## Itron, Inc.

TEST REPORT FOR
CCU100
Model: CCU100TD

Tested to The Following Standards:

FCC Part 15 Subpart C Section(s)
15.207 \& 15.247
(FHSS 902-928MHz)

Report No.: 107462-2

Date of issue: December 5, 2022


This test report bears the accreditation symbol indicating that the testing performed herein meets the test and reporting requirements of ISO/IEC 17025 under the applicable scope of testing for CKC Laboratories, Inc.

We strive to create long-term, trust based relationships by providing sound, adaptive, customer first testing services. We embrace each of our customers' unique EMC challenges, not as an interruption to set processes, but rather as the reason we are in business.

Test Certificate \# 803.01

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# ADMINISTRATIVE INFORMATION 

## Test Report Information

## REPORT PREPARED FOR:

Itron, Inc.
2111 N. Molter Road
Liberty Lake, WA 99019

Representative: Jack McPeck
Customer Reference Number: 266646

DATE OF EQUIPMENT RECEIPT:
DATES) OF TESTING:

REPORT PREPARED BY:

Viviana Prado
CKC Laboratories, Inc.
5046 Sierra Pines Drive
Mariposa, CA 95338

Project Number: 107462

October 26, 2022
October 26-31 and November 1, 2022

## Report Authorization

The test data contained in this report documents the observed testing parameters pertaining to and are relevant for only the equipment provided by the client, tested in the agreed upon operational modes) and configuration (s) as identified herein. Compliance assessment remains the client's responsibility. This report may not be used to claim product endorsement by A2LA or any government agencies. This test report has been authorized for release under quality control from CKC Laboratories, Inc.


Steve Behm
Director of Quality Assurance \& Engineering Services CKC Laboratories, Inc.

## Test Facility Information



Our laboratories are configured to effectively test a wide variety of product types. CKC utilizes first class test equipment, anechoic chambers, data acquisition and information services to create accurate, repeatable and affordable test results.

TEST LOCATION(S):
CKC Laboratories, Inc.
Canyon Park
22116 23rd Drive S.E., Suite A
Bothell, WA 98021

## Software Versions

| CKC Laboratories Proprietary Software | Version |
| :--- | :---: |
| EMITest Emissions | 5.03 .20 |

## Site Registration \& Accreditation Information

| Location | *NIST CB \# | FCC | Canada | Japan |
| :---: | :---: | :---: | :---: | :---: |
| Canyon Park, Bothell, WA | US0103 | US1024 | 3082 C | A-0136 |
| Brea, CA | US0103 | US1024 | 3082 D | A-0136 |
| Fremont, CA | US0103 | US1024 | 3082 B | A-0136 |
| Mariposa, CA | US0103 | US1024 | 3082 A | A-0136 |

*CKC's list of NIST designated countries can be found at: https://standards.gov/cabs/designations.html

TVesting the Future

## SUMMARY OF RESULTS

Standard / Specification: FCC Part 15 Subpart C-15.247 (FHSS 902-928MHz)

| Test Procedure | Description | Modifications | Results |
| :--- | :--- | :--- | :--- |
| $15.247(\mathrm{a})(1)(\mathrm{i})$ | Occupied Bandwidth | NA | Pass |
| $15.247(\mathrm{a})(1)$ | Carrier Separation | NA | Pass |
| $15.247(\mathrm{a})(1)(\mathrm{i})$ | Number of Hopping Channels | NA | Pass |
| $15.247(\mathrm{a})(1)(\mathrm{i})$ | Average Time of Occupancy | NA | NP |
| $15.247(\mathrm{~b})(2)$ | Output Power | NA | Pass |
| $15.247(\mathrm{~d})$ | RF Conducted Emissions \& Band Edge | NA | Pass |
| $15.247(\mathrm{~d})$ | Radiated Emissions \& Band Edge | NA | Pass |
| 15.207 | AC Conducted Emissions | NA | Pass |

NA = Not Applicable
NP = CKC Laboratories Inc. was not contracted to preform test.

## ISO/IEC 17025 Decision Rule

The declaration of pass or fail herein is based upon assessment to the specification(s) listed above, including where applicable, assessment of measurement uncertainties. For performance related tests, equipment was monitored for specified criteria identified in that section of testing.

## Modifications During Testing

This list is a summary of the modifications made to the equipment during testing.

## Summary of Conditions

No modifications were made during testing.

Modifications listed above must be incorporated into all production units.

## Conditions During Testing

This list is a summary of the conditions noted to the equipment during testing.

## Summary of Conditions

DSP Power was set to 255 for all tests except Fundamental and Conducted Spurs/Conducted Band Edge, where it was reduced to 200 at time of test to fine tune the power of the unit for Fundamental compliance. The higher power used for other testing is representative of worst-case. This is a test software setting and the manufacturer performs a calibration of each production unit with its appropriate software.

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## EQUIPMENT UNDER TEST (EUT)

During testing, numerous configurations may have been utilized. The configurations listed below support compliance to the standard(s) listed in the Summary of Results section.

Configuration 1 (Tower) = Remote SuperRaptor, Remote GPS, Remote Cellular
Equipment Tested:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| CCU100 | Itron, Inc. | CCU100TD | 74049603 |

Support Equipment:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Laptop | Dell | Latitude E6430 | NA |
| Switch | Netgear | FS105 | NA |
| Antenna (remote ISM) | PCTEL | BOA9028 | NA |
| 1dB Attenuator (Qty: 2) | Mini-Circuits | 15542 UNAT-1+ | NA |
| Surge Protector | Times Microwave Systems | LP-BTRW-NMP | NA |
| Antenna (remote WAN) | Taoglas | OMB.6912.03F21 | NA |
| Antenna (remote GPS) | Trimble | $101898-00$ | NA |

## General Product Information:

| Product Information | Manufacturer-Provided Details |
| :---: | :---: |
| Equipment Type: | Stand-Alone Equipment |
| Type of Wideband System: | FHSS |
| Operating Frequency Range: | $903-926.8 \mathrm{MHz}$ |
| Number of Hopping Channels: | 80 channels (AM), 120 channels (FM) |
| Receiver Bandwidth and Synchronization: | The manufacturer declares the receiver input bandwidth matches the transmit channel bandwidth and shifts frequencies in synchronization with the transmitter. |
| Modulation Type(s): | $16 \mathrm{kbit} / \mathrm{sec}$ AM (OOK) <br> $12.5 \mathrm{kbit} / \mathrm{sec}$ FM (FSK) <br> 37.5 kbit/sec FM (FSK) |
| Maximum Duty Cycle: | Tested at 100\% |
| Number of TX Chains: | 1 |
| Antenna Type(s) and Gain: | Omni-Directional / 8.15 dBi |
| Beamforming Type: | NA |
| Antenna Connection Type: | External Connector |
| Nominal Input Voltage: | $115 \mathrm{VAC} / 60 \mathrm{~Hz}$ |
| Firmware / Software used for Test: | ```ARM FW 2.27.0.0 DSP FW 7.22.0.0 FPGA FW 4.14 SRTest100 4.11.1.99 TeraTerm 4.62``` |
| The validity of results is dependent on the stated product details, the accuracy of which the manufacturer assumes full responsibility. |  |

## EUT Photo(s)



Support Equipment Photos)


Laptop and Switch


Remote ISM Antenna


Remote WAN and GPS antennas

Block Diagram of Test Setup(s)

Test Setup Block Diagram


## FCC Part 15 Subpart C

### 15.247(a) Transmitter Characteristics

| Test Setup/Conditions |  |  |  |
| :--- | :--- | :--- | :--- |
| Test Location: | Bothell Lab Bench | Test Engineer: | M. Harrison/M. Atkinson |
| Test Method: | ANSI C63.10 (2013) | Test Date(s): | $10 / 27 / 2022$ to 10/31/2022 |
| Configuration: | 1 | EUT is setup for conducted measurements. It is directly connected to the Signal Analyzer <br> via an Attenuator and a Cable. <br> Test Setup: <br>  <br>  <br> For the AM channel plan, normal AM modulation is used. <br> For the FM channel plan, a test mode with CW modulation was used. |  |


| Environmental Conditions |  |  |  |
| :---: | :---: | :---: | :---: |
| Temperature (으) | $22-24$ | Relative Humidity (\%): | $43-50$ |


| Test Equipment |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Asset\# | Description | Manufacturer | Model | Cal Date | Cal Due |  |
| 02872 | Spectrum Analyzer | Agilent | E4440A | $11 / 29 / 2021$ | $11 / 29 / 2023$ |  |
| P05503 | Attenuator | Narda | $766-10$ | $6 / 8 / 2021$ | $6 / 8 / 2023$ |  |
| P06008 | Cable | Andrew | Heliax | $9 / 2 / 2022$ | $9 / 2 / 2024$ |  |

### 15.247(a)(1)(i) $\mathbf{2 0 ~ d B ~ B a n d w i d t h ~}$

| Test Data Summary |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Frequency <br> $\mathbf{( M H z )}$ | Antenna <br> Port | Modulation | Measured <br> $\mathbf{( k H z )}$ | Limit <br> $\mathbf{( k H z )}$ | Results |  |
| 908.0 | 1 | AM | 182.5 | $\leq 500$ | Pass |  |
| 915.0 | 1 | AM | 198.7 | $\leq 500$ | Pass |  |
| 923.8 | 1 | AM | 170.5 | $\leq 500$ | Pass |  |
| 903.0 | 1 | FM 12.5k | 142.1 | $\leq 500$ | Pass |  |
| 915.0 | 1 | FM 12.5k | 142.7 | $\leq 500$ | Pass |  |
| 926.8 | 1 | FM 12.5k | 142.8 | $\leq 500$ | Pass |  |
| 903.0 | 1 | FM 37.5k | 84.4 | $\leq 500$ | Pass |  |
| 915.0 | 1 | FM 37.5k | 85.7 | $\leq 500$ | Pass |  |
| 926.8 | 1 | FM 37.5k | 86.4 | $\leq 500$ | Pass |  |

## Plot(s)

AM


Low Channel


Medium Channel


High Channel

## FM 12.5k



Low Channel


Medium Channel


High Channel

## FM 37.5k



Low Channel


Medium Channel


High Channel
15.247(a)(1) Carrier Separation

Test Data Summary

| Limit applied: 20dB bandwidth of the hopping channel. |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna <br> Port | Operational Mode | Measured <br> $\mathbf{( k H z )}$ | Limit <br> $(\mathbf{k H z})$ | Results |  |
| 1 | AM channel plan | 200.1 | $>198.7$ | Pass |  |
| 1 | FM channel plan | 200.1 | $>142.8$ | Pass |  |

## Plot(s)



AM Channel Plan


FM Channel Plan
15.247(a)(1)(i) Number of Channels

Test Data Summary
Limit $=\left\{\begin{array}{l}50 \text { Channels } \mid 20 \mathrm{~dB} B W<250 \mathrm{kHz} \\ 25 \text { Channels } \mid 20 \mathrm{~dB} B W \geq 250 \mathrm{kHz}\end{array}\right.$

| Antenna <br> Port | Operational Mode | Measured <br> (Channels) | Limit <br> (Channels) | Results |
| :---: | :---: | :---: | :---: | :---: |
| 1 | AM channel plan | 80 | $\geq 50$ | Pass |
| 1 | FM channel plan | 120 | $\geq 50$ | Pass |

## Plot(s)

## AM Number Channels



1 to 20



41 to 60


61 to 80

FM Number Channels


1 to 60


61 to 120

### 15.247(a) Transmitter Characteristics

Test Setup Photo(s)


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### 15.247(b)(2) Output Power

## Test Data Summary - Voltage Variations

| Frequency <br> $(\mathbf{M H z})$ | Modulation / Ant Port | $\mathbf{V}_{\text {Minimum }}$ <br> $(\mathbf{d B m})$ | $\mathbf{V}_{\text {Nominal }}$ <br> $(\mathbf{d B m})$ | $\mathbf{V}_{\text {Maximum }}$ <br> $(\mathbf{d B m})$ | Max Deviation <br> from $\mathbf{V}_{\text {Nominal }}(\mathbf{d B})$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 908.0 | AM | 29.8 | 29.8 | 29.8 | 0.0 |
| 903.0 | FM 12.5k | 29.5 | 29.5 | 29.5 | 0.0 |
| 903.0 | FM 37.5k | 29.4 | 29.4 | 29.4 | 0.0 |

Test performed using operational mode with the highest output power, representing worst-case.

## Parameter Definitions:

Measurements performed at input voltage Vnominal $\pm 15 \%$.

| Parameter | Value |
| :--- | :--- |
| V $_{\text {Nominal }}:$ | 115 |
| V $_{\text {Minimum }}:$ | 90 |
| $\mathrm{~V}_{\text {Maximum: }}$ | 265 |

Test Data Summary - RF Conducted Measurement
Limit $=\left\{\begin{array}{l}30 \mathrm{dBm} \text { Conducted } / 36 \mathrm{dBm} \text { EIRP } \mid \geq 50 \text { Channels } \\ 24 \mathrm{dBm} \text { Conducted } / 30 \mathrm{dBm} \text { EIRP } \mid<50 \text { Channels (min 25) }\end{array}\right.$

| Frequency (MHz) | Modulation | Ant. Type / Gain (dBi) | Measured (dBm) | Limit (dBm) | Results |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 908.0 | AM | Omni-Directional / $8.15 \mathrm{dBi}^{*}$ | 29.8 | $\leq 30$ | Pass |
| 915.0 | AM | Omni-Directional / 8.15dBi* | 29.6 | $\leq 30$ | Pass |
| 923.8 | AM | Omni-Directional / 8.15dBi* | 29.6 | $\leq 30$ | Pass |
| 903.0 | FM 12.5k | Omni-Directional / $8.15 \mathrm{dBi}^{*}$ | 29.5 | $\leq 30$ | Pass |
| 915.0 | FM 12.5k | Omni-Directional / 8.15dBi* | 29.3 | $\leq 30$ | Pass |
| 926.8 | FM 12.5k | Omni-Directional / 8.15dBi* | 29.3 | $\leq 30$ | Pass |
| 903.0 | FM 37.5k | Omni-Directional / 8.15dBi* | 29.4 | $\leq 30$ | Pass |
| 915.0 | FM 37.5k | Omni-Directional / 8.15dBi* | 29.2 | $\leq 30$ | Pass |
| 926.8 | FM 37.5k | Omni-Directional / $8.15 \mathrm{dBi}^{*}$ | 29.3 | $\leq 30$ | Pass |

* Net gain is 5.95 dBi . Manufacturer declares minimum of 2.2 dB of path loss to remote 8.15 dBi antenna.

Plots
AM


Low Channel


Medium Channel


High Channel

FM 12.5k


Low Channel


Medium Channel


High Channel

FM 37.5k


Low Channel


Medium Channel


High Channel

## Test Setup / Conditions / Data

Test Location:
Customer:
Specification Work Order \#:
Test Type:
Tested By:
Software:

CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A • Bothell, WA 98021•(425) 402-1717 Itron, Inc.
15.247(b) Power Output (902-928 MHz DTS)

107462
Conducted Emissions
Matt Harrison
EMITest 5.03.20

Date: 10/31/2022
Time: 12:33:17
Sequence\#: 1
120 VAC

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Test Conditions / Notes:

Test Environment Conditions:
Temperature: $21^{\circ} \mathrm{C}$
Humidity: $40 \%$
Pressure: 102.5 kPa

Frequency Range: Fundamental
Frequency Tested: 908, 915, 923.8
Firmware Power Setting: 200
Protocol /MCS/Modulation: AM
Antenna Type: Omni-Directional
Duty Cycle: Tested at 100\%
Test Method: ANSI C63.10 (2013)
Test Mode: Continuously Transmitting
Test Setup: EUT is setup for Conducted Measurements. It is directly connected to the SA via an Attenuator.

Itron, Inc. WO\#: 107462 Sequence\#: 1 Date: 10/31/2022 15.247 (b) Power Output ( $902-928 \mathrm{MHz}$ DTS) Test Lead: 120VAC Antenna Port

Sweep Data
Peak Readings
Average Readings
Software Version: 5.03 .20

## Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | ANP05503 | Attenuator | $766-10$ | $6 / 8 / 2021$ | $6 / 8 / 2023$ |
| T2 | AN02872 | Spectrum Analyzer | E4440A | $11 / 29 / 2021$ | $11 / 29 / 2023$ |
| T3 | ANP06008 | Cable | Heliax | $9 / 2 / 2022$ | $9 / 2 / 2024$ |


| Measu | ement Data: | Reading listed by margin. |  |  |  | Test Lead: Antenna Port |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | Freq <br> MHz | $\begin{aligned} & \mathrm{Rdng} \\ & \mathrm{~dB} \mu \mathrm{~V} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 3 \\ & \mathrm{~dB} \end{aligned}$ | dB | $\begin{gathered} \text { Dist } \\ \text { Table } \end{gathered}$ | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} \\ \hline \end{gathered}$ | Margin <br> dB | Polar <br> Ant |
| 1 | 907.955M | 126.1 | +10.1 | +0.0 | +0.6 |  | +0.0 | 136.8 | $\begin{aligned} & \quad 137.0 \\ & \text { DSP ISM } \\ & 200 \end{aligned}$ |  | Anten |
| 2 | 915.035M | 125.9 | +10.1 | +0.0 | +0.6 |  | +0.0 | 136.6 | 137.0 DSP ISM 200 | $-0.4$ <br> Power | Anten |
| 3 | 923.860M | 125.9 | +10.1 | +0.0 | +0.6 |  | +0.0 | 136.6 | 137.0 DSP ISM 200 |  | Anten |

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Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Test Location: $\quad$ CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A•Bothell, WA 98021•(425) 402-1717
Itron, Inc.
15.247(b) Power Output (902-928 MHz DTS)

107462 Date: 10/31/2022
Conducted Emissions
Matt Harrison
EMITest 5.03.20

Time: 15:40:48
Sequence\#: 2
120VAC

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Test Conditions / Notes:

Test Environment Conditions:
Temperature: $21^{\circ} \mathrm{C}$
Humidity: 40\%
Pressure: 102.5 kPa
Frequency Range: Fundamental
Frequency Tested: 903, 915, 926.8
Firmware Power Setting: 200
EUT Firmware:
Protocol/MCS/Modulation: FM 12.5k
Antenna Type: Omni-Directional

Duty Cycle: Tested at 100\%
Test Method: ANSI C63.10 (2013)
Test Mode: Continuously Transmitting
Test Setup: EUT is setup for Conducted Measurements. It is directly connected to the SA via an Attenuator.

Itron, Inc. WO\#: 107462 Sequence\#: 2 Date: 10/31/2022
15.247(b) Power Output ( $902-928 \mathrm{MHz}$ DTS) Test Lead: 120VAC Antenna Port


## Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | ANP05503 | Attenuator | $766-10$ | $6 / 8 / 2021$ | $6 / 8 / 2023$ |
|  | AN02872 | Spectrum Analyzer | E4440A | $11 / 29 / 2021$ | $11 / 29 / 2023$ |
| T2 | ANP06008 | Cable | Heliax | $9 / 2 / 2022$ | $9 / 2 / 2024$ |


| Measu | ement Data | Reading listed by margin. |  |  |  |  | Test Lead: Antenna Port |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | Freq <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | dB | dB | Dist Table | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} \end{gathered}$ | Margin dB | Polar <br> Ant |
| 1 | 903.015M | 125.8 | +10.1 | +0.6 |  |  | +0.0 | 136.5 | 137.0 | -0.5 | Anten |
| 2 | 914.930M | 125.6 | +10.1 | +0.6 |  |  | +0.0 | 136.3 | 137.0 | -0.7 | Anten |
| 3 | 926.815M | 125.6 | +10.1 | +0.6 |  |  | +0.0 | 136.3 | 137.0 | -0.7 | Anten |

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Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Test Location: $\quad$ CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A•Bothell, WA 98021•(425) 402-1717
Itron, Inc.
15.247(b) Power Output (902-928 MHz DTS)

107462 Date: 10/31/2022
Conducted Emissions
Matt Harrison
EMIT est 5.03.20

Time: 15:43:45
Sequence\#: 3
120VAC

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Test Environment Conditions:
Temperature: $21^{\circ} \mathrm{C}$
Humidity: $40 \%$
Pressure: 102.5 kPa
Frequency Range: Fundamental
Frequency Tested: 903, 915, 926.8
Firmware Power Setting: 200
EUT Firmware:
Protocol/MCS/Modulation: FM 37.5k
Antenna Type: Omni-Directional
Duty Cycle: Tested at 100\%
Test Method: ANSI C63.10 (2013)
Test Mode: Continuously Transmitting
Test Setup: EUT is setup for Conducted Measurements. It is directly connected to the SA via an Attenuator.

Itron, Inc. WO\#: 107462 Sequence\#: 3 Date: 10/31/2022
15.247 (b) Power Output ( $902-928 \mathrm{MHz}$ DTS) Test Lead: 120VAC Antenna Port


## Test Equipment:

| ID | Asset \#/Serial \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | ANP05503 | Attenuator | $766-10$ | $6 / 8 / 2021$ | $6 / 8 / 2023$ |
|  | AN02872 | Spectrum Analyzer | E4440A | $11 / 29 / 2021$ | $11 / 29 / 2023$ |
| T2 | ANP06008 | Cable | Heliax | $9 / 2 / 2022$ | $9 / 2 / 2024$ |


| Measu | ement Data | Reading listed by margin. |  |  |  |  | Test Lead: Antenna Port |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | Freq <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | dB | dB | Dist Table | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} \end{gathered}$ | Margin dB | Polar <br> Ant |
| 1 | 902.945M | 125.7 | +10.1 | +0.6 |  |  | +0.0 | 136.4 | 137.0 | -0.6 | Anten |
| 2 | 926.820M | 125.6 | +10.1 | +0.6 |  |  | +0.0 | 136.3 | 137.0 | -0.7 | Anten |
| 3 | 915.005M | 125.5 | +10.1 | +0.6 |  |  | +0.0 | 136.2 | 137.0 | -0.8 | Anten |

## Test Setup Photo(s)



### 15.247(d) RF Conducted Emissions \& Band Edge

## Test Setup / Conditions / Data

Test Location: $\quad$ CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A • Bothell, WA 98021•(425) 402-1717

Customer:
Specification: Work Order \#: Test Type: Tested By:
Software:

Itron, Inc.
15.247(d) Conducted Spurious Emissions 107462
Conducted Emissions
Michael Atkinson
EMITest 5.03.20

Date: 10/31/2022
Time: 16:45:26
Sequence\#: 1
120 V 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Test Conditions / Notes:

Test Environment Conditions:
Temperature: $21^{\circ} \mathrm{C}$
Humidity: $48 \%$
Pressure: 100.9 kPa

Test Method: ANSI C63.10 (2013)
Frequency: $9 \mathrm{kHz}-10 \mathrm{GHz}$
EUT is continuously transmitting with modulation, connected to spectrum analyzer directly through appropriate attenuation.

AM Modulation

Itron, Inc. WO\#: 107462 Sequence\#: 1 Date: 10/31/2022 15.247(d) Conducted Spurious Emissions Test Lead: 120 V 60 Hz Antenna Port


Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | ANP05503 | Attenuator | $766-10$ | $6 / 8 / 2021$ | $6 / 8 / 2023$ |
| T2 | ANP06008 | Cable | Heliax | $9 / 2 / 2022$ | $9 / 2 / 2024$ |
|  | AN02872 | Spectrum Analyzer | E4440A | $11 / 29 / 2021$ | $11 / 29 / 2023$ |


| Measurement Data: | Reading listed by margin. |  |  |  |  | Test Lead: Antenna Port |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# $\quad$Freq <br>  <br>  <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | dB | dB | Dist Table | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} \end{gathered}$ | $\begin{gathered} \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} \end{gathered}$ | $\begin{gathered} \text { Margin } \\ \mathrm{dB} \\ \hline \end{gathered}$ | Polar Ant |
| 1 1815.990M | 77.0 | +10.2 | +0.9 |  |  | +0.0 | 88.1 | 116.5 | -28.4 | Anten |
| 2 1830.003M | 76.8 | +10.2 | +0.9 |  |  | +0.0 | 87.9 | 116.5 | -28.6 | Anten |
| 3 1847.603M | 75.2 | +10.2 | +0.9 |  |  | +0.0 | 86.3 | 116.5 | -30.2 | Anten |
| 4 3695.205M | 72.6 | +10.3 | +1.3 |  |  | +0.0 | 84.2 | 116.5 | -32.3 | Anten |
| 53631.996 M | 72.4 | +10.3 | +1.3 |  |  | +0.0 | 84.0 | 116.5 | -32.5 | Anten |
| 63660.008 M | 72.4 | +10.3 | +1.3 |  |  | +0.0 | 84.0 | 116.5 | -32.5 | Anten |
| 7 2771.391M | 71.2 | +10.2 | +1.2 |  |  | +0.0 | 82.6 | 116.5 | -33.9 | Anten |
| 8 2723.971M | 71.1 | +10.2 | +1.2 |  |  | +0.0 | 82.5 | 116.5 | -34.0 | Anten |
| 9 6355.981M | 80.7 | +0.0 | +1.6 |  |  | +0.0 | 82.3 | 116.5 | -34.2 | Anten |
| $10 \quad 6404.990 \mathrm{M}$ | 80.5 | +0.0 | +1.6 |  |  | +0.0 | 82.1 | 116.5 | -34.4 | Anten |
| $11 \quad 5448.009 \mathrm{M}$ | 80.6 | +0.0 | +1.5 |  |  | +0.0 | 82.1 | 116.5 | -34.4 | Anten |
| 12 6466.596M | 80.3 | +0.0 | +1.6 |  |  | +0.0 | 81.9 | 116.5 | -34.6 | Anten |
| $13 \quad 5490.000 \mathrm{M}$ | 80.4 | +0.0 | +1.5 |  |  | +0.0 | 81.9 | 116.5 | -34.6 | Anten |
| 145542.790 M | 80.2 | +0.0 | +1.5 |  |  | +0.0 | 81.7 | 116.5 | -34.8 | Anten |
| 15 2744.999M | 70.3 | +10.2 | +1.2 |  |  | +0.0 | 81.7 | 116.5 | -34.8 | Anten |
| 16 4619.008M | 73.0 | +0.0 | +1.6 |  |  | +0.0 | 74.6 | 116.5 | -41.9 | Anten |
| 17 4575.001M | 71.7 | +0.0 | +1.6 |  |  | +0.0 | 73.3 | 116.5 | -43.2 | Anten |
| 18 4539.997M | 71.5 | +0.0 | +1.6 |  |  | +0.0 | 73.1 | 116.5 | -43.4 | Anten |
| 19 7390.377M | 68.7 | +0.0 | +1.6 |  |  | +0.0 | 70.3 | 116.5 | -46.2 | Anten |
| $20 \quad 7263.973 \mathrm{M}$ | 68.1 | +0.0 | +1.6 |  |  | +0.0 | 69.7 | 116.5 | -46.8 | Anten |
| $21 \quad 7320.000 \mathrm{M}$ | 68.0 | +0.0 | +1.6 |  |  | +0.0 | 69.6 | 116.5 | -46.9 | Anten |
| 22 8314.197M | 64.4 | +0.0 | +2.0 |  |  | +0.0 | 66.4 | 116.5 | -50.1 | Anten |
| $23 \quad 8234.952 \mathrm{M}$ | 63.5 | +0.0 | +1.9 |  |  | +0.0 | 65.4 | 116.5 | -51.1 | Anten |
| 24 8171.976M | 63.4 | +0.0 | +1.9 |  |  | +0.0 | 65.3 | 116.5 | -51.2 | Anten |

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Test Location: CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A•Bothell, WA 98021•(425) 402-1717
Itron, Inc.
15.247(d) Conducted Spurious Emissions

107462
Conducted Emissions
Michael Atkinson
EMIT est 5.03.20

Date: 10/31/2022
Time: 16:49:57
Sequence\#: 2
120 V 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Configuration 1 |  |  |  |
| Support Equipment: |  | Model \# | S/N |
| Device Manufacturer   <br> Configuration 1    $\mathbf{l}$ |  |  |  |

## Test Conditions / Notes:

Test Environment Conditions:
Temperature: $21^{\circ} \mathrm{C}$
Humidity: $48 \%$
Pressure: 100.9 kPa
Test Method: ANSI C63.10 (2013)
Frequency: 9kHz-10GHz
EUT is continuously transmitting with modulation, connected to spectrum analyzer directly through appropriate attenuation.

FM12.5 Modulation

Itron, Inc. WO\#: 107462 Sequence\#: 2 Date: 10/31/2022
15.247(d) Conducted Spurious Emissions Test Lead: 120 V 60 Hz Antenna Port


Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | ANP05503 | Attenuator | $766-10$ | $6 / 8 / 2021$ | $6 / 8 / 2023$ |
| T2 | ANP06008 | Cable | Heliax | $9 / 2 / 2022$ | $9 / 2 / 2024$ |
|  | AN02872 | Spectrum Analyzer | E4440A | $11 / 29 / 2021$ | $11 / 29 / 2023$ |


| Measurement Data: | Reading listed by margin. |  |  |  |  | Test Lead: Antenna Port |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# $\begin{aligned} & \text { Freq } \\ & \\ & \\ & \mathrm{MHz}\end{aligned}$ | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | dB | dB | Dist Table | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} \end{gathered}$ | Spec <br> $\mathrm{dB} \mu \mathrm{V}$ | $\begin{gathered} \text { Margin } \\ \mathrm{dB} \\ \hline \end{gathered}$ | Polar Ant |
| 1829.900 M | 76.6 | +10.2 | +0.9 |  |  | +0.0 | 87.7 | 116.5 | -28.8 | Anten |
| 2 1805.897M | 76.5 | +10.2 | +0.9 |  |  | +0.0 | 87.6 | 116.5 | -28.9 | Anten |
| 3 1853.700M | 75.4 | +10.2 | +0.9 |  |  | +0.0 | 86.5 | 116.5 | -30.0 | Anten |
| 4 3707.010M | 72.3 | +10.3 | +1.3 |  |  | +0.0 | 83.9 | 116.5 | -32.6 | Anten |
| 53660.190 M | 72.1 | +10.3 | +1.3 |  |  | +0.0 | 83.7 | 116.5 | -32.8 | Anten |
| 6 2780.546M | 71.7 | +10.2 | +1.2 |  |  | +0.0 | 83.1 | 116.5 | -33.4 | Anten |
| 7 6487.954M | 81.1 | +0.0 | +1.6 |  |  | +0.0 | 82.7 | 116.5 | -33.8 | Anten |
| 8 6320.664M | 81.0 | +0.0 | +1.6 |  |  | +0.0 | 82.6 | 116.5 | -33.9 | Anten |
| 95418.306 M | 81.0 | +0.0 | +1.5 |  |  | +0.0 | 82.5 | 116.5 | -34.0 | Anten |
| $10 \quad 5560.504 \mathrm{M}$ | 80.5 | +0.0 | +1.5 |  |  | +0.0 | 82.0 | 116.5 | -34.5 | Anten |
| 11 6404.648M | 80.2 | +0.0 | +1.6 |  |  | +0.0 | 81.8 | 116.5 | -34.7 | Anten |
| 12 2744.838M | 70.3 | +10.2 | +1.2 |  |  | +0.0 | 81.7 | 116.5 | -34.8 | Anten |
| 13 5490.290M | 80.2 | +0.0 | +1.5 |  |  | +0.0 | 81.7 | 116.5 | -34.8 | Anten |
| 14 2708.843M | 70.2 | +10.2 | +1.2 |  |  | +0.0 | 81.6 | 116.5 | -34.9 | Anten |
| $15 \quad 4634.250 \mathrm{M}$ | 73.6 | +0.0 | +1.5 |  |  | +0.0 | 75.1 | 116.5 | -41.4 | Anten |
| 16 4574.756M | 71.5 | +0.0 | +1.6 |  |  | +0.0 | 73.1 | 116.5 | -43.4 | Anten |
| 17 4515.260M | 70.8 | +0.0 | +1.6 |  |  | +0.0 | 72.4 | 116.5 | -44.1 | Anten |
| 18 7413.966M | 68.4 | +0.0 | +1.6 |  |  | +0.0 | 70.0 | 116.5 | -46.5 | Anten |
| 19 7319.602M | 67.6 | +0.0 | +1.6 |  |  | +0.0 | 69.2 | 116.5 | -47.3 | Anten |
| $20 \quad 7224.380 \mathrm{M}$ | 67.5 | +0.0 | +1.6 |  |  | +0.0 | 69.1 | 116.5 | -47.4 | Anten |
| 218341.658 M | 64.6 | +0.0 | +2.0 |  |  | +0.0 | 66.6 | 116.5 | -49.9 | Anten |
| 228127.445 M | 64.4 | +0.0 | +1.9 |  |  | +0.0 | 66.3 | 116.5 | -50.2 | Anten |
| 23 8235.494M | 63.1 | +0.0 | +1.9 |  |  | +0.0 | 65.0 | 116.5 | -51.5 | Anten |

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Test Location: CKC Laboratories, Inc. • 22116 23 rd Drive SE, Suite A•Bothell, WA 98021•(425) 402-1717
Itron, Inc.
15.247(d) Conducted Spurious Emissions

107462
Conducted Emissions
Michael Atkinson
EMIT est 5.03.20

Date: 10/31/2022
Time: 16:52:39
Sequence\#: 3
120 V 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Configuration 1 |  |  |  |
| Support Equipment: |  | Model \# | S/N |
| Device Manufacturer   <br> Configuration 1    $\mathbf{l}$ |  |  |  |

## Test Conditions / Notes:

Test Environment Conditions:
Temperature: $21^{\circ} \mathrm{C}$
Humidity: $48 \%$
Pressure: 100.9 kPa
Test Method: ANSI C63.10 (2013)
Frequency: 9kHz-10GHz
EUT is continuously transmitting with modulation, connected to spectrum analyzer directly through appropriate attenuation.

FM37.5 Modulation

Itron, Inc. WO\#: 107462 Sequence\#: 3 Date: 10/31/2022
15.247 (d) Conducted Spurious Emissions Test Lead: 120 V 60 Hz Antenna Port


Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | ANP05503 | Attenuator | $766-10$ | $6 / 8 / 2021$ | $6 / 8 / 2023$ |
| T2 | ANP06008 | Cable | Heliax | $9 / 2 / 2022$ | $9 / 2 / 2024$ |
|  | AN02872 | Spectrum Analyzer | E4440A | $11 / 29 / 2021$ | $11 / 29 / 2023$ |


| Measurement Data: | Reading listed by margin. |  |  |  |  | Test Lead: Antenna Port |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# $\begin{aligned} \text { Freq } \\ \text { MHz }\end{aligned}$ | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \text { dB } \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | dB | dB | $\begin{gathered} \hline \text { Dist } \\ \text { Table } \end{gathered}$ | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} \end{gathered}$ | $\begin{gathered} \hline \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} \end{gathered}$ | $\begin{gathered} \text { Margin } \\ \mathrm{dB} \end{gathered}$ | Polar <br> Ant |
| 1 1830.036M | 76.5 | +10.2 | +0.9 |  |  | +0.0 | 87.6 | 116.5 | -28.9 | Anten |
| 2 1806.028M | 76.4 | +10.2 | +0.9 |  |  | +0.0 | 87.5 | 116.5 | -29.0 | Anten |
| 31853.558 M | 75.4 | +10.2 | +0.9 |  |  | +0.0 | 86.5 | 116.5 | -30.0 | Anten |
| 4 3612.078M | 72.9 | +10.3 | +1.3 |  |  | +0.0 | 84.5 | 116.5 | -32.0 | Anten |
| 53707.272 M | 72.3 | +10.3 | +1.3 |  |  | +0.0 | 83.9 | 116.5 | -32.6 | Anten |
| 63660.076 M | 72.1 | +10.3 | +1.3 |  |  | +0.0 | 83.7 | 116.5 | -32.8 | Anten |
| 7 2780.442M | 71.9 | +10.2 | +1.2 |  |  | +0.0 | 83.3 | 116.5 | -33.2 | Anten |
| 8 6487.474M | 81.0 | +0.0 | +1.6 |  |  | +0.0 | 82.6 | 116.5 | -33.9 | Anten |
| 9 6320.882M | 80.9 | +0.0 | +1.6 |  |  | +0.0 | 82.5 | 116.5 | -34.0 | Anten |
| $10 \quad 5418.084 \mathrm{M}$ | 80.9 | +0.0 | +1.5 |  |  | +0.0 | 82.4 | 116.5 | -34.1 | Anten |
| $11 \quad 5560.692 \mathrm{M}$ | 80.4 | +0.0 | +1.5 |  |  | +0.0 | 81.9 | 116.5 | -34.6 | Anten |
| 12 6405.118M | 80.2 | +0.0 | +1.6 |  |  | +0.0 | 81.8 | 116.5 | -34.7 | Anten |
| 13 5489.906M | 80.3 | +0.0 | +1.5 |  |  | +0.0 | 81.8 | 116.5 | -34.7 | Anten |
| 14 2745.050M | 70.3 | +10.2 | +1.2 |  |  | +0.0 | 81.7 | 116.5 | -34.8 | Anten |
| 15 2709.056M | 70.1 | +10.2 | +1.2 |  |  | +0.0 | 81.5 | 116.5 | -35.0 | Anten |
| 16 4633.920M | 73.5 | +0.0 | +1.5 |  |  | +0.0 | 75.0 | 116.5 | -41.5 | Anten |
| 17 4574.928M | 71.6 | +0.0 | +1.6 |  |  | +0.0 | 73.2 | 116.5 | -43.3 | Anten |
| 184515.068 M | 70.8 | +0.0 | +1.6 |  |  | +0.0 | 72.4 | 116.5 | -44.1 | Anten |
| 197414.512 M | 69.1 | +0.0 | +1.6 |  |  | +0.0 | 70.7 | 116.5 | -45.8 | Anten |
| $20 \quad 7319.892 \mathrm{M}$ | 67.7 | +0.0 | +1.6 |  |  | +0.0 | 69.3 | 116.5 | -47.2 | Anten |
| 21 7224.150M | 67.4 | +0.0 | +1.6 |  |  | +0.0 | 69.0 | 116.5 | -47.5 | Anten |
| 228341.372 M | 63.8 | +0.0 | +2.0 |  |  | +0.0 | 65.8 | 116.5 | -50.7 | Anten |
| 23 8127.148M | 63.5 | +0.0 | +1.9 |  |  | +0.0 | 65.4 | 116.5 | -51.1 | Anten |
| 24 8235.152M | 63.3 | +0.0 | +1.9 |  |  | +0.0 | 65.2 | 116.5 | -51.3 | Anten |

LABORATORIES, INC.

## Band Edge

## Band Edge Summary

Limit applied: Max Power/100kHz-20dB.
Operating Mode: Single Channel (Low and High)

| Frequency <br> $(\mathbf{M H z})$ | Modulation | Measured <br> $(\mathrm{dB} \boldsymbol{\mu} \mathbf{V})$ | Limit <br> $(\mathrm{dB} \boldsymbol{\mathrm { V } )} \mathbf{)}$ | Results |
| :---: | :---: | :---: | :---: | :---: |
| 902 | AM | 91.2 | $<116.5$ | Pass |
| 928 | AM | 100.4 | $<116.5$ | Pass |
| 902 | FM 12.5 | 103.0 | $<116.5$ | Pass |
| 928 | FM 12.5 | 96.8 | $<116.5$ | Pass |
| 902 | FM 37.5 | 102.3 | $<116.5$ | Pass |
| 928 | FM 37.5 | 97.0 | $<116.5$ | Pass |

Note: Limit converted to $\mathrm{dB} \mu \mathrm{V}$ from dBm , for 50 ohm system $\mathrm{dBm}-107=\mathrm{dB} \mu \mathrm{V}$

## Band Edge Summary

Limit applied: Max Power/100kHz - 20dB.
Operating Mode: Hopping

| Frequency <br> $(\mathrm{MHz})$ | Modulation | Measured <br> $(\mathbf{d B m})$ | Limit <br> $(\mathbf{d B m})$ | Results |
| :---: | :---: | :---: | :---: | :---: |
| 902 | AM | 93.4 | $<116.5$ | Pass |
| 928 | AM | 99.4 | $<116.5$ | Pass |
| 902 | FM 12.5 | 99.8 | $<116.5$ | Pass |
| 928 | FM 12.5 | 96.9 | $<116.5$ | Pass |
| 902 | FM 37.5 | 100.6 | $<116.5$ | Pass |
| 928 | FM 37.5 | 97.5 | $<116.5$ | Pass |

Note: Limit converted to $\mathrm{dB} \mu \mathrm{V}$ from dBm , for 50 ohm system $\mathrm{dBm}-107=\mathrm{dB} \mu \mathrm{V}$

## Band Edge Plots

## Single Channel (Low and High)








## Hopping





CondBE 928 Hopping Fu12.5 (Imt corrected for system factors)
Ref Level $136.99 \mathrm{~dB} \mu \mathrm{~V}$ ATTEN 40 dB
RES BW: 100.0 kHz VD BW: 300.0 kNz SWP, 20.0 msec
Marker 928.0 MHz 88.2017 dBuV


- 15.247 (d) Conducted Spurious Emissions




## Test Setup / Conditions / Data

Test Location: $\quad$ CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A • Bothell, WA 98021•(425) 402-1717

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Itron, Inc.
15.247(d) Conducted Spurious Emissions

107462
Conducted Emissions
Michael Atkinson
EMITest 5.03.20

Date: 11/1/2022
Time: 16:42:02
Sequence\#: 4
120 V 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Test Conditions / Notes:

Test Environment Conditions:
Temperature: $21.7^{\circ} \mathrm{C}$
Humidity: $48 \%$
Pressure: 100.8 kPa
Test Method: ANSI C63.10 (2013)
Frequency: Band Edge
EUT is continuously transmitting with modulation, connected to spectrum analyzer directly through appropriate attenuation.

AM Modulation

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | ANP05503 | Attenuator | $766-10$ | $6 / 8 / 2021$ | $6 / 8 / 2023$ |
| T2 | ANP06008 | Cable | Heliax | $9 / 2 / 2022$ | $9 / 2 / 2024$ |
|  | AN02872 | Spectrum Analyzer | E4440A | $11 / 29 / 2021$ | $11 / 29 / 2023$ |


| Measu | ment Data | Reading listed by margin. |  |  |  |  | Test Lead: Antenna Port |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | Freq <br> MHz | $\begin{aligned} & \hline \mathrm{Rdng} \\ & \mathrm{~dB} \mu \mathrm{~V} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | dB | dB | $\begin{gathered} \hline \text { Dist } \\ \text { Table } \end{gathered}$ | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} \end{gathered}$ | Margin <br> dB | Polar Ant |
| 1 | 928.000 M | 89.7 | +10.1 | +0.6 |  |  | +0.0 | 100.4 | $\begin{aligned} & 116.5 \\ & \text { SC } \end{aligned}$ | -16.1 | Anten |
| 2 | 928.000 M | 88.7 | +10.1 | +0.6 |  |  | +0.0 | 99.4 | $116.5$ <br> Hopping | -17.1 | Anten |
| 3 | 902.000 M | 82.7 | +10.1 | +0.6 |  |  | +0.0 | 93.4 | $116.5$ <br> Hopping | -23.1 | Anten |
| 4 | 902.000 M | 80.5 | +10.1 | +0.6 |  |  | +0.0 | 91.2 | SC | -25.3 | Anten |

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Test Location: CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A•Bothell, WA 98021•(425) 402-1717 Itron, Inc.
15.247(d) Conducted Spurious Emissions 107462
Conducted Emissions
Michael Atkinson
EMITest 5.03.20

Date: 11/1/2022
Time: 16:52:13
Sequence\#: 5
5
120 V 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Test Conditions / Notes:

Test Environment Conditions:
Temperature: $21.7^{\circ} \mathrm{C}$
Humidity: $48 \%$
Pressure: 100.8 kPa

Test Method: ANSI C63.10 (2013)
Frequency: Band Edge
EUT is continuously transmitting with modulation, connected to spectrum analyzer directly through appropriate attenuation.

FM12.5 Modulation

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | ANP05503 | Attenuator | $766-10$ | $6 / 8 / 2021$ | $6 / 8 / 2023$ |
| T2 | ANP06008 | Cable | Heliax | $9 / 2 / 2022$ | $9 / 2 / 2024$ |
|  | AN02872 | Spectrum Analyzer | E4440A | $11 / 29 / 2021$ | $11 / 29 / 2023$ |

Measurement Data: $\quad$ Reading listed by margin. Test Lead: Antenna Port

| $\#$ | Freq <br> MHz | Rdng <br> $\mathrm{dB} \mu \mathrm{V}$ | T 1 <br> dB | T 2 <br> dB | dB | dB | Dist <br> Table | Corr <br> $\mathrm{dB} \mu \mathrm{V}$ | Spec <br> $\mathrm{dB} \mu \mathrm{V}$ | Margin <br> dB | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 902.000 M | 92.3 | +10.1 | +0.6 |  | +0.0 | 103.0 | 116.5 | -13.5 | Anten |  |
| 2 | 902.000 M | 89.1 | +10.1 | +0.6 |  |  | +0.0 | 99.8 | 116.5 <br> Hopping | -16.7 | Anten |
| 3 | 928.000 M | 86.2 | +10.1 | +0.6 |  |  | +0.0 | 96.9 | 116.5 <br> Hopping | -19.6 | Anten |
| 4 | 928.000 M | 86.1 | +10.1 | +0.6 | +0.0 | 96.8 | 116.5 | -19.7 | Anten |  |  |

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Test Location: CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A•Bothell, WA 98021•(425) 402-1717 Itron, Inc.
15.247(d) Conducted Spurious Emissions

107462
Conducted Emissions
Michael Atkinson
EMITest 5.03.20

Date: 11/1/2022
Time: 17:04:08
Sequence\#:
120 V 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Test Conditions / Notes:

Test Environment Conditions:
Temperature: $21.7^{\circ} \mathrm{C}$
Humidity: $48 \%$
Pressure: 100.8 kPa

Test Method: ANSI C63.10 (2013)
Frequency: Band Edge
EUT is continuously transmitting with modulation, connected to spectrum analyzer directly through appropriate attenuation.

FM37.5 Modulation

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | ANP05503 | Attenuator | $766-10$ | $6 / 8 / 2021$ | $6 / 8 / 2023$ |
| T2 | ANP06008 | Cable | Heliax | $9 / 2 / 2022$ | $9 / 2 / 2024$ |
|  | AN02872 | Spectrum Analyzer | E4440A | $11 / 29 / 2021$ | $11 / 29 / 2023$ |

Measurement Data: $\quad$ Reading listed by margin. Test Lead: Antenna Port
$\left.\begin{array}{|cccccccccccc|}\hline \# & \begin{array}{c}\text { Freq } \\ \mathrm{MHz}\end{array} & \begin{array}{c}\text { Rdng } \\ \mathrm{dB} \mu \mathrm{V}\end{array} & \begin{array}{c}\mathrm{T} 1 \\ \mathrm{~dB}\end{array} & \begin{array}{c}\mathrm{T} 2 \\ \mathrm{~dB}\end{array} & \mathrm{~dB} & \mathrm{~dB} & \begin{array}{c}\text { Dist } \\ \text { Table }\end{array} & \begin{array}{c}\text { Corr } \\ \mathrm{dB} \mu \mathrm{V}\end{array} & \begin{array}{c}\text { Spec } \\ \mathrm{dB} \mu \mathrm{V}\end{array} & \begin{array}{c}\text { Margin } \\ \mathrm{dB}\end{array} & \begin{array}{c}\text { Polar } \\ \text { Ant }\end{array} \\ \hline 1 & 902.000 \mathrm{M} & 91.6 & +10.1 & +0.6 & & & +0.0 & 102.3 & 116.5 & -14.2 & \text { Anten } \\ \hline 2 & 902.000 \mathrm{M} & 89.9 & +10.1 & +0.6 & & & +0.0 & 100.6 & \begin{array}{rl}116.5 \\ \text { Hopping }\end{array} & -15.9 & \text { Anten } \\ \hline 3 & 928.000 \mathrm{M} & 86.8 & +10.1 & +0.6 & & & +0.0 & 97.5 & 116.5 & -19.0 & \text { Anten } \\ \hline 4 & 928.000 \mathrm{M} & 86.3 & +10.1 & +0.6 & & & & & & & \\ \text { Hopping }\end{array}\right]$

## Test Setup Photo(s)



### 15.247(d) Radiated Emissions \& Band Edge

## Test Setup / Conditions / Data

Test Location: CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A•Bothell, WA 98021•(425) 402-1717
Customer:
Specification: Work Order \#:
Test Type:
Tested By:
Software: Itron, Inc.
15.247(d) / 15.209 Radiated Spurious Emissions

107462 Date: 10/28/2022
Maximized Emissions Time: 13:04:37
Matt Harrison
Sequence\#: 1

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Test Conditions / Notes:

Test Environment Conditions:
Temperature: $24^{\circ} \mathrm{C}$
Humidity: $51 \%$
Pressure: 101.5 kPa
Test Method: ANSI C63.10 (2013)
Frequency: $9 \mathrm{kHz}-9.28 \mathrm{GHz}$
Test Setup: Unit is on foam table 80 cm high for below 1 GHz and 150 cm high for above 1 GHz . Horizontal and Vertical antenna polarities investigated, worst-case reported; unit is continuously transmitting with modulation.

AM Modulation, LMH channels.

Itron, Inc. WO\#: 107462 Sequence\#: 1 Date: 10/28/2022
15.247 (d) / 15.209 Radiated Spurious Emissions Test Distance: 3 Meters Vert

—— Readings
$\times$ QP Readings
$\times \quad$ Ambient
$1-15.247(\mathrm{~d}) / 15.209$ Radiated Spurious Emissions
O Peak Readings

* Average Readings
Software Version: 5.03.20

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02872 | Spectrum Analyzer | E4440A | $11 / 29 / 2021$ | $11 / 29 / 2023$ |
| T2 | ANP06540 | Cable | Heliax | $1 / 17 / 2022$ | $1 / 17 / 2024$ |
| T3 | ANP05305 | Cable | ETSI-50T | $9 / 15 / 2021$ | $9 / 15 / 2023$ |
| T4 | ANP05360 | Cable | RG214 | $2 / 4 / 2022$ | $2 / 4 / 2024$ |
| T5 | AN03628 | Biconilog Antenna | 3142 E | $6 / 3 / 2021$ | $6 / 3 / 2023$ |
| T6 | AN00052 | Loop Antenna | 6502 | $5 / 11 / 2022$ | $5 / 11 / 2024$ |
| T7 | AN03540 | Preamp | $83017 A$ | $5 / 14 / 2021$ | $5 / 14 / 2023$ |
| T8 | AN02374ANSI | Horn Antenna | RGA-60 | $5 / 25 / 2021$ | $5 / 25 / 2023$ |
| T9 | ANP07504 | Cable | CLU40-KMKM- | $1 / 26 / 2021$ | $1 / 26 / 2023$ |
|  |  |  | High Pass Filter | HM1155-11SS | $9 / 16 / 2021$ |
| T10 | AN03170 | Duty Cycle |  | No Cal Required | No Cal Required |
| T11 | ANDCCF | Correction Factor |  |  |  |



| $\begin{gathered} 16 \text { 8314.440M } \\ \text { Ave } \end{gathered}$ | 43.0 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+1.2 \\ & +0.0 \\ & +0.9 \\ & \hline \end{aligned}$ | $\begin{array}{r} +5.2 \\ -34.9 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +38.7 \end{array}$ | +0.0 | 42.3 | 54.0 | -11.7 | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge 8314.440 \mathrm{M}$ | 43.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+1.2 \\ & +0.0 \\ & +0.9 \\ & \hline \end{aligned}$ | $\begin{array}{r} +5.2 \\ -34.9 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +38.7 \end{array}$ | +0.0 | 54.8 | 54.0 | +0.8 | Vert |
| $\begin{aligned} & 187390.460 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 45.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \end{aligned}$ | $\begin{aligned} & \hline+1.3 \\ & +0.0 \\ & +0.7 \end{aligned}$ | $\begin{array}{r} +4.5 \\ -34.9 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +37.4 \end{array}$ | +0.0 | 42.3 | 54.0 | -11.7 | Horiz |
| $\wedge 7390.460 \mathrm{M}$ | 45.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+1.3 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.5 \\ -34.9 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +37.4 \end{array}$ | +0.0 | 54.8 | 54.0 | +0.8 | Horiz |
| $\begin{gathered} 207263.870 \mathrm{M} \\ \text { Ave } \end{gathered}$ | 45.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+1.2 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.5 \\ -34.9 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +37.2 \end{array}$ | +0.0 | 41.6 | 54.0 | -12.4 | Vert |
| $\wedge 7263.870 \mathrm{M}$ | 45.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+1.2 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.5 \\ -34.9 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +37.2 \end{array}$ | +0.0 | 54.1 | 54.0 | +0.1 | Vert |
| $\begin{aligned} & 227320.020 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 44.3 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.3 \\ & +0.0 \\ & +0.6 \end{aligned}$ | $\begin{array}{r} +4.5 \\ -34.9 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +37.5 \end{array}$ | +0.0 | 41.5 | 54.0 | -12.5 | Horiz |
| $\wedge 7320.020 \mathrm{M}$ | 44.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+1.3 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.5 \\ -34.9 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +37.5 \end{array}$ | +0.0 | 54.0 | 54.0 | +0.0 | Horiz |
| 24 3695.080M | 51.3 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.2 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.3 \\ -33.8 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +31.9 \end{array}$ | +0.0 | 41.3 | 54.0 | -12.7 | Horiz |
| 255447.935 M | 44.4 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.8 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.0 \\ -33.6 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +34.7 \end{array}$ | +0.0 | 38.7 | 54.0 | -15.3 | Horiz |
| $\begin{aligned} & 26 \text { 3659.945M } \\ & \text { Ave } \end{aligned}$ | 48.0 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.6 \\ & +0.0 \\ & +0.2 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.3 \\ -33.8 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +31.7 \end{array}$ | +0.0 | 37.9 | 54.0 | -16.1 | Horiz |
| $\wedge 3659.945 \mathrm{M}$ | 48.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.2 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.3 \\ -33.8 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +31.7 \end{array}$ | +0.0 | 50.4 | 54.0 | -3.6 | Horiz |
| $\begin{aligned} & 283632.495 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 46.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.3 \\ -33.8 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +31.7 \end{array}$ | +0.0 | 36.2 | 54.0 | -17.8 | Horiz |
| $\wedge 3632.495 \mathrm{M}$ | 46.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.3 \\ -33.8 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +31.7 \end{array}$ | +0.0 | 48.7 | 54.0 | -5.3 | Horiz |
| $30 \quad 829.300 \mathrm{M}$ | 40.8 | $\begin{array}{r} +0.0 \\ +29.3 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+2.2 \\ & +0.0 \end{aligned}$ | +0.0 | 74.0 | 113.0 | -39.0 | Vert |
| $31 \quad 830.200 \mathrm{M}$ | 34.9 | $\begin{array}{r} +0.0 \\ +29.3 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+2.2 \\ & +0.0 \end{aligned}$ | +0.0 | 68.1 | 113.0 | -44.9 | Horiz |
| 32 6466.780M | 54.4 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.5 \\ -34.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +34.9 \end{array}$ | +0.0 | 62.0 | 113.0 | -51.0 | Vert |

Page 63 of 111

| 33 | 6404.525M | 54.4 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.9 \\ & +0.0 \\ & +0.5 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.5 \\ -34.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +35.0 \end{array}$ | +0.0 | 61.9 | 113.0 | -51.1 | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 34 | 6355.625M | 51.5 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.4 \\ -34.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +35.1 \end{array}$ | +0.0 | 58.9 | 113.0 | -54.1 | Vert |
| 35 | 5542.715 M | 45.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.5 \end{aligned}$ | $\begin{aligned} & +0.8 \\ & +0.0 \\ & +0.5 \end{aligned}$ | $\begin{array}{r} +4.0 \\ -33.6 \\ +0.0 \end{array}$ | $\begin{array}{r} +0.0 \\ +34.6 \end{array}$ | +0.0 | 51.9 | 113.0 | -61.1 | Vert |
| 36 | 5490.285M | 44.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.8 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.0 \\ -33.6 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +34.7 \end{array}$ | +0.0 | 50.9 | 113.0 | -62.1 | Vert |
| 37 | 1830.145M | 53.3 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.4 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{array}{r} +2.1 \\ -34.7 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +27.5 \end{array}$ | +0.0 | 49.5 | 113.0 | -63.5 | Vert |
| 38 | 1847.715M | 52.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.4 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{array}{r} +2.1 \\ -34.7 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +27.6 \end{array}$ | +0.0 | 48.6 | 113.0 | -64.4 | Vert |
| 39 | 1815.760M | 50.9 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.4 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{array}{r} +2.1 \\ -34.7 \\ +0.0 \end{array}$ | $\begin{array}{r} +0.0 \\ +27.4 \end{array}$ | +0.0 | 47.0 | 113.0 | -66.0 | Vert |
| 40 | 68.800M | 30.9 | $\begin{array}{r} +0.0 \\ +12.9 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.5 \\ & +0.0 \end{aligned}$ | +0.0 | 44.8 | 113.0 | -68.2 | Vert |
| 41 | 68.800M | 25.6 | $\begin{array}{r} +0.0 \\ +12.9 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.5 \\ & +0.0 \end{aligned}$ | +0.0 | 39.5 | 113.0 | -73.5 | Horiz |
| 42 | 19.702M | 34.4 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +6.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \end{aligned}$ | -40.0 | 1.1 | 113.0 | -111.9 | Perp/ |
| 43 | 27.164M | 33.7 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +4.9 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -1.1 | 113.0 | -114.1 | Perp/ |
| 44 | 23.134M | 32.2 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +6.1 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -1.4 | 113.0 | -114.4 | Perp/ |
| 45 | 26.597 M | 32.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +5.2 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | $-2.5$ | 113.0 | -115.5 | Perp/ |
| 46 | 33.393 k | 45.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.1 \\ +10.8 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \end{aligned}$ | -80.0 | -23.8 | 113.0 | -136.8 | Perp/ |

Test Location: $\quad$ CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A • Bothell, WA 98021•(425) 402-1717
Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Itron, Inc.
15.247(d) / 15.209 Radiated Spurious Emissions

107462
Maximized Emissions
Matt Harrison
EMIT est 5.03.20

Date: 10/29/2022
Time: 08:20:10
Sequence\#: 2

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Test Environment Conditions
Temperature: $24^{\circ} \mathrm{C}$
Humidity: $51 \%$
Pressure: 101.5 kPa

Test Method: ANSI C63.10 (2013)
Frequency: $9 \mathrm{kHz}-9.28 \mathrm{GHz}$
Test Setup: Unit is on foam table 80 cm high for below 1 GHz and 150 cm high for above 1 GHz . Horizontal and Vertical antenna polarities investigated, worst-case reported; unit is continuously transmitting with modulation.

FM 12.5k Modulation, LMH channels.

Itron, Inc. WO\#: 107462 Sequence\#: 2 Date: 10/29/2022
15.247(d) / 15.209 Radiated Spurious Emissions Test Distance: 3 Meters Horiz


- Readings
$\times$ QP Readings
$\times$ Ambient
$1-15.247$ (d) / 15.209 Radiated Spurious Emissions
O Peak Readings
* Average Readings
Software Version: 5.03.20

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02872 | Spectrum Analyzer | E4440A | $11 / 29 / 2021$ | $11 / 29 / 2023$ |
| T2 | ANP06540 | Cable | Heliax | $1 / 17 / 2022$ | $1 / 17 / 2024$ |
| T3 | ANP05305 | Cable | ETSI-50T | $9 / 15 / 2021$ | $9 / 15 / 2023$ |
| T4 | ANP05360 | Cable | RG214 | $2 / 4 / 2022$ | $2 / 4 / 2024$ |
| T5 | AN03628 | Biconilog Antenna | 3142 E | $6 / 3 / 2021$ | $6 / 3 / 2023$ |
| T6 | AN00052 | Loop Antenna | 6502 | $5 / 11 / 2022$ | $5 / 11 / 2024$ |
| T7 | AN03540 | Preamp | $83017 A$ | $5 / 14 / 2021$ | $5 / 14 / 2023$ |
| T8 | AN02374ANSI | Horn Antenna | RGA-60 | $5 / 25 / 2021$ | $5 / 25 / 2023$ |
| T9 | ANP07504 | Cable | CLU40-KMKM- | $1 / 26 / 2021$ | $1 / 26 / 2023$ |
|  |  |  | High Pass Filter | HM1155-11SS | $9 / 16 / 2021$ |
| T10 | AN03170 | Duty Cycle |  | No Cal Required | No Cal Required |
| T11 | ANDCCF | Correction Factor |  |  |  |



| $\begin{aligned} & 169149.635 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 42.7 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.9 \\ & +0.0 \\ & +1.1 \\ & \hline \end{aligned}$ | $\begin{array}{r} +5.0 \\ -34.4 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +37.7 \end{array}$ | +0.0 | 41.2 | 54.0 | -12.8 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge 9149.635 \mathrm{M}$ | 42.7 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \end{aligned}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +1.1 \end{aligned}$ | $\begin{array}{r} +5.0 \\ -34.4 \\ +0.0 \end{array}$ | $\begin{array}{r} +0.0 \\ +37.7 \end{array}$ | +0.0 | 53.7 | 54.0 | -0.3 | Horiz |
| $\begin{gathered} 18 \text { 9029.315M } \\ \text { Ave } \end{gathered}$ | 43.0 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.7 \end{aligned}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +0.7 \end{aligned}$ | $\begin{array}{r} +4.9 \\ -34.7 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +38.0 \end{array}$ | +0.0 | 41.0 | 54.0 | -13.0 | Horiz |
| $\wedge 9029.315 \mathrm{M}$ | 43.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +0.7 \end{aligned}$ | $\begin{array}{r} +4.9 \\ -34.7 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +38.0 \end{array}$ | +0.0 | 53.5 | 54.0 | -0.5 | Horiz |
| $\begin{gathered} 207413.710 \mathrm{M} \\ \text { Ave } \end{gathered}$ | 43.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+1.3 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.5 \\ -34.9 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +37.4 \end{array}$ | +0.0 | 40.5 | 54.0 | -13.5 | Horiz |
| $\wedge 7413.710 \mathrm{M}$ | 43.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.3 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.5 \\ -34.9 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +37.4 \end{array}$ | $+0.0$ | 53.0 | 54.0 | -1.0 | Horiz |
| $\begin{aligned} & 22 \text { 8340.780M } \\ & \text { Ave } \end{aligned}$ | 41.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.2 \\ & +0.0 \\ & +0.9 \\ & \hline \end{aligned}$ | $\begin{array}{r} +5.2 \\ -34.9 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +38.6 \end{array}$ | +0.0 | 40.4 | 54.0 | -13.6 | Horiz |
| $\wedge 8340.780 \mathrm{M}$ | 41.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+1.2 \\ & +0.0 \\ & +0.9 \\ & \hline \end{aligned}$ | $\begin{array}{r} +5.2 \\ -34.9 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +38.6 \end{array}$ | +0.0 | 52.9 | 54.0 | -1.1 | Horiz |
| $\begin{aligned} & 24 \begin{array}{l} 4633.750 \mathrm{M} \\ \text { Ave } \end{array} \end{aligned}$ | 47.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.4 \end{aligned}$ | $\begin{array}{r} +3.6 \\ -33.6 \\ +12.5 \end{array}$ | $\begin{array}{r} +0.0 \\ +32.4 \end{array}$ | +0.0 | 38.5 | 54.0 | -15.5 | Vert |
| $\wedge 4633.750 \mathrm{M}$ | 47.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.6 \\ -33.6 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +32.4 \end{array}$ | +0.0 | 51.0 | 54.0 | -3.0 | Vert |
| $\begin{aligned} & 26 \text { 3660.155M } \\ & \text { Ave } \end{aligned}$ | 48.5 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.6 \\ & +0.0 \\ & +0.2 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.3 \\ -33.8 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +31.7 \end{array}$ | $+0.0$ | 38.4 | 54.0 | -15.6 | Horiz |
| $\wedge 3660.155 \mathrm{M}$ | 48.5 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.2 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.3 \\ -33.8 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +31.7 \end{array}$ | $+0.0$ | 50.9 | 54.0 | -3.1 | Horiz |
| $\begin{aligned} & 283707.055 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 46.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.2 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.3 \\ -33.8 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +32.0 \end{array}$ | $+0.0$ | 36.4 | 54.0 | -17.6 | Horiz |
| $\wedge 3707.055 \mathrm{M}$ | 46.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.2 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.3 \\ -33.8 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +32.0 \end{array}$ | $+0.0$ | 48.9 | 54.0 | -5.1 | Horiz |
| $\begin{aligned} & 303612.095 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 46.1 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.2 \\ -33.8 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +31.7 \end{array}$ | +0.0 | 35.9 | 54.0 | -18.1 | Horiz |
| $\wedge 3612.095 \mathrm{M}$ | 46.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.2 \\ -33.8 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +31.7 \end{array}$ | +0.0 | 48.4 | 54.0 | -5.6 | Horiz |
| 326487.225 M | 56.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +0.6 \end{aligned}$ | $\begin{array}{r} +4.5 \\ -34.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +34.9 \end{array}$ | $+0.0$ | 63.8 | 108.0 | -44.2 | Vert |


| 33 | 6404.675M | 54.8 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +0.5 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.5 \\ -34.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +35.0 \end{array}$ | +0.0 | 62.3 | 108.0 | -45.7 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 34 | 6321.330M | 51.8 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.4 \\ -34.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +35.2 \end{array}$ | +0.0 | 59.3 | 108.0 | -48.7 | Horiz |
| 35 | 7224.295M | 45.7 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.2 \\ & +0.0 \\ & +0.2 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.6 \\ -34.9 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +37.0 \end{array}$ | +0.0 | 54.5 | 108.0 | -53.5 | Horiz |
| 36 | 9267.585M | 41.5 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.0 \\ & +0.0 \\ & +1.4 \end{aligned}$ | $\begin{array}{r} +5.0 \\ -34.2 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +38.0 \end{array}$ | +0.0 | 53.4 | 108.0 | -54.6 | Horiz |
| 37 | 5489.735M | 45.3 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.5 \\ \hline \end{array}$ | $\begin{aligned} & +0.8 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.0 \\ -33.6 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +34.7 \end{array}$ | +0.0 | 52.1 | 108.0 | -55.9 | Horiz |
| 38 | 5560.560 M | 44.7 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.8 \\ & +0.0 \\ & +0.5 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.0 \\ -33.6 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +34.5 \end{array}$ | +0.0 | 51.4 | 108.0 | -56.6 | Vert |
| 39 | 68.800M | 33.4 | $\begin{array}{r} +0.0 \\ +12.9 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.5 \\ & +0.0 \end{aligned}$ | +0.0 | 47.3 | 108.0 | -60.7 | Vert |
| 40 | 1853.615M | 50.8 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.4 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{array}{r} +2.1 \\ -34.7 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +27.7 \end{array}$ | +0.0 | 47.2 | 108.0 | -60.8 | Vert |
| 41 | 1805.820M | 51.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.4 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{array}{r} +2.1 \\ -34.7 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +27.3 \end{array}$ | +0.0 | 47.0 | 108.0 | -61.0 | Vert |
| 42 | 1829.935M | 50.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.4 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{array}{r} +2.1 \\ -34.7 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +27.5 \end{array}$ | +0.0 | 46.5 | 108.0 | -61.5 | Vert |
| 43 | 50.400 M | 28.9 | $\begin{array}{r} +0.0 \\ +12.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.5 \\ & +0.0 \end{aligned}$ | +0.0 | 42.2 | 108.0 | -65.8 | Vert |
| 44 | 19.702M | 35.4 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +6.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \end{aligned}$ | -40.0 | 2.1 | 108.0 | -105.9 | Perp/ |
| 45 | 23.134M | 33.2 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +6.1 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -0.4 | 108.0 | -108.4 | Perp/ |
| 46 | 27.164 M | 34.3 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +4.9 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -0.5 | 108.0 | -108.5 | Perp/ |
| 47 | 27.343 M | 32.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +4.8 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -2.9 | 108.0 | -110.9 | Perp/ |

Test Location: $\quad$ CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A • Bothell, WA 98021•(425) 402-1717
Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Itron, Inc.
15.247(d) / 15.209 Radiated Spurious Emissions

107462
Maximized Emissions
Matt Harrison
EMIT est 5.03.20

Date: 10/29/2022
Time: 09:22:40
Sequence\#: 3

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Test Environment Conditions:
Temperature: $24^{\circ} \mathrm{C}$
Humidity: $51 \%$
Pressure: 101.5 kPa
Test Method: ANSI C63.10 (2013)
Frequency: $9 \mathrm{kHz}-9.28 \mathrm{GHz}$
Test Setup: Unit is on foam table 80 cm high for below 1 GHz and 150 cm high for above 1 GHz . Horizontal and Vertical antenna polarities investigated, worst-case reported, unit is continuously transmitting with modulation.

FM 37.5k Modulation, LMH channels.

Itron, Inc. WO\#: 107462 Sequence\#: 3 Date: 10/29/2022
15.247(d) / 15.209 Radiated Spurious Emissions Test Distance: 3 Meters Vert


O Peak Readings

* Average Readings

Software Version: 5.03.20

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02872 | Spectrum Analyzer | E4440A | $11 / 29 / 2021$ | $11 / 29 / 2023$ |
| T2 | ANP06540 | Cable | Heliax | $1 / 17 / 2022$ | $1 / 17 / 2024$ |
| T3 | ANP05305 | Cable | ETSI-50T | $9 / 15 / 2021$ | $9 / 15 / 2023$ |
| T4 | ANP05360 | Cable | RG214 | $2 / 4 / 2022$ | $2 / 4 / 2024$ |
| T5 | AN03628 | Biconilog Antenna | 3142 E | $6 / 3 / 2021$ | $6 / 3 / 2023$ |
| T6 | AN00052 | Loop Antenna | 6502 | $5 / 11 / 2022$ | $5 / 11 / 2024$ |
| T7 | AN03540 | Preamp | $83017 A$ | $5 / 14 / 2021$ | $5 / 14 / 2023$ |
| T8 | AN02374ANSI | Horn Antenna | RGA-60 | $5 / 25 / 2021$ | $5 / 25 / 2023$ |
| T9 | ANP07504 | Cable | CLU40-KMKM- | $1 / 26 / 2021$ | $1 / 26 / 2023$ |
|  |  |  | High Pass Filter | HM1155-11SS | $9 / 16 / 2021$ |
| T10 | AN03170 | Duty Cycle |  | No Cal Required | No Cal Required |
| T11 | ANDCCF | Correction Factor |  |  |  |


| Measurement Data: | Reading listed by margin. |  |  |  | Test Distance: 3 Meters |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# $\begin{array}{rr}\text { Freq } \\ & \\ & \mathrm{MHz}\end{array}$ | Rdng | T1 | T2 | T3 | T4 | Dist | Corr | Spec | Margin | Polar |
|  |  | T5 | T6 | T7 | T8 |  |  |  |  |  |
|  |  | T9 | $\mathrm{T} 10$ | $\mathrm{T} 11$ |  |  |  |  |  |  |
|  | $\mathrm{dB} \mu \mathrm{V}$ |  |  |  |  | Table | $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$ | $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$ | dB | Ant |
| $1 \quad 110.760 \mathrm{M}$ | 25.0 | +0.0 | +0.1 | +0.5 | +0.7 | +0.0 | 40.4 | 43.5 | -3.1 | Vert |
| QP |  | +14.1 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| $\wedge 110.760 \mathrm{M}$ | 30.2 | +0.0 | +0.1 | +0.5 | +0.7 | +0.0 | 45.6 | 43.5 | +2.1 | Vert |
|  |  | +14.1 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 34575.115 M | 44.4 | +0.0 | +0.6 | +3.5 | +0.0 | +0.0 | 48.0 | 54.0 | -6.0 | Horiz |
|  |  | +0.0 | +0.0 | -33.6 | +32.2 |  |  |  |  |  |
|  |  | +0.4 | +0.5 | +0.0 |  |  |  |  |  |  |
| 43611.935 M | 45.1 | +0.0 | +0.5 | +3.2 | +0.0 | +0.0 | 47.4 | 54.0 | -6.6 | Horiz |
|  |  | +0.0 | +0.0 | -33.8 | +31.7 |  |  |  |  |  |
|  |  | +0.4 | +0.3 | +0.0 |  |  |  |  |  |  |
| 54514.960 M | 41.4 | +0.0 | +0.6 | +3.5 | +0.0 | +0.0 | 44.9 | 54.0 | -9.1 | Horiz |
|  |  | +0.0 | +0.0 | -33.6 | +32.2 |  |  |  |  |  |
|  |  | +0.3 | +0.5 | +0.0 |  |  |  |  |  |  |
| 62709.035 M | 44.8 | +0.0 | +0.5 | +2.7 | +0.0 | +0.0 | 44.1 | 54.0 | -9.9 | Horiz |
|  |  | +0.0 | +0.0 | -34.1 | +29.5 |  |  |  |  |  |
|  |  | +0.5 | +0.2 | +0.0 |  |  |  |  |  |  |
| 7 2780.155M | 44.8 | +0.0 | +0.5 | +2.7 | +0.0 | +0.0 | 44.0 | 54.0 | -10.0 | Vert |
|  |  | +0.0 | +0.0 | -34.1 | +29.3 |  |  |  |  |  |
|  |  | +0.5 | +0.3 | +0.0 |  |  |  |  |  |  |
| 82745.210 M | 43.7 | +0.0 | +0.5 | +2.7 | +0.0 | +0.0 | 42.9 | 54.0 | -11.1 | Vert |
|  |  | +0.0 | +0.0 | -34.1 | +29.3 |  |  |  |  |  |
|  |  | +0.5 | +0.3 | +0.0 |  |  |  |  |  |  |
| $\begin{aligned} & 9 \text { 8234.960M } \\ & \text { Ave } \end{aligned}$ | 42.7 | +0.0 | +1.2 | +5.1 | +0.0 | +0.0 | 41.7 | 54.0 | -12.3 | Horiz |
|  |  | +0.0 | +0.0 | -34.9 | +38.6 |  |  |  |  |  |
|  |  | +0.7 | +0.8 | +12.5 |  |  |  |  |  |  |
| $\wedge 8234.960 \mathrm{M}$ | 42.7 | +0.0 | +1.2 | +5.1 | +0.0 | +0.0 | 54.2 | 54.0 | +0.2 | Horiz |
|  |  | +0.0 | +0.0 | -34.9 | +38.6 |  |  |  |  |  |
|  |  | +0.7 | +0.8 | +0.0 |  |  |  |  |  |  |
| $\begin{aligned} & 11 \text { 9149.865M } \\ & \text { Ave } \end{aligned}$ | 42.9 | +0.0 | +0.9 | +5.0 | +0.0 | +0.0 | 41.4 | 54.0 | -12.6 | Horiz |
|  |  | +0.0 | +0.0 | -34.4 | +37.7 |  |  |  |  |  |
|  |  | +0.7 | +1.1 | +12.5 |  |  |  |  |  |  |
| $\wedge 9149.865 \mathrm{M}$ | 42.9 | +0.0 | +0.9 | +5.0 | +0.0 | +0.0 | 53.9 | 54.0 | -0.1 | Horiz |
|  |  | +0.0 | +0.0 | -34.4 | +37.7 |  |  |  |  |  |
|  |  | +0.7 | +1.1 | +0.0 |  |  |  |  |  |  |
| $\begin{aligned} & 13 \text { 7320.015M } \\ & \text { Ave } \end{aligned}$ | 44.1 | +0.0 | +1.3 | +4.5 | +0.0 | +0.0 | 41.3 | 54.0 | -12.7 | Vert |
|  |  | +0.0 | +0.0 | -34.9 | +37.5 |  |  |  |  |  |
|  |  | +0.7 | +0.6 | +12.5 |  |  |  |  |  |  |
| $\wedge 7320.015 \mathrm{M}$ | 44.1 | +0.0 | +1.3 | +4.5 | +0.0 | +0.0 | 53.8 | 54.0 | -0.2 | Vert |
|  |  | +0.0 | +0.0 | -34.9 | +37.5 |  |  |  |  |  |
|  |  | +0.7 | +0.6 | +0.0 |  |  |  |  |  |  |


| $\begin{aligned} & 155417.995 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 46.6 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.8 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.0 \\ -33.6 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +34.7 \end{array}$ | $+0.0$ | 41.0 | 54.0 | -13.0 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge 5417.995 \mathrm{M}$ | 46.6 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.8 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.0 \\ -33.6 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +34.7 \end{array}$ | +0.0 | 53.5 | 54.0 | -0.5 | Horiz |
| $\begin{aligned} & 17 \text { 8126.470M } \\ & \text { Ave } \end{aligned}$ | 42.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.2 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{array}{r} +5.1 \\ -35.1 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +38.6 \end{array}$ | +0.0 | 40.6 | 54.0 | -13.4 | Vert |
| $\wedge 8126.470 \mathrm{M}$ | 42.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.2 \\ & +0.0 \\ & +0.6 \end{aligned}$ | $\begin{array}{r} +5.1 \\ -35.1 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +38.6 \end{array}$ | $+0.0$ | 53.1 | 54.0 | -0.9 | Vert |
| $\begin{aligned} & 197414.270 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 43.1 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+1.3 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.4 \\ -34.9 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +37.4 \end{array}$ | +0.0 | 40.2 | 54.0 | -13.8 | Horiz |
| $\wedge 7414.270 \mathrm{M}$ | 43.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+1.3 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.4 \\ -34.9 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +37.4 \end{array}$ | +0.0 | 52.7 | 54.0 | -1.3 | Horiz |
| $\begin{aligned} & 21 \text { 9030.530M } \\ & \text { Ave } \end{aligned}$ | 42.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \end{aligned}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.9 \\ -34.7 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +38.0 \end{array}$ | $+0.0$ | 40.0 | 54.0 | -14.0 | Vert |
| $\wedge 9030.530 \mathrm{M}$ | 42.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.9 \\ -34.7 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +38.0 \end{array}$ | +0.0 | 52.5 | 54.0 | -1.5 | Vert |
| $\begin{aligned} & 23 \text { 8341.160M } \\ & \text { Ave } \end{aligned}$ | 40.7 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.2 \\ & +0.0 \\ & +0.9 \\ & \hline \end{aligned}$ | $\begin{array}{r} +5.2 \\ -34.9 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +38.6 \end{array}$ | $+0.0$ | 39.9 | 54.0 | -14.1 | Vert |
| $\wedge 8341.160 \mathrm{M}$ | 40.7 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+1.2 \\ & +0.0 \\ & +0.9 \\ & \hline \end{aligned}$ | $\begin{array}{r} +5.2 \\ -34.9 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +38.6 \end{array}$ | $+0.0$ | 52.4 | 54.0 | -1.6 | Vert |
| $\begin{aligned} & 25 \text { 4634.135M } \\ & \text { Ave } \end{aligned}$ | 47.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.6 \\ -33.6 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +32.4 \end{array}$ | +0.0 | 38.4 | 54.0 | -15.6 | Vert |
| $\wedge 4634.135 \mathrm{M}$ | 47.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.6 \\ -33.6 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +32.4 \end{array}$ | +0.0 | 50.9 | 54.0 | -3.1 | Vert |
| $\begin{aligned} & 27 \text { 3659.960M } \\ & \text { Ave } \end{aligned}$ | 48.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.6 \\ & +0.0 \\ & +0.2 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.3 \\ -33.8 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +31.7 \end{array}$ | +0.0 | 38.1 | 54.0 | -15.9 | Horiz |
| $\wedge 3659.960 \mathrm{M}$ | 48.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.2 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.3 \\ -33.8 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +31.7 \end{array}$ | $+0.0$ | 50.6 | 54.0 | -3.4 | Horiz |
| $\begin{aligned} & 293707.240 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 46.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +0.2 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.3 \\ -33.8 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +32.0 \end{array}$ | $+0.0$ | 36.2 | 54.0 | -17.8 | Horiz |
| $\wedge 3707.240 \mathrm{M}$ | 46.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.6 \\ & +0.0 \\ & +0.2 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.3 \\ -33.8 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +32.0 \end{array}$ | +0.0 | 48.7 | 54.0 | -5.3 | Horiz |
| 31 6487.280M | 55.2 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.5 \\ -34.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +34.9 \end{array}$ | $+0.0$ | 62.8 | 111.0 | -48.2 | Vert |


| 32 | 6404.950M | 52.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.6 \end{aligned}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +0.5 \end{aligned}$ | $\begin{array}{r} +4.5 \\ -34.0 \\ +0.0 \end{array}$ | $\begin{array}{r} +0.0 \\ +35.0 \end{array}$ | +0.0 | 59.8 | 111.0 | -51.2 | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 33 | 6321.295 M | 51.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.9 \\ +0.0 \\ +0.4 \\ \hline \end{array}$ | $\begin{array}{r} +4.4 \\ -34.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +35.2 \end{array}$ | +0.0 | 58.5 | 111.0 | -52.5 | Vert |
| 34 | 7224.205M | 45.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.7 \end{aligned}$ | $\begin{aligned} & \hline+1.2 \\ & +0.0 \\ & +0.2 \end{aligned}$ | $\begin{array}{r} +4.6 \\ -34.9 \\ +0.0 \end{array}$ | $\begin{array}{r} +0.0 \\ +37.0 \end{array}$ | +0.0 | 53.9 | 111.0 | -57.1 | Horiz |
| 35 | 5489.815M | 45.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.8 \\ & +0.0 \\ & +0.4 \\ & \hline \end{aligned}$ | $\begin{array}{r} +4.0 \\ -33.6 \\ +0.0 \end{array}$ | $\begin{array}{r} +0.0 \\ +34.7 \end{array}$ | +0.0 | 51.9 | 111.0 | -59.1 | Horiz |
| 36 | 5560.390 M | 44.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.5 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.8 \\ +0.0 \\ +0.5 \\ \hline \end{array}$ | $\begin{array}{r} +4.0 \\ -33.6 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +34.5 \end{array}$ | +0.0 | 50.9 | 111.0 | -60.1 | Vert |
| 37 | 1853.575M | 48.4 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.4 \\ +0.0 \\ +0.6 \\ \hline \end{array}$ | $\begin{array}{r} \hline+2.1 \\ -34.7 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +27.7 \end{array}$ | +0.0 | 44.8 | 111.0 | -66.2 | Vert |
| 38 | 68.800M | 30.8 | $\begin{array}{r} +0.0 \\ +12.9 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.5 \\ & +0.0 \end{aligned}$ | +0.0 | 44.7 | 111.0 | -66.3 | Vert |
| 39 | 1806.035M | 48.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.4 \\ +0.0 \\ +0.6 \\ \hline \end{array}$ | $\begin{array}{r} +2.1 \\ -34.7 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +27.3 \end{array}$ | +0.0 | 44.1 | 111.0 | -66.9 | Horiz |
| 40 | 50.400 M | 28.5 | $\begin{array}{r} +0.0 \\ +12.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.5 \\ & +0.0 \end{aligned}$ | +0.0 | 41.8 | 111.0 | -69.2 | Vert |
| 41 | 85.300 M | 27.6 | $\begin{array}{r} +0.0 \\ +12.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.6 \\ & +0.0 \end{aligned}$ | +0.0 | 41.1 | 111.0 | -69.9 | Vert |
| 42 | 60.100M | 26.3 | $\begin{array}{r} +0.0 \\ +12.6 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.5 \\ & +0.0 \end{aligned}$ | +0.0 | 39.9 | 111.0 | -71.1 | Horiz |
| 43 | 1830.155M | 49.5 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.4 \\ & +0.0 \\ & +0.6 \\ & \hline \end{aligned}$ | $\begin{array}{r} +2.1 \\ -34.7 \\ +12.5 \\ \hline \end{array}$ | $\begin{array}{r} +0.0 \\ +27.5 \end{array}$ | +0.0 | 33.2 | 111.0 | -77.8 | Vert |
| 44 | 19.702M | 35.8 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +6.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \end{aligned}$ | -40.0 | 2.5 | 111.0 | -108.5 | Perp/ |
| 45 | 23.134 M | 31.0 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +6.1 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -2.6 | 111.0 | -113.6 | Perp/ |
| 46 | 27.164M | 32.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.1 \\ +4.9 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -2.7 | 111.0 | -113.7 | Perp/ |
| 47 | 27.881M | 30.9 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +4.6 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -4.2 | 111.0 | -115.2 | Perp/ |

LIABORATORIES, INC.

## Band Edge

## Band Edge Summary

Operating Mode: Single Channel (Low and High)

| Frequency <br> $(\mathbf{M H z})$ | Modulation | Ant. Type | Field Strength <br> $(\mathbf{d B u V} / \mathbf{m} @ 3 \mathrm{~m})$ | Limit <br> $(\mathbf{d B u V} / \mathbf{m} @ 3 m)$ | Results |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 614 | AM | Omnidirectional | 38.8 | $<46$ | Pass |
| 902 | AM | Omnidirectional | 68.0 | $<113$ | Pass |
| 928 | AM | Omnidirectional | 58.2 | $<113$ | Pass |
| 960 | AM | Omnidirectional | 42.8 | $<54$ | Pass |
| 614 | FM 12.5k | Omnidirectional | 38.5 | $<46$ | Pass |
| 902 | FM 12.5k | Omnidirectional | 56.7 | $<108$ | Pass |
| 928 | FM 12.5k | Omnidirectional | 58.2 | $<111$ | Pass |
| 960 | FM 12.5k | Omnidirectional | 42.8 | $<54$ | Pass |
| 614 | FM 37.5k | Omnidirectional | 38.6 | $<46$ | Pass |
| 902 | FM 37.5k | Omnidirectional | 58.7 | $<108$ | Pass |
| 928 | FM 37.5k | Omnidirectional | 57.7 | $<111$ | Pass |
| 960 | FM 37.5k | Omnidirectional | 42.9 | $<54$ | Pass |

## Band Edge Summary

Operating Mode: Hopping

| Frequency <br> $(\mathbf{M H z})$ | Modulation | Ant. Type | Field Strength <br> $(\mathbf{d B u V} / \mathbf{m} @ 3 \mathrm{~m})$ | Limit <br> $(\mathbf{d B u V} / \mathrm{m} @ 3 m)$ | Results |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 614 | AM | Omnidirectional | 38.5 | $<46$ | Pass |
| 902 | AM | Omnidirectional | 58.2 | $<113$ | Pass |
| 928 | AM | Omnidirectional | 58.3 | $<113$ | Pass |
| 960 | AM | Omnidirectional | 42.7 | $<54$ | Pass |
| 614 | FM 12.5k | Omnidirectional | 38.5 | $<46$ | Pass |
| 902 | FM 12.5k | Omnidirectional | 58 | $<108$ | Pass |
| 928 | FM 12.5k | Omnidirectional | 58.1 | $<111$ | Pass |
| 960 | FM 12.5k | Omnidirectional | 42.7 | $<54$ | Pass |
| 614 | FM 37.5k | Omnidirectional | 38.5 | $<46$ | Pass |
| 902 | FM 37.5k | Omnidirectional | 57.3 | $<108$ | Pass |
| 928 | FM 37.5k | Omnidirectional | 59.0 | $<111$ | Pass |
| 960 | FM 37.5k | Omnidirectional | 42.8 | $<54$ | Pass |

## Band Edge Plots

## Single Channel (Low and High)














## Hopping






M
LABORATORIES, INC.









Test Setup / Conditions / Data

Test Location:
Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A •Bothell, WA 98021•(425) 402-1717 Itron, Inc.
15.247(d) / 15.209 Radiated Spurious Emissions 107462
Maximized Emissions
Michael Atkinson
EMITest 5.03.20

Date: 10/27/2022
Time: 17:39:40
Sequence\#: 1

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Test Environment Conditions:
Temperature: $24^{\circ} \mathrm{C}$
Humidity: 51\%
Pressure: 101.5 kPa
Test Method: ANSI C63.10 (2013)
Frequency: Band Edge
Test Setup: Unit is on foam table 80 cm high. Horizontal and Vertical antenna polarities investigated, worst-case reported, unit is continuously transmitting with modulation.

AM Modulation

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02872 | Spectrum Analyzer | E4440A | $11 / 29 / 2021$ | $11 / 29 / 2023$ |
| T2 | ANP06540 | Cable | Heliax | $1 / 17 / 2022$ | $1 / 17 / 2024$ |
| T3 | ANP05305 | Cable | ETSI-50T | $9 / 15 / 2021$ | $9 / 15 / 2023$ |
| T4 | ANP05360 | Cable | RG214 | $2 / 4 / 2022$ | $2 / 4 / 2024$ |
| T5 | AN03628 | Biconilog Antenna | 3142E | $6 / 3 / 2021$ | $6 / 3 / 2023$ |


| Measurement Data: | Reading listed by margin. |  |  |  | Test Distance: 3 Meters |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# Freq | Rdng | T1 | T2 | T3 | T4 | Dist | Corr | Spec | Margin | Polar |
| MHz | $\mathrm{dB} \mu \mathrm{V}$ | dB | dB | dB | dB | Table | $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$ | $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$ | dB | Ant |
| $1 \quad 614.000 \mathrm{M}$ | 8.2 | +0.0 | +0.3 | +1.2 | +1.9 | +0.0 | 38.8 | 46.0 | -7.2 | Vert |
| QP |  | +27.2 |  |  |  |  |  | SC |  |  |
| 2 614.000M | 7.9 | +0.0 | +0.3 | +1.2 | +1.9 | +0.0 | 38.5 | $46.0$ <br> Hopping | -7.5 | Vert |
| QP |  | +27.2 |  |  |  |  |  |  |  |  |
| $3 \quad 960.000 \mathrm{M}$ | 7.9 | +0.0 | +0.3 | +1.5 | +2.4 | +0.0 | 42.8 | $\mathrm{SC}^{54.0}$ | -11.2 | Vert |
| QP |  | +30.7 |  |  |  |  |  |  |  |  |
| $4 \quad 960.000 \mathrm{M}$QP50902.000 M | 7.8 | +0.0 | +0.3 | +1.5 | +2.4 | +0.0 | 42.7 | $54.0$ <br> Hopping | -11.3 | Vert |
|  |  | +30.7 |  |  |  |  |  |  |  |  |
| $5 \quad 902.000 \mathrm{M}$ | 34.4 | +0.0 | +0.3 | +1.4 | +2.3 | +0.0 | 68.0 | $\mathrm{SC}^{113.0}$ | -45.0 | Vert |
|  |  | +29.6 |  |  |  |  |  |  |  |  |
| $6 \quad 928.000 \mathrm{M}$ | 23.5 | +0.0 | +0.3 | +1.5 | +2.4 | +0.0 | 58.3 | 113.0 <br> Hopping | -54.7 | Vert |
|  |  | +30.6 |  |  |  |  |  |  |  |  |
| $7 \quad 928.000 \mathrm{M}$ | 23.4 | +0.0 | +0.3 | +1.5 | +2.4 | +0.0 | 58.2 | $\mathrm{SC}^{113.0}$ | -54.8 | Vert |
|  |  | +30.6 |  |  |  |  |  |  |  |  |
| $8 \quad 902.000 \mathrm{M}$ | 24.6 | +0.0 | +0.3 | +1.4 | +2.3 | +0.0 | 58.2 | 113.0 <br> Hopping | -54.8 | Vert |
|  |  | +29.6 |  |  |  |  |  |  |  |  |

Test Location: $\quad$ CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A • Bothell, WA 98021•(425) 402-1717
Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Itron, Inc.
15.247(d) / 15.209 Radiated Spurious Emissions

107462
Maximized Emissions
Michael Atkinson
EMITest 5.03.20

Date: 10/27/2022
Time: 19:15:23
Sequence\#: 2

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Test Environment Conditions:
Temperature: $24^{\circ} \mathrm{C}$
Humidity: $51 \%$
Pressure: 101.5 kPa

Test Method: ANSI C63.10 (2013)
Frequency: Band Edge
Test Setup: Unit is on foam table 80 cm high. Horizontal and Vertical antenna polarities investigated, worst-case reported, unit is continuously transmitting with modulation.

FM12.5 Modulation

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02872 | Spectrum Analyzer | E4440A | $11 / 29 / 2021$ | $11 / 29 / 2023$ |
| T2 | ANP06540 | Cable | Heliax | $1 / 17 / 2022$ | $1 / 17 / 2024$ |
| T3 | ANP05305 | Cable | ETSI-50T | $9 / 15 / 2021$ | $9 / 15 / 2023$ |
| T4 | ANP05360 | Cable | RG214 | $2 / 4 / 2022$ | $2 / 4 / 2024$ |
| T5 | AN03628 | Biconilog Antenna | 3142E | $6 / 3 / 2021$ | $6 / 3 / 2023$ |



Test Location: $\quad$ CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A • Bothell, WA 98021•(425) 402-1717
Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Itron, Inc.
15.247(d) / 15.209 Radiated Spurious Emissions

107462
Maximized Emissions
Michael Atkinson
EMITest 5.03.20

Date: 10/27/2022
Time: 20:06:55
Sequence\#: 3

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:

```
Test Environment Conditions:
Temperature: }2\mp@subsup{4}{}{\circ}\textrm{C
Humidity: 51%
Pressure: 101.5kPa
Test Method: ANSI C63.10 (2013)
Frequency: Band Edge
Test Setup: Unit is on foam table 80cm high. Horizontal and Vertical antenna polarities investigated, worst-case
reported, unit is continuously transmitting with modulation.
```

FM37.5 Modulation

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :---: | :--- | :--- | :--- | :--- | :--- |
|  | AN02872 | Spectrum Analyzer | E4440A | $11 / 29 / 2021$ | $11 / 29 / 2023$ |
| T1 | ANP06540 | Cable | Heliax | $1 / 17 / 2022$ | $1 / 17 / 2024$ |
| T2 | ANP05305 | Cable | ETSI-50T | $9 / 15 / 2021$ | $9 / 15 / 2023$ |
| T3 | ANP05360 | Cable | RG214 | $2 / 4 / 2022$ | $2 / 4 / 2024$ |
| T4 | AN03628 | Biconilog Antenna | 3142E | $6 / 3 / 2021$ | $6 / 3 / 2023$ |

Measurement Data: $\quad$ Reading listed by margin. Test Distance: 3 Meters

| \#Freq <br>  <br>  <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \text { T3 } \\ & \text { dB } \end{aligned}$ | $\begin{aligned} & \mathrm{T} 4 \\ & \mathrm{~dB} \end{aligned}$ | Dist <br> Table | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \end{gathered}$ | Margin <br> dB | Polar Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 1814.000 \mathrm{M} \\ & \mathrm{QP} \end{aligned}$ | 8.0 | +0.3 | +1.2 | +1.9 | +27.2 | +0.0 | 38.6 | $\text { SC }{ }^{46.0}$ | -7.4 | Vert |
| $\begin{aligned} & 2614.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 7.9 | +0.3 | +1.2 | +1.9 | +27.2 | +0.0 | 38.5 | $\begin{gathered} 46.0 \\ \text { Hopping } \end{gathered}$ <br> Hopping | -7.5 | Vert |
| $\begin{aligned} & 3960.000 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | 8.0 | +0.3 | +1.5 | +2.4 | +30.7 | +0.0 | $42.9$ | $\text { SC }{ }^{54.0}$ | -11.1 | Vert |
| $\begin{aligned} & 4960.000 \mathrm{M} \\ & \mathrm{QP} \end{aligned}$ | 7.9 | +0.3 | +1.5 | +2.4 | +30.7 | +0.0 | 42.8 | $54.0$ <br> Hopping | -11.2 | Vert |
| $5 \quad 902.000 \mathrm{M}$ | 25.1 | +0.3 | +1.4 | +2.3 | +29.6 | +0.0 | 58.7 | $\begin{aligned} & 108.0 \\ & \text { SC } \end{aligned}$ | -49.3 | Vert |
| $6 \quad 902.000 \mathrm{M}$ | 23.7 | +0.3 | +1.4 | +2.3 | +29.6 | +0.0 | 57.3 | $108.0$ <br> Hopping | -50.7 | Vert |
| $7 \quad 928.000 \mathrm{M}$ | 24.2 | +0.3 | +1.5 | +2.4 | +30.6 | +0.0 | 59.0 | $111.0$ <br> Hopping | -52.0 | Vert |
| $8 \quad 928.000 \mathrm{M}$ | 22.9 | +0.3 | +1.5 | +2.4 | +30.6 | +0.0 | 57.7 | SC | -53.3 | Vert |

## Test Setup Photo(s)



Below 1GHz; View 1


Below 1GHz; View 2


Above 1GHz; View 1


Above 1GHz; View 2


GPS Antenna Investigation

LABORATORIES, INC.

### 15.207 AC Conducted Emissions

## Test Setup / Conditions / Data

Test Location: Customer: Specification: Work Order \#: Test Type: Tested By: Software:

CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A • Bothell, WA 98021•(425) 402-1717 Itron, Inc.
15.207 AC Mains - Average

107462
Conducted Emissions
Michael Atkinson
EMITest 5.03.20

Date: 10/26/2022
Time: 19:40:44
Sequence\#: 4
120 V 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Test Environment Conditions:
Temperature: $24^{\circ} \mathrm{C}$
Humidity: $43 \%$
Pressure: 101.9 kPa

Test Method: ANSI C63.10 (2013)
Frequency: $0.15-30 \mathrm{MHz}$
Test Setup: Wi-Fi On (802.11b 2442 MHz ), Cell On (1880MHz), ISM on (FM12.5, 915)

AM, FM12.5, and FM37.5 modulations investigated, worst-case reported. Also investigated with GPS antenna PN 57861-20, investigated with RV50 and RV50x cell modems, worst-case data reported.

Itron, Inc. WO\#: 107462 Sequence\#: 4 Date: 10/26/2022 15.207 AC Mains - Average Test Lead: 120 V 60 Hz Line


|  | Sweep Data |
| :--- | :--- |
| $\times \quad$ QP Readings |  |
|  | Software Version. 5.0320 |

Readings

* Average Readings
1-15.207 AC Mains - Average

Software Version: 5.03.20
0 Peak Readings

- Ambient
2-15.207 AC Mains - Quasi-peak

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :---: | :--- | :--- | :--- | :--- | :--- |
|  | ANO2872 | Spectrum Analyzer | E4440A | $11 / 29 / 2021$ | $11 / 29 / 2023$ |
| T1 | AN02611 | High Pass Filter | HE9615-150K- <br> $50-720 B$ | $1 / 5 / 2022$ | $1 / 5 / 2024$ |
|  |  |  | Heliax | $1 / 17 / 2022$ | $1 / 17 / 2024$ |
| T2 | ANP06540 | Cable | ETSI-50T | $9 / 15 / 2021$ | $9 / 15 / 2023$ |
| T3 | ANP05305 | Cable | $768-10$ | $3 / 23 / 2022$ | $3 / 23 / 2024$ |
| T4 | ANP06219 | Attenuator | 50uH LISN-Line1 (L) | $3816 / 2$ | $2 / 23 / 2022$ |
| T5 | AN01311 | 50uH LISN-Line2 (N) | $3816 / 2$ | $2 / 23 / 2024$ |  |
|  | AN01311 | 50u/2022 | $2 / 23 / 2024$ |  |  |

Measurement Data: Reading listed by margin. Test Lead: Line

| \# | Freq <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~T} 5 \\ & \text { dB } \end{aligned}$ | $\mathrm{T} 2$ $\mathrm{dB}$ | T3 <br> dB | T4 $\mathrm{dB}$ | Dist <br> Table | Corr $\mathrm{dB} \mu \mathrm{V}$ | Spec <br> $\mathrm{dB} \mu \mathrm{V}$ | Margin <br> dB | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $3.433 \mathrm{M}$ <br> e | 24.6 | $\begin{aligned} & +0.0 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 34.0 | 46.0 | -12.0 | Line |
| $\wedge$ | 3.433 M | 42.4 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 51.8 | 46.0 | +5.8 | Line |
| 3 | $3.523 \mathrm{M}$ | 24.4 | $\begin{array}{r} +0.0 \\ +0.1 \\ \hline \end{array}$ | +0.1 | +0.1 | +9.1 | +0.0 | 33.8 | 46.0 | -12.2 | Line |
| $\wedge$ | 3.523 M | 43.2 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 52.6 | 46.0 | +6.6 | Line |
| 5 | 3.535M | 24.4 | $\begin{array}{r} +0.0 \\ +0.1 \\ \hline \end{array}$ | +0.1 | +0.1 | +9.1 | +0.0 | 33.8 | 46.0 | -12.2 | Line |
| $\wedge$ | 3.535 M | 43.3 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 52.7 | 46.0 | +6.7 | Line |
| 7 | $3.699 \mathrm{M}$ <br> e | 24.3 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 33.7 | 46.0 | -12.3 | Line |
| 8 | $3.707 \mathrm{M}$ | 24.2 | $\begin{array}{r} +0.0 \\ +0.1 \\ \hline \end{array}$ | +0.1 | +0.1 | +9.1 | +0.0 | 33.6 | 46.0 | -12.4 | Line |
| $\wedge$ | 3.699M | 44.8 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 54.2 | 46.0 | +8.2 | Line |
| $\wedge$ | 3.707 M | 44.7 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 54.1 | 46.0 | +8.1 | Line |
|  | $3.656 \mathrm{M}$ | 24.1 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 33.5 | 46.0 | -12.5 | Line |
| $\wedge$ | 3.656M | 44.8 | $\begin{aligned} & +0.0 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 54.2 | 46.0 | +8.2 | Line |
|  | $3.332 \mathrm{M}$ | 24.1 | $\begin{array}{r} +0.0 \\ +0.1 \\ \hline \end{array}$ | +0.1 | +0.1 | +9.1 | +0.0 | 33.5 | 46.0 | -12.5 | Line |
| $\wedge$ | 3.332M | 42.3 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 51.7 | 46.0 | +5.7 | Line |
|  | $3.676 \mathrm{M}$ | 24.0 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 33.4 | 46.0 | -12.6 | Line |
| $\wedge$ | 3.676 M | 44.0 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 53.4 | 46.0 | +7.4 | Line |
|  | $3.552 \mathrm{M}$ | 23.8 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 33.2 | 46.0 | -12.8 | Line |
| $\wedge$ | 3.552 M | 43.1 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 52.5 | 46.0 | +6.5 | Line |
|  | $3.575 \mathrm{M}$ | 23.8 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 33.2 | 46.0 | -12.8 | Line |
| $\wedge$ | 3.575 M | 43.0 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 52.4 | 46.0 | +6.4 | Line |
|  | $3.727 \mathrm{M}$ | $23.8$ | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | $+0.1$ | +0.1 | +9.1 | +0.0 | 33.2 | 46.0 | -12.8 | Line |
| $\wedge$ | 3.727 M | 44.9 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 54.3 | 46.0 | +8.3 | Line |


| ${ }^{23}$ Ave $^{3.739 \mathrm{M}}$ |  | 23.6 | $\begin{array}{r} \hline+0.0 \\ +0.1 \\ \hline \end{array}$ | +0.1 | +0.1 | +9.1 | +0.0 | 33.0 | 46.0 | -13.0 | Line |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 3.739M | 44.1 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 53.5 | 46.0 | +7.5 | Line |
| 25 | $\mathrm{e}^{3.597 \mathrm{M}}$ | 23.5 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 32.9 | 46.0 | -13.1 | Line |
| $\wedge$ | 3.597M | 43.2 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 52.6 | 46.0 | +6.6 | Line |
| 27 | $3.777 \mathrm{M}$ | 22.9 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 32.3 | 46.0 | -13.7 | Line |
| $\wedge$ | 3.777M | 44.4 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 53.8 | 46.0 | +7.8 | Line |
| Ave |  | 22.4 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 31.8 | 46.0 | -14.2 | Line |
| $\wedge$ | 3.822M | 42.9 | $\begin{array}{r} \hline+0.0 \\ +0.1 \\ \hline \end{array}$ | +0.1 | +0.1 | +9.1 | +0.0 | 52.3 | 46.0 | +6.3 | Line |
| Ave |  | 22.1 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 31.5 | 46.0 | -14.5 | Line |
| 32 | $\mathrm{e}^{3.855 \mathrm{M}}$ | 22.0 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 31.4 | 46.0 | -14.6 | Line |
| 3.855M |  | 42.7 | $\begin{array}{r} +0.0 \\ +0.1 \\ \hline \end{array}$ | +0.1 | +0.1 | +9.1 | +0.0 | 52.1 | 46.0 | +6.1 | Line |
|  | $3.187 \mathrm{M}$ | 21.8 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 31.2 | 46.0 | -14.8 | Line |
| $\wedge$ | 3.187M | 39.9 | $\begin{aligned} & +0.0 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 49.3 | 46.0 | +3.3 | Line |
| 36 | $\mathrm{e}^{3.867 \mathrm{M}}$ | 21.6 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 31.0 | 46.0 | -15.0 | Line |
| $\wedge$ | 3.867M | 42.5 | $\begin{aligned} & +0.0 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 51.9 | 46.0 | +5.9 | Line |
| $\wedge$ | 3.863M | 42.5 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 51.9 | 46.0 | +5.9 | Line |
| Ave | $3.929 \mathrm{M}$ | 21.3 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 30.7 | 46.0 | -15.3 | Line |
| $\wedge$ | 3.929M | 39.2 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 48.6 | 46.0 | +2.6 | Line |
| 41 | $\mathrm{e}^{3.068 \mathrm{M}}$ | 20.8 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 30.2 | 46.0 | -15.8 | Line |
| $\wedge$ | 3.068M | 38.3 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 47.7 | 46.0 | +1.7 | Line |
| Ave | $\mathrm{e}^{2.957 \mathrm{M}}$ | 20.4 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 29.8 | 46.0 | -16.2 | Line |
| $\wedge$ | 2.957M | 37.1 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 46.5 | 46.0 | +0.5 | Line |


| Ave |  | 19.6 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 29.0 | 46.0 | -17.0 | Line |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 4.003 M | 37.1 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 46.5 | 46.0 | +0.5 | Line |
| Ave |  | 19.2 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 28.6 | 46.0 | -17.4 | Line |
| $\wedge$ | 2.891 M | 36.1 | $\begin{aligned} & +0.0 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 45.5 | 46.0 | -0.5 | Line |
|  | $4.047 \mathrm{M}$ | 18.7 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 28.1 | 46.0 | -17.9 | Line |
| $\wedge$ | 4.047 M | 37.2 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 46.6 | 46.0 | +0.6 | Line |

LABORATORIES, INC.

Test Location: $\quad$ CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A•Bothell, WA 98021•(425) 402-1717
Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Itron, Inc.
15.207 AC Mains - Average

107462
Conducted Emissions
Michael Atkinson
EMITest 5.03.20

Date: 10/26/2022
Time: 19:18:02
Sequence\#: 3
120 V 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Test Environment Conditions:
Temperature: $24^{\circ} \mathrm{C}$
Humidity: $43 \%$
Pressure: 101.9 kPa
Test Method: ANSI C63.10 (2013)
Frequency: $0.15-30 \mathrm{MHz}$
Test Setup: Wi-Fi On (802.11b 2442MHz), Cell On (1880MHz), ISM on (FM12.5, 915)
AM, FM12.5, and FM37.5 modulations investigated, worst-case reported. Also investigated with GPS antenna PN 57861-20, investigated with RV50 and RV50x cell modems, worst-case data reported.

Itron, Inc. WO\#: 107462 Sequence\#: 3 Date: 10/26/2022 15.207 AC Mains - Average Test Lead: 120 V 60 Hz Neutral



Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :---: | :--- | :--- | :--- | :--- | :--- |
|  | ANO2872 | Spectrum Analyzer | E4440A | $11 / 29 / 2021$ | $11 / 29 / 2023$ |
| T1 | AN02611 | High Pass Filter | HE9615-150K- <br> 50-720B | $1 / 5 / 2022$ | $1 / 5 / 2024$ |
|  |  |  | Heliax | $1 / 17 / 2022$ | $1 / 17 / 2024$ |
| T2 | ANP06540 | Cable | ETSI-50T | $9 / 15 / 2021$ | $9 / 15 / 2023$ |
| T3 | ANP05305 | Cable | $768-10$ | $3 / 23 / 2022$ | $3 / 23 / 2024$ |
| T4 | ANP06219 | Attenuator | 50uH LISN-Line1 (L) | $3816 / 2$ | $2 / 23 / 2022$ |
|  | AN01311 | 50uH LISN-Line2 (N) | $3816 / 2$ | $2 / 23 / 2024$ |  |
| T5 | AN01311 | 5020 | $2 / 2022$ | $2 / 23 / 2024$ |  |


| Measu | ent Data | Reading listed by margin. |  |  |  | Test Lead: Neutral |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | Freq | Rdng |  | T2 | T3 | T4 | Dist | Corr | Spec | Margin | Polar |
|  | MHz | $\mathrm{dB} \mu \mathrm{V}$ | dB | dB | dB | dB | Table | $\mathrm{dB} \mu \mathrm{V}$ | $\mathrm{dB} \mu \mathrm{V}$ | dB | Ant |
| 1 | 3.473 M | 24.9 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 34.3 | 46.0 | -11.7 | Neutr |
| Ave |  |  | +0.1 |  |  |  |  |  |  |  |  |
| $\wedge$ | 3.473 M | 42.9 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 52.3 | 46.0 | +6.3 | Neutr |
|  |  |  | +0.1 |  |  |  |  |  |  |  |  |
| 3 | 3.452 M | 24.8 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 34.2 | 46.0 | -11.8 | Neutr |
|  | Ave |  | +0.1 |  |  |  |  |  |  |  |  |
| $\wedge$ | 3.452 M | 42.8 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 52.2 | 46.0 | +6.2 | Neutr |
|  |  |  | +0.1 |  |  |  |  |  |  |  |  |
| 5 | 3.428 M | 24.6 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 34.0 | 46.0 | -12.0 | Neutr |
|  | Ave |  | +0.1 |  |  |  |  |  |  |  |  |
| $\wedge$ | 3.428 M | 43.3 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 52.7 | 46.0 | +6.7 | Neutr |
|  |  |  | +0.1 |  |  |  |  |  |  |  |  |
| 7 | 3.562 M | 24.2 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 33.6 | 46.0 | -12.4 | Neutr |
|  | Ave |  | +0.1 |  |  |  |  |  |  |  |  |
| $\wedge$ | 3.562 M | 41.3 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 50.7 | 46.0 | +4.7 | Neutr |
|  |  |  | +0.1 |  |  |  |  |  |  |  |  |
| 9 | 3.634 M | 24.1 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 33.5 | 46.0 | -12.5 | Neutr |
|  | Ave |  | +0.1 |  |  |  |  |  |  |  |  |
| $\wedge$ | 3.634 M | 43.9 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 53.3 | 46.0 | +7.3 | Neutr |
|  |  |  | +0.1 |  |  |  |  |  |  |  |  |
| 11 | 3.697 M | 24.1 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 33.5 | 46.0 | -12.5 | Neutr |
| Ave |  |  | +0.1 |  |  |  |  |  |  |  |  |
| 12 | 3.618 M | 23.9 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 33.3 | 46.0 | -12.7 | Neutr |
| Ave |  |  | +0.1 |  |  |  |  |  |  |  |  |
| $\wedge$ | 3.618 M | 44.0 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 53.4 | 46.0 | +7.4 | Neutr |
|  |  |  | +0.1 |  |  |  |  |  |  |  |  |
| 14 | 3.732 M | 23.9 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 33.3 | 46.0 | -12.7 | Neutr |
|  | Ave |  | +0.1 |  |  |  |  |  |  |  |  |
| $\wedge$ | 3.732 M | 43.6 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 53.0 | 46.0 | +7.0 | Neutr |
|  |  |  | +0.1 |  |  |  |  |  |  |  |  |
| $16{ }^{16}$ Ave ${ }^{3.707 \mathrm{M}}$ |  | 23.8 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 33.2 | 46.0 | -12.8 | Neutr |
|  |  |  | +0.1 |  |  |  |  |  |  |  |  |
| $\wedge$ | 3.697 M | 45.3 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 54.7 | 46.0 | +8.7 | Neutr |
|  |  |  | +0.1 |  |  |  |  |  |  |  |  |
| $\wedge$ | 3.707 M | 44.7 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 54.1 | 46.0 | +8.1 | Neutr |
|  |  |  | +0.1 |  |  |  |  |  |  |  |  |
| 19 | 3.580 M | 23.6 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 33.0 | 46.0 | -13.0 | Neutr |
|  | Ave |  | +0.1 |  |  |  |  |  |  |  |  |
| $\wedge$ | 3.580 M | 40.4 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 49.8 | 46.0 | +3.8 | Neutr |
|  |  |  | +0.1 |  |  |  |  |  |  |  |  |
| 2 | 3.248M | 23.4 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 32.8 | 46.0 | -13.2 | Neutr |
|  | Ave |  | +0.1 |  |  |  |  |  |  |  |  |
| $\wedge$ | 3.248 M | 40.4 | +0.0 | +0.1 | +0.1 | +9.1 | +0.0 | 49.8 | 46.0 | +3.8 | Neutr |
|  |  |  | +0.1 |  |  |  |  |  |  |  |  |


|  | $3.342 \mathrm{M}$ | 23.4 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 32.8 | 46.0 | -13.2 | Neutr |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 3.342 M | 42.2 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 51.6 | 46.0 | +5.6 | Neutr |
|  | $3.811 \mathrm{M}$ | 22.5 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 31.9 | 46.0 | -14.1 | Neutr |
| $\wedge$ | 3.811 M | 43.9 | $\begin{aligned} & +0.0 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 53.3 | 46.0 | +7.3 | Neutr |
| 27 | 3.870M | 21.9 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 31.3 | 46.0 | -14.7 | Neutr |
| $\wedge$ | 3.870 M | 41.8 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 51.2 | 46.0 | +5.2 | Neutr |
|  | $3.860 \mathrm{M}$ | 21.8 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 31.2 | 46.0 | -14.8 | Neutr |
| $\wedge$ | 3.860 M | 41.7 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 51.1 | 46.0 | +5.1 | Neutr |
|  | 3.890M | 21.7 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 31.1 | 46.0 | -14.9 | Neutr |
| $\wedge$ | 3.890 M | 41.4 | $\begin{aligned} & +0.0 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 50.8 | 46.0 | +4.8 | Neutr |
|  | $3.108 \mathrm{M}$ <br> e | 21.4 | $\begin{aligned} & +0.0 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 30.8 | 46.0 | -15.2 | Neutr |
| $\wedge$ | 3.108M | 38.1 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 47.5 | 46.0 | +1.5 | Neutr |
|  | $3.125 \mathrm{M}$ | 21.1 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 30.5 | 46.0 | -15.5 | Neutr |
| $\wedge$ | 3.125 M | 38.6 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 48.0 | 46.0 | +2.0 | Neutr |
|  | $3.079 \mathrm{M}$ | 20.9 | $\begin{array}{r} +0.0 \\ +0.1 \\ \hline \end{array}$ | +0.1 | +0.1 | +9.1 | +0.0 | 30.3 | 46.0 | -15.7 | Neutr |
| $\wedge$ | 3.079 M | 37.3 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 46.7 | 46.0 | +0.7 | Neutr |
|  | $3.036 \mathrm{M}$ | 20.8 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 30.2 | 46.0 | -15.8 | Neutr |
| $\wedge$ | 3.036 M | 37.2 | $\begin{aligned} & +0.0 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 46.6 | 46.0 | +0.6 | Neutr |
|  | $3.945 \mathrm{M}$ | 20.7 | $\begin{aligned} & +0.0 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 30.1 | 46.0 | -15.9 | Neutr |
| $\wedge$ | 3.945M | 38.4 | $\begin{aligned} & +0.0 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 47.8 | 46.0 | +1.8 | Neutr |
|  | $3.970 \mathrm{M}$ | 20.3 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 29.7 | 46.0 | -16.3 | Neutr |
| $\wedge$ | 3.970 M | 36.8 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 46.2 | 46.0 | +0.2 | Neutr |
|  | 3.059M | 20.3 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 29.7 | 46.0 | -16.3 | Neutr |
| $\wedge$ | 3.059 M | 37.1 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 46.5 | 46.0 | +0.5 | Neutr |
|  | $2.961 \mathrm{M}$ | 19.9 | $\begin{aligned} & +0.0 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 29.3 | 46.0 | -16.7 | Neutr |
| $\wedge$ | 2.961 M | 36.8 | $\begin{array}{r} +0.0 \\ +0.1 \\ \hline \end{array}$ | $+0.1$ | +0.1 | +9.1 | +0.0 | 46.2 | 46.0 | +0.2 | Neutr |

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| Ave |  | 19.3 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 28.7 | 46.0 | -17.3 | Neutr |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 4.017 M | 37.5 | $\begin{array}{r} +0.0 \\ +0.1 \\ \hline \end{array}$ | +0.1 | +0.1 | +9.1 | +0.0 | 46.9 | 46.0 | +0.9 | Neutr |
| Ave | $\mathrm{e}^{2.902 \mathrm{M}}$ | 19.0 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | +0.0 | 28.4 | 46.0 | -17.6 | Neutr |
| $\wedge$ | 2.902 M | 35.6 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.1 | +0.1 | +9.1 | $+0.0$ | 45.0 | 46.0 | -1.0 | Neutr |

Test Setup Photo(s)


LABORATORIES, INC.

## Appendix A: Customer Provided Data

### 15.35(c) Duty Cycle Correction Factor

| Test Data Summary |  |  |  |
| :---: | :---: | :---: | :---: |
| Antenna <br> Port | Operational Mode | Measured On Time <br> $(\mathrm{mS} /$ Pobs) | Declared DCCF <br> (dB) |
| 1 | Operating | 23.8 | 12.5 |

Observation Period, Pobs is the duration of the pulse train or maximum 100 mS

Measured results are calculated as follows:

$$
\text { On Time }=\left.\left(\sum_{\text {Bursts }} R F \text { Burst On Time }+\sum_{\text {Control }} \text { Control Signal On time }\right)\right|_{P_{o b s}(\max 100 \mathrm{~ms})}
$$

Measured Values:

| Parameter | Value |
| :--- | :--- |
| Observation Period (Pobs): | 100 |
| Number of RF Bursts / Pobs:: | 1 |
| On time of RF Burst: | 23.8 |
| Number of Control or other signals / Pobs: | 0 |
| On time of Control or other Signals: | 0 |
| Total Measured On Time: | 23.8 |

Duty Cycle Correction Factor (DCCF) is calculated in accordance with ANSI C63.10:

$$
D C C F=20 \cdot \log \left(\frac{\text { On Time }}{P_{\text {obs }}}\right)
$$

## Duty Cycle Correction Factor Test Data



## SUPPLEMENTAL INFORMATION

## Measurement Uncertainty

| Uncertainty Value | Parameter |
| :---: | :---: |
| 4.73 dB | Radiated Emissions |
| 3.34 dB | Mains Conducted Emissions |
| 3.30 dB | Disturbance Power |

Uncertainties reported are worst-case for all CKC Laboratories' sites and represent expanded uncertainties expressed at approximately the $95 \%$ confidence level using a coverage factor of $\mathrm{k}=2$. Compliance is deemed to occur provided measurements are below the specified limits.

## Emissions Test Details

## TESTING PARAMETERS

Unless otherwise indicated, the following configuration parameters are used for equipment setup: The cables were routed consistent with the typical application by varying the configuration of the test sample. Interface cables were connected to the available ports of the test unit. The effect of varying the position of the cables was investigated to find the configuration that produced maximum emissions. Cables were of the type and length specified in the individual requirements. The length of cable that produced maximum emissions was selected.

The equipment under test (EUT) was set up in a manner that represented its normal use, as shown in the setup photographs. Any special conditions required for the EUT to operate normally are identified in the comments that accompany the emissions tables.

The emissions data was taken with a spectrum analyzer or receiver. Incorporating the applicable correction factors for distance, antenna, cable loss and amplifier gain, the data was reduced as shown in the table below. The corrected data was then compared to the applicable emission limits. Preliminary and final measurements were taken in order to ensure that all emissions from the EUT were found and maximized.

## CORRECTION FACTORS

The basic spectrum analyzer reading was converted using correction factors as shown in the highest emissions readings in the tables. For radiated emissions in $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$, the spectrum analyzer reading in $\mathrm{dB} \mu \mathrm{V}$ was corrected by using the following formula. This reading was then compared to the applicable specification limit. Individual measurements were compared with the displayed limit value in the margin column. The margin was calculated based on subtracting the limit value from the corrected measurement value; a positive margin represents a measurement exceeding the limit, while a negative margin represents a measurement less than the limit.

| SAMPLE CALCULATIONS |  |  |  |
| :--- | :--- | :--- | :---: |
|  | Meter reading | $(\mathrm{dB} \mu \mathrm{V})$ |  |
| + | Antenna Factor | $(\mathrm{dB} / \mathrm{m})$ |  |
| + | Cable Loss | $(\mathrm{dB})$ |  |
| - | Distance Correction | $(\mathrm{dB})$ |  |
| - | Preamplifier Gain | $(\mathrm{dB})$ |  |
| $=$ | Corrected Reading | $(\mathrm{dB} \mu \mathrm{V} / \mathrm{m})$ |  |

## TEST INSTRUMENTATION AND ANALYZER SETTINGS

The test instrumentation and equipment listed were used to collect the emissions data. A spectrum analyzer or receiver was used for all measurements. Unless otherwise specified, the following table shows the measuring equipment bandwidth settings that were used in designated frequency bands. For testing emissions, an appropriate reference level and a vertical scale size of 10 dB per division were used.

| MEASURING EQUIPMENT BANDWIDTH SETTINGS PER FREQUENCY RANGE |  |  |  |
| :---: | :---: | :---: | :---: |
| TEST | BEGINNING FREQUENCY | ENDING FREQUENCY | BANDWIDTH SETTING |
| CONDUCTED EMISSIONS | 150 kHz | 30 MHz | 9 kHz |
| RADIATED EMISSIONS | 9 kHz | 150 kHz | 200 Hz |
| RADIATED EMISSIONS | 150 kHz | 30 MHz | 9 kHz |
| RADIATED EMISSIONS | 30 MHz | 1000 MHz | 120 kHz |
| RADIATED EMISSIONS | 1000 MHz | $>1 \mathrm{GHz}$ | 1 MHz |

## SPECTRUM ANALYZER/RECEIVER DETECTOR FUNCTIONS

The notes that accompany the measurements contained in the emissions tables indicate the type of detector function used to obtain the given readings. Unless otherwise noted, all readings were made in the "positive peak" detector mode. Whenever a "quasi-peak" or "average" reading was recorded, the measurement was annotated with a "QP" or an "Ave" on the appropriate rows of the data sheets. In cases where quasi-peak or average limits were employed and data exists for multiple measurement types for the same frequency then the peak measurement was retained in the report for reference, however the numbering for the affected row was removed and an arrow or caret ("^") was placed in the far left-hand column indicating that the row above takes precedence for comparison to the limit. The following paragraphs describe in more detail the detector functions and when they were used to obtain the emissions data.

## Peak

In this mode, the spectrum analyzer or receiver recorded all emissions at their peak value as the frequency band selected was scanned. By combining this function with another feature called "peak hold," the measurement device had the ability to measure intermittent or low duty cycle transient emission peak levels. In this mode the measuring device made a slow scan across the frequency band selected and measured the peak emission value found at each frequency across the band.

## Quasi-Peak

Quasi-peak measurements were taken using the quasi-peak detector when the true peak values exceeded or were within 2 dB of a quasi-peak specification limit. Additional QP measurements may have been taken at the discretion of the operator.

## Average

Average measurements were taken using the average detector when the true peak values exceeded or were within 2 dB of an average specification limit. Additional average measurements may have been taken at the discretion of the operator. If the specification or test procedure requires trace averaging, then the averaging was performed using 100 samples or as required by the specification. All other average measurements are performed using video bandwidth averaging. To make these measurements, the test engineer reduces the video bandwidth on the measuring device until the modulation of the signal is filtered out. At this point the measuring device is set into the linear mode and the scan time is reduced.

