Engineering Report in Support of Certification FCC Form 731 for MCUB5R radiomodem

Subject:	Compliance of Radio Modem with Respect to FCC Rules & Regulations Parts 2 and 90 Certification FCC Form 731
Equipment: FCC Id: Applicant:	UHF Radio Modem EOTMCUB5R Dataradio Inc. 5500 Royal Mount Ave., Suite 200 Town of Mount Royal, H4P 1H7 Quebec, Canada

April 16, 1999 Dataradio Inc Johnson Data Telemetry Corporation Waseca, Minnesota

ENGINEERING STATEMENT OF MARK CHRISTENSEN

The application consisting of the attached engineering exhibit and associated FCC form 731, has been prepared in support of a request for Type Acceptance for the Johnson Data Telemetry (JDT) DL-3412, 403-512 MHz Transceiver with the Data Radio 3315(Integra) Modem. The Transceiver mated with the Integra Modem will be identified by the part number INA12XY0T where X represents range and Y represents IF bandwidth (see below for part#). The model name is MCUB5R. The Transceiver/Modem will be identified by the FCC number EOTMCUB5R. The transceiver operates pursuant to Part(s) 90 and 15 of the Rules and Regulations.

EXISTING CONDITIONS

The units utilized for these type acceptance measurements were obtained from the pilot-production. The transceiver is designed to operate on frequencies ranging from 403.000 MHz to 512.000 MHz. The frequency tolerance of the transceiver is .00015% or 1.5 parts per million. The frequency stability of the transceiver is controlled by a temperature compensated crystal oscillator (TCXO) operating at 17.5 MHz.

PROPOSED CONDITIONS

It is proposed to Type Accept the MCUB5R, 403-512 MHz Transceiver/Modem for operation in the band of frequencies previously outlined. The applicant anticipates marketing the device for use in wireless transmission of data.

PERFORMANCE MEASUREMENTS

All Type Acceptance measurements were conducted in accordance with the Rules and Regulations Section 2.1041of Pike & Fischer Inc., CD ROM revision 9/28/98. Equipment performance measurements were made in the engineering laboratory and on the FCC certified Open Area Test Site at the Transcrypt International / E.F. Johnson Radio Products located at 299 Johnson Avenue in Waseca, Minnesota. All measurements were made and recorded by myself or under my direction. The performance measurements were made between Jan 28, 1999 and Feb 8,1999.

CONCLUSION

Given the results of the measurements contained herein, the applicant requests that Type Acceptance be granted for the INA12XY0T, 403-512 MHz Transceiver/Modem as tested for data communications.

4/5/99

Mark Christensen Director of Engineering, Johnson Data Telemetry

Part Number			
Х	Freq Range		
1	380-403 MHz		
2	403-419 MHz		
3	419-435 MHz		
4	435-451 MHz		
5	450-470 MHz		
6	464-480 MHz		
7	480-496 MHz		
8	496-512 MHz		

IF Bandwidth

QUALIFICATIONS OF ENGINEERING PERSONNEL (2.911)

NAME:	Allen Frederick		
TITLE:	Certified Technologist		
TECHNICAL EDUCATION:	Bachelor of Science Degree in Electronic Engineering Technology (1998) from Mankato State University		
TECHNICAL EXPERIENCE:	2 years experience in analog and radio frequency communications		
NAME:	Constantin Pintilei		
TITLE:	R&D Test Engineer		
TECHNICAL EDUCATION:	Bachelor of Science Degree in Radiotechnique Electronic Engineering (1993) from Technical University of Iasi, Romania		
TECHNICAL EXPERIENCE:	5 years experience in radio frequency measurements		

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15. Other data TESTS RESULTS FOR MCUB5R RADIO MODEM	
NAME OF TEST: TRANSMITTER RATED POWER OUTPUT NAME OF TEST: TRANSMITTER OCCUPIED BANDWIDTH Necessary Bandwidth Measurement Theory of Measurement Set-Up Dataradio's Measurement Set-Up INTEGRA Modem at 9600 bps MASK: D,5W MASK: D,5W MASK: D,1W WIDE SPAN = 100 MHz INTEGRA Modem at 19.2 Kbps MASK: B,5W MASK: B,5W MASK: B,1W NAME OF TEST: TRANSMITTER SPURIOUS AND HARMONIC OUTPUTS NAME OF TEST: FIELD STRENGTH OF SPURIOUS RADIATION. NAME OF TEST: FIELD STRENGTH OF SPURIOUS RADIATION. NAME OF TEST: FREQUENCY STABILITY with Variation in Ambient Temperature	
-with Variation in Amolent Temperature -with Variation in Supply Voltage NAME OF TEST: TRANSIENT FREQUENCY BEHAVIOR	

Engineering Summary

This report contains the results of the engineering evaluation performed on a Dataradio Inc. radio modem, having a frequency range of 403-512 MHz, model MCUB5R. Johnson Data Telemetry (JDT) Corporation carried out the tests in accordance with FCC Rules and Regulation Part 2 and Part 90.

The radio modem was evaluated for output power levels of 1 and 5 watts.

Based on test results, it is certified that the product meets the requirements as set forth in the above specifications for Certification.

The MCUB5R UHF radio modem is comprised of a Dataradio 3315 loader/modem board and a DL 3412 Telemetry transceiver. Test data and graphs for this configuration are presented in this report.

General Information

FCC submission information

FCC Id:	EOTMCUB5R
Equipment:	UHF radio modem
Model:	MCUB5R
Applicant:	Dataradio Incorporated
	5500 Royal Mount Ave., Suite 200
	Town of Mount Royal, H4P 1H7
	Quebec, Canada
Manufacturer	Dataradio Incorporated
	5500 Royal Mount Ave., Suite 200
	Town of Mount Royal, H4P 1H7
	Quebec, Canada
Test laboratory	Johnson Data Telemetry Corporation (JDT)
	299 Johnson Ave. SW
	Waseca, MN 56093

Manufacturer's data

Equipment:	UHF radio modem
Model:	MCUB5R
Serial Number:	xxxx (prototype serial)
Reference:	FCC Rules and Regulations Part 2 and Part 90
Manufacturer:	Dataradio Incorporated

Product's general specifications

1	Frequency range	403-512 MHz	Z
2	Rated transmitted	1 - 5W	
	output power		
3	Data modulation	DRCMSK	
4	Channel spacing	25 KHz	12.5 KHz
5	Emission type	15K3 F1D	9K30 F1D
6	Frequency deviation	±4 KHz	±2.5 KHz
7	Data rate	19200 bps	9600 bps
8	Antenna impedance	50 Ω	
9	Power source	13.3 V	

Information for Certification

Ref: FCC Part 2 paragraph 2.1033 (c)

1. Name of Applicant:

Ref: FCC Part 2 paragraph 2.1033 (c)(1)

Applicant:	Dataradio Incorporated		
	5500 Royal Mount Ave., Suite 200		
	Town of Mount Royal, H4P 1H7		
	Quebec, Canada		
Manufacturer	Same as applicant		

2. FCC Identifier

Ref: FCC Part 2 paragraph 2.1033 (c)(2)

Model No.:	MCUB5R, comprised of two boards:
	MCU 3315 (Dataradio 210-03315-0xx)- modem board
	DL 3412 (JDT 242-3412-xx0)- transceiver board
Serial No.:	xxxx (prototype serial)
	xxx-3315-0xx-modem board
	3412- xxxxxx-5x0-transceiver board
FCC Id:	EOTMCUB5R

3. Instruction book

Ref: FCC Part 2 paragraph 2.1033 (c) (3)

See technical manual in Integra-TR Technical Manual, Attachment D,

4. Types of emission

Ref: FCC Part 2 paragraph 2.1033(c)(4)

Channel spacing	25 KHz	12.5 KHz
Emission type	15K3 F1D	9K30 F1D
Frequency deviation	±4 KHz	±2.5 KHz

5. Frequency range

Ref: FCC Part 2 paragraph 2.1033(c)(5)

403-512 MHz

6. Range of operating power levels

Ref: FCC Part 2 paragraph 2.1033(c)(6)

The power is adjusted at the manufacturer at a level of 5W.

7. Maximum Power rating

Ref: FCC Part 2 paragraph 2.1033(c)(7)

5 Watts

8. DC voltages and currents into final amplifier

Ref: FCC Part 2 paragraph 2.1033(c)(8)

Refer also to RF output and DC input power measurement in section "Test Results".

9. Tune-up procedure

Ref: FCC Part 2 paragraph 2. 1033(c)(9)

- 1. Connect the transceiver to be aligned to a DC power source. A DC current meter capable of measuring at least 2.5 Amps should be connect in line with the DC source. Connect the output of the transceiver through a watt meter and into a 50 ohm dummy load.
- 2. Load the synthesizer with the center channel frequency.
- 3. Key the transmitter and make certain that the supply voltage at the RF board is 13.3 VDC. (Do not transmit for extended periods of time.)
- 4. Adjust R535 clockwise for 5.0 Watts of output power.
- 5. Check the power levels on the low and the high frequencies for 5.0 Watts +/- 1 Watt.

10. Complete circuit diagram, circuitry and devices for determining and stabilizing frequency, circuits for suppression of spurious radiation, limiting of modulation and limiting of power

Ref: FCC Part 2 paragraph 2. 1033(c)(10)

For the main control circuits and the modem circuits see the section Dataradio MCU modem, in Description of Circuitry, Attachment A part 1.

For the transceiver circuits see the section JDT DL-3412 Telemetry Transceiver, in Description of Circuitry, Attachment A part 2.

Circuitry's mainly involved in determining and stabilizing frequency are VCO block and Synthesizer block described in Transceiver's part.

- i) spurious radiation- The main suppression of spurious radiation is performed by the filter described in "Low Pass Filter" paragraph from JDT DL-3412 Telemetry Transceiver, Description of Circuitry part 2, Attachment A
- ii) limiting of modulation- Limiting of modulation is given by amplitude limited audio signal provided by modem part as it was explained in "Modem" paragraph from Dataradio MCU modem, Description of Circuitry part 1, Attachment A. Supplementary limiting of modulation is described in " Frequency Modulation" paragraph from Synthesizer section JDT DL-3412 Telemetry Transceiver, Description of Circuitry part 2, Attachment A.
- iii) limiting of power- A very tight control of transmission power is maintained by circuitry described in "Power Control" paragraph from JDT DL-3412 Telemetry Transceiver, Description of Circuitry part 2, Attachment A

See schematics in Schematics, Attachment B

11. Equipment identification plate/label

Ref: FCC Part 2 paragraph 2.1033(c)(11)

A scanned image of the Equipment identification label is provided in Photographs, Attachment C

12.Photographs of the equipment

Ref: FCC Part 2 paragraph 2.1033 (c)(12)

All scanned photographs of the Equipment are provided in Photographs, Attachment C

13. Digital modulation techniques

Ref: FCC Part 2 paragraph 2.1033 (c) (13)

The digital modulation used by the MCU modem is DRCMSK (Differential Raised Cosine Minimum Shift Keying). A modem using such type of modulation is divided in three main units. They are:

- 1. Scrambler,
- 2. Differential encoder,
- 3. Waveshape generator.

We will explain each of those units, starting with the scrambler.

1. Scrambler:

The scrambler converts data stream to a new data stream having better characteristics for a FM radio system. Here are the main advantages:

-It removes the DC component from a DRCFSK signal,

- -It randomizes the data in such a way we can avoid predictable patterns, by example:
 - 00000000, 111111111, 01010101, 00110011, etc.
- -It keeps the power spectrum more compact by avoiding sequences like 01010101...

All these functions are performed with a serial shift register and 2 exclusive OR gates that implement the polynomial form X^7+X^5-1 . The receiver side of our radio modems has a similar circuit called descrambler to decode the received scrambled data.

2. Differential encoder:

After data is scrambled, we encode the data with a differential encoder. Here is the process that differential encoder does:

previous	current	output
input bit	input bit	bit
0	0	0
0	1	1
1	0	1
1	1	0

Example:

From a sequence of 0100101111010001010100010, differentially encoded data stream is:

110111000111001111110011.

The differential encoder is used to make the modem insensitive to audio polarity inversion of the FM radio system.

3. Waveshape generator:

The waveshape generator converts the processed data bits (scrambled and differentially encoded for DRCMSK) to the audio signal that will modulate a FM transmitter. This gives the DRCMSK waveshape having a compact spectrum to fit inside FCC Part 90 masks according to the channel bandwidth intended.

Furthermore, the modem itself generates a RF signal heading the transmission in normal usage and a test pattern for test purposes.

1. Transmission preamble:

Each data transmission begins by sending a 15ms preamble of sinewave (101010...). This is to synchronize the digital phase looked loop of the receiver modem.

2. Test pattern generator:

A 30s test pattern sequence is generated by test software at "test data" click button event. According to the baud rate, the highest resulting modulating frequency is (baud rate)/2 Hz. The sequence is sent with baud rate speed, and its data has the pattern:

###ABCDEFGHIJKLMNOPQRSTUVWXYZabcdefghijklmnopqrstuvwxyz0123456789\r\n,

repeated for 30 seconds.

14. Test data Ref: FCC Part 2 paragraph 2.1033 (c)(14)

All applicable test data according to: -Part 2: 2.1046, 2.1047, 2.1049, 2.1051, 2.1053, and 2.1057 -Part 90, Subpart I: 90.209, 90.210, 90.211, 90.213 and 90.214 are provided in section Test Results of this Engineering Report

15. Other data

For data according to 2.1033(c)(15,16), this unit is not designed for the mentioned purposes.

Tests Results for MCUB5R radio modem

NAME OF TEST: Transmitter Rated Power Output

RULE PART NUMBER: 2.1033 (c)(6)(7) and 2.1046 (a)

TEST RESULTS: See results below

TEST CONDITIONS: Standard Test Conditions, 25 C

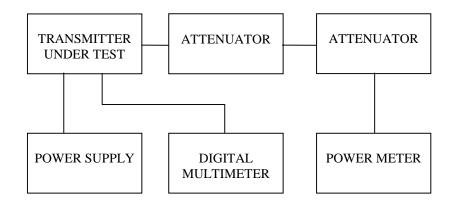
TEST EQUIPMENT: Attenuator, BIRD Model / 9715 / 50-A-MFN-06 / 6 dB / 50 Watt Attenuator, BIRD Model / 9716 / 25-A-MFN-20 / 20 dB / 25 Watt Digital Voltmeter, Fluke Model 8012A DC Power Source, Model HP6284A Power Meter, Hewlett Packard 436A

Allen Frederick

PERFORMED BY:

DATE: 2/2/99

TEST SET-UP:



TEST RESULTS:

Frequency	DC Voltage at	DC Current into	DC Power into	RF Power Output
<u>(MHz</u>)	Final (VDC)	Final (ADC)	Final (W)	<u>(W)</u>
450.000	13.3	1.75	23.28	5.0

NAME OF TEST: Transmitter Occupied Bandwidth

RULE PART NUMBER: 2.201, 2.202, 2.1033 (c)(14), 2.1049 (h), 2.1041

Necessary Bandwidth Measurement

This radiomodem uses digital modulation signals, passing through a linear 8^{th} order low-pass filter (Raise-Cosine alpha 1 approximation), to an FM transceiver. The necessary bandwidth calculation for this type of modulation (DRCMSK) is not covered by paragraphs (1), (2) or (3) from 2.202(c). Therefore, the approach outlined in (2.202(c)(4)) is applicable in this case.

The measurement explanations are provided in "Annex" (following pages)

Necessary Bandwidth Measurement:

Peak deviation = ± 4 kHz Modulator signal bit rate 19200 bps,

Bn=15260 Hz The corresponding emission designator prefix for necessary bandwidth = 15K3

Table 1 - Measurements results for the INTEGRA unit , 9600 bps BT.3 and 19200 bps BT.3 and frequency deviations set to obtain specified values .

unit's software	measured data (kHz	Emission	
settings		designator	
bit rate (data settings)	freq. dev	99% occupied BW	
9600 BT.3	3.0	9.24	9K30
19200 BT.3	4.0	15.26	15K3

Also, Spectrum Efficiency (90.203 (j)(3)) requirement: 4800 bits per second per 6.25 kHz of channel bandwidth.

19200bps=4*4800bps so it is efficient for 25 kHz channel

9600bps=2*4800bps so it is efficient for 12.5 kHz channel

ANNEX

Theory of Measurement

The way to define the *Occupied Bandwidth* is "the frequency bandwidth such that, below its lower and above its upper frequency limits, the mean powers radiated are each equal to 0.5 percent of the total mean power radiated by a given emission" (FCC 2.202), the mathematics are as follows:

$$0.005*TP = P_{(f1)} = \int_{0}^{f1} PSD_{(f)} df$$
$$0.995*TP = P_{(f2)} = \int_{0}^{f2} PSD_{(f)} df$$

OBW=f2-f1

where TP (total mean power) is

$$TP = \int_{0}^{+\infty} PSD_{(f)} df = (1/t) \int_{-\infty}^{+\infty} |z_{(t)}|^2 dt$$

and PSD (power spectral distribution) is

$$PSD_{(f)} = |Z_{(f)}|^2 + |Z_{(-f)}|^2$$
 $0 \le f < 4$

and expresses the positive frequency representation of the transmitter output power for z(t) signal.

By applying these mathematics to the measurements, it is possible to measure the Occupied Bandwidth using the RF signal's trace provided by a digital spectrum analyzer and processed further by computational methods.

The Occupied Bandwidth measurement is in two parts relatively independent of each other. The first gives the RF spectrum profile, and the second calculates the frequency limits and they result in the Occupied bandwidth. While the first involves RF measurement instrumentation, the second is strictly a computational part related to measured trace.

Getting an equally-sampled RF power spectrum profile requires a Digital Spectrum Analyzer. In addition to the instrument's usual requirements, a special attention must be paid to the analyzer's span (bandwidth to be investigated).

This bandwidth must be large enough to contain all the power spectral components created by the transmitter. The frequency step, where the samples are picked, is directly dependent on the span's value.

$\Delta f = \text{span/number of points displayed}$

The frequency resolution will determine the measurement accuracy. So for greater accuracy, less bandwidth will give better values because of the constant number of points that can be displayed. Taking into account the purpose of transmitter, an acceptable balance can be set. For channel-limited transmitters all the power spectral components can be found in main channel and a number of adjacent channels, upper and lower, from the main channel. The relation between these two requirements, number of channels and accuracy, is depicted by:

$$a(\%) \cong (2*k*n/N)*100,$$

where a is desired accuracy, in percentage units, n is the number of channels in span, including main channel, N is displayed number of points and k= (authorized bandwidth) /channel bandwidth.

For usual spectrum analyzers N \cong 500, k=0.8 (20/25) for 25kHz channel transmitters or k=0.9 (11.25/12.5) for 12.5kHz channel transmitters, so a \cong n/2.5 (%) can estimate the expected precision for measurement.

All other requirements for spectrum analyzer are the same as they are for mask compliance determination.

The second part has computational requirements related to the trace's values processing.

The following operations must be performed over the trace's (x,y) points:

- 1. convert y value in dBm (or the analyzer's display y units) units power sample
- 2. convert y value in W units power sample,
- 3. add to total power every power sample and get total power value (W units for total power)
- 4. set low level (0.5% *total power)
- 5. detect x1-sample which pass low level (convert f1 integrals to sample summing)
- 6. convert (x1-1)-sample value in frequency units (the x-sample is already in occupied bandwidth),
- 7. store first frequency correspondent to (x1-1)-sample
- 8. set up level (99.5% *total power)
- 9. detect x2-sample which pass up level (convert f2 integrals to sample summing)
- 10. convert (x2)-sample value in frequency units (the x-sample is now out of occupied bandwidth),
- 11. store second frequency correspondent to (x2)-sample
- 12. read the frequency difference, this is Occupied Bandwidth, and display the result.

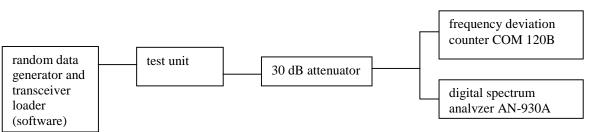
Standard calculation precision is all that is required. The main error factor being the y display resolution is covering calculation precision.

The absolute error for this measurement is $-0/+2^*$)f. It is not possible to decrease span bandwidth under 2 channels bandwidth because this will affect the significance of result by cutting off the power's spectral distribution edges.

Dataradio's Measurement Set-Up

For the above requirements, the occupied bandwidth of a transmitter was measured using an IFR AN930 A spectrum analyzer having adequate macrofunction to perform computational part. The number of power spectrum samples (N) is 500. Because in test results frequency deviation was also a parameter, measurement instruments were completed with an IFR COM-120 B for frequency deviation determination.

The measurement set-up is:



The AN-930 A spectrum analyzer's parameters are adjusted as follow:

-total span is adjusted at 2.8*channel space this means 70 kHz for 25 kHz channel and 35 kHz for 12.5 kHz channel. This setting will result in frequency sample step (f) of 140 Hz for 25 kHz channel and 70 Hz for 12.5 kHz channel.

-RBW is set to 300 Hz, this is better than 1% of total span bandwidth.

-video filter is set to 1Khz;

-all other parameter of the instrument are automatically adjusted to obtain calibrated measurements (sweep time 4s).

-central frequency and reference level are adjusted to the unmodulated carrier frequency and level.

The AN 930 A spectrum analyzer's Occupied Bandwidth macrofunction input parameters are: -central frequency, same as above, the unmodulated carrier frequency. -channel spacing, 25 kHz or 12.5 kHz according to the signal, -percentage of Occupied Bandwidth 99%.

The macro operations are:

-the trace is read;

-follow all the computational steps required.

Each sample is converted from dBm to mW and add to total power (tpow) variable. Then are computed the limits of 0.5% and 99.5% by using variable remaining percent (RemPer), and in same time are stored sample number where these two percentage meet. Then are assigned to the markers the correspondent frequencies of numbers.

- Occupied Bandwidth is then displayed as Delta mode marker (difference between markers).

-return to operational mode.

NOTE 1: The computational part could be performed on every device featured with data acquisition. NOTE 2: An approximation of the occupied bandwidth calculation can be performed by measuring at the points at which the spectrum, measured with a spectrum analyzer of 300 Hz resolution bandwidth, is 25dB down relative to the unmodulated carrier reference level.

NAME OF TEST:	Transmitter Occupied Bandwidth
INTEGRA M	odem at 9600 bps In Support of Emission Designator 9K30F1D
RULE PART NUMBER:	2.201, 2.202, 2.1033 (c)(14), 2.1049(h), 2.1041, 90.209(b)(5), 90.210 (d)
MINIMUM STANDARD	$ \begin{array}{ll} & \mbox{Mask D} \\ & \mbox{Sidebands and Spurious [Rule 90.210 (d), P = 5 Watts]} \\ & \mbox{Authorized Bandwidth} = 11.25 \ \mbox{kHz} \ [Rule 90.209(b) (5)] \\ & \mbox{From Fo to } 5.625 \ \mbox{kHz}, \ \mbox{down 0 dB}. \ \mbox{Greater than } 5.625 \ \mbox{kHz} \ \mbox{to } 12.5 \ \mbox{kHz}, \\ & \mbox{down 7.27(f_d-2.88 \ \mbox{kHz}) dB}. \ \mbox{Greater than } 12.5 \ \mbox{kHz}, \ \mbox{at least } 50+10 \ \mbox{log}_{10}(P) \\ & \mbox{or 70 dB}, \ \mbox{whichever is the lesser of the attenuation}. \\ & \mbox{Attenuation} = 0 \ \mbox{dB} \ \mbox{at Fo to } 5.625 \ \mbox{kHz} \\ & \mbox{Attenuation} = 20 \ \mbox{dB} \ \mbox{at 5.625 \ \mbox{kHz}} \\ & \mbox{Attenuation} = 57 \ \mbox{dB} \ \mbox{at > 12.5 \ \mbox{kHz}} \\ \end{array} $
TEST RESULTS:	Meets minimum standard (see data on the following pages)
TEST CONDITIONS:	Standard Test Conditions, 25 C
TEST EQUIPMENT:	Attenuator, BIRD Model / 9715 / 50-A-MFN-06 / 6 dB / 50 Watt Attenuator, BIRD Model / 9716 / 25-A-MFN-20 / 20 dB / 25 Watt Digital Voltmeter, Fluke Model 8012A DC Power Source, Model HP6284A Modulation Analyzer, Model HP8901A Spectrum Analyzer, Model HP8563E Plotter, HP7470A

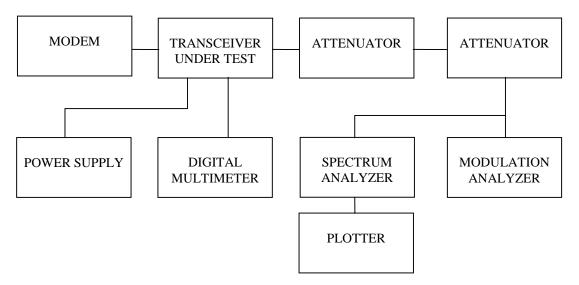
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PERFORMED BY:

DATE: 1/29/99

Allen Frederick

TEST SET-UP:



NAME OF TEST:	Transmitter Occupied Bandwidth (Continued)
	INTEGRA Modem at 9600 bps
	In Support of Emission Designator 9K30F1D

MODULATION SOURCE DESCRIPTION:

The digital modulation type used in the INTEGRA is DRCMSK (Differential Raised Cosine Minimum Shift Keying). A modem using such type of modulation is divided into three main functional units in a CPLD chip: Scrambler:

The scrambler converts the data stream to a new data stream more suitable for FM transmission.

-It keeps the power spectrum more compact by avoiding sequences like 01010101...

The scrambler is made with a serial shift register and 2 exclusive OR gates which implement the polynomial form X^7+X^5-1 . For the receiver side, a similar circuit performs the descrambling function to decode the received scrambled data.

Differential encoder:

After data is scrambled, we encode the data with a differential encoder. The differential encoder XOR's the current input bit with the previous bit. The differential encoder is used to make the modem insensitive to audio polarity inversion of the FM radio system.

Waveshape generator:

The waveshape generator converts the processed data bits (scrambled and differentially encoded for DRCMSK) to the DRCMSK audio signal. This audio signal is passed through a low-pass filter before modulating the RF transmitter.

TRANSMISSION PREAMBLE:

Each data transmission begins by sending a 15 millisecond preamble of sinewave (101010...). This is to synchronize the digital phase locked loop of the receiver modem.

TEST PATTERN GENERATOR:

A 30 s test pattern sequence is generated by the test software when the "test data" button is clicked. The highest resulting modulating frequency is (baud rate)/2 Hz. The following pseudo random test pattern was used to modulate the transmitter:

###ABCDEFGHIJKLMNOPQRSTUVWXYZabcdefghijklmnopqrstuvwxyz0123456789\r\n,

In this pattern ### is replaced by the number of replays, \r is a carriage return and \n is a linefeed. The data is fed to the RS232 interface IC and processed as described above. The async-to-sync conversion, scrambler and differential encoder make the ABCDE... pattern appear random over the air.

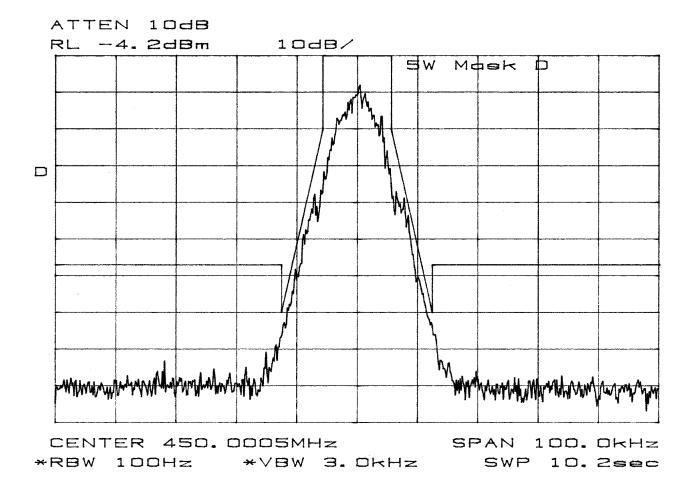
NECESSARY BANDWIDTH (Bn) CALCULATION

See page 13 for Emission Designator determination.

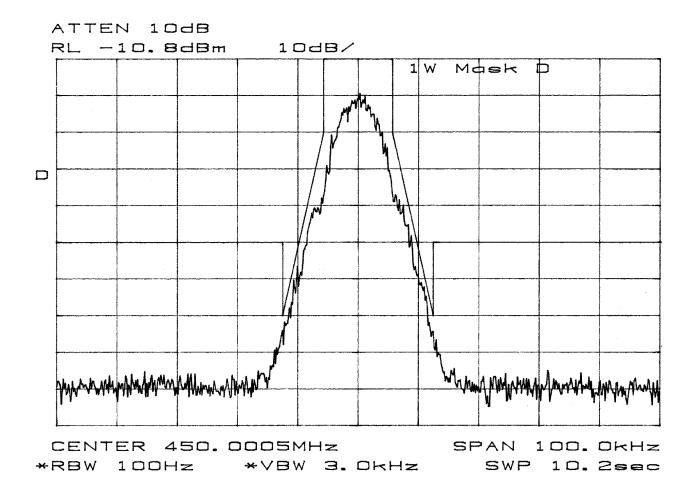
The corresponding emission designator prefix for necessary bandwidth = 9K30

TEST DATA: Refer to the following graphs:

MASK: D,5W SPECTRUM FOR EMISSION 9K30F1D OUTPUT POWER: 5 Watts 9600 bps PEAK DEVIATION = 2500 Hz SPAN = 100 kHz



MASK: D,1W SPECTRUM FOR EMISSION 9K30F1D OUTPUT POWER: 1 Watts 9600 bps PEAK DEVIATION = 2500 Hz SPAN = 100 kHz



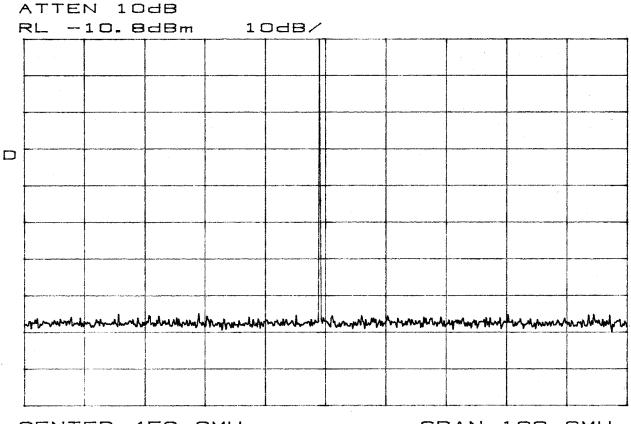
WIDE SPAN = 100 MHz OUTPUT POWER: 5 Watts

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כ										
										-
	maprowh	mm	water	www.wptm-r.n	minne	hours	muhanman	water	hynn	Mynophine
							· · · · · · · · · · · · · · · · · · ·			

*RBW 10kHz *VBW 10kHz

SWP 2.50sec

WIDE SPAN = 100 MHz OUTPUT POWER: 1 Watts



CENTER 450. OMHZ SPAN *RBW 10kHz *VBW 10kHz SWP

SPAN 100.0MHz SWP 2.50sec

NAME OF TEST:	Transmitter Occu	Transmitter Occupied Bandwidth				
INTEGRA Mod	dem at 19.2 Kbps In Support of Err	nission Designator 15K3F	1D			
RULE PART NUMBER:	2.201, 2.202, 2.1	033 (c)(14), 2.1049(h), 2.	1041, 90.209(b)(5), 90.210 (b)			
MINIMUM STANDARD:	Authorized Band From Fo to 50% From 50% to 100 From 100% to 25	purious [Rule 90.210 (b), lwidth = 20 kHz [Rule 90. of Authorized BW Remov 0% removed, at least 25 d 50% removed, at least 35 % remove, at least 43 + 10	209(b) (5)] ved from Fo, down 0 dB. IB. dB.			
TEST RESULTS:	20 kHz to 50 kHz > 50 kHz, Atten > 50 kHz, Atten	tenuation = 0 dB Iz, Attenuation = 25 dB m z, Attenuation = 35 dB mi uation = 50 dB minimum uation = 43 dB minimum standard (see data on the s	nimum (5 watts) (1 watt)			
TEST CONDITIONS:	Standard Test Co	onditions, 25 C				
TEST EQUIPMENT:	Attenuator, BIRI Digital Voltmete DC Power Sourc Modulation Anal	D Model / 9715 / 50-A-MI D Model / 9716 / 25-A-MI r, Fluke Model 8012A e, Model HP6284A lyzer, Model HP8901A zer, Model HP8563E A				
PERFORMED BY:		accerta	DATE: 1/29/99			
TEST SET-UP:	Allen Frederick					
MODEM	TRANSCEIVER UNDER TEST	ATTENUATOR	ATTENUATOR			
POWER SUPPLY	DIGITAL MULTIMETER	SPECTRUM ANALYZER	MODULATION ANALYZER			
		PLOTTER				
156-90002-100	Data	radio ©	FCC submission			

NAME OF TEST:	Transmitter Occupied Bandwidth (Continued)
	INTEGRA Modem at 19200 bps
	In Support of Emission Designator 15K3F1D

MODULATION SOURCE DESCRIPTION:

The digital modulation type used in the INTEGRA is DRCMSK (Differential Raised Cosine Minimum Shift Keying). A modem using such type of modulation is divided into three main functional units in a CPLD chip: Scrambler:

The scrambler converts the data stream to a new data stream more suitable for FM transmission.

-It keeps the power spectrum more compact by avoiding sequences like 01010101...

The scrambler is made with a serial shift register and 2 exclusive OR gates which implement the polynomial form X^7+X^5-1 . For the receiver side, a similar circuit performs the descrambling function to decode the received scrambled data.

Differential encoder:

After data is scrambled, we encode the data with a differential encoder. The differential encoder XOR's the current input bit with the previous bit. The differential encoder is used to make the modem insensitive to audio polarity inversion of the FM radio system.

Waveshape generator:

The waveshape generator converts the processed data bits (scrambled and differentially encoded for DRCMSK) to the DRCMSK audio signal. This audio signal is passed through a low-pass filter before modulating the RF transmitter.

TRANSMISSION PREAMBLE:

Each data transmission begins by sending a 15 millisecond preamble of sinewave (101010...). This is to synchronize the digital phase locked loop of the receiver modem.

TEST PATTERN GENERATOR:

A 30 s test pattern sequence is generated by the test software when the "test data" button is clicked. The highest resulting modulating frequency is (baud rate)/2 Hz. The following pseudo random test pattern was used to modulate the transmitter:

###ABCDEFGHIJKLMNOPQRSTUVWXYZabcdefghijklmnopqrstuvwxyz0123456789\r\n,

In this pattern ### is replaced by the number of replays, \r is a carriage return and \n is a linefeed. The data is fed to the RS232 interface IC and processed as described above. The async-to-sync conversion, scrambler and differential encoder make the ABCDE... pattern appear random over the air.

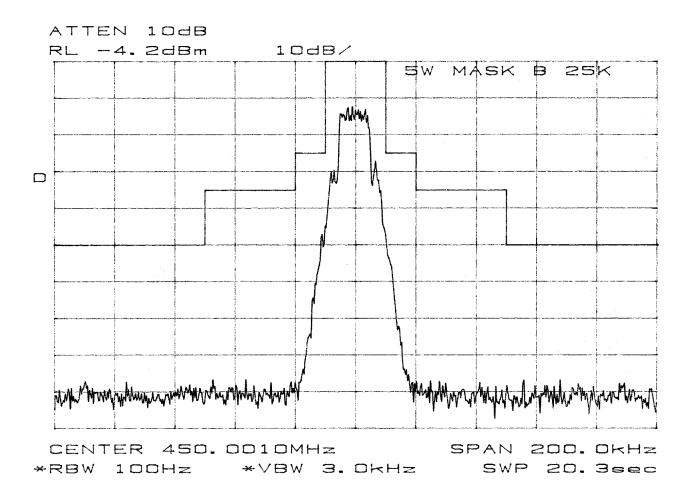
NECESSARY BANDWIDTH (Bn) CALCULATION

See page 13 for Emission Designator determination.

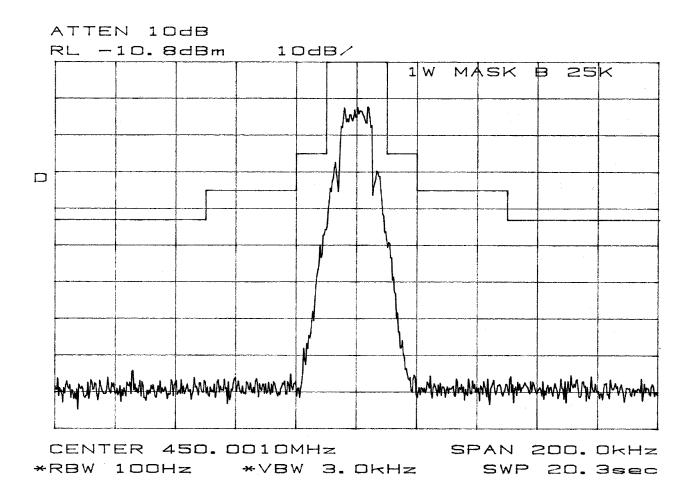
The corresponding emission designator prefix for necessary bandwidth = **15K3**

TEST DATA: Refer to the following graphs:

MASK: B,5W SPECTRUM FOR EMISSION 15K3F1D OUTPUT POWER: 5 Watts 19200 bps PEAK DEVIATION = 4000 Hz SPAN = 200 kHz



MASK: **B,1W** SPECTRUM FOR EMISSION **15K3F1D** OUTPUT POWER: 1 Watts 19200 bps PEAK DEVIATION = 4000 Hz SPAN = 200 kHz



NAME OF TEST: Transmitter Spurious and Harmonic Outputs

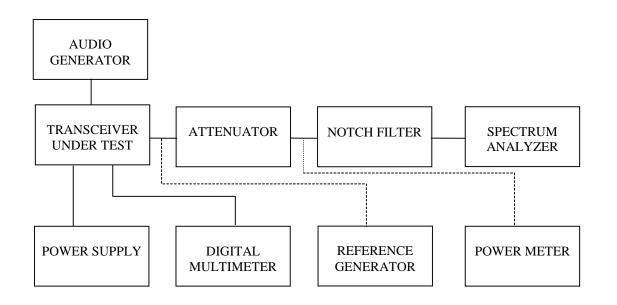
RULE PART NUMBER:	2.1033 c(14), 2.1041, 2.1051, 90.210 (d)(3)
MINIMUM STANDARD:	For 5 Watt; $50+10Log_{10}(5 \text{ Watts}) = -57 \text{ dBc}$ or -70 dBc whichever is the lesser attenuation.
TEST RESULTS:	Meets minimum standard (see data on the following page)
TEST CONDITIONS:	Standard Test Conditions, 25 C RF voltage measured at antenna terminals
TEST PROCEDURE:	TIA/EIA - 603, 2.2.13
TEST EQUIPMENT:	Attenuator, BIRD Model / 9715 / 50-A-MFN-06 / 6 dB / 50 Watt Attenuator, BIRD Model / 9716 / 25-A-MFN-20 / 20 dB / 25 Watt Digital Voltmeter, Fluke Model 8012A DC Power Source, Model HP6284A Modulation Analyzer, Model HP8901A Spectrum Analyzer, Model HP8563E Plotter, HP7470A Reference Generator, Model HP83732B Power Meter, Model HP436A Audio Generator, Model HP8903B

Allen Frederick

PERFORMED BY:

Date:1/28/99

TEST SET-UP:



NAME OF TEST: Transmitter Spurious and Harmonic Outputs (Continued)

MEASUREMENT PROCEDURE:

1. The transmitter carrier output frequency is 403.000, 450.000 and 512.000 MHz. The reference oscillator frequency is 17.5000 MHz.

2. After carrier reference was established on spectrum analyzer, the notch filter was adjusted to null the carrier Fc to extend the range of the spectrum analyzer for harmonic measurements.

3. At each spurious frequency, Generator substitution was used to establish the true spurious level.

4. The spectrum was scanned to the 10th harmonic.

TEST DATA:

Tuned Frequency	403 MHz		Tuned Frequency	403 MHz	
Power	1 Watts		Power	5	Watts
	30.0 c	lBm		37.0	dBm
Minimum Specification	50.0 c	lBm	Minimum Specification	57.0	dBm
Worse Case	68.5 0	lBc	Worse Case	69.5	dBc
Spurious	Relation to	Relative to	Spurious	Relation to	Relative to
Frequency (MHz)	Carrier_	Carrier (dBc)	Frequency (MHz)	Carrier	Carrier (dBc)
806	2 fo	76.0	806	2 fo	69.5
1209	3 fo	91.5	1209	3 fo	75.5
1612	4 fo	68.5	1612	4 fo	73.0
2015	5 fo	96.0	2015	5 fo	102.0
2418	6 fo	95.0	2418	6 fo	99.0
2821	7 fo	93.5	2821	7 fo	96.5
3224	8 fo	94.5	3224	8 fo	98.0
3627	9 fo	85.0	3627	9 fo	90.0
4030	10 fo	95.5	4030	10 fo	96.5

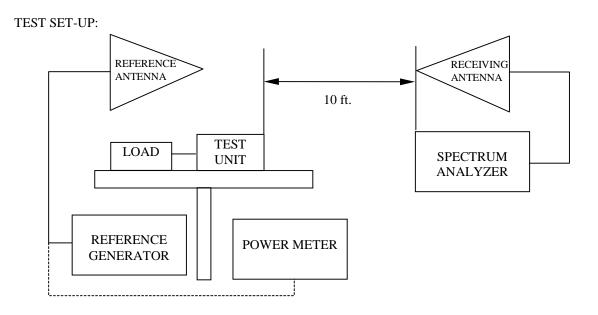
NAME OF TEST: Transmitter Spurious and Harmonic Outputs (Continued)							
Tuned Frequency	450]	MHz	Tuned Frequency	450	MHz		
Power	1 '	Watts	Power	5	Watts		
	30.0 0	dBm		37.0	dBm		
Minimum Specification	50.0 0	dBm	Minimum Specification	57.0	dBm		
Worse Case	72.5 0	dBc	Worse Case	76.5	dBc		
Spurious	rious Relation to Relative to		Spurious	Relation to	Relative to		
Frequency (MHz)	Carrier	Carrier (dBc)	Frequency (MHz)	Carrier	Carrier (dBc)		
900	2 fo	78.5	900	2 fo	86.0		
1303	3 fo	84.5	1303	3 fo	89.5		
1706	4 fo	82.0	1706	4 fo	89.0		
2109	5 fo	84.5	2109	5 fo	88.5		
2512	6 fo	105.5	2512	6 fo	114.0		
2915	7 fo 84.0		2915	7 fo	92.0		
3318	8 fo	72.5	3318	8 fo	76.5		
3721	9 fo	88.5	3721	9 fo	98.5		
4124	10 fo	97.0	4124	10 fo	101.0		
Tuned Frequency	512]	MHz	Tuned Frequency	512	MHz		
Power	1 `	Watts	Power	5	Watts		
	30.0 0	dBm		37.0 dBm			
Minimum Specification	50.0 0	Bm Minimum Specification		57.0	dBm		
Worse Case	67.5 dBc		Worse Case	72.5	dBc		
Spurious	Relation to	Relative to	Spurious	Relation to	Relative to		
Frequency (MHz)	Carrier	Carrier (dBc)	Frequency (MHz)	Carrier	Carrier (dBc)		
1024	2 fo	83.0	1024	2 fo	78.0		
1427	3 fo	84.0	1427	3 fo	79.0		
1830	4 fo	104.5	1830	4 fo	87.5		
2233	5 fo	67.5	2233	5 fo	72.5		
2636	6 fo	87.5	2636 6 fo		94.5		
3039	7 fo	83.0	3039	7 fo	85.5		
3442	8 fo	106.0	3442	8 fo	113.0		
3845	9 fo	92.5	3845	9 fo	86.0		
4248	10 fo	104.0	4248	10 fo	108.0		

RULE PART NUMBER:	2.1033 c(14), 2.1041, 2.1053, 90.210 (d)(3)
MINIMUM STANDARD:	For 5 Watts; $50+10Log_{10}(5) = -57 \text{ dBc}$
TEST RESULTS:	Meets minimum standard (see data on the following page)
TEST CONDITIONS:	Standard Test Conditions, 25 C
TEST PROCEDURE:	TIA/EIA - 603, 2.2.12
Test Equipment:	Dipole Antenna Kit, Electro-Mechanics Model 3121C Load, Tenuline Model 8340-200 (20 dB) Spectrum Analyzer, HP 8563E Reference Generator, HP83732A Power Meter, HP437A

NAME OF TEST: Field Strength of Spurious Radiation

MEASUREMENT PROCEDURE:

Radiated spurious attenuation was measured according to TIA/EIA Standard 603 Section 2.2.12



Alen

PERFORMED BY:

Allen Frederick

DATE: 4/5/99

Freqency: Power:		MHz Watt=30.0dBr	MHz Minimum Spec = Watt=30.0dBm Worse Case =			50.0 52.8	dBc dBc
Spurious			Substitution		Antenna	Circular	Spurious
Frequency	Polarization	Spurious	Generator	Cable Loss	Gain	Polarization	Attenuation
(MHz)	(Horz/Vert)	Level (dBm)	(dBm)	(dB)	(dBd)	Correction (dB)	dBc
900	Н	-54.7	-19.0	5.67	-0.10	0.0	-54.8
	V	-55.0	-17.0	5.67	-0.10	0.0	-52.8
1350	Н	-64.8	-21.0	6.50	1.20	3.0	-59.3
	V	-62.8	-20.0	6.50	1.20	3.0	-58.3
1800	Н	-78.2	-32.0	7.67	1.20	3.0	-71.5
	V	-75.5	-30.0	7.67	1.20	3.0	-69.5
2250	Н	-76.2	-29.0	8.30	1.20	3.0	-69.1
	V	-74.8	-24.0	8.30	1.20	3.0	-64.1
2700	Н	-85.7	-35.0	8.83	1.20	3.0	-75.6
	V	-82.7	-32.0	8.83	1.20	3.0	-72.6
3150	Н	-80.7	-28.0	9.30	1.20	3.0	-69.1
	V	-78.8	-25.0	9.30	1.20	3.0	-66.1
3600	Н	-90.2	-28.0	10.67	1.20	3.0	-70.5
	V	-87.8	-30.0	10.67	1.20	3.0	-72.5
4050	Н	-95.0	-36.0	11.67	1.20	3.0	-79.5
	V	-90.7	-31.0	11.67	1.20	3.0	-74.5
4500	Н	-93.8	-33.0	11.67	1.20	3.0	-76.5
	V	-92.0	-32.0	11.67	1.20	3.0	-75.5

Freqency: Power:		MHz Watts=37.0dB	Hz Minimum Spec = atts=37.0dBm Worse Case =			57.0 60.3	dBc dBc
Spurious			Substitution		Antenna	Circular	Spurious
Frequency	Polarization	Spurious	Generator	Cable Loss	Gain	Polarization	Attenuation
(MHz)	(Horz/Vert)	Level (dBm)	(dBm)	(dB)	(dBd)	Correction (dB)	dBc
900	Н	-53.2	-18.0	5.67	-0.10	0.0	-60.8
	V	-57.0	-18.0	5.67	-0.10	0.0	-60.8
1350	Н	-59.7	-17.0	6.50	1.20	3.0	-62.3
	V	-56.8	-15.0	6.50	1.20	3.0	-60.3
1800	Н	-82.2	-37.0	7.67	1.20	3.0	-83.5
	V	-78.8	-33.6	7.67	1.20	3.0	-80.1
2250	Н	-73.3	-26.0	8.30	1.20	3.0	-73.1
	V	-70.0	-21.0	8.30	1.20	3.0	-68.1
2700	Н	-80.2	-29.0	8.83	1.20	3.0	-76.6
	V	-76.0	-25.0	8.83	1.20	3.0	-72.6
3150	Н	-81.5	-30.0	9.30	1.20	3.0	-78.1
	V	-75.7	-23.0	9.30	1.20	3.0	-71.1
3600	Н	-83.7	-28.0	10.67	1.20	3.0	-77.5
	V	-81.7	-25.0	10.67	1.20	3.0	-74.5
4050	Н	-89.8	-32.0	11.67	1.20	3.0	-82.5
	V	-84.5	-25.0	11.67	1.20	3.0	-75.5
4500	Н	-92.7	-32.0	11.67	1.20	3.0	-82.5
	V	-90.5	-30.0	11.67	1.20	3.0	-80.5
156 90002 100 Detend in @ ECC							

156-90002-100

CALCULATIONS FOR FIELD STRENGTH OF SPURIOUS RADIATION TESTS:

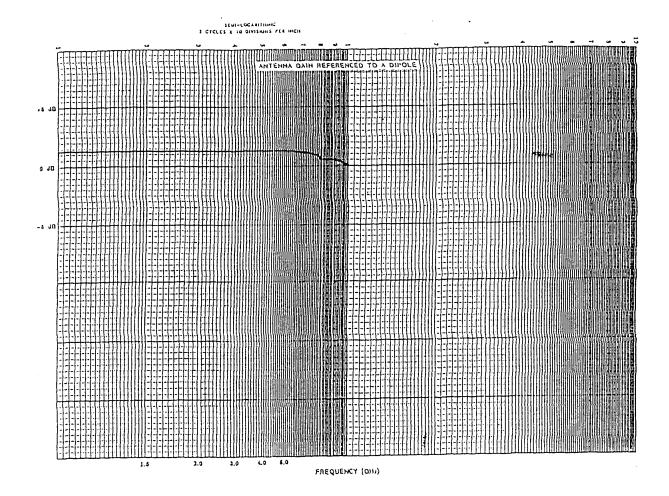
The transmitter carrier frequency was 450.000 MHz. The reference oscillator frequency of all the transceivers used is 17.50 MHz. The output of the transceiver was searched from 17.50 MHz to the tenth harmonic of the carrier frequencies. The tests were conducted with the transceiver and modem inside of the enclosure.

Because the antennas used for the measurements recorded above 1 GHz were not flat in gain and differed from a dipole, the generator output was corrected for gain at each spurious frequency. The cable loss in the measurements is the loss in the cable between the signal generator and the substitution antenna. An additional 3 dB correction was also made to the spurious responses measured above 1 GHz to correct for the 3 dB polarization loss in the reference path.

EXAMPLE:

At 900 MHz (450 MHz tuned), 5 Watts and horizontal polarization.

r = Substitution Gen - Cable Loss	-18.0 - 5.67	= -23.67
R - Reference Generator (dBm)	-23.67	
A - Antenna Gain (dB)	+-0.10	
P - Polarization Correction Factor (dB)	0.0	
R' (Corrected Reference (dBm)) = $R + A - P$	= -23.67 +1 - 0.0	= -23.77 dBm
Po - Radiated Carrier Power (dBm)	5 Watts = 37 dBm	
Radiated Spurious Emission (dBc) = Po - R'	= -23.77 - (+37)	= -60.77 dBc



ANTENNA GAIN GRAPH OF SUBSTITUTION ANTENNA REFERENCED TO A DIPOLE

NAME OF TEST: Frequency Stability

-with Variation in Ambient Temperature

RULE PART NUMBER:	2.1055 (a)(1), 90.213 (a) (7)
MINIMUM STANDARD:	Shall not exceed $\pm 0.000150\%$ from test frequency, or 1.50 ppm
TEST RESULTS:	Meets minimum standard, see data on following page
TEST CONDITIONS:	Standard Test Conditions, 25 C
TEST EQUIPMENT:	Attenuator, BIRD Model / 9715 / 50-A-MFN-06 / 6 dB / 50 Watt Attenuator, BIRD Model / 9716 / 25-A-MFN-20 / 20 dB / 25 Watt Frequency Counter, Fluke Model 1920A Digital Voltmeter, Fluke Model 8012A DC Power Source, Model HP6284A Climate Chamber, TempGard III, Tenney Jr.

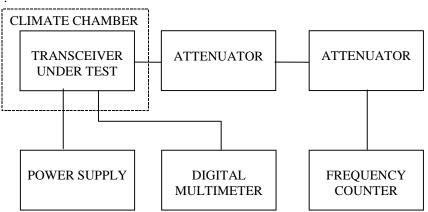
Allen Trederic

PERFORMED BY:

Allen Frederick

DATE: 2/8/99

TEST SET-UP:



(Test data on next page)

NAME OF TEST:

Frequency Stability with Variation in Ambient Temperature (Continued)

Frequency Reference:
Tolerance Requirement:
Highest Variation (ppm):

450000000 Hz 1.5 ppm 0.716 ppm

TEMP	FREQUENCY	FREQ DELTA	ppm from assigned
°C	MHz	Hz	frequency
-30	449999678	-322	0.716
-20	449999794	-206	0.458
-10	449999727	-273	0.607
0	449999794	-206	0.458
10	449999907	-93	0.207
20	449999955	-45	0.100
30	450000156	156	0.347
40	450000039	39	0.087
50	449999863	-137	0.304
60	449999863	-137	0.304

NAME OF TEST: -with Variation in Supply Volta	Frequency Stability ge	
RULE PART NUMBER:	2.1055 (d)	
MINIMUM STANDARD:	Shall not exceed $\pm 0.000150\%$ from test frequency, 1.50 ppm for $\pm 15\%$ change in supply voltage	
TEST RESULTS:	Meets minimum standard, see data on following page	
TEST CONDITIONS:	Standard Test Conditions, 25 C	
TEST EQUIPMENT:	Attenuator, BIRD Model / 9715 / 50-A-MFN-06 / 6 dB / 50 Watt Attenuator, BIRD Model / 9716 / 25-A-MFN-20 / 20 dB / 25 Watt Frequency Counter, Fluke Model 1920A Digital Voltmeter, Fluke Model 8012A DC Power Source, Model HP6284A	
PERFORMED BY: TEST SET-UP:	Allen Frederick DATE: 2/8/99	
TEST UNIT		
(Test data on next page)		

NAME OF TEST:

Frequency Stability with Variation in Supply Voltage (Continued)

MEASUREMENTS TAKEN:

1.5 ppm Reference Oscillator

Frequency Reference Set at 25° C: Tolerance Requirement: Highest Variation (%): Highest Variation (ppm): 450.00001 MHz 0.00015 % 0.0000000 % 0.000 ppm

SUPPLY	FREQUENCY	DELT FREQ	SPEC LIMIT	ppm from assigned
VDC	MHz	% of assigned f	% of assigned f	frequency
10	450.00001	0.00000000	0.00015	0.000
13	450.00001	0.00000000	0.00015	0.000
16	450.00001	0.00000000	0.00015	0.000

NAME OF TEST: Transient Frequency Behavior

RULE PART NUMBER:	90.214
TEST CONDITIONS:	The transient test was performed with the transmitter transmitting an unmodulated carrier tone. Also supplied is a transient test which was conducted with the INTEGRA modem modulating the transmitter at 4 kHz deviation. Also supplied is a transient test which was conducted with the INTEGRA modem modulating the transmitter at 2.5 kHz deviation.
MINIMUM STANDARD:	12.5 kHz channel (used worst case numbers from 403 to 512 MHz)25 kHz channel (used worst case numbers from 403 to 512 MHz)

TIME INTERVAL	MAXIMUM FREQUENCY DIFFERENCE (kHz)		TIME (mS)
	12.5KHz CH	25KHz CH	
T1	+/- 12.5	+/- 25	5
T2	+/- 6.25	+/- 12.5	20
Т3	+/- 12.5	+/- 25	5

TEST RESULTS:	Meets minimum standards, see data on following pages
TEST CONDITIONS:	RF Power Level = 5 Watts Standard Test Conditions, 25 C
TEST PROCEDURE:	TIA/EIA - 603, 2.2.19
TEST EQUIPMENT:	Attenuator, BIRD Model / 9716 / 25-A-MFN-20 / 20 dB / 25 Watt Digital Voltmeter, Fluke Model 8012A DC Power Source, Model HP6284A Modulation Analyzer, Model HP8901A RF Detector (Spectrum Analyzer), Model HP8563E Plotter, Model HP2671G Reference Generator, Fluke Model 6071A Power Meter, Model HP436A Power Combiner, Model MCL ZFSC-4-1 Oscilloscope, Model HP54503A Directional Coupler, Model HP778D

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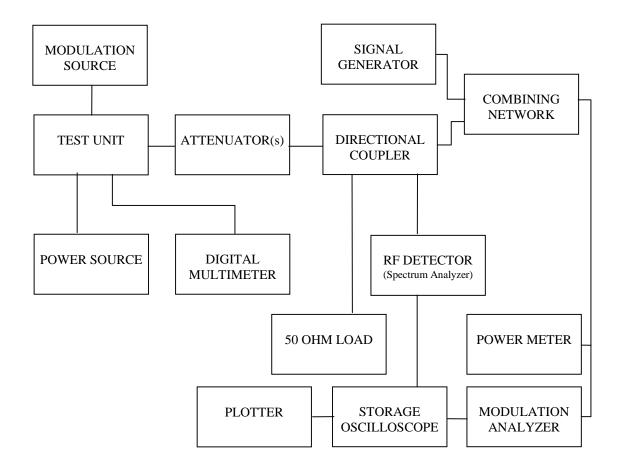
PERFORMED BY:

Allen Frederick

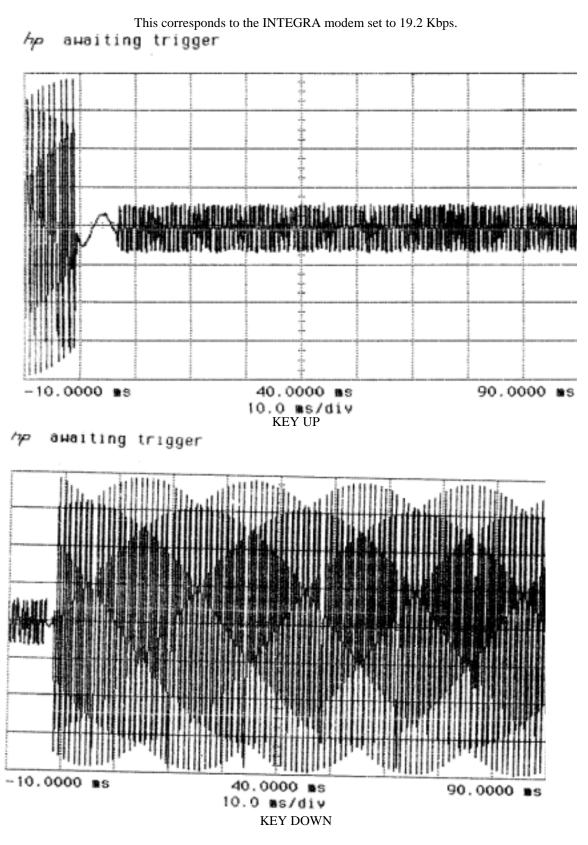
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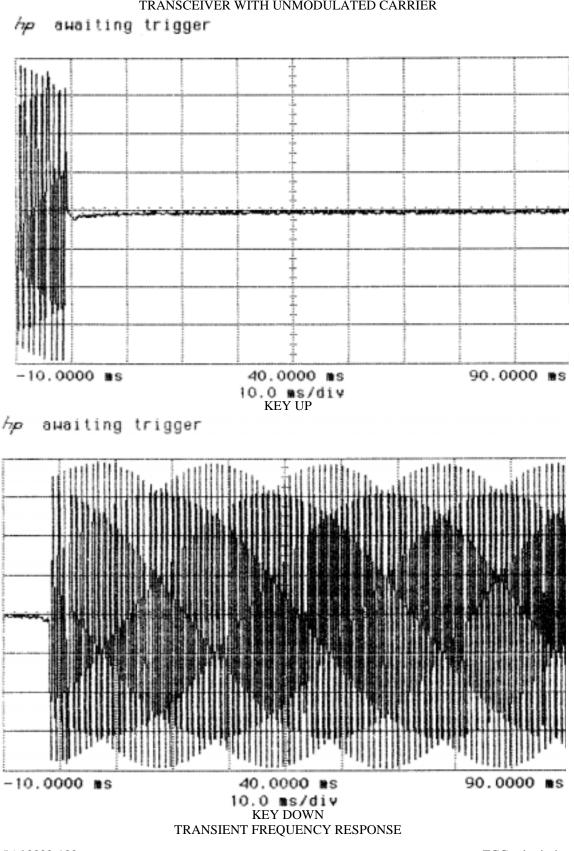
NAME OF TEST:

TEST SET-UP:

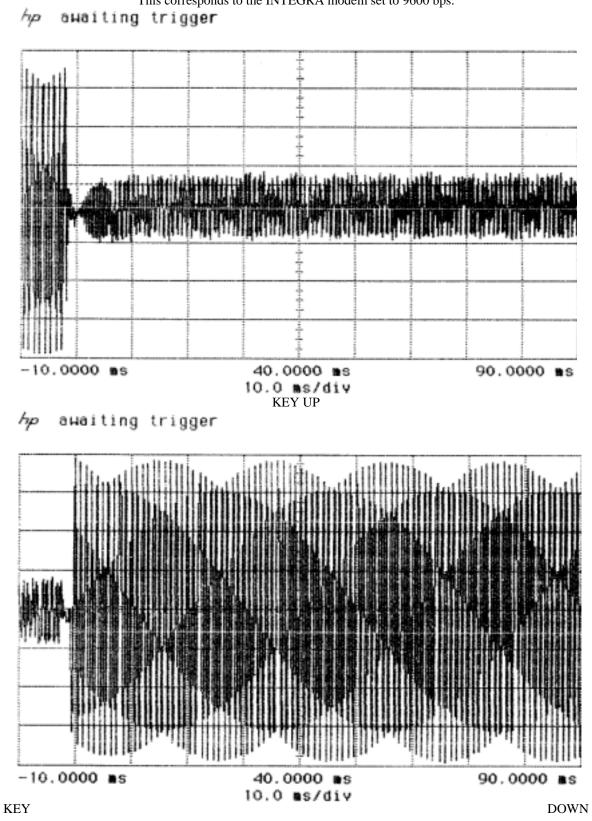


TRANSIENT FREQUENCY RESPONSE TRANSCEIVER MODULATED BY INTEGRA MODEM 4 kHz DEVIATION





TRANSIENT FREQUENCY RESPONSE TRANSCEIVER WITH UNMODULATED CARRIER



TRANSCEIVER MODULATED BY INTEGRA MODEM This corresponds to the INTEGRA modem set to 9600 bps.

