# Itron, Inc. 

TEST REPORT FOR

ORRNA Model: RN-EGS

Tested to The Following Standards:

FCC Part 15 Subpart C Section(s)
15.207 \& 15.247
(FHSS 902-928 MHz)

Report No.: 100619-5

Date of issue: December 15, 2017


Testing Certificates: 803.01, 803.02, 803.05, 803.06

This test report bears the accreditation symbol indicating that the testing performed herein meets the test and reporting requirements of ISO/IEC 17025 under the applicable scope of EMC testing for CKC Laboratories, Inc.

We strive to create long-term, trust based relationships by providing sound, adaptive, customer first testing services. We embrace each of our customers' unique EMC challenges, not as an interruption to set processes, but rather as the reason we are in business.

TABLE OF CONTENTS
Administrative Information ..... 3
Test Report Information .....  3
Report Authorization .....  3
Test Facility Information .....  4
Software Versions .....  4
Site Registration \& Accreditation Information .....  .4
Summary of Results ..... 5
Modifications During Testing .....  .5
Conditions During Testing .....  .5
Equipment Under Test .....  6
General Product Information ..... 6
FCC Part 15 Subpart C ..... 7
15.247(a) Transmitter Characteristics ..... 7
15.247(a)(1)(i) 20 dB Bandwidth ..... 7
15.247(a)(1) Carrier Separation ..... 12
15.247(a)(1)(i) Number of Channels ..... 13
15.247(b)(2) Output Power ..... 16
15.35(c) Duty Cycle Correction Factor ..... 24
15.247(d) RF Conducted Emissions \& Band Edge ..... 26
15.247(d) Radiated Emissions \& Band Edge ..... 34
15.207 AC Conducted Emissions ..... 53
Appendix A: Customer Provided Information ..... 64
Manufacturer's Declaration: 15.247(a)(1)(i) Average Time of Occupancy ..... 64
DCCF Plot Data ..... 64
Supplemental Information ..... 65
Measurement Uncertainty ..... 65
Emissions Test Details. ..... 65

# ADMINISTRATIVE INFORMATION 

## Test Report Information

## REPORT PREPARED FOR:

Iron, Inc.
2111 N. Molter Road
Liberty Lake, WA 99019

Representative: Jay Holcomb
Customer Reference Number: 135842

DATE OF EQUIPMENT RECEIPT:
DATES) OF TESTING:

REPORT PREPARED BY:

Dianne Dudley
CKC Laboratories, Inc.
5046 Sierra Pines Drive
Mariposa, CA 95338

Project Number: 100619

November 27, 2017
November 27-29, 2017

## Report Authorization

The test data contained in this report documents the observed testing parameters pertaining to and are relevant for only the sample equipment tested in the agreed upon operational modes) and configurations) as identified herein. Compliance assessment remains the client's responsibility. This report may not be used to claim product endorsement by A2LA or any government agencies. This test report has been authorized for release under quality control from CKC Laboratories, Inc.


Steve Behm
Director of Quality Assurance \& Engineering Services CKC Laboratories, Inc.

## Test Facility Information



Our laboratories are configured to effectively test a wide variety of product types. CKC utilizes first class test equipment, anechoic chambers, data acquisition and information services to create accurate, repeatable and affordable test results.

TEST LOCATION(S):
CKC Laboratories, Inc.
Canyon Park
22116 23rd Drive S.E., Suite A
Bothell, WA 98021

## Software Versions

| CKC Laboratories Proprietary Software | Version |
| :--- | :---: |
| EMITest Emissions | 5.03 .11 |

Site Registration \& Accreditation Information

| Location | NIST CB \# | TAIWAN | CANADA | FCC | JAPAN |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Canyon Park <br> Bothell, WA | US0081 | SL2-IN-E-1145R | $3082 \mathrm{C}-1$ | US1022 | A-0148 |

## SUMMARY OF RESULTS

Standard / Specification: FCC Part 15 Subpart C-15.247 (FHSS 902-928MHz)

| Test Procedure | Description | Modifications | Results |
| :--- | :--- | :--- | :--- |
| $15.247(\mathrm{a})(1)(\mathrm{i})$ | Occupied Bandwidth | NA | Pass |
| $15.247(\mathrm{a})(1)$ | Carrier Separation | NA | Pass |
| $15.247(\mathrm{a})(1)(\mathrm{i})$ | Number of Hopping Channels | NA | Pass |
| $15.247(\mathrm{a})(1)(\mathrm{i})$ | Average Time of Occupancy | NA | NP |
| $15.247(\mathrm{~b})(2)$ | Output Power | NA | Pass |
| $15.247(\mathrm{~d})$ | RF Conducted Emissions \& Band Edge | NA | Pass |
| $15.247(\mathrm{~d})$ | Radiated Emissions \& Band Edge | NA | Pass |
| 15.207 | AC Conducted Emissions | NA | Pass |

NA = Not Applicable
NP = CKC Laboratories was not contracted to perform test. See Appendix A for Manufacturer's Declaration.

## Modifications During Testing

This list is a summary of the modifications made to the equipment during testing.

## Summary of Conditions

No modifications were made during testing.

Modifications listed above must be incorporated into all production units.

Conditions During Testing
This list is a summary of the conditions noted to the equipment during testing.

## Summary of Conditions

None

## EQUIPMENT UNDER TEST (EXT)

The following device has been tested by CKC Laboratories: ORRN

Since the time of testing the manufacturer has updated the device name from ORRN to ORRNA and declares the device is identical electrically, any differences between them do not affect their EMC characteristics, and therefore meets the level of testing equivalent to the tested device.

During testing, numerous configurations may have been utilized. The configurations listed below support compliance to the standards) listed in the Summary of Results section.

## Configuration 1

Equipment Tested:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| ORRNA | Itron, Inc. | RN-EGS | 321128365 |

## Support Equipment:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Laptop | Dell | E6430 | NA |
| AC/DC Adapter (for Laptop) | Dell | DA130PE-00 | NA |

## General Product Information:

| Product Information | Manufacturer-Provided Details |
| :---: | :---: |
| Equipment Type: | Stand-Alone Equipment |
| Type of Wideband System: | Proprietary FHSS |
| Operating Frequency Range: | $903-926.9 \mathrm{MHz}$ |
| Number of Hopping Channels: | 120 |
| Modulation Types): | $12.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK), $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK) |
| Maximum Duty Cycle: | $23.8 \%$ |
| Number of TX Chains: | 1 |
| Antenna Types) and Gain: | External Monopole, 5.15 or 5.5 dBi |
| Beamforming Type: | N/A |
| Antenna Connection Type: | External Connector |
| Nominal Input Voltage: | $115-230 \mathrm{VAC}, 60 \mathrm{~Hz}$ |
| Firmware / Software used for Test: | Firmware: ARM 1.0.0.0 DSP 1.0.0.0, FPGA 4.14 |
|  | Software: SrTest100 v4.1.1.25 |

## FCC Part 15 Subpart C

### 15.247(a) Transmitter Characteristics

| Test Setup/Conditions |  |  |  |
| :--- | :--- | :--- | :--- |
| Test Location: | Bothell Lab Bench | Test Engineer: | M. Atkinson |
| Test Method: | ANSI C63.10 (2013) | Test Date(s): | $11 / 27 / 17$ |
| Configuration: | 1 | The EUT ISM port is continuously transmitting with modulation. The EUT ISM port is <br> connected directly to a spectrum analyzer for direct connected measurements. Low, Mid, <br> High channels investigated, all modulation types investigated, worst case reported. |  |
| Test Setup: |  |  |  |


| Environmental Conditions |  |  |  |
| :---: | :---: | ---: | :---: |
| Temperature (으) | 21 | Relative Humidity (\%): | 37 |


| Test Equipment |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Asset\# | Description | Manufacturer | Model | Cal Date | Cal Due |  |
| 02871 | Spectrum Analyzer | Agilent | E4440A | $2 / 24 / 2017$ | $2 / 24 / 2019$ |  |
| P06219 | Attenuator | Narda | $768-10$ | $4 / 12 / 2016$ | $4 / 12 / 2018$ |  |
| 02871 | Spectrum Analyzer | Agilent | E4440A | $2 / 24 / 2017$ | $2 / 24 / 2019$ |  |

### 15.247(a)(1)(i) 20 dB Bandwidth

| Test Data Summary |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Frequency <br> $(\mathbf{M H z})$ | Antenna <br> Port | Modulation | Measured <br> $\mathbf{( k H z )}$ | Limit <br> $(\mathbf{k H z})$ | Results |
| 903 | 1 | $12.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK) | 138.92 | $\leq 500$ | Pass |
| 915 | 1 | $12.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK) | 138.79 | $\leq 500$ | Pass |
| 926.9 | 1 | $12.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK) | 138.98 | $\leq 500$ | Pass |
| 903 | 1 | $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK) | 83.82 | $\leq 500$ | Pass |
| 915 | 1 | $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK) | 84.52 | $\leq 500$ | Pass |
| 926.9 | 1 | $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK) | 85.07 | $\leq 500$ | Pass |



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## Plots)


12.5 k 903 MHz

12.5k 915MHz

12.5k 926.9MHz

37.5k 903MHz

37.5k 915MHz

37.5 k 926.9 MHz


### 15.247(a)(1) Carrier Separation

| Test Data Summary |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Limit applied: 20dB bandwidth of the hopping channel. |  |  |  |  |
| Antenna <br> Port | Operational Mode | Measured <br> $\mathbf{( k H z )}$ | Limit <br> $(\mathbf{k H z})$ | Results |
| 1 | Continuously Transmitting while <br> Hopping | 200.3 | $\geq 138.98 \mathrm{kHz}$ | Pass |

## Plot (s)



### 15.247(a)(1)(i) Number of Channels

| Test Data Summary |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Limit $=\left\{\begin{array}{l}50 \text { Channels } \mid 20 d B \quad B W<250 \mathrm{kHz} \\ 25 \text { Channels } \mid 20 d B \quad B W \geq 250 \mathrm{kHz}\end{array}\right.$ |  |  |  |  |
| Antenna <br> Port | Operational Mode | Measured <br> (Channels) | Limit <br> (Channels) | Results |
| 1 | Continuously Transmitting while <br> Hopping | 120 | $\geq 50$ | Pass |

## Plot(s)



902-914.9MHz, 60 Channels

914.9-928MHz, 60 Channels

## Test Setup Photo(s)



### 15.247(b)(2) Output Power

| Test Setup/Conditions |  |  |  |
| :--- | :--- | :--- | :--- |
| Test Location: | Bothell Lab Bench | Test Engineer: | M. Atkinson |
| Test Method: | ANSI C63.10 (2013) | Test Date(s): | $11 / 27 / 17$ |
| Configuration: | 1 |  |  |
| Test Setup: | See data sheet below. |  |  |


| Environmental Conditions |  |  |  |
| :---: | :---: | :---: | :---: |
| Temperature (으) | 22 | Relative Humidity (\%): | 36 |


| Test Data Summary - Voltage Variations |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Frequency <br> $(\mathrm{MHz})$ | Modulation / Ant Port | $\mathbf{V}_{\text {Minimum }}$ <br> $(\mathbf{d B m})$ | $\mathbf{V}_{\text {Nominal }}$ <br> $(\mathrm{dBm})$ | $\mathbf{V}_{\text {Maximum }}$ <br> $(\mathrm{dBm})$ | Max Deviation <br> from V $_{\text {Nominal }}(\mathbf{d B})$ |  |
| 903 | $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK) | 28.9 | 28.9 | 28.9 | 0.0 |  |
| 915 | $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK) | 28.7 | 28.7 | 28.7 | 0.0 |  |
| 926.9 | $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK) | 28.7 | 28.7 | 28.7 | 0.0 |  |

Test performed using operational mode with the highest output power, representing worst case.

## Parameter Definitions:

Measurements performed at input voltage according to manufacturer specification.
The EUT does not operate beyond the listed Vminimum and Vmaximum

| Parameter | Value |
| :--- | :--- |
| V $_{\text {Nominal }}:$ | $115-230 \mathrm{VAC}, 60 \mathrm{~Hz}$ |
| V Minimum: | $85 \mathrm{VAC}, 60 \mathrm{~Hz}$ |
| V Maximum: | $264 \mathrm{VAC}, 60 \mathrm{~Hz}$ |

Test Data Summary - RF Conducted Measurement
Limit $=\left\{\begin{array}{l}30 \mathrm{dBm} \text { Conducted } / 36 \mathrm{dBm} \text { EIRP } \mid \geq 50 \text { Channels } \\ 24 \mathrm{dBm} \text { Conducted } / 30 \mathrm{dBm} \text { EIRP } \mid<50 \text { Channels (min 25) }\end{array}\right.$

| Frequency <br> $(\mathrm{MHz})$ | Modulation | Ant. Type $/$ Gain (dBi) | Measured <br> $(\mathrm{dBm})$ | Limit <br> $(\mathbf{d B m})$ | Results |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 903 | $12.5 \mathrm{Kbit} / \mathrm{sec}$ FM <br> $(2 \mathrm{GFSK})$ | External Monopole, 5.5 dBi <br> Max | 28.9 | $\leq 30$ | Pass |
| 915 | $12.5 \mathrm{Kbit} / \mathrm{sec}$ FM <br> $(2 \mathrm{GFSK})$ | External Monopole, 5.5 dBi <br> Max | 28.8 | $\leq 30$ | Pass |
| 926.9 | $12.5 \mathrm{Kbit} / \mathrm{sec}$ FM <br> $(2 \mathrm{GFSK})$ | External Monopole, 5.5 dBi <br> Max | 28.6 | $\leq 30$ | Pass |
| 903 | $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM <br> $(2 \mathrm{GFSK})$ | External Monopole, 5.5 dBi <br> Max | 28.9 | $\leq 30$ | Pass |
| 915 | $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM <br> $(2 \mathrm{GFSK})$ | External Monopole, 5.5 dBi <br> Max | 28.7 | $\leq 30$ | Pass |
| 926.9 | $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM <br> $(2 \mathrm{GFSK})$ | External Monopole, 5.5 dBi <br> Max | 28.7 | $\leq 30$ | Pass |

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## Plots


12.5k 903MHz

12.5 k 915 MHz

12.5k 926.9MHz

37.5 k 903 MHz

37.5 k 915 MHz

37.5k 926.9MHz

## Test Setup / Conditions / Data

| Test Location: | CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362) |
| :---: | :---: |
| Customer: | Itron, Inc. |
| Specification: | 15.247(b) Power Output (902-928 MHz FHSS >50 Channels) |
| Work Order \#: | 100619 Date: 11/27/2017 |
| Test Type: | Conducted Emissions Time: 12:02:13 |
| Tested By: | Michael Atkinson Sequence\#: 4 |
| Software: | EMITest 5.03.11 115VAC 60Hz |

## Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Test Conditions / Notes:

Frequency Range: Fundamental
Frequency tested: $903,915,926.9 \mathrm{MHz}$
Firmware power setting: Max
Firmware: ARM 1.0.0.0 DSP 1.0.0.0, FPGA 4.1, Test Software: SrTest100 v4.1.1.25
Modulation: $12.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK), $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK)
Antenna type: External Monopole
Antenna Gain: 5.15 dBi or 5.5 dBi
Duty Cycle: Tested at $100 \%$
Setup: EUT ISM port is continuously transmitting with modulation. The EUT ISM port is connected directly to a
spectrum analyzer for direct connected measurements. Low, Mid, High channels investigated, all modulation types
investigated, worst case reported. Also investigated voltage variations based on manufacturer specified Vmin and
Vmax.

Itron, Inc. WO\#: 100619 Sequence\#: 4 Date: 11/27/2017
15.247 (b) Power Output ( $902-928 \mathrm{MHz}$ FHSS $>50$ Channels) Test Lead: 115 VAC 60 Hz None


- Sweep Data
- Readings

0 Peak Readings

* QP Readings
* Average Readings
- Ambient

Software Version: 5.03.11

- 1 - 15.247(b) Power Output ( $902-928 \mathrm{MHz}$ FHSS $>50$ Channels)

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02871 | Spectrum Analyzer | E4440A | $2 / 24 / 2017$ | $2 / 24 / 2019$ |
| T2 | ANP06219 | Attenuator | $768-10$ | $4 / 12 / 2016$ | $4 / 12 / 2018$ |
| T3 | ANP06011 | Cable | Heliax | $10 / 25 / 2017$ | $10 / 25 / 2019$ |


| Measurement Data: |
| :--- |
| \# Freq <br> MHz Rdng <br> $\mathrm{dB} \mu \mathrm{V}$ T 1 <br> dB T 2 <br> dB T 3 <br> dB dB Dist <br> Table Corr <br> dBm Spec <br> dBm Margin <br> dB Polar <br> Ant <br> 1 903.004 M 19.3 +0.0 +9.1 +0.5  +0.0 28.9 30.0   <br> FM 37.5 K            |
| 2 |

### 15.35(c) Duty Cycle Correction Factor

| Test Data Summary |  |  |  |
| :---: | :---: | :---: | :---: |
| Antenna <br> Port | Operational Mode | Measured On Time <br> $(\mathrm{mS} /$ Pobs) | Calculated DCCF <br> (dB) |
| 1 | Longest Pulse Possible | 0.238 | -12.4 |

Observation Period, Pobs is the duration of the pulse train or maximum 100 mS
Measured results are calculated as follows:

$$
\text { On Time }=\left.\left(\sum_{\text {Bursts }} R F \text { Burst On Time }+\sum_{\text {Control }} \text { Control Signal On time }\right)\right|_{P_{o b s}(\max 100 \mathrm{~ms})}
$$

Measured Values:

| Parameter | Value |
| :--- | :--- |
| Observation Period (Pobs): | 100 |
| Number of RF Bursts / Pobs:: | 1 |
| On time of RF Burst: | 23.8 mS |
| Number of Control or other signals / Pobs: | 0 |
| On time of Control or other Signals: | 0 |
| Total Measured On Time: | 23.8 mS |

Duty Cycle Correction Factor (DCCF) is calculated in accordance with ANSI C63.10:

$$
D C C F=20 \cdot \log \left(\frac{\text { On Time }}{P_{\text {obs }}}\right)
$$

## Duty Cycle Correction Factor Test Data

DCCF is based on manufacturer measured worst case data, due to the firmware not being available to allow this measurement to be made at the test lab during time of test. See Appendix A, Customer Provided Information for manufacturer provided data.

Test Setup Photo(s)


### 15.247(d) RF Conducted Emissions \& Band Edge

| Test Setup/Conditions |  |  |  |  |
| :--- | :--- | :--- | :--- | :---: |
| Test Location: | Bothell Lab Bench | Test Engineer: | M. Atkinson |  |
| Test Method: | ANSI C63.10 (2013) | Test Date(s): | $11 / 27 / 17$ |  |
| Configuration: | 1 |  |  |  |
| Environmental Conditions    <br> Temperature (oC) 22 Relative Humidity (\%): 36 |  |  |  |  |

## See data sheets for test setup and test equipment.

## Test Setup / Conditions / Data

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

## Itron, Inc.

15.247(d) Conducted Spurious Emissions

100619
Conducted Emissions
Michael Atkinson
EMITest 5.03.11

Date: 11/27/2017
Time: 13:54:50
Sequence\#: 3
115 VAC 60 Hz

## Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Support Equipment:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Configuration 1 |  |  |  |

## Test Conditions / Notes:

Frequency Range:9kHz-9.28GHz
Frequency tested: $903,915,926.9 \mathrm{MHz}$
Firmware power setting: Max
Firmware: ARM 1.0.0.0 DSP 1.0.0.0, FPGA 4.1, Test Software: SrTest100 v4.1.1.25
Modulation: $12.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK), $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK)
Antenna type: External Monopole
Antenna Gain: 5.15 dBi or 5.5 dBi
Duty Cycle: Tested at $100 \%$
Setup: The EUT ISM port is continuously transmitting with modulation. The EUT ISM port is connected directly
to a spectrum analyzer for direct connected measurements.
Low, Mid, and High channels investigated. In addition to the Low/Mid/High investigation, spurious emissions also
investigated with EUT channel Hopping with modulation. All modulation types investigated, worst case reported.

Itron, Inc. WO\#t: 100619 Sequence\#: 3 Date: 11/27/2017 15.247 (d) Conducted Spurious Emissions Test Lead: 115 VAC 60 Hz RF Output


## Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :---: | :--- | :--- | :--- | :--- | :--- |
|  | AN02871 | Spectrum Analyzer | E4440A | $2 / 24 / 2017$ | $2 / 24 / 2019$ |
| T1 | ANP06219 | Attenuator | $768-10$ | $4 / 12 / 2016$ | $4 / 12 / 2018$ |
| T2 | ANP06011 | Cable | Heliax | $10 / 25 / 2017$ | $10 / 25 / 2019$ |



## Band Edge

## Band Edge Summary

Limit applied: Max Power/100kHz - 20dB.

| Frequency <br> $(\mathbf{M H z})$ | Modulation | Measured <br> $(\mathbf{d B m})$ | Limit <br> $(\mathbf{d B m})$ | Results |
| :---: | :---: | :---: | :---: | :---: |
| 902 | $12.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK) | -4.2 | $<8.9$ | Pass |
| 928 | $12.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK) | -8.9 | $<8.9$ | Pass |
| 902 | $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK) | -4.7 | $<8.9$ | Pass |
| 928 | $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK) | -9.2 | $<8.9$ | Pass |
| 902 | Hopping with modulation <br> $(12.5 \mathrm{Kbit} / \mathrm{sec}$ Modulations worst case) | -5.1 | $<8.9$ | Pass |
| 928 | Hopping with modulation <br> $(12.5$ Kbit/sec Modulations worst case) | -12.0 | $<8.9$ | Pass |

## Band Edge Plots




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## Test Setup / Conditions / Data

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

## Itron, Inc.

15.247(d) Conducted Spurious Emissions

100619
Conducted Emissions
Michael Atkinson
EMITest 5.03.11

Date: 11/27/2017
Time: 13:43:46
Sequence\#: 2
115 VAC 60 Hz

## Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Test Conditions / Notes:

| Frequency Range: Band Edge |
| :--- |
| Frequency tested: $903,926.9 \mathrm{MHz}$ |
| Firmware power setting: Max |
| Firmware: ARM 1.0.0.0 DSP 1.0.0.0, FPGA 4.1, Test Software: SrTest100 v4.1.1.25 |
| Modulation: $12.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK), $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK) |
| Antenna type: External Monopole |
| Antenna Gain: 5.15 dBi or 5.5 dBi |
| Duty Cycle: Tested at $100 \%$ |
| Setup: The EUT ISM port is continuously transmitting with modulation. The EUT ISM port is connected directly |
| to a spectrum analyzer for direct connected measurements. |
| Low, Mid, and High channels investigated. In addition to the Low/Mid/High investigation, spurious emissions also |
| investigated with EUT channel Hopping with modulation. All modulation types investigated, worst case reported. |

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02871 | Spectrum Analyzer | E4440A | $2 / 24 / 2017$ | $2 / 24 / 2019$ |
| T2 | ANP06219 | Attenuator | $768-10$ | $4 / 12 / 2016$ | $4 / 12 / 2018$ |
| T3 | ANP06011 | Cable | Heliax | $10 / 25 / 2017$ | $10 / 25 / 2019$ |

Measurement Data: Reading listed by margin. Test Lead: RF Output

| $\#$ | Freq <br> MHz | Rdng <br> $\mathrm{dB} \mu \mathrm{V}$ | T 1 <br> dB | T 2 <br> dB | T 3 <br> dB | dB | Dist <br> Table | Corr <br> dBm | Spec <br> dBm | Margin <br> dB | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 902.000 M | -13.8 | +0.0 | +9.1 | +0.5 |  | +0.0 | -4.2 | 8.9 <br> 12.5 k | -13.1 | RF Ou |
| 2 | 902.000 M | -14.3 | +0.0 | +9.1 | +0.5 | +0.0 | -4.7 | 8.9 <br> 37.5 k | -13.6 | RF Ou |  |
| 3 | 902.000 M | -14.7 | +0.0 | +9.1 | +0.5 | +0.0 | -5.1 | 8.9 <br> Hopping | -14.0 | RF Ou |  |
| 4 | 928.000 M | -18.6 | +0.0 | +9.2 | +0.5 | +0.0 | -8.9 | 8.9 | -17.8 | RF Ou |  |
| 5 | 928.000 M | -18.9 | +0.0 | +9.2 | +0.5 | +0.0 | -9.2 | 8.9 <br> 37.5 k | -18.1 | RF Ou |  |
| 6 | 928.000 M | -21.7 | +0.0 | +9.2 | +0.5 | +0.0 | -12.0 | 8.9 <br> Hopping | -20.9 | RF Ou |  |

## Test Setup Photo(s)



LABORATORIES, INE.

### 15.247(d) Radiated Emissions \& Band Edge

| Test Setup/Conditions |  |  |  |
| :--- | :--- | :--- | :--- |
| Test Location: | Bothell Lab C3 | Test Engineer: | M. Atkinson |
| Test Method: | ANSI C63.10 (2013) | Test Date(s): | $11 / 27 / 17$ to 11/29/17 |
| Configuration: | 1 |  |  |
| Environmental Conditions    <br> Temperature (으) $21-23$ Relative Humidity (\%):  |  |  |  |

## See data sheets for test setup and test equipment.

## Test Setup / Conditions / Data

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

## Itron, Inc.

15.247(d) / 15.209 Radiated Spurious Emissions

100619 Date: 11/28/2017
Maximized Emissions Time: 13:34:53
Michael Atkinson Sequence\#: 8
EMITest 5.03.11

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Test Conditions / Notes:

Frequency Range: $9 \mathrm{kHz}-9.28 \mathrm{GHz}$
Frequency tested: $903,915 \mathrm{MHz}, 926.9 \mathrm{MHz}$
Firmware power setting: Max
Firmware: ARM 1.0.0.0 DSP 1.0.0.0, FPGA 4.1, Test Software: SrTest100 v4.1.1.25
Modulation: 12.5 Kbit/sec FM (2GFSK), 37.5 Kbit/sec FM (2GFSK)
Antenna type: External Monopole
Antenna Gain: 5.15 dBi or 5.5 dBi
Duty Cycle: Tested at 100\%
Setup: The EUT ISM port is continuously transmitting with modulation. The EUT ISM port has an external antenna installed, both 5.15 and 5.5 dBi antennas investigated, only worst case reported.
Low, Mid, and High channels investigated. In addition to Low/Mid/High channel investigation, spurious emissions also investigated with EUT channel Hopping with modulation. All modulation types investigated, worst case reported. Both Horizontal and Vertical antenna polarities investigated above 30 MHz , only worst case reported. 3 orthogonal axes investigated below 30 MHz , only worst case reported.

All average data points marked Low, Mid, High have duty cycle correction applied ( $23.8 \%,-12.44 \mathrm{~dB}$ )

Itron, Inc. WO\#: 100619 Sequence\#: 8 Date: 11/28/2017 15.247(d) / 15.209 Radiated Spurious Emissions Test Distance: 3 Meters Various


[^0]O Peak Readings

* Average Readings
Software Version: 5.03.11

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :---: | :--- | :--- | :--- | :--- | :--- |
|  | AN02871 | Spectrum Analyzer | E4440A | $2 / 24 / 2017$ | $2 / 24 / 2019$ |
| T1 | ANP06540 | Cable | Heliax | $10 / 30 / 2017$ | $10 / 30 / 2019$ |
| T2 | ANP06515 | Cable | Heliax | $1 / 21 / 2016$ | $1 / 21 / 2018$ |
| T3 | AN03540 | Preamp | 83017 A | $5 / 2 / 2017$ | $5 / 2 / 2019$ |
| T4 | AN01467 | Horn Antenna- <br> ANSI C63.5 <br> Calibration | 3115 | $7 / 21 / 2017$ | $7 / 21 / 2019$ |
|  |  | Cable |  |  |  |
| T5 | ANP06934 |  | $32026-29801-$ | $3 / 11 / 2016$ | $3 / 11 / 2018$ |
| T6 | AN03170 | High Pass Filter | HM1155-11SS | $11 / 27 / 2017$ | $11 / 27 / 2019$ |
| T7 | ANDCCF | Test Data <br> Adjustment |  | $5 / 13 / 2016$ | $5 / 13 / 2018$ |
| T8 | ANP05963 | Cable | RG-214 | $2 / 15 / 2016$ | $2 / 15 / 2018$ |
| T9 | ANP05360 | Cable | RG214 | $11 / 30 / 2016$ | $11 / 30 / 2018$ |
| T10 | ANP06123 | Attenuator | $18 N-6$ | $5 / 5 / 2017$ | $5 / 5 / 2019$ |
| T11 | AN03628 | Biconilog Antenna | 3142 E | $6 / 7 / 2017$ | $6 / 7 / 2019$ |
| T12 | AN00052 | Loop Antenna | 6502 | $4 / 8 / 2016$ | $4 / 8 / 2018$ |


| Measurement Data: | Reading listed by margin. |  |  |  | Test Distance: 3 Meters |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FreqMHz | Rdng | T1 | T2 | T3 | T4 | Dist | Corr | Spec | Margin | Polar |
|  |  | T5 | T6 | T7 | T8 |  |  |  |  |  |
|  |  | T9 | T10 | T11 | T12 |  |  |  |  |  |
|  | $\mathrm{dB} \mu \mathrm{V}$ | dB | dB | dB | dB | Table | $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$ | $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$ | dB | Ant |
| $1 \quad 37.547 \mathrm{M}$ | 18.4 | +0.1 | +0.0 | +0.0 | +0.0 | +0.0 | 37.0 | 40.0 | -3.0 | Vert |
| QP |  | +0.0 | +0.0 | +0.0 | +0.5 |  |  |  |  |  |
|  |  | +0.3 | +5.9 | +11.8 | +0.0 |  |  |  |  |  |
| $2 \quad 37.619 \mathrm{M}$ | 17.5 | +0.1 | +0.0 | +0.0 | +0.0 | +0.0 | 36.0 | 40.0 | -4.0 | Vert |
| QP |  | +0.0 | +0.0 | +0.0 | +0.5 |  |  |  |  |  |
|  |  | +0.3 | +5.9 | +11.7 | +0.0 |  |  |  |  |  |
| $\wedge 37.547 \mathrm{M}$ | 20.9 | +0.1 | +0.0 | +0.0 | +0.0 | +0.0 | 39.5 | 40.0 | -0.5 | Vert |
|  |  | +0.0 | +0.0 | +0.0 | +0.5 |  |  |  |  |  |
|  |  | +0.3 | +5.9 | +11.8 | +0.0 |  |  |  |  |  |
| $\wedge 37.619 \mathrm{M}$ | 20.5 | +0.1 | +0.0 | +0.0 | +0.0 | +0.0 | 39.0 | 40.0 | -1.0 | Vert |
|  |  | +0.0 | +0.0 | +0.0 | +0.5 |  |  |  |  |  |
|  |  | +0.3 | +5.9 | +11.7 | +0.0 |  |  |  |  |  |
| $\begin{aligned} & 5 \text { 4515.027M } \\ & \text { Ave } \end{aligned}$ | 56.8 | +0.5 | +3.8 | -33.1 | +31.9 | +0.0 | 48.8 | 54.0 | -5.2 | Horiz |
|  |  | +0.5 | +0.8 | -12.4 | +0.0 |  | Low |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| $\wedge 4515.027 \mathrm{M}$ | 58.8 | +0.5 | +3.8 | -33.1 | +31.9 | +0.0 | 50.8 | 54.0 | -3.2 | Horiz |
|  |  | +0.5 | +0.8 | -12.4 | +0.0 |  | Low |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |


| $\begin{aligned} & 75417.965 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 52.4 | $\begin{aligned} & \hline+0.6 \\ & +0.5 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +4.3 \\ & +1.0 \\ & +0.0 \end{aligned}$ | $\begin{gathered} \hline-33.1 \\ -12.4 \\ +0.0 \end{gathered}$ | $\begin{array}{r} \hline+33.9 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 47.2 | $\begin{aligned} & 54.0 \\ & \text { Low } \end{aligned}$ | -6.8 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge 5417.965 \mathrm{M}$ | 54.1 | $\begin{aligned} & +0.6 \\ & +0.5 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+4.3 \\ & +1.0 \\ & +0.0 \end{aligned}$ | $\begin{gathered} -33.1 \\ -12.4 \\ +0.0 \end{gathered}$ | $\begin{array}{r} \hline+33.9 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 |  | $\begin{aligned} & 54.0 \\ & \text { Low } \end{aligned}$ | -5.1 | Horiz |
| $\begin{aligned} & 9 \text { 4634.480M } \\ & \text { Ave } \end{aligned}$ | 53.0 | $\begin{aligned} & +0.5 \\ & +0.5 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +3.9 \\ & +0.8 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{gathered} -33.2 \\ -12.4 \\ +0.0 \\ \hline \end{gathered}$ | $\begin{array}{r} \hline+32.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $+0.0$ | 45.2 | $\begin{aligned} & 54.0 \\ & \text { High } \end{aligned}$ | -8.8 | Horiz |
| $\wedge ~ 4634.480 \mathrm{M}$ | 55.8 | $\begin{aligned} & +0.5 \\ & +0.5 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +3.9 \\ & +0.8 \\ & +0.0 \end{aligned}$ | $\begin{gathered} -33.2 \\ -12.4 \\ +0.0 \end{gathered}$ | $\begin{array}{r} \hline+32.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.0 |  | $\begin{aligned} & 54.0 \\ & \text { High } \end{aligned}$ | -6.0 | Horiz |
| $\begin{aligned} & 11 \quad 1007.000 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 33.5 | $\begin{aligned} & \hline+0.4 \\ & +0.3 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +1.7 \\ +22.2 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} -36.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+23.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.0 | 45.1 | 54.0 | -8.9 | Horiz |
| $\begin{aligned} & 12 \text { 4574.900M } \\ & \text { Ave } \end{aligned}$ | 52.8 | $\begin{aligned} & +0.5 \\ & +0.5 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +3.8 \\ & +0.8 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{gathered} -33.1 \\ -12.4 \\ +0.0 \end{gathered}$ | $\begin{array}{r} \hline+32.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.0 |  | $\begin{aligned} & \text { 54.0 } \\ & \text { Mid } \end{aligned}$ | -9.1 | Horiz |
| $\wedge 4574.900 \mathrm{M}$ | 56.1 | $\begin{aligned} & +0.5 \\ & +0.5 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +3.8 \\ & +0.8 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} -33.1 \\ -12.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+32.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.0 | 48.2 | $\begin{aligned} & \text { } 54.0 \\ & \text { Mid } \end{aligned}$ | -5.8 | Horiz |
| $\begin{aligned} & 14 \quad 995.440 \mathrm{M} \\ & \mathrm{QP} \end{aligned}$ | 8.8 | $\begin{aligned} & \hline+0.4 \\ & +0.0 \\ & +2.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +5.9 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +24.4 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +2.5 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 44.3 | 54.0 | -9.7 | Vert |
| ^ 995.440M | 12.4 | $\begin{aligned} & +0.4 \\ & +0.0 \\ & +2.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +5.9 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +24.4 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +2.5 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 47.9 | 54.0 | -6.1 | Vert |
| $\begin{aligned} & 162708.999 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 56.6 | $\begin{aligned} & +0.5 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.8 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline-33.8 \\ -12.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+28.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $+0.0$ |  | $\begin{aligned} & 54.0 \\ & \text { Low } \end{aligned}$ | -10.6 | Vert |
| ^ 2708.999M | 57.4 | $\begin{aligned} & +0.5 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.8 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline-33.8 \\ -12.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+28.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $+0.0$ |  | $\begin{aligned} & 54.0 \\ & \text { Low } \end{aligned}$ | -9.8 | Vert |
| $\begin{aligned} & 182709.027 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 55.3 | $\begin{aligned} & \hline+0.5 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.8 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline-33.8 \\ -12.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+28.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.0 |  | $\begin{aligned} & 54.0 \\ & \text { Low } \end{aligned}$ | -11.9 | Horiz |
| $\wedge 2709.010 \mathrm{M}$ | 57.3 | $\begin{aligned} & +0.5 \\ & +0.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.8 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline-33.8 \\ -12.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+28.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.0 |  | $\begin{aligned} & 54.0 \\ & \text { Low } \end{aligned}$ | -9.9 | Horiz |
| $20 \quad 7320.120 \mathrm{M}$ | 43.2 | $\begin{aligned} & +0.9 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +5.3 \\ & +0.5 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline-34.1 \\ -12.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+36.5 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $+0.0$ |  | $\begin{aligned} & \text { } 54.0 \\ & \text { Mid } \end{aligned}$ | -13.5 | Horiz |
| 21 1128.000M | 47.9 | $\begin{aligned} & \hline+0.4 \\ & +0.3 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +1.8 \\ & +1.9 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} -36.2 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{array}{r} \hline+24.3 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 40.4 | 54.0 | -13.6 | Horiz |

Page 37 of 66

| $\begin{aligned} & 223707.600 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 49.4 | +0.4 | +3.4 | -33.4 | +30.9 | +0.0 | 39.7 | 54.0 | -14.3 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | +0.5 | +0.9 | -12.4 | +0.0 | High |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| ^ 3707.600M | 49.2 | +0.4 | +3.4 | -33.4 | +30.9 | $+0.0$ | 39.5 | $\begin{aligned} & 54.0 \\ & \text { High } \end{aligned}$ | -14.5 | Horiz |
|  |  | +0.5 | +0.9 | -12.4 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 24 1482.000M | 43.6 | +0.4 | +2.0 | -35.0 | +25.5 | +0.0 | 37.6 | 54.0 | -16.4 | Horiz |
|  |  | +0.3 | +0.8 | +0.0 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 25 1168.000M | 45.1 | +0.4 | +1.8 | -36.0 | +24.5 | +0.0 | 37.4 | 54.0 | -16.6 | Horiz |
|  |  | +0.3 | +1.3 | +0.0 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 26 2745.060M | 50.2 | +0.5 | +2.8 | -33.8 | +28.8 | +0.0 | 37.1 | $\text { Mid }^{54.0}$ | -16.9 | Vert |
|  |  | +0.4 | +0.6 | -12.4 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| $\begin{aligned} & 27 \text { 3660.000M } \\ & \text { Ave } \end{aligned}$ | 46.1 | +0.4 | +3.4 | -33.4 | +30.8 | +0.0 | 36.3 | $\text { Mid }^{54.0}$ | -17.7 | Horiz |
|  |  | +0.5 | +0.9 | -12.4 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| ^ 3659.920M | 48.0 | +0.4 | +3.4 | -33.4 | +30.8 | +0.0 | 38.2 | $\text { Mid }^{54.0}$ | -15.8 | Horiz |
|  |  | +0.5 | +0.9 | -12.4 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| $\begin{aligned} & 29 \text { 2745.040M } \\ & \text { Ave } \end{aligned}$ | 48.8 | +0.5 | +2.8 | -33.8 | +28.8 | +0.0 | 35.7 | $\begin{aligned} & \text { 54.0 } \\ & \text { Mid } \end{aligned}$ | -18.3 | Horiz |
|  |  | +0.4 | +0.6 | -12.4 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| ^ 2745.040M | 51.9 | +0.5 | +2.8 | -33.8 | +28.8 | +0.0 | 38.8 | $\text { Mid }^{54.0}$ | -15.2 | Horiz |
|  |  | +0.4 | +0.6 | -12.4 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| $\begin{aligned} & 31 \quad 2744.953 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 48.0 | +0.5 | +2.8 | -33.8 | +28.8 | +0.0 | 34.9 | $\text { Mid }{ }^{54.0}$ | -19.1 | Vert |
|  |  | +0.4 | +0.6 | -12.4 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| $\begin{aligned} & 323612.000 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 43.7 | +0.4 | +3.3 | -33.5 | +30.7 | +0.0 | 33.4 | $\begin{gathered} 54.0 \\ \text { Low } \end{gathered}$ | -20.6 | Horiz |
|  |  | +0.4 | +0.8 | -12.4 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| ^ 3612.000M | 46.8 | +0.4 | +3.3 | -33.5 | +30.7 | $+0.0$ | 36.5 | $\begin{gathered} 54.0 \\ \text { Low } \end{gathered}$ | -17.5 | Horiz |
|  |  | +0.4 | +0.8 | -12.4 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| $\begin{aligned} & 34 \text { 7320.000M } \\ & \text { Ave } \end{aligned}$ | 35.3 | +0.9 | +5.3 | -34.1 | +36.5 | +0.0 | 32.6 | $\begin{aligned} & \text { Mid } \\ & \text { Mid } \end{aligned}$ | -21.4 | Horiz |
|  |  | +0.6 | +0.5 | -12.4 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| $\begin{aligned} & 35 \text { 2780.700M } \\ & \text { Ave } \end{aligned}$ | 45.2 | +0.5 | +2.8 | -33.8 | +28.9 | +0.0 | 32.2 | $\begin{gathered} 54.0 \\ \text { High } \end{gathered}$ | -21.8 | Vert |
|  |  | +0.4 | +0.6 | -12.4 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| ^ 2780.740M | 47.3 | +0.5 | +2.8 | -33.8 | +28.9 | +0.0 | 34.3 | $\begin{gathered} 54.0 \\ \text { High } \end{gathered}$ | -19.7 | Vert |
|  |  | +0.4 | +0.6 | -12.4 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| $\begin{aligned} & 37 \text { 7415.200M } \\ & \text { Ave } \end{aligned}$ | 34.5 | +1.1 | +5.4 | -34.4 | +36.8 | +0.0 | 32.1 | $\begin{gathered} 54.0 \\ \text { High } \end{gathered}$ | -21.9 | Horiz |
|  |  | +0.6 | +0.5 | -12.4 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| ^ 7415.200M | 40.4 | +1.1 | +5.4 | -34.4 | +36.8 | +0.0 | 38.0 | 54.0 | -16.0 | Horiz |
|  |  | +0.6 | +0.5 | -12.4 | +0.0 |  |  | High |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |



Page 39 of 66

| 56 | 756.400 M | 14.2 | $\begin{aligned} & \hline+0.3 \\ & +0.0 \\ & +1.8 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +5.9 \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +22.5 \end{array}$ | $\begin{aligned} & +0.0 \\ & +2.2 \\ & +0.0 \end{aligned}$ | +0.0 | 46.9 | 111.5 | -64.6 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 57 | 5490.000M | 50.9 | $\begin{aligned} & +0.7 \\ & +0.5 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+4.3 \\ & +0.9 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline-33.1 \\ -12.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +34.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.0 | 46.0 | $\begin{aligned} & 111.5 \\ & \text { Mid } \end{aligned}$ | -65.5 | Horiz |
| 58 | 5561.320 M | 50.5 | $\begin{aligned} & +0.7 \\ & +0.5 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+4.3 \\ & +0.7 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline-33.2 \\ -12.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +34.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.0 | 45.4 | $\begin{aligned} & 111.5 \\ & \text { High } \end{aligned}$ | -66.1 | Horiz |
| 59 | 569.400 M | 14.4 | $\begin{aligned} & \hline+0.3 \\ & +0.0 \\ & +1.6 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +5.9 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +19.8 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +2.0 \\ & +0.0 \end{aligned}$ | +0.0 | 44.0 | 111.5 | -67.5 | Horiz |
| 60 | 6405.040M | 46.1 | $\begin{aligned} & +0.6 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +4.8 \\ & +0.5 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline-33.6 \\ -12.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+35.4 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.0 | 42.0 | $\begin{aligned} & 111.5 \\ & \text { Mid } \end{aligned}$ | -69.5 | Horiz |
| 61 | 414.500M | 14.7 | $\begin{aligned} & \hline+0.2 \\ & +0.0 \\ & +1.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +5.9 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +17.9 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +1.8 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 41.8 | 111.5 | -69.7 | Horiz |
| 62 | 6321.120M | 45.2 | $\begin{aligned} & +0.6 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+4.8 \\ & +0.5 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} -33.5 \\ -12.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +35.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.0 | 41.1 | $\begin{aligned} & 111.5 \\ & \text { Low } \end{aligned}$ | -70.4 | Horiz |
| 63 | 38.820M | 23.2 | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +5.9 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +11.1 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.5 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 41.1 | 111.5 | -70.4 | Vert |
| 64 | 7224.040M | 43.6 | $\begin{aligned} & \hline+0.8 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +5.3 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} -33.9 \\ -12.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +36.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $+0.0$ | 40.8 | $\begin{aligned} & 111.5 \\ & \text { Low } \end{aligned}$ | -70.7 | Horiz |
| 65 | 2128.000 M | 42.3 | $\begin{aligned} & \hline+0.4 \\ & +0.3 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.5 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} -34.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +28.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $+0.0$ | 40.1 | 111.5 | -71.4 | Vert |
| 66 | 44.800 M | 24.5 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +5.9 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +8.2 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.5 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | 39.6 | 111.5 | -71.9 | Vert |
| 67 | 9269.040M | 38.7 | $\begin{aligned} & +0.9 \\ & +0.7 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +5.7 \\ & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline-33.8 \\ -12.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +37.3 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.0 |  | $\begin{aligned} & 111.5 \\ & \text { High } \end{aligned}$ | -73.8 | Horiz |
| 68 | 57.000M | 22.0 | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +5.9 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +6.6 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.6 \\ & +0.0 \end{aligned}$ | +0.0 | 35.6 | 111.5 | -75.9 | Horiz |
| 69 | 105.700M | 17.6 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +5.9 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +8.2 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +1.2 \\ & +0.0 \end{aligned}$ | +0.0 | 33.6 | 111.5 | -77.9 | Vert |
| 70 | 144.000M | 17.1 | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +5.9 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +8.2 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +1.3 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | 33.4 | 111.5 | -78.1 | Vert |
| 71 | 1853.840M | 47.5 | $\begin{aligned} & \hline+0.4 \\ & +0.3 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+2.3 \\ & +0.7 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline-34.5 \\ -12.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+26.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.0 |  | $\begin{aligned} & 111.5 \\ & \text { High } \end{aligned}$ | -80.4 | Horiz |
| 72 | 1830.040M | 46.0 | $\begin{aligned} & +0.4 \\ & +0.3 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+2.3 \\ & +0.7 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline-34.5 \\ -12.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+26.6 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $+0.0$ | 29.4 | $\begin{aligned} & 111.5 \\ & \text { Mid } \end{aligned}$ | -82.1 | Horiz |

Page 40 of 66


| 73 | 1806.130M | 45.7 | $\begin{aligned} & +0.5 \\ & +0.3 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+2.2 \\ & +0.7 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline-34.5 \\ -12.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +26.4 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | +0.0 | 28.9 | $\begin{aligned} & 111.5 \\ & \text { ow } \end{aligned}$ | -82.6 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 74 | 552.070 k | 15.8 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +9.8 \end{aligned}$ | -40.0 | -14.4 | 111.5 | -125.9 | Perp |
| 75 | 19.328 M | 15.6 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +8.3 \\ & \hline \end{aligned}$ | -40.0 | -16.1 | 111.5 | -127.6 | Perp |
| 76 | 19.821 M | 14.9 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +8.3 \\ & \hline \end{aligned}$ | -40.0 | -16.8 | 111.5 | -128.3 | Perp |
| 77 | 19.803 M | 14.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +8.3 \\ & \hline \end{aligned}$ | -40.0 | -17.5 | 111.5 | -129.0 | Para |
| 78 | 3.068M | 12.9 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +9.5 \\ & \hline \end{aligned}$ | -40.0 | -17.6 | 111.5 | -129.1 | Para |
| 79 | 19.792M | 13.8 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +8.3 \\ & \hline \end{aligned}$ | -40.0 | -17.9 | 111.5 | -129.4 | Perp |
| 80 | 32.196k | 32.2 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +12.0 \\ \hline \end{array}$ | -80.0 | -35.8 | 111.5 | -147.3 | Para |
| 81 | 83.513 k | 22.0 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +10.1 \\ \hline \end{array}$ | -80.0 | -47.9 | 111.5 | -159.4 | Perp |
| 82 | 29.113 k | 18.9 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +12.3 \end{array}$ | -80.0 | -48.8 | 111.5 | -160.3 | Para |

LABORATORIES, INC.

## Band Edge

| Band Edge Summary |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Frequency (MHz) | Modulation | Ant. Type | Field Strength (dBuV/m @3m) | Limit (dBuV/m@3m) | Results |
| 614 (QP) | $12.5 \mathrm{Kbit} / \mathrm{sec}$ FM <br> (2GFSK) | External Monopole, 5.15 dBi Max | 39.5 | < 46.0 | Pass |
| 902 | $12.5 \mathrm{Kbit} / \mathrm{sec}$ FM <br> (2GFSK) | External Monopole, 5.15 dBi Max | 98.6 | < 111.5 | Pass |
| 928 | $\begin{gathered} 12.5 \mathrm{Kbit} / \mathrm{sec} \mathrm{FM} \\ \text { (2GFSK) } \end{gathered}$ | External Monopole, 5.15dBi Max | 94.0 | < 111.5 | Pass |
| 960 (QP) | $\begin{aligned} & 12.5 \mathrm{Kbit} / \mathrm{sec} \mathrm{FM} \\ & \text { (2GFSK) } \end{aligned}$ | External Monopole, 5.15 dBi Max | 47.4 | < 54.0 | Pass |
| 614 (QP) | $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM <br> (2GFSK) | External Monopole, 5.15 dBi Max | 39.5 | < 46.0 | Pass |
| 902 | $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM <br> (2GFSK) | External Monopole, 5.15 dBi Max | 97.5 | < 111.5 | Pass |
| 928 | $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM <br> (2GFSK) | External Monopole, 5.15 dBi Max | 93.8 | < 111.5 | Pass |
| 960 (QP) | 37.5 Kbit/sec FM <br> (2GFSK) | External Monopole, 5.15dBi Max | 47.0 | < 54.0 | Pass |
| 614 (QP) | Hopping with modulation (12.5 Kbit/sec <br> Modulations worst case) | External Monopole, 5.15 dBi Max | 39.4 | < 46.0 | Pass |
| 902 | Hopping with modulation (12.5 Kbit/sec <br> Modulations worst case) | External Monopole, 5.15dBi Max | 97.8 | < 111.5 | Pass |
| 928 | Hopping with modulation (12.5 Kbit/sec <br> Modulations worst case) | External Monopole, 5.15dBi Max | 93.0 | < 111.5 | Pass |
| 960 (QP) | Hopping with modulation (12.5 Kbit/sec <br> Modulations worst case) | External Monopole, 5.15 dBi Max | 46.4 | < 54.0 | Pass |

## Band Edge Plots














LABORATORIES, INC.

## Test Setup / Conditions / Data

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)
Customer:
Specification:
Itron, Inc.
15.247(d) / 15.209 Radiated Spurious Emissions

Work Order \#:
Test Type:
Tested By:
100619
Date: 11/28/2017
Maximized Emissions
Time: 06:38:33

Software:
Michael Atkinson
Sequence\#: 4
EMITest 5.03.11

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Test Conditions / Notes:

Frequency Range: Band Edge
Frequency tested: $903,926.9 \mathrm{MHz}$
Firmware power setting: Max
Firmware: ARM 1.0.0.0 DSP 1.0.0.0, FPGA 4.1, Test Software: SrTest100 v4.1.1.25
Modulation: $12.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK), 37.5 Kbit/sec FM (2GFSK)

Antenna type: External Monopole
Antenna Gain: 5.15 dBi or 5.5 dBi
Duty Cycle: Tested at $100 \%$
Setup: The EUT ISM port is continuously transmitting with modulation. The EUT ISM port has an external antenna installed, both 5.15 and 5.5 d Bi antennas investigated, only worst case reported.
Low, Mid, and High channels investigated. In addition to Low/Mid/High channel investigation, spurious emissions also investigated with EUT channel Hopping with modulation. All modulation types investigated, worst case reported. Both Horizontal and Vertical antenna polarities investigated above 30 MHz , only worst case reported. 3 orthogonal axes investigated below 30 MHz , only worst case reported.

All average data points marked Low, Mid, High have duty cycle correction applied (23.8\%, -12.44 dB )

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02871 | Spectrum Analyzer | E4440A | $2 / 24 / 2017$ | $2 / 24 / 2019$ |
| T2 | ANP06540 | Cable | Heliax | $10 / 30 / 2017$ | $10 / 30 / 2019$ |
| T3 | ANP05963 | Cable | RG-214 | $2 / 15 / 2016$ | $2 / 15 / 2018$ |
| T4 | ANP05360 | Cable | RG214 | $11 / 30 / 2016$ | $11 / 30 / 2018$ |
| T5 | ANP06123 | Attenuator | 18N-6 | $5 / 5 / 2017$ | $5 / 5 / 2019$ |
| T6 | AN03628 | Biconilog Antenna | 3142E | $6 / 7 / 2017$ | $6 / 7 / 2019$ |



## Test Setup Photos)



Below 1GHz, 5.5 dBi


Below 1GHz, 5.15 dBi


Above 1GHz, $5.5 \mathrm{dBi}(150 \mathrm{~cm})$, Cone Placement


Above $1 \mathrm{GHz}, 5.15 \mathrm{dBi}(150 \mathrm{~cm})$, Cone Placement

LABORATORIES, INE.

### 15.207 AC Conducted Emissions

| Test Setup/Conditions |  |  |  |
| :--- | :--- | :--- | :--- |
| Test Location: | Bothell Lab C3 | Test Engineer: | M. Atkinson |
| Test Method: | ANSI C63.10 (2013) | Test Date(s): | $11 / 29 / 2017$ |
| Configuration: | 1 |  |  |
| Environmental Conditions    <br> Temperature (oC) 22 Relative Humidity (\%): 33 |  |  |  |

## See data sheets for test setup and test equipment.

## Test Setup / Conditions / Data

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Itron, Inc.
15.207 AC Mains - Average

100619 Date: 11/29/2017
Conducted Emissions
Michael Atkinson
EMITest 5.03.11

Time: 10:50:25
Sequence\#: 20
115 VAC 60 Hz

## Equipment Tested:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Configuration 1 |  |  |  |

## Support Equipment:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Configuration 1 |  |  |  |

## Test Conditions / Notes:

Frequency Range: $150 \mathrm{kHz}-30 \mathrm{MHz}$
Frequency tested: $903,915,926.9 \mathrm{MHz}$
Firmware power setting: Max
Firmware: ARM 1.0.0.0 DSP 1.0.0.0, FPGA 4.1, Test Software: SrTest100 v4.1.1.25
Modulation: $12.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK), $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK)
Antenna type: External Monopole
Antenna Gain: 5.15 dBi or 5.5 dBi
Duty Cycle: Tested at $100 \%$

| Setup: The EUT connected to AC mains through LISN. EUT ISM port is continuously transmitting with |
| :--- |
| modulation. The EUT ISM port is connected directly to a spectrum analyzer for direct connected measurements. |
| Low, Mid, and High channels investigated, as well as Hopping with modulation, all modulation types investigated, |
| worst case reported. |

Itron, Inc. WO\#: 100619 Sequence\#: 20 Date: 11/29/2017
15.207 AC Mains - Average Test Lead: 115 VAC 60 Hz Line


[^1]Readings

* Average Readings
1-15.207 AC Mains - Average

0 Peak Readings

- Ambient

2-15.207 AC Mains - Quasi-peak

Test Equipment:
\(\left.\begin{array}{|llllll|}\hline ID \& Asset \# \& Description \& Model \& Calibration Date \& Cal Due Date <br>

T1 \& AN02871 \& Spectrum Analyzer \& E4440A \& 2 / 24 / 2017 \& 2 / 24 / 2019\end{array}\right]\)| T2 | AN02611 | High Pass Filter | HE9615-150K- <br> $50-720 B$ | $2 / 18 / 2016$ |
| :--- | :--- | :--- | :--- | :--- |

Measurement Data: Reading listed by margin. Test Lead: Line

| \# |  | Freq MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \text { T1 } \\ & \text { T5 } \\ & \text { dB } \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~T} 6 \\ & \mathrm{~dB} \end{aligned}$ | T3 dB | T4 dB | Dist Table | Corr <br> dBuV | Spec <br> $\mathrm{dB} \mu \mathrm{V}$ | Margin dB | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 4.968M | 27.4 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 36.8 | 46.0 | -9.2 | Line |
| Ave |  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ |  | 4.968M | 36.3 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 45.7 | 46.0 | -0.3 | Line |
|  |  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 3 |  | 153.700k | 35.5 | +0.0 | +0.7 | +0.0 | +0.0 | +0.0 | 45.4 | 55.8 | -10.4 | Line |
|  |  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 4 |  | 5.220 M | 29.5 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 38.9 | 50.0 | -11.1 | Line |
|  |  | Ave |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
|  | $\wedge$ | 5.220 M | 38.9 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 48.3 | 50.0 | -1.7 | Line |
|  |  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
|  | 6 | 5.252M | 28.8 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 38.2 | 50.0 | -11.8 | Line |
| Ave |  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
|  | $\wedge$ | 5.252 M | 35.9 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 45.3 | 50.0 | -4.7 | Line |
|  |  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
|  | 8 | 3.800M | 23.2 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 32.6 | 46.0 | -13.4 | Line |
| Ave |  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
|  | $\wedge$ | 3.800 M | 42.4 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 51.8 | 46.0 | +5.8 | Line |
|  |  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
|  | 10 | 3.369M | 22.8 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 32.2 | 46.0 | -13.8 | Line |
| Ave |  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ |  | 3.369 M | 41.0 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 50.4 | 46.0 | +4.4 | Line |
|  |  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 12 |  | 16.400 M | 26.2 | +0.0 | +0.1 | +0.0 | +0.3 | +0.0 | 35.8 | 50.0 | -14.2 | Line |
|  |  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
|  | 13 | 4.595 M | 22.1 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 31.5 | 46.0 | -14.5 | Line |
| Ave |  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
|  | $\wedge$ | 4.595 M | 42.4 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 51.8 | 46.0 | +5.8 | Line |
|  |  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
|  | 15 | 4.240M | 21.9 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 31.3 | 46.0 | -14.7 | Line |
| Ave |  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ |  | 4.240M | 41.6 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 51.0 | 46.0 | +5.0 | Line |
|  |  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
|  | 17 | 2.456 M | 21.8 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 31.2 | 46.0 | -14.8 | Line |
| Ave |  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |

Page 55 of 66

| $\wedge$ | 2.456 M | 38.5 | $\begin{aligned} & +0.0 \\ & +9.1 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.1 \end{aligned}$ | +0.0 | +0.1 | +0.0 | 47.9 | 46.0 | +1.9 | Line |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 19 | 3.556M | 21.4 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 30.8 | 46.0 | -15.2 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 3.556 M | 41.0 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 50.4 | 46.0 | +4.4 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 21 | 3.255 M | 21.4 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 30.8 | 46.0 | -15.2 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 3.255 M | 41.7 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 51.1 | 46.0 | +5.1 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 23 | 4.218M | 20.9 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 30.3 | 46.0 | -15.7 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 4.218 M | 41.4 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 50.8 | 46.0 | +4.8 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 25 | 3.994M | 19.3 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 28.7 | 46.0 | -17.3 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 3.994M | 41.1 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 50.5 | 46.0 | +4.5 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 27 | 2.858 M | 19.2 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 28.6 | 46.0 | -17.4 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 2.858 M | 42.8 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 52.2 | 46.0 | +6.2 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 29 | 3.676 M | 19.2 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 28.6 | 46.0 | -17.4 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 3.676 M | 42.1 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 51.5 | 46.0 | +5.5 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 31 | 3.702M | 19.1 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 28.5 | 46.0 | -17.5 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 3.702 M | 41.3 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 50.7 | 46.0 | +4.7 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 33 | 2.702 M | 19.0 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 28.4 | 46.0 | -17.6 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 2.702 M | 42.9 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 52.3 | 46.0 | +6.3 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 35 | 4.301 M | 18.7 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 28.1 | 46.0 | -17.9 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 4.301 M | 40.8 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 50.2 | 46.0 | +4.2 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 37 | 2.992M | 18.6 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 28.0 | 46.0 | -18.0 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 2.992M | 40.0 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 49.4 | 46.0 | +3.4 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 39 | 3.335M | 18.6 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 28.0 | 46.0 | -18.0 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 3.335 M | 40.6 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 50.0 | 46.0 | +4.0 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 41 | 3.347M | 18.6 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 28.0 | 46.0 | -18.0 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 3.347 M | 41.2 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 50.6 | 46.0 | +4.6 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 43 | 4.109M | 18.6 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 28.0 | 46.0 | -18.0 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |

Page 56 of 66

| $\wedge$ | 4.109M | 40.9 | $\begin{aligned} & +0.0 \\ & +9.1 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.1 \end{aligned}$ | +0.0 | +0.1 | +0.0 | 50.3 | 46.0 | +4.3 | Line |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 45 | 3.951 M | 18.3 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 27.7 | 46.0 | -18.3 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 3.951 M | 41.4 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 50.8 | 46.0 | +4.8 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 47 | 3.308M | 18.2 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 27.6 | 46.0 | -18.4 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 3.308M | 40.7 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 50.1 | 46.0 | +4.1 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 49 | 3.008M | 17.8 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 27.2 | 46.0 | -18.8 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 3.008 M | 42.1 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 51.5 | 46.0 | +5.5 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 51 | 2.328 M | 17.3 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 26.7 | 46.0 | -19.3 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 2.328 M | 35.7 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 45.1 | 46.0 | -0.9 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 53 | 3.486M | 17.0 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 26.4 | 46.0 | -19.6 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 3.486M | 43.9 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 53.3 | 46.0 | +7.3 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 55 | 4.077 M | 16.8 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 26.2 | 46.0 | -19.8 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 4.077 M | 41.3 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 50.7 | 46.0 | +4.7 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 57 | 3.128 M | 16.1 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 25.5 | 46.0 | -20.5 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 3.128 M | 42.4 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 51.8 | 46.0 | +5.8 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)
Customer: Itron, Inc.
Specification: $\quad \mathbf{1 5 . 2 0 7}$ AC Mains - Average
Work Order \#: 100619
Test Type: Conducted Emissions
Tested By: Michael Atkinson
Software:
EMITest 5.03.11

Date: 11/29/2017
Time: 10:01:40
Sequence\#: 19
115 VAC 60 Hz

## Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Frequency Range: $150 \mathrm{kHz}-30 \mathrm{MHz}$
Frequency tested: 903, 915, 926.9MHz
Firmware power setting: Max
Firmware: ARM 1.0.0.0 DSP 1.0.0.0, FPGA 4.1, Test Software: SrTest100 v4.1.1.25
Modulation: 12.5 Kbit/sec FM (2GFSK), 37.5 Kbit/sec FM (2GFSK)
Antenna type: External Monopole
Antenna Gain: 5.15 dBi or 5.5 dBi
Duty Cycle: Tested at 100\%
Setup: The EUT connected to AC mains through LISN. EUT ISM port is continuously transmitting with modulation. The EUT ISM port is connected directly to a spectrum analyzer for direct connected measurements. Low, Mid, and High channels investigated, as well as Hopping with modulation, all modulation types investigated, worst case reported.

Itron, Inc. WO\#: 100619 Sequence\#: 19 Date: 11/29/2017
15.207 AC Mains - Average Test Lead: 115 VAC 60 Hz Return



Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | AN02871 | Spectrum Analyzer | E4440A | 2/24/2017 | 2/24/2019 |
| T1 | AN02611 | High Pass Filter | $\begin{aligned} & \text { HE9615-150K- } \\ & \text { 50-720B } \end{aligned}$ | 2/18/2016 | 2/18/2018 |
| T2 | ANP06540 | Cable | Heliax | 10/30/2017 | 10/30/2019 |
| T3 | ANP06515 | Cable | Heliax | 1/21/2016 | 1/21/2018 |
| T4 | ANP06219 | Attenuator | 768-10 | 4/12/2016 | 4/12/2018 |
| T5 | AN01311 | 50uH LISN-Line1 (N) | 3816/2 | 3/7/2016 | 3/7/2018 |
|  | AN01311 | 50uH LISN-Line2 <br> (L) | 3816/2 | 3/7/2016 | 3/7/2018 |

Measurement Data: $\quad$ Reading listed by margin. $\quad$ Test Lead: Return

| \# | Freq <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \hline \text { T1 } \\ & \text { T5 } \\ & \text { dB } \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{array}{r} \mathrm{T} 3 \\ \mathrm{~dB} \\ \hline \end{array}$ | T4 <br> dB | Dist <br> Table | Corr <br> $\mathrm{dB} \mu \mathrm{V}$ | Spec <br> $\mathrm{dB} \mu \mathrm{V}$ | Margin <br> dB | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 181.400k | 34.1 | $\begin{aligned} & +0.3 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +9.1 | +0.0 | 43.5 | 54.4 | -10.9 | Retur |
|  | $\mathrm{ve}^{3.936 \mathrm{M}}$ | 24.9 | $\begin{array}{r} +0.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.1 | +9.1 | +0.0 | 34.2 | 46.0 | -11.8 | Retur |
| $\wedge$ | 3.936M | 41.4 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 50.7 | 46.0 | +4.7 | Retur |
|  | $2.931 \mathrm{M}$ | 24.1 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 33.4 | 46.0 | -12.6 | Retur |
| $\wedge$ | 2.931 M | 41.4 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 50.7 | 46.0 | +4.7 | Retur |
|  | $3.674 \mathrm{M}$ <br> ve | 23.9 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 33.2 | 46.0 | -12.8 | Retur |
| $\wedge$ | 3.674 M | 42.1 | $\begin{array}{r} +0.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.1 | +9.1 | +0.0 | 51.4 | 46.0 | +5.4 | Retur |
|  | $3.747 \mathrm{M}$ <br> ve | 23.9 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 33.2 | 46.0 | -12.8 | Retur |
| $\wedge$ | 3.747 M | 43.2 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 52.5 | 46.0 | +6.5 | Retur |
|  | $2.762 \mathrm{M}$ <br> ve | 23.6 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 32.9 | 46.0 | -13.1 | Retur |
| $\wedge$ | 2.762 M | 41.5 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 50.8 | 46.0 | +4.8 | Retur |
|  | $3.080 \mathrm{M}$ <br> ve | 23.2 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 32.5 | 46.0 | -13.5 | Retur |
| $\wedge$ | 3.080M | 42.2 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 51.5 | 46.0 | +5.5 | Retur |
|  | $2.716 \mathrm{M}$ <br> ve | 23.2 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | $+0.0$ | +0.1 | +9.1 | +0.0 | 32.5 | 46.0 | -13.5 | Retur |
| $\wedge$ | 2.716 M | 42.8 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 52.1 | 46.0 | +6.1 | Retur |
|  | $3.855 \mathrm{M}$ <br> ve | 23.1 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 32.4 | 46.0 | -13.6 | Retur |
| $\wedge$ | 3.855 M | 41.9 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 51.2 | 46.0 | +5.2 | Retur |

Page 60 of 66

|  | $\begin{aligned} & 2.600 \mathrm{M} \\ & \hline \end{aligned}$ | 22.7 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 32.0 | 46.0 | -14.0 | Retur |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 2.600 M | 41.8 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 51.1 | 46.0 | +5.1 | Retur |
| 20 | $2.472 \mathrm{M}$ <br> e | 22.5 | $\begin{aligned} & +0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 31.8 | 46.0 | -14.2 | Retur |
| $\wedge$ | 2.472 M | 39.7 | $\begin{aligned} & +0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 49.0 | 46.0 | +3.0 | Retur |
|  | $\begin{aligned} & 2.748 \mathrm{M} \\ & \hline \text { ve } \\ & \hline \end{aligned}$ | 22.5 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 31.8 | 46.0 | -14.2 | Retur |
| 23 | 15.700M | 26.2 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.3 | +9.1 | $+0.0$ | 35.7 | 50.0 | -14.3 | Retur |
|  | 3.888M <br> e | 22.2 | $\begin{aligned} & +0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 31.5 | 46.0 | -14.5 | Retur |
| $\wedge$ | 3.888 M | 42.4 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 51.7 | 46.0 | +5.7 | Retur |
|  | $\begin{aligned} & \text { 4.004M } \\ & \hline \end{aligned}$ | 22.1 | $\begin{array}{r} +0.1 \\ +0.0 \\ \hline \end{array}$ | $+0.0$ | +0.1 | +9.1 | $+0.0$ | 31.4 | 46.0 | -14.6 | Retur |
| $\wedge$ | 4.004 M | 40.6 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 49.9 | 46.0 | +3.9 | Retur |
|  | $3.386 \mathrm{M}$ | 21.7 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 31.0 | 46.0 | -15.0 | Retur |
| $\wedge$ | 3.386M | 41.2 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 50.5 | 46.0 | +4.5 | Retur |
|  | $3.014 \mathrm{M}$ <br> e | 21.4 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 30.7 | 46.0 | -15.3 | Retur |
| $\wedge$ | 3.014 M | 43.1 | $\begin{aligned} & +0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 52.4 | 46.0 | +6.4 | Retur |
|  | $2.639 \mathrm{M}$ | 21.2 | $\begin{aligned} & +0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 30.5 | 46.0 | -15.5 | Retur |
| $\wedge$ | 2.639 M | 42.1 | $\begin{array}{r} +0.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | $+0.1$ | +9.1 | $+0.0$ | 51.4 | 46.0 | +5.4 | Retur |
|  | $3.359 \mathrm{M}$ | 21.0 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 30.3 | 46.0 | -15.7 | Retur |
| $\wedge$ | 3.359 M | 41.5 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 50.8 | 46.0 | +4.8 | Retur |
|  | $3.371 \mathrm{M}$ | 20.9 | $\begin{array}{r} +0.1 \\ +0.0 \\ \hline \end{array}$ | $+0.0$ | +0.1 | +9.1 | $+0.0$ | 30.2 | 46.0 | -15.8 | Retur |
| $\wedge$ | 3.371 M | 41.4 | $\begin{aligned} & +0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | $+0.1$ | +9.1 | +0.0 | 50.7 | 46.0 | +4.7 | Retur |
|  | $4.460 \mathrm{M}$ | 20.5 | $\begin{aligned} & +0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 29.8 | 46.0 | -16.2 | Retur |
| $\wedge$ | 4.460M | 36.7 | $\begin{array}{r} +0.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.1 | +9.1 | +0.0 | 46.0 | 46.0 | +0.0 | Retur |
|  | $3.788 \mathrm{M}$ <br> e | 20.5 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 29.8 | 46.0 | -16.2 | Retur |
| $\wedge$ | 3.788 M | 42.3 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 51.6 | 46.0 | +5.6 | Retur |
|  | $3.052 \mathrm{M}$ | 20.5 | $\begin{array}{r} +0.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 29.8 | 46.0 | -16.2 | Retur |
| $\wedge$ | 3.052 M | 41.3 | $\begin{aligned} & +0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 50.6 | 46.0 | +4.6 | Retur |

Page 61 of 66

| 44 | $2.739 \mathrm{M}$ | 20.2 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | $+0.0$ | +0.1 | +9.1 | +0.0 | 29.5 | 46.0 | -16.5 | Retur |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 2.739 M | 42.4 | $\begin{aligned} & +0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 51.7 | 46.0 | +5.7 | Retur |
| $\wedge$ | 2.748 M | 41.7 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 51.0 | 46.0 | +5.0 | Retur |
|  | $2.889 \mathrm{M}$ | 19.5 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 28.8 | 46.0 | -17.2 | Retur |
| $\wedge$ | 2.889 M | 41.9 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 51.2 | 46.0 | +5.2 | Retur |
|  | $2.308 \mathrm{M}$ | 18.8 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 28.1 | 46.0 | -17.9 | Retur |
| $\wedge$ | 2.308 M | 36.7 | $\begin{aligned} & +0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 46.0 | 46.0 | +0.0 | Retur |
|  | $4.288 \mathrm{M}$ <br> ve | 18.3 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 27.6 | 46.0 | -18.4 | Retur |
| $\wedge$ | 4.288M | 38.5 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 47.8 | 46.0 | +1.8 | Retur |
|  | $3.325 \mathrm{M}$ | 17.3 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | $+0.0$ | +0.1 | +9.1 | +0.0 | 26.6 | 46.0 | -19.4 | Retur |
| $\wedge$ | 3.325 M | 41.7 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 51.0 | 46.0 | +5.0 | Retur |
| 55 | $\begin{aligned} & \text { 5.076M } \\ & \mathrm{ve}^{2} \\ & \hline \end{aligned}$ | 15.0 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | +0.1 | +9.1 | +0.0 | 24.3 | 50.0 | -25.7 | Retur |
| $\wedge$ | 5.076M | 37.1 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 46.4 | 50.0 | -3.6 | Retur |
| 57 | $159.800 \mathrm{k}$ <br> ve | 5.2 | $\begin{aligned} & +0.6 \\ & +0.0 \end{aligned}$ | +0.0 | +0.0 | +9.1 | +0.0 | 14.9 | 55.5 | -40.6 | Retur |
| $\wedge$ | 159.800k | 38.1 | $\begin{aligned} & +0.6 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +9.1 | +0.0 | 47.8 | 55.5 | -7.7 | Retur |

## Test Setup Photo(s)



LABORATORIES, INC.

## APPENDIX A: CUSTOMER PROVIDED INFORMATION

Manufacturer's Declaration: 15.247(a)(1)(i) Average Time of Occupancy

The manufacturer declares:
Each transmission is a maximum of 23.8 mS long. Each transmission takes place on one 120 different channels in a pseudorandom sequence. All 120 channels are used equally on the average. The algorithm that determines the pseudo-random hop sequence does not allow the device to transmit on the same channel more than 6 times in a 20 second period. The maximum possible occupancy time on any one frequency is 142.8 mS ( 6 times) within a 20 second period.

## DCCF Plot Data



DCCF Plot

## SUPPLEMENTAL INFORMATION

## Measurement Uncertainty

| Uncertainty Value | Parameter |
| :---: | :---: |
| 4.73 dB | Radiated Emissions |
| 3.34 dB | Mains Conducted Emissions |
| 3.30 dB | Disturbance Power |

Uncertainties reported are worst case for all CKC Laboratories' sites and represent expanded uncertainties expressed at approximately the $95 \%$ confidence level using a coverage factor of $\mathrm{k}=2$. Compliance is deemed to occur provided measurements are below the specified limits.

## Emissions Test Details

## TESTING PARAMETERS

Unless otherwise indicated, the following configuration parameters are used for equipment setup: The cables were routed consistent with the typical application by varying the configuration of the test sample. Interface cables were connected to the available ports of the test unit. The effect of varying the position of the cables was investigated to find the configuration that produced maximum emissions. Cables were of the type and length specified in the individual requirements. The length of cable that produced maximum emissions was selected.

The equipment under test (EUT) was set up in a manner that represented its normal use, as shown in the setup photographs. Any special conditions required for the EUT to operate normally are identified in the comments that accompany the emissions tables.

The emissions data was taken with a spectrum analyzer or receiver. Incorporating the applicable correction factors for distance, antenna, cable loss and amplifier gain, the data was reduced as shown in the table below. The corrected data was then compared to the applicable emission limits. Preliminary and final measurements were taken in order to ensure that all emissions from the EUT were found and maximized.

## CORRECTION FACTORS

The basic spectrum analyzer reading was converted using correction factors as shown in the highest emissions readings in the tables. For radiated emissions in $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$, the spectrum analyzer reading in $\mathrm{dB} \mu \mathrm{V}$ was corrected by using the following formula. This reading was then compared to the applicable specification limit. Individual measurements were compared with the displayed limit value in the margin column. The margin was calculated based on subtracting the limit value from the corrected measurement value; a positive margin represents a measurement exceeding the limit, while a negative margin represents a measurement less than the limit.

| SAMPLE CALCULATIONS |  |  |  |
| :--- | :--- | :--- | :---: |
|  | Meter reading | $(\mathrm{dB} \mu \mathrm{V})$ |  |
| + | Antenna Factor | $(\mathrm{dB} / \mathrm{m})$ |  |
| + | Cable Loss | $(\mathrm{dB})$ |  |
| - | Distance Correction | $(\mathrm{dB})$ |  |
| - | Preamplifier Gain | $(\mathrm{dB})$ |  |
| $=$ | Corrected Reading | $(\mathrm{dB} \mu \mathrm{V} / \mathrm{m})$ |  |

## TEST INSTRUMENTATION AND ANALYZER SETTINGS

The test instrumentation and equipment listed were used to collect the emissions data. A spectrum analyzer or receiver was used for all measurements. Unless otherwise specified, the following table shows the measuring equipment bandwidth settings that were used in designated frequency bands. For testing emissions, an appropriate reference level and a vertical scale size of 10 dB per division were used.

| MEASURING EQUIPMENT BANDWIDTH SETTINGS PER FREQUENCY RANGE |  |  |  |
| :---: | :---: | :---: | :---: |
| TEST | BEGINNING FREQUENCY | ENDING FREQUENCY | BANDWIDTH SETTING |
| CONDUCTED EMISSIONS | 150 kHz | 30 MHz | 9 kHz |
| RADIATED EMISSIONS | 9 kHz | 150 kHz | 200 Hz |
| RADIATED EMISSIONS | 150 kHz | 30 MHz | 9 kHz |
| RADIATED EMISSIONS | 30 MHz | 1000 MHz | 120 kHz |
| RADIATED EMISSIONS | 1000 MHz | $>1 \mathrm{GHz}$ | 1 MHz |

## SPECTRUM ANALYZER/RECEIVER DETECTOR FUNCTIONS

The notes that accompany the measurements contained in the emissions tables indicate the type of detector function used to obtain the given readings. Unless otherwise noted, all readings were made in the "positive peak" detector mode. Whenever a "quasi-peak" or "average" reading was recorded, the measurement was annotated with a "QP" or an "Ave" on the appropriate rows of the data sheets. In cases where quasi-peak or average limits were employed and data exists for multiple measurement types for the same frequency then the peak measurement was retained in the report for reference, however the numbering for the affected row was removed and an arrow or caret (" $\wedge$ ") was placed in the far left-hand column indicating that the row above takes precedence for comparison to the limit. The following paragraphs describe in more detail the detector functions and when they were used to obtain the emissions data.

## Peak

In this mode, the spectrum analyzer or receiver recorded all emissions at their peak value as the frequency band selected was scanned. By combining this function with another feature called "peak hold," the measurement device had the ability to measure intermittent or low duty cycle transient emission peak levels. In this mode the measuring device made a slow scan across the frequency band selected and measured the peak emission value found at each frequency across the band.

## Quasi-Peak

Quasi-peak measurements were taken using the quasi-peak detector when the true peak values exceeded or were within 2 dB of a quasi-peak specification limit. Additional QP measurements may have been taken at the discretion of the operator.

## Average

Average measurements were taken using the average detector when the true peak values exceeded or were within 2 dB of an average specification limit. Additional average measurements may have been taken at the discretion of the operator. If the specification or test procedure requires trace averaging, then the averaging was performed using 100 samples or as required by the specification. All other average measurements are performed using video bandwidth averaging. To make these measurements, the test engineer reduces the video bandwidth on the measuring device until the modulation of the signal is filtered out. At this point the measuring device is set into the linear mode and the scan time is reduced.


[^0]:    - Readings
    $\times$ QP Readings
    - Ambient

    1-15.247(d) / 15.209 Radiated Spurious Emissions

[^1]:    weep Data
    $\times$ QP Readings
    Software Version: 5.03.11

