## SAR EVALUATION REPORT

Applicant Name:<br>Logitech Far East Ltd.<br>7700 Gateway Boulevard<br>Newark, California 94560 USA

## Date of Testing:

10/19/2022-10/27/2022
Test Site/Location:
Element, Morgan Hill, CA, USA
Document Serial No.:
1C2208220054-01.JNZ (Rev 4)
FCC ID:
JNZYR0089

## APPLICANT:

## LOGITECH FAR EAST LTD.

| DUT Type: | Bluetooth Keyboard Case Accessory |
| :--- | :--- |
| Application Type: | Certification |
| FCC Rule Part(s): | CFR $\S 2.1093$ |


| Equipment <br> Class | Band \& Mode |  | Tx Frequency |
| :---: | :---: | :---: | :---: |

Note: This revised Test Report supersedes and replaces the previously issued test report on the same subject device for the same type of testing as indicated. Please discard or destroy the previously issued test report(s) and dispose of it accordingly.

This wireless portable device has been shown to be capable of compliance for localized specific absorption rate (SAR) for uncontrolled environment/general population exposure limits specified in ANSI/IEEE C95.1-1992 and has been tested in accordance with the measurement procedures specified in Section 1.8 of this report; for North American frequency bands only.

I attest to the accuracy of data. All measurements reported herein were performed by me or were made under my supervision and are correct to the best of my knowledge and belief. I assume full responsibility for the completeness of these measurements and vouch for the qualifications of all persons taking them. Test results reported herein relate only to the item(s) tested.


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## 1 DEVICE UNDER TEST

### 1.1 Device Overview

| Band \& Mode | Operating Modes | Tx Frequency |
| :---: | :---: | :---: |
| Bluetooth | Data | $2402-2480 \mathrm{MHz}$ |

### 1.2 Nominal and Maximum Output Power Specifications

This device operates using the following maximum and nominal output power specifications. SAR values were scaled to the maximum allowed power to determine compliance per KDB Publication 447498 D01v06.

### 1.2.1 Bluetooth Maximum and Reduced Output Power

| Mode / Band |  | Modulated Average - Single Tx Chain <br> $(\mathrm{dBm})$ |
| :--- | :---: | :---: |
| Bluetooth LE | Maximum | $\mathbf{4 . 5}$ |
|  | Nominal | $\mathbf{3 . 0}$ |

### 1.3 DUT Antenna Locations

Based on the expected use conditions, Body SAR was evaluated. The DUT is a Bluetooth keyboard accessory case for the tablet (FCC ID: BCGA2696 and FCC ID: BCGA2757). A diagram showing the location of the device antenna can be found in Appendix E. More information about the configurations evaluated for SAR can be found in Section 4.2.

### 1.4 Simultaneous Transmission Capabilities

According to FCC KDB Publication 447498 D01v06, transmitters are considered to be operating simultaneously when there is overlapping transmission, with the exception of transmissions during network hand-offs with maximum hand-off duration less than 30 seconds.

This device contains multiple transmitters that may operate simultaneously, and therefore requires a simultaneous transmission analysis according to FCC KDB Publication 447498 D01v06 procedures.

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Table 1-1
Simultaneous Transmission Scenarios

| No. | Capable Transmit Configuration | Body |
| :---: | :--- | :---: |
| 1 | Bluetooth + Tablet | Yes |

1. Bluetooth keyboard case accessory can transmit simultaneously with Tablet (FCC ID: BCGA2696 and FCC ID: BCGA2757).

### 1.5 Miscellaneous SAR Test Considerations

The DUT has two variants. These two variants are identical except for different PCB and LDO manufacturers. Investigation was performed and it was determined variant \#1 is the worst case. All test data in this report pertains to the worst test configuration, variant \#1, with the final modification of moving the hall sensor location to avoid triggering Keyboard by the device speaker magnets in the reading mode, and introducing a second source RF inductor. All other circuitry and features are identical.

Per FCC KDB 447498 D01v06 Sec. 4.3.1, standalone 10-g extremity SAR evaluation for general population exposure conditions, by measurement or numerical simulation, is not required when the corresponding SAR Test Exclusion Threshold conditions are satisfied.

### 2.4 GHz Bluetooth Extremity SAR Test Exclusion

a) $\frac{\text { Max Power of Channel }(\mathrm{mW})}{\text { Test Separation }(\mathrm{mm})} * \sqrt{\text { Frequency }(\mathrm{GHz})} \leq 7.5$

Based on the maximum conducted source-based time-averaged power of Bluetooth (adjusted for duty cycle) and the antenna to user separation distance, Bluetooth SAR was not required; $[(0.14 / 5) * \sqrt{2} .480]=0.04 \leq 7.5$. Since the minimum separation distance is $<5 \mathrm{~mm}$, a distance of 5 mm is applied to determine SAR test exclusion according to FCC KDB Publication 447498 D01v06.

### 1.6 Guidance Applied

- FCC KDB Publication 248227 D01v02r02 (SAR Considerations for 802.11 Devices)
- FCC KDB Publication 447498 D01v06 (General SAR Guidance)
- FCC KDB Publication 865664 D01v01r04, D02v01r02 (SAR Measurements up to 6 GHz )


### 1.7 Device Serial Numbers

Several samples with identical hardware were used to support SAR testing. The manufacturer has confirmed that the device(s) tested have the same physical, mechanical and thermal characteristics and are within operational tolerances expected for production units. The serial numbers used for each test are indicated alongside the results in Section 8.

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### 1.8 Bibliography

| Report Type | Report Serial Number |
| :---: | :---: |
| BCGA2696 Part 1 SAR Report | 1C2205090022-11.BCG (Rev 1) |
| BCGA2757 Part 1 SAR Report | 1C2205090023-21.BCG |

Note: Please refer to the Tablet SAR report serial number above for reference.

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## 2 INTRODUCTION

The FCC and Innovation, Science, and Economic Development Canada have adopted the guidelines for evaluating the environmental effects of radio frequency (RF) radiation in ET Docket 93-62 on Aug. 6, 1996 and Health Canada Safety Code 6 to protect the public and workers from the potential hazards of RF emissions due to FCC-regulated portable devices. [1]

The safety limits used for the environmental evaluation measurements are based on the criteria published by the American National Standards Institute (ANSI) for localized specific absorption rate (SAR) in IEEE/ANSI C95.11992 Standard for Safety Levels with Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 3 kHz to 300 GHz [3] and Health Canada RF Exposure Guidelines Safety Code 6 [22]. The measurement procedure described in IEEE/ANSI C95.3-2002 Recommended Practice for the Measurement of Potentially Hazardous Electromagnetic Fields - RF and Microwave [4] is used for guidance in measuring the Specific Absorption Rate (SAR) due to the RF radiation exposure from the Equipment Under Test (EUT). These criteria for SAR evaluation are similar to those recommended by the International Committee for Non-lonizing Radiation Protection (ICNIRP) in Biological Effects and Exposure Criteria for Radiofrequency Electromagnetic Fields," Report No. Vol 74. SAR is a measure of the rate of energy absorption due to exposure to an RF transmitting source. SAR values have been related to threshold levels for potential biological hazards.

### 2.1 SAR Definition

Specific Absorption Rate is defined as the time derivative (rate) of the incremental energy (dU) absorbed by (dissipated in) an incremental mass (dm) contained in a volume element ( dV ) of a given density ( $\rho$ ). It is also defined as the rate of RF energy absorption per unit mass at a point in an absorbing body (see Equation 2-1).

## Equation 2-1

SAR Mathematical Equation

$$
S A R=\frac{d}{d t}\left(\frac{d U}{d m}\right)=\frac{d}{d t}\left(\frac{d U}{\rho d v}\right)
$$

SAR is expressed in units of Watts per Kilogram (W/kg).

$$
S A R=\frac{\sigma \cdot E^{2}}{\rho}
$$

where:
$\sigma=$ conductivity of the tissue-simulating material (S/m)
$\rho=$ mass density of the tissue-simulating material $\left(\mathrm{kg} / \mathrm{m}^{3}\right)$
$E=$ Total RMS electric field strength (V/m)

NOTE: The primary factors that control rate of energy absorption were found to be the wavelength of the incident field in relation to the dimensions and geometry of the irradiated organism, the orientation of the organism in relation to the polarity of field vectors, the presence of reflecting surfaces, and whether conductive contact is made by the organism with a ground plane.[6]

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## 3 DOSIMETRIC ASSESSMENT

### 3.1 Measurement Procedure

The evaluation was performed using the following procedure compliant to FCC KDB Publication 865664 D01v01r04 and IEEE 1528-2013:

1. The SAR distribution at the exposed side of the head or body was measured at a distance no greater than 5.0 mm from the inner surface of the shell. The area covered the entire dimension of the device-head and body interface and the horizontal grid resolution was determined per FCC KDB Publication 865664 D01v01r04 (See Table 3-1) and IEEE 1528-2013.
2. The point SAR measurement was taken at the maximum SAR region determined from Step 1 to enable the monitoring of SAR fluctuations/drifts during the $1 \mathrm{~g} / 10 \mathrm{~g}$ cube evaluation. SAR at this fixed point was measured and used as a reference value.
3. Based on the area scan data, the peak of the region with maximum SAR was


Figure 3-1
Sample SAR Area Scan determined by spline interpolation. Around this point, a volume was assessed according to the measurement resolution and volume size requirements of FCC KDB Publication 865664 D01v01r04 (See Table 3-1) and IEEE 1528-2013. On the basis of this data set, the spatial peak SAR value was evaluated with the following procedure (see references or the DASY manual online for more details):
a. SAR values at the inner surface of the phantom are extrapolated from the measured values along the line away from the surface with spacing no greater than that in Table 3-1. The extrapolation was based on a least-squares algorithm. A polynomial of the fourth order was calculated through the points in the $z$-axis (normal to the phantom shell).
b. After the maximum interpolated values were calculated between the points in the cube, the SAR was averaged over the spatial volume ( 1 g or 10 g ) using a 3D-Spline interpolation algorithm. The 3D-spline is composed of three one-dimensional splines with the "Not a knot" condition (in $x, y$, and $z$ directions). The volume was then integrated with the trapezoidal algorithm. One thousand points ( $10 \times 10 \times 10$ ) were obtained through interpolation, in order to calculate the averaged SAR.
c. All neighboring volumes were evaluated until no neighboring volume with a higher average value was found.
4. The SAR reference value, at the same location as step 2, was re-measured after the zoom scan was complete to calculate the SAR drift. If the drift deviated by more than $5 \%$, the SAR test and drift measurements were repeated.

Table 3-1
Area and Zoom Scan Resolutions per FCC KDB Publication 865664 D01v01r04*

| Frequency | Maximum Area Scan Resolution (mm)$\left(\Delta x_{\text {area }}, \Delta y_{\text {area }}\right)$ | $\begin{gathered} \text { Maximum Zoom Scan } \\ \text { Resolution }(\mathrm{mm}) \\ \left(\Delta \mathrm{x}_{\text {zoom }}, \Delta \mathrm{y}_{\text {zoom }}\right) \end{gathered}$ | Maximum Zoom Scan Spatial Resolution ( mm ) |  |  | Minimum Zoom Scan Volume (mm) ( $\mathrm{x}, \mathrm{y}, \mathrm{z}$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Uniform Grid | Graded Grid |  |  |
|  |  |  | $\Delta z_{\text {zoom }}(\mathrm{n})$ | $\Delta z_{\text {zoom }}(1)^{*}$ | $\Delta z_{\text {zoom }}(n>1)^{*}$ |  |
| $\leq 2 \mathrm{GHz}$ | $\leq 15$ | $\leq 8$ | $\leq 5$ | $\leq 4$ | $\leq 1.5^{*} \Delta z_{\text {zoom }}(\mathrm{n}-1)$ | $\geq 30$ |
| $2-3 \mathrm{GHz}$ | $\leq 12$ | $\leq 5$ | $\leq 5$ | $\leq 4$ | $\leq 1.5^{*} \Delta z_{\text {zoom }}(\mathrm{n}-1)$ | $\geq 30$ |
| $3-4 \mathrm{GHz}$ | $\leq 12$ | $\leq 5$ | $\leq 4$ | $\leq 3$ | $\leq 1.5^{*} \Delta z_{\text {zoom }}(\mathrm{n}-1)$ | $\geq 28$ |
| $4-5 \mathrm{GHz}$ | $\leq 10$ | $\leq 4$ | $\leq 3$ | $\leq 2.5$ | $\leq 1.5^{*} \Delta z_{\text {zoom }}(\mathrm{n}-1)$ | $\geq 25$ |
| $5-6 \mathrm{GHz}$ | $\leq 10$ | $\leq 4$ | $\leq 2$ | $\leq 2$ | $\leq 1.5^{*} \Delta z_{\text {zoom }}(\mathrm{n}-1)$ | $\geq 22$ |

*Also compliant to IEEE 1528-2013 Table 6

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## 4 TEST CONFIGURATION POSITIONS AND MEASUREMENT PROCEDURES

### 4.1 Device Holder

The device holder is made out of low-loss POM material having the following dielectric parameters: relative permittivity $\varepsilon=3$ and loss tangent $\delta=0.02$.

### 4.2 SAR Testing for Accessories with RF Transmitters

Per FCC KDB Publication 447498 D01v06 sec. 6.4, separate equipment approval is required for accessories containing transmitter(s) that are available from the host manufacturer or third-party accessory suppliers. When simultaneous transmission applies, all transmitter combinations must be addressed for the accessory alone and also with the accessory operating in conjunction with the host equipment. The keyboard case provides two viewing positions-one for typing and another for browsing. The keyboard case automatically turns on in typing position and powers off in browsing position. In typing position, the left edge of the tablet is closest to the body. The standalone transmission of the Bluetooth keyboard accessory was tested for SAR for back side which is closest to the body. Additionally, SAR was retested for the tablet (FCC ID: BCGA2696 and FCC ID: BCGA2757) with the keyboard attached based on the overall worst-case configuration for left edge for simultaneous consideration. Head tissue was used for SAR testing.

### 4.3 Measured and Reported SAR

Per FCC KDB Publication 447498 D01v06, when SAR is not measured at the maximum power level allowed for production units, the results must be scaled to the maximum tune-up tolerance limit according to the power applied to the individual channels tested to determine compliance. For simultaneous transmission, the measured aggregate SAR must be scaled according to the sum of the differences between the maximum tune-up tolerance and actual power used to test each transmitter. When SAR is measured at or scaled to the maximum tune-up tolerance limit, the results are referred to as reported SAR. The highest reported SAR results are identified on the grant of equipment authorization according to procedures in KDB 690783 D01v01r03.

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## 5 RF EXPOSURE LIMITS

### 5.1 Uncontrolled Environment

UNCONTROLLED ENVIRONMENTS are defined as locations where there is the exposure of individuals who have no knowledge or control of their exposure. The general population/uncontrolled exposure limits are applicable to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Members of the general public would come under this category when exposure is not employment-related; for example, in the case of a wireless transmitter that exposes persons in its vicinity.

### 5.2 Controlled Environment

CONTROLLED ENVIRONMENTS are defined as locations where there is exposure that may be incurred by persons who are aware of the potential for exposure, (i.e. as a result of employment or occupation). In general, occupational/controlled exposure limits are applicable to situations in which persons are exposed as a consequence of their employment, who have been made fully aware of the potential for exposure and can exercise control over their exposure. This exposure category is also applicable when the exposure is of a transient nature due to incidental passage through a location where the exposure levels may be higher than the general population/uncontrolled limits, but the exposed person is fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Table 5-1
SAR Human Exposure Specified in ANSI/IEEE C95.1-1992 and Health Canada Safety Code 6

| HUMAN EXPOSURE LIMITS |  |  |
| :--- | :---: | :---: |
|  | UNCONTROLLED <br> ENVIRONMENT <br> General Population <br> $(\mathrm{W} / \mathrm{kg})$ or $(\mathrm{mW} / \mathrm{g})$ | CONTROLLED <br> ENVIRONMENT <br> Occupational <br> $(\mathrm{W} / \mathrm{kg})$ or $(\mathrm{mW} / \mathrm{g})$ |
| Peak Spatial Average SAR <br> Head | 1.6 | 8.0 |
| Whole Body SAR | 0.08 | 0.4 |
| Peak Spatial Average SAR <br> Hands, Feet, Ankle, Wrists, etc. | 4.0 | 20 |

1. The Spatial Peak value of the SAR averaged over any 1 gram of tissue (defined as a tissue volume in the shape of a cube) and over the appropriate averaging time.
2. The Spatial Average value of the SAR averaged over the whole body.
3. The Spatial Peak value of the SAR averaged over any 10 grams of tissue (defined as a tissue volume in the shape of a cube) and over the appropriate averaging time.

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## 6 RF CONDUCTED POWERS

### 6.1 Bluetooth Maximum Conducted Powers

Table 6-1

| Frequency [MHz] | Modulation | Data Rate [Mbps] | Channel No. | Avg ConductedPower |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | [dBm] | [mW] |
| 2402 | GFSK | 1.0 | Low | 3.52 | 2.249 |
| 2440 | GFSK | 1.0 | Mid | 3.58 | 2.280 |
| 2480 | GFSK | 1.0 | High | 3.57 | 2.275 |

Table 6-2
Bluetooth Average RF Power - 2 Mbps

| Frequency <br> [MHz] | Modulation | Data <br> Rate <br> [Mbps] | Channel | Avg Conducted <br> [dBm] |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | [mW] |  |  |  |  |
| 2404 | GFSK | 2.0 | Low | 3.46 | 2.218 |
| 2440 | GFSK | 2.0 | Mid | 3.52 | 2.249 |
| 2478 | GFSK | 2.0 | High | 3.57 | 2.275 |


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### 6.2 Bluetooth Duty Cycle Plots

Figure 6-1
Bluetooth Transmission Plot


Equation 6-1
Bluetooth Duty Cycle Calculation
Duty Cycle $=\frac{\text { Pulse Width }}{\text { Period }} * 100 \%=\frac{350 \mu s}{7.056 \mathrm{~ms}} * 100 \%=4.96 \%$

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### 6.3 Notes for Bluetooth

- Full power measurements were performed per FCC KDB Procedures 248227.


Figure 6-3
Power Measurement Setup


## 7 SYSTEM VERIFICATION

### 7.1 Tissue Verification

Table 7-1
Measured Tissue Properties

| Calibrated for Tests Performed on: | Tissue Type | Tissue Temp During Calibration ( ${ }^{\circ} \mathrm{C}$ ) | Measured <br> Frequency <br> (MHz) | Measured Conductivity, $\sigma$ (S/m) | Measured Dielectric Constant, $\varepsilon$ | TARGET Conductivity, $\sigma$ (S/m) | TARGET <br> Dielectric <br> Constant, $\varepsilon$ | \% dev $\boldsymbol{\sigma}$ | \% $\operatorname{dev} \boldsymbol{\varepsilon}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10/19/2022 | 2450 Head | 20.4 | 2400 | 1.782 | 38.243 | 1.756 | 39.289 | 1.48\% | -2.66\% |
|  |  |  | 2450 | 1.822 | 38.166 | 1.800 | 39.200 | 1.22\% | -2.64\% |
|  |  |  | 2480 | 1.844 | 38.125 | 1.833 | 39.162 | 0.60\% | -2.65\% |
|  |  |  | 2500 | 1.858 | 38.101 | 1.855 | 39.136 | 0.16\% | -2.64\% |
| 10/24/2022 | 2450 Head | 20.4 | 2400 | 1.779 | 37.832 | 1.756 | 39.289 | 1.31\% | -3.71\% |
|  |  |  | 2450 | 1.817 | 37.743 | 1.800 | 39.200 | 0.94\% | -3.72\% |
|  |  |  | 2480 | 1.837 | 37.715 | 1.833 | 39.162 | 0.22\% | -3.69\% |
|  |  |  | 2500 | 1.850 | 37.683 | 1.855 | 39.136 | -0.27\% | -3.71\% |
| 10/26/2022 | 2450 Head | 20.7 | 2400 | 1.789 | 37.983 | 1.756 | 39.289 | 1.88\% | -3.32\% |
|  |  |  | 2450 | 1.826 | 37.897 | 1.800 | 39.200 | 1.44\% | -3.32\% |
|  |  |  | 2480 | 1.850 | 37.847 | 1.833 | 39.162 | 0.93\% | -3.36\% |
|  |  |  | 2500 | 1.865 | 37.822 | 1.855 | 39.136 | 0.54\% | -3.36\% |
| 10/27/2022 | 3600 Head | 19.4 | 3600 | 3.021 | 38.773 | 3.015 | 37.814 | 0.20\% | 2.54\% |
|  |  |  | 3650 | 3.066 | 38.732 | 3.066 | 37.757 | 0.00\% | 2.58\% |
|  |  |  | 3690 | 3.097 | 38.654 | 3.107 | 37.711 | -0.32\% | 2.50\% |
|  |  |  | 3700 | 3.107 | 38.642 | 3.117 | 37.700 | -0.32\% | 2.50\% |

The above measured tissue parameters were used in the cDASY6/DASY8 software. The cDASY6/DASY8 software was used to perform interpolation to determine the dielectric parameters at the SAR test device frequencies (per KDB Publication 865664 D01v01r04 and IEEE 1528-2013 6.6.1.2). The tissue parameters listed in the SAR test plots may slightly differ from the table above due to significant digit rounding in the software.

Per April 2019 TCB Workshop Notes, single head-tissue simulating liquid specified in IEC 62209-1 is permitted to use for all SAR tests.

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| :--- |
| Technical Manager |

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### 7.2 Test System Verification

Prior to SAR assessment, the system is verified to $\pm 10 \%$ of the SAR measurement on the reference dipole at the time of calibration by the calibration facility. Full system validation status and result summary can be found in Appendix D.

Table 7-2
System Verification Results $\mathbf{- 1 g}$

| System Verification TARGET \& MEASURED |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SAR System | Tissue Frequency (MHz) | Tissue Type | Date | Amb. Temp. (C) | Liquid Temp. (C) | Input <br> Power <br> (W) | Source SN | Probe SN | $\begin{gathered} \text { Measured SAR1g } \\ (\mathrm{W} / \mathrm{kg}) \end{gathered}$ | 1W Target SAR1g (W/kg) | 1W Normalized SAR 1g (W/kg) | Deviation1g (\%) |
| AM8 | 2450 | HEAD | 10/19/2022 | 20.3 | 19.9 | 0.10 | 750 | 7546 | 5.210 | 52.60 | 52.100 | -0.95\% |
| AM8 | 2450 | HEAD | 10/24/2022 | 20.2 | 20.0 | 0.10 | 921 | 7546 | 5.620 | 54.20 | 56.200 | 3.69\% |
| AM8 | 2450 | HEAD | 10/26/2022 | 21.2 | 20.7 | 0.10 | 750 | 7546 | 5.110 | 52.60 | 51.100 | -2.85\% |
| AM1 | 3700 | HEAD | 10/27/2022 | 21.5 | 19.4 | 0.10 | 1097 | 7639 | 6.980 | 68.10 | 69.800 | 2.50\% |



Figure 7-1
System Verification Setup Diagram


Figure 7-2
System Verification Setup Photo

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## 8 SAR DATA SUMMARY

### 8.1 Standalone SAR Data

Table 8-1
Bluetooth Body SAR Data

| MEASUREMENT RESULTS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| frequency |  | Mode | $\begin{array}{\|c\|} \hline \begin{array}{c} \text { Maximum } \\ \text { Allowed } \\ \text { Power [dBm] } \end{array} \\ \hline \end{array}$ | $\begin{array}{\|c} \text { Conducted } \\ \text { Power [dBm] } \end{array}$ | Power Drift [dB] | Spacing | Variant | Device Serial Number | $\begin{gathered} \text { Data } \\ \text { Rate } \\ \text { (Mbps) } \end{gathered}$ | Side | $\begin{gathered} \text { Duty } \\ \text { Cyycle } \\ \text { (\%) } \end{gathered}$ | SAR (19) | ScalingFactor (CondPower) | $\begin{array}{\|c} \begin{array}{c} \text { Scaling } \\ \text { Factor (Duty } \\ \text { Cycle) } \end{array} \\ \hline \end{array}$ | $\begin{array}{\|c\|} \hline \begin{array}{c} \text { Reported SAR } \\ (\mathrm{Ig}) \end{array} \\ \hline(\mathrm{W} / \mathrm{kg}) \\ \hline \end{array}$ | Plot \# |
| MHz | ch. |  |  |  |  |  |  |  |  |  |  | (W/kg) |  |  |  |  |
| 2440 | Mid | Bluetooth | 4.50 | 3.58 | -0.20 | 0 mm | V1 | 2222LZ907NY8 | 1 | Back | 4.96 | 0.003 | 1.236 | 1.008 | 0.004 | A1 |
| ANSI / IEEE C95.1 1992 - SAFETY LIMIT$\quad$ Spatial PeakUncontrolled Exposure/General Population |  |  |  |  |  | $1.6 \mathrm{~W} / \mathrm{kg}(\mathrm{mW} / \mathrm{g})$ averaged over 1 gram |  |  |  |  |  |  |  |  |  |  |

Note: The reported SAR was scaled to the 5\% transmission duty factor to determine compliance since the duty factor of the device is permanently limited to $5 \%$ per the manufacturer.

### 8.2 Spotcheck SAR Data for Tablet with Case for Simultaneous Consideration

Table 8-2
BCGA2696 2.4 GHz WLAN Body SAR Data

| MEASUREMENT RESULTS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FREQUENCY |  | Mode | Service | Bandwidth [MHz] | Maximum Allowed Power [dBm] | Conducted Power [dBm] | Power Drift[dB] | Spacing | Antenna Config. | Device Serial Number | Data Rate (Mbps) | Side | DutyCycle (\%) | SAR (1g) | Scaling Factor (Power) | $\begin{aligned} & \text { Scaling } \\ & \text { Factor (Duty } \\ & \text { Cycle) } \end{aligned}$ | $\begin{array}{\|c\|} \hline \begin{array}{c} \text { Reported SAR } \\ (1 \mathrm{~g}) \end{array} \\ \hline(\mathrm{W} / \mathrm{kg}) \\ \hline \end{array}$ |
| MHz | Ch. |  |  |  |  |  |  |  |  |  |  |  |  | (W/kg) |  |  |  |
| 2437 | 6 | 802.11b | DSSS | 22 | 20.25 | 19.14 | -0.02 | 0 mm | Ant WF7B | R76DF4H6D6 | 1 | left | 99.7 | 0.450 | 1.291 | 1.003 | 0.583 |
| 2437 | 6 | 802.11b | DSSS | 22 | 20.50 | 19.62 | 0.00 | 0 mm | Ant WF8 | KKGJYGGJ9V | 1 | left | 99.7 | 0.002 | 1.225 | 1.003 | 0.002 |
| ANSI / IEEE C95.1 1992 - SAFETY LIMIT |  |  |  |  |  |  |  | Body |  |  |  |  |  |  |  |  |  |
| Spatial Peak |  |  |  |  |  |  |  | 1.6 W/kg (mW/g) |  |  |  |  |  |  |  |  |  |
| Uncontrolled Exposure/General Population |  |  |  |  |  |  |  | averaged over 1 gram |  |  |  |  |  |  |  |  |  |

Table 8-3
BCGA2757 Cellular Body SAR Data

| MEASUREMENT RESULTS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 CC Uplink \| 2CC Uplink | Component | frequency |  |  | Mode | Bandwidth [ $\mathrm{MHz]}$ | $\underset{\substack{\text { Maximum } \\ \text { Allowed Power } \\ \text { [dBm] }}}{\text { and }}$ | $\begin{gathered} \text { Conducted } \\ \text { Power }[\mathrm{dBm}] \end{gathered}$ | $\begin{array}{\|l\|l} \hline \text { Power } \\ \text { Drift [dB] } \end{array}$ | MPR [dB] | $\begin{gathered} \text { Antenna } \\ \text { Config. } \end{gathered}$ | Device SerialNumber | Modulation | RB Size | RB oftrst | Spacing | Side | Duty Cycle | SAR (19) | ScalingFactor | $\begin{array}{\|c\|} \hline \text { Reported SAR } \\ (1 \mathrm{~g}) \end{array}$ |
|  |  | MHz | Ch |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | (W/kg) |  | (W/kg) |
| 2 CC Uplink | PCC | 3690.00 | 56640 | High | LTE Band 48 | 20 | 13.50 | 12.90 | -0.04 | 0 | Ant 1a | G3Q2X6LP70 | QPSK | 50 | 0 | 0 mm | left | 1:1 | 0.322 | 1.148 | 0.370 |
| 2 CC Uplink | scc | 3670.20 | 56442 | High | LTE Band 48 | 20 |  |  |  |  |  |  |  | 50 | 50 |  |  |  |  |  |  |
| ANSI / IEEE C95.1 1992 - SAFETY LIMIT |  |  |  |  |  |  |  |  |  | Body$1.6 \mathrm{~W} / \mathrm{kg}(\mathrm{mW} / \mathrm{g})$averaged over 1 gram |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Uncontrolled Exposure/General Population |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |



Table 8-4
BCGA2757 2.4 GHz WLAN Body SAR Data

| MEASUREMENT RESULTS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FREQUENCY |  | Mode | Service | Bandwidth [MHz] | MaximumAllowed Power$[d B m]$ | Conducted Power [dBm] | Power Drift [dB] | Spacing | Antenna Config. | Device Serial Number | $\begin{aligned} & \text { Data } \\ & \text { Rate } \\ & \text { (Mbps) } \end{aligned}$ | Side | $\begin{gathered} \hline \text { Duty } \\ \text { Cycle } \\ \text { (\%) } \end{gathered}$ | SAR (1g) | ScalingFactor (Power) | ScalingFactor (DutyCycle) | Reported SAR <br> $(1 \mathrm{~g})$ <br> $(W / \mathrm{kg})$ |
| MHz | Ch. |  |  |  |  |  |  |  |  |  |  |  |  | (W/kg) |  |  |  |
| 2462 | 11 | 802.11b | DSss | 22 | 12.50 | 12.12 | 0.05 | 0 mm | Ant 3a | Q93JKF6L7J | 1 | left | 99.7 | 0.000 | 1.091 | 1.003 | 0.000 |
| 2462 | 11 | 802.11b | DSSS | 22 | 8.50 | 7.56 | -0.01 | 0 mm | Ant 1a | Y6L2P59NKJ | 1 | left | 99.7 | 0.164 | 1.242 | 1.003 | 0.204 |
|  |  |  | SI / IEEE | C95.1 1992 Spatial Pe Eposure/G | SAFETY LIMIT |  |  |  |  |  |  | 1.6 W | dy |  |  |  |  |

### 8.3 SAR Test Notes

## General Notes:

1. The test data reported are the worst-case SAR values according to test procedures specified in FCC KDB Publication 616217 D04v01r02, and FCC KDB Publication 447498 D01v06.
2. The DUT has two variants. These two variants are identical except for different PCB and LDO manufacturers. Investigation was performed and it was determined variant \#1 is the worst case. All test data in this report pertains to the worst test configuration, variant \#1, with the final modification of moving the hall sensor location to avoid triggering Keyboard by the device speaker magnets in the reading mode, and introducing a second source RF inductor. All other circuitry and features are identical.
3. Liquid tissue depth was at least 15.0 cm for all frequencies.
4. The manufacturer has confirmed that the device(s) tested have the same physical, mechanical and thermal characteristics and are within operational tolerances expected for production units.
5. SAR results were scaled to the maximum allowed power to demonstrate compliance per FCC KDB Publication 447498 D01v06.
6. Per FCC KDB 865664 D01v01r04, variability SAR test was not performed since the measured SAR results for a frequency band was less than $0.8 \mathrm{~W} / \mathrm{kg}$.
7. The orange highlight throughout the report represent the highest scaled SAR per Equipment Class.

## Bluetooth Notes

1. Bluetooth SAR was evaluated with a test mode with hopping disabled with DH5 operation. The reported SAR was scaled to the $5 \%$ transmission duty factor to determine compliance since the duty factor of the device is limited to $5 \%$ per the manufacturer. See Section 6.2 for the time domain plot and calculation for the duty factor of the device.

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| $\begin{array}{\|l\|} \hline \text { Document S/N: } \\ \text { 1C2208220054-01.JNZ (Rev 4) } \\ \hline \end{array}$ | DUT Type: <br> Bluetooth Keyboard Case Accessory | Page 16 of 23 |

## 9 FCC MULTI-TX AND ANTENNA SAR CONSIDERATIONS

### 9.1 Introduction

The following procedures adopted from FCC KDB Publication 447498 D01v06 are applicable to devices with builtin unlicensed transmitters such as 802.11 and Bluetooth devices which may simultaneously transmit with the licensed transmitter.

### 9.2 Simultaneous Transmission Procedures

This keyboard case accessory contains a Bluetooth transmitter that may operate simultaneously with the host equipment. Therefore, simultaneous transmission analysis is required. Per FCC KDB Publication 447498 D01v06 and IEEE 1528-2013 Section 6.3.4.1.2, simultaneous transmission SAR test exclusion may be applied when the sum of the 1 g SAR for all the simultaneous transmitting antennas in a specific a physical test configuration is $\leq 1.6$ W/kg. The standalone transmission of the Bluetooth keyboard accessory was tested for SAR for back side since it is closest to the body based on expected use conditions. Additionally, SAR was retested for the tablet with the keyboard attached based on the overall worst-case configuration for left edge (closest to body in typing position) for simultaneous consideration. Please see complete compliance evaluation of tablet FCC ID: BCGA2696 in RF Exposure Technical Report S/N: 1C2205090022-11.BCG (Rev 1) and FCC ID: BCGA2757 in RF Exposure Technical Report S/N: 1C2205090023-21.BCG for reference.

### 9.3 Body SAR Simultaneous Transmission Analysis

Table 9-1
BCGA2696 Simultaneous Transmission Scenario with Keyboard

| Simult Tx | Tablet w/case Left Edge 2.4 <br> GHz WLAN Ant WF7B SAR <br> $(\mathrm{W} / \mathrm{kg})$ | Tablet w/case Left Edge 2.4 <br> GHz WLAN Ant WF8 SAR <br> $(\mathrm{W} / \mathrm{kg})$ | 2.4 GHz Bluetooth <br> Keyboard Back Side <br> SAR (W/kg) | $\sum$ SAR <br> $(W / k g)$ |
| :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | $1+2+3$ |
| Body | 0.583 | 0.002 | 0.004 | 0.589 |

Table 9-2
BCGA2757 Simultaneous Transmission Scenario with Keyboard

| Simult Tx | Tablet w/case Left Edge <br> Cellular Band Ant 1a <br> SAR (W/kg) | Tablet w/case Left Edge 2.4 <br> GHz WLAN Ant 3a SAR <br> $(\mathrm{W} / \mathrm{kg})$ | Tablet w/case Left Edge 2.4 <br> GHz WLAN Ant 1a Reduced <br> at 8.5 dBm SAR (W/kg) | 2.4 GHz Bluetooth <br> Keyboard Back Side <br> SAR (W/kg) | $\sum$ SAR <br> $(W / \mathrm{kg})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | $1+2+3+4$ |
|  | 0.370 | 0.000 | 0.204 | 0.004 | $\mathbf{0 . 5 7 8}$ |

### 9.4 Simultaneous Transmission Conclusion

The above numerical summed SAR results for all the worst-case simultaneous transmission conditions were below the SAR limit. Therefore, the above analysis is sufficient to determine that simultaneous transmission cases will not exceed the SAR limit and therefore no measured volumetric simultaneous SAR summation is required per FCC KDB Publication 447498 D01v06 and IEEE 1528-2013 Section 6.3.4.1.2.

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| :--- |
| Bluetooth Keyboard Case Accessory |

## 10 SAR MEASUREMENT VARIABILITY

### 10.1 Measurement Variability

Per FCC KDB Publication 865664 D01v01r04, SAR measurement variability was not assessed for each frequency band since all measured SAR values are $<0.8 \mathrm{~W} / \mathrm{Kg}$ for 1 g SAR.

### 10.2 Measurement Uncertainty

The measured SAR was <1.5 W/kg for 1 g for all frequency bands. Therefore, per KDB Publication 865664 D01v01r04, the extended measurement uncertainty analysis per IEEE 1528-2013 was not required.

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## 11 EQUIPMENT LIST

| Manufacturer | Model | Description | Cal Date | Cal Interval | Cal Due | Serial Number |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Agilent | E4404B | Spectrum Analyzer | N/A | N/A | N/A | MY45113242 |
| Agilent | E4438C | ESG Vector Signal Generator | 3/24/2022 | Annual | 3/24/2023 | MY45093678 |
| Agilent | E4438C | ESG Vector Signal Generator | 3/22/2022 | Annual | 3/22/2023 | US41460739 |
| Agilent | N5182A | MXG Vector Signal Generator | 1/12/2022 | Annual | 1/12/2023 | MY47420837 |
| Agilent | N5182A | MXG Vector Signal Generator | 11/17/2021 | Annual | 11/17/2022 | US46240505 |
| Agilent | 8753ES | S-Parameter Vector Network Analyzer | 6/14/2022 | Annual | 6/14/2023 | US39170118 |
| Agilent | 8753ES | S-Parameter Vector Network Analyzer | 2/11/2022 | Annual | 2/11/2023 | MY40003841 |
| Amplifier Research | 15S1G6 | Amplifier | CBT | N/A | CBT | 343971 |
| Amplifier Research | 150A100C | Amplifier | CBT | N/A | CBT | 350132 |
| Anritsu | MN8110B | I/O Adaptor | CBT | N/A | CBT | 6261747881 |
| Anritsu | ML2496A | Power Meter | 2/11/2022 | Annual | 2/11/2023 | 1405003 |
| Anritsu | ML2496A | Power Meter | 8/16/2022 | Annual | 8/16/2023 | 1351001 |
| Anritsu | MA2411B | Pulse Power Sensor | 3/28/2022 | Annual | 3/28/2023 | 1339007 |
| Anritsu | MA2411B | Pulse Power Sensor | 3/2/2022 | Annual | 3/2/2023 | 1126066 |
| Anritsu | MT8821C | Radio Communication Analyzer MT8821C | 5/11/2022 | Annual | 5/11/2023 | 6262044715 |
| Anritsu | MT8821C | Radio Communication Analyzer MT8821C | 5/2/2022 | Annual | 5/2/2023 | 6200901190 |
| Anritsu | MA24106A | USB Power Sensor | 3/28/2022 | Annual | 3/28/2023 | 1520503 |
| Anritsu | MA24106A | USB Power Sensor | 3/28/2022 | Annual | 3/28/2023 | 1520501 |
| Control Company | 4353 | Long Stem Thermometer | 10/28/2020 | Biennial | 10/28/2022 | 200670623 |
| Control Company | 4353 | Long Stem Thermometer | 10/28/2020 | Biennial | 10/28/2022 | 200670633 |
| Control Company | 4353 | Long Stem Thermometer | 10/28/2020 | Biennial | 10/28/2022 | 200670635 |
| Control Company | 4040 | Therm./ Clock/ Humidity Monitor | 1/21/2022 | Annual | 1/21/2023 | 160574418 |
| Mitutoyo | 500-196-30 | CD-6"ASX 6Inch Digital Caliper | 2/16/2022 | Triennial | 2/16/2025 | A20238413 |
| Keysight Technologies | N9020A | MXA Signal Analyzer | 3/4/2022 | Annual | 3/4/2023 | US46470561 |
| MCL | BW-N6W5+ | 6dB Attenuator | CBT | N/A | CBT | 1139 |
| Mini-Circuits | VLF-6000+ | Low Pass Filter DC to 6000 MHz | CBT | N/A | CBT | N/A |
| Mini-Circuits | BW-N20W5+ | DC to 18 GHz Precision Fixed 20 dB Attenuator | CBT | N/A | CBT | N/A |
| Mini-Circuits | NLP-1200+ | Low Pass Filter DC to 1000 MHz | CBT | N/A | CBT | N/A |
| Mini-Circuits | NLP-2950+ | Low Pass Filter DC to 2700 MHz | CBT | N/A | CBT | N/A |
| Mini-Circuits | BW-N20W5 | Power Attenuator | CBT | N/A | CBT | 1226 |
| Mini-Circuits | ZUDC10-83-S+ | Directional Coupler | CBT | N/A | CBT | 2050 |
| Narda | 4772-3 | Attenuator (3dB) | CBT | N/A | CBT | 9406 |
| Narda | BW-S3W2 | Attenuator (3dB) | CBT | N/A | CBT | 120 |
| Rohde \& Schwarz | CMW500 | Wideband Radio Communication Tester | 4/14/2022 | Annual | 4/14/2023 | 167284 |
| Rohde \& Schwarz | CMW500 | Wideband Radio Communication Tester | 4/14/2022 | Annual | 4/14/2023 | 167285 |
| SPEAG | DAK-3.5 | Dielectric Assessment Kit | 5/12/2022 | Annual | 5/12/2023 | 1070 |
| SPEAG | MAIA | Modulation and Audio Interference Analyzer | N/A | N/A | N/A | 1237 |
| SPEAG | D2450V2 | 2450 MHz SAR Dipole | 5/11/2022 | Annual | 5/11/2023 | 750 |
| SPEAG | D2450V2 | 2450 MHz SAR Dipole | 11/9/2021 | Annual | 11/9/2022 | 921 |
| SPEAG | D3700V2 | 3700 MHz SAR Dipole | 6/9/2021 | Biennial | 6/9/2023 | 1097 |
| SPEAG | DAE4 | Dasy Data Acquisition Electronics | 4/14/2022 | Annual | 4/14/2023 | 1402 |
| SPEAG | DAE4 | Dasy Data Acquisition Electronics | 11/11/2021 | Annual | 11/11/2022 | 1646 |
| SPEAG | EX3DV4 | SAR Probe | 4/22/2022 | Annual | 4/22/2023 | 7546 |
| SPEAG | EX3DV4 | SAR Probe | 11/16/2021 | Annual | 11/16/2022 | 7639 |

Note: CBT (Calibrated Before Testing). Prior to testing, the measurement paths containing a cable, amplifier, attenuator, coupler or filter were connected to a calibrated source (i.e. a signal generator) to determine the losses of the measurement path. The power meter offset was then adjusted to compensate for the measurement system losses. This level offset is stored within the power meter before measurements are made. This calibration verification procedure applies to the system verification and output power measurements. The calibrated reading is then taken directly from the power meter after compensation of the losses for all final power measurements.

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## 12 MEASUREMENT UNCERTAINTIES

| a | b | c | d | $\mathrm{e}=$ <br> $\mathrm{f}(\mathrm{d}, \mathrm{k})$ | f | g | $\begin{aligned} & h= \\ & c \times f / e \end{aligned}$ | $\mathrm{i}=$ <br> cxg/e | k |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Uncertainty Component | $\begin{aligned} & \text { IEEE } \\ & 1528 \\ & \text { Sec. } \end{aligned}$ | Tol. $( \pm \%)$ | Prob. <br> Dist. | Div. | $\begin{gathered} c_{i} \\ 1 \mathrm{gm} \end{gathered}$ | $\mathrm{C}_{\mathrm{i}}$ <br> 10 gms | $\begin{gathered} 1 \mathrm{gm} \\ \mathrm{u}_{\mathrm{i}} \\ ( \pm \%) \end{gathered}$ | 10 gms <br> $\mathrm{u}_{\mathrm{i}}$ <br> ( $\pm$ \%) | $\mathrm{v}_{\mathrm{i}}$ |
| Measurement System |  |  |  |  |  |  |  |  |  |
| Probe Calibration | E.2.1 | 7 | N | 1 | 1 | 1 | 7.0 | 7.0 | $\infty$ |
| Axial Isotropy | E.2.2 | 0.25 | N | 1 | 0.7 | 0.7 | 0.2 | 0.2 | $\infty$ |
| Hemishperical Isotropy | E.2.2 | 1.3 | N | 1 | 0.7 | 0.7 | 0.9 | 0.9 | $\infty$ |
| Boundary Effect | E.2.3 | 2 | R | 1.732 | 1 | 1 | 1.2 | 1.2 | $\infty$ |
| Linearity | E.2.4 | 0.3 | N | 1 | 1 | 1 | 0.3 | 0.3 | $\infty$ |
| System Detection Limits | E.2.4 | 0.25 | R | 1.732 | 1 | 1 | 0.1 | 0.1 | $\infty$ |
| Modulation Response | E.2.5 | 4.8 | R | 1.732 | 1 | 1 | 2.8 | 2.8 | $\infty$ |
| Readout Electronics | E.2.6 | 0.3 | N | 1 | 1 | 1 | 0.3 | 0.3 | $\infty$ |
| Response Time | E.2.7 | 0.8 | R | 1.732 | 1 | 1 | 0.5 | 0.5 | $\infty$ |
| Integration Time | E.2.8 | 2.6 | R | 1.732 | 1 | 1 | 1.5 | 1.5 | $\infty$ |
| RF Ambient Conditions - Noise | E.6.1 | 3 | R | 1.732 | 1 | 1 | 1.7 | 1.7 | $\infty$ |
| RF Ambient Conditions - Reflections | E.6.1 | 3 | R | 1.732 | 1 | 1 | 1.7 | 1.7 | $\infty$ |
| Probe Positioner Mechanical Tolerance | E.6.2 | 0.8 | R | 1.732 | 1 | 1 | 0.5 | 0.5 | $\infty$ |
| Probe Positioning w/ respect to Phantom | E.6.3 | 6.7 | R | 1.732 | 1 | 1 | 3.9 | 3.9 | $\infty$ |
| Extrapolation, Interpolation \& Integration algorithms for Max. SAR Evaluation | E. 5 | 4 | R | 1.732 | 1 | 1 | 2.3 | 2.3 | $\infty$ |
| Test Sample Related |  |  |  |  |  |  |  |  |  |
| Test Sample Positioning | E.4.2 | 3.12 | N | 1 | 1 | 1 | 3.1 | 3.1 | 35 |
| Device Holder Uncertainty | E.4.1 | 1.67 | N | 1 | 1 | 1 | 1.7 | 1.7 | 5 |
| Output Power Variation - SAR drift measurement | E. 2.9 | 5 | R | 1.732 | 1 | 1 | 2.9 | 2.9 | $\infty$ |
| SAR Scaling | E.6.5 | 0 | R | 1.732 | 1 | 1 | 0.0 | 0.0 | $\infty$ |
| Phantom \& Tissue Parameters |  |  |  |  |  |  |  |  |  |
| Phantom Uncertainty (Shape \& Thickness tolerances) | E.3.1 | 7.6 | R | 1.73 | 1.0 | 1.0 | 4.4 | 4.4 | $\infty$ |
| Liquid Conductivity - measurement uncertainty | E.3.3 | 4.3 | N | 1 | 0.78 | 0.71 | 3.3 | 3.0 | 76 |
| Liquid Permittivity - measurement uncertainty | E.3.3 | 4.2 | N | 1 | 0.23 | 0.26 | 1.0 | 1.1 | 75 |
| Liquid Conductivity - Temperature Uncertainty | E.3.4 | 3.4 | R | 1.732 | 0.78 | 0.71 | 1.5 | 1.4 | $\infty$ |
| Liquid Permittivity - Temperature Unceritainty | E.3.4 | 0.6 | R | 1.732 | 0.23 | 0.26 | 0.1 | 0.1 | $\infty$ |
| Liquid Conductivity - deviation from target values | E.3.2 | 5.0 | R | 1.73 | 0.64 | 0.43 | 1.8 | 1.2 | $\infty$ |
| Liquid Permittivity - deviation from target values | E.3.2 | 5.0 | R | 1.73 | 0.60 | 0.49 | 1.7 | 1.4 | ${ }^{\infty}$ |
| Combined Standard Uncertainty (k=1) |  |  | RSS |  |  |  | 12.2 | 12.0 | 191 |
| Expanded Uncertainty $\mathrm{k}=2$ <br> (95\% CONFIDENCE LEVEL) |  |  |  |  |  |  | 24.4 | 24.0 |  |

The above measurement uncertainties are according to IEEE Std. 1528-2013

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## 13 CONCLUSION

### 13.1 Measurement Conclusion

The SAR evaluation indicates that the EUT complies with the RF radiation exposure limits of the FCC and Innovation, Science, and Economic Development Canada, with respect to all parameters subject to this test. These measurements were taken to simulate the RF effects of RF exposure under worst-case conditions. Precise laboratory measures were taken to assure repeatability of the tests. The results and statements relate only to the item(s) tested.

Please note that the absorption and distribution of electromagnetic energy in the body are very complex phenomena that depend on the mass, shape, and size of the body, the orientation of the body with respect to the field vectors, and the electrical properties of both the body and the environment. Other variables that may play a substantial role in possible biological effects are those that characterize the environment (e.g. ambient temperature, air velocity, relative humidity, and body insulation) and those that characterize the individual (e.g. age, gender, activity level, debilitation, or disease). Because various factors may interact with one another to vary the specific biological outcome of an exposure to electromagnetic fields, any protection guide should consider maximal amplification of biological effects as a result of field-body interactions, environmental conditions, and physiological variables. [3]

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