## Itron, Inc

## TEST REPORT FOR

IRM-STAR
Model: OW3

## Tested to The Following Standards:

FCC Part 15 Subpart C Section(s)
15.207 \& 15.247
(FHSS 902-928MHz)

Report No.: 108561-2

Date of issue: November 20, 2023


This test report bears the accreditation symbol indicating that the testing performed herein meets the test and reporting requirements of ISO/IEC 17025 under the applicable scope of testing for CKC Laboratories, Inc.

We strive to create long-term, trust based relationships by providing sound, adaptive, customer first testing services. We embrace each of our customers' unique EMC challenges, not as an interruption to set processes, but rather as the reason we are in business.

Test Certificate \# 803.01

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## ADMINISTRATIVE INFORMATION

## Test Report Information

## REPORT PREPARED FOR:

Itron, Inc.
2111 N. Molter Road
Liberty Lake, WA 99019

Representative: Jack McPeck
Customer Reference Number: 283655

DATE OF EQUIPMENT RECEIPT:
DATES) OF TESTING:

REPORT PREPARED BY:

Viviana Prado
CKC Laboratories, Inc.
5046 Sierra Pines Drive
Mariposa, CA 95338

Project Number: 108561

September 8, 2023
September 8, 11, 13, and 19, 2023
and October 13, 2023

## Report Authorization

The test data contained in this report documents the observed testing parameters pertaining to and are relevant for only the equipment provided by the client, tested in the agreed upon operational modes) and configurations) as identified herein. Compliance assessment remains the client's responsibility. This report may not be used to claim product endorsement by A2LA or any government agencies. This test report has been authorized for release under quality control from CKC Laboratories, Inc.


Steve Behm
Director of Quality Assurance \& Engineering Services
CKC Laboratories, Inc.

## Test Facility Information



Our laboratories are configured to effectively test a wide variety of product types. CKC utilizes first class test equipment, anechoic chambers, data acquisition and information services to create accurate, repeatable, and affordable test results.

TEST LOCATION(S):
CKC Laboratories, Inc.
22116 23rd Drive SE, Suite A Bothell, WA 98021

## Software Versions

| CKC Laboratories Proprietary Software | Version |
| :--- | :--- |
| EMITest Emissions | 5.03 .20 |

## Site Registration \& Accreditation Information

| Location | ${ }^{\text {}}$ NIST CB \# | FCC | Canada | Japan |
| :---: | :---: | :---: | :---: | :---: |
| Canyon Park, Bothell, WA | US0103 | US1024 | 3082C | A-0136 |
| Brea, CA | US0103 | US1024 | 3082D | A-0136 |
| Fremont, CA | US0103 | US1024 | 3082B | A-0136 |
| Mariposa, CA | US0103 | US1024 | $3082 A$ | A-0136 |

*CKC's list of NIST designated countries can be found at: https://standards.gov/cabs/designations.html

## SUMMARY OF RESULTS

Standard / Specification: FCC Part 15 Subpart C-15.247 (FHSS 902-928MHz)

| Test Procedure | Description | Modifications | Results |
| :--- | :--- | :--- | :--- |
| $15.247(\mathrm{a})(1)(\mathrm{i})$ | Occupied Bandwidth | NA | NP |
| $15.247(\mathrm{a})(1)$ | Carrier Separation | NA | NP |
| $15.247(\mathrm{a})(1)(\mathrm{i})$ | Number of Hopping Channels | NA | NP |
| $15.247(\mathrm{a})(1)(\mathrm{i})$ | Average Time of Occupancy | NA | NP |
| $15.247(\mathrm{~b})(2)$ | Output Power | NA | Pass |
| $15.247(\mathrm{~d})$ | RF Conducted Emissions \& Band Edge | NA | NP |
| $15.247(\mathrm{~d})$ | Radiated Emissions \& Band Edge | NA | Pass |
| 15.207 | AC Conducted Emissions | NA | Pass |

NA = Not Applicable
NP = CKC Laboratories was not contracted to perform test.

## ISO/IEC 17025 Decision Rule

The equipment sample utilized for testing is selected by the manufacturer. The declaration of pass or fail herein is a binary statement for simple acceptance rule (ILAC G8) based upon assessment to the specification(s) listed above, without consideration of measurement uncertainties. For performance related tests, equipment was monitored for specified criteria identified in that section of testing.

## Modifications During Testing

This list is a summary of the modifications made to the equipment during testing.

## Summary of Conditions

No modifications were made during testing.

Modifications listed above must be incorporated into all production units.

This list is a summary of the conditions noted to the equipment during testing.

## Summary of Conditions

None

## EQUIPMENT UNDER TEST (EXT)

During testing, numerous configurations may have been utilized. The configurations listed below support compliance to the standards) listed in the Summary of Results section.

## Configuration 1

Equipment Tested:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| IRM-STAR | tron, Inc. | OW3 | 354233798 |

Support Equipment:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Integrated Multi-purpose | Cisco | ANT-5G-MP-OUT-N | NA |
| Antenna |  | ANT-5G-MP-OUT-N | NA |
| Integrated Multi-purpose Cisco Latitude E6430 NA <br> Antenna Dell ANT-5G-MP-OUT-N NA <br> Laptop Cisco IR8140H NA <br> Integrated Multi-purpose <br> Antenna Cisco   <br> Router Host    $\mathbf{l}$ |  |  |  |

## Configuration 2

Equipment Tested:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| IRM-STAR | Itron, Inc. | OW3 | 354233798 |

Support Equipment:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Integrated Multi-purpose | Cisco | ANT-5G-MP-OUT-N | NA |
| Antenna |  | ANT-5G-MP-OUT-N | NA |
| Integrated Multi-purpose <br> Antenna | Cisco | Latitude E6430 | NA |
| Laptop | Dell | BOA9025NM-ITR | NA |
| Antenna (5.5 dBi remote PCTEL  NA <br> ISM) Cisco IR8140H  $\mathbf{l}$ |  |  |  |

Configuration 3
Equipment Tested:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| IRM-STAR | Itron, Inc. | OW3 | 354233798 |

Support Equipment:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Integrated Multi-purpose <br> Antenna | Cisco | ANT-5G-MP-OUT-N | NA |
| Integrated Multi-purpose <br> Antenna | Cisco | ANT-5G-MP-OUT-N | NA |
| Laptop | Dell | Latitude E6430 | NA |
| Antenna (8.15 dBi remote <br> ISM) | PCTEL | BOA9028 | NA |
| 1dB Attenuator (Qty: 2) | Mini-Circuits | 15542 UNAT-1+ | NA |
| Surge Protector | Times Microwave Systems | LP-BTRW-NMP | NA |
| Router Host | Cisco | IR8140H | NA |

## Configuration 4

Equipment Tested:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| IRM-STAR | Itron, Inc. | OW3 | 354233798 |
|  |  |  |  |
| Support Equipment: |  |  |  |
| Device | Manufacturer | Model \# | S/N |
| Laptop | Dell | Latitude E6430 | NA |
| Router Host | Cisco | IR8140H | NA |

## Configuration 5

Equipment Tested:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| IRM-STAR | Itron, Inc. | OW3 | 354233791 |

## Support Equipment:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Integrated Multi-purpose <br> Antenna | Cisco | ANT-5G-MP-OUT-N | NA |
| Integrated Multi-purpose <br> Antenna | Cisco | ANT-5G-MP-OUT-N | NA |
| Laptop | Dell | Latitude E6430 | NA |
| Integrated Multi-purpose Cisco ANT-5G-MP-OUT-N NA <br> Antenna Cisco IR8140H NA <br> Router Host    $\mathbf{l}$ |  |  |  |

## Configuration 6

Equipment Tested:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| IRM-STAR | Itron, Inc. | OW3 | 354233791 |

Support Equipment:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Integrated Multi-purpose <br> Antenna | Cisco | ANT-5G-MP-OUT-N | NA |
| Integrated Multi-purpose <br> Antenna | Cisco | ANT-5G-MP-OUT-N | NA |
| Laptop | Dell | Latitude E6430 | NA |
| Antenna (5.5 dBi remote <br> ISM) | PCTEL | BOA9025NM-ITR | NA |
| Router Host | Cisco | IR8140H | NA |

## Configuration 7

Equipment Tested:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| IRM-STAR | Itron, Inc. | OW3 | 354233791 |

Support Equipment:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Integrated Multi-purpose <br> Antenna | Cisco | ANT-5G-MP-OUT-N | NA |
| Integrated Multi-purpose <br> Antenna | Cisco | ANT-5G-MP-OUT-N | NA |
| Laptop | Dell | Latitude E6430 | NA |
| Antenna (8.15 dBi remote PCTEL BOA9028 NA <br> ISM) Cisco IR8140H NA <br> Router Host    $\mathbf{l}$ |  |  |  |

## Configuration 8

Equipment Tested:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| IRM-STAR | Itron, Inc. | OW3 | 354233802 |
|  |  |  |  |
| Support Equipment: |  |  |  |
| Device | Manufacturer | Model \# | S/N |
| Laptop | Dell | Latitude E6430 | NA |
| 12V Power Supply | Cisco | IR8140 Power Module | NA |

## General Product Information:

| Product Information | Manufacturer-Provided Details |
| :---: | :---: |
| Equipment Type: | Limited Modular, CISCO IR8140H Host |
| Type of Wideband System: | Proprietary FHSS |
| Operating Frequency Range: | $902.20-927.75 \mathrm{MHz}$ |
| Number of Hopping Channels: | 512 |
| Receiver Bandwidth and Synchronization: | The manufacturer declares the receiver input bandwidth matches the transmit channel bandwidth and shifts frequencies in synchronization with the transmitter. |
| Modulation Type(s): | 10k and 25k GFSK |
| Maximum Duty Cycle: | Tested 100\% as worst case |
| Number of TX Chains: | 1 |
| Antenna Type(s) and Gain: | $1 \times$ external attached 2.0 dBi 1 x external remote 5.5 dBi <br> 1 x external remote 8.15 dBi (requires 3 dB of cable loss/attenuators to be attached per manufacturer) |
| Beamforming Type: | N/A |
| Antenna Connection Type: | External Connector |
| Nominal Input Voltage: | $115 \mathrm{VAC}, 60 \mathrm{~Hz}$ |
| Firmware / Software used for Test: | CAM3 FCC Test Helper v1 Putty Release 0.78 Firmware 5.3.194 |
| The validity of results is dependent on the stated product details, the accuracy of which the manufacturer assumes full responsibility. |  |

EUT Photo(s)


Support Equipment Photo(s)


Antenna Configuration 1 and Cellular


Antenna Configuration 2


Antenna Configuration 3


Laptop

Block Diagram of Test Setup(s)

## Test Setup Block Diagram



## FCC Part 15 Subpart C

### 15.247(b)(2) Output Power

| Test Data Summary - Voltage Variations |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Frequency <br> $(\mathbf{M H z})$ | Modulation / Ant Port | $\mathbf{V}_{\text {Minimum }}$ <br> $(\mathbf{d B m})$ | $\mathbf{V}_{\text {Nominal }}$ <br> $(\mathbf{d B m})$ | $\mathbf{V}_{\text {Maximum }}$ <br> $(\mathbf{d B m})$ | Max Deviation <br> from $\mathbf{V}_{\text {Nominal }}(\mathbf{d B})$ |
| 902.2 | 10 kHz FSK | 25.4 | 25.4 | 25.4 | 0.0 |
| 915.0 | 10 kHz FSK | 26.0 | 26.0 | 26.0 | 0.0 |
| 927.75 | 10 kHz FSK | 24.5 | 24.5 | 24.5 | 0.0 |
| 902.2 | 25 kHz FSK | 25.3 | 25.3 | 25.3 | 0.0 |
| 915.0 | 25 kHz FSK | 25.9 | 25.9 | 25.9 | 0.0 |
| 927.75 | 25 kHz FSK | 24.5 | 24.5 | 24.5 | 0.0 |

Test performed using operational mode with the highest output power, representing worst case.

## Parameter Definitions:

Measurements performed at input voltage Vnominal $\pm 15 \%$.

| Parameter | Value |
| :--- | :--- |
| $\mathrm{V}_{\text {Nominal }}:$ | $132.25 \mathrm{~V} / 60 \mathrm{~Hz}$ |
| $\mathrm{~V}_{\text {Minimum }}:$ | $115 \mathrm{~V} / 60 \mathrm{~Hz}$ |
| $\mathrm{~V}_{\text {Maximum: }}:$ | $97.75 \mathrm{~V} / 60 \mathrm{~Hz}$ |

Test Data Summary - RF Conducted Measurement
Limit $=\left\{\begin{array}{l}30 \mathrm{dBm} \text { Conducted } / 36 \mathrm{dBm} \text { EIRP } \mid \geq 50 \text { Channels } \\ 24 \mathrm{dBm} \text { Conducted } / 30 \mathrm{dBm} \text { EIRP } \mid<50 \text { Channels (min 25) }\end{array}\right.$

| $\begin{gathered} \text { Frequency } \\ \text { (MHz) } \\ \hline \end{gathered}$ | Modulation | Ant. Type / Gain (dBi) | Measured (dBm) | Limit (dBm) | Results |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 902.2 | 10kHz FSK | Multi-purpose 2 dBi , Omni 5.5 dBi and Remote ISM 8.15 dBi with $>2.15$ cable loss. | 25.4 | $\leq 30$ | Pass |
| 915.0 | 10kHz FSK | Multi-purpose $2 \mathrm{dBi}, 0 \mathrm{mni} 5.5 \mathrm{dBi}$ and Remote ISM 8.15 dBi with $>2.15$ cable loss. | 26.0 | $\leq 30$ | Pass |
| 927.75 | 10kHz FSK | Multi-purpose 2 dBi , Omni 5.5 dBi and Remote ISM 8.15 dBi with $>2.15$ cable loss. | 24.5 | $\leq 30$ | Pass |
| 902.2 | 25kHz FSK | Multi-purpose $2 \mathrm{dBi}, \mathrm{Omni} 5.5 \mathrm{dBi}$ and Remote ISM 8.15 dBi with $>2.15$ cable loss. | 25.3 | $\leq 30$ | Pass |
| 915.0 | 25 kHz FSK | Multi-purpose $2 \mathrm{dBi}, O m n i 5.5 \mathrm{dBi}$ and Remote ISM 8.15 dBi with $>2.15$ cable loss. | 25.9 | $\leq 30$ | Pass |
| 927.75 | 25 kHz FSK | Multi-purpose $2 \mathrm{dBi}, \mathrm{Omni} 5.5 \mathrm{dBi}$ and Remote ISM 8.15 dBi with $>2.15$ cable loss. | 24.5 | $\leq 30$ | Pass |

## Plots

10kHz FSK


Low Channel


Middle Channel


High Channel

25kHz FSK


Low Channel


Middle Channel

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High Channel

## Test Setup / Conditions / Data

Test Location:
Customer:
Specification: Work Order \#: Test Type:
Tested By:
Software:

CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A • Bothell, WA 98021•(425) 402-1717 Itron, Inc.
15.247(b) Power Output (902-928 MHz DTS)

108561
Conducted Emissions
Steven Pittsford
EMITest 5.03.20

Date: 9/13/2023
Time: 07:59:30
Sequence\#: 21
230 V 50 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 4 |  | S/N |

## Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 4 |  | S/N |

## Test Conditions / Notes:

Test Environment Conditions:
Temperature: $24^{\circ} \mathrm{C}$
Humidity: $47 \%$
Pressure: 101.5 kPa

Test Method: ANSI C63.10 (2013)

Frequency Range: $902.2,915 \mathrm{MHz}$, and 927.75 MHz
Test Setup:
Transmitting continuously with modulation at $902.20 \mathrm{MHz}, 915.00 \mathrm{MHz}$, and 927.75 MHz .10 k and 25 k modulations investigated.

Top two LTE antenna ports have Cisco p/n ANT-5G-MP-OUT-N antennas attached.
Itron IRM-Star (CAM3) radio module has Cisco p/n ANT-5G-MP-OUT-N, PCTEL p/n BOA9025NM-ITR, or PCTEL p/n BOA9028 antenna attached. Worst case reported.
EUT Connected to support laptop via shielded Ethernet cable.
Vertical and horizontal antenna polarities investigated, worst case reported.
$2 \times 31$ material ferrites with 3 wraps each on Ethernet cable underneath the ground plane. The ferrites are out of the test volume and these are NOT considered a modification.

No change during voltage variations.
tron. Inc. WO\#: 108561 Sequence\#: 21 Date: 9/13/2023
15.247 (b) Power Output (902-928 MHz DTS) Test Lead: 230 V 50 Hz Ant


Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | ANP06219 | Attenuator | $768-10$ | $3 / 23 / 2022$ | $3 / 23 / 2024$ |
| T2 | ANP05546 | Cable | Heliax | $8 / 1 / 2023$ | $8 / 1 / 2025$ |
| T3 | ANP06515 | Cable | Heliax | $3 / 1 / 2023$ | $3 / 1 / 2025$ |

Measurement Data: $\quad$ Reading listed by margin. $\quad$ Test Lead: Ant


Test Setup Photo(s)


LABORATORIES, INC.

### 15.247(d) Radiated Emissions \& Band Edge

## Test Setup / Conditions / Data

Test Location: CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A•Bothell, WA 98021• (425) 402-1717

Customer:
Specification:
Work Order \#:
Test Type
Tested By:
Software:

Itron, Inc.
15.247(d) / 15.209 Radiated Spurious Emissions

108561 Date: 9/11/2023
Maximized Emissions Time: 6:31:38 AM
Steven Pittsford
EMITest 5.03.20

Sequence\#: 20

## Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1, 2, \& 3 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1, 2, \& 3 |  | S/N |

## Test Conditions / Notes:

Test Environment Conditions:
Temperature: $24^{\circ} \mathrm{C}$
Humidity: $47 \%$
Pressure: 101.5 kPa

Test Method: ANSI C63.10 (2013)
Frequency Range: $9 \mathrm{k}-30 \mathrm{MHz}$
Test Setup:
Transmitting continuously with modulation at $902.20 \mathrm{MHz}, 915.00 \mathrm{MHz}$, and 927.75 MHz .10 k and 25 k modulations investigated.

Top two LTE antenna ports have Cisco p/n ANT-5G-MP-OUT-N antennas attached.
Itron IRM-Star (CAM3) radio module has Cisco p/n ANT-5G-MP-OUT-N, PCTEL p/n BOA9025NM-ITR, or PCTEL p/n BOA9028 antenna attached. Worst case reported.
EUT Connected to support laptop via shielded Ethernet cable.
Perpendicular, parallel, and ground parallel antenna polarities investigated, worst case reported.
$2 \times 31$ material ferrites with 3 wraps each on Ethernet cable underneath the ground plane. The ferrites are out of the test volume and these are NOT considered a modification.

Itron, Inc. WO\#: 108561 Sequence\#: 20 Date: 9/11/2023
15.247 (d) / 15.209 Radiated Spurious Emissions Test Distance: 3 Meters Perp, Para \& Ground Para

—— Readings
$\times$ QP Readings
$\times$ Ambient
$\quad 1-15.247$ (d) / 15.209 Radiated Spurious Emissions

O Peak Readings

* Average Readings

Software Version: 5.03.20

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :---: | :--- | :--- | :--- | :--- | :--- |
|  | AN02673 | Spectrum Analyzer | E4446A | $3 / 2 / 2023$ | $3 / 2 / 2025$ |
| T1 | ANP05546 | Cable | Heliax | $8 / 1 / 2023$ | $8 / 1 / 2025$ |
| T2 | AN00052 | Loop Antenna | 6502 | $5 / 11 / 2022$ | $5 / 11 / 2024$ |
| T3 | ANP06515 | Cable | Heliax | $3 / 1 / 2023$ | $3 / 1 / 2025$ |

Measurement Data: $\quad$ Reading listed by margin. Test Distance: 3 Meters

| \# | Freq <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 3 \\ & \mathrm{~dB} \end{aligned}$ | dB | Dist Table | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \end{gathered}$ | $\begin{gathered} \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \end{gathered}$ | Margin dB | Polar Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 505.000k | 40.0 | +0.0 | +9.3 | +0.0 |  | -40.0 | 9.3 | 33.5 | -24.2 | Perp, |
| 2 | 495.800k | 39.2 | +0.0 | +9.3 | +0.0 |  | -40.0 | 8.5 | 33.7 | -25.2 | Perp, |
| 3 | 2.180M | 22.7 | +0.0 | +9.2 | +0.1 |  | -40.0 | -8.0 | 29.5 | -37.5 | Perp, |
| 4 | 25.522 M | 23.3 | +0.1 | +5.7 | +0.3 |  | -40.0 | -10.6 | 29.5 | -40.1 | Perp, |
| 5 | 13.369M | 16.1 | +0.1 | +8.6 | +0.2 |  | -40.0 | -15.0 | 29.5 | -44.5 | Perp, |
| 6 | 4.126M | 14.5 | +0.1 | +8.9 | +0.1 |  | -40.0 | -16.4 | 29.5 | -45.9 | Perp, |
| 7 | 6.216M | 13.1 | +0.1 | +8.9 | +0.1 |  | -40.0 | -17.8 | 29.5 | -47.3 | Perp, |
| 8 | 8.378M | 9.5 | +0.1 | +8.9 | +0.1 |  | -40.0 | -21.4 | 29.5 | -50.9 | Perp, |
| 9 | 8.414M | 7.7 | +0.1 | +9.0 | +0.1 |  | -40.0 | -23.1 | 29.5 | -52.6 | Perp, |
| 10 | 94.927 k | 36.8 | +0.0 | +9.4 | +0.0 |  | -80.0 | -33.8 | 28.0 | -61.8 | Perp, |
| 11 | 92.168k | 35.4 | +0.0 | +9.5 | +0.0 |  | -80.0 | -35.1 | 28.3 | -63.4 | Perp, |
| 12 | 104.963k | 33.8 | +0.0 | +9.4 | +0.0 |  | -80.0 | -36.8 | 27.2 | -64.0 | Perp, |
| 13 | 106.217k | 33.5 | +0.0 | +9.4 | +0.0 |  | -80.0 | -37.1 | 27.1 | -64.2 | Perp, |
| 14 | 108.224k | 32.6 | +0.0 | +9.4 | +0.0 |  | -80.0 | -38.0 | 26.9 | -64.9 | Perp, |
| 15 | 100.070k | 33.0 | +0.0 | +9.4 | +0.0 |  | -80.0 | -37.6 | 27.6 | -65.2 | Perp, |

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Test Location: CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A•Bothell, WA 98021•(425) 402-1717
Itron, Inc.
15.247(d) / 15.209 Radiated Spurious Emissions

108561 Date: 9/11/2023
Maximized Emissions
Steven Pittsford
EMITest 5.03.20

Time: 11:58:47
Sequence\#: 21

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1, 2, \& 3 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1, $2, \& 3$ |  | S/N |

Test Conditions / Notes:
Test Environment Conditions:
Temperature: $24^{\circ} \mathrm{C}$
Humidity: 47\%
Pressure: 101.5 kPa
Test Method: ANSI C63.10 (2013)
Frequency Range: $30 \mathrm{MHz}-9.28 \mathrm{GHz}$
Test Setup:
Transmitting continuously with modulation at $902.20 \mathrm{MHz}, 915.00 \mathrm{MHz}$, and 927.75 MHz .10 k and 25 k modulations investigated.

Top two LTE antenna ports have Cisco p/n ANT-5G-MP-OUT-N antennas attached.
Itron IRM-Star (CAM3) radio module has Cisco p/n ANT-5G-MP-OUT-N, PCTEL p/n BOA9025NM-ITR, or PCTEL p/n BOA9028 antenna attached. Worst case reported.
EUT Connected to support laptop via shielded Ethernet cable.
Vertical and horizontal antenna polarities investigated, worst case reported.
$2 \times 31$ material ferrites with 3 wraps each on Ethernet cable underneath the ground plane. The ferrites are out of the test volume and these are NOT considered a modification.

```
Itron, Inc. WO#: 108561 Sequence#: 21 Date: 9/11/2023
```

15.247(d) / 15.209 Radiated Spurious Emissions Test Distance: 3 Meters Horiz


```
-_Readings
\(\times\) QP Readings
- Ambient
1-15.247(d) / 15.209 Radiated Spurious Emissions
```

O Peak Readings

* Average Readings

Software Version: 5.03.20

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02673 | Spectrum Analyzer | E4446A | $3 / 2 / 2023$ | $3 / 2 / 2025$ |
| T2 | AN03824 | Biconilog Antenna | 3142E | $5 / 9 / 2023$ | $5 / 9 / 2025$ |
| T3 | ANP05360 | Cable | RG214 | $8 / 8 / 2023$ | $8 / 8 / 2025$ |
| T4 | ANP05333 | Cable | Heliax | $8 / 8 / 2023$ | $8 / 8 / 2025$ |
| T5 | ANP05546 | Cable | Heliax | $8 / 1 / 2023$ | $8 / 1 / 2025$ |
| T6 | ANP06515 | Cable | Heliax | $3 / 1 / 2023$ | $3 / 1 / 2025$ |
| T7 | AN03170 | High Pass Filter | HM1155-11SS | $9 / 16 / 2021$ | $9 / 16 / 2023$ |
| T8 | AN03540 | Preamp | 83017A | $3 / 24 / 2023$ | $3 / 24 / 2025$ |
| T9 | AN02374ANSI | Horn Antenna | RGA-60 | $5 / 26 / 2023$ | $5 / 26 / 2025$ |
| T10 | ANP07504 | Cable | CLU40-KMKM- | $1 / 24 / 2023$ | $1 / 24 / 2025$ |
|  |  |  | $02.00 F$ |  |  |

Measurement Data: $\quad$ Reading listed by margin.
Test Distance: 3 Meters

| \# Freq $\mathrm{MHz}$ | Rdng $\mathrm{dB} \mu \mathrm{~V}$ | $\begin{aligned} & \hline \mathrm{T} 1 \\ & \mathrm{~T} 5 \\ & \mathrm{~T} 9 \\ & \mathrm{~dB} \\ & \hline \end{aligned}$ | $\begin{gathered} \hline \mathrm{T} 2 \\ \mathrm{~T} 6 \\ \mathrm{~T} 10 \\ \mathrm{~dB} \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{T} 3 \\ & \mathrm{~T} 7 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 4 \\ & \mathrm{~T} 8 \\ & \\ & \mathrm{~dB} \\ & \hline \end{aligned}$ | Dist <br> Table | Corr $\mathrm{dB} \mu \mathrm{~V} / \mathrm{m}$ | Spec $\mathrm{dB} \mu \mathrm{~V} / \mathrm{m}$ | Margin $\mathrm{dB}$ | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 1 \quad 610.826 \mathrm{M} \\ & \mathrm{QP} \end{aligned}$ | 9.3 | $\begin{aligned} & +0.0 \\ & +0.5 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline+27.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+2.3 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+1.2 \\ & +0.0 \end{aligned}$ | +0.0 | 40.5 | 46.0 | -5.5 | $\begin{array}{r} \hline \text { Vert } \\ 129 \end{array}$ |
| $\wedge 610.826 \mathrm{M}$ | 15.9 | $\begin{aligned} & +0.0 \\ & +0.5 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+27.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+2.3 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+1.2 \\ & +0.0 \end{aligned}$ | +0.0 | 47.1 | 46.0 | +1.1 | $\begin{array}{r} \hline \text { Vert } \\ 129 \end{array}$ |
| 3 5413.200M | 37.6 | $\begin{array}{r} +0.0 \\ +1.7 \\ +34.4 \end{array}$ | $\begin{array}{r} +0.0 \\ +4.9 \\ +1.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.0 \\ & +0.4 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -33.8 \end{array}$ | +0.0 | 46.2 | $\begin{aligned} & 54.0 \\ & \text { Low } \end{aligned}$ | -7.8 | $\begin{array}{r} \hline \text { Vert } \\ 160 \end{array}$ |
| $\begin{aligned} & 4 \quad 964.260 \mathrm{M} \\ & \mathrm{QP} \end{aligned}$ | 9.4 | $\begin{aligned} & +0.0 \\ & +0.7 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +31.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +2.6 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+1.6 \\ & +0.0 \end{aligned}$ | +0.0 | 45.3 | 54.0 | -8.7 | $\begin{array}{r} \hline \text { Vert } \\ 400 \end{array}$ |
| $\wedge 964.260 \mathrm{M}$ | 15.4 | $\begin{aligned} & +0.0 \\ & +0.7 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+31.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+2.6 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+1.6 \\ & +0.0 \end{aligned}$ | +0.0 | 51.3 | 54.0 | -2.7 | $\begin{gathered} \hline \text { Vert } \\ 129 \end{gathered}$ |
| 63662.060 M | 41.4 | $\begin{array}{r} +0.0 \\ +1.4 \\ +31.4 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.0 \\ & +3.7 \\ & +0.9 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.2 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -34.0 \end{array}$ | $+0.0$ | $45.0$ | $\begin{aligned} & \text { Mid } \\ & \text { M4.0 } \end{aligned}$ | -9.0 | $\begin{array}{r} \hline \text { Vert } \\ 145 \end{array}$ |
| 7 4636.380M | 38.9 | $\begin{array}{r} +0.0 \\ +1.3 \\ +32.4 \end{array}$ | $\begin{aligned} & +0.0 \\ & +4.2 \\ & +1.4 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.4 \end{aligned}$ | $\begin{gathered} +0.0 \\ -33.8 \end{gathered}$ | +0.0 | $44.8$ | $\begin{aligned} & 54.0 \\ & \text { High } \end{aligned}$ | -9.2 | $\begin{gathered} \hline \text { Vert } \\ 169 \end{gathered}$ |
| $\begin{gathered} 8998.043 \mathrm{M} \\ \mathrm{QP} \end{gathered}$ | 9.5 | $\begin{aligned} & +0.0 \\ & +0.7 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+30.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+2.6 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +1.6 \\ & +0.0 \end{aligned}$ | +0.0 | 44.7 | 54.0 | -9.3 | $\begin{gathered} \text { Horiz } \\ 400 \end{gathered}$ |
| 9 4576.970M | 38.8 | $\begin{array}{r} +0.0 \\ +1.3 \\ +32.2 \end{array}$ | $\begin{aligned} & \hline+0.0 \\ & +4.2 \\ & +1.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.5 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -33.8 \end{array}$ | +0.0 | $44.5$ | $\begin{aligned} & \text { Mid } \\ & \text { M4.0 } \end{aligned}$ | -9.5 | $\begin{array}{r} \text { Vert } \\ 145 \end{array}$ |
| $\begin{gathered} 10 \quad 403.640 \mathrm{M} \\ \mathrm{QP} \end{gathered}$ | 9.3 | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+24.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.5 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+1.0 \\ & +0.0 \end{aligned}$ | $+0.0$ | 36.2 | 46.0 | -9.8 | $\begin{array}{r} \hline \text { Vert } \\ 103 \end{array}$ |
| $\wedge 403.640 \mathrm{M}$ | 16.1 | $\begin{aligned} & \hline+0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+24.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.5 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+1.0 \\ & +0.0 \end{aligned}$ | +0.0 | 43.0 | 46.0 | -3.0 | $\begin{array}{r} \hline \text { Vert } \\ 129 \end{array}$ |
| 12 4511.000M | 38.8 | $\begin{array}{r} +0.0 \\ +1.2 \\ +32.1 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +4.2 \\ & +1.1 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.5 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -33.8 \end{array}$ | +0.0 | $44.1$ | $\begin{aligned} & 54.0 \\ & \text { Low } \end{aligned}$ | -9.9 | $\begin{gathered} \hline \text { Vert } \\ 160 \end{gathered}$ |
| 13 3608.800M | 40.0 | $\begin{array}{r} +0.0 \\ +1.4 \\ +31.3 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +3.7 \\ & +1.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.3 \end{aligned}$ | $\begin{gathered} +0.0 \\ -34.0 \end{gathered}$ | $+0.0$ | $43.7$ | $\begin{aligned} & 54.0 \\ & \text { Low } \end{aligned}$ | -10.3 | $\begin{gathered} \hline \text { Vert } \\ 160 \end{gathered}$ |
| 14 3708.790M | 37.8 | $\begin{array}{r} +0.0 \\ +1.5 \\ +31.6 \end{array}$ | $\begin{aligned} & +0.0 \\ & +3.6 \\ & +0.8 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.2 \end{aligned}$ | $\begin{gathered} +0.0 \\ -33.9 \end{gathered}$ | $+0.0$ | $41.6$ | $\begin{aligned} & 54.0 \\ & \text { High } \end{aligned}$ | -12.4 | $\begin{gathered} \hline \text { Vert } \\ 169 \end{gathered}$ |

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| $\begin{gathered} 15{ }^{37.664 \mathrm{M}} \\ \mathrm{QP} \end{gathered}$ | 9.2 | $\begin{aligned} & +0.0 \\ & +0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+17.6 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.4 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.3 \\ & +0.0 \end{aligned}$ | +0.0 | 27.6 | 40.0 | -12.4 | $\begin{array}{r} \hline \text { Vert } \\ 103 \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge 37.664 \mathrm{M}$ | 15.8 | $\begin{aligned} & +0.0 \\ & +0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +17.6 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.4 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.3 \\ & +0.0 \end{aligned}$ | $+0.0$ | 34.2 | 40.0 | -5.8 | $\begin{gathered} \hline \text { Vert } \\ 99 \end{gathered}$ |
| 17 2706.600M | 40.6 | $\begin{array}{r} +0.0 \\ +1.2 \\ +29.3 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +3.0 \\ & +0.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.2 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -34.5 \end{array}$ | +0.0 |  | $54.0$ | -13.7 | $\begin{array}{r} \hline \text { Vert } \\ 160 \end{array}$ |
| 18 2783.625M | 40.4 | $\begin{array}{r} +0.0 \\ +1.2 \\ +29.3 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +3.0 \\ & +0.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.3 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -34.5 \end{array}$ | $+0.0$ |  | $\begin{aligned} & 54.0 \\ & \text { gh } \end{aligned}$ | -13.8 | $\begin{array}{r} \hline \text { Vert } \\ 169 \end{array}$ |
| $\begin{aligned} & 19329.449 \mathrm{M} \\ & \mathrm{QP} \end{aligned}$ | 9.2 | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+19.4 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.3 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.9 \\ & +0.0 \end{aligned}$ | +0.0 | 31.2 | 46.0 | -14.8 | $\begin{array}{r} \hline \text { Vert } \\ 103 \end{array}$ |
| $\wedge 329.449 \mathrm{M}$ | 15.5 | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+19.4 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.3 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.9 \\ & +0.0 \end{aligned}$ | +0.0 | 37.5 | 46.0 | -8.5 | $\begin{gathered} \hline \text { Vert } \\ 129 \end{gathered}$ |
| 21 2747.475M | 39.4 | $\begin{array}{r} +0.0 \\ +1.2 \\ +29.3 \end{array}$ | $\begin{aligned} & +0.0 \\ & +3.0 \\ & +0.5 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.3 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -34.5 \end{array}$ | +0.0 | $39.2$ | $\begin{aligned} & 54.0 \\ & \mathrm{~d} \end{aligned}$ | -14.8 | $\begin{array}{r} \hline \text { Vert } \\ 145 \end{array}$ |
| $\begin{aligned} & 22 \text { 8119.800M } \\ & \text { Ave } \end{aligned}$ | 22.2 | $\begin{array}{r} +0.0 \\ +2.6 \\ +38.9 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +5.7 \\ & +0.9 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.6 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -35.4 \end{array}$ | +0.0 | $35.5$ | $54.0$ | -18.5 | $\begin{array}{r} \hline \text { Vert } \\ 150 \end{array}$ |
| $\wedge 8119.800 \mathrm{M}$ | 37.4 | $\begin{array}{r} +0.0 \\ +2.6 \\ +38.9 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +5.7 \\ & +0.9 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.6 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -35.4 \end{array}$ | $+0.0$ | $50.7$ | $\begin{aligned} & 54.0 \\ & \mathrm{w} \end{aligned}$ | -3.3 | $\begin{array}{r} \hline \text { Vert } \\ 160 \end{array}$ |
| $\begin{aligned} & 24 \begin{array}{l} 7320.770 \mathrm{M} \\ \text { Ave } \end{array} \end{aligned}$ | 23.5 | $\begin{array}{r} +0.0 \\ +1.9 \\ +37.2 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.0 \\ & +5.3 \\ & +1.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.6 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -35.1 \end{array}$ | $+0.0$ | $34.8$ | $54.0$ | -19.2 | $\begin{array}{r} \hline \text { Vert } \\ 139 \end{array}$ |
| $\wedge 7320.770 \mathrm{M}$ | 38.5 | $\begin{array}{r} +0.0 \\ +1.9 \\ +37.2 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +5.3 \\ & +1.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.6 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -35.1 \end{array}$ | $+0.0$ | $49.8$ | $54.0$ | -4.2 | $\begin{array}{r} \hline \text { Vert } \\ 145 \end{array}$ |
| $\begin{aligned} & 26 \text { 8233.145M } \\ & \text { Ave } \end{aligned}$ | 22.2 | $\begin{array}{r} +0.0 \\ +2.6 \\ +38.4 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +5.5 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.8 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -35.4 \end{array}$ | $+0.0$ | $34.8$ | $\overline{54.0}$ | -19.2 | $\begin{array}{r} \hline \text { Vert } \\ 139 \end{array}$ |
| $\wedge 8233.145 \mathrm{M}$ | 37.8 | $\begin{array}{r} +0.0 \\ +2.6 \\ +38.4 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +5.5 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.8 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -35.4 \end{array}$ | $+0.0$ | $50.4$ | $54.0$ | -3.6 | $\begin{array}{r} \hline \text { Vert } \\ 145 \end{array}$ |
| $\begin{aligned} & 287424.485 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 22.8 | $\begin{array}{r} +0.0 \\ +2.0 \\ +37.4 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +5.6 \\ & +1.2 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.7 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -35.1 \end{array}$ | $+0.0$ | $34.6$ | $54.0$ <br> h | -19.4 | $\begin{array}{r} \hline \text { Vert } \\ 169 \end{array}$ |
| $\wedge 7424.485 \mathrm{M}$ | 38.0 | $\begin{array}{r} +0.0 \\ +2.0 \\ +37.4 \end{array}$ | $\begin{aligned} & +0.0 \\ & +5.6 \\ & +1.2 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.7 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -35.1 \end{array}$ | $+0.0$ |  | $\begin{aligned} & 54.0 \\ & \text { gh } \end{aligned}$ | -4.2 | $\begin{array}{r} \hline \text { Vert } \\ 169 \end{array}$ |
| $\begin{aligned} & 309149.705 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 21.1 | $\begin{array}{r} +0.0 \\ +2.4 \\ +37.7 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +5.9 \\ & +0.8 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +1.1 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -34.7 \end{array}$ | $+0.0$ | $34.3$ | $54.0$ | -19.7 | Vert 139 |
| $\wedge 9149.705 \mathrm{M}$ | 36.7 | $\begin{array}{r} +0.0 \\ +2.4 \\ +37.7 \end{array}$ | $\begin{aligned} & +0.0 \\ & +5.9 \\ & +0.8 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +1.1 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -34.7 \end{array}$ | $+0.0$ | $49.9$ | $54.0$ | -4.1 | $\begin{array}{r} \hline \text { Vert } \\ 145 \end{array}$ |


| 328347.348 MAve |  | 21.7 | +0.0 | +0.0 | +0.0 | ${ }^{+0.0}$ | +0.0 | 34.1 | $54.0$ | -19.9 | $\begin{gathered} \text { Vert } \\ 169 \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{array}{r} +2.6 \\ +38.3 \end{array}$ | $\begin{array}{r} +5.5 \\ +0.4 \\ \hline \end{array}$ | +0.9 | -35.3 |  |  | High |  |  |
| $\wedge$ | ( 8347.350 M |  | 37.6 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 50.0 | 54.0 | -4.0 | Vert |
|  |  |  | +2.6 | +5.5 | +0.9 | -35.3 |  | High |  |  | 169 |
|  |  |  | +38.3 | +0.4 |  |  |  |  |  |  |  |
| $\wedge$ | ^ 8347.350 M | 33.5 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 45.9 | 54.0 | -8.1 | 169 |
|  |  |  | +2.6 | +5.5 | +0.9 | -35.3 |  | High |  |  |  |
|  |  |  | +38.3 | +0.4 |  |  |  |  |  |  |  |
| 35 | 9022.000M | 19.9 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 33.3 | 54.0 | -20.7 | $\begin{gathered} \hline \text { Vert } \\ 150 \end{gathered}$ |
|  | Ave |  | +2.4 | +6.0 | +0.7 | -34.8 |  | Low |  | $150$ |  |
|  |  |  | +37.9 | +1.2 |  |  |  |  |  |  |  |
|  | 9022.000M | 35.4 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 48.8 | 54.0 | -5.2 | $\begin{gathered} \hline \text { Vert } \\ 160 \end{gathered}$ |
|  |  |  | +2.4 | +6.0 | +0.7 | -34.8 |  | Low |  |  |  |
|  |  |  | +37.9 | +1.2 |  |  |  |  |  |  |  |
| 37 | 6403.385M | 38.5 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 48.1 | 107.5 | -59.4 | $\begin{gathered} \hline \text { Vert } \\ 145 \end{gathered}$ |
|  |  |  | +2.1 | +5.6 | +0.5 | -34.3 |  |  | Mid |  |  |
|  |  |  | +34.7 | +1.0 |  |  |  |  |  |  |  |
| 38 | 5488.550M | 38.8 | +0.0 | +0.0 | +0.0 | $+0.0$ | +0.0 | 47.9 | 107.5 | -59.6 | $\begin{gathered} \hline \text { Vert } \\ 145 \end{gathered}$ |
|  |  |  | +1.7 | +5.1 | +0.4 | -33.8 |  | Mid |  |  |  |
|  |  |  | +34.4 | +1.3 |  |  |  |  |  |  |  |
| 39 | 6493.585M | 37.5 | +0.0 | +0.0 | +0.0 | +0.0 | $+0.0$ | 47.7 | 107.5 | -59.8 | $\begin{array}{r} \hline \text { Vert } \\ 169 \end{array}$ |
|  |  |  | +2.1 | +5.8 | +0.6 | -34.3 |  |  | High |  |  |
|  |  |  | +34.8 | +1.2 |  |  |  |  |  |  |  |
| 40 | 6315.400M | 37.6 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 46.9 | 107.5 | -60.6 | $\begin{gathered} \hline \text { Vert } \\ 160 \end{gathered}$ |
|  |  |  | +2.1 | +5.4 | +0.4 | -34.2 |  |  | Low |  |  |
|  |  |  | +34.7 | +0.9 |  |  |  |  |  |  |  |
| 41 | 5564.535M | 37.3 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 46.7 | 107.5 | -60.8 | $\begin{array}{r} \hline \text { Vert } \\ 169 \end{array}$ |
|  |  |  | +1.8 | +5.2 | +0.5 | -33.8 |  |  | High |  |  |
|  |  |  | +34.4 | +1.3 |  |  |  |  |  |  |  |
| $\begin{aligned} & 42 \quad \text { 1804.450M } \\ & \text { Ave } \end{aligned}$ |  | 44.7 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 40.8 | 107.5 | -66.7 | $\begin{gathered} \text { Horiz } \\ 201 \end{gathered}$ |
|  |  | +0.7 | +2.2 | +0.6 | -35.1 |  |  | Low Config 2 |  |  |  |
|  |  | +27.3 | +0.4 |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 43 \text { 1804.400M } \\ & \text { Ave } \end{aligned}$ |  |  | 43.7 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 39.8 | 107.5 | -67.7 | $\begin{gathered} \hline \text { Horiz } \\ 169 \end{gathered}$ |
|  |  | +0.7 |  | +2.2 | +0.6 | -35.1 |  |  | Low Config 3 |  |  |  |
|  |  | +27.3 |  | +0.4 |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 449278.025 \mathrm{M} \\ & \text { Ave } \end{aligned}$ |  |  | 21.7 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 35.0 | 107.5 | -72.5 | $\begin{array}{r} \hline \text { Vert } \\ 169 \end{array}$ |
|  |  | +2.4 |  | +5.9 | +1.3 | -34.6 |  |  | High |  |  |  |
|  |  | +37.9 |  | +0.4 |  |  |  |  |  |  |  |  |
| ^ 9278.025M |  | 36.7 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 50.0 | 107.5 | -57.5 | $\begin{array}{r} \hline \text { Vert } \\ 169 \end{array}$ |  |
|  |  | +2.4 | +5.9 | +1.3 | -34.6 |  |  | High |  |  |  |  |
|  |  | +37.9 | +0.4 |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 46 \text { 1830.045M } \\ & \text { Ave } \end{aligned}$ |  |  | 37.4 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 33.9 | 107.5 | -73.6 | Horiz 187 |
|  |  | +0.7 |  | +2.3 | +0.6 | -35.1 |  |  | Mid Config 3 |  |  |  |
|  |  | +27.6 |  | +0.4 |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 47 \text { 7217.600M } \\ & \text { Ave } \end{aligned}$ |  |  | 23.1 | +0.0 | +0.0 | +0.0 | +0.0 | +0.0 | 33.5 | 107.5 | -74.0 | $\begin{array}{r} \hline \text { Vert } \\ 150 \end{array}$ |
|  |  | +1.8 |  | +5.2 | +0.2 | -35.0 |  |  | Low |  |  |  |
|  |  | +36.8 |  | +1.4 |  |  |  |  |  |  |  |  |
| ^ 7217.600M |  | 38.4 | +0.0 | +0.0 | +0.0 | $+0.0$ | +0.0 | 48.8 | 107.5 | -58.7 | Vert <br> 160 |  |
|  |  | +1.8 | +5.2 | +0.2 | -35.0 |  |  | Low |  |  |  |  |
|  |  | +36.8 | +1.4 |  |  |  |  |  |  |  |  |  |



## Band Edge

## Band Edge Summary

Operating Mode: Single Channel (Low and High)

| Frequency <br> $(\mathbf{M H z})$ | Modulation | Configuration <br> /Antenna Type | Field Strength <br> $(\mathbf{d B u V} / \mathbf{m} @ 3 m)$ | Limit <br> (dBuV/m @3m) | Results |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 614 | 10 k | 1 | 40.7 | 46.0 | Pass |
| 902 | 10 k | 1 | 77.5 | 106.5 | Pass |
| 928 | 10 k | 1 | 76.5 | 106.5 | Pass |
| 960 | 10 k | 1 | 45.4 | 54.0 | Pass |
| 614 | 25 k | 1 | 40.8 | 46.0 | Pass |
| 902 | 25 k | 1 | 77.7 | 106.5 | Pass |
| 928 | 25 k | 1 | 74.8 | 106.5 | Pass |
| 960 | 25 k | 1 | 45.4 | 54.0 | Pass |

Band Edge Summary
Operating Mode: Single Channel (Low and High)

| Frequency <br> $(\mathbf{M H z})$ | Modulation | Configuration <br> /Antenna Type | Field Strength <br> $(\mathbf{d B u V} / \mathbf{m} @ 3 \mathrm{~m})$ | Limit <br> $(\mathbf{d B u V} / \mathbf{m} @ 3 m)$ | Results |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 614 | 10 k | 2 | 40.8 | 46.0 | Pass |
| 902 | 10 k | 2 | 80.2 | 109.5 | Pass |
| 928 | 10 k | 2 | 78.8 | 109.5 | Pass |
| 960 | 10 k | 2 | 45.4 | 54.0 | Pass |
| 614 | 25 k | 2 | 40.8 | 46.0 | Pass |
| 902 | 25 k | 2 | 82.4 | 109.5 | Pass |
| 928 | 25 k | 2 | 78.4 | 109.5 | Pass |
| 960 | 25 k | 2 | 45.4 | 54.0 | Pass |

## Band Edge Summary

Operating Mode: Single Channel (Low and High)

| Frequency <br> $(\mathbf{M H z})$ | Modulation | Configuration <br> /Antenna Type | Field Strength <br> $(\mathbf{d B u V} / \mathbf{m} @ 3 m)$ | Limit <br> (dBuV/m @3m) | Results |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 614 | 10 k | 3 | 40.8 | 46.0 | Pass |
| 902 | 10 k | 3 | 80.0 | 107.5 | Pass |
| 928 | 10 k | 3 | 75.4 | 107.5 | Pass |
| 960 | 10 k | 3 | 45.4 | 54.0 | Pass |
| 614 | 25 k | 3 | 40.6 | 46.0 | Pass |
| 902 | 25 k | 3 | 80.6 | 107.5 | Pass |
| 928 | 25 k | 3 | 75.9 | 107.5 | Pass |
| 960 | 25 k | 3 | 45.4 | 54.0 | Pass |

## Band Edge Summary

Operating Mode: Hopping

| Frequency <br> $\mathbf{( M H z )}$ | Modulation | Configuration <br> /Antenna Type | Field Strength <br> $(\mathbf{d B u V} / \mathbf{m @ 3 m})$ | Limit <br> $(\mathbf{d B u V} / \mathbf{m}$ @3m) | Results |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 614 | 10 k | 5 | 40.7 | 46.0 | Pass |
| 902 | 10 k | 5 | 77.8 | 106.5 | Pass |
| 928 | 10 k | 5 | 74.5 | 106.5 | Pass |
| 960 | 10 k | 5 | 45.3 | 54.0 | Pass |
| 614 | 25 k | 5 | 40.6 | 46.0 | Pass |
| 902 | 25 k | 5 | 76.9 | 106.5 | Pass |
| 928 | 25 k | 5 | 72.3 | 106.5 | Pass |
| 960 | 25 k | 5 | 45.3 | 54.0 | Pass |


| Band Edge Summary |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Operating Mode: Hopping |  |  |  |  |  |
| Frequency <br> $(\mathrm{MHz})$ | Modulation | Configuration <br> /Antenna Type | Field Strength <br> (dBuV/m @3m) | Limit <br> (dBuV/m @3m) | Results |
| 614 | 10 k | 6 | 40.6 | 46.0 | Pass |
| 902 | 10 k | 6 | 81.8 | 109.5 | Pass |
| 928 | 10 k | 6 | 76.0 | 109.5 | Pass |
| 960 | 10 k | 6 | 45.3 | 54.0 | Pass |
| 614 | 25 k | 6 | 40.6 | 46.0 | Pass |
| 902 | 25 k | 6 | 80.5 | 109.5 | Pass |
| 928 | 25 k | 6 | 76.3 | 109.5 | Pass |
| 960 | 25 k | 6 | 45.2 | 54.0 | Pass |

## Band Edge Summary

Operating Mode: Hopping

| Frequency <br> $(\mathbf{M H z})$ | Modulation | Configuration <br> /Antenna Type | Field Strength <br> $(\mathbf{d B u V} / \mathbf{m} @ 3 m)$ | Limit <br> (dBuV/m @3m) | Results |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 614 | 10 k | 7 | 40.6 | 46.0 | Pass |
| 902 | 10 k | 7 | 77.9 | 107.5 | Pass |
| 928 | 10 k | 7 | 76.5 | 107.5 | Pass |
| 960 | 10 k | 7 | 45.3 | 54.0 | Pass |
| 614 | 25 k | 7 | 40.7 | 46.0 | Pass |
| 902 | 25 k | 7 | 78.0 | 107.5 | Pass |
| 928 | 25 k | 7 | 74.8 | 107.5 | Pass |
| 960 | 25 k | 7 | 45.3 | 54.0 | Pass |

## Band Edge Plots

## Configuration 1




Page 34 of 91 1 Tosting the Futuro LABORATORIES, INC.


| BE 960 Config $1,10 \mathrm{k}, \mathrm{SC}$ (limit corrected for system factors) |
| :--- |
| Ref Level $96.99 \mathrm{~dB} \mathrm{~V} \quad$ ATTEN 0 dB |
| RES BW: 120.0 kHz VID BW: 1.0 MHz SWP: 10.476 sec |
| Marker: $960.0 \mathrm{MHz} 9.3567 \mathrm{~dB} \mathrm{\mu} \mathrm{~V}$ |


—— 15.247(d) / 15.209 Radiated Spurious Emissions $\mathcal{W}_{\text {Tosting the Futuro }}$ LABORATORIES, INC.

 $\mathcal{W}_{\text {Tosting the Futuro }}$ LABORATORIES, INC.



LABORATORIES, INC.

## Configuration 2



$\mathcal{M}_{\text {Testing me muture }}$
LABORATORIES, INC.

 $\mathcal{W}_{\text {Tosting the Futuro }}$ LABORATORIES, INC.



Page 40 of 91
$\mathcal{M}_{\text {Testing me muture }}$
LABORATORIES, INC.



LABORATORIES, INC.

## Configuration 3


 1 Tosting the Futuro LABORATORIES, INC.

 $\mathcal{W}_{\text {Tosting the Futuro }}$ LABORATORIES, INC.

 1 Tosting the Futuro LABORATORIES, INC.



LABORATORIES, INC.

## Configuration 5



$\mathcal{M}_{\text {Testing me muture }}$
LABORATORIES, INC.

 $\mathcal{W}_{\text {Tosting the Futuro }}$ LABORATORIES, INC.



Page 48 of 91
$\wedge_{\text {Tesating me future }}$
LABORATORIES, INC.



LABORATORIES, INC.

## Configuration 6



$\mathcal{M}_{\text {Testing me muture }}$
LABORATORIES, INC.


$\mathcal{M}_{\text {Testing me muture }}$
LABORATORIES, INC.


$\mathcal{M}_{\text {Testing me muture }}$
LABORATORIES, INC.



LABORATORIES, INC.

## Configuration 7



$\mathcal{M}_{\text {Testing me muture }}$
LABORATORIES, INC.

 $\mathcal{W}_{\text {Tosting the Futuro }}$ LABORATORIES, INC.


$\mathcal{M}_{\text {Testing me muture }}$
LABORATORIES, INC.



LABORATORIES, INC.

## Test Setup / Conditions / Data

Test Location: CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A • Bothell, WA 98021•(425) 402-1717
Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

## Itron, Inc.

15.247(d) / 15.209 Radiated Spurious Emissions

108561 Date: 9/8/2023
Maximized Emissions Time: 18:07:52
Michael Atkinson
EMIT est 5.03.20
Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Test Conditions / Notes:

Test Environment Conditions:
Temperature: $23^{\circ} \mathrm{C}$
Humidity: $48 \%$
Pressure: 101.7 kPa
Test Method: ANSI C63.10 (2013)
Frequency Range: Band Edge
Test Setup:
Transmitting continuously with modulation, 10k and 25 k modulations investigated.
Top two LTE antenna ports have Cisco p/n ANT-5G-MP-OUT-N antennas attached.
Itron IRM-Star (CAM3) radio module has Cisco p/n ANT-5G-MP-OUT-N antenna attached.
EUT Connected to support laptop via shielded Ethernet cable.
Horizontal and Vertical antenna polarities investigated, worst case reported.
$2 \times 31$ material ferrites with 3 wraps each on Ethernet cable underneath the ground plane. The ferrites are out of the test volume and these are NOT considered a modification.

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN03824 | Biconilog Antenna | 3142E | $5 / 9 / 2023$ | $5 / 9 / 2025$ |
| T2 | ANP05333 | Cable | Heliax | $8 / 8 / 2023$ | $8 / 8 / 2025$ |
| T3 | ANP05360 | Cable | RG214 | $8 / 8 / 2023$ | $8 / 8 / 2025$ |
| T4 | ANP05546 | Cable | Heliax | $8 / 1 / 2023$ | $8 / 1 / 2025$ |
|  | AN02673 | Spectrum Analyzer | E4446A | $3 / 2 / 2023$ | $3 / 2 / 2025$ |


| Measurement Data: | Reading listed by margin. |  |  |  |  | Test Distance: 3 Meters |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# $\quad$Freq <br> MHz | $\begin{aligned} & \text { Rdng } \\ & \mathrm{dB} \mu \mathrm{~V} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 3 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 4 \\ & \mathrm{~dB} \\ & \hline \end{aligned}$ | Dist Table | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \end{gathered}$ | Margin <br> dB | Polar <br> Ant |
| $\begin{aligned} & 1814.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 9.4 | +27.4 | +1.2 | +2.3 | $+0.5$ | +0.0 | 40.8 | $\begin{aligned} & 46.0 \\ & 25 \mathrm{k} \end{aligned}$ | -5.2 | Vert |
| $\begin{aligned} & 2614.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 9.3 | +27.4 | +1.2 | +2.3 | +0.5 | +0.0 | 40.7 | $\begin{aligned} & 46.0 \\ & 10 \mathrm{k} \end{aligned}$ | -5.3 | Vert |
| $\begin{aligned} & 3 \begin{array}{l} 960.000 \mathrm{M} \\ \mathrm{QP} \end{array} \\ & \hline \end{aligned}$ | 9.4 | +31.1 | +1.6 | +2.6 | +0.7 | +0.0 | 45.4 | $$ | -8.6 | Vert |
| $\begin{aligned} & 4690.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 9.4 | +31.1 | +1.6 | +2.6 | +0.7 | +0.0 | 45.4 | $\begin{aligned} & 54.0 \\ & 10 \mathrm{k} \end{aligned}$ | -8.6 | Vert |
| $5 \quad 902.000 \mathrm{M}$ | 43.6 | +29.5 | +1.5 | +2.5 | +0.6 | +0.0 | 77.7 | $\begin{aligned} & 106.5 \\ & 25 \mathrm{k} \end{aligned}$ | -28.8 | Vert |
| $6 \quad 902.000 \mathrm{M}$ | 43.4 | +29.5 | +1.5 | +2.5 | +0.6 | +0.0 | 77.5 | $\begin{aligned} & 106.5 \\ & 10 \mathrm{k} \end{aligned}$ | -29.0 | Vert |
| $7 \quad 928.000 \mathrm{M}$ | 40.5 | +31.2 | +1.5 | +2.6 | +0.7 | +0.0 | 76.5 | $\begin{aligned} & 106.5 \\ & 10 \mathrm{k} \end{aligned}$ | -30.0 | Vert |
| $8 \quad 928.000 \mathrm{M}$ | 38.8 | +31.2 | +1.5 | +2.6 | +0.7 | +0.0 | 74.8 | $\begin{aligned} & 106.5 \\ & 25 \mathrm{k} \end{aligned}$ | -31.7 | Vert |

Test Location: CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A•Bothell, WA 98021•(425) 402-1717
Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Itron, Inc.
15.247(d) / 15.209 Radiated Spurious Emissions

108561
Maximized Emissions
Michael Atkinson
EMITest 5.03.20

Date: 9/8/2023
Time: 18:58:25
Sequence\#: 18

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Test Conditions / Notes:
Test Environment Conditions:
Temperature: $23^{\circ} \mathrm{C}$
Humidity: $48 \%$
Pressure: 101.7 kPa
Test Method: ANSI C63.10 (2013)
Frequency Range: Band Edge
Test Setup:
Transmitting continuously with modulation, 10 k and 25 k modulations investigated.
Top two LTE antenna ports are have Cisco p/n ANT-5G-MP-OUT-N antennas attached.
Itron IRM-Star (CAM3) radio module has PCTEL p/n BOA9025NM-ITR antenna attached
EUT Connected to support laptop via shielded Ethernet cable.
Horizontal and Vertical antenna polarities investigated, worst case reported.
$2 \times 31$ material ferrites with 3 wraps each on Ethernet cable underneath the ground plane. The ferrites are out of the test volume and these are NOT considered a modification.

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN03824 | Biconilog Antenna | 3142E | $5 / 9 / 2023$ | $5 / 9 / 2025$ |
| T2 | ANP05333 | Cable | Heliax | $8 / 8 / 2023$ | $8 / 8 / 2025$ |
| T3 | ANP05360 | Cable | RG214 | $8 / 8 / 2023$ | $8 / 8 / 2025$ |
| T4 | ANP05546 | Cable | Heliax | $8 / 1 / 2023$ | $8 / 1 / 2025$ |
|  | AN02673 | Spectrum Analyzer | E4446A | $3 / 2 / 2023$ | $3 / 2 / 2025$ |


| Measurement Data: | Reading listed by margin. |  |  |  |  | Test Distance: 3 Meters |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# $\quad$Freq <br> MHz | $\begin{aligned} & \text { Rdng } \\ & \mathrm{dB} \mu \mathrm{~V} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 3 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 4 \\ & \mathrm{~dB} \\ & \hline \end{aligned}$ | Dist Table | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \end{gathered}$ | Margin <br> dB | Polar <br> Ant |
| $\begin{aligned} & 1814.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 9.4 | +27.4 | +1.2 | +2.3 | $+0.5$ | +0.0 | 40.8 | $\begin{aligned} & 46.0 \\ & 25 \mathrm{k} \end{aligned}$ | -5.2 | Vert |
| $\begin{aligned} & 2614.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 9.4 | +27.4 | +1.2 | +2.3 | +0.5 | +0.0 | 40.8 | $\begin{aligned} & 46.0 \\ & 10 \mathrm{k} \end{aligned}$ | -5.2 | Vert |
| $\begin{aligned} & 3 \begin{array}{l} 960.000 \mathrm{M} \\ \mathrm{QP} \end{array} \\ & \hline \end{aligned}$ | 9.4 | +31.1 | +1.6 | +2.6 | +0.7 | +0.0 | 45.4 | $$ | -8.6 | Vert |
| $\begin{aligned} & 4690.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 9.4 | +31.1 | +1.6 | +2.6 | +0.7 | +0.0 | 45.4 | $\begin{aligned} & 54.0 \\ & 10 \mathrm{k} \end{aligned}$ | -8.6 | Vert |
| $5 \quad 902.000 \mathrm{M}$ | 48.3 | +29.5 | +1.5 | +2.5 | +0.6 | +0.0 | 82.4 | $\begin{aligned} & 109.5 \\ & 25 \mathrm{k} \end{aligned}$ | -27.1 | Vert |
| $6 \quad 902.000 \mathrm{M}$ | 46.1 | +29.5 | +1.5 | +2.5 | +0.6 | +0.0 | 80.2 | $\begin{aligned} & 109.5 \\ & 10 \mathrm{k} \end{aligned}$ | -29.3 | Vert |
| $7 \quad 928.000 \mathrm{M}$ | 42.8 | +31.2 | +1.5 | +2.6 | +0.7 | +0.0 | 78.8 | $\begin{aligned} & 109.5 \\ & 10 \mathrm{k} \end{aligned}$ | -30.7 | Vert |
| $8 \quad 928.000 \mathrm{M}$ | 42.4 | +31.2 | +1.5 | +2.6 | +0.7 | +0.0 | 78.4 | $\begin{aligned} & 109.5 \\ & 25 \mathrm{k} \end{aligned}$ | -31.1 | Vert |

Test Location: CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A•Bothell, WA 98021•(425) 402-1717
Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Itron, Inc.
15.247(d) / 15.209 Radiated Spurious Emissions

108561
Maximized Emissions
Michael Atkinson
EMIT est 5.03.20

Date: 9/8/2023
Time: 19:38:58
Sequence\#: 19

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 3 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 3 |  | S/N |

Test Conditions / Notes:
Test Environment Conditions:
Temperature: $23^{\circ} \mathrm{C}$
Humidity: $48 \%$
Pressure: 101.7 kPa
Test Method: ANSI C63.10 (2013)
Frequency Range: Band Edge
Test Setup:
Transmitting continuously with modulation, 10 k and 25 k modulations investigated.
Top two LTE antenna ports have Cisco p/n ANT-5G-MP-OUT-N antennas attached.
Itron IRM-Star (CAM3) radio module has PCTEL p/n BOA9028 antenna attached.
EUT Connected to support laptop via shielded Ethernet cable.
Horizontal and Vertical antenna polarities investigated, worst case reported.
$2 \times 31$ material ferrites with 3 wraps each on Ethernet cable underneath the ground plane. The ferrites are out of the test volume and these are NOT considered a modification.

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN03824 | Biconilog Antenna | 3142E | $5 / 9 / 2023$ | $5 / 9 / 2025$ |
| T2 | ANP05333 | Cable | Heliax | $8 / 8 / 2023$ | $8 / 8 / 2025$ |
| T3 | ANP05360 | Cable | RG214 | $8 / 8 / 2023$ | $8 / 8 / 2025$ |
| T4 | ANP05546 | Cable | Heliax | $8 / 1 / 2023$ | $8 / 1 / 2025$ |
|  | AN02673 | Spectrum Analyzer | E4446A | $3 / 2 / 2023$ | $3 / 2 / 2025$ |


| Measurement Data: | Reading listed by margin. |  |  |  |  | Test Distance: 3 Meters |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \#Freq <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \text { T3 } \\ & \text { dB } \end{aligned}$ | $\begin{aligned} & \mathrm{T} 4 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{gathered} \text { Dist } \\ \text { Table } \end{gathered}$ | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \end{gathered}$ | Margin dB | Polar <br> Ant |
| $\begin{aligned} & 1814.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 9.4 | +27.4 | +1.2 | +2.3 | $+0.5$ | +0.0 | 40.8 | $\begin{aligned} & 46.0 \\ & 10 \mathrm{k} \end{aligned}$ | -5.2 | Vert |
| $\begin{aligned} & 2614.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 9.2 | +27.4 | +1.2 | +2.3 | +0.5 | +0.0 | 40.6 | $\begin{aligned} & 46.0 \\ & 25 \mathrm{k} \end{aligned}$ | -5.4 | Vert |
| $\begin{aligned} & 3960.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 9.4 | +31.1 | +1.6 | +2.6 | +0.7 | +0.0 | 45.4 | $\begin{aligned} & 54.0 \\ & 25 \mathrm{k} \end{aligned}$ | -8.6 | Vert |
| $\begin{aligned} & 4960.000 \mathrm{M} \\ & \mathrm{QP} \end{aligned}$ | 9.4 | +31.1 | +1.6 | +2.6 | +0.7 | +0.0 | 45.4 | $\begin{aligned} & 54.0 \\ & 10 \mathrm{k} \\ & \hline \end{aligned}$ | -8.6 | Vert |
| $5 \quad 902.000 \mathrm{M}$ | 46.5 | +29.5 | +1.5 | +2.5 | +0.6 | +0.0 | 80.6 | $\begin{aligned} & 107.5 \\ & 25 \mathrm{k} \\ & \hline \end{aligned}$ | -26.9 | Vert |
| $6 \quad 902.000 \mathrm{M}$ | 45.9 | +29.5 | +1.5 | +2.5 | +0.6 | +0.0 | 80.0 | $\begin{aligned} & 107.5 \\ & 10 \mathrm{k} \end{aligned}$ | -27.5 | Vert |
| $7 \quad 928.000 \mathrm{M}$ | 39.9 | +31.2 | +1.5 | +2.6 | +0.7 | +0.0 | 75.9 | $\begin{aligned} & 107.5 \\ & 25 \mathrm{k} \end{aligned}$ | -31.6 | Vert |
| $8 \quad 928.000 \mathrm{M}$ | 39.4 | +31.2 | +1.5 | +2.6 | +0.7 | +0.0 | 75.4 | $\begin{aligned} & 107.5 \\ & 10 \mathrm{k} \\ & \hline \end{aligned}$ | -32.1 | Vert |

Test Location: CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A•Bothell, WA 98021•(425) 402-1717
Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Itron, Inc.
15.247(d) / 15.209 Radiated Spurious Emissions

108561
Maximized Emissions
Michael Atkinson
EMIT est 5.03.20

Date: 9/19/2023
Time: 09:03:18
Sequence\#: 37

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 5 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 5 |  | S/N |

Test Conditions / Notes:
Test Environment Conditions:
Temperature: $23^{\circ} \mathrm{C}$
Humidity: $48 \%$
Pressure: 101.7 kPa
Test Method: ANSI C63.10 (2013)
Frequency Range: Band Edge
Test Setup:
Transmitting with modulation, hopping mode, 10k and 25 k modulations investigated.
Top two LTE antenna ports have Cisco p/n ANT-5G-MP-OUT-N antennas attached.
Itron IRM-Star (CAM3) radio module has Cisco p/n ANT-5G-MP-OUT-N antenna attached.
EUT Connected to support laptop via shielded Ethernet cable.
Horizontal and Vertical antenna polarities investigated, worst case reported.
$2 \times 31$ material ferrites with 3 wraps each on Ethernet cable underneath the ground plane. The ferrites are out of the test volume and these are NOT considered a modification.

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN03824 | Biconilog Antenna | 3142E | $5 / 9 / 2023$ | $5 / 9 / 2025$ |
| T2 | ANP05333 | Cable | Heliax | $8 / 8 / 2023$ | $8 / 8 / 2025$ |
| T3 | ANP05360 | Cable | RG214 | $8 / 8 / 2023$ | $8 / 8 / 2025$ |
| T4 | ANP05546 | Cable | Heliax | $8 / 1 / 2023$ | $8 / 1 / 2025$ |
|  | AN02673 | Spectrum Analyzer | E4446A | $3 / 2 / 2023$ | $3 / 2 / 2025$ |


| Measurement Data: | Reading listed by margin. |  |  |  |  | Test Distance: 3 Meters |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \#Freq <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 3 \\ & \mathrm{~dB} \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{T} 4 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{gathered} \hline \text { Dist } \\ \text { Table } \end{gathered}$ | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \end{gathered}$ | $\begin{gathered} \text { Margin } \\ \mathrm{dB} \end{gathered}$ | Polar <br> Ant |
| $\begin{aligned} & 1814.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 9.3 | +27.4 | +1.2 | +2.3 | $+0.5$ | +0.0 | 40.7 | ${ }_{10 \mathrm{k}}{ }^{46.0}$ | -5.3 | Vert |
| $\begin{aligned} & 2614.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 9.2 | +27.4 | +1.2 | +2.3 | +0.5 | +0.0 | 40.6 | $\begin{aligned} & 46.0 \\ & 25 \mathrm{k} \end{aligned}$ | -5.4 | Vert |
| $\begin{aligned} & 3960.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 9.3 | +31.1 | +1.6 | +2.6 | +0.7 | +0.0 | $45.3$ | $\begin{aligned} & 54.0 \\ & 25 \mathrm{k} \\ & \hline \end{aligned}$ | -8.7 | Vert |
| $\begin{aligned} & 4 \begin{array}{l} 960.000 \mathrm{M} \\ \mathrm{QP} \end{array} \\ & \hline \end{aligned}$ | 9.3 | +31.1 | +1.6 | +2.6 | +0.7 | +0.0 | 45.3 | $\begin{aligned} & 54.0 \\ & 10 \mathrm{k} \\ & \hline \end{aligned}$ | -8.7 | Vert |
| $5 \quad 902.000 \mathrm{M}$ | 43.7 | +29.5 | +1.5 | +2.5 | +0.6 | +0.0 | 77.8 | $\begin{aligned} & 106.5 \\ & 10 \mathrm{k} \\ & \hline \end{aligned}$ | -28.7 | Vert |
| $6 \quad 902.000 \mathrm{M}$ | 42.8 | +29.5 | +1.5 | +2.5 | +0.6 | +0.0 | 76.9 | $\begin{aligned} & 106.5 \\ & 25 \mathrm{k} \end{aligned}$ | -29.6 | Vert |
| $7 \quad 928.000 \mathrm{M}$ | 38.5 | +31.2 | +1.5 | +2.6 | +0.7 | +0.0 | 74.5 | $\begin{aligned} & 106.5 \\ & 10 \mathrm{k} \end{aligned}$ | -32.0 | Vert |
| $8 \quad 928.000 \mathrm{M}$ | 36.3 | +31.2 | +1.5 | +2.6 | +0.7 | +0.0 | 72.3 | $\begin{aligned} & 106.5 \\ & 25 \mathrm{k} \\ & \hline \end{aligned}$ | -34.2 | Vert |

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Test Location: CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A•Bothell, WA 98021•(425) 402-1717
Itron, Inc.
15.247(d) / 15.209 Radiated Spurious Emissions

108561
Maximized Emissions
Michael Atkinson
EMITest 5.03.20

Date: 9/19/2023
Time: 09:44:40
Sequence\#: 38

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 6 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 6 |  | S/N |

Test Conditions / Notes:
Test Environment Conditions:
Temperature: $23^{\circ} \mathrm{C}$
Humidity: 48\%
Pressure: 101.7 kPa
Test Method: ANSI C63.10 (2013)
Frequency Range: Band Edge
Test Setup:
Transmitting with modulation, hopping mode, 10 k and 25 k modulations investigated.
Top two LTE antenna ports have Cisco p/n ANT-5G-MP-OUT-N antennas attached.
Itron IRM-Star (CAM3) radio module has PCTEL p/n BOA9025NM-ITR antenna attached.
EUT Connected to support laptop via shielded Ethernet cable.
Horizontal and Vertical antenna polarities investigated, worst case reported.
$2 \times 31$ material ferrites with 3 wraps each on Ethernet cable underneath the ground plane. The ferrites are out of the test volume and these are NOT considered a modification.

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN03824 | Biconilog Antenna | 3142E | $5 / 9 / 2023$ | $5 / 9 / 2025$ |
| T2 | ANP05333 | Cable | Heliax | $8 / 8 / 2023$ | $8 / 8 / 2025$ |
| T3 | ANP05360 | Cable | RG214 | $8 / 8 / 2023$ | $8 / 8 / 2025$ |
| T4 | ANP05546 | Cable | Heliax | $8 / 1 / 2023$ | $8 / 1 / 2025$ |
|  | AN02673 | Spectrum Analyzer | E4446A | $3 / 2 / 2023$ | $3 / 2 / 2025$ |


| Measurement Data: | Reading listed by margin. |  |  |  |  | Test Distance: 3 Meters |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \#Freq <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{~V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \text { T3 } \\ & \text { dB } \end{aligned}$ | $\begin{aligned} & \mathrm{T} 4 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{gathered} \text { Dist } \\ \text { Table } \end{gathered}$ | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \end{gathered}$ | Margin dB | Polar <br> Ant |
| $\begin{aligned} & 1814.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 9.2 | +27.4 | +1.2 | +2.3 | $+0.5$ | +0.0 | 40.6 | $25 \mathrm{k}$ | -5.4 | Vert |
| $\begin{aligned} & 2614.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 9.2 | +27.4 | +1.2 | +2.3 | +0.5 | +0.0 | 40.6 | $\begin{aligned} & 46.0 \\ & 10 \mathrm{k} \end{aligned}$ | -5.4 | Vert |
| $\begin{aligned} & 3960.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 9.3 | +31.1 | +1.6 | +2.6 | +0.7 | +0.0 | 45.3 | $\begin{aligned} & 54.0 \\ & 10 \mathrm{k} \end{aligned}$ | -8.7 | Vert |
| $\begin{aligned} & 4960.000 \mathrm{M} \\ & \mathrm{QP} \end{aligned}$ | 9.2 | +31.1 | +1.6 | +2.6 | +0.7 | +0.0 | 45.2 | $\begin{aligned} & 54.0 \\ & 25 \mathrm{k} \end{aligned}$ | -8.8 | Vert |
| $5 \quad 902.000 \mathrm{M}$ | 47.7 | +29.5 | +1.5 | +2.5 | +0.6 | +0.0 | 81.8 | $\begin{aligned} & 109.5 \\ & 10 \mathrm{k} \end{aligned}$ | -27.7 | Vert |
| $6 \quad 902.000 \mathrm{M}$ | 46.4 | +29.5 | +1.5 | +2.5 | +0.6 | +0.0 | 80.5 | $\begin{aligned} & 109.5 \\ & 25 \mathrm{k} \end{aligned}$ | -29.0 | Vert |
| $7 \quad 928.000 \mathrm{M}$ | 40.3 | +31.2 | +1.5 | +2.6 | +0.7 | +0.0 | 76.3 | $\begin{aligned} & 109.5 \\ & 25 \mathrm{k} \end{aligned}$ | -33.2 | Vert |
| $8 \quad 928.000 \mathrm{M}$ | 40.0 | +31.2 | +1.5 | +2.6 | +0.7 | +0.0 | 76.0 | $\begin{aligned} & 109.5 \\ & 10 \mathrm{k} \\ & \hline \end{aligned}$ | -33.5 | Vert |

Test Location: CKC Laboratories • 2211623 rd Drive SE, Suite A • Bothell, WA. 98021 • 1-800-500-4EMC (4362)
Customer:
Specification:
Work Order \#:
Test Type:
Tested By: Itron, Inc.
15.247(d) / 15.209 Radiated Spurious Emissions

108561
Maximized Emissions
Date: 9/19/2023

Michael Atkinson
Time: 10:37:31

Software:
EMIT est 5.03.20
Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 7 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 7 |  | S/N |

Test Conditions / Notes:
Test Environment Conditions:
Temperature: $23^{\circ} \mathrm{C}$
Humidity: 48\%
Pressure: 101.7 kPa
Test Method: ANSI C63.10 (2013)
Frequency Range: Band Edge
Test Setup:
Transmitting with modulation, hopping mode, 10 k and 25 k modulations investigated
Top two LTE antenna ports have Cisco p/n ANT-5G-MP-OUT-N antennas attached. Itron IRM-Star (CAM3) radio module has PCTEL p/n BOA9028 antenna attached.
EUT Connected to support laptop via shielded Ethernet cable.
Horizontal and Vertical antenna polarities investigated, worst case reported.
$2 \times 31$ material ferrites with 3 wraps each on Ethernet cable underneath the ground plane. The ferrites are out of the test volume and these are NOT considered a modification.

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN03824 | Biconilog Antenna | 3142E | $5 / 9 / 2023$ | $5 / 9 / 2025$ |
| T2 | ANP05333 | Cable | Heliax | $8 / 8 / 2023$ | $8 / 8 / 2025$ |
| T3 | ANP05360 | Cable | RG214 | $8 / 8 / 2023$ | $8 / 8 / 2025$ |
| T4 | ANP05546 | Cable | Heliax | $8 / 1 / 2023$ | $8 / 1 / 2025$ |
|  | AN02673 | Spectrum Analyzer | E4446A | $3 / 2 / 2023$ | $3 / 2 / 2025$ |


| Measurement Data: | Reading listed by margin. |  |  |  |  | Test Distance: 3 Meters |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# $\quad$Freq <br> MHz | $\begin{aligned} & \text { Rdng } \\ & \mathrm{dB} \mu \mathrm{~V} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 3 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 4 \\ & \mathrm{~dB} \\ & \hline \end{aligned}$ | Dist Table | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \end{gathered}$ | Margin <br> dB | Polar <br> Ant |
| $\begin{aligned} & 1814.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 9.3 | +27.4 | +1.2 | +2.3 | $+0.5$ | +0.0 | 40.7 | $\begin{aligned} & 46.0 \\ & 25 \mathrm{k} \end{aligned}$ | -5.3 | Vert |
| $\begin{aligned} & 2614.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 9.2 | +27.4 | +1.2 | +2.3 | +0.5 | +0.0 | 40.6 | $\begin{aligned} & 46.0 \\ & 10 \mathrm{k} \end{aligned}$ | -5.4 | Vert |
| $\begin{aligned} & 3 \begin{array}{l} 960.000 \mathrm{M} \\ \mathrm{QP} \end{array} \\ & \hline \end{aligned}$ | 9.3 | +31.1 | +1.6 | +2.6 | +0.7 | +0.0 | 45.3 | $$ | -8.7 | Vert |
| $\begin{aligned} & 4690.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 9.3 | +31.1 | +1.6 | +2.6 | +0.7 | +0.0 | 45.3 | $\begin{aligned} & 54.0 \\ & 10 \mathrm{k} \end{aligned}$ | -8.7 | Vert |
| $5 \quad 902.000 \mathrm{M}$ | 43.9 | +29.5 | +1.5 | +2.5 | +0.6 | +0.0 | 78.0 | $\begin{aligned} & 107.5 \\ & 25 \mathrm{k} \end{aligned}$ | -29.5 | Vert |
| $6 \quad 902.000 \mathrm{M}$ | 43.8 | +29.5 | +1.5 | +2.5 | +0.6 | +0.0 | 77.9 | $\begin{aligned} & 107.5 \\ & 10 \mathrm{k} \\ & \hline \end{aligned}$ | -29.6 | Vert |
| $7 \quad 928.000 \mathrm{M}$ | 40.5 | +31.2 | +1.5 | +2.6 | +0.7 | +0.0 | 76.5 | $\begin{aligned} & 107.5 \\ & 10 \mathrm{k} \end{aligned}$ | -31.0 | Vert |
| $8 \quad 928.000 \mathrm{M}$ | 38.8 | +31.2 | +1.5 | +2.6 | +0.7 | +0.0 | 74.8 | $\begin{aligned} & 107.5 \\ & 25 \mathrm{k} \end{aligned}$ | -32.7 | Vert |

## Test Setup Photo(s)

## Configuration 1



Below 1GHz, 80cm; View 1


Below 1GHz, 80cm; View 2


Above $1 \mathrm{GHz}, 150 \mathrm{~cm}$

## Configuration 2



Below 1GHz, View 1


Below 1GHz, View 2


Above 1 GHz , 1.5 m

## Configuration 3



Below 1GHz, 80cm; View 1


Below 1GHz, 80cm; View 2


Above $1 \mathrm{GHz}, 150 \mathrm{~cm}$

Hopping Only


Configuration 5


Configuration 6


Configuration 7

LABORATORIES, INC.

### 15.207 AC Conducted Emissions

## Test Setup / Conditions / Data

Test Location: CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A•Bothell, WA 98021• (425) 402-1717

Customer:
Specification: Work Order \#: Test Type Tested By:
Software:

Itron, Inc.
15.207 AC Mains - Quasi-peak

108561 Date: 10/13/2023
Conducted Emissions Time: 15:47:58
Michael Atkinson
EMITest 5.03.20

Sequence\#: 50
115 V 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 8 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 8 |  | S/N |

## Test Conditions / Notes:

Test Environment Conditions:
Temperature: $22^{\circ} \mathrm{C}$
Humidity: $47 \%$
Pressure: 100.5 kPa

Test Method: ANSI C63.10 (2013)
Frequency Range: 150k-30MHz
Test Setup:
Unit has ISM radio transmitting at $915 \mathrm{MHz}, 10 \mathrm{k}$, and 25 k data rates investigated, worst case reported. This is a test setup to show the ISM module can pass 15.207 limits. Antenna port terminated into 50ohm load.

Itron, Inc. WO\#: 108561 Sequence\#: 50 Date: 10/13/2023
15.207 AC Mains - Quasi-peak Test Lead: 115 V 60 Hz Line



Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | ANP06219 | Attenuator | $768-10$ | $3 / 23 / 2022$ | $3 / 23 / 2024$ |
| T2 | ANP05546 | Cable | Heliax | $8 / 1 / 2023$ | $8 / 1 / 2025$ |
| T3 | ANP06515 | Cable | Heliax | $3 / 1 / 2023$ | $3 / 1 / 2025$ |
| T4 | AN01492 | 50uH LISN-Line (L1) | $3816 / 2 N M$ | $3 / 18 / 2022$ | $3 / 18 / 2024$ |
|  | AN01492 | 50uH LISN-Neutral (L2) | $3816 / 2 N M$ | $3 / 18 / 2022$ | $3 / 18 / 2024$ |
|  | AN02673 | Spectrum Analyzer | E4446A | $3 / 2 / 2023$ | $3 / 2 / 2025$ |
| T5 | AN02611 | High Pass Filter | HE9615-150K- | $1 / 5 / 2022$ | $1 / 5 / 2024$ |
|  |  |  | $50-720 B$ |  |  |

Measurement Data: Reading listed by margin. Test Lead: Line

| \# | Freq <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \text { T5 } \\ & \text { dB } \end{aligned}$ | T2 <br> dB | $\begin{array}{r} \mathrm{T} 3 \\ \mathrm{~dB} \\ \hline \end{array}$ | T4 <br> dB | Dist <br> Table | Corr <br> $\mathrm{dB} \mu \mathrm{V}$ | Spec <br> dBu V | Margin <br> dB | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { 384.100k } \\ & \text { Ave } \end{aligned}$ | 36.1 | $\begin{aligned} & \hline+9.1 \\ & +0.1 \end{aligned}$ | +0.0 | +0.0 | +0.1 | +0.0 | 45.4 | 48.2 | -2.8 | Line |
|  | $384.925 \mathrm{k}$ | 36.1 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 45.4 | 48.2 | -2.8 | Line |
|  | $384.100 \mathrm{k}$ <br> QP | 45.6 | $\begin{aligned} & \hline+9.1 \\ & +0.1 \end{aligned}$ | +0.0 | +0.0 | +0.1 | +0.0 | 54.9 | 58.2 | -3.3 | Line |
|  | $\begin{aligned} & 384.925 \mathrm{k} \\ & \mathrm{P} \\ & \hline \end{aligned}$ | 45.6 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 54.9 | 58.2 | -3.3 | Line |
|  | 384.100k | 48.4 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 57.7 | 48.2 | +9.5 | Line |
|  | 384.925k | 48.4 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 57.7 | 48.2 | +9.5 | Line |
|  | $\begin{aligned} & \text { 418.748k } \\ & \text { Ave } \\ & \hline \end{aligned}$ | 34.6 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 43.9 | 47.5 | -3.6 | Line |
|  | 418.747 k | 45.8 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 55.1 | 47.5 | +7.6 | Line |
|  | $\begin{aligned} & 537.132 \mathrm{k} \\ & \mathrm{ve} \end{aligned}$ | 30.7 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 40.0 | 46.0 | -6.0 | Line |
|  | 537.131 k | 43.5 | $\begin{aligned} & +9.1 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +0.1 | +0.0 | 52.8 | 46.0 | +6.8 | Line |
|  | $\begin{aligned} & 499.032 \mathrm{k} \\ & \text { Ave } \\ & \hline \end{aligned}$ | 30.1 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 39.4 | 46.0 | -6.6 | Line |
|  | 499.031k | 43.8 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 53.1 | 46.0 | +7.1 | Line |
| 13 | $\begin{aligned} & \text { 460.932k } \\ & \text { Ave } \end{aligned}$ | 30.1 | $\begin{aligned} & \hline+9.1 \\ & +0.1 \end{aligned}$ | +0.0 | +0.0 | +0.1 | +0.0 | 39.4 | 46.7 | -7.3 | Line |
|  | 460.931k | 43.8 | $\begin{aligned} & \hline+9.1 \\ & +0.1 \end{aligned}$ | +0.0 | +0.0 | +0.1 | +0.0 | 53.1 | 46.7 | +6.4 | Line |
|  | $729.447 \mathrm{k}$ <br> Ave | 29.3 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 38.6 | 46.0 | -7.4 | Line |
|  | 729.446k | 41.9 | $\begin{aligned} & +9.1 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +0.1 | +0.0 | 51.2 | 46.0 | +5.2 | Line |
| 17 | $\begin{aligned} & 1.955 \mathrm{M} \\ & \text { Ave } \\ & \hline \end{aligned}$ | 27.9 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.1 | +0.2 | +0.0 | 37.4 | 46.0 | -8.6 | Line |
|  | 1.955 M | 42.6 | $\begin{aligned} & +9.1 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +0.2 | +0.0 | 52.1 | 46.0 | +6.1 | Line |
|  | $\begin{aligned} & \text { 575.232k } \\ & \text { Ave } \end{aligned}$ | 27.9 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 37.2 | 46.0 | -8.8 | Line |
|  | 575.231 k | 39.8 | $\begin{aligned} & +9.1 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +0.1 | +0.0 | 49.1 | 46.0 | +3.1 | Line |
| 21 | $\begin{aligned} & 1.764 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 27.7 | $\begin{aligned} & +9.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.1 | +0.1 | +0.2 | +0.0 | 37.2 | 46.0 | -8.8 | Line |
|  | 1.764 M | 41.2 | $\begin{aligned} & \hline+9.1 \\ & +0.0 \end{aligned}$ | +0.1 | +0.1 | +0.2 | +0.0 | 50.7 | 46.0 | +4.7 | Line |


| $23$ | $921.129 \mathrm{k}$ <br> ve | 27.7 | $\begin{aligned} & +9.1 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +0.1 | +0.0 | 37.1 | 46.0 | -8.9 | Line |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 921.128 k | 40.3 | $\begin{aligned} & +9.1 \\ & +0.1 \end{aligned}$ | +0.0 | +0.1 | +0.1 | +0.0 | 49.7 | 46.0 | +3.7 | Line |
|  | $690.742 \mathrm{k}$ <br> ve | 27.5 | $\begin{aligned} & +9.1 \\ & +0.2 \end{aligned}$ | +0.0 | +0.0 | +0.1 | $+0.0$ | 36.9 | 46.0 | -9.1 | Line |
| $\wedge$ | 690.741 k | 40.8 | $\begin{aligned} & +9.1 \\ & +0.2 \end{aligned}$ | +0.0 | +0.0 | +0.1 | +0.0 | 50.2 | 46.0 | +4.2 | Line |
|  | $1.994 \mathrm{M}$ | 26.9 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.1 | +0.2 | $+0.0$ | 36.4 | 46.0 | -9.6 | Line |
| $\wedge$ | 1.994 M | 40.3 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.1 | +0.2 | +0.0 | 49.8 | 46.0 | +3.8 | Line |
|  | $1.574 \mathrm{M}$ | 26.7 | $\begin{aligned} & +9.1 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +0.2 | +0.0 | 36.3 | 46.0 | -9.7 | Line |
| $\wedge$ | 1.574 M | 40.3 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.1 | +0.1 | +0.2 | +0.0 | 49.9 | 46.0 | +3.9 | Line |
|  | $\begin{aligned} & 735.191 \mathrm{k} \\ & \text { ve } \\ & \hline \end{aligned}$ | 26.3 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 35.6 | 46.0 | -10.4 | Line |
| $\wedge$ | 735.191k | 41.1 | $\begin{aligned} & +9.1 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +0.1 | $+0.0$ | 50.4 | 46.0 | +4.4 | Line |
|  | $1.113 \mathrm{M}$ <br> ve | 25.9 | $\begin{aligned} & +9.1 \\ & +0.1 \end{aligned}$ | +0.0 | +0.1 | +0.1 | +0.0 | 35.3 | 46.0 | -10.7 | Line |
| $\wedge$ | 1.113 M | 38.6 | $\begin{aligned} & +9.1 \\ & +0.1 \end{aligned}$ | +0.0 | +0.1 | +0.1 | +0.0 | 48.0 | 46.0 | +2.0 | Line |
|  | $1.152 \mathrm{M}$ | 25.8 | $\begin{aligned} & +9.1 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +0.1 | +0.0 | 35.3 | 46.0 | -10.7 | Line |
| $\wedge$ | 1.152 M | 38.3 | $\begin{aligned} & +9.1 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +0.1 | +0.0 | 47.8 | 46.0 | +1.8 | Line |
|  | $\mathrm{ve}^{1.344 \mathrm{M}}$ | 25.5 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.1 | +0.1 | +0.1 | $+0.0$ | 35.0 | 46.0 | -11.0 | Line |
| $\wedge$ | 1.344 M | 38.4 | $\begin{aligned} & +9.1 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +0.1 | $+0.0$ | 47.9 | 46.0 | +1.9 | Line |
|  | $345.200 \mathrm{k}$ <br> ve | 28.9 | $\begin{aligned} & +9.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +0.1 | +0.0 | 38.1 | 49.1 | -11.0 | Line |
| $\wedge$ | 345.200 k | 41.9 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 51.1 | 49.1 | +2.0 | Line |
|  | $\begin{aligned} & 2.765 \mathrm{M} \\ & \mathrm{ve} \\ & \hline \end{aligned}$ | 25.4 | $\begin{aligned} & +9.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +0.2 | $+0.0$ | 34.8 | 46.0 | -11.2 | Line |
| $\wedge$ | 2.765 M | 39.6 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.1 | +0.2 | $+0.0$ | 49.0 | 46.0 | +3.0 | Line |
|  | $\mathrm{ve}^{1.727 \mathrm{M}}$ | 25.2 | $\begin{aligned} & +9.1 \\ & +0.0 \end{aligned}$ | +0.1 | +0.1 | +0.2 | $+0.0$ | 34.7 | 46.0 | -11.3 | Line |
| $\wedge$ | 1.727 M | 39.5 | $\begin{aligned} & +9.1 \\ & +0.0 \end{aligned}$ | +0.1 | +0.1 | +0.2 | +0.0 | 49.0 | 46.0 | +3.0 | Line |
|  | $\begin{aligned} & 429.251 \mathrm{k} \\ & \mathrm{ve} \\ & \hline \end{aligned}$ | 26.4 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | $+0.0$ | 35.7 | 47.3 | -11.6 | Line |
|  | $\mathrm{ve}^{2.032 \mathrm{M}}$ | 24.9 | $\begin{aligned} & +9.1 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +0.2 | +0.0 | 34.4 | 46.0 | -11.6 | Line |
| $\wedge$ | 2.032 M | 39.3 | $\begin{aligned} & +9.1 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +0.2 | +0.0 | 48.8 | 46.0 | +2.8 | Line |

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|  | $\begin{aligned} & 1.918 \mathrm{M} \\ & \mathrm{ve} \\ & \hline \end{aligned}$ | 24.9 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.1 | +0.2 | +0.0 | 34.3 | 46.0 | -11.7 | Line |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 1.918M | 40.5 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.1 | +0.2 | +0.0 | 49.9 | 46.0 | +3.9 | Line |
|  | $431.387 \mathrm{k}$ <br> ve | 25.8 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 35.1 | 47.2 | -12.1 | Line |
|  | $3.802 \mathrm{M}$ <br> ve | 23.4 | $\begin{aligned} & \hline+9.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.1 | +0.1 | +0.2 | +0.0 | 32.9 | 46.0 | -13.1 | Line |
| $\wedge$ | 3.802 M | 39.0 | $\begin{aligned} & +9.1 \\ & +0.0 \end{aligned}$ | +0.1 | +0.1 | +0.2 | +0.0 | 48.5 | 46.0 | +2.5 | Line |
|  | $2.729 \mathrm{M}$ | 23.5 | $\begin{aligned} & \hline+9.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | $+0.2$ | $+0.0$ | 32.9 | 46.0 | -13.1 | Line |
| $\wedge$ | 2.729 M | 40.0 | $\begin{aligned} & +9.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +0.2 | +0.0 | 49.4 | 46.0 | +3.4 | Line |
|  | $\begin{aligned} & \text { 433.717k } \\ & \text { ve } \end{aligned}$ | 24.2 | $\begin{aligned} & \hline+9.1 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +0.1 | +0.0 | 33.5 | 47.2 | -13.7 | Line |
| 56 | $\begin{aligned} & 2.581 \mathrm{M} \\ & \mathrm{ve}^{2} \\ & \hline \end{aligned}$ | 22.3 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.1 | +0.2 | +0.0 | 31.7 | 46.0 | -14.3 | Line |
| $\wedge$ | 2.581 M | 40.5 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.1 | +0.2 | $+0.0$ | 49.9 | 46.0 | +3.9 | Line |
|  | $\begin{aligned} & \text { ve }{ }^{2.542 \mathrm{M}} \\ & \text { ve } \end{aligned}$ | 22.3 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.1 | +0.2 | +0.0 | 31.7 | 46.0 | -14.3 | Line |
| $\wedge$ | 2.542 M | 40.6 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.1 | +0.2 | +0.0 | 50.0 | 46.0 | +4.0 | Line |
|  | $2.114 \mathrm{M}$ <br> ve | 22.2 | $\begin{aligned} & +9.1 \\ & +0.1 \end{aligned}$ | +0.0 | +0.1 | +0.2 | +0.0 | 31.7 | 46.0 | -14.3 | Line |
| $\wedge$ | 2.114 M | 39.6 | $\begin{array}{r} \hline+9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.1 | +0.2 | +0.0 | 49.1 | 46.0 | +3.1 | Line |
|  | $10.940 \mathrm{M}$ | 25.9 | $\begin{aligned} & +9.1 \\ & +0.0 \end{aligned}$ | +0.1 | +0.1 | +0.4 | +0.0 | 35.6 | 50.0 | -14.4 | Line |
| $\wedge$ | 10.940M | 39.7 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | +0.1 | +0.1 | +0.4 | +0.0 | 49.4 | 50.0 | -0.6 | Line |
|  | $\begin{aligned} & 429.251 \mathrm{k} \\ & \mathrm{P} \\ & \hline \end{aligned}$ | 33.0 | $\begin{array}{r} \hline+9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 42.3 | 57.3 | -15.0 | Line |
|  | $\begin{aligned} & 307.700 \mathrm{k} \\ & \text { ve } \end{aligned}$ | 25.7 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 34.9 | 50.0 | -15.1 | Line |
| $\wedge$ | 307.700k | 38.2 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 47.4 | 50.0 | -2.6 | Line |
|  | $\begin{aligned} & 2.394 \mathrm{M} \\ & \mathrm{ve} \\ & \hline \end{aligned}$ | 21.4 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.1 | +0.2 | +0.0 | 30.8 | 46.0 | -15.2 | Line |
| $\wedge$ | 2.394 M | 40.0 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.1 | +0.2 | +0.0 | 49.4 | 46.0 | +3.4 | Line |
|  | $2.073 \mathrm{M}$ <br> ve | 21.0 | $\begin{array}{r} \hline+9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.1 | +0.2 | +0.0 | 30.5 | 46.0 | -15.5 | Line |
| $\wedge$ | 2.073 M | 39.2 | $\begin{aligned} & \hline+9.1 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +0.2 | +0.0 | 48.7 | 46.0 | +2.7 | Line |
|  | $\begin{aligned} & 2.175 \mathrm{M} \\ & \mathrm{ve} \end{aligned}$ | 20.9 | $\begin{aligned} & +9.1 \\ & +0.1 \end{aligned}$ | +0.0 | +0.1 | +0.2 | +0.0 | 30.4 | 46.0 | -15.6 | Line |
| $\wedge$ | 2.175 M | 41.1 | $\begin{aligned} & \hline+9.1 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +0.2 | +0.0 | 50.6 | 46.0 | +4.6 | Line |

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| 73 | $2.358 \mathrm{M}$ | 20.3 | $\begin{aligned} & \hline+9.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +0.2 | +0.0 | 29.7 | 46.0 | -16.3 | Line |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 2.358 M | 40.8 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.1 | +0.2 | +0.0 | 50.2 | 46.0 | +4.2 | Line |
|  | $\begin{aligned} & 433.717 \mathrm{k} \\ & \mathrm{p} \end{aligned}$ | 30.7 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 40.0 | 57.2 | -17.2 | Line |
| $\wedge$ | 429.250 k | 47.5 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 56.8 | 47.3 | +9.5 | Line |
| $\wedge$ | 433.717 k | 46.2 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.1 | +0.0 | 55.5 | 47.2 | +8.3 | Line |
| $\wedge$ | 431.386k | 45.6 | $\begin{aligned} & \hline+9.1 \\ & +0.1 \end{aligned}$ | +0.0 | +0.0 | +0.1 | +0.0 | 54.9 | 47.2 | +7.7 | Line |
|  | $\begin{aligned} & \text { 15.930M } \\ & \text { ive } \end{aligned}$ | 22.6 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | +0.1 | +0.2 | +0.4 | +0.0 | 32.4 | 50.0 | -17.6 | Line |
| $\wedge$ | 15.930M | 39.9 | $\begin{aligned} & \hline+9.1 \\ & +0.0 \end{aligned}$ | +0.1 | +0.2 | +0.4 | +0.0 | 49.7 | 50.0 | -0.3 | Line |
| 81 | $16.590 \mathrm{M}$ <br> ve | 18.0 | $\begin{aligned} & \hline+9.1 \\ & +0.1 \end{aligned}$ | +0.1 | +0.2 | +0.5 | +0.0 | 28.0 | 50.0 | -22.0 | Line |
| $\wedge$ | 16.590 M | 40.1 | $\begin{array}{r} +9.1 \\ +0.1 \\ \hline \end{array}$ | +0.1 | +0.2 | +0.5 | +0.0 | 50.1 | 50.0 | +0.1 | Line |

Test Location: CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A•Bothell, WA 98021•(425) 402-1717
Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software: Itron, Inc.
15.207 AC Mains - Quasi-peak

108561
Conducted Emissions
Date: 10/13/2023

Michael Atkinson
EMITest 5.03.20

Time: 16:04:12
Sequence\#: 51
115 V 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 8 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 8 |  | S/N |

Test Conditions / Notes:
Test Environment Conditions:
Temperature: $22^{\circ} \mathrm{C}$
Humidity: 47\%
Pressure: 100.5 kPa
Test Method: ANSI C63.10 (2013)
Frequency Range: $150 \mathrm{k}-30 \mathrm{MHz}$
Test Setup:
Unit has ISM radio transmitting at $915 \mathrm{MHz}, 10 \mathrm{k}$, and 25 k data rates investigated, worst case reported. This is a test setup to show the ISM module can pass 15.207 limits. Antenna port terminated into 50ohm load.

Itron, Inc. WO\#: 108561 Sequence\#: 51 Date: 10/13/2023
15.207 AC Mains - Quasi-peak Test Lead: 115 V 60 Hz Neutral


|  | Sweep Data |
| :--- | :--- |
| $\times \quad$ QP Readings |  |
|  | Software Version: 5.03 .20 |

- Readings
Average Readings

Software Version: 5.03 .20
1-15.207 AC Mains - Average $\quad$ Ambient $\quad 2$-15.207 AC Mains - Quasi-peak

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | ANP06219 | Attenuator | $768-10$ | $3 / 23 / 2022$ | $3 / 23 / 2024$ |
| T2 | ANP05546 | Cable | Heliax | $8 / 1 / 2023$ | $8 / 1 / 2025$ |
| T3 | ANP06515 | Cable | Heliax | $3 / 1 / 2023$ | $3 / 1 / 2025$ |
|  | AN01492 | 50uH LISN-Line (L1) | $3816 / 2 N M$ | $3 / 18 / 2022$ | $3 / 18 / 2024$ |
| T4 | AN01492 | 50uH LISN-Neutral (L2) | $3816 / 2 N M$ | $3 / 18 / 2022$ | $3 / 18 / 2024$ |
| T5 | AN02673 | Spectrum Analyzer | E4446A | $3 / 2 / 2023$ | $3 / 2 / 2025$ |
| T6 | AN02611 | High Pass Filter | HE9615-150K- | $1 / 5 / 2022$ | $1 / 5 / 2024$ |
|  |  |  | $50-720 B$ |  |  |


| Measurement Data: |  | ading lis | d by m | gin. |  |  | Test Lea | Neutral |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Freq <br> MHz | $\begin{aligned} & \text { Rdng } \\ & \mathrm{dB} \mu \mathrm{~V} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~T} 5 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \hline \mathrm{T} 2 \\ & \mathrm{~T} 6 \\ & \mathrm{~dB} \end{aligned}$ | T3 <br> dB | T4 <br> dB | Dist <br> Table | $\begin{array}{r} \hline \text { Corr } \\ \text { dB } \mu \mathrm{V} \\ \hline \end{array}$ | $\begin{array}{r} \hline \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} \\ \hline \end{array}$ | Margin <br> dB | Polar Ant |
| $\begin{aligned} & 1 \quad 417.324 \mathrm{k} \\ & \text { Ave } \end{aligned}$ | 34.5 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.0 | +0.0 | +0.0 | 43.7 | 47.5 | -3.8 | Neutr |
| $\begin{aligned} & \hline 2383.679 \mathrm{k} \\ & \text { Ave } \\ & \hline \end{aligned}$ | 34.9 | $\begin{aligned} & +9.1 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.0 | +0.0 | +0.0 | 44.1 | 48.2 | -4.1 | Neutr |
| $\begin{gathered} 3{ }^{383.679 \mathrm{k}} \\ \mathrm{QP} \\ \hline \end{gathered}$ | 44.5 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.0 | 53.7 | 58.2 | -4.5 | Neutr |
| $\wedge 383.679 \mathrm{k}$ | 47.5 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.0 | +0.0 | +0.0 | 56.7 | 48.2 | +8.5 | Neutr |
| $\begin{gathered} 5{ }^{517.324 \mathrm{k}} \\ \mathrm{QP} \end{gathered}$ | 43.0 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.0 | 52.2 | 57.5 | -5.3 | Neutr |
| ^ 417.323 k | 45.8 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +0.1 \\ +0.1 \end{array}$ | +0.0 | +0.0 | $+0.0$ | 55.0 | 47.5 | +7.5 | Neutr |
| $\begin{aligned} & 7538.946 \mathrm{k} \\ & \text { Ave } \\ & \hline \end{aligned}$ | 30.9 | $\begin{aligned} & +9.1 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.0 | 40.1 | 46.0 | -5.9 | Neutr |
| ^ 538.946k | 43.7 | $\begin{aligned} & +9.1 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.0 | 52.9 | 46.0 | +6.9 | Neutr |
| $\begin{aligned} & \hline 9{ }^{462.746 \mathrm{k}} \\ & \mathrm{QPP} \\ & \hline \end{aligned}$ | 40.9 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.0 | 50.1 | 56.6 | -6.5 | Neutr |
| $\begin{gathered} 10 \begin{array}{c} 498.427 \mathrm{k} \\ \mathrm{QP} \end{array} \\ \hline \end{gathered}$ | 40.3 | $\begin{array}{r} +9.1 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{array}{r} +0.0 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.0 | 49.5 | 56.0 | -6.5 | Neutr |
| $\begin{aligned} & 11 \begin{array}{l} 498.427 \mathrm{k} \\ \text { Ave } \end{array} \end{aligned}$ | 30.3 | $\begin{aligned} & +9.1 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.0 | 39.5 | 46.0 | -6.5 | Neutr |
| ^ 498.426k | 43.7 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.0 | 52.9 | 46.0 | +6.9 | Neutr |
| $\begin{gathered} \hline 13 \begin{array}{l} 462.746 \mathrm{k} \\ \text { Ave } \end{array} \\ \hline \end{gathered}$ | 30.9 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +0.1 \\ + \\ \hline \end{array}$ | +0.0 | +0.0 | $+0.0$ | 40.1 | 46.6 | -6.5 | Neutr |
| ^ 462.745k | 44.7 | $\begin{array}{r} +9.1 \\ +0.0 \end{array}$ | $\begin{array}{r} +0.0 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.0 | 53.9 | 46.6 | +7.3 | Neutr |
| $\begin{gathered} \hline 15 \begin{array}{c} 728.540 \mathrm{k} \\ \text { Ave } \end{array} \\ \hline \end{gathered}$ | 29.7 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +0.1 \\ \hline \end{array}$ | +0.0 | +0.0 | +0.0 | 38.9 | 46.0 | -7.1 | Neutr |
| $\wedge 728.539 \mathrm{k}$ | 42.2 | $\begin{array}{r} +9.1 \\ +9.1 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.1 \\ & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.0 | +0.0 | $+0.0$ | 51.4 | 46.0 | +5.4 | Neutr |
| $\begin{gathered} 17 \mathrm{Ave}^{2.803 \mathrm{M}} \\ \mathrm{~A}^{2} \end{gathered}$ | 28.8 | $\begin{aligned} & +9.1 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.1 | +0.0 | +0.0 | 38.0 | 46.0 | -8.0 | Neutr |
| ^ 2.803 M | 42.8 | $\begin{aligned} & +9.1 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.1 | +0.0 | +0.0 | 52.0 | 46.0 | +6.0 | Neutr |
| $\begin{gathered} 19{ }^{3.374 \mathrm{M}} \\ \text { Ave } \\ \hline \end{gathered}$ | 28.7 | $\begin{aligned} & +9.1 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.1 | +0.0 | +0.0 | 37.9 | 46.0 | -8.1 | Neutr |
| 3.374M | 42.5 | $\begin{array}{r} +9.0 \\ +9.1 \\ +0.0 \end{array}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.1 | +0.0 | +0.0 | 51.7 | 46.0 | +5.7 | Neutr |
| $\begin{gathered} 21 \quad 2.956 \mathrm{M} \\ \mathrm{Ave}^{2} \\ \hline \end{gathered}$ | 28.5 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.1 | +0.0 | +0.0 | 37.7 | 46.0 | -8.3 | Neutr |
| 2.956M | 42.7 | $\begin{aligned} & +9.1 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.1 | +0.0 | +0.0 | 51.9 | 46.0 | +5.9 | Neutr |

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| 23 | $3.142 \mathrm{M}$ | 28.5 | $\begin{aligned} & +9.1 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.1 | +0.0 | +0.0 | 37.7 | 46.0 | -8.3 | Neutr |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 3.142 M | 42.0 | $\begin{aligned} & +9.1 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \end{aligned}$ | +0.1 | +0.0 | +0.0 | 51.2 | 46.0 | +5.2 | Neutr |
| 25 | $1.954 \mathrm{M}$ | 28.4 | $\begin{aligned} & +9.1 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | $+0.1$ | $+0.0$ | $+0.0$ | 37.7 | 46.0 | -8.3 | Neutr |
| $\wedge$ | 1.954 M | 42.5 | $\begin{aligned} & +9.1 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.0 | +0.0 | 51.8 | 46.0 | +5.8 | Neutr |
|  | $\begin{aligned} & 1.573 \mathrm{M} \\ & \mathrm{ve} \\ & \hline \end{aligned}$ | 27.7 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.1 \\ & +0.1 \end{aligned}$ | +0.1 | +0.0 | +0.0 | 37.1 | 46.0 | -8.9 | Neutr |
| $\wedge$ | 1.573 M | 40.3 | $\begin{aligned} & +9.1 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.1 \end{aligned}$ | +0.1 | $+0.0$ | $+0.0$ | 49.7 | 46.0 | +3.7 | Neutr |
|  | $345.290 \mathrm{k}$ | 31.0 | $\begin{aligned} & +9.1 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | +0.0 | +0.0 | 40.1 | 49.1 | -9.0 | Neutr |
| $\wedge$ | 345.290k | 43.9 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +0.0 | 53.0 | 49.1 | +3.9 | Neutr |
|  | $922.000 \mathrm{k}$ <br> ve | 27.6 | $\begin{aligned} & \hline+9.1 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.0 | +0.0 | 36.9 | 46.0 | -9.1 | Neutr |
| $\wedge$ | 922.000 k | 40.1 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.1 | +0.0 | +0.0 | 49.4 | 46.0 | +3.4 | Neutr |
|  | $\mathrm{ve}^{3.224 \mathrm{M}}$ | 27.6 | $\begin{aligned} & +9.1 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.1 | +0.0 | +0.0 | 36.8 | 46.0 | -9.2 | Neutr |
| $\wedge$ | 3.224 M | 42.2 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.1 | +0.0 | $+0.0$ | 51.4 | 46.0 | +5.4 | Neutr |
|  | $\begin{aligned} & 1.768 \mathrm{M} \\ & \mathrm{ve} \end{aligned}$ | 27.3 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.1 \\ +0.0 \\ \hline \end{array}$ | +0.1 | +0.0 | +0.0 | 36.6 | 46.0 | -9.4 | Neutr |
| $\wedge$ | 1.768 M | 41.0 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.1 | +0.0 | +0.0 | 50.3 | 46.0 | +4.3 | Neutr |
|  | $735.191 \mathrm{k}$ | 26.9 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +0.0 | 36.1 | 46.0 | -9.9 | Neutr |
| $\wedge$ | 735.191k | 41.7 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.0 | +0.0 | $+0.0$ | 50.9 | 46.0 | +4.9 | Neutr |
|  | $\begin{aligned} & 1.382 \mathrm{M} \\ & \mathrm{ve} \\ & \hline \end{aligned}$ | 26.6 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.1 \\ +0.1 \\ \hline \end{array}$ | $+0.1$ | +0.0 | +0.0 | 36.0 | 46.0 | -10.0 | Neutr |
| $\wedge$ | 1.382 M | 39.0 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.1 \\ & +0.1 \\ & \hline \end{aligned}$ | $+0.1$ | +0.0 | $+0.0$ | 48.4 | 46.0 | +2.4 | Neutr |
|  | $2.767 \mathrm{M}$ | 26.7 | $\begin{aligned} & +9.1 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \end{aligned}$ | +0.1 | +0.0 | +0.0 | 35.9 | 46.0 | -10.1 | Neutr |
| $\wedge$ | 2.767 M | 42.8 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.1 | +0.0 | +0.0 | 52.0 | 46.0 | +6.0 | Neutr |
|  | $3.572 \mathrm{M}$ <br> ve | 26.7 | $\begin{aligned} & \hline+9.1 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.1 | +0.0 | +0.0 | 35.9 | 46.0 | -10.1 | Neutr |
| $\wedge$ | 3.572 M | 43.2 | $\begin{array}{r} +9.1 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.0 \end{aligned}$ | +0.1 | +0.0 | +0.0 | 52.4 | 46.0 | +6.4 | Neutr |
|  | $2.615 \mathrm{M}$ <br> ve | 26.3 | $\begin{aligned} & \hline+9.1 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.1 | +0.0 | $+0.0$ | 35.5 | 46.0 | -10.5 | Neutr |
| $\wedge$ | 2.615 M | 43.3 | $\begin{array}{r} +9.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.1 | +0.0 | +0.0 | 52.5 | 46.0 | +6.5 | Neutr |

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| Ave | $\mathrm{ve}^{1.113 \mathrm{M}}$ | 26.1 | $\begin{aligned} & +9.1 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.0 | +0.0 | 35.4 | 46.0 | -10.6 | Neutr |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 1.113M | 38.8 | +9.1 | +0.0 | +0.1 | +0.0 | +0.0 | 48.1 | 46.0 | +2.1 | Neutr |
|  |  |  | +0.0 | +0.1 |  |  |  |  |  |  |  |
| 49 | 3.686M | 25.9 | +9.1 | +0.1 | +0.1 | +0.0 | +0.0 | 35.2 | 46.0 | -10.8 | Neutr |
| Ave |  |  | +0.0 | +0.0 |  |  |  |  |  |  |  |
| $\wedge$ | 3.686 M | 41.7 | +9.1 | +0.1 | +0.1 | +0.0 | $+0.0$ | 51.0 | 46.0 | +5.0 | Neutr |
|  |  |  | +0.0 | +0.0 |  |  |  |  |  |  |  |
| 51 | 2.579 M | 25.3 | +9.1 | +0.0 | +0.1 | +0.0 | +0.0 | 34.5 | 46.0 | -11.5 | Neutr |
| Ave |  |  | +0.0 | +0.0 |  |  |  |  |  |  |  |
| $\wedge$ | 2.579 M | 43.0 | +9.1 | +0.0 | +0.1 | +0.0 | $+0.0$ | 52.2 | 46.0 | +6.2 | Neutr |
|  |  |  | +0.0 | +0.0 |  |  |  |  |  |  |  |
| 53 | 2.433 M | 24.9 | +9.1 | +0.0 | +0.1 | +0.0 | +0.0 | 34.1 | 46.0 | -11.9 | Neutr |
| Ave |  |  | +0.0 | +0.0 |  |  |  |  |  |  |  |
| $\wedge$ | 2.433 M | 42.6 | +9.1 | +0.0 | +0.1 | +0.0 | +0.0 | 51.8 | 46.0 | +5.8 | Neutr |
|  |  |  | +0.0 | +0.0 |  |  |  |  |  |  |  |
| 55 | 2.396M | 24.3 | +9.1 | +0.0 | +0.1 | +0.0 | +0.0 | 33.5 | 46.0 | -12.5 | Neutr |
| Ave |  |  | +0.0 | +0.0 |  |  |  |  |  |  |  |
| $\wedge$ | 2.395M | 42.9 | +9.1 | +0.0 | +0.1 | +0.0 | +0.0 | 52.1 | 46.0 | +6.1 | Neutr |
|  |  |  | +0.0 | +0.0 |  |  |  |  |  |  |  |
| 57 | 2.212 M | 22.9 | +9.1 | +0.0 | +0.1 | +0.0 | +0.0 | 32.2 | 46.0 | -13.8 | Neutr |
| Ave |  |  | +0.0 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 2.212M | 42.1 | +9.1 | +0.0 | +0.1 | +0.0 | +0.0 | 51.4 | 46.0 | +5.4 | Neutr |
|  |  |  | +0.0 | +0.1 |  |  |  |  |  |  |  |
| 59 | 11.365M | 24.8 | +9.1 | +0.1 | +0.1 | +0.2 | +0.0 | 34.3 | 50.0 | -15.7 | Neutr |
| Ave |  |  | +0.0 | +0.0 |  |  |  |  |  |  |  |
| $\wedge$ | 11.365M | 39.9 | +9.1 | +0.1 | +0.1 | +0.2 | +0.0 | 49.4 | 50.0 | -0.6 | Neutr |
|  |  |  | +0.0 | +0.0 |  |  |  |  |  |  |  |
| 61 | 15.355M | 23.9 | +9.1 | +0.1 | +0.2 | +0.2 | +0.0 | 33.5 | 50.0 | -16.5 | Neutr |
| Ave |  |  | +0.0 | +0.0 |  |  |  |  |  |  |  |
| $\wedge$ | 15.355M | 39.5 | +9.1 | +0.1 | +0.2 | +0.2 | +0.0 | 49.1 | 50.0 | -0.9 | Neutr |
|  |  |  | +0.0 | +0.0 |  |  |  |  |  |  |  |
| 63 | 21.940M | 18.6 | +9.1 | +0.1 | +0.2 | +0.5 | +0.0 | 28.6 | 50.0 | -21.4 | Neutr |
| Ave |  |  | +0.0 | +0.1 |  |  |  |  |  |  |  |
| ^ 21.940 M |  | 39.4 | +9.1 | +0.1 | +0.2 | +0.5 | +0.0 | 49.4 | 50.0 | -0.6 | Neutr |
|  |  |  | +0.0 | +0.1 |  |  |  |  |  |  |  |

Test Setup Photos)


## SUPPLEMENTAL INFORMATION

## Measurement Uncertainty

| Uncertainty Value | Parameter |
| :---: | :---: |
| 4.73 dB | Radiated Emissions |
| 3.34 dB | Mains Conducted Emissions |
| 3.30 dB | Disturbance Power |

Uncertainties reported are worst case for all CKC Laboratories' sites and represent expanded uncertainties expressed at approximately the $95 \%$ confidence level using a coverage factor of $\mathrm{k}=2$. Compliance is deemed to occur provided measurements are below the specified limits.

## Emissions Test Details

## TESTING PARAMETERS

Unless otherwise indicated, the following configuration parameters are used for equipment setup: The cables were routed consistent with the typical application by varying the configuration of the test sample. Interface cables were connected to the available ports of the test unit. The effect of varying the position of the cables was investigated to find the configuration that produced maximum emissions. Cables were of the type and length specified in the individual requirements. The length of cable that produced maximum emissions was selected

The equipment under test (EUT) was set up in a manner that represented its normal use, as shown in the setup photographs. Any special conditions required for the EUT to operate normally are identified in the comments that accompany the emissions tables.

The emissions data was taken with a spectrum analyzer or receiver. Incorporating the applicable correction factors for distance, antenna, cable loss and amplifier gain, the data was reduced as shown in the table below. The corrected data was then compared to the applicable emission limits. Preliminary and final measurements were taken in order to ensure that all emissions from the EUT were found and maximized.

## CORRECTION FACTORS

The basic spectrum analyzer reading was converted using correction factors as shown in the highest emissions readings in the tables. For radiated emissions in $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$, the spectrum analyzer reading in $\mathrm{dB} \mu \mathrm{V}$ was corrected by using the following formula. This reading was then compared to the applicable specification limit. Individual measurements were compared with the displayed limit value in the margin column. The margin was calculated based on subtracting the limit value from the corrected measurement value; a positive margin represents a measurement exceeding the limit, while a negative margin represents a measurement less than the limit.

| SAMPLE CALCULATIONS |  |  |  |
| :--- | :--- | :--- | :---: |
|  | Meter reading | $(\mathrm{dB} \mu \mathrm{V})$ |  |
| + | Antenna Factor | $(\mathrm{dB} / \mathrm{m})$ |  |
| + | Cable Loss | $(\mathrm{dB})$ |  |
| - | Distance Correction | $(\mathrm{dB})$ |  |
| - | Preamplifier Gain | $(\mathrm{dB})$ |  |
| $=$ | Corrected Reading | $(\mathrm{dB} \mu \mathrm{V} / \mathrm{m})$ |  |

## TEST INSTRUMENTATION AND ANALYZER SETTINGS

The test instrumentation and equipment listed were used to collect the emissions data. A spectrum analyzer or receiver was used for all measurements. Unless otherwise specified, the following table shows the measuring equipment bandwidth settings that were used in designated frequency bands. For testing emissions, an appropriate reference level and a vertical scale size of 10 dB per division were used.

| MEASURING EQUIPMENT BANDWIDTH SETTINGS PER FREQUENCY RANGE |  |  |  |
| :---: | :---: | :---: | :---: |
| TEST | BEGINNING FREQUENCY | ENDING FREQUENCY | BANDWIDTH SETTING |
| CONDUCTED EMISSIONS | 150 kHz | 30 MHz | 9 kHz |
| RADIATED EMISSIONS | 9 kHz | 150 kHz | 200 Hz |
| RADIATED EMISSIONS | 150 kHz | 30 MHz | 9 kHz |
| RADIATED EMISSIONS | 30 MHz | 1000 MHz | 120 kHz |
| RADIATED EMISSIONS | 1000 MHz | $>1 \mathrm{GHz}$ | 1 MHz |

## SPECTRUM ANALYZER/RECEIVER DETECTOR FUNCTIONS

The notes that accompany the measurements contained in the emissions tables indicate the type of detector function used to obtain the given readings. Unless otherwise noted, all readings were made in the "positive peak" detector mode. Whenever a "quasi-peak" or "average" reading was recorded, the measurement was annotated with a "QP" or an "Ave" on the appropriate rows of the data sheets. In cases where quasi-peak or average limits were employed and data exists for multiple measurement types for the same frequency then the peak measurement was retained in the report for reference, however the numbering for the affected row was removed and an arrow or caret ("^") was placed in the far left-hand column indicating that the row above takes precedence for comparison to the limit. The following paragraphs describe in more detail the detector functions and when they were used to obtain the emissions data.

## Peak

In this mode, the spectrum analyzer or receiver recorded all emissions at their peak value as the frequency band selected was scanned. By combining this function with another feature called "peak hold," the measurement device had the ability to measure intermittent or low duty cycle transient emission peak levels. In this mode the measuring device made a slow scan across the frequency band selected and measured the peak emission value found at each frequency across the band.

## Quasi-Peak

Quasi-peak measurements were taken using the quasi-peak detector when the true peak values exceeded or were within 2 dB of a quasi-peak specification limit. Additional QP measurements may have been taken at the discretion of the operator.

## Average

Average measurements were taken using the average detector when the true peak values exceeded or were within 2 dB of an average specification limit. Additional average measurements may have been taken at the discretion of the operator. If the specification or test procedure requires trace averaging, then the averaging was performed using 100 samples or as required by the specification. All other average measurements are performed using video bandwidth averaging. To make these measurements, the test engineer reduces the video bandwidth on the measuring device until the modulation of the signal is filtered out. At this point the measuring device is set into the linear mode and the scan time is reduced.

