the evaporation of the liquid.

Reference markings on the Phantom allow the complete setup of all predefined phantom positions and measurement grids by manually teaching three points in the robot. (see Fig. 3.6)

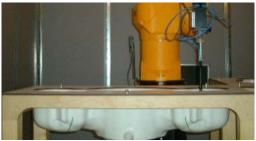


Figure 3.6 SAM Twin Phantom

SAM Twin Phantom Specification

Construction	 The shell corresponds to the specifications of the Specific Anthropomorphic Mannequin (SAM) phantom defined in IEEE 1528 and IEC 62209. It enables the dosimetric evaluation of left and right hand phone usage as well as body mounted usage at the flat phantom region. A cover prevents evaporation of the liquid. Reference markings on the phantom allow the complete setup of all predefined phantom positions and measurement grids by teaching three points with the robot. Twin SAM V5.0 has the same shell geometry and is manufactured from the same material as Twin SAM V4.0, but has reinforced top structure.
Shell Thickness	2 ± 0.2 mm
Filling Volume	Approx. 25 liters
Dimensions	Length: 1000 mm
	Width: 500 mm
	Height: adjustable feet

3.6Device Holder for Transmitters

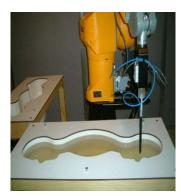
In combination with the Twin SAM Phantom V4.0/V4.0c or ELI4, the Mounting Device enables the rotation of the mounted transmitter device in spherical coordinates. Rotation point is the ear opening point. Transmitter devices can be easily and accurately positioned according to IEC, IEEE, FCC or other specifications. The device holder can be locked for positioning at different phantom sections (left head, right head, flat).

Note: A simulating human hand is not used due to the complex anatomical and geometrical structure of the hand that may produce infinite number of configurations. To produce the worst-case condition (the hand absorbs antenna output power), the hand is omitted during the tests.



Figure 3.7 Mounting Device

3.7 Brain & Muscle Simulation Mixture Characterization



The brain and muscle mixtures consist of a viscous gel using hydrox-ethyl cellulose (HEC) gelling agent and saline solution (see Table 3.1). Preservation with a bactericide is added and visual inspection is made to make sure air bubbles are not trapped during the mixing process. The mixture is calibrated to obtain proper dielectric constant (permittivity) and conductivity of the desired tissue. The mixture characterizations used for the brain and muscle tissue simulating liquids are according to the data by C. Gabriel and G. Harts grove.

Figure 3.8 SimulatedTissue

		SIMULATING TISSUE									
INGREDIE	NTS	835 MHz Brain	835 MHz Muscle	1900 MHz Brain	1900 MHz Muscle	2450 MHz Brain	2450 MHz Muscle	5200 ~ 5800 MHz Brain	5200 ~ 5800 MHz Muscle		
	Mixture Percentage										
WATER	२	40.19	50.75	55.24	70.23	71.88	73.40	65.52	80.00		
DGBE		-	-	44.45	29.48	7.990	26.54	-	-		
SUGAF	२	57.90	48.21	-	-	-	-	-	-		
SALT		1.480	0.940	0.310	0.290	0.160	0.060	-	-		
BACTERIC	CIDE	0.180	0.100	-	-	-	-	-	-		
HEC		0.250	-	-	-	-	-	-	-		
Triton X-1	00	-	-	-	-	19.97	-	17.24	-		
Diethylengl monohexyle		-	-	-	-	-	-	17.24	-		
Polysorbate(Tw	/een) 80	-	-	-	-	-	-	-	20.00		
Dielectric Constant	Target	41.5	55.2	40.0	53.3	39.2	52.7	-	-		
Conductivity (S/m)	Target	0.90	0.97	1.40	1.52	1.80	1.95	-	-		

Table3.1 Composition of the Tissue Equivalent Matter

Salt: 99 % Pure Sodium Chloride Sugar: 98 % Pure Sucrose

Water: De-ionized, 16M resistivity HEC: Hydroxyethyl Cellulose

DGBE: 99 % Di(ethylene glycol) butyl ether,[2-(2-butoxyethoxy) ethanol]

Triton X-100(ultra pure): Polyethylene glycol mono[4-(1,1,3,3-tetramethylbutyl)phenyl]

Test Faultum and Calibratian

3.8 SAR TEST EQUIPMENT

	Table 3.2 Test Equipment Calibration											
	Туре	Manufacturer	Model	Cal.Date	Next.Cal.Date	S/N						
\boxtimes	SEMITEC Engineering	SEMITEC	N/A	N/A	N/A	Shield Room						
\boxtimes	Robot	SCHMID	RX90BL	N/A	N/A	F02/5Q85A1/A/01						
\boxtimes	Robot Controller	SCHMID	CS7MB	N/A	N/A	F02/5Q85A1/C/01						
\boxtimes	Joystick	SCHMID	N/A	N/A	N/A	D221340031						
\boxtimes	Intel Core i5-2500 3,31 GHz Windows XP Professional	N/A	N/A	N/A	N/A	N/A						
\boxtimes	Probe Alignment Unit LB	N/A	N/A	N/A	N/A	SE UKS 030 AA						
\boxtimes	Mounting Device	SCHMID	SD000H01HA	N/A	N/A	N/A						
\boxtimes	Twin SAM Phantom	SCHMID	TP1223	N/A	N/A	N/A						
\boxtimes	Twin SAM Phantom	SCHMID	TP1224	N/A	N/A	N/A						
	Twin SAM Phantom	SCHMID	QD000P40CD	N/A	N/A	1679						
	Head/Body Equivalent Matter(835MHz)	N/A	N/A	2013-01-01	2014-01-01	N/A						
\boxtimes	Head/Body Equivalent Matter(1900MHz)	N/A	N/A	2013-01-01	2014-01-01	N/A						
\boxtimes	Head/Body Equivalent Matter(2450MHz)	N/A	N/A	2013-01-01	2014-01-01	N/A						
	Head/Body Equivalent Matter(5000MHz)	N/A	N/A	2013-01-01	2014-01-01	N/A						
\boxtimes	Data Acquisition Electronics	SCHMID	DAE3V1	2013-01-23	2014-01-23	519						
\boxtimes	Dosimetric E-Field Probe	SCHMID	EX3DV4	2013-01-24	2014-01-24	3643						
	Dummy Probe	N/A	N/A	N/A	N/A	N/A						
\boxtimes	835MHz SAR Dipole	SCHMID	D835V2	2012-03-14	2014-03-14	464						
	1900MHz SAR Dipole	SCHMID	D1900V2	2012-03-16	2014-03-16	5d029						
	2450MHz SAR Dipole	SCHMID	D2450V2	2012-03-15	2014-03-15	726						
	5000MHz SAR Dipole	SCHMID	D5GHzV2	2012-01-20	2014-01-20	1103						
\boxtimes	Network Analyzer	Agilent	E5071C	2012-11-02	2013-11-02	MY46106970						
\boxtimes	Signal Generator	Rohde Schwarz	SMR20	2013-02-27	2014-02-27	101251						
\boxtimes	Amplifier	EMPOWER	BBS3Q7ELU	2012-09-18	2013-09-18	1020						
\boxtimes	High Power RF Amplifier	EMPOWER	BBS3Q8CCJ	2012-11-02	2013-11-02	1005						
\boxtimes	Power Meter	HP	EPM-442A	2013-02-28	2014-02-28	GB37170267						
\boxtimes	Power Sensor	HP	8481A	2013-02-28	2014-02-28	3318A96566						
\boxtimes	Power Sensor	HP	8481A	2013-02-14	2014-02-14	3318A96030						
\boxtimes	Dual Directional Coupler	Agilent	778D-012	2013-01-08	2014-01-08	50228						
	Directional Coupler	HP	773D	2012-07-01	2013-07-01	2389A00640						
\boxtimes	Low Pass Filter 1,5 GHz	Micro LAB	LA-15N	2013-01-08	2014-01-08	N/A						
	Low Pass Filter 3,0 GHz	Micro LAB	LA-30N	2012-09-17	2013-09-17	N/A						
\boxtimes	Attenuators(3 dB)	Agilent	8491B	2012-07-02	2013-07-02	MY39260700						
\boxtimes	Attenuators(10 dB)	WEINSCHEL	23-10-34	2013-01-08	2014-01-08	BP4387						
	Step Attenuator	HP	8494A	2012-09-17	2013-09-17	3308A33341						
\boxtimes	Dielectric Probe kit	SCHMID	DAK-3.5	2012-04-03	2013-04-03	1046						
\boxtimes	8960 Series 10 Wireless Comms. Test Set	Agilent	E5515C	2013-02-28	2014-02-28	GB43461134						

NOTE: The E-field probe was calibrated by SPEAG, by temperature measurement procedure. Dipole Verification measurement is performed by Digital EMC before each test. The brain and muscle simulating material are calibrated by Digital EMC using the dielectric probe system and network analyzer to determine the conductivity and permittivity (dielectric constant) of the brain-equivalent material.

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3.8.1 Extended Dipole Calibrations

Referring to FCC KDB 865664 D01 SAR measurement 100 MHz to 6 GHz v01, the dipole calibration interval can be extended to 3 years with justification. The dipoles are also not physically damaged, or repaired during the interval. The Justification data of dipole D835V2, SN: 464 can be found in Table 3.2.

Justification Procedure of Dipole Calibration

- 1. Setup a Network Analyzer (Agilent E5071C) and set the start frequency and stop frequency to Network Analyzer according to the dipole frequency, at least +/- 200 MHz around the calibration point.
- 2. Using calibration kit to perform Network Analyzer Open, Short and Load calibration.
- 3. Connect the dipole with the calibrated Network Analyzer.
- 4. Set the Network Analyzer frequency by the dipole calibration frequency. Monitor the return-loss and impedance results with Log Magnitude format and Smith Chart, respectively.
- 5. Record the result and compare with the prior calibration.

Referring to FCC KDB 865664 D01 SAR measurement 100 MHz to 6 GHz v01, if dipoles are verified in return loss (< -20 dB, within 20 % of prior calibration), and in impedance (with 5 ohm of prior calibration), the annual calibration is not necessary and the calibration interval can be extended.

	D835V2 – Serial No. 464											
	835 MHz Head							835 MHz Body				
Date of Measurement	Return- Loss (dB)	Delta (%)	Real Impedance (ohm)	Delta (ohm)	Imaginary Impedance (ohm)	Delta (ohm)	Return- Loss (dB)Delta (%)Real Impedance (ohm)Delta (ohm)Imaginary Impedance (ohm)Delta (ohm)					
2012-03-14 (Calibration)	-32.137		51.215		-2.1855		-25.168		46.469		-3.9863	
2013-03-14 (Measured)	-32.864	-2.26	51.758	-0.543	-2.2259	0.040	-25.295	-0.50	46.591	-0.122	-3.8298	-0.1565

Table 3.2 Justification of the extended calibration Result

4. TEST SYSTEM SPECIFICATIONS

Automated TEST SYSTEM SPECIFICATIONS

Positioner

Robot Repeatability No. of axis	Stäubli Unimation Corp. Robot Model: RX90BL 0.02 mm 6
Data Acquisition Electro	nic (DAE) System
Cell Controller	
Processor Clock Speed	Intel Core i5-2500 3.31 GHz
Operating System	Windows XP Professional
Data Card	DASY4 PC-Board
Data Converter	
Features	Signal, multiplexer, A/D converter. & control logic
Software	DASY4
Connecting Lines	Optical downlink for data and status info
	Optical uplink for commands and clock
PC Interface Card	
Function	24 bit (64 MHz) DSP for real time processing
	Link to DAE 3
	16 bit A/D converter for surface detection system
	serial link to robot
	direct emergency stop output for robot
E-Field Probes	
Model	EX3DV4 S/N: 3643
Construction	Triangular core fiber optic detection system
Frequency	10 MHz to 6 GHz
Linearity	± 0.2 dB (30 MHz to 6 GHz)
Phantom	
Phantom	SAM Twin Phantom (V4.0)
Shell Material	Composite
Thickness	2.0 ± 0.2 mm

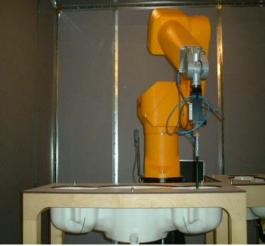
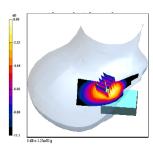


Figure 2.2 DASY4 Test System

5. SAR MEASUREMENT PROCEDURE

The evaluation was performed using the following procedure:

- 1. The SAR distribution at the exposed side of the head or body was measured at a distance no greater than 5.0 mm from the inner surface of the shell. The area covered the entire dimension of the device-head and body interface and the horizontal grid resolution was determined per FCC KDB Publication 865664 D01v01.
- 2. The point SAR measurement was taken at the maximum SAR region determined from Step 1 to enable the monitoring of SAR fluctuations/drifts during the 1g/10g cube evaluation. SAR at this fixed point was measured and used as a reference value.



Sample SAR Area Scan

- 3. Based on the area scan data, the peak of the region with maximum SAR was determined by spline interpolation. Around this point, a volume was assessed according to the measurement resolution and volume size requirements of FCC KDB Publication 865664 D01v01 (See Table 5.1). On the basis of this data set, the spatial peak SAR value was evaluated with the following procedure (see references or the DASY manual online for more details):
 - a. The data was extrapolated to the surface of the outer-shell of the phantom. The combined distance extrapolated was the combined distance from the center of the dipoles 2.7mm away from the tip of the probe housing plus the 1.2 mm distance between the surface and the lowest measuring point. The extrapolation was based on a least-squares algorithm. A polynomial of the fourth order was calculated through the points in the z-axis (normal to the phantom shell).
 - b. After the maximum interpolated values were calculated between the points in the cube, the SAR was averaged over the spatial volume (1g or 10g) using a 3D-Spline interpolation algorithm. The 3D-spline is composed of three one-dimensional splines with the "Not a knot" condition (in x, y, and z directions). The volume was then integrated with the trapezoidal algorithm. One thousand points (10 x 10 x 10) were obtained through interpolation, in order to calculate the averaged SAR.
 - c. All neighboring volumes were evaluated until no neighboring volume with a higher average value was found.
- 4. The SAR reference value, at the same location as step 2, was re-measured after the zoom scan was complete to calculate the SAR drift. If the drift deviated by more than 5%, the SAR test and drift measurements were repeated.

Frequency	Maximum Area Scan Resolution (mm) (Δx _{area} , Δy _{area})	Maximum Zoom Scan Resolution (mm) (Δx _{zoom} , Δy _{zoom})	Maximum Zoom Scan Spatial Resolution (mm) Δz _{zoom} (n)	Minimum Zoom Scan Volume (mm) (x,y,z)
≤2GHz	≤ 15	≤8	≤5	≥ 30
2-3 GHz	≤ 12	≤5	≤5	≥ 30
3-4 GHz	≤12	≤5	≤4	≥ 28
4-5 GHz	≤ 10	≤4	≤3	≥ 25
5-6 GHz	≤ 10	≤4	≤2	≥ 22

Table 5.1 Area and Zoom Scan Resolutions per FCC KDB Publication 865664 D01v01

Specific Anthropomorphic Mannequin (SAM) Specifications

The phantom for handset SAR assessment testing is a low-loss dielectric shell, with shape and dimensions derived from the anthropometric data of the 90th percentile adult male head dimensions as tabulated by the US Army. The SAM Twin Phantom shell is bisected along the mid-sagittal plane into right and left halves (see Fig. 5.1). The perimeter side walls of each phantom halves are extended to allow filling with liquid to a depth that is sufficient to minimized reflections from the upper surface. The liquid depth is maintained at a minimum depth of 15cm to minimize reflections from the upper surface.



Figure 5.1 Sam Twin Phantom shell

6. DESCRIPTION OF TEST POSITION

6.1 Ear Reference Point

Figure 6.1 shows the front, back and side views of the SAM Twin Phantom. The point "M" is the reference point for the center of the mouth, "LE" is the left ear reference point (ERP), and "RE" is the right ERP. The ERPs are 15mm posterior to the entrance to the Ear canal (EEC) along the B-M line (Back-Mouth), as shown in Figure 6.5. The plane Passing, through the two ear canals and M is defined as the Reference Plane. The line N-F (Neck- Front) is perpendicular to the reference plane and passing through the RE (or LE) is called the Reference Pivoting Line (see Figure 6.2). Line B-M is perpendicular to the N-F line. Both N-F and B-M lines are marked on the external phantom shell to facilitate hand set positioning.

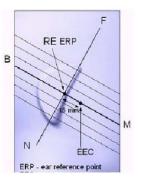


Figure 6.2 Close-up side view of ERP

6.2 Handset Reference Points

Two imaginary lines on the handset were established: the vertical centerline and the horizontal line. The test device was placed in a normal operating position with the "test device reference point" located along the "vertical centerline" on the front of the device aligned to the "ear reference point" (See Fig. 6.3). The "test device reference point" was than located at the same level as the center of the ear reference point. The test device was positioned so that the "vertical centerline" was bisecting the front surface of the handset at it's top and bottom edges, positioning the "ear reference point" on the outer surface of the both the left and right head phantoms on the ear reference point.



Figure 6.1 Front, back and side view SAM Twin Phantom

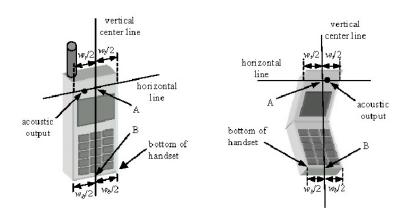


Figure 6.3 Handset Vertical Center & Horizontal Line Reference Points

6.3 Device Holder

The device holder is made out of low-loss POM material having the following dielectric parameters: relative permittivity ε = 3 and loss tangent δ = 0.02.

6.4 Positioning for Cheek/Touch

1. The test device was positioned with the handset close to the surface of the phantom such that point A is on the (virtual) extension of the line passing through points RE and LE on the phantom (see Figure 6.4), such that the plane defined by the vertical center line and the horizontal line of the phone is approximately parallel to the sagittal plane of the phantom.



Figure 6.4 Front. Side and Top View of Cheek/Touch Position

- 2. The handset was translated towards the phantom along the line passing through RE & LE until the handset touches the ear.
- 3. While maintaining the handset in this plane, the handset was rotated around the LE-RE line until the vertical centerline was in the plane normal to MB-NF including the line MB (reference plane).
- 4. The phone was hen rotated around the vertical centerline until the phone (horizontal line) was symmetrical was respect to the line NF.
- 5. While maintaining the vertical centerline in the reference plane, keeping point A on the line passing through RE and LE, and maintaining the phone contact with the ear, the handset was rotated about the line NF until any point on the handset made contact with a phantom point below the ear (cheek). (See Figure 6.5)

6.5 Positioning for Ear / 15 ° Tilt

With the test device aligned in the "Cheek/Touch Position":

- 1. While maintaining the orientation of the phone, the phone was retracted parallel to the reference plane far enough to enable a rotation of the phone by 15 degree.
- 2. The phone was then rotated around the horizontal line by 15 degree.
- 3. While maintaining the orientation of the phone, the phone was moved parallel to the reference plane until any part of the phone touches the head. (In this position, point A was located on the line RE-LE). The tilted position is obtained when the contact is on the pinna. If the contact was at any location other than the pinna, the angle of the phone would then be reduced. The tilted position was obtained when any part of the phone was in contact of the ear as well as a second part of the phone was in contact with the head (see Figure 6.6).



Figure 6.5Side view w/relevant markings

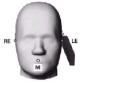




Figure 6.6 Front, Side and Top View of Ear/15°Position



Figure 6.7 Sample Body-Worn Diagram

6.6 Body-Worn Accessory Configurations

Body-worn operating configurations are tested with the belt-clips and holsters attached to the device and positioned against a flat phantom in a normal use configuration (see Figure 6.7). Per FCC KDB Publication 648474 D04_v01, Body-worn accessory exposure is typically related to voice mode operations when handsets are carried in body-worn accessories. The body-worn accessory procedures in FCC KDB Publication 447498 D01_v05 should be used to test for body-worn accessory SAR compliance, without a headset connected to it. This enables the test results for such configuration to be compatible with that required for hotspot mode when the body-worn accessory test separation distance is greater than or equal to that required for hotspot mode, when applicable. When the reported SAR for a body-worn accessory, measured without a headset connected to the handset, is > 1.2 W/kg, the highest reported SAR configuration for that wireless mode and frequency band should be repeated for that body-worn accessory with a headset attached to the handset.

Accessories for Body-worn operation configurations are divided into two categories: those that do not contain metallic components and those that do contain metallic components. When multiple accessories that do not contain metallic components are supplied with the device, the device is tested with only the accessory that dictates the closest spacing to the body. Then multiple accessories that contain metallic components are tested with the device with each accessory. If multiple accessories share an identical metallic component (i.e. the same metallic belt-clip used with different holsters with no other metallic components) only the accessory that dictates the closest spacing to the body is tested.

Body-worn accessories may not always be supplied or available as options for some devices intended to be authorized for body-worn use. In this case, a test configuration with a separation distance between the back of the device and the flat phantom is used. Test position spacing was documented.

Transmitters that are designed to operate in front of a person's face, as in push-to-talk configurations, are tested for SAR compliance with the front of the device positioned to face the flat phantom in head fluid. For devices that are carried next to the body such as a shoulder, waist or chest-worn transmitters, SAR compliance is tested with the accessories, including headsets and microphones, attached to the device and positioned against a flat phantom in a normal use configuration.

6.7 Wireless Router Configurations

Some battery-operated handsets have the capability to transmit and receive user data through simultaneous transmission of WIFI simultaneously with a separate licensed transmitter. The FCC has provided guidance in FCC KDB Publication 941225 D06 v01 where SAR test considerations for handsets (L x W \ge 9 cm x 5 cm) are based on a composite test separation distance of 10 mm from the front, back and edges of the device containing transmitting antennas within 2.5 cm of their edges, determined from general mixed use conditions for this type of devices. Since the hotspot SAR results may overlap with the body-worn accessory SAR requirements, the more conservative configurations can be considered, thus excluding some body-worn accessory SAR tests.

When the user enables the personal wireless router functions for the handset, actual operations include simultaneous transmission of both the WIFI transmitter and another licensed transmitter. Both transmitters often do not transmit at the same transmitting frequency and thus cannot be evaluated for SAR under actual use conditions due to the limitations of the SAR assessment probes. Therefore, SAR must be evaluated for each frequency transmission and mode separately and spatially summed with the WIFI transmitter according to FCC KDB Publication 447498 D01v05 publication procedures. The "Portable Hotspot" feature on the handset was NOT activated during SAR assessments, to ensure the SAR measurements were evaluated for a single transmission frequency RF signal at a time.

7. IEEE P1528 - MEASUREMENT UNCERTAINTIES

835 MHz Head

	Uncertaint	Probability	Divisor	(Ci)	Standard	vi 2 or
Error Description	value ±%	Distribution	DIVISOI	1g	(1g)	Veff
Measurement System						
Probe calibration	± 6.0	Normal	1	1	± 6.0 %	∞
Axial isotropy	± 4.7	Rectangular	√3	1	± 2.714 %	∞
Hemispherical isotropy	± 9.6	Rectangular	√3	1	± 5.543 %	∞
Boundary Effects	± 0.8	Rectangular	√3	1	± 0.462 %	∞
Probe Linearity	± 4.7	Rectangular	√3	1	± 2.714 %	∞
Detection limits	± 0.25	Rectangular	√3	1	± 0.144 %	∞
Readout Electronics	± 1.0	Normal	1	1	± 1.0 %	∞
Response time	± 0.8	Rectangular	√3	1	± 0.462 %	∞
Integration time	± 2.6	Rectangular	√3	1	± 1.501 %	∞
RF Ambient Conditions	± 3.0	Rectangular	√3	1	± 1.732 %	∞
Probe Positioner	± 0.4	Rectangular	√3	1	± 0.231 %	∞
Probe Positioning	± 2.9	Rectangular	√3	1	± 1.674 %	∞
Algorithms for Max. SAR Eval.	± 1.0	Rectangular	√3	1	± 0.577 %	∞
Test Sample Related						
Device Positioning	± 2.9	Normal	1	1	± 2.9 %	145
Device Holder	± 3.6	Normal	1	1	± 3.6 %	5
Power Drift	± 5.0	Rectangular	√3	1	± 2.887 %	8
Physical Parameters						
Phantom Shell	± 4.0	Rectangular	√3	1	± 2.309 %	×
Liquid conductivity (Target)	± 5.0	Rectangular	√3	0.64	± 2.887 %	×
Liquid conductivity (Meas.)	± 3.9	Normal	1	0.64	± 3.9 %	×
Liquid permittivity (Target)	± 5.0	Rectangular	√3	0.6	± 2.887 %	∞
Liquid permittivity (Meas.)	± 4.0	Normal	1	0.6	± 4.0 %	∞
CombinedStandard Uncertainty					± 12.0 %	330
Expanded Uncertainty (k=2)					± 24.0 %	

The above measurement uncertainties are according to IEEE P1528 (2003)

835 MHz Body

	Uncertaint	Probability	Divisor	(Ci)	Standard	vi 2 or
Error Description	value ±%	Distribution	Divisor	1g	(1g)	Veff
Measurement System						
Probe calibration	± 6.0	Normal	1	1	± 6.0 %	8
Axial isotropy	± 4.7	Rectangular	√3	1	± 2.714 %	8
Hemispherical isotropy	± 9.6	Rectangular	√3	1	± 5.543 %	8
Boundary Effects	± 0.8	Rectangular	√3	1	± 0.462 %	8
Probe Linearity	± 4.7	Rectangular	√3	1	± 2.714 %	8
Detection limits	± 0.25	Rectangular	√3	1	± 0.144 %	8
Readout Electronics	± 1.0	Normal	1	1	± 1.0 %	8
Response time	± 0.8	Rectangular	√3	1	± 0.462 %	8
Integration time	± 2.6	Rectangular	√3	1	± 1.501 %	8
RF Ambient Conditions	± 3.0	Rectangular	√3	1	± 1.732 %	8
Probe Positioner	± 0.4	Rectangular	√3	1	± 0.231 %	8
Probe Positioning	± 2.9	Rectangular	√3	1	± 1.674 %	∞
Algorithms for Max. SAR Eval.	± 1.0	Rectangular	√3	1	± 0.577 %	8
Test Sample Related						
Device Positioning	± 2.9	Normal	1	1	± 2.9 %	145
Device Holder	± 3.6	Normal	1	1	± 3.6 %	5
Power Drift	± 5.0	Rectangular	√3	1	± 2.887 %	×
Physical Parameters						
Phantom Shell	± 4.0	Rectangular	√3	1	± 2.309 %	∞
Liquid conductivity (Target)	± 5.0	Rectangular	√3	0.64	± 2.887 %	×
Liquid conductivity (Meas.)	± 4.1	Normal	1	0.64	± 4.1 %	∞
Liquid permittivity (Target)	± 5.0	Rectangular	√3	0.6	± 2.887 %	∞
Liquid permittivity (Meas.)	± 4.3	Normal	1	0.6	± 4.3 %	×
CombinedStandard Uncertainty					± 12.1 %	330
Expanded Uncertainty (k=2)					± 24.2 %	

The above measurement uncertainties are according to IEEE P1528 (2003)

8. ANSI / IEEE C95.1-2005 RF EXPOSURE LIMITS

Uncontrolled Environment

UNCONTROLLED ENVIRONMENTS are defined as locations where there is the exposure of individuals who have no knowledge or control of their exposure. The general population/uncontrolled exposure limits are applicable to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Members of the general public would come under this category when exposure is not employmentrelated; for example, in the case of a wireless transmitter that exposes persons in its vicinity.

Controlled Environment

CONTROLLED ENVIRONMENTS are defined as locations where there is exposure that may be incurred by persons who are aware of the potential for exposure, (i.e. as a result of employment or occupation). In general, occupational/controlled exposure limits are employment, which have been made fully aware of the potential for exposure and can exercise control over their exposure. This exposure category is also applicable when the exposure is of a transient nature due to incidental passage through a location where the exposure levels may be higher than the general population/uncontrolled limits, but the exposed person is fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Table 8.1.SAR Human Exposure Specified in ANSI/IEEE C95.1-2005

	HUMAN EXPOSURE LIMITS					
	General Public Exposure (W/kg) or (mW/g)	Occupational Exposure (W/kg) or (mW/g)				
SPATIAL PEAK SAR * (Brain)	1.60	8.00				
SPATIAL AVERAGE SAR ** (Whole Body)	0.08	0.40				
SPATIAL PEAK SAR *** (Hands / Feet / Ankle / Wrist)	4.00	20.0				

NOTES:

* The Spatial Peak value of the SAR averaged over any 1 g of tissue

(defined as a tissue volume in the shape of a cube) and over the appropriate averaging time.

** The Spatial Average value of the SAR averaged over the whole-body.

*** The Spatial Peak value of the SAR averaged over any 10 g of tissue

(defined as a tissue volume in the shape of a cube) and over the appropriate averaging time.

Uncontrolled Environments are defined as locations where there is the exposure of individuals who have no knowledge or control of their exposure.

Controlled Environments are defined as locations where there is exposure that may be incurred by persons who are aware of the potential for exposure, (i.e.as a result of employment or occupation).

9. SYSTEM VERIFICATION

9.1 Tissue Verification

	MEASURED TISSUE PARAMETERS													
Date(s)	Tissue Type	Ambient Temp.[°C]	Liquid Temp.[°C]	Measured Frequency [MHz]	Target Dielectric Constant, εr	Target Conductivity, σ (S/m)	Measured Dielectric Constant, εr	Measured Conductivity, σ (S/m)	εr Deviation [%]	σ Deviation [%]				
	835 24 2			824.7	41.549	0.899	42.000	0.868	1.09	-3.45				
Apr. 08, 2013			21.7	835.0	41.500	0.900	41.900	0.876	0.96	-2.67				
Api. 00, 2013	Head		21.7	836.52	41.500	0.902	41.900	0.877	0.96	-2.77				
				848.31	41.500	0.914	41.900	0.886	0.96	-3.06				
								824.7	55.240	0.969	53.200	0.949	-3.69	-2.06
Apr 08 2012	835	21.3	21.6	835.0	55.200	0.970	53.100	0.958	-3.80	-1.24				
Apr. 08, 2013 Boo	Body	Body 21.3		836.52	55.195	0.972	53.100	0.959	-3.80	-1.34				
				848.31	55.159	0.986	53.000	0.971	-3.91	-1.52				

Tissue Verification Note

Note: The above measured tissue parameters were used in the DASY software. The DASY software was used to perform interpolation to determine the dielectric parameters at the SAR test device frequencies (per IEEE 1528 6.6.1.2). The tissue parameters listed in the SAR test plots may slightly differ from the table above due to significant digit rounding in the software.

Measurement Procedure for Tissue verification

- 1) The network analyzer and probe system was configured and calibrated.
- The probe was immersed in the sample which was placed in a nonmetallic container. Trapped air bubbles beneath the flange were minimized by placing the probe at a slight angle.
- 3) The complex admittance with respect to the probe aperture was measured
- The complex relative permittivity , for example from the below equation (Pournaropoulos and Misra):

$$Y = \frac{j2\omega\varepsilon_r\varepsilon_0}{\left[\ln(b/a)\right]^2} \int_a^b \int_a^b \int_0^\pi \cos\phi' \frac{\exp\left[-j\omega r(\mu_0\varepsilon_r'\varepsilon_0)^{1/2}\right]}{r} d\phi' d\rho' d\rho$$

where Y is the admittance of the probe in contact with the sample, the primed and unprimed coordinates refer to source and observation points, respectively, $r^2 = \rho^2 + {\rho'}^2 - 2\rho\rho'\cos\phi'$, ω is the angular frequency, and $j = \sqrt{-1}$.

9.2 Test System Verification

Prior to assessment, the system is verified to the \pm 10 % of the specifications at 835 MHz by using the SAR dipole kit(s). (Graphic Plots Attached)

	SYSTEM DIPOLE VERIFICATION TARGET & MEASURED										
Freq. [MHz]	SAR Dipole Kit	Date(s)	Liquid	Ambient Temp.[°C]	Liquid Temp.[°C]	Probe S/N	Input Power (mW)	1 W Target SAR _{1g} (W/kg)	Measured SAR _{1g} (W/kg)	1 W Normalized SAR _{1g} (W/kg)	Deviation [%]
835	D835V2, SN:464	Apr. 08, 2013	Head	21.3	21.7	3643	250	9.40	2.32	9.28	-1.28
835	D835V2, SN:464	Apr. 08, 2013	Body	21.3	21.6	3643	250	9.53	2.48	9.92	4.09

Note1 : System verification was measured with input 250 mW and normalized to 1W.

Note2 : To confirm the proper SAR liquid depth, the z-axis plots from the system verifications were included since the system verifications were performed using the same liquid, probe and DAE as the SAR tests in the same time period.

Note3: Full system validation status and results can be found in Attachment 3.

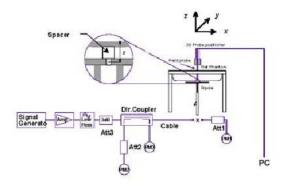




Figure 9.1 Dipole Verification Test Setup

10. FCC MULTI-TX AND ANTENNA SAR CONSIDERATIONS

10.1 Introduction

The following procedures adopted from FCC KDB Publication 447498 D01v05 are applicable to handsets with built-in unlicensed transmitters such as 802.11b/g/n and Bluetooth devices which may simultaneously transmit with the licensed transmitter.

10.2 Simultaneous Transmission Procedures

This device contains transmitters that may operate simultaneously. Therefore simultaneous transmission analysis is required. Per FCC KDB 447498 D01v05 IV.C.1.iii, simultaneous transmission SAR test exclusion may be applied when the sum of the 1-g SAR for all the simultaneous transmitting antennas in a specific a physical test configuration is \leq 1.6 W/kg. When standalone SAR is not required to be measured, per FCC KDB 447498 D01v05 4.3.2 2), the following equation must be used to estimate the standalone 1g SAR for simultaneous transmission assessment involving that transmitter.

Estimated SAR=
$$\frac{\sqrt{f(GHz)}}{7.5} * \frac{(Max Power of channel, mW)}{Min. Separation Distance, mm}$$

Mode	Frequency	Maximum Allowed Power		Separation Distance (Body)	Estimated SAR (Body)
	[MHz]	[dBm]	[mW]	[mm]	[W/kg]
Bluetooth	2402	-2.20	0.603	15	0.008

Table 10.1 Estimated SAR

Note1: Held-to ear configurations are not applicable to Bluetooth operations and therefore were not considered for simultaneous transmission.

10.3 Simultaneous Transmission Capabilities

Ref.		Head	Body-Worn Accessory								
	Simultaneous Transmit Configurations	IEEE1528, Supp C	Supplement C								
1	1x CDMA Voice + 2.4 GHz Bluetooth	N/A	Yes								
Notes: 1. EVDO does not support.											

10.5 Body-Worn Simultaneous Transmission Analysis

Configuration	Mode	2G/3G SAR (W/kg)	Bluetooth SAR (W/kg)	∑ SAR (W/kg)
Front Side		0.457	0.008	0.465
Rear Side	Cell. CDMA 0.444 0.008		0.008	0.452

Note: Bluetooth SAR was not required to be measured per FCC KDB 447498. Estimated SAR results were used in the above table to determine simultaneous transmission SAR test exclusion.

Simultaneous Transmission Conclusion

The above numerical summed SAR results for all the worst-case simultaneous transmission conditions were below the SAR limit. Therefore, the above analysis is sufficient to determine that simultaneous transmission cases will not exceed the SAR limit and therefore no measured volumetric simultaneous SAR summation is required per FCC KDB Publication 447498 D01_v05.

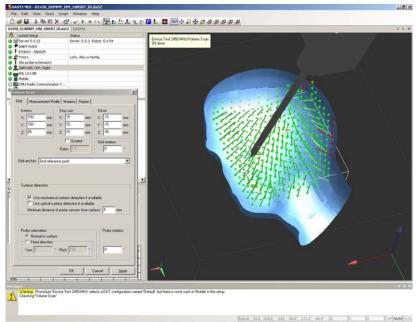
10.7 Description of Volume Scan

In order to determine the EM field distribution in a three-dimensional spatial extension, volume scans are required. In free space, these assessments can help to gain more information on the performance of the DUT (e.g., to determine the degree of symmetry of the filed radiated from a horn antenna).

For dosimetric application, it is necessary to assess the peak spatial SAR value averaged over a volume. For this purpose, fine resolution volume scans need to be performed at the peak SAR location(s) determined during the Area Scan. In DASY4 software these scans are called Zoom Scan jobs. The default Zoom Scan measures $7 \times 7 \times 7$ points with a step size of 5 mm. Faster evaluations can be achieved with a reduced number of measurement points. For example, a Zoom Scan with a grid step size in x- and y-directions of 7.5 mm (5 x 5 x 7cube configuration) reduces the measurement time to almost half with only 1-2% difference in SAR reading compared to the fine-resolution 7 x 7 x 7 scan.

For SAR evaluations with larger spatial extensions (e.g., within a complete phantom head section) a Volume Scan job should be used.

The Volume Scan job is compatible with DASY4 SAR, PRO and NEO system levels. Volume Scans are used to assess peak SAR and averaged SAR measurement in largely extended 3-dimensional volumes within any phantom. This measurement does not need any previous area scan. The grid can be anchored to a user specific point or to the current probe location With an Administrator access mode, the grid can be optionally graded in Z-direction, whereby the smallest grid step and the grading ratio can be defined. Chosen grading ratio is automatically adjusted so that the desired extent in Z-direction is fully covered.



Under the Report page, the quantity to be evaluated for an instant report may be selected. This quantity can be: field magnitude, SAR, interpolated SAR or averaged SAR.

10.8 SAR Assessment

Alternative1

- Evaluation Method
- Maximum summed SAR Value
- Description
 - Easiest and most conservative method to determine the upper limit of multi-band SAR
 - Example
 - F1's SAR Value is 0.9
 - F2's SAR Value is 1.3
 - Multi-band SAR Value is 0.9 + 1.3 = 2.2

Alternative2

- Evaluation Method
 - Selection of highest assessed maximum SAR Value
- Description
 - Accurate estimate of the multi-band SAR
 - Example
 - F1's SAR Value is 0.9
 - F2's SAR Value is 1.3
 - Multi-band SAR Value is 1.3

Alternative3

- Evaluation Method
- Combining existing Area and Zoom Scan results by Post-Processor
- Description
 - Rapid way of obtaining the multi-band SAR. It is always applicable.
 - Example
 - F1's SAR Value is 0.9
 - F2's SAR Value is 1.3
 - Combining results by Post-Processor

Alternative4

- Evaluation Method
 - Combining existing Area and Zoom Scan results by Post-Processor
- Description
 - The most accurate way of assessing the multi-band SAR and always applicable.
 - Example
 - F1's SAR Value is 0.9
 - F2's SAR Value is 1.3
 - Combining results by Post-Processor

MIMO Antenna System Design & Evaluation	
Alternative 1 Peak SAR	 Evaluation by summation of peak spatial-averaged SAR values
Alternative 2 Maximum SAR	Evaluation by selection of highest assessed maximum SAR values
Alternative 3 Volumetric SAR Calculation	Evaluation by calculated volumetric SAR data
Alternative 4 Volumetric Scanning	Evaluation by volumetric scanning
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11. FCC MEASUREMENT PROCEDURES

Power measurements were performed using a base station simulator under digital average power.

11.1 Measured and Reported SAR

Per FCC KDB Publication 447498 D01v05, When SAR is not measured at the maximum power level allowed for production units; the results must be scaled to the maximum tune-up tolerance limit according to the power applied to the individual channels tested to determine compliance. For simultaneous transmission, the measured aggregate SAR must be scaled according to the sum of the differences between the maximum tune-up tolerance and actual power used to test each transmitter. When SAR is measured at or scaled to the maximum tune-up tolerance limit, the results are referred to as *reported* SAR. The highest *reported* SAR results are identified on the grant of equipment authorization according to procedures in KDB 690783 D01v01r02.

11.2 Procedures Used to Establish RF Signal for SAR

The following procedures are according to FCC KDB Publication 941225 D01 "SAR Measurement Procedures for 3G Devices" v02, October 2007.

The device was placed into a simulated call using a base station simulator in a RF shielded chamber. Establishing connections in this manner ensure a consistent means for testing SAR and are recommended for evaluating SAR. Devices under test were evaluated prior to testing, with a fully charged battery and were configured to operate at maximum output power. In order to verify that the device was tested throughout the SAR test at maximum output power, the SAR measurement system measures a "point SAR" at an arbitrary reference point at the start and end of the 1 gram SAR evaluation, to assess for any power drifts during the evaluation. If the power drift deviated by more than 5%, the SAR test and drift measurements were repeated.

11.2.1 SAR Measurement Conditions for CDMA2000

The following procedures were performed according to FCC KDB Publication 941225 D01 "SAR Measurement Procedures for 3G Devices" v02, October 2007.

Output Power Verification

See 3GPP2 C.S0011/TIA-98-E as recommended by "SAR Measurement Procedures for 3G Devices" v02, October 2007. Maximum output power is verified on the High, Middle and Low channels according to procedures in section 4.4.5.2 of 3GPP2 C.S0011/TIA-98-E. SO55 tests were measured with power control bits in the "All Up" condition.

- 1. If the mobile station (MS) supports Reverse TCH RC 1 and Forward TCH RC 1, set up a call using Fundamental Channel Test Mode 1 (RC=1/1) with 9600 bps data rate only.
- 2. Under RC1, C.S0011 Table 4.4.5.2-1, Table 11-1 parameters were applied.
- 3. If the MS supports the RC 3 Reverse FCH, RC3 Reverse SCH0 and demodulation of RC 3, 4, or 5, set up a call using Supplemental Channel Test Mode 3 (RC 3/3) with 9600 bps Fundamental Channel and 9600 bps SCH0 data rate.
- 4. Under RC3, C.S0011 Table 4.4.5.2-2, Table 11-2 was applied.

Parameters for Max. Power for RC1

Parameter	Units	Value
lor	dBm/1.23 MHz	-104
$\frac{Pilot \ E_c}{I_{or}}$	dB	-7
Traffic E _c	dB	-7.4

Table 11-1

Parameters for Max. Power for RC3

Parameter	Units	Value
I _{or}	dBm/1.23 MHz	-86
Pilot E _c	dB	-7
Traffic E _c	dB	-7.4

Table 11-2

5. FCHs were configured at full rate for maximum SAR with "All Up" power control bits.

CDMA 2000 1x Advanced

This device additionally supports 1x Advanced. Conducted powers were measured using SO75 with RC8 on the uplink and RC11 on the downlink per Oct 2012 TCB Workshop notes. Smart blanking was disabled for all measurements. The EUT was configured with forward power control Mode 000 and reverse power control at 400 bps. Conducted powers were measured on an Agilent 8960 Series 10 Wireless Communications Test Set, Model E5515C using the CDMA2000 1x Advanced application, Option E1962B-410.

Based on the maximum output power measured for 1x Advanced, SAR is required for 1x advanced when if the maximum output for 1x Advanced is more than 0.25 dB higher than the maximum measured for 1x. Also, if the measured SAR in any 1x mode exposure conditions (head, body etc.) is larger than 1.2 W/kg, the highest of those configurations above 1.2 W/kg for each exposure condition in 1x Advanced has to be repeated. All measured SAR in 1x mode higher than 1.5 W/kg must be repeated for 1x Advanced.

Head SAR Measurements

SAR for head exposure configurations is measured in RC3 with the DUT configured to transmit at full rate using Loopback Service Option SO55. SAR for RC1 is not required when the maximum average output of each channel is less than ¼ dB higher than that measured in RC3. Otherwise, SAR is measured on the maximum output channel in RC1 using the exposure configuration that results in the highest SAR for that channel in RC3.

Body SAR Measurements

SAR for body exposure configurations is measured in RC3 with the DUT configured to transmit at full rate on FCH with all other code channels disabled using TDSO / SO32. SAR for multiple code channels (FCH + SCHn) is not required when the maximum average output of each RF channel is less than ¼ dB higher than that measured with FCH only. Otherwise, SAR is measured on the maximum output channel (FCH + SCHn) with FCH at full rate and SCH0 enabled at 9600 bps using the exposure configuration that results in the highest SAR for that channel with FCH only. When multiple code channels are enabled, the DUT output may shift by more than 0.5 dB and lead to higher SAR drifts and SCH dropouts. Body SAR was measured using TDSO / SO32 with power control bits in the "All Up".

Body SAR in RC1 is not required when the maximum average output of each channel is less than ¼ dB higher than that measured in RC3. Otherwise, SAR is measured on the maximum output channel in RC1; with Loopback Service Option SO55, at full rate, using the body exposure configuration that results in the highest SAR for that channel in RC3.

12. RF CONDUCTED POWERS

CDMA Conducted Powers

			Loopb	Data			
Band	Channel	Frequency SO55 [dBm]		SO55 [dBm]	SO75 [dBm]	TDSO SO32 [dBm]	TDSO SO32 [dBm]
	F-RC	MHz	RC1	RC3	RC8	FCH+SCH	FCH
	1013	824.70	21.44	21.48	^{Note2} N/A	21.38	21.41
Cellular	384	836.52	21.43	21.45	^{Note2} N/A	21.35	21.38
	777	848.31	21.31	21.37	Note2N/A	21.25	21.26

Table 12.1 The power was measured by E5515C

Note1: RC1 is only applicable for IS-95 compatibility.

Note2: This device does not support 1xAdvanced (SO75) and EVDO.

Per KDB Publication 941225 D01v02:

- 1. Head SAR was tested with SO55 RC3. SO55 RC1 was not required since the average output power was not more than 0.25 dB than the SO55 RC3 powers.
- Body-Worn SAR was tested with 1x RTT with TDSO / SO32 FCH Only. Ev-Do and TDSO / SO32 FCH+SCH SAR tests were not required since the average output power was not more than 0.25 dB higher than the TDSO / SO32 FCH only powers.

CDMA2000 Power Measurement Setup



Bluetooth Conducted Powers

Channel	Frequency	Output Pov	ver(1Mbps)	Output pow	ver (2Mbps)	Output power (3Mbps)		
Channel	(MHz)	(dBm)	(mW)	(dBm)	(mW)	(dBm)	(mW)	
Low	2402	-3.206	0.478	-4.802	0.331	-4.789	0.332	
Mid	2441	-3.706	0.426	-5.017	0.315	-5.003	0.316	
High	2480	-3.799	0.417	-5.058	0.312	-5.045	0.313	

Table 12.2 The power was measured by the Average Power Meter

Bluetooth Power Measurement Setup



13. SAR TEST RESULTS

13.1 Standalone Head SAR Results

	Table 13.1 CDMA Head SAR														
FREQU	-	Mode/ Band	Service	Maximum Allowed Power	Conducted Power	Drift Power	Phantom Position	Device Serial	Duty Cycle	1g SAR	Scaling Factor	1g Scaled SAR			
MHz	Ch	Danu					[dBm]	[dBm]	[dB]	POSITION	Number	Cycle	(W/kg)	Factor	(W/kg)
824.70	1013	Cell. CDMA	RC3/SO55	22.5	21.48	0.053	Left Touch	SAR#1	1:1	0.939	1.265	1.188			
836.52	384	Cell. CDMA	RC3/SO55	22.5	21.45	0.095	Left Touch	SAR#1	1:1	0.830	1.274	1.057			
848.31	777	Cell. CDMA	RC3/SO55	22.5	21.37	-0.021	Left Touch	SAR#1	1:1	0.910	1.297	1.180			
836.52	384	Cell. CDMA	RC3/SO55	22.5	21.45	-0.001	Right Touch	SAR#1	1:1	0.480	1.274	0.611			
836.52	384	Cell. CDMA	RC3/SO55	22.5	21.45	0.162	Left Tilt	SAR#1	1:1	0.263	1.274	0.335			
836.52	384	Cell. CDMA	RC3/SO55	22.5	21.45	-0.063	Right Tilt	SAR#1	1:1	0.126	1.274	0.160			
824.70	1013	Cell. CDMA	RC3/SO55	22.5	21.48	0.022	Left Touch	SAR#1	1:1	0.933	1.265	1.180			
	ANSI / IEEE C95.1-2005– SAFETY LIMIT Spatial Peak Uncontrolled Exposure/General Population Exposure									Head 6 W/kg (mW aged over 1	0,				

Note: Green entries represent repeatability measurements.

13.2 Standalone Body-Worn SAR Results

Table 13.2 CDMA Body-Worn SAR

FREQU	ENCY	Mode/Band	Service	Maximum Allowed	Conducted	Power Drift	Spacing	Device Serial	Duty	1g SAR	Scaling	1g Scaled
MHz	Ch	wode/band	Service	Power [dBm]	Power [dBm]	[dB]	[Side]	Number	Cycle	(W/kg)	Factor	SAR (W/kg)
836.52	384	Cell. CDMA	TDSO/SO32	22.5	21.38	0.150	Front [15 mm]	SAR#1	1:1	0.353	1.294	0.457
836.52	384	Cell. CDMA	TDSO/SO32	22.5	21.38	0.053	Rear [15 mm]	SAR#1	1:1	0.343	1.294	0.444
ANSI / IEEE C95.1-2005– SAFETY LIMIT Spatial Peak Uncontrolled Exposure/General Population Exposure										Body 6 W/kg (mW aged over 1	•	

13.3 SAR Test Notes

General Notes:

- 1. The test data reported are the worst-case SAR values according to test procedures specified in IEEE 1528-2003, FCC/OET Bulletin 65, Supplement C [June 2001] and FCC KDB Publication 447498 D01v05.
- 2. Batteries are fully charged at the beginning of the SAR measurements. A standard battery was used for all SAR measurements.
- 3. Liquid tissue depth was at least 15.0 cm for all frequencies.
- 4. The manufacturer has confirmed that the device(s) tested have the same physical, mechanical and thermal characteristics and are within operational tolerances expected for production units
- 5. SAR results were scaled to the maximum allowed power to demonstrate compliance per FCC KDB Publication 447498 D01v05.
- 6. Device was tested using a fixed spacing for body-worn accessory testing. A separation distance of 15 mm was considered because the manufacturer has determined that there will be body-worn accessories available in the marketplace for users to support this separation distance.
- 7. Per FCC KDB Publication 648474 D04v01, SAR was evaluated without a headset connected to the device. Since the standalone reported SAR was ≤ 1.2 W/kg, no additional SAR evaluations using a headset cable were required.
- 8. Per FCC KDB 865664 D01 v01, variability SAR tests were performed when the measured SAR results for a frequency band were greater than 0.8 W/kg. Repeated SAR measurements are highlighted in the tables above for clarity. Please see Section 14 for variability analysis.

CDMA Test Notes:

- 1. Head SAR for CDMA2000 mode was tested under RC3/SO55 per FCC KDB Publication 941225 D01v02.
- Body-Worn SAR was tested with 1x RTT with TDSO / SO32 FCH Only. EVDO and TDSO / SO32 FCH+SCH SAR tests were not required since the average output power was not more than 0.25 dB higher than the TDSO / SO32 FCH only powers, per FCC KDB Publication 941225 D01v02.
- 3. Per FCC KDB Publication 447498 D01v05, if the reported (scaled) SAR measured at the middle channel or highest output power channel for each test configuration i≤ 0.8 W/kg then testing at the other channels is not required for such test configuration(s). When the maximum output power variation across the required test channels is > ½ dB, instead of the middle channel, the highest output power channel must be used.

14. SAR MEASUREMENT VARIABILITY

Measurement Variability

Per FCC KDB Publication 865664 D01v01, SAR measurement variability was assessed for each frequency band, which was determined by the SAR probe calibration point and tissue-equivalent medium used for the device measurements. When both head and body tissue-equivalent media were required for SAR measurements in a frequency band, the variability measurement procedures were applied to the tissue medium with the highest measured SAR, using the highest measured SAR configuration for that tissue-equivalent medium. These additional measurements were repeated after the completion of all measurements requiring the same head or body tissue-equivalent medium in a frequency band. The test device was returned to ambient conditions (normal room temperature) with the battery fully charged before it was remounted on the device holder for the repeated measurement(s) to minimize any unexpected variations in the repeated results.

SAR Measurement Variability was assessed using the following procedures for each frequency band:

- 1. When the original highest measured SAR is \geq 0.80 W/kg, the measurement was repeated once.
- 2. A second repeated measurement was preformed only if the ratio of largest to smallest SAR for the original and first repeated measurements was > 1.20 or when the original or repeated measurement was ≥ 1.45 W/kg (~ 10% from the 1-g SAR limit).
- 3. A third repeated measurement was performed only if the original, first or second repeated measurement was ≥ 1.5 W/kg and the ratio of largest to smallest SAR for the original, first and second repeated measurements is > 1.20.
- 4. Repeated measurements are not required when the original highest measured SAR is < 0.80 W/kg

Frequency		Mode	Service	Phantom Position	Measured SAR (1g)	1st Repeated SAR(1g)	Ratio	2nd Repeated SAR(1g)	Ratio	3rd Repeated SAR(1g)	Ratio
MHz	Ch.				(W/kg)	(W/kg)		(W/kg)		(W/kg)	
824.70	1013	Cell. CDMA	RC3/SO55	Left Touch	0.939	0.933	1.01	N/A	N/A	N/A	N/A
	ANSI / IEEE C95.1-2005– SAFETY LIMIT Spatial Peak Uncontrolled Exposure/General Population Exposure							Head 1.6 W/kg (r averaged ove	nW/g)		

Table 14.1 Standalone Head SAR Measurement Variability Results

Measurement Uncertainty

The measured SAR was < 1.5 W/kg for all frequency bands. Therefore, per KDB Publication 865664 D01v01, the standard measurement uncertainty analysis per IEEE 1528-2003 was not required.

15. CONCLUSION

Measurement Conclusion

The SAR measurement indicates that the EUT complies with the RF radiation exposure limits of the FCC. These measurements are taken to simulate the RF effects exposure under the worst-case conditions. Precise laboratory measures were taken to assure repeatability of the tests. The tested device complies with the requirements in respect to all parameters subject to the test. The test results and statements relate only to the item(s) tested.

Please note that the absorption and distribution of electromagnetic energy in the body are very complex phenomena that depend on the mass, shape, and size of the body, the orientation of the body with respect to the field vectors, and the electrical properties of both the body and the environment. Other variables that may play a substantial role impossible biological effect are those that characterize the environment (e.g. ambient temperature, air velocity, relative humidity, and body insulation) and those that characterize the individual (e.g. age, gender, activity level, debilitation, or disease).

Because innumerable factors may interact to determine the specific biological outcome of an exposure to electromagnetic fields, any protection guide shall consider maximal amplification of biological effects as a result of field-body interactions, environmental conditions, and physiological variables.

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