# Itron, Inc. 

TEST REPORT FOR

> SRR+RV50WWAN+WIFI+GPSRx Models: CCU100B, CCU100B Repeater, CCU100RB \& CCU100RB Repeater

Tested to The Following Standards:

FCC Part 15 Subpart C, Section: 15.247
(FHSS 902-928 MHz)

Report No.: 98384-15

Date of issue: May 25, 2016


Testing Certificates: 803.01, 803.02, 803.05, 803.06

This test report bears the accreditation symbol indicating that the testing performed herein meets the test and reporting requirements of ISO/IEC 17025 under the applicable scope of EMC testing for CKC Laboratories, Inc.

We strive to create long-term, trust based relationships by providing sound, adaptive, customer first testing services. We embrace each of our customers' unique EMC challenges, not as an interruption to set processes, but rather as the reason we are in business.

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# ADMINISTRATIVE INFORMATION 

## Test Report Information

## REPORT PREPARED FOR:

Iron, Inc.
2111 N. Molter Road
Liberty Lake, WA 99019

Representative: Jay Holcomb
Customer Reference Number: 96653

DATE OF EQUIPMENT RECEIPT:
DATES) OF TESTING:

REPORT PREPARED BY:

Dianne Dudley
CKC Laboratories, Inc.
5046 Sierra Pines Drive
Mariposa, CA 95338

Project Number: 98384

May 11, 2016
May 11-13, 2016

## Report Authorization

The test data contained in this report documents the observed testing parameters pertaining to and are relevant for only the sample equipment tested in the agreed upon operational modes) and configurations) as identified herein. Compliance assessment remains the client's responsibility. This report may not be used to claim product endorsement by A2LA or any government agencies. This test report has been authorized for release under quality control from CKC Laboratories, Inc.


Steve Behm
Director of Quality Assurance \& Engineering Services CKC Laboratories, Inc.

## Test Facility Information



Our laboratories are configured to effectively test a wide variety of product types. CKC utilizes first class test equipment, anechoic chambers, data acquisition and information services to create accurate, repeatable and affordable test results.

TEST LOCATION(S):
CKC Laboratories, Inc.
22116 23rd Drive S.E., Suite A
Bothell, WA 98021-4413

## Software Versions

| CKC Laboratories Proprietary Software | Version |
| :--- | :---: |
| EMITest Emissions | 5.03 .02 |

## Site Registration \& Accreditation Information

| Location | CB \# | TAIWAN | CANADA | FCC | JAPAN |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Bothell | USO081 | SL2-IN-E-1145R | $3082 \mathrm{C}-1$ | 318736 | A-0148 |

LABORATORIES, INC.

## SUMMARY OF RESULTS

Standard / Specification: FCC Part 15 Subpart C-15.247 (FHSS 902-928MHz)

| Test Procedure | Description | Modifications | Results |
| :--- | :--- | :--- | :--- |
| $15.247(\mathrm{a})(1)(\mathrm{i})$ | Occupied Bandwidth | NA | NP |
| $15.247(\mathrm{a})(1)$ | Carrier Separation | NA | NP |
| $15.247(\mathrm{a})(1)(\mathrm{i})$ | Number of Hopping Channels | NA | NP |
| $15.247(\mathrm{a})(1)(\mathrm{i})$ | Average Time of Occupancy | NA | NP |
| $15.247(\mathrm{~b})(2)$ | Output Power | NA | NP |
| $15.247(\mathrm{~d})$ | RF Conducted Emissions \& Band Edge | NA | Pass |
| $15.247(\mathrm{~d})$ | Radiated Emissions \& Band Edge | NA | NA |
| 15.207 | AC Conducted Emissions | NA | NP |

NA = Not applicable.
NP = Not performed because CKC was not contracted to perform the required testing.

## Modifications During Testing

This list is a summary of the modifications made to the equipment during testing.

## Summary of Conditions

No modifications were made during testing.

Modifications listed above must be incorporated into all production units.

## Conditions During Testing

This list is a summary of the conditions noted to the equipment during testing.

## Summary of Conditions

None

## EQUIPMENT UNDER TEST (EUT)

The following model was tested by CKC Laboratories: CCU100RB

During previous testing it was found that the two devices with a cellular modem had a much worse emissions profile than without a cellular modem in the device. The difference between the repeater versions of these devices and the non-repeater versions is that the repeater versions do not have a cellular modem in them. Therefore, the manufacturer claims that any difference between the following devices without modem in them do not affect their EMC characteristics, and therefore meet the level of testing equivalent to the tested models: CCU100B, CCU100B Repeater and CCU100RB Repeater

For the CCU family, these have the same ISM transmitter as what was tested, except they have a Tx/Rx switch with more loss. So the CCUB tested would be worse case, less attenuation to the antenna. For the CCUA family, these have the identical ISM transmitter as what was tested. Therefore, the manufacturer claims that any difference between the following devices do not affect their EMC characteristics, and therefore meet the level of testing equivalent to the tested models:

```
CCU100, CCU100R, CCU100 Repeater, CCU100R Repeater, CCU100A, CCU100AR, CCU100A Repeater and
CCU100AR Repeater
```

During testing numerous configurations may have been utilized. The configurations listed below support compliance to the standard(s) listed in the Summary of Results section.

## Configuration 2

Equipment Tested:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| SRR+RV50WWAN+WIFI+GPSRx | Itron, Inc. | CCU100RB | NA |

Support Equipment:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| High Gain V-Pol Omni | PC Tel | BOA9028 | NA |
| External WWAN Antenna | Taoglas | OMB.6912.03F21 | NA |
| GPS Antenna | Trimble | $57861-00$ | 213100611 |
| Attenuator | Pasternack | $7000-2$ | NA |
| Lightning Protector | iPolyPhaser | DSXL-ME | NA |

## General Product Information:

| Product Information | Manufacturer-Provided Details |
| :---: | :---: |
| Equipment Type: | Stand-Alone Equipment |
| Type of Wideband System: | Proprietary FHSS |
| Operating Frequency Range: | $903-926.8 \mathrm{MHz}$ |
| Number of Hopping Channels: | 120 |
| Modulation Type(s): | $16 \mathrm{Kbit} / \mathrm{sec}$ AM (OOK), 12.5 Kbit/sec FM (2GFSK), $37.5 \mathrm{Kbit} / \mathrm{sec}$ FM (2GFSK) |
| Maximum Duty Cycle: | 23.5\% |
| Number of TX Chains: | 1 |
| Antenna Type(s) and Gain: | Monopole, 6.15 dBi (8.15dBi with 2 dB attenuation) <br> Note: The Manufacturer declares that a minimum of 2.0 dB attenuation is always required when these units are using the 8.15 dBi High Gain V-Pol Omni antenna. |
| Beamforming Type: | NA |
| Antenna Connection Type: | External Connector |
| Nominal Input Voltage: | 100-250VAC, $50-60 \mathrm{~Hz}$ |
| Firmware / Software used for Test: | 10.02-06 |

## FCC Part 15 Subpart C

### 15.247(d) Radiated Emissions \& Band Edge

| Test Setup/Conditions |  |  |  |  |
| :--- | :--- | :--- | :--- | :---: |
| Test Location: | Bothell Lab C3 | Test Engineer: | M. Atkinson |  |
| Test Method: | ANSI C63.10 (2013) | Test Date(s): | $5 / 11 / 16$ to $5 / 13 / 16$ |  |
| Configuration: | 2 |  |  |  |


| Environmental Conditions |  |  |  |
| :---: | :---: | :---: | :---: |
| Temperature (으) | $21-25$ | Relative Humidity (\%): | $30-35$ |

See data sheets for test setup and test equipment.

## Test Data

Test Location: CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A • Bothell, WA. 98021•1-800-500-4EMC

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

## Itron, Inc.

15.247(d) / 15.209 Radiated Spurious Emissions

98384 Date: 5/13/2016
Maximized Emissions
Michael Atkinson
EMITest 5.03.02

Time: 12:38:56
Sequence\#: 21

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

## Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

## Test Conditions / Notes:

Temperature: $25^{\circ} \mathrm{C}$
Humidity: $31 \%$
Pressure: 102.1 kPa

Frequency tested: $9 \mathrm{kHz}-13 \mathrm{GHz}$
Firmware power setting: Max Power
EUT Firmware: 10.02-06
Modulation: AM
Antenna type: Monopole
Antenna Gain: 6.15 dBi ( 8.15 dBi with 2 dB attenuator)
Duty Cycle: Measured with $100 \%$ (end use limited to $23.5 \%$ duty)
Test Method: ANSI C63.10 (2013)
Setup: The EUT is a 900 MHz range radio. EUT is transmitting continuously modulated. 900 MHz antenna is connected using approximately 2.5 m of $1 / 2$ inch Andrews Heliax FS14-50B cable, along with 2 dB attenuator and lightning protector. The EUT antenna height set to stay within test volume boundaries. Both antenna polarities investigated, only worst case reported. The Power output validated to be within manufacturer tolerances.

Wifi transmitter on EUT marked as ambient, this is the fundamental from the integrated certified module in the EUT which is to be excluded from the measurement limits. All average data points marked Low, Mid, High have duty cycle correction applied ( $23.87 \%,-12.44 \mathrm{~dB}$ ).

Itron, Inc WO\#: 98384 Sequence\#: 21 Date: 5/13/2016 15.247 (d) / 15.209 Radiated Spurious Emissions Test Distance: 3 Meters $\mathrm{H}+\mathrm{V}$


[^0]O Peak Readings

* Average Readings

Software Version: 5.03.02

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :---: | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02872 | Spectrum Analyzer | E4440A | $11 / 18 / 2015$ | $11 / 18 / 2017$ |
| T2 | ANP06540 | Cable | Heliax | $10 / 29 / 2015$ | $10 / 29 / 2017$ |
| T3 | ANP05305 | Cable | ETSI-50T | $2 / 15 / 2016$ | $2 / 15 / 2018$ |
| T4 | AN03540 | Preamp | 83017 A | $4 / 30 / 2015$ | $4 / 30 / 2017$ |
| T5 | AN01467 | Horn Antenna- <br> ANSI C63.5 <br> Calibration | 3115 | $8 / 12 / 2015$ | $8 / 12 / 2017$ |
|  |  | Cable |  |  |  |
| T6 | ANP06935 |  | $32026-29801-$ | $3 / 11 / 2016$ | $3 / 11 / 2018$ |
| T7 | AN03170 | High Pass Filter | HM1155-11SS | $12 / 17 / 2015$ | $12 / 17 / 2017$ |
| T8 | AN02307 | Preamp | $8447 D$ | $2 / 15 / 2016$ | $2 / 15 / 2018$ |
| T9 | ANP05360 | Cable | RG214 | $12 / 1 / 2014$ | $12 / 1 / 2016$ |
| T10 | ANP05963 | Cable | RG-214 | $2 / 15 / 2016$ | $2 / 15 / 2018$ |
| T11 | AN01994 | Biconilog Antenna | CBL6111C | $3 / 11 / 2016$ | $3 / 11 / 2018$ |
| T12 | ANP05505 | Attenuator | NAT-6 | $3 / 31 / 2016$ | $3 / 31 / 2018$ |
| T13 | ANP06219 | Attenuator | $768-10$ | $4 / 12 / 2016$ | $4 / 12 / 2018$ |
| T14 | AN00052 | Loop Antenna | 6502 | $4 / 8 / 2016$ | $4 / 8 / 2018$ |
| T15 | ANDCCF | Test Data |  | $5 / 13 / 2016$ | $5 / 13 / 2018$ |
|  |  | Adjustment |  |  |  |

Measurement Data: $\quad$ Reading listed by margin.
Test Distance: 3 Meters


| $\begin{aligned} & 5 \quad 116.837 \mathrm{M} \\ & \mathrm{QP} \end{aligned}$ | 38.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.6 \\ & +9.1 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +1.2 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +11.8 \\ +0.0 \end{array}$ | $\begin{array}{r} +0.0 \\ -27.6 \\ +6.1 \end{array}$ | +0.0 | 39.3 | 43.5 | -4.2 | $\mathrm{H}+\mathrm{V}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge 116.800 \mathrm{M}$ | 41.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 41.9 | 43.5 | -1.6 | H+V |
| $\begin{aligned} & 77320.070 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 53.5 | $\begin{array}{r} +0.0 \\ +36.1 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.2 \\ & +0.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{gathered} +4.7 \\ +0.0 \\ +0.0 \\ -12.4 \end{gathered}$ | $\begin{array}{r} \hline-34.6 \\ +0.0 \\ +0.0 \end{array}$ |  | 49.1 | $\begin{aligned} & \quad 54.0 \\ & \text { MID } \end{aligned}$ | -4.9 | $\mathrm{H}+\mathrm{V}$ |
| $\wedge 7320.070 \mathrm{M}$ | 61.5 | $\begin{array}{r} +0.0 \\ +36.1 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.2 \\ & +0.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +4.7 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-34.6 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 69.5 | $\begin{aligned} & \quad 54.0 \\ & \text { MID } \end{aligned}$ | +15.5 | H+V |
| $\begin{aligned} & 97414.231 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 51.2 | $\begin{array}{r} +0.0 \\ +36.5 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.3 \\ & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+4.8 \\ +0.0 \\ +0.0 \\ -12.4 \\ \hline \end{array}$ | $\begin{array}{r} \hline-34.7 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 47.3 | $\begin{gathered} 54.0 \\ \text { HIGH } \end{gathered}$ | -6.7 | H+V |
| $\wedge 7414.231 \mathrm{M}$ | 61.2 | $\begin{array}{r} +0.0 \\ +36.5 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.3 \\ & +0.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+4.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-34.7 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 69.7 | $\begin{aligned} & \hline 54.0 \\ & \text { HIGH } \end{aligned}$ | +15.7 | H+V |
| $\begin{aligned} & 112440.000 \mathrm{M} \\ & \text { Ambient } \end{aligned}$ | 96.1 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.6 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +2.9 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 99.6 | 110.7 | -11.1 | H+V |
| $\begin{aligned} & 125417.932 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 49.4 | $\begin{array}{r} +0.0 \\ +33.1 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.0 \\ & +0.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +4.5 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-34.2 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 42.0 | $\begin{aligned} & \text { 54.0 } \\ & \text { LOW } \end{aligned}$ | -12.0 | H+V |
| $\wedge 5417.910 \mathrm{M}$ | 56.4 | $\begin{array}{r} +0.0 \\ +33.1 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.0 \\ & +0.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +4.5 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} -34.2 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 61.4 | $\begin{aligned} & 54.0 \\ & \text { LOW } \end{aligned}$ | +7.4 | H+V |
| $\begin{aligned} & 148235.000 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 45.0 | $\begin{array}{r} +0.0 \\ +36.7 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.3 \\ & +0.7 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +5.3 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-35.1 \\ +0.0 \\ +0.0 \end{array}$ |  | 41.5 | $\begin{aligned} & \text { 54.0 } \\ & \text { MID } \end{aligned}$ | -12.5 | H+V |
| $\wedge 8235.000 \mathrm{M}$ | 53.7 | $\begin{array}{r} +0.0 \\ +36.7 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.3 \\ & +0.7 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+5.3 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-35.1 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 |  | $\begin{aligned} & \quad 54.0 \\ & \text { MID } \end{aligned}$ | +8.6 | H+V |
| $\begin{aligned} & 164515.020 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | $48.9$ | $\begin{array}{r} +0.0 \\ +32.5 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +4.2 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-34.1 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 40.5 | $\begin{aligned} & 54.0 \\ & \text { LOW } \end{aligned}$ | -13.5 | H+V |
| ^ 4515.020 M | 55.8 | $\begin{array}{r} +0.0 \\ +32.5 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+4.2 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline-34.1 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 59.8 | $\begin{aligned} & 54.0 \\ & \text { LOW } \end{aligned}$ | +5.8 | H+V |

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| $\begin{aligned} & 18 \text { 8126.980M } \\ & \text { Ave } \end{aligned}$ | 43.5 | $\begin{array}{r} +0.0 \\ +36.7 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.3 \\ & +0.7 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +5.3 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-35.1 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 40.0 | $\begin{aligned} & \text { 54.0 } \\ & \text { LOW } \end{aligned}$ | -14.0 | $\mathrm{H}+\mathrm{V}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ^ 8126.980M | 49.6 | $\begin{array}{r} +0.0 \\ +36.7 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.3 \\ & +0.7 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +5.3 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-35.1 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 58.5 | $\begin{aligned} & 54.0 \\ & \text { LOW } \end{aligned}$ | +4.5 | H+V |
| $\begin{aligned} & 208341.179 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 43.0 | $\begin{array}{r} +0.0 \\ +36.6 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.4 \\ & +0.7 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +5.4 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-35.0 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 39.7 | $\begin{gathered} \hline 54.0 \\ \text { HIGH } \end{gathered}$ | -14.3 | $\mathrm{H}+\mathrm{V}$ |
| ^ 8341.180M | 50.5 | $\begin{array}{r} +0.0 \\ +36.6 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.4 \\ & +0.7 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+5.4 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} -35.0 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 59.6 | $$ | +5.6 | H+V |
| $22 \quad 1189.000 \mathrm{M}$ | 47.9 | $\begin{array}{r} +0.0 \\ +24.2 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.4 \\ & +0.3 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +2.0 \\ & +1.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-36.6 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 39.4 | 54.0 | -14.6 | H+V |
| $\begin{aligned} & 23 \text { 3659.970M } \\ & \text { Ave } \end{aligned}$ | 49.8 | $\begin{array}{r} +0.0 \\ +29.9 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.7 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.7 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-34.2 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 38.0 | $\begin{aligned} & \text { 54.0 } \\ & \text { MID } \end{aligned}$ | -16.0 | $\mathrm{H}+\mathrm{V}$ |
| $\begin{aligned} & 242780.222 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 50.9 | $\begin{array}{r} +0.0 \\ +28.9 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.7 \\ & +0.4 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +3.0 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-34.5 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 37.0 | $\begin{gathered} 54.0 \\ \text { HIGH } \end{gathered}$ | -17.0 | $\mathrm{H}+\mathrm{V}$ |
| ^ 2780.222M | 57.6 | $\begin{array}{r} +0.0 \\ +28.9 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.7 \\ & +0.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +3.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} -34.5 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 56.1 | $\begin{gathered} \hline 54.0 \\ \text { HIGH } \end{gathered}$ | +2.1 | H+V |
| $\begin{gathered} 263707.290 \mathrm{M} \\ \text { Ave } \end{gathered}$ | 48.3 | $\begin{array}{r} +0.0 \\ +30.1 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.7 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.8 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-34.1 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 36.9 | $\begin{gathered} \hline 54.0 \\ \text { HIGH } \end{gathered}$ | -17.1 | H+V |
| ^ 3707.200M | 55.6 | $\begin{array}{r} +0.0 \\ +30.1 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.7 \\ & +0.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +3.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline-34.1 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 56.6 | $\begin{gathered} \hline 54.0 \\ \text { HIGH } \end{gathered}$ | +2.6 | H+V |
| $\begin{aligned} & 28 \text { 9150.050M } \\ & \text { Ave } \end{aligned}$ | 36.0 | $\begin{array}{r} +0.0 \\ +37.7 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +1.4 \\ & +0.7 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +6.1 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-34.7 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 34.8 | $\begin{aligned} & \quad 54.0 \\ & \text { MID } \end{aligned}$ | -19.2 | H+V |
| ^ 9150.050M | 44.6 | $\begin{array}{r} +0.0 \\ +37.7 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.4 \\ & +0.7 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +6.1 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-34.7 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 55.8 | $\begin{aligned} & \text { 54.0 } \\ & \text { MID } \end{aligned}$ | +1.8 | H+V |


| $\begin{gathered} 303611.915 \mathrm{M} \\ \text { Ave } \end{gathered}$ |  | 45.8 | +0.0 | +0.8 | +3.6 | -34.2 | ${ }^{+0.0}$ | 33.8 | 54.0 | -20.2 | H+V |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | +29.8 | +0.4 | +0.0 | $+0.0$ |  |  | LOW |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  | $+0.0$ | +0.0 | -12.4 |  |  |  |  |  |  |
| $\wedge$ | 3611.915M |  | 52.6 | +0.0 | +0.8 | +3.6 | -34.2 | +0.0 | 53.0 | 54.0 | -1.0 | H+V |
|  |  |  |  | +29.8 | +0.4 | +0.0 | $+0.0$ |  |  | LOW |  |  |
|  |  |  |  | +0.0 | +0.0 | +0.0 | $+0.0$ |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 32 | 3659.430M | 43.1 | +0.0 | +0.7 | +3.7 | -34.2 | $+0.0$ | 31.3 | ${ }^{54.0}$ | -22.7 | $\mathrm{H}+\mathrm{V}$ |  |
|  | Ave |  | +29.9 | +0.5 | $+0.0$ | $\begin{aligned} & +0.0 \\ & +0.0 \end{aligned}$ |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | -12.4 |  |  |  |  |  |  |  |
| $\wedge$ | 3659.430M | 57.3 | +0.0 | +0.7 | +3.7 | -34.2 | ${ }^{+0.0}$ | 57.9 | $\begin{aligned} & \hline 54.0 \\ & \text { MID } \end{aligned}$ | +3.9 | H+V |  |
|  |  |  | +29.9 | +0.5 | +0.0 | $\begin{array}{r} +0.0 \\ +0.0 \end{array}$ |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |  |
| $\begin{aligned} & 34 \text { 9029.894M } \\ & \text { Ave } \end{aligned}$ |  | 32.4 | +0.0 | +1.3 | +6.0 | -34.6 | +0.0 | 31.2 | $\begin{aligned} & 54.0 \\ & \text { LOW } \end{aligned}$ | -22.8 | H+V |  |
|  |  | +37.8 | +0.7 | $+0.0$ | +0.0 |  |  |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | $+0.0$ |  |  |  |  |  |  |  |
|  |  | +0.0 | +0.0 | -12.4 |  |  |  |  |  |  |  |  |
|  | ^ 9029.894M |  | 42.0 | +0.0 | +1.3 | +6.0 | -34.6 | +0.0 | 53.2 | $\begin{aligned} & 54.0 \\ & \text { LOW } \end{aligned}$ | -0.8 | H+V |
|  |  |  |  | +37.8 | +0.7 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  |  | +0.0 | +0.0 | +0.0 | $+0.0$ |  |  |  |  |  |
|  |  | +0.0 |  | +0.0 | +0.0 |  |  |  |  |  |  |  |
| 36 | $\begin{aligned} & 36 \text { 4870.000M } \\ & \text { Ave } \end{aligned}$ | 25.9 | +0.0 | +0.9 | +4.3 | $\begin{gathered} -34.2 \\ +0.0 \\ +0.0 \end{gathered}$ | ${ }^{+0.0}$ | 30.6 | 54.0 | -23.4 | H+V |  |
|  |  |  | +32.7 | +0.5 | +0.5 |  |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | $+0.0$ |  |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |  |
|  | 4870.000M | 49.9 | +0.0 | +0.9 | +4.3 | $\begin{aligned} & \hline-34.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 54.1 | 54.0 | +0.1 | H+V |  |
| $\wedge$ |  |  | +32.7 | +0.5 | +0.0 |  |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |  |
| $\begin{aligned} & 382745.090 \mathrm{M} \\ & \text { Ave } \end{aligned}$ |  | 44.3 | +0.0 | +0.7 | +3.0 | -34.5 | +0.0 | 30.3 | $\begin{aligned} & \quad 54.0 \\ & \text { MID } \end{aligned}$ | -23.7 | H+V |  |
|  |  | +28.8 | +0.4 | +0.0 | +0.0 |  |  |  |  |  |  |  |
|  |  | +0.0 | +0.0 | $+0.0$ | $+0.0$ |  |  |  |  |  |  |  |
|  |  | +0.0 | +0.0 | -12.4 |  |  |  |  |  |  |  |  |
| $\wedge$ | 2745.090M |  | 52.3 | +0.0 | +0.7 | +3.0 | $\begin{gathered} -34.5 \\ +0.0 \\ +0.0 \end{gathered}$ | +0.0 | 50.7 | $\begin{aligned} & \quad 54.0 \\ & \text { MID } \end{aligned}$ | -3.3 | H+V |
|  |  |  |  | +28.8 | +0.4 | $+0.0$ |  |  |  |  |  |  |
|  |  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
|  |  | +0.0 |  | +0.0 | +0.0 |  |  |  |  |  |  |  |
| $\begin{aligned} & 40 \quad 2709.020 \mathrm{M} \\ & \text { Ave } \end{aligned}$ |  | 41.9 | +0.0 | +0.7 | +3.0 | -34.5 | +0.0 | 27.7 | $\begin{aligned} & \hline 54.0 \\ & \text { LOW } \end{aligned}$ | -26.3 | H+V |  |
|  |  | +28.6 | +0.4 | +0.0 | $\begin{aligned} & +0.0 \\ & +0.0 \end{aligned}$ |  |  |  |  |  |  |  |
|  |  | +0.0 | +0.0 | $+0.0$ |  |  |  |  |  |  |  |  |
|  |  | +0.0 | +0.0 | -12.4 |  |  |  |  |  |  |  |  |
|  | ^ 2709.020M |  | 54.0 | +0.0 | +0.7 | +3.0 | -34.5 | $+0.0$ | 52.2 | $\begin{aligned} & 54.0 \\ & \text { LOW } \end{aligned}$ | -1.8 | H+V |
|  |  |  |  | +28.6 | +0.4 | +0.0 | $\begin{aligned} & +0.0 \\ & +0.0 \end{aligned}$ |  |  |  |  |  |
|  |  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
|  |  | +0.0 |  | +0.0 | $+0.0$ |  |  |  |  |  |  |  |



| 426490.000 M | 58.9 | $\begin{array}{r} +0.0 \\ +34.4 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.2 \\ & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +4.6 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-34.2 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 65.5 | $\begin{aligned} & 110.7 \\ & \text { HIGH } \end{aligned}$ | -45.2 | $\mathrm{H}+\mathrm{V}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $43 \quad 5563.000 \mathrm{M}$ | 52.2 | $\begin{array}{r} +0.0 \\ +33.4 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.0 \\ & +0.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +4.5 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-34.1 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 57.6 | $\begin{aligned} & 110.7 \\ & \text { HIGH } \end{aligned}$ | -53.1 | H+V |
| $\begin{aligned} & 44 \text { 6404.804M } \\ & \text { Ave } \end{aligned}$ | 60.3 | $\begin{array}{r} +0.0 \\ +34.6 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.2 \\ & +0.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +4.7 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-34.2 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 54.8 | $\begin{aligned} & 110.7 \\ & \text { MID } \end{aligned}$ | -55.9 | H+V |
| $\wedge$ 6404.804M | 67.9 | $\begin{array}{r} +0.0 \\ +34.6 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.2 \\ & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +4.7 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline-34.2 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 74.8 | $\begin{aligned} & 110.7 \\ & \text { MID } \end{aligned}$ | -35.9 | H+V |
| $46 \quad 1855.000 \mathrm{M}$ | 54.8 | $\begin{array}{r} +0.0 \\ +27.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +2.5 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-35.1 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 50.0 | $\begin{gathered} 110.7 \\ \text { HIGH } \end{gathered}$ | -60.7 | H+V |
| 47 1829.846M | 53.8 | $\begin{array}{r} +0.0 \\ +26.9 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.5 \\ & +0.3 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +2.5 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-35.1 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 48.9 | $\begin{aligned} & 110.7 \\ & \text { MID } \end{aligned}$ | -61.8 | H+V |
| $\begin{aligned} & 48 \text { 6320.950M } \\ & \text { Ave } \end{aligned}$ | 54.1 | $\begin{array}{r} +0.0 \\ +34.8 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.3 \\ & +0.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +4.7 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} -34.2 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 48.9 | $\begin{aligned} & 110.7 \\ & \text { LOW } \end{aligned}$ | -61.8 | H+V |
| $\wedge 6320.950 \mathrm{M}$ | 61.7 | $\begin{array}{r} +0.0 \\ +34.8 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.3 \\ & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+4.7 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-34.2 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 68.9 | $\begin{aligned} & 110.7 \\ & \text { LOW } \end{aligned}$ | -41.8 | H+V |
| $\begin{aligned} & 50 \text { 6487.358M } \\ & \text { Ave } \end{aligned}$ | 51.5 | $\begin{array}{r} +0.0 \\ +34.4 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.2 \\ & +0.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +4.6 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} -34.2 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 45.7 | $\begin{aligned} & 110.7 \\ & \text { HIGH } \end{aligned}$ | -65.0 | H+V |
| $\begin{aligned} & 51 \text { 7223.950M } \\ & \text { Ave } \end{aligned}$ | 49.5 | $\begin{array}{r} +0.0 \\ +35.8 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.2 \\ & +0.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +4.6 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-34.5 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 44.8 | $\begin{aligned} & 110.7 \\ & \text { LOW } \end{aligned}$ | -65.9 | H+V |
| $\wedge 7223.950 \mathrm{M}$ | 57.1 | $\begin{array}{r} +0.0 \\ +35.8 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.2 \\ & +0.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +4.6 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-34.5 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 64.8 | $\begin{aligned} & 110.7 \\ & \text { LOW } \end{aligned}$ | -45.9 | H+V |
| $53 \quad 75.600 \mathrm{M}$ | 45.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.5 \\ & +9.1 \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.8 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +7.4 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -27.8 \\ +6.1 \end{array}$ | +0.0 | 41.5 | 110.7 | -69.2 | H+V |


| $5^{54} \mathrm{QP}^{75.431 \mathrm{M}}$ | 43.7 | $+0.0$ | +0.1 | $+0.0$ | +0.0 | +0.0 | 39.9 | 110.7 | -70.8 | H+V |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | +0.0 | +0.0 | +0.0 | $\begin{array}{r} -27.8 \\ +6.1 \end{array}$ |  |  |  |  |  |
|  |  | +0.5 | +0.8 | +7.4 |  |  |  |  |  |  |
|  |  | +9.1 | +0.0 | +0.0 |  |  |  |  |  |  |
| 55 5490.020MAve | 46.7 | +0.0 | +1.0 | +4.5 | -34.1 | +0.0 | 39.4 | $\begin{aligned} & \quad 110.7 \\ & \text { MID } \end{aligned}$ | -71.3 | H+V |
|  |  | +33.1 | +0.6 | $+0.0$ | $+0.0$ |  |  |  |  |  |
|  |  | +0.0 | +0.0 | $+0.0$ | $+0.0$ |  |  |  |  |  |
|  |  | +0.0 | +0.0 | -12.4 |  |  |  |  |  |  |
| ^ 5490.020M | 52.6 | +0.0 | +1.0 | +4.5 | $\begin{array}{r} -34.1 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 57.7 | $\begin{aligned} & \quad 110.7 \\ & \text { MID } \end{aligned}$ | -53.0 | H+V |
|  |  | +33.1 | +0.6 | +0.0 |  |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 57 199.800M | 38.5 | +0.0 | +0.2 | $+0.0$ | +0.0 | $+0.0$ | 38.7 | 110.7 | -72.0 | H+V |
|  |  | $+0.0$ | +0.0 | $+0.0$ | -27.2 |  |  |  |  |  |
|  |  | +0.8 | +1.4 | +9.7 | +6.2 |  |  |  |  |  |
|  |  | +9.1 | +0.0 | +0.0 |  |  |  |  |  |  |
| 58 5560.902M | 45.6 | +0.0 | +1.0 | +4.5 | -34.1 | ${ }^{+0.0}$ | 38.6 | $\begin{aligned} & 110.7 \\ & \text { HIGH } \end{aligned}$ | -72.1 | H+V |
| Ave |  | +33.4 | +0.6 | +0.0 | $+0.0$ |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | -12.4 |  |  |  |  |  |  |
| 59 75.420M | 41.8 | +0.0 | +0.1 | $+0.0$ | +0.0 | $+0.0$ | 38.0 | 110.7 | -72.7 | H+V |
| QP |  | $+0.0$ | +0.0 | $+0.0$ | -27.8 |  |  |  |  |  |
|  |  | +0.5 | +0.8 | +7.4 | +6.1 |  |  |  |  |  |
|  |  | +9.1 | +0.0 | +0.0 |  |  |  |  |  |  |
| $60 \quad 75.600 \mathrm{M}$ | 41.5 | $+0.0$ | +0.1 | $+0.0$ | +0.0 | $+0.0$ | 37.7 | 110.7 | -73.0 | H+V |
|  |  | +0.0 | +0.0 | +0.0 | -27.8 |  |  |  |  |  |
|  |  | +0.5 | +0.8 | +7.4 | +6.1 |  |  |  |  |  |
|  |  | +9.1 | +0.0 | +0.0 |  |  |  |  |  |  |
| $61 \quad 69.800 \mathrm{M}$ | 40.0 | $+0.0$ | +0.1 | $+0.0$ | +0.0 | $+0.0$ | 36.4 | 110.7 | -74.3 | $\mathrm{H}+\mathrm{V}$ |
| QP |  | $+0.0$ | +0.0 | $+0.0$ | -27.8 |  |  |  |  |  |
|  |  | +0.4 | +0.7 | +7.8 | +6.1 |  |  |  |  |  |
|  |  | +9.1 | +0.0 | +0.0 |  |  |  |  |  |  |
| $\wedge 69.800 \mathrm{M}$ | 46.0 | $+0.0$ | +0.1 | $+0.0$ | +0.0 | $+0.0$ | 42.4 | 110.7 | -68.3 | H+V |
|  |  | +0.0 | +0.0 | +0.0 | -27.8 |  |  |  |  |  |
|  |  | +0.4 | +0.7 | +7.8 | +6.1 |  |  |  |  |  |
|  |  | +9.1 | +0.0 | +0.0 |  |  |  |  |  |  |
| 63 592.600M | 23.3 | $+0.0$ | +0.3 | $+0.0$ | $\begin{array}{r} +0.0 \\ -28.1 \\ +6.2 \end{array}$ | $+0.0$ | 35.0 | 110.7 | -75.7 | $\mathrm{H}+\mathrm{V}$ |
| QP |  | $+0.0$ | $+0.0$ | $+0.0$ |  |  |  |  |  |  |
|  |  | +1.6 | +2.1 | +20.5 |  |  |  |  |  |  |
|  |  | +9.1 | +0.0 | +0.0 |  |  |  |  |  |  |
| $\wedge 592.600 \mathrm{M}$ | 36.4 | $+0.0$ | +0.3 | $+0.0$ | +0.0 | +0.0 | 48.1 | 110.7 | -62.6 | H+V |
|  |  | +0.0 | +0.0 | $+0.0$ | $\begin{array}{r} -28.1 \\ +6.2 \end{array}$ |  |  |  |  |  |
|  |  | +1.6 | +2.1 | +20.5 |  |  |  |  |  |  |
|  |  | +9.1 | $+0.0$ | +0.0 |  |  |  |  |  |  |

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| $\begin{aligned} & 65 \text { 9268.036M } \\ & \text { Ave } \end{aligned}$ | 35.6 | $\begin{array}{r} +0.0 \\ +37.6 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.4 \\ & +0.7 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +6.2 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} -34.8 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 34.3 | $\begin{aligned} & 110.7 \\ & \text { HIGH } \end{aligned}$ | -76.4 | H+V |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ^ 9268.036M | 46.4 | $\begin{array}{r} +0.0 \\ +37.6 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.4 \\ & +0.7 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+6.2 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} -34.8 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 57.5 | $\begin{aligned} & 110.7 \\ & \text { HIGH } \end{aligned}$ | -53.2 | H+V |
| $\begin{gathered} 67 \quad 200.016 \mathrm{M} \\ \mathrm{QP} \end{gathered}$ |  | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.8 \\ & +9.1 \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \\ & +1.4 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +9.7 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -27.2 \\ +6.2 \end{array}$ | +0.0 | 33.3 | 110.7 | -77.4 | H+V |
| $\begin{gathered} 68 \text { 1805.820M } \\ \text { Ave } \end{gathered}$ | 50.5 | $\begin{array}{r} +0.0 \\ +26.8 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.5 \\ & +0.3 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +2.5 \\ +0.0 \\ +0.0 \\ -12.4 \\ \hline \end{array}$ | $\begin{array}{r} -35.1 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 33.1 | $\begin{aligned} & 110.7 \\ & \text { LOW } \end{aligned}$ | -77.6 | H+V |
| $\wedge 1805.820 \mathrm{M}$ | 58.1 | $\begin{array}{r} +0.0 \\ +26.8 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.5 \\ & +0.3 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+2.5 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-35.1 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 53.1 | $\begin{aligned} & 110.7 \\ & \text { LOW } \end{aligned}$ | -57.6 | H+V |
| $\begin{gathered} 70 \quad 98.900 \mathrm{M} \\ \mathrm{QP} \end{gathered}$ | 32.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.6 \\ & +9.1 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +1.1 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +10.1 \\ +0.0 \end{array}$ | $\begin{array}{r} +0.0 \\ -27.7 \\ +6.1 \end{array}$ | +0.0 | 31.7 | 110.7 | -79.0 | H+V |
| $\wedge \quad 98.900 \mathrm{M}$ | 41.7 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.6 \\ & +9.1 \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +1.1 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +10.1 \\ +0.0 \end{array}$ | $\begin{array}{r} +0.0 \\ -27.7 \\ +6.1 \end{array}$ | +0.0 | 41.1 | 110.7 | -69.6 | H+V |
| $\begin{aligned} & 72 \quad 1853.587 \mathrm{M} \\ & \text { Ave } \end{aligned}$ |  | $\begin{array}{r} +0.0 \\ +27.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +2.5 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-35.1 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 31.5 | $\begin{aligned} & 110.7 \\ & \text { MID } \end{aligned}$ | -79.2 | H+V |
| $\begin{aligned} & 73 \quad 295.800 \mathrm{M} \\ & \mathrm{QP} \end{aligned}$ | 25.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.0 \\ & +9.1 \end{aligned}$ | $\begin{aligned} & \hline+0.2 \\ & +0.0 \\ & +1.6 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +14.2 \\ +0.0 \end{array}$ | $\begin{array}{r} +0.0 \\ -27.1 \\ +6.2 \end{array}$ | +0.0 | 30.5 | 110.7 | -80.2 | H+V |
| ^ 295.800M | 30.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.0 \\ & +9.1 \end{aligned}$ | $\begin{aligned} & \hline+0.2 \\ & +0.0 \\ & +1.6 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +14.2 \\ +0.0 \end{array}$ | $\begin{array}{r} +0.0 \\ -27.1 \\ +6.2 \end{array}$ | $+0.0$ | 35.2 | 110.7 | -75.5 | $\mathrm{H}+\mathrm{V}$ |
| $\begin{aligned} & 75 \text { 1853.636M } \\ & \text { Ave } \end{aligned}$ | 43.5 | $\begin{array}{r} +0.0 \\ +27.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.5 \\ & +0.3 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline+2.5 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-35.1 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 26.3 | $\begin{aligned} & 110.7 \\ & \text { HIGH } \end{aligned}$ | -84.4 | $\mathrm{H}+\mathrm{V}$ |
| $76 \quad 12.395 \mathrm{M}$ | 18.9 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +8.9 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.2 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -12.0 | 110.7 | -122.7 | H+V |
| $77 \quad 27.751 \mathrm{M}$ | 18.3 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +6.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.3 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -15.1 | 110.7 | -125.8 | H+V |

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| 78 | 19.233 M | 15.0 | +0.0 | +0.0 | +0.3 | +0.0 | -40.0 | -16.4 | 110.7 | -127.1 | $\mathrm{H}+\mathrm{V}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
| 79 | 16.294 k | 42.8 | +0.0 | +0.0 | +0.0 | +0.0 | -80.0 | -22.3 | 110.7 | -133.0 | $\mathrm{H}+\mathrm{V}$ |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +14.9 | +0.0 |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |

Test Location: CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A•Bothell, WA. 98021•1-800-500-4EMC
Customer:
Specification:
Work Order \#:
Test Type:
Tested By: Itron, Inc.
15.247(d) / 15.209 Radiated Spurious Emissions

Software: EMITest 5.03.02

98384
Maximized Emissions
Michael Atkinson

Date: 5/13/2016
Time: 12:32:16
Sequence\#: 22

## Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

## Test Conditions / Notes:

Temperature: $25^{\circ} \mathrm{C}$
Humidity: 31\%
Pressure: 102.1 kPa

Frequency tested: $9 \mathrm{kHz}-13 \mathrm{GHz}$
Firmware power setting: Max Power
EUT Firmware: 10.02-06
Modulation: FM
Antenna type: Monopole
Antenna Gain: $\quad 6.15 \mathrm{dBi}$ ( 8.15 dBi with 2 dB attenuator
Duty Cycle: Measured with $100 \%$ (end use limited to $23.5 \%$ duty)
Test Method: ANSI C63.10 (2013)
Setup: EUT is a 900 MHz range radio. EUT is transmitting continuously modulated. 900 MHz antenna is connected using approximately 2.5 m of $1 / 2$ inch Andrews Heliax FS14-50B cable, along with 2 dB attenuator and lightning protector. EUT antenna height set to stay within test volume boundaries. Both antenna polarities investigated, as well as both FM12.7k and FM37.5k modulations investigated, only worst case reported. Power output validated to be within manufacturer tolerances.

Wifi transmitter on EUT marked as ambient, this is the fundamental from the integrated certified module in the EUT which is to be excluded from the measurement limits. All average data points marked Low, Mid, High have duty cycle correction applied ( $23.87 \%,-12.44 \mathrm{~dB}$ ).

Itron, Inc WO\#: 98384 Sequence\#: 22 Date: 5/13/2016 15.247 (d) / 15.209 Radiated Spurious Emissions Test Distance: 3 Meters H+V


[^1]O Peak Readings

* Average Readings

Software Version: 5.03.02

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02872 | Spectrum Analyzer | E4440A | $11 / 18 / 2015$ | $11 / 18 / 2017$ |
| T2 | ANP06540 | Cable | Heliax | $10 / 29 / 2015$ | $10 / 29 / 2017$ |
| T3 | ANP05305 | Cable | ETSI-50T | $2 / 15 / 2016$ | $2 / 15 / 2018$ |
| T4 | AN03540 | Preamp | 83017 A | $4 / 30 / 2015$ | $4 / 30 / 2017$ |
| T5 | AN01467 | Horn Antenna- <br> ANSI C63.5 <br> Calibration | 3115 | $8 / 12 / 2015$ | $8 / 12 / 2017$ |
|  |  | Cable |  |  |  |
| T6 | ANP06935 |  | $32026-29801-$ | $3 / 11 / 2016$ | $3 / 11 / 2018$ |
| T7 | AN03170 | High Pass Filter | HM1155-11SS | $12 / 17 / 2015$ | $12 / 17 / 2017$ |
| T8 | ANP05963 | Cable | RG-214 | $2 / 15 / 2016$ | $2 / 15 / 2018$ |
| T9 | ANP05360 | Cable | RG214 | $12 / 1 / 2014$ | $12 / 1 / 2016$ |
| T10 | AN02307 | Preamp | $8447 D$ | $2 / 15 / 2016$ | $2 / 15 / 2018$ |
| T11 | AN01994 | Biconilog Antenna | CBL6111C | $3 / 11 / 2016$ | $3 / 11 / 2018$ |
| T12 | ANP05505 | Attenuator | NAT-6 | $3 / 31 / 2016$ | $3 / 31 / 2018$ |
| T13 | ANP06219 | Attenuator | $768-10$ | $4 / 12 / 2016$ | $4 / 12 / 2018$ |
| T14 | AN00052 | Loop Antenna | 6502 | $4 / 8 / 2016$ | $4 / 8 / 2018$ |
| T15 | ANDCCF | Test Data |  | $5 / 13 / 2016$ | $5 / 13 / 2018$ |
|  |  | Adjustment |  |  |  |

Measurement Data: $\quad$ Reading listed by margin. Test Distance: 3 Meters

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline \multirow[t]{5}{*}{\#} \& \multirow[t]{5}{*}{Freq

MHz} \& \multirow[t]{4}{*}{Rdng} \& T1 \& T2 \& T3 \& T4 \& Dist \& Corr \& Spec \& Margin \& \multirow[t]{4}{*}{Polar} <br>
\hline \& \& \& T5 \& T6 \& T7 \& T8 \& \& \& \& \& <br>
\hline \& \& \& T9 \& T10 \& T11 \& T12 \& \& \& \& \& <br>

\hline \& \& \& T13 \& T14 \& $$
\mathrm{T} 15
$$ \& \& \& \& \& \& <br>

\hline \& \& $\mathrm{dB} \mu \mathrm{V}$ \& \& \& \& dB \& Table \& $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$ \& $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$ \& dB \& Ant <br>

\hline \multicolumn{2}{|r|}{\multirow[t]{4}{*}{$$
\begin{aligned}
& 17320.189 \mathrm{M} \\
& \text { Ave }
\end{aligned}
$$}} \& \multirow[t]{4}{*}{54.7} \& +0.0 \& +1.2 \& +4.7 \& -34.6 \& \multirow[t]{4}{*}{+0.0} \& \multirow[t]{4}{*}{50.3} \& \multirow[t]{4}{*}{\[

$$
\begin{aligned}
& 54.0 \\
& \text { Mid }
\end{aligned}
$$
\]} \& \multirow[t]{4}{*}{-3.7} \& \multirow[t]{4}{*}{H+V} <br>

\hline \& \& \& +36.1 \& +0.6 \& +0.0 \& +0.0 \& \& \& \& \& <br>
\hline \& \& \& +0.0 \& +0.0 \& +0.0 \& +0.0 \& \& \& \& \& <br>
\hline \& \& \& +0.0 \& +0.0 \& -12.4 \& \& \& \& \& \& <br>

\hline \multicolumn{2}{|r|}{\multirow[t]{4}{*}{^ 7320.189M}} \& \multirow[t]{4}{*}{58.4} \& +0.0 \& +1.2 \& +4.7 \& -34.6 \& \multirow[t]{4}{*}{+0.0} \& \multirow[t]{4}{*}{66.4} \& \multirow[t]{4}{*}{$$
\begin{aligned}
& \quad 54.0 \\
& \text { Mid }
\end{aligned}
$$} \& \multirow[t]{4}{*}{+12.4} \& \multirow[t]{4}{*}{$\mathrm{H}+\mathrm{V}$} <br>

\hline \& \& \& +36.1 \& +0.6 \& +0.0 \& +0.0 \& \& \& \& \& <br>
\hline \& \& \& +0.0 \& +0.0 \& +0.0 \& +0.0 \& \& \& \& \& <br>
\hline \& \& \& +0.0 \& +0.0 \& +0.0 \& \& \& \& \& \& <br>

\hline \multicolumn{2}{|r|}{\multirow[t]{4}{*}{$$
\begin{aligned}
& 34634.005 \mathrm{M} \\
& \text { Ave }
\end{aligned}
$$}} \& \multirow[t]{4}{*}{58.3} \& +0.0 \& +0.9 \& +4.3 \& -34.1 \& \multirow[t]{4}{*}{+0.0} \& \multirow[t]{4}{*}{50.1} \& \multirow[t]{4}{*}{\[

$$
\begin{aligned}
& 54.0 \\
& \text { High }
\end{aligned}
$$
\]} \& \multirow[t]{4}{*}{-3.9} \& \multirow[t]{4}{*}{H+V} <br>

\hline \& \& \& +32.6 \& +0.5 \& +0.0 \& +0.0 \& \& \& \& \& <br>
\hline \& \& \& +0.0 \& +0.0 \& +0.0 \& +0.0 \& \& \& \& \& <br>
\hline \& \& \& +0.0 \& +0.0 \& -12.4 \& \& \& \& \& \& <br>

\hline \multicolumn{2}{|r|}{\multirow[t]{4}{*}{$\wedge 4634.005 \mathrm{M}$}} \& \multirow[t]{4}{*}{62.1} \& +0.0 \& +0.9 \& +4.3 \& -34.1 \& \multirow[t]{4}{*}{+0.0} \& \multirow[t]{4}{*}{66.3} \& \multirow[t]{4}{*}{$$
\begin{aligned}
& 54.0 \\
& \text { High }
\end{aligned}
$$} \& \multirow[t]{4}{*}{+12.3} \& \multirow[t]{4}{*}{H+V} <br>

\hline \& \& \& +32.6 \& +0.5 \& +0.0 \& +0.0 \& \& \& \& \& <br>
\hline \& \& \& +0.0 \& +0.0 \& +0.0 \& +0.0 \& \& \& \& \& <br>
\hline \& \& \& +0.0 \& +0.0 \& +0.0 \& \& \& \& \& \& <br>
\hline
\end{tabular}



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| $\begin{gathered} 16 \text { 8344.000M } \\ \text { Ave } \end{gathered}$ | 49.1 | $\begin{array}{r} +0.0 \\ +36.6 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.5 \\ & +0.7 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +5.4 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} -35.0 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 45.9 | $\begin{aligned} & 54.0 \\ & \text { High } \end{aligned}$ | -8.1 | H+V |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ^ 8344.000M | 52.3 | $\begin{array}{r} +0.0 \\ +36.6 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.5 \\ & +0.7 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+5.4 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-35.0 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 61.5 | $\begin{aligned} & 54.0 \\ & \text { High } \end{aligned}$ | +7.5 | H+V |
| $\begin{aligned} & 185417.998 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 53.2 | $\begin{array}{r} +0.0 \\ +33.1 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.0 \\ & +0.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +4.5 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-34.2 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 45.8 | $\begin{aligned} & 54.0 \\ & \text { Low } \end{aligned}$ | -8.2 | $\mathrm{H}+\mathrm{V}$ |
| ^ 5417.998M | 58.3 | $\begin{array}{r} +0.0 \\ +33.1 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.0 \\ & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +4.5 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline-34.2 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 63.3 | $\begin{aligned} & 54.0 \\ & \text { Low } \end{aligned}$ | +9.3 | H+V |
| $\begin{aligned} & 202780.287 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 58.4 | $\begin{array}{r} +0.0 \\ +28.9 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.7 \\ & +0.4 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +3.0 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} -34.5 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 44.5 | $\begin{aligned} & 54.0 \\ & \text { High } \end{aligned}$ | -9.5 | H+V |
| $\wedge 2780.280 \mathrm{M}$ | 59.8 | $\begin{array}{r} +0.0 \\ +28.9 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.7 \\ & +0.4 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +3.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-34.5 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ |  | $\begin{aligned} & 54.0 \\ & \text { High } \end{aligned}$ | +4.3 | $\mathrm{H}+\mathrm{V}$ |
| 221072.000 M | 45.4 | $\begin{array}{r} +0.0 \\ +24.2 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.4 \\ & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.9 \\ & +8.9 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} -37.2 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 43.8 | 54.0 | -10.2 | H+V |
| $\begin{aligned} & 233659.962 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 55.4 | $\begin{array}{r} +0.0 \\ +29.9 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.7 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.7 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-34.2 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 43.6 | $\begin{aligned} & 54.0 \\ & \text { Mid } \end{aligned}$ | -10.4 | H+V |
| ^ 3659.962M | 56.0 | $\begin{array}{r} +0.0 \\ +29.9 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.7 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +3.7 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline-34.2 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 56.6 | $\begin{aligned} & 54.0 \\ & \text { Mid } \end{aligned}$ | +2.6 | H+V |
| $\begin{gathered} 253707.290 \mathrm{M} \\ \text { Ave } \end{gathered}$ | 54.7 | $\begin{array}{r} +0.0 \\ +30.1 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.7 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +3.8 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-34.1 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 43.3 | $\begin{aligned} & 54.0 \\ & \text { High } \end{aligned}$ | -10.7 | H+V |
| $\wedge 3707.290 \mathrm{M}$ | 56.3 | $\begin{array}{r} +0.0 \\ +30.1 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.7 \\ & +0.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +3.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-34.1 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 57.3 | $\begin{aligned} & 54.0 \\ & \text { High } \end{aligned}$ | +3.3 | H+V |


| $\begin{aligned} & 27 \begin{array}{c} 2458.000 \mathrm{M} \\ \text { Ambient } \end{array} \\ & \hline \end{aligned}$ |  | 101.3 | $+0.0$ | +0.6 | +2.9 | -34.5 | $+0.0$ | 98.8 | 110.7 | -11.9 | H+V |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | +27.7 | +0.4 | +0.4 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 28 | 1189.000M | 49.9 | +0.0 | +0.4 | +2.0 | -36.6 | +0.0 | 41.4 | 54.0 | -12.6 | $\mathrm{H}+\mathrm{V}$ |
|  |  |  | +24.2 | +0.3 | +1.2 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 29 | 8235.033M | 44.3 | +0.0 | +1.3 | +5.3 | -35.1 | +0.0 | 40.8 | 54.0 | -13.2 | H+V |
|  | Ave |  | +36.7 | +0.7 | +0.0 | +0.0 |  |  | Mid |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | $+0.0$ | +0.0 | -12.4 |  |  |  |  |  |  |
|  | 8235.033M | 46.4 | +0.0 | +1.3 | +5.3 | -35.1 | ${ }^{+0.0}$ | 55.3 | 54.0 | +1.3 | H+V |
|  |  |  | +36.7 | +0.7 | +0.0 | +0.0 |  |  | Mid |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | $+0.0$ |  |  |  |  |  |  |
| 31 | 1378.000M | 47.6 | +0.0 | +0.5 | +2.2 | -36.0 | +0.0 | 40.1 | 54.0 | -13.9 | H+V |
|  |  |  | +24.8 | +0.3 | +0.7 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 32 | $\begin{aligned} & 3611.987 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 52.0 | +0.0 | +0.8 | +3.6 | -34.2 | ${ }^{+0.0}$ | 40.0 | $\begin{gathered} 54.0 \\ \text { Low } \end{gathered}$ | -14.0 | H+V |
|  |  |  | +29.8 | +0.4 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | -12.4 |  |  |  |  |  |  |
| $\wedge$ | 3611.987M | 54.6 | +0.0 | $+0.8$ | +3.6 | -34.2 | +0.0 | 55.0 | $\begin{gathered} 54.0 \\ \text { Low } \end{gathered}$ | +1.0 | H+V |
|  |  |  | +29.8 | +0.4 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 34 | $\begin{aligned} & 9029.919 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 38.6 | +0.0 | +1.3 | +6.0 | -34.6 | +0.0 | 37.4 | $\begin{gathered} 54.0 \\ \text { Low } \end{gathered}$ | -16.6 | H+V |
|  |  |  | +37.8 | +0.7 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | -12.4 |  |  |  |  |  |  |
| $\wedge$ | 9029.919M | 45.6 | +0.0 | +1.3 | +6.0 | -34.6 | +0.0 | 56.8 | $\begin{gathered} 54.0 \\ \text { Low } \end{gathered}$ | +2.8 | H+V |
|  |  |  | +37.8 | +0.7 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 36 | $\begin{aligned} & \text { 2708.960M } \\ & \text { Ave } \end{aligned}$ | 50.6 | +0.0 | +0.7 | +3.0 | -34.5 | +0.0 | 36.4 | $\begin{aligned} & 54.0 \\ & \text { Low } \end{aligned}$ | -17.6 | H+V |
|  |  |  | +28.6 | +0.4 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | -12.4 |  |  |  |  |  |  |
| $\wedge$ | 2708.960M | 52.5 | +0.0 | +0.7 | +3.0 | -34.5 | +0.0 | 50.7 | 54.0 | -3.3 | H+V |
|  |  |  | +28.6 | +0.4 | +0.0 | +0.0 |  |  | Low |  |  |
|  |  |  | +0.0 | $+0.0$ | +0.0 | $+0.0$ |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| $\begin{gathered} 38 \text { 2744.937M } \\ \text { Ave } \end{gathered}$ |  | 47.9 | +0.0 | +0.7 | +3.0 | -34.5 | +0.0 | 33.9 | Mid ${ }^{54.0}$ | -20.1 | H+V |
|  |  | +28.8 | +0.4 | +0.0 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | -12.4 |  |  |  |  |  |  |




| 51 1810.000M | 57.5 | $\begin{array}{r} +0.0 \\ +26.8 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.3 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+2.5 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-35.1 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 52.5 | $\begin{aligned} & 110.7 \\ & \text { Low } \end{aligned}$ | -58.2 | $\mathrm{H}+\mathrm{V}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 527223.965 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 54.0 | $\begin{array}{r} +0.0 \\ +35.8 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.2 \\ & +0.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline+4.6 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-34.5 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 49.3 | $\begin{aligned} & 110.7 \\ & \text { Low } \end{aligned}$ | -61.4 | H+V |
| $\wedge 7223.965 \mathrm{M}$ | 57.8 | $\begin{array}{r} +0.0 \\ +35.8 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.2 \\ & +0.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +4.6 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-34.5 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 65.5 | $\begin{aligned} & 110.7 \\ & \text { Low } \end{aligned}$ | -45.2 | $\mathrm{H}+\mathrm{V}$ |
| 54 1855.000M | 52.0 | $\begin{array}{r} +0.0 \\ +27.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.3 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+2.5 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-35.1 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 47.2 | $\begin{aligned} & 110.7 \\ & \text { High } \end{aligned}$ | -63.5 | H+V |
| 551828.000 M | 50.8 | $\begin{array}{r} +0.0 \\ +26.9 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.3 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+2.5 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline-35.1 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $+0.0$ |  | $\begin{aligned} & 110.7 \\ & \text { Mid } \end{aligned}$ | -64.8 | H+V |
| $\begin{aligned} & 56 \begin{array}{c} 5490.006 \mathrm{M} \\ \text { Ave } \end{array} \end{aligned}$ | 52.0 | $\begin{array}{r} +0.0 \\ +33.1 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.0 \\ & +0.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +4.5 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-34.1 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 44.7 | $\begin{aligned} & 110.7 \\ & \text { Mid } \end{aligned}$ | -66.0 | H+V |
| $\wedge 5490.006 \mathrm{M}$ | 53.8 | $\begin{array}{r} +0.0 \\ +33.1 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.0 \\ & +0.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +4.5 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-34.1 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 58.9 | $\begin{aligned} & 110.7 \\ & \text { Mid } \end{aligned}$ | -51.8 | H+V |
| $\begin{aligned} & 58 \text { 5560.716M } \\ & \text { Ave } \end{aligned}$ | 51.0 | $\begin{array}{r} +0.0 \\ +33.4 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.0 \\ & +0.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +4.5 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-34.1 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 44.0 | $\begin{aligned} & 110.7 \\ & \text { High } \end{aligned}$ | -66.7 | H+V |
| $\wedge 5560.716 \mathrm{M}$ | 53.3 | $\begin{array}{r} +0.0 \\ +33.4 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.0 \\ & +0.6 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +4.5 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-34.1 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 58.7 | $\begin{aligned} & 110.7 \\ & \text { High } \end{aligned}$ | -52.0 | H+V |
| $\begin{aligned} & 60 \quad 9267.892 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 43.2 | $\begin{array}{r} +0.0 \\ +37.6 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.4 \\ & +0.7 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +6.2 \\ +0.0 \\ +0.0 \\ -12.4 \end{array}$ | $\begin{array}{r} \hline-34.8 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 41.9 | $\begin{aligned} & 110.7 \\ & \text { High } \end{aligned}$ | -68.8 | H+V |
| ^ 9267.892M | 48.0 | $\begin{array}{r} +0.0 \\ +37.6 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.4 \\ & +0.7 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +6.2 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-34.8 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 59.1 | $\begin{aligned} & 110.7 \\ & \text { High } \end{aligned}$ | -51.6 | H+V |


| 62 | 75.426M | 44.1 | $+0.0$ | +0.1 | +0.0 | +0.0 | $+0.0$ | 40.3 | 110.7 | -70.4 | H+V |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| QP |  |  | +0.0 | +0.0 | +0.0 | $\begin{aligned} & +0.8 \\ & +6.1 \end{aligned}$ |  |  |  |  |  |
|  |  |  | +0.5 | -27.8 | +7.4 |  |  |  |  |  |  |
|  |  |  | +9.1 | +0.0 | +0.0 |  |  |  |  |  |  |
| 63 | 75.600M | 43.9 | +0.0 | +0.1 | +0.0 | +0.0 | $+0.0$ | 40.1 | 110.7 | -70.6 | H+V |
|  |  |  | +0.0 | +0.0 | +0.0 | $\begin{aligned} & +0.8 \\ & +6.1 \end{aligned}$ |  |  |  |  |  |
|  |  |  | +0.5 | -27.8 | +7.4 |  |  |  |  |  |  |
|  |  |  | +9.1 | +0.0 | +0.0 |  |  |  |  |  |  |
| $\begin{aligned} & 64 \text { 1806.041M } \\ & \text { Ave } \end{aligned}$ |  | 56.0 | +0.0 | +0.5 | +2.5 | $\begin{array}{r} \hline-35.1 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 38.6 | $\begin{aligned} & 110.7 \\ & \text { Low } \end{aligned}$ | -72.1 | H+V |
|  |  | +26.8 | +0.3 | +0.0 |  |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
|  |  | +0.0 | +0.0 | -12.4 |  |  |  |  |  |  |
| $\begin{aligned} & 65141.500 \mathrm{M} \\ & \mathrm{QP} \end{aligned}$ |  |  | 34.9 | +0.0 | +0.1 | +0.0 | +0.0 | $+0.0$ | 36.6 | 110.7 | -74.1 | $\mathrm{H}+\mathrm{V}$ |
|  |  | +0.0 |  | +0.0 | +0.0 | +1.3 |  |  |  |  |  |  |
|  |  | +0.7 |  | -27.5 | +11.9 | +6.1 |  |  |  |  |  |  |
|  |  | +9.1 |  | +0.0 | +0.0 |  |  |  |  |  |  |  |
| $\wedge$ | 141.500M |  | 37.3 | +0.0 | +0.1 | +0.0 | $+0.0$ | +0.0 | 39.0 | 110.7 | -71.7 | H+V |
|  |  |  |  | +0.0 | +0.0 | +0.0 | +1.3 |  |  |  |  |  |
|  |  |  | +0.7 | -27.5 | +11.9 | +6.1 |  |  |  |  |  |  |
|  |  |  | +9.1 | +0.0 | +0.0 |  |  |  |  |  |  |  |
|  | $\begin{aligned} & 1853.683 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 51.6 | +0.0 | +0.5 | +2.5 | $\begin{array}{r} \hline-35.1 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 34.4 | $110.7$ <br> High | -76.3 | H+V |  |
|  |  |  | +27.0 | +0.3 | +0.0 |  |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | -12.4 |  |  |  |  |  |  |  |
| $\begin{gathered} 68 \quad 203.600 \mathrm{M} \\ \mathrm{QP} \end{gathered}$ |  | 33.0 | +0.0 | +0.2 | +0.0 | $\begin{aligned} & +0.0 \\ & +1.4 \\ & +6.2 \end{aligned}$ | +0.0 | 33.5 | 110.7 | -77.2 | $\mathrm{H}+\mathrm{V}$ |  |
|  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |  |
|  |  | +0.8 | -27.2 | +10.0 |  |  |  |  |  |  |  |
|  |  | +9.1 | +0.0 | +0.0 |  |  |  |  |  |  |  |
| $\wedge$ | 203.600M |  | 35.8 | +0.0 | +0.2 | +0.0 | +0.0 | $+0.0$ | 36.3 | 110.7 | -74.4 | H+V |
|  |  |  |  | +0.0 | +0.0 | $+0.0$ | +1.4 |  |  |  |  |  |
|  |  |  |  | +0.8 | -27.2 | +10.0 | +6.2 |  |  |  |  |  |
|  |  | +9.1 |  | +0.0 | +0.0 |  |  |  |  |  |  |  |
| 70 | 96.900 M | 34.2 | +0.0 | +0.1 | +0.0 | $\begin{aligned} & \hline+0.0 \\ & +1.1 \\ & +6.1 \end{aligned}$ | +0.0 | 33.3 | 110.7 | -77.4 | $\mathrm{H}+\mathrm{V}$ |  |
| QP |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |  |
|  |  | +0.6 | -27.7 | +9.8 | $+6.1$ |  |  |  |  |  |  |  |
|  |  | +9.1 | +0.0 | +0.0 |  |  |  |  |  |  |  |  |
| $\wedge$ | 96.900M |  | 40.3 | +0.0 | +0.1 | +0.0 | $\begin{aligned} & +0.0 \\ & +1.1 \\ & +6.1 \end{aligned}$ | $+0.0$ | 39.4 | 110.7 | -71.3 | $\mathrm{H}+\mathrm{V}$ |
|  |  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
|  |  | +0.6 |  | -27.7 | +9.8 |  |  |  |  |  |  |  |
|  |  | +9.1 |  | +0.0 | +0.0 |  |  |  |  |  |  |  |
| $\begin{aligned} & 721829.991 \mathrm{M} \\ & \text { Ave } \end{aligned}$ |  | 49.7 | +0.0 | +0.5 | +2.5 | -35.1 | $+0.0$ | 32.4 | $\begin{aligned} & 110.7 \\ & \text { Mid } \end{aligned}$ | -78.3 | H+V |  |
|  |  | +26.9 | +0.3 | +0.0 | $\begin{aligned} & +0.0 \\ & +0.0 \end{aligned}$ |  |  |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |  |  |
|  |  | +0.0 | +0.0 | -12.4 |  |  |  |  |  |  |  |  |



Test Location: CKC Laboratories, Inc. • 22116 23rd Drive SE, Suite A•Bothell, WA. 98021•1-800-500-4EMC
Customer:
Specification:
Work Order \#:
Test Type:
Tested By: Itron, Inc
15.247(d) / 15.209 Radiated Spurious Emissions

98384 Date: 5/16/2016
Maximized Emissions
Time: 11:14:46
Michael Atkinson
Sequence\#: 24
Software:
EMITest 5.03.02

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

## Test Conditions / Notes:

Temperature: $25^{\circ} \mathrm{C}$
Humidity: 31\%
Pressure: 102.1 kPa
Frequency Range: Low (903MHz), High (926.8MHz)
Firmware power setting: Max Power
EUT Firmware: 10.02-06
Modulation: AM, FM37.5k, FM12.5k

Antenna type: Monopole
Antenna Gain: $\quad 6.15 \mathrm{dBi}$ ( 8.15 dBi with 2 dB attenuator)
Duty Cycle: Measured with $100 \%$ (end use limited to $23.5 \%$ duty)

Test Method: ANSI C63.10 (2013)
Setup: The EUT is a 900 MHz range radio. The EUT is transmitting continuously modulated. 900 MHz antenna is connected using approximately 2.5 m of $1 / 2$ inch Andrews Heliax FS14-50B cable, along with 2 dB attenuator and lightning protector. The EUT antenna height set to stay within test volume boundaries. Both antenna polarities investigated, only worst case reported. Power output validated to be within manufacturer tolerances.

Itron, Inc WOO: 98384 Sequence\#: 24 Date: 5/16/2016
15.247 (d) / 15.209 Radiated Spurious Emissions Test Distance: 3 Meters Horiz


—— Readings<br>$\times \quad$ Peak Readings<br>Software Version: 5.03.02

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02872 | Spectrum Analyzer | E4440A | $11 / 18 / 2015$ | $11 / 18 / 2017$ |
|  | ANP05747 | Attenuator | PE7004-20 | $1 / 29 / 2016$ | $1 / 29 / 2018$ |
| T2 | ANP06540 | Cable | Heliax | $10 / 29 / 2015$ | $10 / 29 / 2017$ |
| T3 | ANP05963 | Cable | RG-214 | $2 / 15 / 2016$ | $2 / 15 / 2018$ |
| T4 | ANP05360 | Cable | RG214 | $12 / 1 / 2014$ | $12 / 1 / 2016$ |
| T5 | AN02307 | Preamp | $8447 D$ | $2 / 15 / 2016$ | $2 / 15 / 2018$ |
| T6 | AN01994 | Biconilog Antenna | CBL6111C | $3 / 11 / 2016$ | $3 / 11 / 2018$ |
| T7 | ANP05505 | Attenuator | NAT-6 | $3 / 31 / 2016$ | $3 / 31 / 2018$ |
| T8 | ANP06219 | Attenuator | $768-10$ | $4 / 12 / 2016$ | $4 / 12 / 2018$ |

Measurement Data: Reading listed by order taken. Test Distance: 3 Meters

| \# | Freq <br> MHz | Rdng <br> $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \text { T1 } \\ & \text { T5 } \\ & \text { dB } \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \text { T6 } \\ & \text { dB } \end{aligned}$ | $\begin{aligned} & \mathrm{T} 3 \\ & \mathrm{~T} 7 \\ & \text { dB } \end{aligned}$ | $\begin{aligned} & \mathrm{T} 4 \\ & \mathrm{~T} 8 \\ & \mathrm{~dB} \\ & \hline \end{aligned}$ | Dist Table | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \end{gathered}$ | Spec $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$ | Margin dB | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 614.000 M | 29.5 | +0.0 | +0.3 | +2.1 | +1.6 | +0.0 | 41.5 | 46.0 | -4.5 | H+V |
|  |  |  | -28.1 | +20.8 | +6.2 | +9.1 | AM |  |  |  |  |
| 2 | 902.000 M | 78.5 | +0.0 | +0.3 | +2.4 | +2.0 | +0.0 | 95.2 | 110.7 | -15.5 | H+V |
|  |  |  | -27.4 | +24.1 | +6.2 | +9.1 | AM |  |  |  |  |
| 3 | 902.000 M | 72.4 | +0.0 | +0.3 | +2.4 | +2.0 | +0.0 | 89.1 | 110.7 | -21.6 | H+V |
|  |  |  | -27.4 | +24.1 | +6.2 | +9.1 | FM 37.5k |  |  |  |  |
| 4 | 614.000M | 29.1 | +0.0 | +0.3 | +2.1 | +1.6 | $+0.0$ | 41.1 | 46.0 | -4.9 | H+V |
|  |  |  | -28.1 | +20.8 | +6.2 | +9.1 | FM 37.5k |  |  |  |  |
| 5 | 902.000 M | 72.5 | +0.0 | +0.3 | +2.4 | +2.0 | +0.0 | 89.2 | 110.7 | -21.5 | $\mathrm{H}+\mathrm{V}$ |
|  |  |  | -27.4 | +24.1 | +6.2 | +9.1 | FM 12.5 k |  |  |  |  |
| 6 | 614.000 M | 30.3 | +0.0 | +0.3 | +2.1 | +1.6 | +0.0 | 42.3 | 46.0 | -3.7 | H+V |
|  |  |  | -28.1 | +20.8 | +6.2 | +9.1 | FM 12.5k |  |  |  |  |
| 7 | 928.000M | 80.0 | +0.0 | +0.4 | +2.4 | +2.1 | $+0.0$ | 97.4 | 110.7 | -13.3 | H+V |
|  |  |  | -27.3 | +24.4 | +6.2 | +9.2 | AM |  |  |  |  |
| 8 | 960.000 M | 28.3 | +0.0 | +0.4 | +2.5 | +2.1 | $+0.0$ | 46.5 | 54.0 | -7.5 | $\mathrm{H}+\mathrm{V}$ |
|  |  |  | -27.1 | +24.8 | +6.3 | +9.2 | AM |  |  |  |  |
| 9 | 928.000 M | 59.3 | +0.0 | +0.4 | +2.4 | +2.1 | +0.0 | 76.7 | 110.7 | -34.0 | $\mathrm{H}+\mathrm{V}$ |
|  |  |  | -27.3 | +24.4 | +6.2 | +9.2 | FM 37.5k |  |  |  |  |
| 10 | 960.000 M | 28.7 | +0.0 | +0.4 | +2.5 | +2.1 | +0.0 | 46.9 | 54.0 | -7.1 | H+V |
|  |  |  | -27.1 | +24.8 | +6.3 | +9.2 | FM 37.5k |  |  |  |  |
| 11 | 928.000 M | 59.5 | +0.0 | +0.4 | +2.4 | +2.1 | +0.0 | 76.9 | 110.7 | -33.8 | H+V |
|  |  |  | -27.3 | +24.4 | +6.2 | +9.2 | FM 12.5k |  |  |  |  |
| 12 | 960.000 M | 28.6 | +0.0 | +0.4 | +2.5 | +2.1 | +0.0 | 46.8 | 54.0 | -7.2 | H+V |
|  |  |  | -27.1 | +24.8 | +6.3 | +9.2 |  |  | FM 12.5k |  |  |

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| Band Edge Summary |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Frequency (MHz) | Modulation | Ant. Type | Field Strength (dBuV/m @3m) | $\begin{gathered} \text { Limit } \\ \text { (dBuV/m@3m) } \end{gathered}$ | Results |
| 614 | AM | External <br> Monopole | 41.5 | <46.0 | Pass |
| 902 | AM | External Monopole | 95.2 | <110.7 | Pass |
| 928 | AM | External Monopole | 97.4 | <110.7 | Pass |
| 960 | AM | External Monopole | 46.5 | <54 | Pass |
| 614 | FM12.5k | External Monopole | 42.3 | <46.0 | Pass |
| 902 | FM12.5k | External Monopole | 89.2 | <110.7 | Pass |
| 928 | FM12.5k | External Monopole | 76.9 | <110.7 | Pass |
| 960 | FM12.5k | External <br> Monopole | 46.8 | <54 | Pass |
| 614 | FM37.5k | External Monopole | 41.1 | <46.0 | Pass |
| 902 | FM37.5k | External Monopole | 89.2 | <110.7 | Pass |
| 928 | FM37.5k | External Monopole | 76.7 | <110.7 | Pass |
| 960 | FM37.5k | External Monopole | 46.9 | <54 | Pass |

## Band Edge Plots



Band Edge Low AM Zoom
Ref Level $114.99 \mathrm{~dB} \mu \mathrm{~V}$ ATTEN 20 dB
RES BW: 120.0 kHz VID BW: 360.0 kHz SWP: 20.0 msec
Marker: $902.0 \mathrm{MHz} 78.4857 \mathrm{~dB} \mathrm{\mu} \mathrm{~V}$

15.247(d) / 15.209 Radiated Spurious Emissions


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### 15.35(c) Duty Cycle Correction Factor

| Test Data Summary |  |  |  |
| :---: | :---: | :---: | :---: |
| Antenna <br> Port | Operational Mode | Measured On Time <br> $(\mathrm{mS} /$ Pobs | Calculated DCCF <br> (dB) |
| 1 | FM 37.5k (worst case) | 0.2387 | -12.44 |

Observation Period, $\mathrm{P}_{\text {obs }}$ is the duration of the pulse train or maximum 100 mS

Measured results are calculated as follows:

$$
\text { On Time }=\left.\left(\sum_{\text {Bursts }} R F \text { Burst On Time }+\sum_{\text {Control }} \text { Control Signal On time }\right)\right|_{P_{o b s}(\max 100 \mathrm{~ms})}
$$

Measured Values:

| Parameter | Value |
| :--- | :--- |
| Observation Period (Pobs): | 100 mS |
| Number of RF Bursts / Pobs:: | 1 |
| On time of RF Burst: | 23.87 mS |
| Number of Control or other signals / Pobs: | 0 |
| On time of Control or other Signals: | 0 |
| Total Measured On Time: | 23.87 mS |

Duty Cycle Correction Factor (DCCF) is calculated in accordance with ANSI C63.10:

$$
D C C F=20 \cdot \log \left(\frac{\text { On Time }}{P_{o b s}}\right)
$$

## Duty Cycle Correction Factor Test Data



## Test Setup Photo(s)


$9 \mathrm{kHz}-1 \mathrm{GHz}$


Note: Photo below shows setup for preliminary measurements; final measurements were taken with cables $>40 \mathrm{~cm}$ off ground plane.

$1-13 \mathrm{GHz}$

## SUPPLEMENTAL INFORMATION

## Measurement Uncertainty

| Uncertainty Value | Parameter |
| :---: | :---: |
| 4.73 dB | Radiated Emissions |
| 3.34 dB | Mains Conducted Emissions |
| 3.30 dB | Disturbance Power |

Reported uncertainties represent expanded uncertainties expressed at approximately the 95\% confidence level using a coverage factor of $\mathrm{k}=2$. Compliance is deemed to occur provided measurements are below the specified limits.

## Emissions Test Details

## TESTING PARAMETERS

Unless otherwise indicated, the following configuration parameters are used for equipment setup: The cables were routed consistent with the typical application by varying the configuration of the test sample. Interface cables were connected to the available ports of the test unit. The effect of varying the position of the cables was investigated to find the configuration that produced maximum emissions. Cables were of the type and length specified in the individual requirements. The length of cable that produced maximum emissions was selected.

The equipment under test (EUT) was set up in a manner that represented its normal use, as shown in the setup photographs. Any special conditions required for the EUT to operate normally are identified in the comments that accompany the emissions tables.

The emissions data was taken with a spectrum analyzer or receiver. Incorporating the applicable correction factors for distance, antenna, cable loss and amplifier gain, the data was reduced as shown in the table below. The corrected data was then compared to the applicable emission limits. Preliminary and final measurements were taken in order to ensure that all emissions from the EUT were found and maximized.

## CORRECTION FACTORS

The basic spectrum analyzer reading was converted using correction factors as shown in the highest emissions readings in the tables. For radiated emissions in $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$, the spectrum analyzer reading in $\mathrm{dB} \mu \mathrm{V}$ was corrected by using the following formula. This reading was then compared to the applicable specification limit. Individual measurements were compared with the displayed limit value in the margin column. The margin was calculated based on the limit value subtracting the corrected measured value; a negative margin represents a measurement less than the limit while a positive margin represents a measurement exceeding the limit.

| SAMPLE CALCULATIONS |  |  |  |
| :--- | :--- | :--- | :---: |
|  | Meter reading | $(\mathrm{dB} \mu \mathrm{V})$ |  |
| + | Antenna Factor | $(\mathrm{dB} / \mathrm{m})$ |  |
| + | Cable Loss | $(\mathrm{dB})$ |  |
| - | Distance Correction | $(\mathrm{dB})$ |  |
| - | Preamplifier Gain | $(\mathrm{dB})$ |  |
| $=$ | Corrected Reading | $(\mathrm{dB} \mu \mathrm{V} / \mathrm{m})$ |  |

## TEST INSTRUMENTATION AND ANALYZER SETTINGS

The test instrumentation and equipment listed were used to collect the emissions data. A spectrum analyzer or receiver was used for all measurements. Unless otherwise specified, the following table shows the measuring equipment bandwidth settings that were used in designated frequency bands. For testing emissions, an appropriate reference level and a vertical scale size of 10 dB per division were used.

| MEASURING EQUIPMENT BANDWIDTH SETTINGS PER FREQUENCY RANGE |  |  |  |
| :---: | :---: | :---: | :---: |
| TEST | BEGINNING FREQUENCY | ENDING FREQUENCY | BANDWIDTH SETTING |
| CONDUCTED EMISSIONS | 150 kHz | 30 MHz | 9 kHz |
| RADIATED EMISSIONS | 9 kHz | 150 kHz | 200 Hz |
| RADIATED EMISSIONS | 150 kHz | 30 MHz | 9 kHz |
| RADIATED EMISSIONS | 30 MHz | 1000 MHz | 120 kHz |
| RADIATED EMISSIONS | 1000 MHz | $>1 \mathrm{GHz}$ | 1 MHz |

## SPECTRUM ANALYZER/RECEIVER DETECTOR FUNCTIONS

The notes that accompany the measurements contained in the emissions tables indicate the type of detector function used to obtain the given readings. Unless otherwise noted, all readings were made in the "positive peak" detector mode. Whenever a "quasi-peak" or "average" reading was recorded, the measurement was annotated with a "QP" or an "Ave" on the appropriate rows of the data sheets. In cases where quasi-peak or average limits were employed and data exists for multiple measurement types for the same frequency then the peak measurement was retained in the report for reference, however the numbering for the affected row was removed and an arrow or caret (" $\wedge$ ") was placed in the far left-hand column indicating that the row above takes precedence for comparison to the limit. The following paragraphs describe in more detail the detector functions and when they were used to obtain the emissions data.

## Peak

In this mode, the spectrum analyzer or receiver recorded all emissions at their peak value as the frequency band selected was scanned. By combining this function with another feature called "peak hold," the measurement device had the ability to measure intermittent or low duty cycle transient emission peak levels. In this mode the measuring device made a slow scan across the frequency band selected and measured the peak emission value found at each frequency across the band.

## Quasi-Peak

Quasi-peak measurements were taken using the quasi-peak detector when the true peak values exceeded or were within 2 dB of a quasi-peak specification limit. Additional QP measurements may have been taken at the discretion of the operator.

## Average

Average measurements were taken using the average detector when the true peak values exceeded or were within 2 dB of an average specification limit. Additional average measurements may have been taken at the discretion of the operator. If the specification or test procedure requires trace averaging, then the averaging was performed using 100 samples or as required by the specification. All other average measurements are performed using video bandwidth averaging. To make these measurements, the test engineer reduces the video bandwidth on the measuring device until the modulation of the signal is filtered out. At this point the measuring device is set into the linear mode and the scan time is reduced.


[^0]:    - Readings
    $\times$ QP Readings
    - Ambient

[^1]:    - Readings
    $\times$ QP Readings
    - Ambient

