Specific Absorption Rate (SAR) Test Report

for **ZyXEL Communications Corporation** on the 11Mbps Wireless USB Stick Model Number: ZyAIR B-220

> Test Report: EME-030565 Date of Report: June 10, 2003 Date of test: May 15, 2003

Total No of Pages Contained in this Report: 66



0597 ILAC MRA

Accredited for testing to FCC Part 15						
Tested by:	Kevin Chen	Kein Chin				
Reviewed by:	Elton Chen	At Key				

Review Date: June 18, 2003

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STATEMENT OF COMPLIANCE

The ZyXEL sample device, model # ZyAIR B-220 was evaluated in accordance with the requirements for compliance testing defined in FCC OET Bulletin 65, Supplement C (Edition 01-01). Testing was performed at the Intertek Testing Services facility in Hsinchu, Taiwan.

For the evaluation, the dosimetric assessment system INDEXSAR SARA2 was used. The phantom employed was the box phantom of 2mm thick in one wall. The total uncertainty for the evaluation of the spatial peak SAR values averaged over a cube of 1g tissue mass had been assessed for this system to be $\pm 27.5\%$.

The device was tested at their maximum output power declared by the ZyXEL

In summary, the maximum spatial peak SAR value for the sample device averaged over 1g was found to be:

Phantom	Position	SAR _{1g} , mW/g
	The EUT inserted into the left	
2mm thick box phantom	side of notebook PC, with	0.652 mW/a
wall	EUT bottom touching the	0.032 mW/g.
	phantom.	

In conclusion, the tested Sample device was found to be in compliance with the requirements defined in OET Bulletin 65, Supplement C (Edition 01-01) for body configurations.



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1.0 JOB DESCRIPTION

1.1 Client Information

The ZyAIR B-220 has been tested at the request of:

Company: ZyXEL Communications Corporation No. 6, Innovation Rd II, Science-Based Industrial Park, Hsin-Chu, Taiwan

1.2 Equipment under test (EUT)

Product Descriptions:

Equipment	11Mbps Wireless USB Stick		
Trade Name	ZyXEL	Model No:	ZyAIR B-220
FCC ID	I88B220	S/N No.	Not Labeled
Category	Portable	RF Exposure	Uncontrolled Environment
Frequency Band	2412 – 2462 MHz	System	DSSS

EUT Antenna Description							
TypeCeramic antennaConfigurationFixed							
Dimensions	30 x 93mm	Gain	-3 dBi				
Location	Location Embedded						

Note: The serial models, Lantech WL-555, Lantech 8800-555, B-220, Telefonica B-220 are identical to the basic model, 11Mbps Wireless USB Stick, for marketing purpose only.

Use of Product :	Wireless Data Communication
Manufacturer:	ZyXEL Communications Corporation
Production is planned:	[X] Yes, [] No
EUT receive date:	May 8, 2003
EUT received condition:	Good operating condition prototype.
Test start date:	May 15, 2003
Test end date:	May 15, 2003



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1.3 Test plan reference

FCC Rule: Part 2.1093, FCC's OET Bulletin 65, Supplement C (Edition 01-01)

- 1.4 System test configuration
- 1.4.1 System block diagram & Support equipment

Support Equipment							
Item #	Item # Equipment Model No. S/N						
1	hp Laptop Computer	XE ₃	TW20705468				





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1.4.3 Test Condition

During tests the worst-case data (max RF coupling) was determined with following conditions:

Usage	Operates with a portable computer	Distance between antenna axis at the joint and the liquid surface:	Laptop is touching the Phantom bottom position	
Simulating human Head/ Body/Hand	Body	EUT Battery	Device is powered from host computer through battery.	
Conducted	Channel	Frequency MHz	Before SAR Test (dBm)	After SAR Test (dBm)
output Power	Low Channel - 1	2412	17.85	17.81
	Mid Channel - 6	2437	17.74	17.73
	High Channel- 11	2462	17.88	17.89

The spatial peak SAR values were assessed for lowest, middle and highest operating channels, defined by the manufacturer.

The conducted output power was measured before and after the test using an average power meter.

Plug the EUT into notebook, and turn on the power, then run the test program "ZDGonfig" under Windows OS.

The EUT was transmitted continuously during the test.

1.5 Modifications required for compliance

Intertek Testing Services implemented no modifications.

1.6 Additions, deviations and exclusions from standards

The phantom employed was the box phantom of 2mm thick in vertical wall.



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2.0 SAR EVALUATION

2.1 SAR Limits

The following FCC limits for SAR apply to devices operate in General Population/Uncontrolled Exposure environment:

EXPOSURE	SAR
(General Population/Uncontrolled Exposure environment)	(W/kg)
Average over the whole body	0.08
Spatial Peak (1g)	1.60
Spatial Peak for hands, wrists, feet and ankles (10g)	4.00



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2.2 Configuration Photographs

SAR Measurement Test Setup

Test System





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SAR Measurement Test Setup

Bottom side of Laptop facing phantom touching



Bottom side of Laptop facing phantom touching – Zoom In





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SAR Measurement Test Setup EUT perpendicular to phantom, 15 mm separation

EUT perpendicular to phantom, 15 mm separation – Zoom In





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SAR Measurement Test Setup EUT perpendicular to phantom, 0 mm separation



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2.3 SAR measurement system

Robot system specification

The SAR measurement system being used is the IndexSAR SARA2 system, which consists of a Mitsubishi RV-E2 6-axis robot arm and controller, IndexSAR probe and amplifier and SAM phantom Head Shape. The robot is used to articulate the probe to programmed positions inside the phantom head to obtain the SAR readings from the DUT.

The system is controlled remotely from a PC, which contains the software to control the robot and data acquisition equipment. The software also displays the data obtained from test scans.



Figure 1: Schematic diagram of the SAR measurement system

The position and digitised shape of the phantom heads are made available to the software for accurate positioning of the probe and reduction of set-up time.

The SAM phantom heads are individually digitised using a Mitutoyo CMM machine to a precision of 0.02mm. The data is then converted into a shape format for the software, providing an accurate description of the phantom shell.

In operation, the system first does an area (2D) scan at a fixed depth within the liquid from the inside wall of the phantom. When the maximum SAR point has been found, the system will then carry out a 3D scan centred at that point to determine volume averaged SAR level.



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2.4 SAR measurement system validation

Prior to the assessment, the system was verified to the $\pm 10\%$ of the specifications by using the system validation equipments. The validation was performed at 2450 MHz on the bottom side of box phantom.

Procedures

The SAR evaluation was performed with the following procedures:

- a. The SAR distribution was measured at the exposed side of the bottom of the box phantom and was measured at a distance of 8 mm from the inner surface of the shell. The feed power was 1/4W.
- b. The dimension for this cube is 32 mm x 32 mm x 34 mm was assessed by measuring 5 x 5 x 7 points. On the basis of this data set, the spatial peak SAR value was evaluated with the following procedure:
 - i) The data at the surface were extrapolated, since the center of the dipoles is 3 mm away from the tip of the probe and the distance between the surface and the lowest measurement point is 5 mm. The extrapolation was based on a least square algorithm. A polynomial of the fourth order was calculated through the points in Z-axes. This polynomial was then used to evaluate the points between the surface and the probe tip.
 - ii) The maximum interpolated value was searched with a straightforward algorithm. Around this maximum, the SAR values averaged over the spatial volumes (1g or 10g) were computed using the 3-D spline interpolation algorithm. The 3-D spline is composed of three one-dimensional splines with the "Not a knot" condition (in x, y and z directions). The volume was integrated with the trapezoidal algorithm. 1000 points (10 x 10 x 10) were interpolated to calculate the average.
 - iii) All neighboring volumes were evaluated until no neighboring volume with a higher average value was found.

System Validation (2450 MHz Head)						
Frequency MHzOperating ModeTarget SAR1g (mW/g)Measured SAR1g (mW/g)Deviation (±10%)Plot Numb						
2450	CW	52.4	50.16	-5.92%	7	



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Test Results

The results on the following page(s) were obtained when the device was tested in the condition described in this report. Detailed measurement data and plots, which reveal information about the location of the maximum SAR with respect to the device, are reported in Appendix A.



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System performance check (2450 MHz Head)							
Frequency	Frequency Operating Target SAR _{1g} Measured SAR _{1g} Deviation Plot Number						
MHZ	Mode	(mw/g)	(mw/g)	(±10%)			
2450	CW	52.4	53.928	2.92%	8		

Note: a) Worst case data were reported b) Uncertainty of the system is not included



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Measurement Results

Trade Name:	ZyXEL		M	odel No.:	ZyAIR B-220	0
Serial No.:	Not Labl	ed Test Engineer:		Kevin Chen		
TEST CONDITIONS						
Ambient Temperature		23.3 °C		Relative Humidity		50 %
Test Signal Source		Test Mode		Signal Modulation		DSSS
Output Power Before		See page 7		Output Power After SAR		See page 7
SAR Test				Test		
Test Duration		22 min. each scar	n	Number of Battery Change		1

EUT Position								
Channel (MHz)	Operating Mode	Crest Factor	Description	Distance (mm)	Measured SAR _{1g} (mW/g)	Plot Number		
2437	DSSS	1	Bottom of NoteBook PC	0	0.506	1		
2412	DSSS	1	Bottom of NoteBook PC	0	0.652	2		
2462	DSSS	1	Bottom of Note Book PC	0	0.533	3		
2437	DSSS	1	Perpendicular to phantom	0	0.062	4		
2412	DSSS	1	Perpendicular to phantom	0	0.103	5		
2462	DSSS	1	Perpendicular to phantom	0	0.099	6		
2437	DSSS	1	Perpendicular to phantom	15	Note	9		
2412	DSSS	1	Perpendicular to phantom	15	Note	10		
2462	DSSS	1	Perpendicular to phantom	15	Note	11		

Note: The measurement was only performed in Area Scan due to scanning system couldn't continue performing Zoom Scan with such a low SAR distribution.



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TEST EQUIPMENT

3.1 Equipment List

The Specific Absorption Rate (SAR) tests were performed with the INDEXSAR SARA2 SYSTEM.

The following major	equipment/components were used for the SAR e	evaluations:					
	SAR Measurement System	1					
EQUIPMENT	SPECIFICATIONS	S/N #	LAST CAL. DATE				
Balanced Validation dipole	2450MHz	0048	Mar. 26, 2003				
Robot	Mitsubishi RV-E2	EA009002	N/A				
	Repeatability: ± 0.04mm; Number of Axes: 6						
E-Field Probe	IXP-050	0114	09/06/2002				
	Frequency Range: Probe outer diameter: 5 mm the probe tip and the dipole center: 3 mm	n; Length: 350 m	m; Distance between				
Data Acquisition	SARA2	N/A	N/A				
	Processor: Pentium 4; Clock speed: 1.5GHz; OS: Windows XP; I/O: two RS232; Software: SARA2 ver. 0.401N;						
Phantom	2mm wall thickness box phantom	N/A	N/A				
	Shell Material: clear Perspex; Thickness: $2 \pm x L x D$) mm ³ ; Dielectric constant: less than 2	0.1 mm; Capacity 2.85 above 500MH	r: 154 x 200 x 200 (W Hz;				
Device holder	Material: clear Perspex; Dielectric constant: less than 2.85 above 500MHz	N/A	N/A				
Simulated Tissue	Mixture	N/A	N/A				
	Please see section 3.2 for details						
RF	Boonton 4231A with 51011-EMC power sensor	79401-32482	03/21/2003				
Power Meter	Frequency Range: 0.03 to 8 GHz, <24dBm						
RF	INDEXSAR VTL5400	0302	01/23/2003				
Power Amplifier	10MHz to 2.5GHz, Gain >30dB						
Directional	INDEXSAR VDC0830-20	0302	05/19/2003				
Coupler	0.8 to 3 GHz, Max. Power<500W						
Vector Network Analyzer	HP 8753B HP 85046A	2807J04037 2729A01958	12/13/2002				
	300k to 3GHz						
Signal Generator	Rohde & Schwarz SMR27	1104.0002.27	08/16/2002				
	10M to 27GHz, <120dBuV						



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3.2 Body Tissue Simulating Liquid for evaluation test

Body Ingredients Frequency (2.45 GHz)						
DGBE Dilethylene Glycol Butyl Ether	26.7%					
Salt	0.04%					
Water	73.2%					

The dielectric parameters were verified prior to assessment using the HP 85046A dielectric probe kit and the HP 8753B network Analyzer. The dielectric parameters were:

Frequency (MHz)	Temp. (℃)	e _r / Relat	ive Perm	ittivity	s / Condu	r *(kg/m ³)		
2450	22.1	measured	target	$\Delta(\pm 5\%)$	measured	target	$\Delta(\pm 5\%)$	1000
2450	23.1	50.76	52.7	-3.68%	1.897	1.95	-2.72%	1000

* Worst-case assumption

Test data is included in Appendix B.

Head Tissue Simulating Liquid for System performance Check test

Head Ingredients Frequency (2.45 GHz)						
DGBE Dilethylene Glycol	53.3%					
Water	46.7%					

The dielectric parameters were verified prior to assessment using the HP 85046A dielectric probe kit and the HP 8753B network Analyzer. The dielectric parameters were:

Frequency (MHz)	Тетр. (°С)	e _r / Relat i	ive Perm	ittivity	s / Conductivity (mho/m)			r *(kg/m ³)
2450	22.1	measured	target	$\Delta(\pm 5\%)$	measured	target	$\Delta(\pm 5\%)$	1000
2450	23.1	38.221	39.2	-2.5%	1.88	1.80	4.44%	1000

* Worst-case assumption



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3.3 E-Field Probe Calibration

Probe calibration factors are included in Appendix C.



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3.4 Measurement Uncertainty

The uncertainty budget has been determined for the INDEXSAR SARA2 measurement system according to IEEE P1528 documents [3] and is given in the following table. The extended uncertainty (95% confidence level) was assessed to be 27.5 %

Uncertainty Component	Sec.	(dB)	Tol.(+/-)	(%)	Prob. Dist.	Divisor (descript)	Divisor (value)	c1	Standard Uncertainty (%)	
Measurement System										
Probe Calibration	E 1.1			10	Ν	1 or k	2	1	5.00	25.00
Axial Isotropy	E 1.2	0.25	5.93	5.93	R	√3	1.73	0	0.00	0.00
Hemispherical Isotropy	E 1.2	0.45	10.92	10.92	R	√3	1.73	1	6.30	39.73
Boundary effects	E 1.3		4	4.00	R	√3	1.73	1	2.31	5.33
Linearity	E 1.4	0.04	0.93	0.93	R	√3	1.73	1	0.53	0.29
System Detection Limits	E 1.5		1	1.00	R	√3	1.73	1	0.58	0.33
Readout Electronics	E 1.6		1	1.00	Ν	1 or k	1.73	1	1.00	1.00
Response time	E 1.7		0	0.00	R	√3	1.73	1	0.00	0.00
Integration time	E 1.8		1.8	1.80	R	√3	1.73	1	1.04	1.08
RF Ambient Conditions	E 5.1		3	3.00	R	√3	1.73	1	1.73	3.00
Probe Positioner Mechanical Tolerance	E 5.2		0.6	0.60	R	√3	1.73	1	0.35	0.12
Probe Position wrt. Phantom Shell	E 5.3		5	5.00	R	√3	1.73	1	2.89	8.33
SAR Evaluation Algorithms	E 4.2		8	8.00	R	√3	1.73	1	4.62	21.33
Test Sample Related										
Test Sample Positioning	E 3.2.1		10	10.00	R	√3	1.73	1	5.77	33.33
Device Holder Uncertainty	E 3.1.1		10	10.00	R	√3	1.73	1	5.77	33.33
Output Power Variation	E 5.6.2		5	4.00	R	√3	1.73	0.5	2.89	8.33
Phantom and tissue Parameters										
Phantom Uncertainty (shape and thickness)	E 2.1		4	4.00	R	√3	1.73	0.5	1.15	1.33
Liquid conductivity (Deviation from target)	E 2.2		5	5.00	R	√3	1.73	0.5	1.44	2.08
Liquid conductivity (Meas. Uncertainty)	E 2.2		10	10.00	R	√3	1.73	0.5	2.89	8.33
Combined standard uncertainty					RSS		14.0			



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3.5 Measurement Traceability

All measurements described in this report are traceable to Chinese National Laboratory Accreditation (CNLA) standards or appropriate national standards.



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4.0 WARNING LABEL INFORMATION - USA

See user manual.



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5.0 REFERENCES

- [1] ANSI, ANSI/IEEE C95.1-1991: IEEE Standard for Safety Levels with Respect to Human Exposure to Radio Frequency Electromagnetic Fields, 3kHz to 300 GHz, The Institute of electrical and Electronics Engineers, Inc., New York, NY 10017, 1992
- [2] Federal Communications Commission, "Evaluating Compliance with FCC Guidelines for Human Exposure to Radiofrequency Electromagnetic Fields", OET Bulletin 65, FCC, Washington, D.C. 20554, 1997

[3] IEEE Standards Coordinating Committee 34, "*DRAFT* Recommended Practice for Determining the Peak Spatial-Average Specific Absorption Rate (SAR) in the Human Body Due to Wireless Communications Devices: Experimental Techniques", IEEE Std 1528-200X, Draft CD 1.0 – September 15, 2002



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6.0 DOCUMENT HISTORY

Revision/ Job Number	Writer Initials	Date	Change
TC0300445	J.C.	June 10, 2003	Original document



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APPENDIX A - SAR Evaluation Data

Power drift is the measurement of power drift of the device over one complete SAR scan. To assess the drift of the power of the device under test, a SAR measurement was made in the middle of the zoom scan volume at the start of the scan and a measurement at this point was then also made after the measurement scan. The difference between the two measurements should be less than 5%.

FCC ID. : I88B220

Plot #1 (1/2)

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Date / Time:	2003/5/15	Position:	bottom 0mm
Filename:	B-220 bot2437.txt	Phantom:	HeadBox1.csv
Device Tested:	ZyAIR B-220	Head Rotation:	0
Antenna:	Ceramic	Test Frequency:	2437MHz
Shape File:	B-220 bottom(HP NB)-1.csv	Power Level:	17.74dBm

Probe:	0114			
Cal File:	SN0114	_2450_	CW_BO	DY
		X	Y	Z
	Air	532	494	450
Cal Factors:	DCP	20	20	20
	Lin	.528	.528	.528
Amp Gain:	2			
Averaging:	1			
Batteries	M. 15			
Replaced:	May 15			
-				





Plot #1 (2/2)

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Date / Time:	2003/5/15	Position:	bottom 0mm
Filename:	B-220 bot2437.txt	Phantom:	HeadBox1.csv
Device Tested:	ZyAIR B-220	Head Rotation:	0
Antenna:	Ceramic	Test Frequency:	2437MHz
Shape File:	B-220 bottom(HP NB)-1.csv	Power Level:	17.74dBm

AREA SCAN:

		Min	Max	Steps
Scan Extent:				
Scan Extent.	Y	-20.0	20.0	4.0
	Ζ	-180.0	-120.0	6.0



FCC ID. : I88B220

Plot #2 (1/2)

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Date / Time:	2003/5/15	Position:	bottom 0mm
Filename:	B-220 bot2412.txt	Phantom:	HeadBox1.csv
Device Tested:	ZyAIR B-220	Head Rotation:	0
Antenna:	Ceramic	Test Frequency:	2412MHz
Shape File:	B-220 bottom(HP NB)-1.csv	Power Level:	17.85dBm

Probe:	0114			
Cal File:	SN0114	_2450_	CW_BO	DY
		X	Y	Z
	Air	532	494	450
Cal Factors:	DCP	20	20	20
	Lin	.528	.528	.528
Amp Gain:	2	L		
Averaging:	1			
Batteries	Mar. 15			
Replaced:	May 15			





plot #2 (2/2)

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Date / Time:	2003/5/15	Position:	bottom 0mm
Filename:	B-220 bot2412.txt	Phantom:	HeadBox1.csv
Device Tested:	ZyAIR B-220	Head Rotation:	0
Antenna:	Ceramic	Test Frequency:	2412MHz
Shape File:	B-220 bottom(HP NB)-1.csv	Power Level:	17.85dBm
Antenna: Shape File:	Ceramic B-220 bottom(HP NB)-1.csv	Test Frequency: Power Level:	2412MHz 17.85dBm

AREA SCAN:

		Min	Max	Steps
Scan Extant:				
Scan Extent.	Y	-20.0	20.0	4.0
	Ζ	-170.0	-100.0	7.0



FCC ID. : I88B220

plot #3 (1/2)

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Date / Time:	2003/5/15	Position:	bottom 0mm
Filename:	B-220 bot2462.txt	Phantom:	HeadBox1.csv
Device Tested:	ZyAIR B-220	Head Rotation:	0
Antenna:	Ceramic	Test Frequency:	2462MHz
Shape File:	B-220 bottom(HP NB)-1.csv	Power Level:	17.88dBm

Probe:	0114			
Cal File:	SN0114	_2450_0	CW_BO	DY
		X	Y	Z
	Air	532	494	450
Cal Factors:	DCP	20	20	20
	Lin	.528	.528	.528
Amp Gain:	2			
Averaging:	1			
Batteries	More 15			
Replaced:	May 15			





plot #3 (2/2)

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Date / Time:	2003/5/15	Position:	bottom 0mm
Filename:	B-220 bot2462.txt	Phantom:	HeadBox1.csv
Device Tested:	ZyAIR B-220	Head Rotation:	0
Antenna:	Ceramic	Test Frequency:	2462MHz
Shape File:	B-220 bottom(HP NB)-1.csv	Power Level:	17.88dBm
_			

AREA SCAN:

		Min	Max	Steps
Scan Extent:	Y	-20.0	20.0	4.0
	Ζ	-180.0	-120.0	6.0



FCC ID. : I88B220

plot #4 (1/2)

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Date / Time:	2003/5/15	Position:	perpendicular 0mm
Filename:	B-220_per2437.txt	Phantom:	HeadBox1.csv
Device Tested:	ZyAIR B-220	Head Rotation:	0
Antenna:	Ceramic	Test Frequency:	2437MHz
Shape File:	B-220 perpendicular(HP NB).csv	Power Level:	17.74dBm

Probe:	0114			
Cal File:	SN0114	_2450_	CW_BO	DY
		X	Y	Z
	Air	532	494	450
Cal Factors:	DCP	20	20	20
	Lin	.528	.528	.528
Amp Gain:	2			
Averaging:	1			
Batteries	Mov 15			
Replaced:	May 15			





plot #4 (2/2)

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Date / Time:	2003/5/15	Position:	perpendicular 0mm
Filename:	B-220_per2437.txt	Phantom:	HeadBox1.csv
Device Tested:	ZyAIR B-220	Head Rotation:	0
Antenna:	Ceramic	Test Frequency:	2437MHz
Shape File:	B-220 perpendicular(HP NB).csv	Power Level:	17.74dBm

AREA SCAN:

		Min	Max	Steps
Scan Extent:				
Seun Extent.	Y	-30.0	30.0	6.0
	Ζ	-190.0	-140.0	6.0



FCC ID. : I88B220

plot #5 (1/2)

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Date / Time:	2003/5/15	Position:	perpendicular 0mm
Filename:	B-220_per2412.txt	Phantom:	HeadBox1.csv
Device Tested:	ZyAIR B-220	Head Rotation:	0
Antenna:	Ceramic	Test Frequency:	2412MHz
Shape File:	B-220 perpendicular(HP NB).csv	Power Level:	17.85dBm

Cal File:SN0114_2450_CW_BODYType:X <yz< td="">Conductivity:Air532494450Relative Permittivity:</yz<>
XYZConductivity:Air532494450Relative Permittivity:
Air 532 494 450 Relative Permittivity:
Cal Factors:DCP202020ILiquid Temp (deg C):
Lin .528 .528 .528 Ambient Temp (deg C):
Amp Gain: 2 Ambient RH (%):
Averaging: 1 Density (kg/m3):
Batteries Software Version:
Replaced: May 15 Crest Factor=1





plot #5 (2/2)

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Date / Time:	2003/5/15	Position:	perpendicular 0mm
Filename:	B-220_per2412.txt	Phantom:	HeadBox1.csv
Device Tested:	ZyAIR B-220	Head Rotation:	0
Antenna:	Ceramic	Test Frequency:	2412MHz
Shape File:	B-220 perpendicular(HP NB).csv	Power Level:	17.85dBm

AREA SCAN:

		Min	Max	Steps
Scan Extent:		20.0	20.0	C 0
	Y	-30.0	30.0	6.0
	Ζ	-190.0	-140.0	6.0



FCC ID. : I88B220

plot #6 (1/2)

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Date / Time:	2003/5/15	Position:	perpendicular 0mm
Filename:	B-220_per2462.txt	Phantom:	HeadBox1.csv
Device Tested:	ZyAIR B-220	Head Rotation:	0
Antenna:	Ceramic	Test Frequency:	2462MHz
Shape File:	B-220 perpendicular(HP NB).csv	Power Level:	17.88dBm

Probe:	0114			
Cal File:	SN0114	_2450_	CW_BO	DY
		X	Y	Z
	Air	532	494	450
Cal Factors:	DCP	20	20	20
	Lin	.528	.528	.528
Amp Gain:	2			
Averaging:	1			
Batteries	Mov 15			
Replaced:	May 15			





plot #6 (2/2)

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Date / Time:	2003/5/15	Position:	perpendicular 0mm
Filename:	B-220_per2462.txt	Phantom:	HeadBox1.csv
Device Tested:	ZyAIR B-220	Head Rotation:	0
Antenna:	Ceramic	Test Frequency:	2462MHz
Shape File:	B-220 perpendicular(HP NB).csv	Power Level:	17.88dBm

AREA SCAN:

		Min	Max	Steps
Scan Extent:				
	Y	-30.0	30.0	6.0
	Ζ	-190.0	-140.0	6.0



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Plot #7

Date:	2003	3/3/7		
Filename:	2450)val5-15	.txt	
Device Tested:	SAR	A2 syst	em	
Antenna:	2450	Odipole		
Shape File:	none	e.csv		
	0111			
Probe:	0114			
Cal File:	SN0114	_2450_	CW_HE	AD
		X	Y	Ζ
Cal Factors:	Air	532	494	450
Call'actors.	DCP	20	20	20
	Lin	.495	.495	.495
Amp Gain:	2			
Averaging:	1			
Batteries	N/a			
Replaced:				



ZOOM SCAN RESULTS:

Spot SAR	Start Sca	n Ei	nd Scan	
(W/kg):				
Change during				
Scan (%)				
Max E-field (V/m):	76.31			
	1g		10g	
Max SAK (W/Kg)	12.54		6.23	
Location of Max	X	Y	Z	
(mm):	1.5	1.2	-220.0	

Normalized to an input power of 1W Averaged over 1 cm³ (1g) of tissue **50.16 W/kg**

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Plot #8

Date / Time:	2003/5/15	Position:	bottom of box phantom
Filename:	2450 performance check	Phantom:	HeadBox1.csv
Device Tested:	SARA2 system	Head Rotation:	0
Antenna:	2.45GHz dipole	Test Frequency:	2450MHz
Shape File:	Dipole2450.csv	Power Level:	24 dBm /CW

Probe:	0114				
Cal File:	SN0114_2450_CW_HEAD				
		X	Y	Z	
Cal Eastana	Air	532	494	450	
Cal Factors:	DCP	20	20	20	
	Lin	.495	.495	.495	
Amp Gain:	2				
Averaging:	3				
Batteries Replaced:	-				

Liquid:	15.2cm
Туре:	2450MHz head
Conductivity:	1.882
Relative Permittivity:	38.952
Liquid Temp (deg C):	23.1
Ambient Temp (deg C):	22.5
Ambient RH (%):	60
Density (kg/m3):	1000
Software Version:	0.421N
Crest factor $= 1$	



ZOOM SCAN RESULTS:

Spot SAR	Start So	can	En	d Scan
(W/kg):				
Change during				
Scan (%)				
Max E-field (V/m):	73.42			
Moy SAD (W/leg)	1g			10g
Max SAR (W/Kg)	13.482		6.255	
Location of Max	X	Y		Ζ
(mm):	0.0	0.0		-220.5

Normalized to an input power of 1W Averaged over 1 cm³ (1g) of tissue 53.928 W/kg

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<u>plot</u> #9								C
Date / Time:	2003	3/5/15			Pos	ition:	perpendic	cular 15mm
Filename:	ZyA	IR B-22	20a 2437	for	Pha	ntom:	HeadBox	1.csv
Device Tested:	15m ZyA	15mm per.a.txt ZyAIR B-220		Hea	d Rotation:	0		
Antenna:	Cera	amic			Tes	t Frequency:	2437MHz	Z
Shape File:	B-22	20 perpe	ndicular	(HP	Pov	ver Level:	17.74dBn	n
	NB)	.CSV						
Probe:	0114					quid:		15.3cm
Cal File:	SN0114	_2450_	CW_BC	DY	Ty	pe:		2450MHz body
		X	Y	Z	Co	onductivity:		1.89659
	Air	532	494	450	Re	lative Permitti	ivity:	50.756798
Cal Factors:	DCP	20	20	20	Lie	quid Temp (de	eg C):	23.1
	Lin	.528	.528	.528	An	nbient Temp (deg C):	20
Amp Gain:	1				An	nbient RH (%)):	50
Averaging:	1				De	nsity (kg/m3):		1000
Batteries	Moy 15				So	ftware Version	1:	0.421N
Replaced:	way 15				Cre	est Factor=1		



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Replaced:

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Date / Time: 2003/5/15 Position: perpendicular 15mm Filename: ZyAIR B-220a 2412 for 15mm per.a.txt Phantom: HeadBox1.csv Device Tested: ZyAIR B-220 Head Rotation: 0 Image: Component of the component	plot #10								1 480 10 01
Filename:ZyAIR B-220a 2412 for 15mm per.a.txtPhantom:HeadBox1.csvDevice Tested:ZyAIR B-220Head Rotation:0Antenna:CeramicTest Frequency:2412MHzShape File:B-220 perpendicular(HP NB).csvPower Level:17.85dBmProbe:0114Liquid:15.3cmCal File:SN0114_2450_CW_BODYLiquid:1.89659Cal Factors:Air532494450 DCPDeveraging:1ZAmbient Temp (deg C):23.1Amp Gain:1Ambient RH (%):50Amp Gain:1IIIAveraging:1IIIBatteriesMm 15Mm 150.421N	Date / Time:	2003	3/5/15			Posit	tion:	perpendic	cular 15mm
Device Tested: $ZyAIR B-220$ Head Rotation: 0 Antenna: Ceramic Test Frequency: $2412MHz$ Shape File: $B-220$ perpendicular(HP NB).csv Power Level: $17.85dBm$ Probe: 0114 Liquid: $15.3cm$ Cal File: SN0114_2450_CW_BODY Liquid: $15.3cm$ Air 532 494 450 DCP 20 20 20 20 Liquid Temp (deg C): 23.1 Amp Gain: 1 Ambient Temp (deg C): 20 Amp Gain: 1 45 50 Batteries Mer 15 50 50	Filename:	ZyA 15m	IR B-22 m per.a.	0a 2412 txt	l for	Phar	ntom:	HeadBox	1.csv
Antenna: Ceramic Test Frequency: $2412MHz$ Shape File: B-220 perpendicular(HP NB).csv Power Level: $17.85dBm$ Probe: 0114 Image: Ceramic Single Si	Device Tested:	ZyA	IR B-22	0		Head	l Rotation:	0	
Shape File: B-220 perpendicular(HP NB).csv Power Level: $17.85dBm$ Probe: 0114 Image: Comparison of the	Antenna:	Cera	amic			Test	Frequency:	2412MH	Z
Probe: 0114 Liquid: 15.3cm Cal File: SN0114_2450_CW_BODY Z 2450MHz body Cal Factors: Air 532 494 450 Relative Permittivity: 50.756798 Cal Factors: Im .528 .528 .528 .528 .528 Amp Gain: 1 K K K K Z Amp Gain: 1 K K Solution Solution Solution Batteries Mm 15 Mm 15 K Solution Solution Solution	Shape File:	B-22 NB)	20 perpe .csv	ndicula	r(HP	Powe	er Level:	17.85dBr	n
Probe: 0114 Liquid: 15.3cm Cal File: SN0114_2450_CW_BODY Type: 2450MHz body Cal Factors: X Y Z Air 532 494 450 Relative Permittivity: 50.756798 DCP 20 20 20 20 20 20 Lin .528 .528 .528 .528 Ambient Temp (deg C): 23.1 Amp Gain: 1 Jack Jack Jack Jack Jack Jack Batteries Max 15 Max 15 Jack Jack Jack Jack Jack] [
Cal File: SN0114_2450_CW_BODY Type: 2450MHz body Cal Factors: X Y Z Relative Permittivity: 50.756798 Cal Factors: Air 532 494 450 Liquid Temp (deg C): 23.1 Amp Gain: 1 Ambient Temp (deg C): 20 20 Ambient RH (%): 50 Batteries Mm 15 Mm 15 Mm 15 Software Version: 0.421N	Probe:	0114				Liq	uid:		15.3cm
X Y Z Air 532 494 450 DCP 20 20 20 20 Lin .528 .528 .528 .528 Amp Gain: 1 .528 .528 .528 Batteries Mm 15 Mm 15 Software Version: 0.421N	Cal File:	SN0114	_2450_	CW_BC	DY	Typ	e:		2450MHz body
Air 532 494 450 DCP 20 20 20 Lin .528 .528 .528 Amp Gain: 1 .528 .528 Averaging: 1 .528 .528 Batteries Mm 15 .532 .532			X	Y	Z	Cor	nductivity:		1.89659
Cal Factors: DCP 20 20 20 20 Lin .528 .528 .528 .528 .528 .528 .528 .528 .528 .528 .528 .528 .528 .528 .528 .528 .500 Ambient Temp (deg C): 20 .50 Averaging: 1		Air	532	494	450	Rela	ative Permitt	ivity:	50.756798
Lin .528 .528 .528 .528 Ambient Temp (deg C): 20 Amp Gain: 1 .528 .528 .528 Density (kg/m3): 1000 Batteries Mm 15 Software Version: 0.421N	Cal Factors:	DCP	20	20	20	Liq	uid Temp (de	eg C):	23.1
Amp Gain: 1 Ambient RH (%): 50 Averaging: 1 Density (kg/m3): 1000 Batteries Max 15 Software Version: 0.421N		Lin	.528	.528	.528	Am	bient Temp (deg C):	20
Averaging:1Density (kg/m3):1000BatteriesMax 15Software Version:0.421N	Amp Gain:	1	1			Am	bient RH (%):	50
Batteries New 15 Oct 21N	Averaging:	1				Den	sity (kg/m3):		1000
- IVIAV 15	Batteries	May 15				Soft	tware Versio	n:	0.421N

Crest Factor=1



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plot #11								1 480 11 01
Date / Time:	2003	3/5/15				Position:	perpendic	cular 15mm
Filename:	ZyA	IR B-22	20a 2462	for		Phantom:	HeadBox	1.csv
Device Tested:	15m ZyA	m per.a. IR B-22	txt 20			Head Rotation:	0	
Antenna:	Cera	mic				Test Frequency:	2462MH	Z
Shape File:	B-22	20 perpe	ndicular	(HP		Power Level:	17.88dBr	n
	NB)	.csv						
					٦			
Probe:	0114					Liquid:		15.3cm
Cal File:	SN0114	_2450_0	CW_BO	DY		Туре:		2450MHz body
		X	Y	Z		Conductivity:		1.89659
	Air	532	494	450		Relative Permitti	ivity:	50.756798
Cal Factors:	DCP	20	20	20		Liquid Temp (de	eg C):	23.1
	Lin	.528	.528	.528		Ambient Temp (deg C):	20
Amp Gain:	1					Ambient RH (%)):	50
Averaging:	1					Density (kg/m3):		1000
Batteries	Mar. 15					Software Version	1:	0.421N
Replaced:	way 15					Crest Factor=1		





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APPENDIX B – 2450MHz body liquid Calibration Data



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Date	27 Mar 2003	Temperature	23.2°C	Tested by	Bruce
2400, 51.4561731074	4, -1.9042983162	•	2450, 51.5399962214	4, -1.9709742142	•
2401, 51.4618622908	8, -1.9074318666		2451, 51.5253820963	3, -1.9714888178	
2402, 51.4491455736	5, -1.9032053975		2452, 51.5138376197	7, -1.9712764191	
2403, 51.4597447905	5, -1.9053580588		2453, 51.506264452,	-1.9744307721	
2404, 51.47/33312, -	1.9024853703		2454, 51.4/9/118628	3, -1.9/81930314	
2405, 51.452108198	1, -1.9049122745		2455, 51.4815882983	5, -1.9809404159	
2400, 51.4004005099	9, -1.9024950108		2450, 51.481025547	1, -1.9825590219	
2407, 51.4027500203	1 0052446227		2457, 51.4050051570	5, -1.9623321603	
2400, 51.475080404,	3 1 0021558205		2458, 51.4090792740	0, -1.9042303434	
2409, 51.470485892	7 -1 9036953101		2460 51 426121960	1, -1.9034790903	
2410, 51.400415747	3 -1 90565/989/		2461 51 4433050331	, -1.9905052004	
2412 51 473792562	-1 9010364732		2462 51 4351797909	9 -1 991614928	
2413, 51,470333650	5 -1.9080418825		2463, 51 4192833694	4 -1.9926441596	
2414 51 4853170469	9 -1.9075814689		2464 51 3935248988	8 -1.9951662021	
2415, 51,477748072	11.9039314052		2465, 51,4067807362	21.9940377601	
2416, 51.497507792	1, -1.9081039443		2466, 51.3973497372	2, -1.9965390767	
2417, 51.4910256185	5, -1.9076696526		2467, 51.4035945152	2, -1.996413623	
2418, 51.4910256185	5, -1.9077555336		2468, 51.3752221594	4, -1.9983473438	
2419, 51.5205793847	7, -1.9110002928		2469, 51.3657334963	3, -2.0013612312	
2420, 51.5015907146	5, -1.9112969669		2470, 51.3821659658	3, -1.9975422712	
2421, 51.5186299965	5, -1.913333299		2471, 51.3494044323	3, -2.000827518	
2422, 51.5199444738	8, -1.9132995662		2472, 51.3316014489	9, -2.005838666	
2423, 51.5383678105	5, -1.9164616343		2473, 51.3302917020	5, -2.0041845906	
2424, 51.507022345,	-1.9159470284		2474, 51.327048332,	-2.0023612572	
2425, 51.5535636155	5, -1.9228209833		2475, 51.280946061	1, -2.0067604224	
2426, 51.5434783921	1, -1.9230193922		2476, 51.3079480027	7, -2.00626195	
2427, 51.556772906	/, -1.923435/151		24/7, 51.2992831/5	7, -2.0084/10545	
2428, 51.544032736	1, -1.9242282308		24/8, 51.2936112023	3, -2.0054399112	
2429, 51.545911510	1, -1.9284002105		24/9, 51.3011522/11	1, -2.0090308/19	
2430, 31.3469796726	5, -1.9264127959 1 1 0203015476		2480, 51.2650146701	1, -2.00/3936227 2.0088772501	
2431, 51.5506566555	1, -1.9293913470		2481, 51.254910415	2 2 0100721385	
2432, 51.549545492	+, -1.93++2/1/31		2482, 51.2475815108	1 -2 0088889846	
2434 51 5280836419	8 -1 9339312378		2483, 51.2577700005	7 -2.000000000000	
2435 51 5634320839	9 -1 938072836		2485 51 231906470	7 -2 0091094983	
2436. 51.5596101838	81.9410064722		2486, 51,241119396.	-2.0114765135	
2437. 51.519783227.	-1.9421099893		2487. 51.2241626656	52.0136195162	
2438, 51, 5708848449	91.9422852073		2488, 51,2399895297	72.0157126805	
2439, 51.5708848449	9, -1.9456341184		2489, 51.23507108, -	2.0150913632	
2440, 51.520244181,	-1.9474993194		2490, 51.2307133103	3, -2.0143129528	
2441, 51.545493223,	-1.9493233493		2491, 51.24467433, -	2.0083690716	
2442, 51.561983199	7, -1.9490242373		2492, 51.2165763995	5, -2.0189383173	
2443, 51.5688118794	4, -1.9535325295		2493, 51.2193393653	3, -2.0165741161	
2444, 51.53784239, -	-1.956085257		2494, 51.2198994488	3, -2.0185948185	
2445, 51.5581514210	6, -1.9585172362		2495, 51.2248156116	5, -2.0178354949	
2446, 51.5285668156	5, -1.9596063202		2496, 51.23616024, -	2.0181454203	
2447, 51.5383078584	4, -1.9614054013		2497, 51.2234992958	3, -2.0182098569	
2448, 51.5287890744	4, -1.9649943839		2498, 51.20/2/6331,	-2.0180287515	
2449, 51.5361/68938	8, -1.9651226896		2499, 51.21/993/402	2, -2.0181685351	
1			12500, 51.220831360.	52.0196352693	





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APPENDIX C - E-Field Probe Certificate and Calibration Data Validation dipole certificate and performance measurements





Report No.: EME-030565 Page 45 of 66 Indexsar Limited Oakfield House Cudworth Lane Newdigate Surrey RH5 5DR

Tel: +44 (0) 1306 631 233 Fax: +44 (0) 1306 631 834 e-mail: <u>enquiries@indexsar.com</u>

Calibration Certificate Dosimetric E-field Probe

Туре:	IXP-050
Manufacturer:	IndexSAR, UK
Serial Number:	0114
Place of Calibration:	IndexSAR UK

IndexSAR Limited hereby declares that the IXP-050 Probe named above has been calibrated for conformity to the IEEE 1528 and CENELEC En 50361 standards on the date shown below.

Date of Initial Calibration:

6th September 2002

The probe named above will require a calibration check on the date shown below.

Next Calibration Date:

September 2003

The calibration was carried out using the methods described in the calibration document. Where applicable, the standards used in the calibration process are traceable to the UK's National Physical Laboratory.

kinlad **Calibrated By:**

Approved By:

<u>Please keep this certificate with the calibration document.</u> When the probe is sent for a calibration check, please include the calibration document.



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IMMERSIBLE SAR PROBE

CALIBRATION REPORT

Part Number: IXP - 050

S/N 0114

6th September 2002



Indexsar Limited Oakfield House Cudworth Lane Newdigate Surrey RH5 5DR Tel: +44 (0) 1306 631 233 Fax: +44 (0) 1306 631 834 e-mail: <u>enquiries @indexsar.com</u>



INTRODUCTION

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This Report presents measured calibration data for a particular Indexsar SAR probe (S/N 0114) and describes the procedures used for characterisation and calibration.

Indexsar probes are characterised using procedures that, where applicable, follow the recommendations of CENELEC [1] and IEEE [2] standards. The procedures incorporate techniques for probe linearisation, isotropy assessment and determination of liquid factors (conversion factors). Calibrations are determined by comparing probe readings with analytical computations in canonical test geometries (waveguides, boxes and spheres) using normalised power inputs.

Each step of the calibration procedure and the equipment used is described in the sections below.

CALIBRATION PROCEDURE

1. Equipment Used

For the first part of the calibration procedure, the probe is placed in a calibration jig as pictured in Figure 1. In this position the probe can be rotated about its axis by a non-metallic belt driven by a stepper motor.

The probe is attached via its amplifier and an optical cable to a PC. A schematic representation of the test geometry is illustrated in Figure 2.

A balanced dipole (900 MHz) is inserted horizontally into the bracket attached to a second belt (Figure 1). The dipole can also be rotated about its axis. A cable connects the dipole to a signal generator, via a directional coupler and power meter. The signal generator feeds an RF amplifier at constant power, the output of which is monitored using the power meter. The probe is positioned so that its sensors line up with the rotation center of the source dipole. By recording output voltage measurements of each channel as both the probe and the dipole are rotated, data are obtained from which the spherical isotropy of the probe can be optimised and its magnitude determined.

The calibration process requires E-field measurements to be taken in air, in 900 MHz simulated brain liquid and at other frequencies/liquids as appropriate. When it is necessary to place the probe in liquid, a rectangular box made from PMMA (200mm internal width, 200mm internal height and 100mm internal depth; wall thickness 4mm) is filled with the appropriate liquid and positioned on the stand so that the probe tip is positioned within the liquid (Figure 1). The box is positioned so that its outer surface is 2mm from the dipole. The procedure follows that described in Ref [2]. Section A.5.2.1.

2. Linearising probe output

The probe channel output signals are linearised in the manner set out in Refs [1] and [2]. The following equation is utilized for each channel:

$$U_{lin} = U_{o/p} + U_{o/p}^{2} / DCP$$
 (1)



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where U_{lin} is the linearised signal, $U_{o/p}$ is the raw output signal in voltage units and DCP is the diode compression potential in similar voltage units.

DCP is determined from fitting equation (1) to measurements of U_{lin} versus source feed power over the full dynamic range of the probe. The DCP is a characteristic of the schottky diodes used as the sensors. For the IXP-050 probes with CW signals the DCP values are typically 0.10V (or 20 in the voltage units used by Indexsar software, which are V*200).

3. Selecting channel sensitivity factors to optimise isotropic response

The basic measurements obtained using the calibration jig (Fig 1) represent the output from each diode sensor as a function of the presentation angle of the source (probe and dipole rotation angles). The directionality of the orthogonally-arranged sensors can be checked by analysing the data using dedicated Indexsar software, which displays the data in 3D format as in Figure 3. The left-hand side of this diagram shows the individual channel outputs after linearisation (see above). The program uses these data to balance the channel outputs and then applies an optimisation process, which makes fine adjustments to the channel factors for optimum isotropic response.

The next stage of the process is to calibrate the Indexsar probe to a W&G EMR300 E-field meter in air. The principal reasons for this are to obtain conversion factors applicable should the probe be used in air and to provide an overall measure of the probe sensitivity.

A multiplier is applied to factors to bring the magnitudes of the average E-field measurements as close as possible to those of the W&G probe.

The following equation is used (where linearised output voltages are in units of V*200):

$$E_{air}^{2} (V/m) = U_{linx} * Air Factor_{x} + U_{liny} * Air Factor_{y} + U_{linz} * Air Factor_{z}$$
(2)

It should be noted that the air factors are not separately used for normal SAR testing. The IXP-050 probes are optimised for use in tissue-simulating liquids and do not behave isotropically in air.

4. 900 MHz Liquid Calibration

Conversion factors for use when the probes are immersed in tissue-simulant liquids at 900 MHz are determined either using a waveguide or by comparison to a reference probe that has been calibrated by NPL. Waveguide procedures are described later. The summary sheet indicates the method used for the probe S/N 0114.

The conversion factor, referred to as the 'liquid factor' is also applied to the measurements of each channel. The following equation is used (where output voltages are in units of V*200):



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 $E_{liq}^{2} (V/m) = U_{linx} * Air Factor_{x} * Liq Factor_{x}$ $+ U_{liny} * Air Factor_{y} * Liq Factor_{y}$ $+ U_{linz} * Air Factor_{z} * Liq Factor_{z}$ (3)

A 3D representation of the spherical isotropy for probe S/N 0114 using these factors is shown in Figure 3.

The rotational isotropy can also determined from the calibration jig measurements and is reported as the 900MHz isotropy in the summary table. Note that waveguide measurements can also be used to determine rotational isotropy (Fig. 5).

For other frequencies, probe conversion factors are determined using waveguide cells as shown in Figure 4. The cells consist of a coax to waveguide transition and an open-ended section of waveguide containing a dielectric separator. Each waveguide cell stands in the upright positition and is filled with liquid within 10 mm of the open end. The seperator provides a liquid seal and is designed for a good electrical transition from air filled guide to liquid filled guide. The choice of cell depends on the portion of the frequency band to be examined and the choice of liquid used. The depth of liquid ensures there is negligible radiation from the waveguide open top and that the probe calibration is not influenced by reflections from nearby objects. The return loss at the coaxial connector of the filled waveguide cell is measured initially using a network analyser and this information is used subsequently in the calibration procedure. The probe is positioned in the centre of the waveguide and is adjusted vertically or rotated using stepper motor arrangements. The signal generator is connected to the waveguide cell and the power is monitored with a coupler and a power meter. A fuller description of the waveguide method is given below.

The liquid dielectric parameters used for the probe calibrations are listed in the Tables below. The final calibration factors for the probe are listed in the summary chart.

WAVEGUIDE MEASUREMENT PROCEDURE

The calibration method is based on setting up a calculable specific absorption rate (SAR) in a vertically-mounted WG8 (R22) waveguide section [1]. The waveguide has an air-filled, launcher section and a liquid-filled section separated by a matching window that is designed to minimise reflections at the liquid interface. A TE_{01} mode is launched into the waveguide by means of a N-type-to-waveguide adapter. The power delivered to the liquid section is calculated from the forward power and reflection coefficient measured at the input to the waveguide. At the centre of the cross-section of the waveguide, the local spot SAR in the liquid as a function of distance from the window is given by functions set out in IEEE1528 as below:

Because of the low cutoff frequency, the field inside the liquid nearly propagates as a TEM wave. The depth of the medium (greater than three penetration depths) ensures that reflections at the upper surface of the liquid are negligible. The power absorbed in the liquid is determined by measuring the waveguide forward and reflected power. Equation (4) shows the relationship between the SAR at the cross-sectional center of the lossy waveguide and the longitudinal distance (z) from the dielectric separator



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$$SAR(z) = \frac{4(P_f - P_b)}{rabd} e^{-2z/d}$$
(4)

where the density r is conventionally assumed to be 1000 kg/m³, ab is the cross-sectional area of the waveguide, P_f and P_b are the forward and reflected power inside the lossless section of the waveguide, respectively. The penetration depth d, which is the reciprocal of the waveguide-mode attenuation coefficient, is determined from a scan along the *z*-axis and compared with the theoretical value determined from Equation (5) using the measured dielectric properties of the lossy liquid.

$$\boldsymbol{d} = \left[\operatorname{Re}\left\{ \sqrt{\left(\boldsymbol{p} / \boldsymbol{a}\right)^{2} + j\boldsymbol{w}\boldsymbol{m}_{o}\left(\boldsymbol{s} + j\boldsymbol{w}\boldsymbol{e}_{o}\boldsymbol{e}_{r}\right)} \right\} \right]^{-1}.$$
(5)

Table A.1 of [1] can be used for designing calibration waveguides with a return loss greater than 30 dB at the most important frequencies used for personal wireless communications. Values for the penetration depth for these specific fixtures and tissue-simulating mixtures are also listed in Table A.1.

According to [1], this calibration technique provides excellent accuracy, with standard uncertainty less than 3.6% depending on the frequency and medium. The calibration itself is reduced to power measurements traceable to a standard calibration procedure. The practical limitation to the frequency band of 800 to 2500 MHz because of the waveguide size is not severe in the context of compliance testing.

CALIBRATION FACTORS MEASURED FOR PROBE S/N 0114

The probe was calibrated at 1800, 1900 and 2450MHz MHz in liquid samples representing both brain liquid and body fluid at these frequencies. The calibration was for CW signals only, and the axis of the probe was parallel to the direction of propagation of the incident field i.e. end-on to the incident radiation. The axial isotropy of the probe was measured by rotating the probe about its axis in 10 degree steps through 360 degrees in this orientation.

The reference point for the calibration is in the centre of the probe's cross-section at a distance of 2.5 mm from the probe tip in the direction of the AD converter. A value of 2.5 mm should be used for the tip to sensor offset distance in the software.

It is important that the diode compression point and air factors used in the software are the same as those quoted in the results tables, as these are used to convert the diode output voltages to a SAR value.

DIELECTRIC PROPERTIES OF LIQUIDS

The dielectric properties of the brain and body tissue-simulant liquids employed for calibration are listed in the tables below. The measurements were performed using an Indexsar DiLine measurement kit, which uses the TEM method as recommended in [2].



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AMBIENT CONDITIONS

Measurements were made in the open laboratory laboratory at $23 \pm 0.5^{\circ}$ C. The temperature of the liquids in the waveguide used was measured using a mercury thermometer.

GSM RESPONSE

SAR probes are required to measure the effective value (RMS value) of the electric field strength. The averaging time is defined in the standards as being over 6 minutes but with most of the signals that occur in the real world, such a long averaging time is unnecessary since the fluctuations are eliminated with significantly shorter averaging times. With most signals, a much shorter averaging time is sufficient. For example the GSM frame rate is 120mS and averaging over this time period will remove the fluctuations.

In diode probes, a single Schottky diode is used as the detector for each of the three channels (X, Y and Z). For small field strengths, these offer a very good approximation to a true RMS rectifier. For higher field strengths, higher or lower values than the RMS value can be displayed - depending on the modulation frequency.

The theoretical maximum deviation from the RMS value can be derived based on the behavior of the two extremes [4]:

An average-value rectifier

• displays a value proportional to the average value of the magnitude of a measured quantity.

A peak-value rectifier

• displays a value proportional to the peak value of the magnitude of a measured quantity

The proportionality factor for a practical probe is chosen so that the probe reads the true RMS value for a continuous (CW) signal.

For pulsed signals, a diode rectifier must deliver a value lying somewhere between the two extremes of an average value rectifier and a peak value rectifier. By way of example, for a GSM signal with a 1 in 8 duty cycle (ratio of 'on' time to total time), the power measurement at higher powers can vary between being a factor of 8 too low (average value extreme) and a factor of 8 too high (peak-value extreme).

The actual behaviour is complex as it depends on the period of the modulation in relation to various time constants in the measuring system. These include the holding time of the diode (typically 50 uS), the time constant of the high-resistance leads and the time constant and integration periods of the measurement electronics. Also, the modulation periods are complex – GSM has a basic burst rate of 4.615mS, but the full modulation scheme only repeats every 120mS.



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To correct for the errors due to the diode response to pulsed signals, a multiplier can be added to the second term of Equation 1 (see earlier). In principle, this multiplier can have a range for a GSM signal of between 8 and 1/8. The correction scheme will

$$U_{\text{lin}} = U_{\text{o/p}} + U_{\text{o/p}}^{2} * \text{PCF/ DCP}$$
(4)

Where PCF is a pulse correction factor ranging between the duty cycle and the reciprocal of the duty cycle.

Indexsar SAR probes show a qualitatively similar behaviour in response to GSM signals, but with a much lesser degree of over or underestimation than indicated by the possible ranges above. Indeed, for many Indexsar probes, the PCF has been established by measurement to be close to unity. A probe with a unity PCF reads true RMS for a pulsed signal without correction.

The PCF has the effect of altering the effective diode compression potential and a modification to the DCP value is how the GSM correction is implemented in the Indexsar probe calibration scheme.

The modified DCP values for GSM are included in the summary page. The value has been determined by finding the modified DCP required to linearise the probe response as indicated in Figure 7.

Non-amplitude modulated carriers can be considered as CW as far as the probe calibration is concerned.

The effects of amplitude modulation of the CDMA signal on SAR measurements has been considered in a draft paper [see ref. 4] submitted to IEEE SCC-34.



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SUMMARY OF CALIBRATION FACTORS FOR PROBE IXP-050 S/N 0114

IXP-050	S/I	N0114			06/08/2002	2
F	Spherical is	otropy measure	ed at 900	MHz	0.50	(+/-) dB
	Cu Cu Cu Cu Cu Cu Cu Cu Cu Cu Cu Cu Cu C	¢ ion rotation)			n n (probe rotation)	
	Air factors DCPs CW DCPs GSM	X 532 20 7	Y 494 20 7	Z 450 20 7	(V*200) (V*200) (V*200)	
	f (MHz)	Axial isotropy		SAR conver	sion factors	Notes

f (MHz)	Axial (+/- d	isotro IB)	ру	SAR conv (liq/air)	Notes		
	BRA	IN	BODY	BRAIN	BODY		
90	0 0	0 10	0.10	0 340	0.374		3 1
180	0 0	.08	0.08	0.381	0.417		ο, ι
190	0 0	0.09	0.08	0.387	0.417		
245	0 0	.08	0.08	0.495	0.528		

Notes

1) Extrapolated values in italics

2) Calibrations done at 22C +/- 2C

- 3) Probe calibration by substitution against NPL-calibrated probe
 - (Probe IXP-050 S/N0071; NPL Cal Rept. No: EF07/2002/03/IndexSAR
- 4) Waveguide calibration
- 5) Checked using box-phantom validation test

(the graph shows a simple, spreadsheet representation of surface shown in 3D in Figure 3 below)



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PROBE SPECIFICATIONS

Indexsar probe 0106, along with its calibration, is compared with CENELEC and IEEE standards recommendations (Refs [1] and [2]) in the Tables below. A listing of relevant specifications is contained in the tables below:

Dimensions	S/N 0114	CENELEC	IEEE [2]			
Overall length (mm)	350	[1]				
Tin length (mm)	10					
Rody diameter (mm)	10					
Tin diameter (mm)	52	8	8			
Distance from probe tip to dipole centers	3.0	0	0			
(mm)	5.0					
	<u> </u>					
Dynamic range	S/N 0114	CENELEC	IEEE [2]			
2		[1]				
Minimum (W/kg)	0.01	< 0.02	0.01			
Maximum (W/kg)	>35	>100	100			
N.B. only measured to 35 W/kg						
Linearity of response	S/N 0114	CENELEC	IEEE [2]			
		[1]				
	0.125	0.50	0.25			
Over range 0.01 – 100 W/kg (+/- dB)						
	·		1			
Isotropy (measured at 900MHz)	S/N 0114	CENELEC	IEEE [2]			
		[1]				
Axial rotation with probe normal to source	Max. 0.10 (see	0.5	0.25			
(+/- dB) at 900, 1800, 1900 and 2450 MHz	summary					
	table)	1.0	0.50			
Spherical isotropy covering all orientations	0.50	1.0	0.50			
to source (+/- dB)						
Construction	Each proba con	toing three ortho	ronal dinala			
Construction	Each probe con	d on a triangular	prism coro			
	sensors arranged on a triangular prism core,					
	protected against static charges by built-in shielding, and covered at the tip by DEEV					
	cylindrical enclosure material. No adhesives					
	materials are PF	EEK and heat-sh	ink sleeving.			
			in side ing.			
Chemical resistance	Tested to be res	istant to glycol a	nd alcohol			
	containing simu	lant liquids but p	probes should			
	be removed, cle	aned and dried v	when not in			

use.



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REFERENCES

[1] CENELEC, EN 50361, July 2001. Basic Standard for the measurement of specific absorption rate related to human exposure to electromagnetic fields from mobile phones.

[2] IEEE 1528, Recommended practice for determining the spatial-peak specific absorption rate (SAR) in the human body due to wireless communications devices: Experimental techniques.

[3] Calibration report on SAR probe IXP-050 S/N 0071 from National Physical Laboratory. Test Report EF07/2002/03/IndexSAR. Dated 20 February 2002.

[4] The response of Indexsar SAR probes to amplitude modulated (pulsed) RF signals, Indexsar Support document IXS211.



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Figure 2. Schematic diagram of the test geometry used for isotropy determination





Figure 3. Graphical representation of the probe response to fields applied from each direction. The diagram on the left shows the individual response characteristics of each of the three channels and the diagram on the right shows the resulting probe sensitivity in each direction. The colour range in the figure images the lowest values as blue and the maximum values as red. For the probe S/N 0114, this range is

(+/-) 0.50 dB. The probe is more sensitive to fields parallel to the axis and less sensitive to



Figure 4. Geometry used for waveguide calibration (after Ref [2]. Section A.3.2.2)



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IXP-050 S/N 0114

08-Aug-02





Figure 5. Example of the rotational isotropy of probe S/N 0114 obtained by rotating the probe in a liquid-filled waveguide at 1800 MHz. Similar distributions are obtained at the other test frequencies (1900 and 2450 MHz) both in brain liquids and body fluids (see summary table)



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Figure 6. The measured SAR decay function along the centreline of the R22 waveguide with conversion factors adjusted to fit to the theoretical function for the particular dimension. frequency, power and liquid properties employed.



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Figure 7. The GSM response of IXP-050 probe S/N 0114 at 1800MHz (max. SAR level 1.6 W/kg)

jrequency		
Liquid used	Relative permittivity (measured)	Conductivity (S/m) (measured)
835 MHz BRAIN	42.85	0.90
900 MHz BRAIN	42.43	1.01
1800 MHz BRAIN	39.09	1.37
1800 MHz BODY	52.53	1.49
1900 MHz BRAIN	38.6	1.48
1900 MHz BODY	52.21	1.60
2450 MHz BRAIN	38.13	1.82
2450 MHz BODY	55.28	1.92

Table indicating the dielectric parameters of the liquids used for calibrations at each frequency



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Report No. SN0048_2450 26th March 2003

INDEXSAR 2450MHz validation Dipole Type IXD-245 S/N 0048

Performance measurements

• MI Manning



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Calibration / Conformance statement Balanced Validation dipole

Туре:	IXD-245 2450MHz	
Manufacturer:	IndexSAR, UK	
Serial Number:	0048	
Place of Calibration:	IndexSAR, UK	

IndexSAR Limited hereby declares that the IXD series dipole named above has been checked for conformity to the specifications given in the draft IEEE 1528 and CENELEC En 50361 standards on the date shown below.

Date of Calibration/Check: 26th March 2003

The dipole named above should be periodically re-checked using the procedures set out in the dipole calibration document. It is important that the cautions regarding handling of the dipoles (given in the calibration document) are adhered to.

Next Calibration Date:

March 2005

The calibration measurements were carried out using the methods described in the calibration document. Where applicable, the standards used in the calibration process are traceable to the UK's National Physical Laboratory.

kinladby

Calibrated By:

	M J. Marine	
Approved By:	\rightarrow	



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1. Tests on Validation Dipole

Tests have been performed on a balanced dipole made for 2450MHz application according to the construction guidelines, dimensions and tolerances given in the draft IEEE1528 standard [1]. Measurements have been made of the impedance and return loss when positioned against the liquid-filled phantom and a validation test has been performed according to the procedures set out in IEEE 1528 [1].

2. Measurement Conditions

Measurements were performed using a box-shaped phantom made of PMMA with dimensions designed to meet the accuracy criteria for reasonably-sized phantoms that do not have liquid capacities substantially in excess of the volume of liquid required to fill the Indexsar upright SAM phantoms used for SAR testing of handsets against the ear.

An HP 8753B vector network analyser was used for the return loss measurements. The dipole was placed in a special holder made of low-permittivity, low-loss materials. This holder enables the dipole to be positioned accurately in the centre of the base of the Indexsar box-phantom used for flat-surface testing and validation checks.

The validation dipoles are supplied with special spacers made from a low-permittivity, low-loss foam material. These spacers are fitted to the dipole arms to ensure that, when the dipole is offered up to the phantom surface, the spacing between the dipole and the liquid surface is accurately aligned according to the guidance in the relevant standards documentation. The spacers are rectangular with a central hole equal to the dipole arm diameter and dimensioned so that the longer side can be used to ensure a spacing of 15mm from the liquid in the phantom (for tests at 900MHz and below) and the shorter side can be used for tests at 1800MHz and above to ensure a spacing of 10mm from the liquid in the phantom. The spacers are made on a CNC milling machine with an accuracy of 1/40th mm but they may suffer wear and tear and need to be replaced periodically. The material used is Rohacell, which has a relative permittivity of approx. 1.05 and a negligible loss tangent.

The apparatus supplied by Indexsar for dipole validation tests thus includes:

Balanced dipoles for each frequency required are dimensioned according to the guidelines given in IEEE 1528 [1]. The dipoles are made from semi-rigid 50 Ohm co-ax, which is joined by soldering and is gold-plated subsequently. The constructed dipoles are easily deformed, if mis-handled, and periodic checks need to be made of their symmetry.

Rohacell foam spacers designed for presenting the dipoles to 2mm thick PMMA box phantoms. These components also suffer wear and tear and should be replaced when the central hole is a loose-fit on the dipole arms or if the edges are too worn to ensure accurate alignment. The standard spacers are dimensioned for use with 2mm wall thickness (additional spacers are available for 4mm wall thickness).

3. SAR Validation Measurement

A SAR validation check was performed with the box-phantom located on the SARA2 phantom support base on the SARA2 robot system. Tests were then conducted at a feed power level of approx. 0.25W. The actual power level was recorded and used to normalise the results obtained to the standard input power conditions of 1W (forward power). The ambient temperature was 24°C.

The phantom was filled with a 2450MHz brain liquid using a recipe from [1], which was measured using



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an Indexsar DiLine kit at 2450MHz. Measurements were taken at 23°C and 30°C and interpolation was used to find the properties at 24°C which were as below:

Relative Permittivity	39.221
Conductivity	1.8714 S/m

The SARA2 software version 0.420N was used with an Indexsar probe previously calibrated using waveguide techniques.

The 3D measurement made using the dipole at the bottom of the phantom box is shown below:



The volume-averaged SAR results, normalised to an input power of 1W (forward power) are:

Averaged over 1 cm^3 (1g) of tissue	51.376 W/kg
Averaged over 10cm^3 (10g) of tissue	23.888 W/kg

These results can be compared with Table 8.1 in [1]. The agreement is within 10%.

4. Dipole impedance and return loss

The dipoles are designed to have low return loss ONLY when presented against a lossy-phantom at the specified distance. A Vector Network Analyser (VNA) was used to perform a return loss measurement on the specific dipole when in the measurement-location against the box phantom. The distance was as specified in the standard i.e. 10mm from the liquid (for 2450MHz). The Indexsar foam spacers (described above) were used to ensure this condition during measurement.



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The impedance was measured at the SMA-connector with the network analyser. The following parameters were measured:

Dipole impedance at 2450 MHz Re{Z} = 44.814 Ω Im{Z} = -5.3359 Ω

Return loss at 2450MHz -22.122 dB



5. Dipole handling

The dipoles are made from standard, copper-sheathed coaxial cable. In assembly, the sections are joined using ordinary soft-soldering. This is necessary to avoid excessive heat input in manufacture, which would destroy the polythene dielectric used for the cable. The consequence of the construction material and the assembly technique is that the dipoles are fragile and can be deformed by rough handling. Conversely, they can be straightened quite easily as described in this report.

If a dipole is suspected of being deformed, a normal workshop lathe can be used as an alignment jig to restore the symmetry. To do this, the dipole is first placed in the headstock of the lathe (centred on the plastic or brass spacers) and the headstock is rotated by hand (do NOT use the motor). A marker (lathe tool or similar) is brought up close to the end of one dipole arm and then the headstock is rotated by 0.5 rev. to check the opposing arm. If they are not balanced, judicious deformation of the arms can be used to



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restore the symmetry.

If a dipole has a failed solder joint, the dipole can be fixed down in such a way that the arms are co-linear and the joint re-soldered with a reasonably-powerful electrical soldering iron. Do not use gas soldering irons. After such a repair, electrical tests must be performed as described below.

Please note that, because of their construction, the dipoles are short-circuited for DC signals.

6. Tuning the dipole

The dipole dimensions are based on calculations that assumed specific liquid dielectric properties. If the liquid dielectric properties are somewhat different, the dipole tuning will also vary. A pragmatic way of accounting for variations in liquid properties is to 'tune' the dipole (by applying minor variations to its effective length). For this purpose, Indexsar can supply short brass tube lengths to extend the length of the dipole and thus 'tune' the dipole. It cannot be made shorter without removing a bit from the arm. An alternative way to tune the dipole is to use copper shielding tape to extend the effective length of the dipole. Do both arms equally.

It should be possible to tune a dipole as described, whilst in place in the measurement position as long as the user has access to a VNA for determining the return loss.

7. Reference

[1] Draft recommended practice for determining the peak spatial-average specific absorption rate (SAR) in the human body due to wireless communications devices: Measurement Techniques. Draft CD1.1 – December 29, 2002.