Exhibit 6

INDEX OF TEST RESULTS

Exhibit #	Description
6A	800 band/Part 22: RF Power
6B	800 band/Part 22: Modulation Characteristics
6C	800 band/Part 22: Occupied bandwidth
6D	800 band/Part 22: Spurious Emissions (conducted)
6E	800 band/Part 22: Spurious Emissions (radiated)
6F	800 band/Part 22: Frequency Stability
6G	1900MHz/Part 24: RF Power
6H	1900MHz/Part 24: Modulation Characteristics
61	1900MHz/Part 24: Occupied bandwidth
6J	1900MHz/Part 24: Spurious Emissions (conducted)
6K	1900MHz/Part 24: Spurious Emissions (radiated)
6L	1900MHz/Part 24: Frequency Stability

EXHIBIT 6A1

800 MHz: RF POWER OUTPUT

Para. 2.985 (a) and 22.913 (a)

The RF power measured at the output terminals (antenna connector) is plotted against supply voltage variation and temperature variations at the highest levels.

Supply

Exhibit	Voltage (V)	Temperature	TX Freq	Output (W)	Power Level	Analog/Digital
6A2	4.8	Varied	Mid Band	.4 W	0	Analog
6A3	Varied	+25 C	Mid Band	.4 W	0	Analog
6A4	4.8	Varied	Mid Band	.4 W	0	Digital
6A5	Varied	+25 C	Mid Band	.4 W	0	Digital

The measurements were made per IS-137A using a Hewlett Packard 8953DT North American Dual Mode Cellular Test System which includes the following equipment:

HP8958A Cellular Interface
HP6623A DC Power Supply
HP8596E Spectrum Analyzer
HP437B RF Power Meter
HP8901B Modulation Analyzer
HP8903B Audio Analyzer

Thermotron SM-8C Temperature Chamber

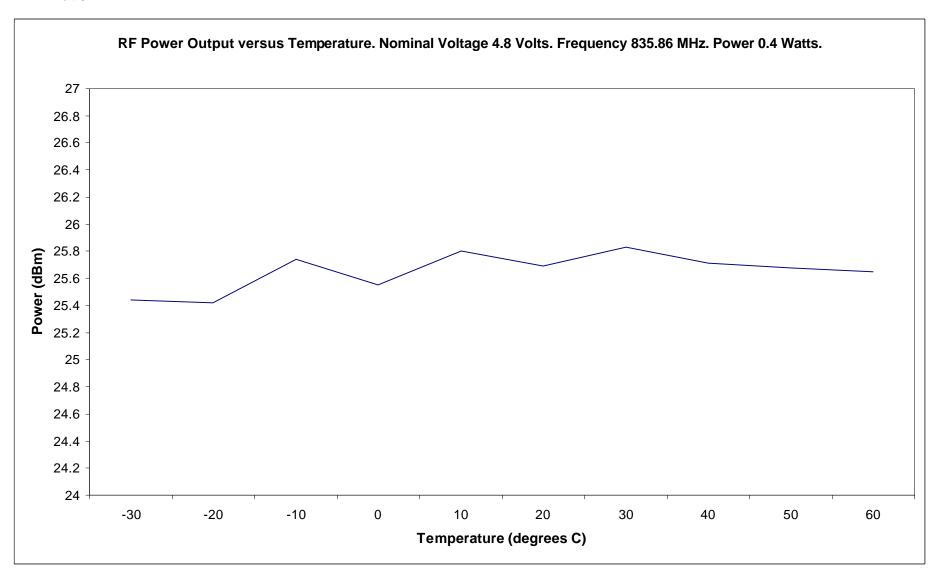
EFFECTIVE RADIATED POWER

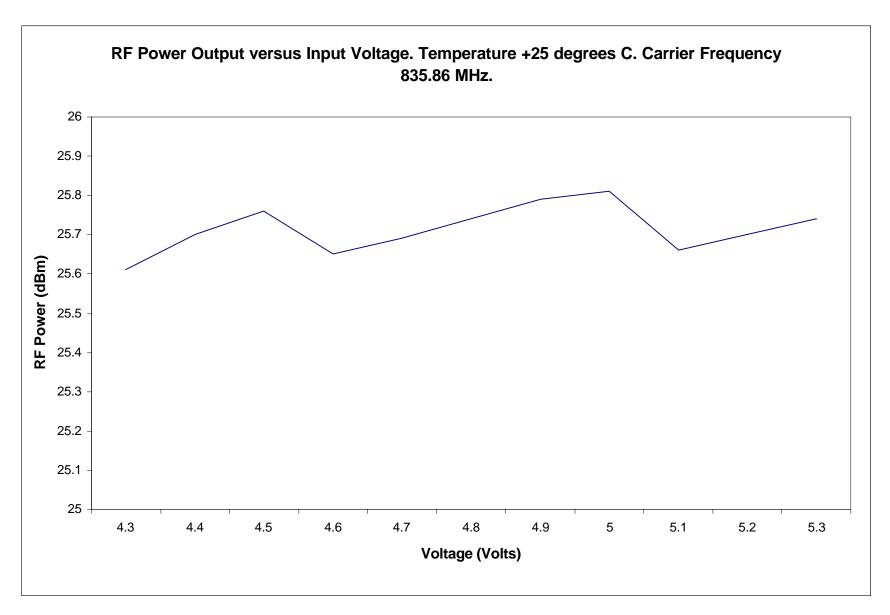
The following is a description of the substitution method used in accordance with IS-137A to obtain accurate ERP readings at the carrier fundamental frequency:

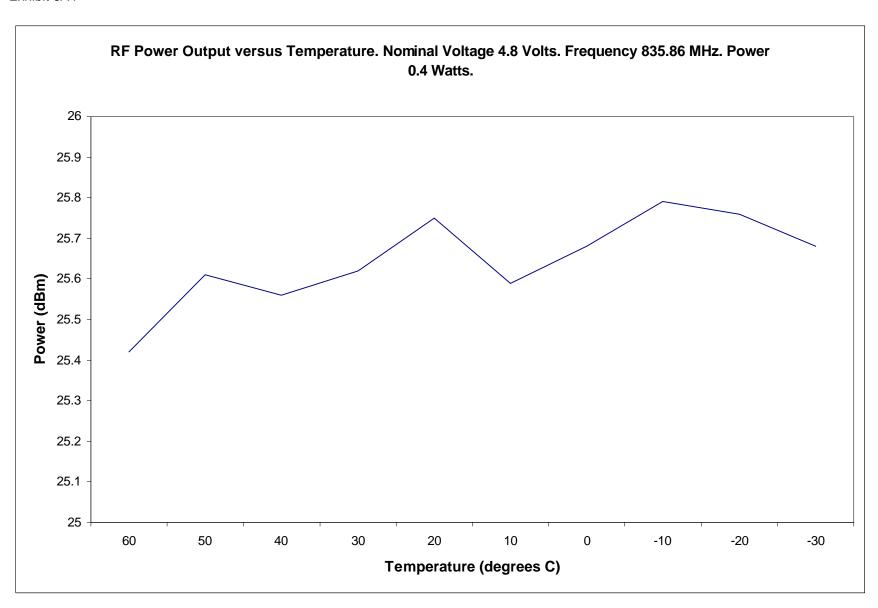
- (1) EUT measurements are made at 3 m using calibrated antennas and equipment with known cable losses.
- (2) A peak measurement is made by raising and lowering the antenna and rotating the EUT 360 degrees. Horizontal and vertical polarization data is recorded.
- (3) A generator and dipole antenna are then substituted for the EUT. The dipole antenna is a half-wave dipole. If a dipole antenna cannot be used, then the designated antenna is referenced to a dipole antenna.
- (4) Measurements are made through the dipole antenna at known power levels to determine the system calibration factors at a given frequency.
- (5) At frequencies where no calibration data is taken, the value is interpolated between the closest data point above and below the transmit frequency. Calibration data is taken with a half-wave dipole antenna.

Measurements at a distance of 3 m from the source at the highest power level setting:

Frequency (MHz)	Rated Output Power (W)	EDRP (dBm)
836.49	0.214	23.3







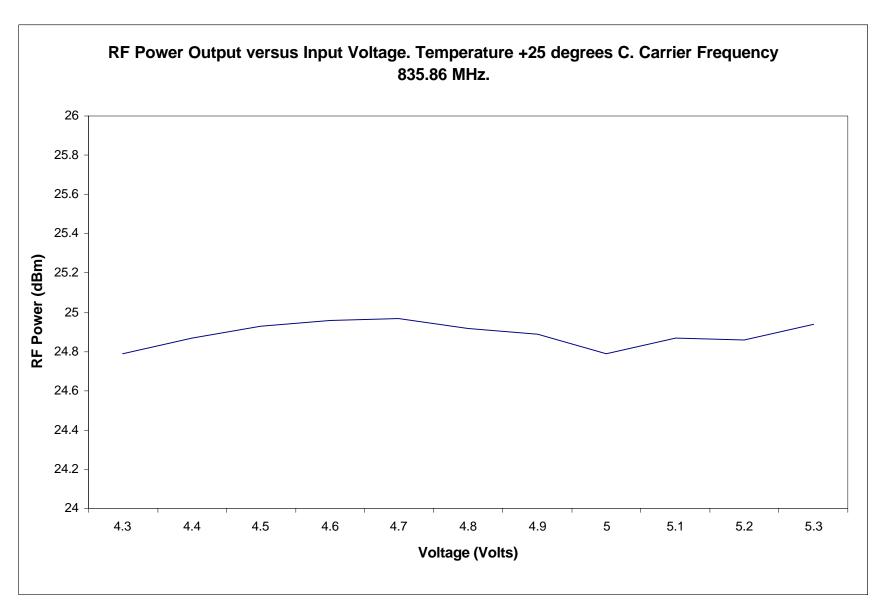


EXHIBIT 6B1

800 MHz: MODULATION CHARACTERISTICS

Per 2.987 (a), (b), (d) and 22.915 (b)(4)

The frequency and amplitude response to audio inputs measured per IS-137A are shown on the following:

Exhibit

6B2	Transmit Audio Frequency Response	2.987 (a)
6B3	Post Limiter Filter Attenuation	22.915 (d)(1)
6B4	Modulation Limiting vs. Frequency	22.915 (b)(1)
6B5	Modulation Limiting vs. Input Voltage	2.987 (b)

The measurements were made per IS-137A using a Hewlett Packard 8953DT North American Dual Mode Cellular Test System which includes the following equipment:

HP8958A Cellular Interface

HP 6623A DC Power Supply

HP 8596E Spectrum Analyzer

HP 437B RF Power Meter

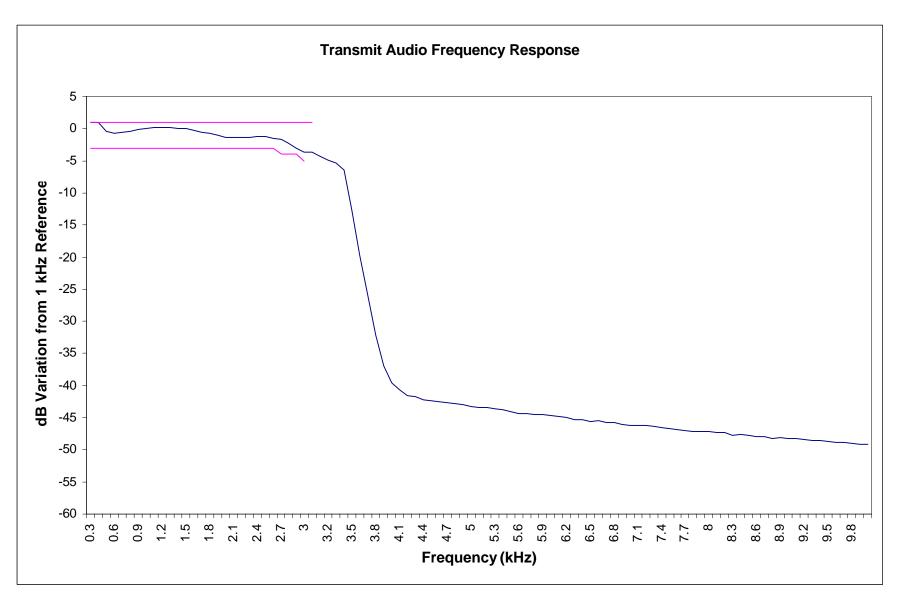
HP 8901B Modulation Analyzer

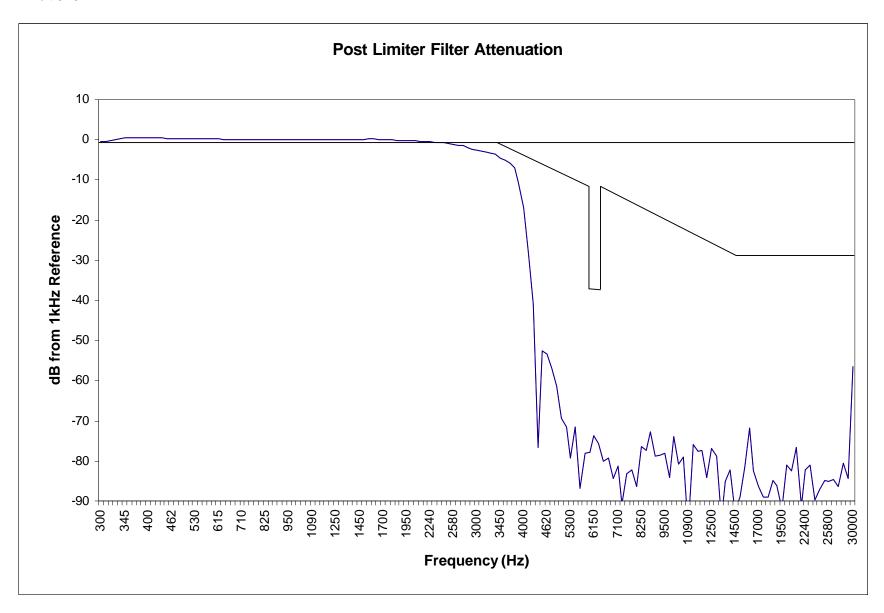
HP 8903B Audio Analyzer

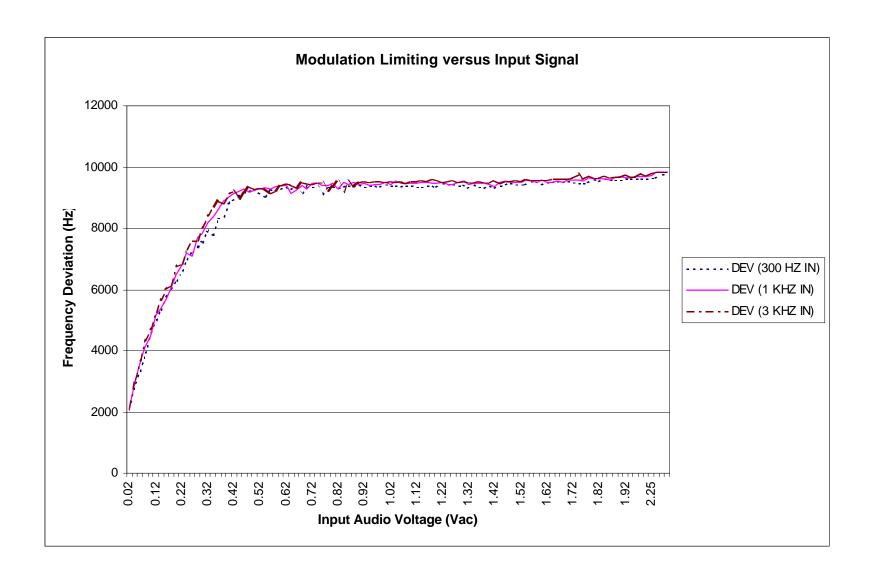
HP 35679 Signal Analyzer

B&KJ 2012 B&K Audio Analyzer (Exhibit 6B3 only)

Thermotron SM-8C Temperature Chamber







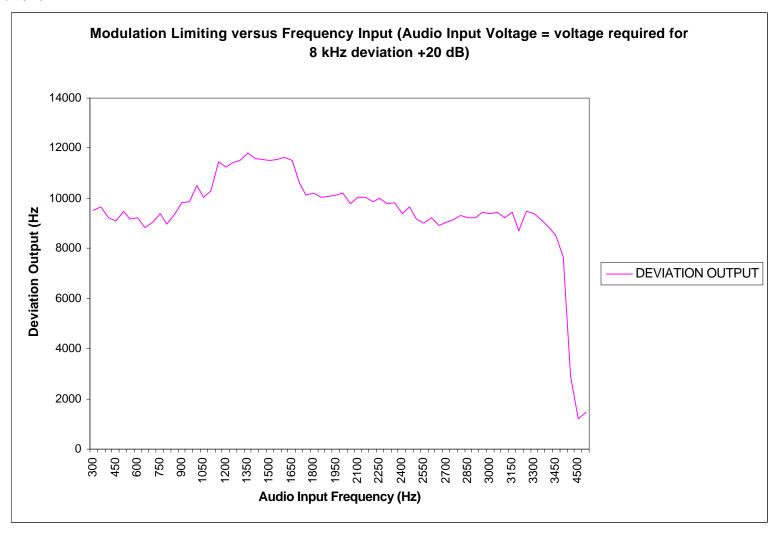


EXHIBIT 6C1

800 MHz: OCCUPIED BANDWIDTH

Per 2.989 (c), (1) (h) and 22.917 (d)(1) the exhibits presented show the modulations that co-exist in a cellular system:

The method of measuring occupied bandwidth of a US digital cellular is different from the analog FM signal. The traditional method for specifying occupied bandwidth of a FM signal is to use a mask drawn over the spectral plot of the modulated signal. If any point of the modulation signal exceeds the mask a failure is noted.

A different method is used for the US DAMPS system. This is described in the TIA IS 137A document. The method employed in digital applications is to measure average power within a 30kHz bandwidth corresponding to a channel bandwidth for he system. This measurement is used to determine and specify power in neighboring channels relative to the fundamental occupied channel; i.e.: the average power in the adjacent channels is compared to the average power in the fundamental channel for specifying occupied bandwidth.

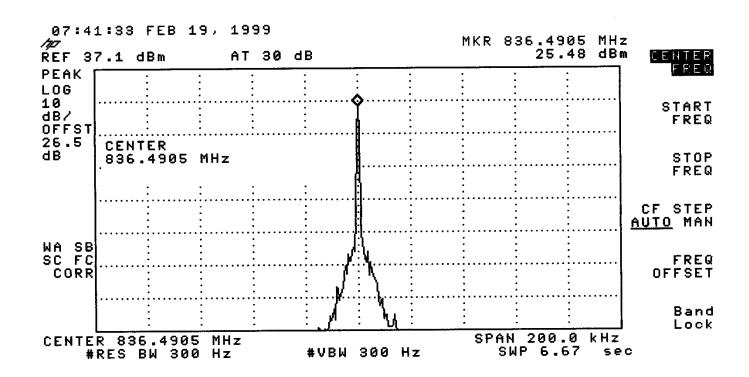
The power in each channel is an average of all the energy within that channel. This is less than the peak within the channel due to the nature of an average power measurement. This characteristic of measuring average power prohibits the use of a spectral mask. The mask could only be drawn relative to the spectral peaks and would not give an indication of the average power as specified in IS 137A, section 3.4.1.2. Consequently, the only way to accurately measure and specify occupied bandwidth for DAMPS is with special equipment designed to collect all the energy within a specified bandwidth and display the average power of this energy. This can't be done with a simple spectrum analyzer measurement as was traditionally possible for FM only signals.

Exhibit #	Description	Power Level
6C2	Unmodulated Carrier	0
6C3	SAT and Voice	0
6C4	SAT and Signal Tone	0
6C5	SAT and DTMF #3	0
6C6	SAT and 10kb/s Wideband Data	0
6C7	Unmodulated Carrier	7
6C8	SAT and Voice	7
6C9	SAT and Signal Tone	7
6C10	SAT and DTMF #3	7
6C11	SAT and 10 kb/s Wideband Data	7

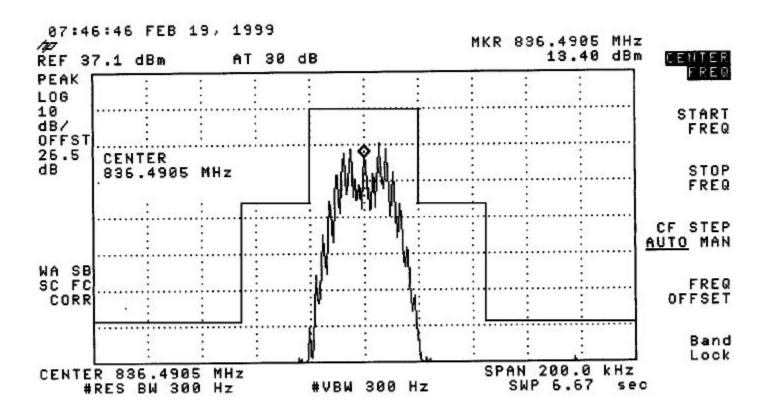
All deviations are set independently of each other and limits and nominal values per Exhibit 12.

These measurements wee made per IS-137A using a Hewlett Packard 8953DT North American Dual Mode Cellular Test System which includes the following equipment:

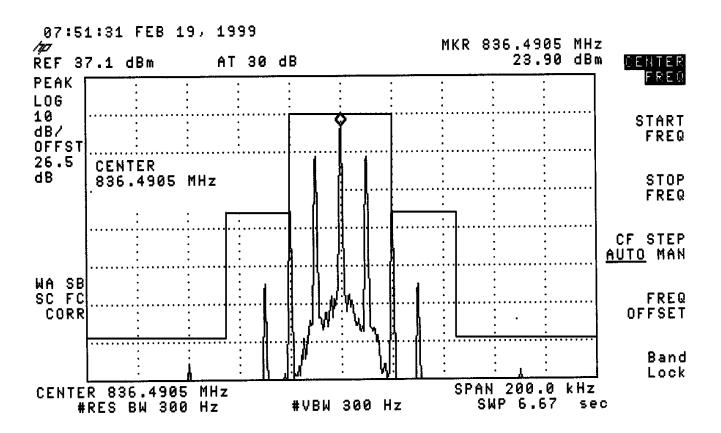
HP 8958A	Cellular Interface
HP 6623A	DC Power Supply
HP 8596E	Spectrum Analyzer
HP 437B	RF Power Meter
HP 8901B	Modulation Analyzer
HP 8903B	Audio Analyzer
Thermotron SM-8C	Temperature Chamber



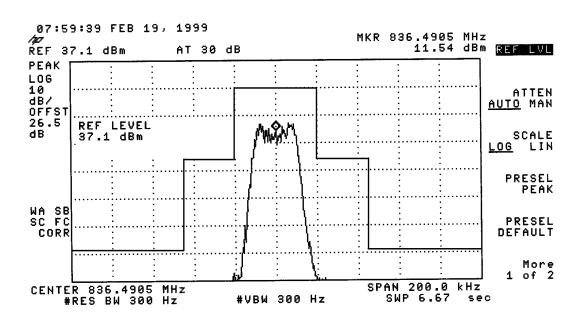
Unmodulated Carrier. Power Level 0, Carrier Frequency 836.49 MHz, Carrier Power 25.48 dBm.



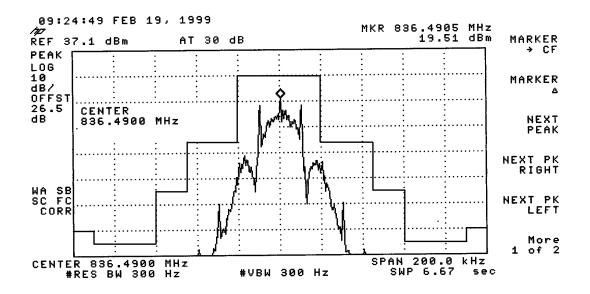
SAT and Voice. Power Level 0, Carrier Frequency 836.49 MHz, Carrier Power 25.48 dBm. Voice Tone 2500 Hz, SAT 6000 Hz, Total Deviation 11000Hz. F3E Emissions Mask.



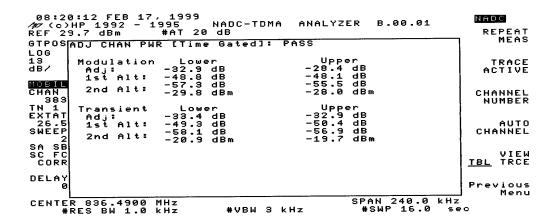
SAT and Signalling Tone. Power Level 0, Carrier Frequency 836.49 MHz, Carrier Power 25.48 dBm. F3E Emissions Mask.

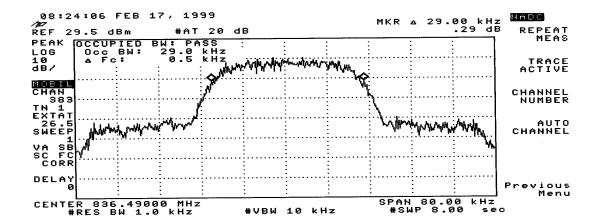


SAT and DTMF #3. Power Level 0, Carrier Frequency 836.49 MHz, Carrier Power 25.48 dBm. F3E Emissions Mask

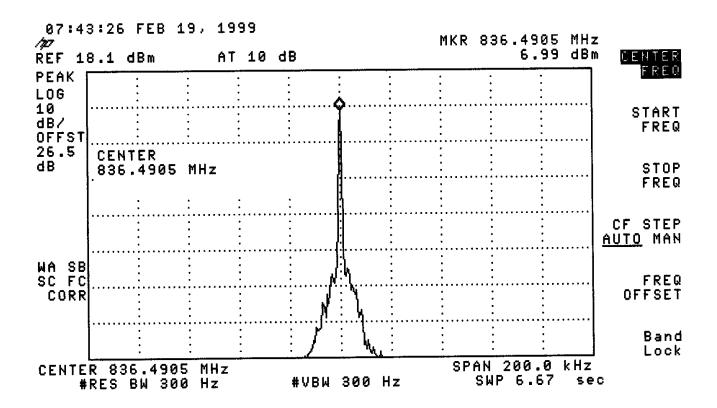


SAT and Wideband 10 kb/S Digital data. Power Level 0, Carrier Frequency 836.49 MHz, Carrier Power 25.48 dBm. F1D Emissions Mask.

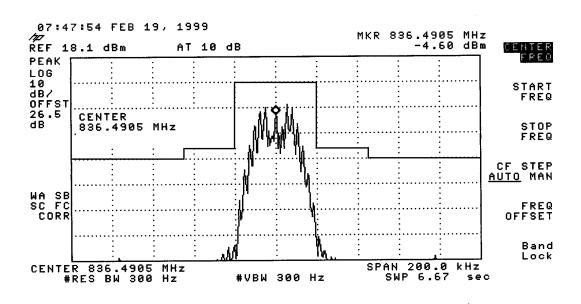




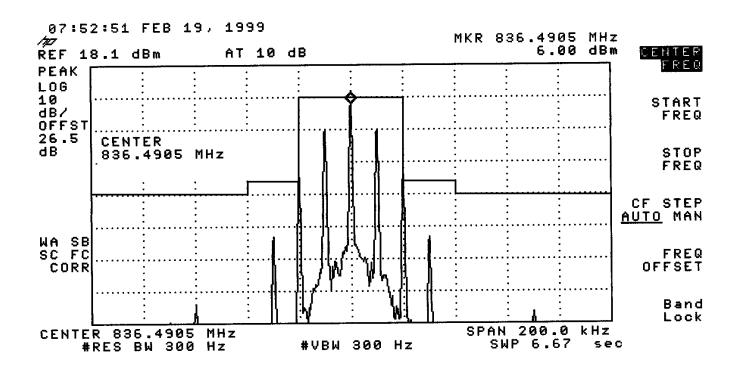
Wideband Data 48.6 kb/s switched (Data). Power Level 0, Carrier Frequency 836.49 MHz, Carrier Power 25.43 dBm. Plots showing occupied bandwidth of 28.8 kHz and alternate and adjacent power



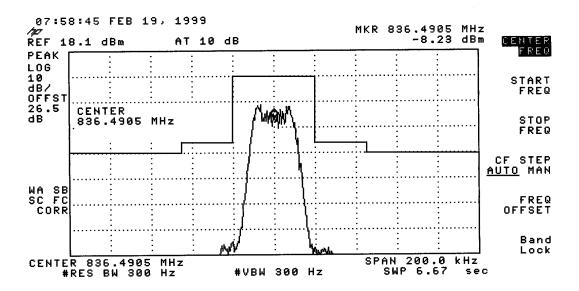
Unmodulated Carrier. Power Level 7, Carrier Frequency 836.49 MHz, Carrier Power 6.99 dBm.



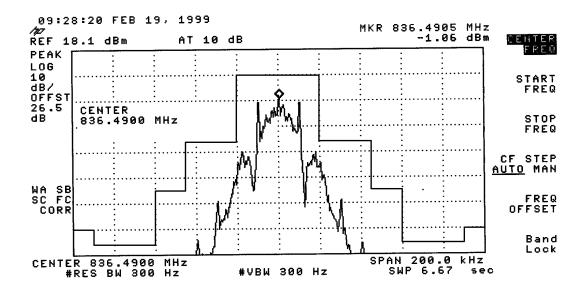
SAT and Voice. Power Level 7, Carrier Frequency 836.49 MHz, Carrier Power 6.99 dBm. F3E Emissions Mask.



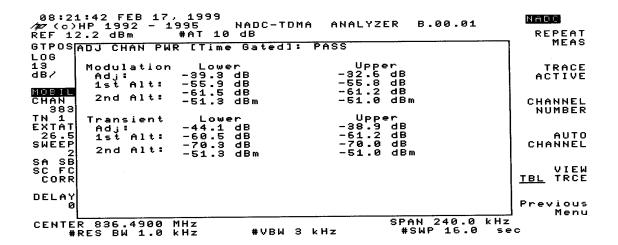
SAT and Signalling Tone. Power Level 7, Carrier Frequency 836.49 MHz, Carrier Power 6.99 dBm. F3E Emissions Mask.

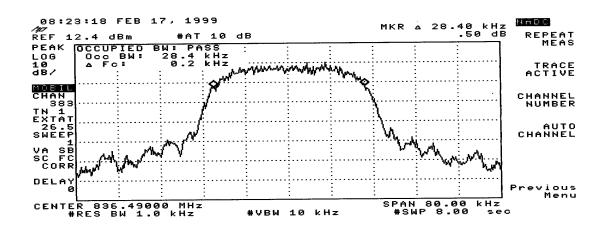


SAT and DTMF #3. Power Level 7, Carrier Frequency 836.49 MHz, Carrier Power 6.99 dBm. F3E Emissions Mask.



SAT and Wideband 10 kb/S Digital data. Power Level 7, Carrier Frequency 836.49 MHz, Carrier Power –4.51 dBm. F1D Emissions Mask.





Wideband Data 48.6 kb/s switched (Data). Power Level 7, Carrier Frequency 836.49 MHz, Carrier Power 6.99 dBm.

Plots showing occupied bandwidth of 28.4 kHz and alternate and adjacent power.

EXHIBIT 6D1

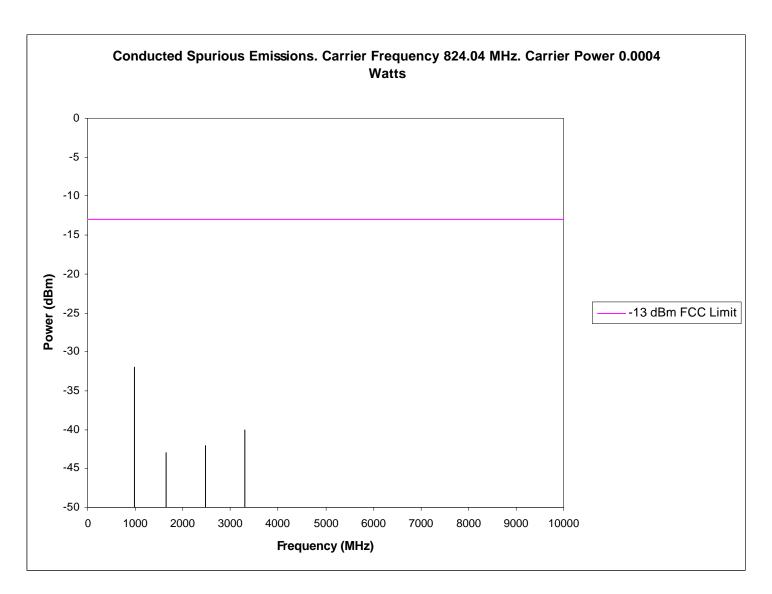
800 MHz: SPURIOUS EMISSIONS (CONDUCTED)

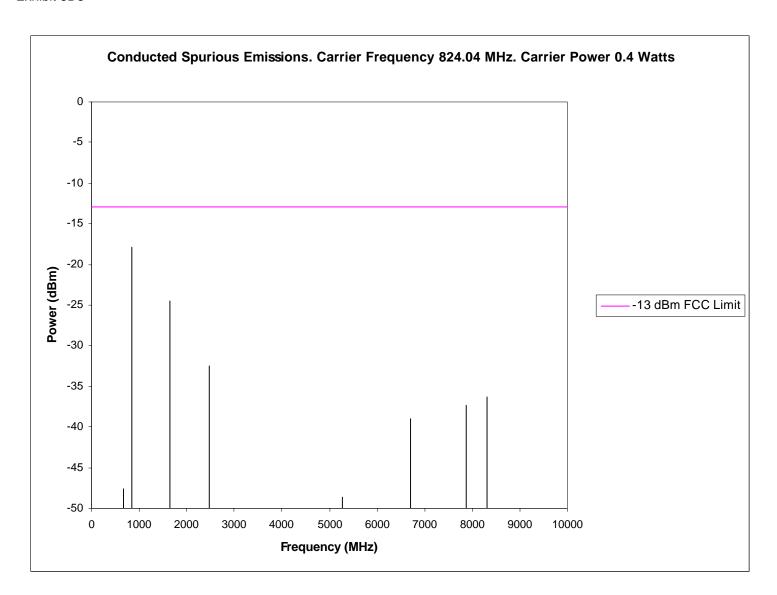
Per 2.991 Spurious emissions at the antenna terminals (conducted) when properly loaded with an appropriate artificial antenna were measured per IS-137A.

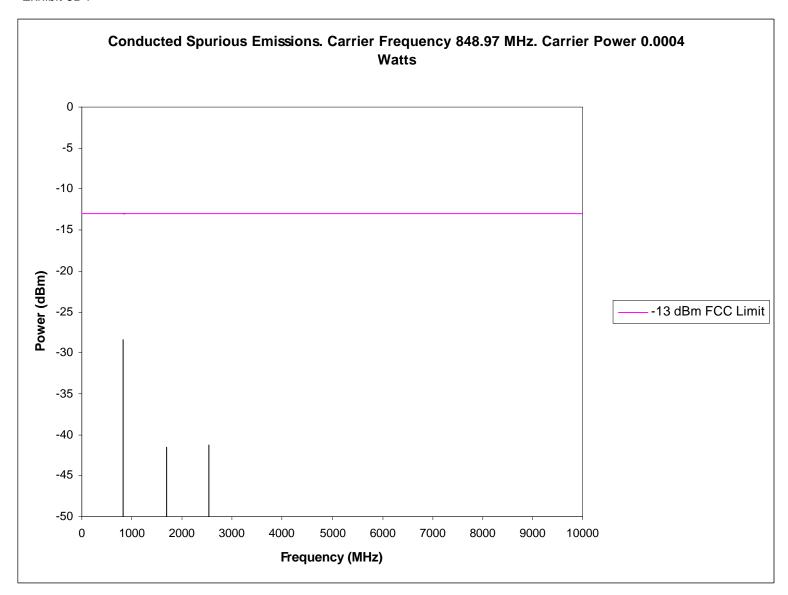
EXHIBIT #	FREQUENCY	Output Power
6D2	824.04	.0004
6D3	824.04	.4
6D4	848.97	.0004
6D5	848.97	.4

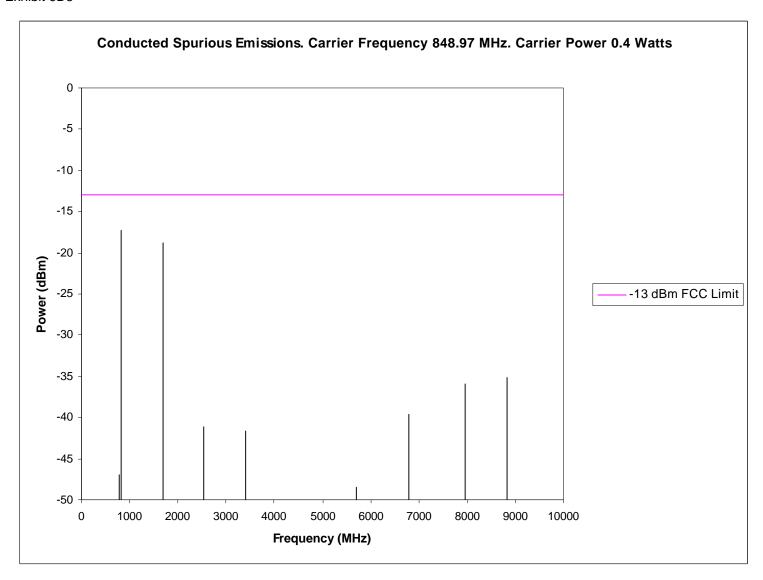
The measurements were made per IS-137A using the following equipment:

Hp 8958A	Cellular Interface
Hp 8901B	Modulation Analyzer
Hp 8559A	Spectrum Analyzer









APPLICANT: FCC ID NO:

ERICSSON INC AXATR-392-A2 EXHIBIT 6E1

800 MHz: SPURIOUS EMISSIONS (Radiated)

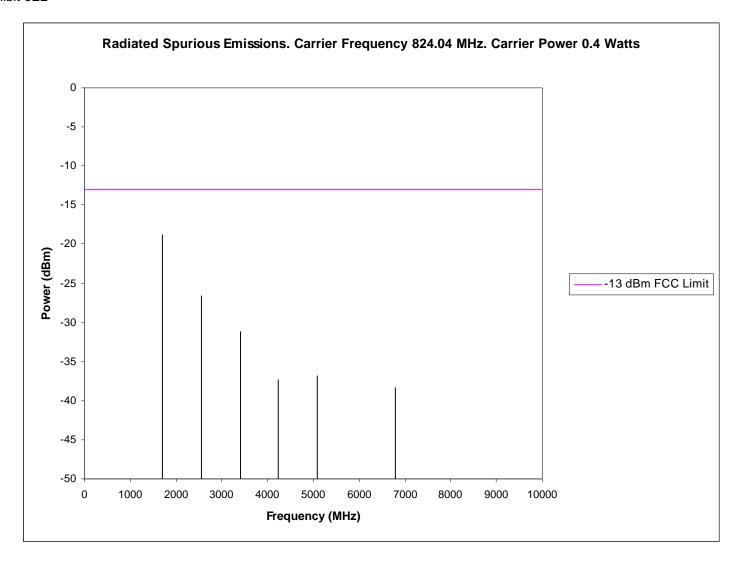
Per 2.993 and 22.917 (e), field strength of spurious radiation was measured at Underwriters Laboratories Inc. Research Triangle Park, NC site. Underwriter Laboratories Inc. Research Triangle site is NVLAP and FCC registered. The measurement procedure is per EIA IS-137 conducted on a 3 meter test site. Results are shown on the following Exhibits.

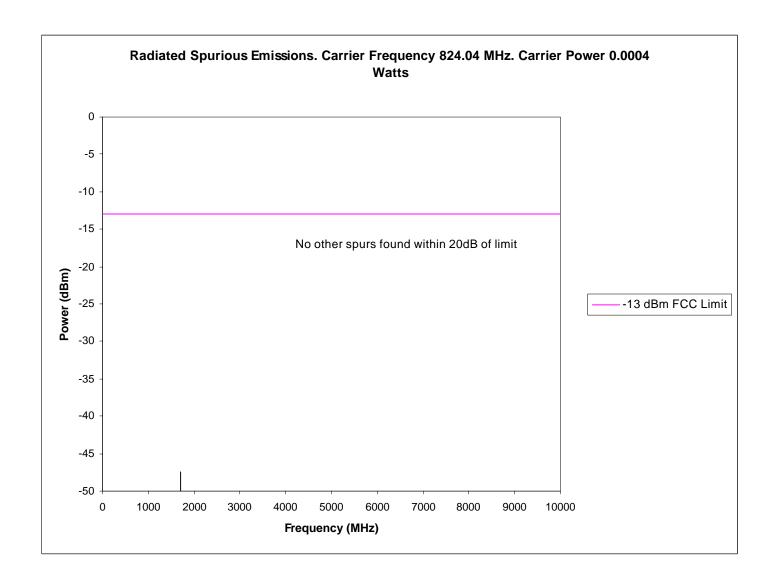
Note: The spectrum was examined through the 10^{th} harmonic of the carrier. Measurements recorded are peak measurements.

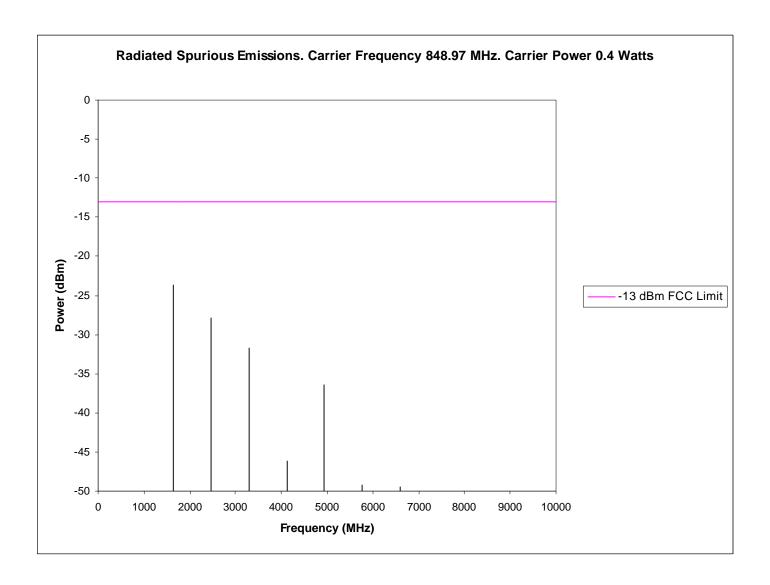
<u>EXHIBIT</u>	FREQUENCY	OUTPUT POWER
6E2	824.04/channel 799	.4
6E3	824.04 channel 799	.0004
6E4	848.97 channel 991	.4
6E5	848.97 channel 991	.0004

The measurements were made per IS-137A using the following equipment:

8566B Spectrum Analyzer 100 Hz - 2.5GHz \ 2 - 22 GHz 85650A Quasi Peak Detector HP Amplifier 8449B Opt H02 1 - 26.5 GHz HP Signal Generator 8657B .1 - 2060 MHz







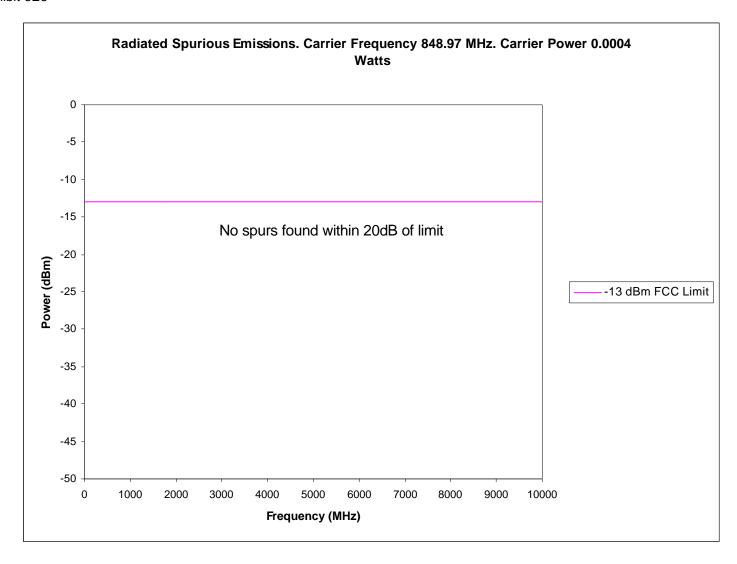


EXHIBIT 6F1

800 MHz: FREQUENCY STABILITY

Per 2.995 (a)(1),(b),(d)(1)

Per 2.995 (a)(1),(b),(d)(1), variation of output frequency as a result of Varying either voltage or temperature is shown in Exhibit 6F2 and 6F3 respectively.

EXHIBIT #	Voltage	<u>Temperature</u>
6F2	4.3 to 5.3 Volts (varied)	+25 C
6F3	4.8 Volts	Varied

Note: The manufacturers rated voltage for the battery is 4.3 VDC to 5.3 VDC.

The measurements were made per IS-137A using a Hewlett Packard 8953DT North American Dual Mode Cellular Test System which includes the following equipment:

HP8958A Cellular Interface
HP 6623A DC Power Supply
HP 8596E Spectrum Analyzer
HP 437B RF Power Meter
HP 8901B Modulation Analyzer
HP 8903B Audio Analyzer
Thermotron SM-8C Temperature Chamber

Exhibit 6F2

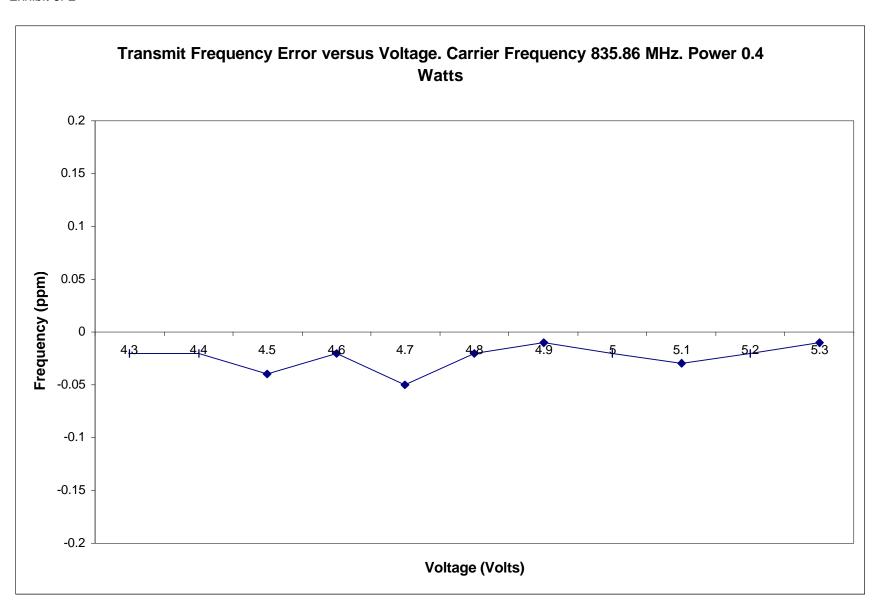


Exhibit 6F3

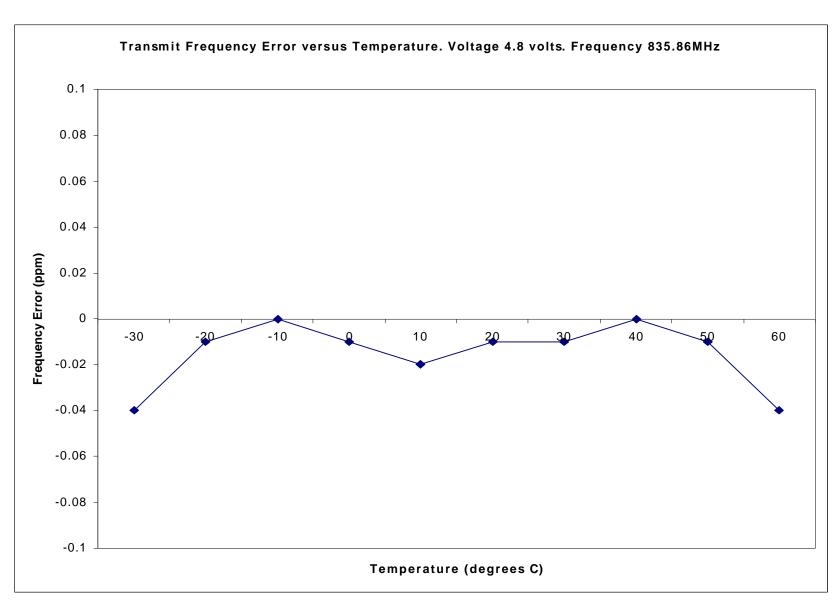


EXHIBIT 6G1

1900 MHz: RF POWER OUTPUT

Para. 2.985 (a)

The RF Power measured at the output terminals (antenna connector) is plotted against supply voltage variations at the highest levels.

EXHIBIT	SUPPLY VOLTAGE (V)	TEMPERATURE	POWER LEVEL	TX FREQ Output (Watts)
6G2	4.8Volts	Varied	0	Mid Band .4
6G3	Varied	+ 25 C	0	Mid Band .4

Output power was measured conducted, via a standard antenna connector.

The measurements were made per IS137A using the following equipment:

Hewlett Packard 8593 E Spectrum Analyzer Hewlett Packard 8566 B Spectrum Analyzer Hewlett Packard 437B Power Meter Thermotron SM-8C temperature Chamber

EFFECTIVE ISOTROPIC RADIATED POWER

The following is a description of the substitution method used to obtain accurate EIRP readings at the carrier fundamental frequency:

- (1) EUT measurements are made at 3 m using calibrated antennas and equipment with known cable losses.
- (2) A peak measurement is made by raising and lowering the antenna and rotating the EUT 360 degrees. Horizontal and Vertical Polarization data is recorded.
- (3) A generator and dipole antenna are then substituted for the EUT. The dipole antenna is a half-wave dipole. If a dipole antenna cannot be used, then the designated antenna is referenced to a dipole antenna.
- (4) Measurements are made through the dipole antenna at known power levels to determine the system calibration factors at a given frequency.
- (5) At frequencies where no calibration data is taken, the value is interpolated between the closest data point above and below the transmit frequency. Calibration data is taken with a half-wave dipole antenna.

Measurements at a distance of 3 m from the source at the highest power level setting:

Frequency (MHz)	Rated Output Power (W)	EIRP (dBm)
1879.98	0.375	25.7

Exhibit 6G2

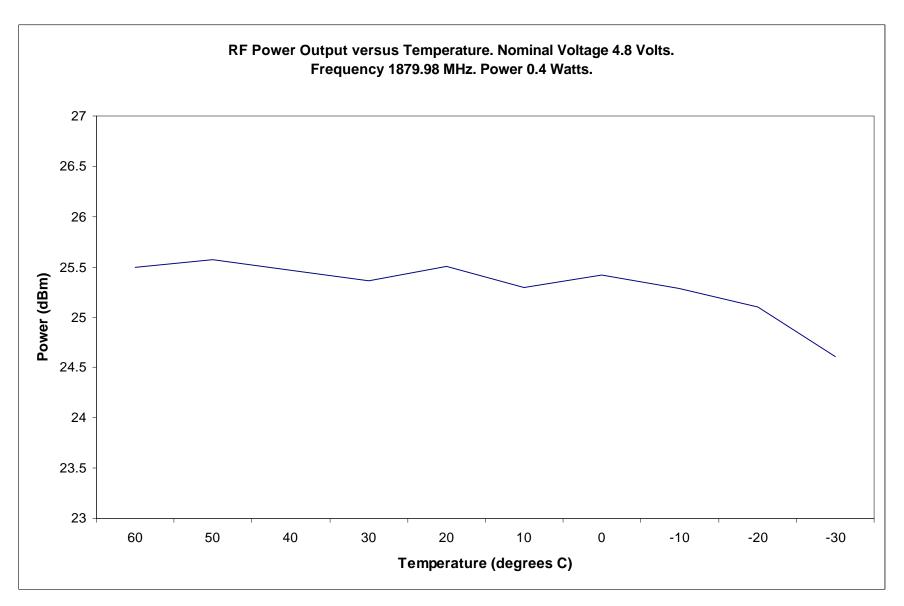


Exhibit 6G3

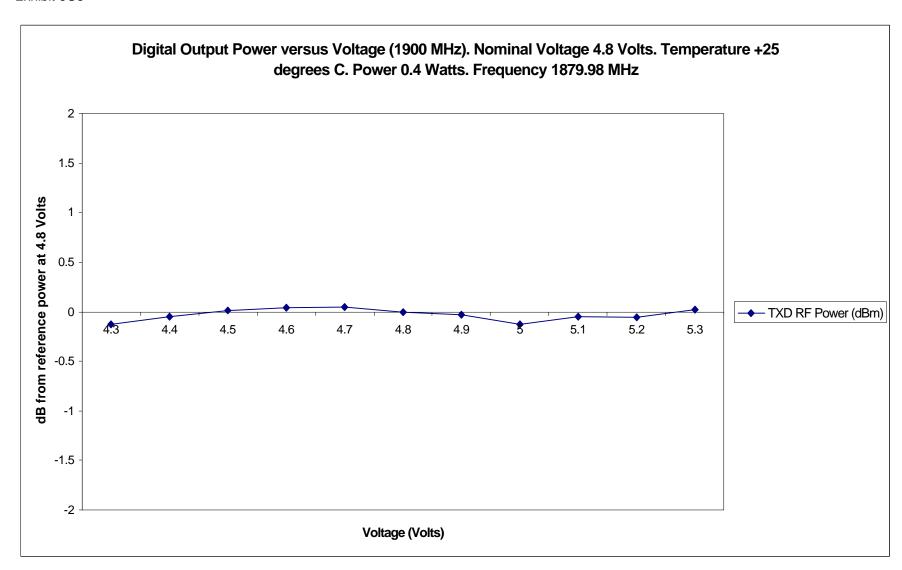


EXHIBIT 6H1

800/1900 MHz: MODULATION CHARACTERISTICS

Definition

The transceiver shall be capable of generating $\pi/4$ shifted differentially encoded quadrature phase shift keying signals. The transmitted signal is given by:

$$S(t) = \sum_{n} g(t-nT) \cos (\phi n) \cos (\omega ct) - \sum_{n} g(t-nT) \sin (\phi n) \sin (\omega ct)$$

where g(t) is the pulse shaping function that corresponds to a square root raised cosine baseband filter with roll off factor of 0.35, ωc is the radian carrier frequency, T is the symbol period, and ϕn is the absolute phase corresponding to the nth symbol interval. The symbol rate (1/T) is 24.3 k symbols /sec.

The modulation accuracy requirement is specified by setting limits on the RMS difference between the actual transmitted signal waveform and the ideal signal waveform. The ideal waveform is derived mathematically from the specification of modulation shown above. The specified requirement is error vector magnitude.

For this measurement, frequency accuracy shall meet the requirements of Section 3.1 prior to measurement.

The average carrier frequency error is the difference between the average carrier frequency of the actual transmitted waveform and the average signal waveform carrier frequency.

The ideal modulation is defined above. The definition is such that, observing an ideal transmitter through an ideal root raised-cosine receiver filter at the correct sampling instants one symbol apart would result in the sequence of values given by:

$$j{\pi/4+B(k)^*\pi/2}$$
 S(k)=S(k-1)e

where B(k) = 0,1,2,3 according to the following table:

Xk	Yk	B(k)
0	0	0
0	1	1
1	1	2
1	0	3

In the forward channel, S(k) forms part of a continuous data stream. In the reverse channel, the transit bursts from the mobile are truncated by power up and down ramping. In this case, S(6) is the first sample that enters into demodulation, which yields the first two information bits by comparing S(6) with S(7). The last information bits lie in the comparison of S(162) and S(161).

The ideal transmit and receive filters in cascade form a raised cosine Nyquist filter having an impulse response going through zero at symbol period intervals, so there is no inter-symbol interference at the ideal sampling points. The ideal signal sampler therefore, take on one of the eight values defined above, at the output of the receive filter.

This section defines how the output signal from a transmitter is to be evaluated against the ideal signal.

Let Z(k) be the complex vectors produced by observing the real transmitter through an ideal measuring receive filter at instants k, one symbol period apart. With S(k) defined as above, the transmitter is modeled as:

$$Z(k) = [C0 + C1 * [S(k)+E(k)]] * W$$

where:

k = n/24.3KHz

dr=jda

W = e accounts for both a frequency offset giving "da" radians per symbol phase rotation and an amplitude changes of "dr" nepers per symbol:

C0 is a constant origin offset representing quadrature modulator imbalance, C1 is a complex constant representing the arbitrary phase and output power of the transmitter, and

E(k) is the residual vector error on sample S(k)

The sum square vector error is then:

 $\sum_{k = MAX} k=MAX$ $\sum_{k = MIN} |\{[Z(k) * W -C0]/C1\} -S(k)|$

C0, C1 and W shall be chosen to minimize this expression and are then used to compute the individual vector errors E(k) on each symbol. The symbol timing phase of the receiver output samples used to compute the vector error shall also be chosen to give the lowest value.

The values of MAX and MIN for the reverse channel (mobile station transmitter) are:

MIN = 6 MAX = 162

The RMS vector error is then computed as the square root of the sum-square vector divided by the number of symbols in the slot, (157 in the reverse direction).

Method of Measurement

Connect the mobile station to the Standard Test Source and Modulation Accuracy Equipment. Modulate the Standard Test Source with pseudo-random Data Field bits. The mobile station shall transpond the Data Field bits using the TDMAON command. Use the Modulation Accuracy Measurement Equipment to measure the modulation accuracy of the mobile station.

Minimum Standard

The RMS vector error in any burst shall be less than 12.5%. In addition, the normalized error vector magnitude during the first 10 symbols (20 bits) of a burst following the ramp-up, must have an RMS value of less than 25% when averaged over 10 bursts within a 1 minute interval. The minimum standard for frequency offset is specified in section 3.1.2.2.3 of IS 137. The origin offset in any burst shall be less than -20 dBc.

EXHIBIT 611

1900 MHz: OCCUPIED BANDWIDTH

Per 2.989 (c, I, h) the exhibits presented show the modulations that have to exist in a 1900 MHz Cellular System.

All the exhibits listed below are plots where the modulation condition is Psuedorandom Data (48.6 kb/s switched), operating in the DAMPS (TDMA) mode. All plots were taken while transmitting at Power Level 0. Any frequency span not covered at the exhibits below was found to be unaffected by the transmitter/modulation.

The emissions mask is not provided for this exhibit. The method of measuring occupied bandwidth of a US digital cellular is different from the analog FM signal. The traditional method for specifying occupied bandwidth of a FM signal is to use a mask drawn over the spectral plot of the modulated signal. If any point of the modulation signal exceeds the mask a failure is noted.

A different method is used for the US DAMPS system. This is described in the TIA IS 137A document. The method employed in digital applications is to measure average power within a 30kHz bandwidth corresponding to a channel bandwidth for he system. This measurement is used to determine and specify power in neighboring channels relative to the fundamental occupied channel; i.e.: the average power in the adjacent channels is compared to the average power in the fundamental channel for specifying occupied bandwidth.

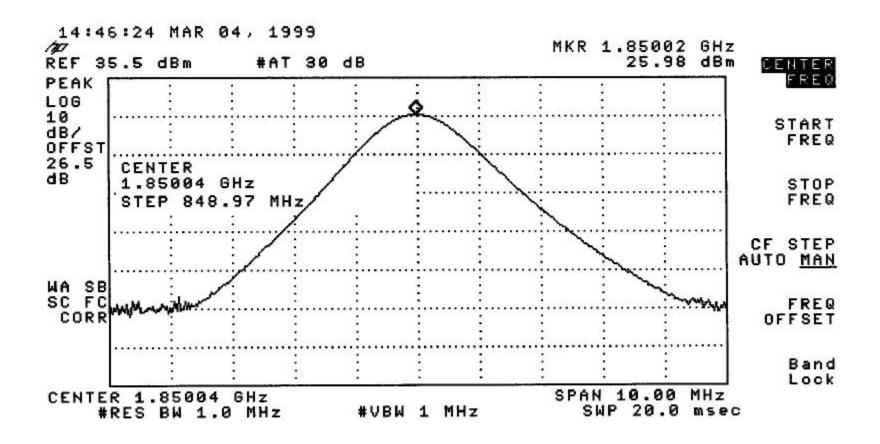
The power in each channel is an average of all the energy within that channel. This is less than the peak within the channel due to the nature of an average power measurement. This characteristic of measuring average power prohibits the use of a spectral mask. The mask could only be drawn relative to the spectral peaks and would not give an indication of the average power as specified in IS 137A, section 3.4.1.2. Consequently, the only way to accurately measure and specify occupied bandwidth for DAMPS is with special equipment designed to collect all the energy within a specified bandwidth and display the average power of this energy. This can't be done with a simple spectrum analyzer measurement as was traditionally possible for FM only signals.

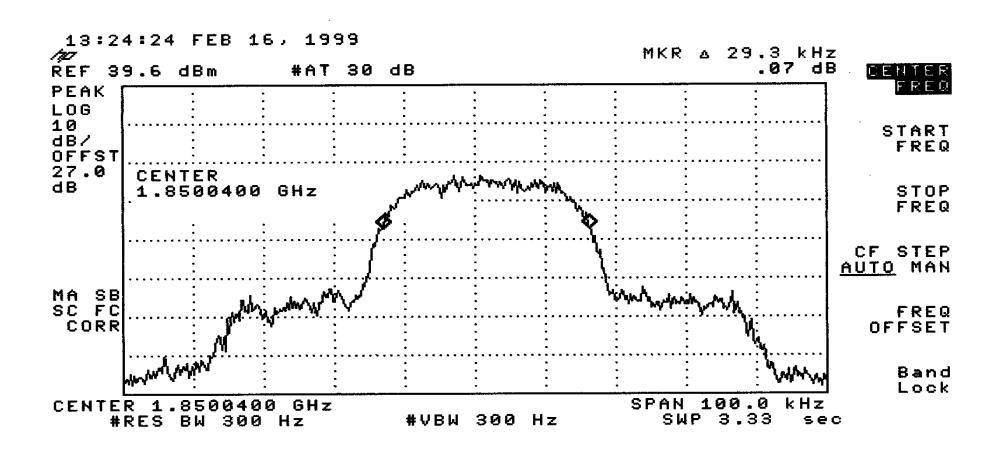
EXHIBIT

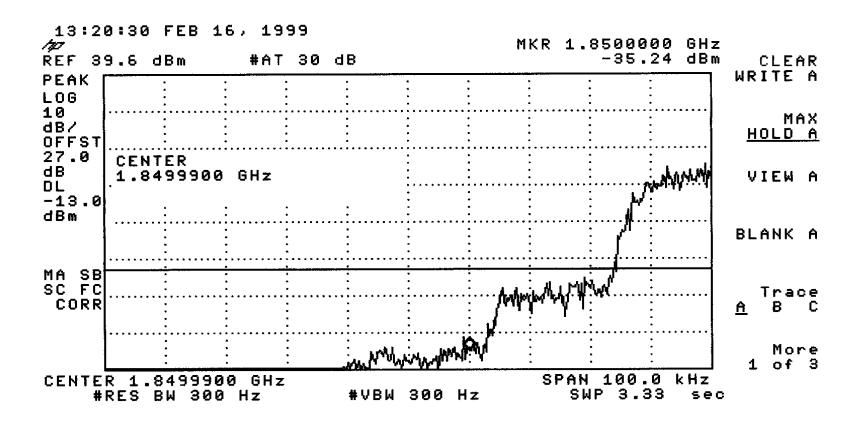
6l2 6l3 6l4	Lower Channel (Channel 2) Normal bursted operation; data rate 48.6 kb/s, Output power 0.4 Watts, 1850.04 MHz. 1 MHz Resolution Bandwidth reference plot. Emission Bandwidth 1 MHz span, Center Frequency 1849.99 MHz.
6I5 6I6 6I7	Upper Channel (Channel 1998) Normal bursted operation; data rate 48.6 kb/s, Output power 0.4 Watts, 1909.90 MHz. 1 MHz Resolution Bandwidth reference plot. Emission Bandwidth 1 MHz span, Center Frequency 1909.92 MHz.

The measurements were made per CFR 47, part 24 using the following equipment:

Hewlett Packard 8593 E Spectrum Analyzer







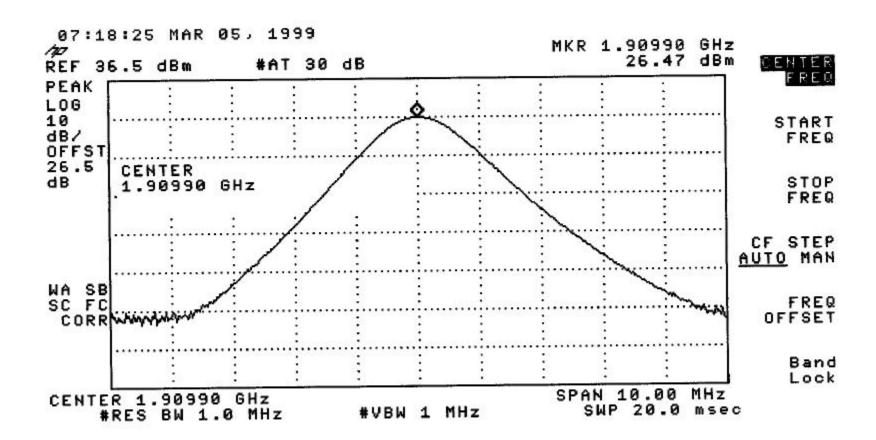


Exhibit 616

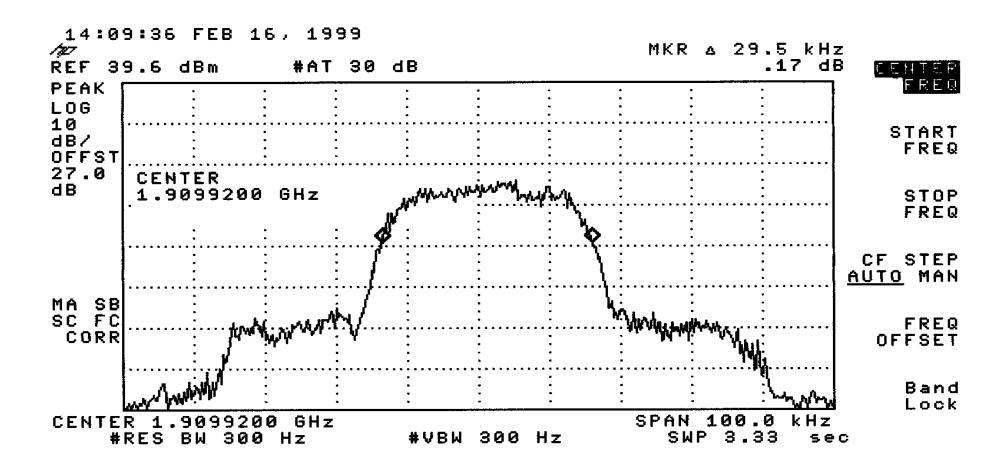


Exhibit 617

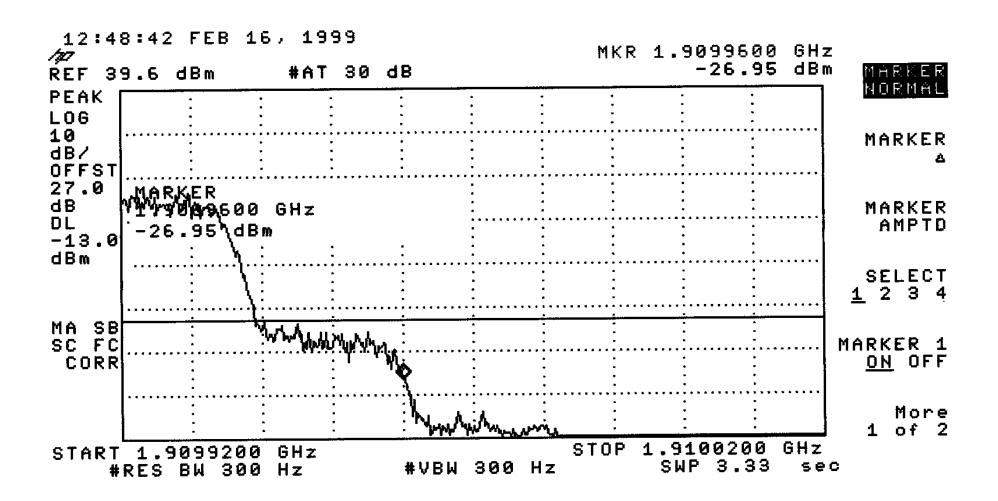


EXHIBIT 6J1

1900 MHz: SPURIOUS EMISSIONS (Conducted)

Para: 2.991 and Part 24

Per 2.991 Spurious emissions at the antenna terminals (conducted) when properly loaded with an appropriate artificial antenna were measured per IS137A.

<u>Exhibit</u>	Frequency (MHz)	Output Power (W)
6J2	1850.4	.4
6J3	1850.4	.0004
6J4	1909.92	.4
6J5	1909.92	.0004

The measurements were made using the following equipment:

HP8958A Cellular Interface HP 6623A DC Power Supply HP 8596E Spectrum Analyzer

Exhibit 6J2

APPLICANT: ERICSSON INC

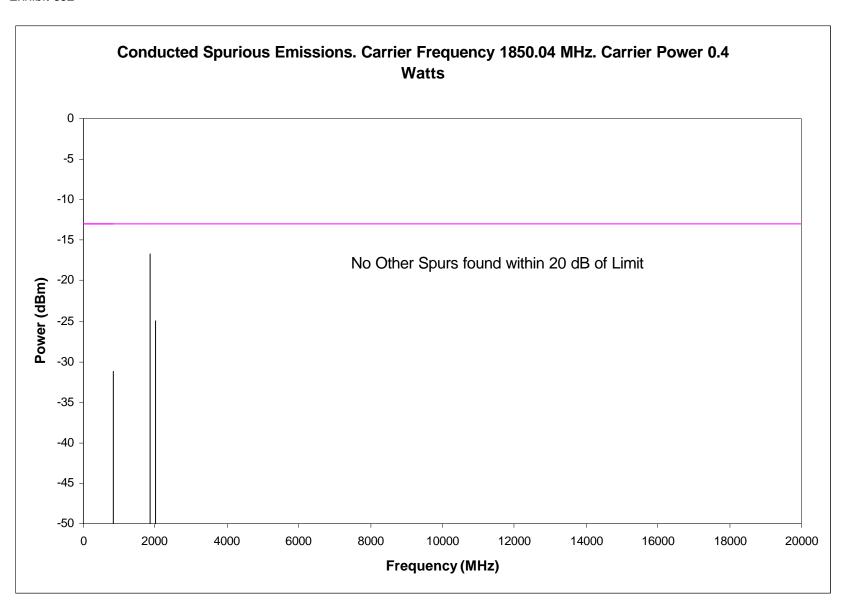


Exhibit 6J3

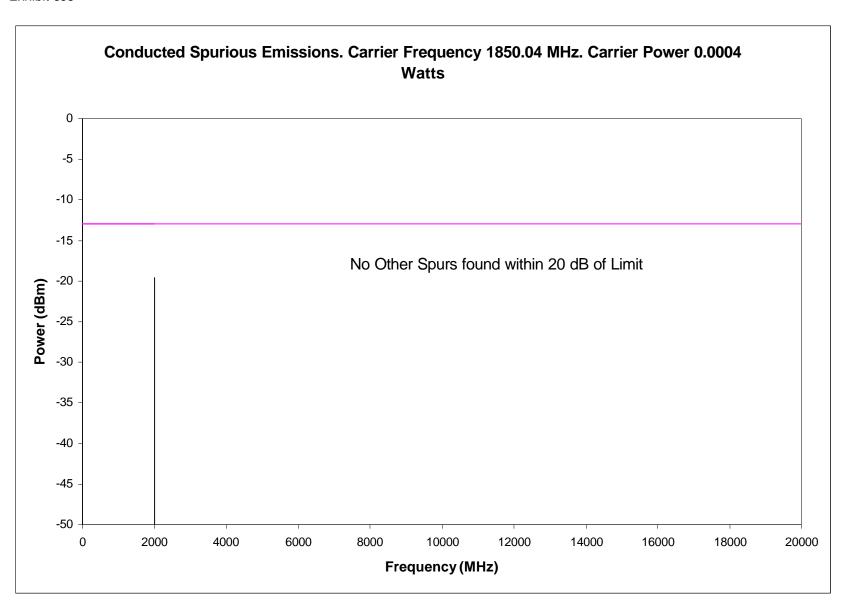


Exhibit 6J4

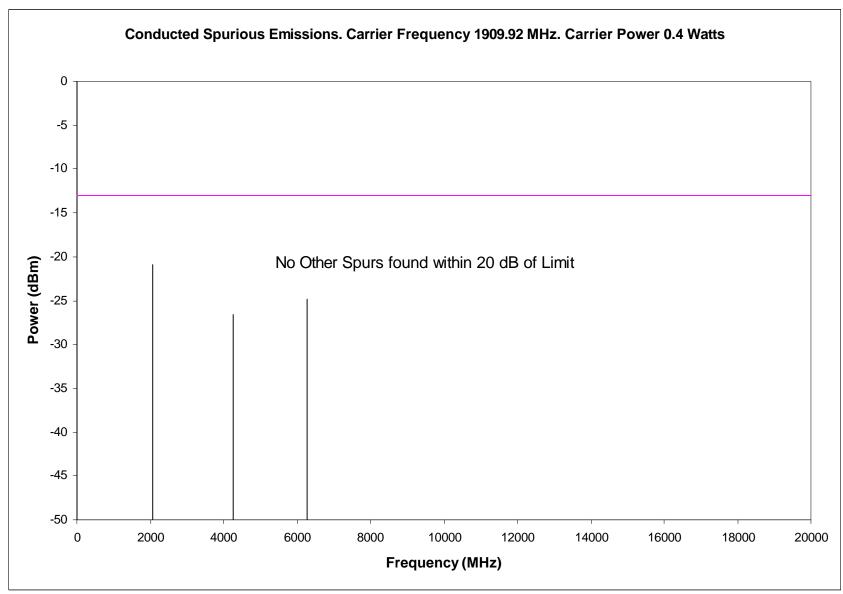


Exhibit 6J5

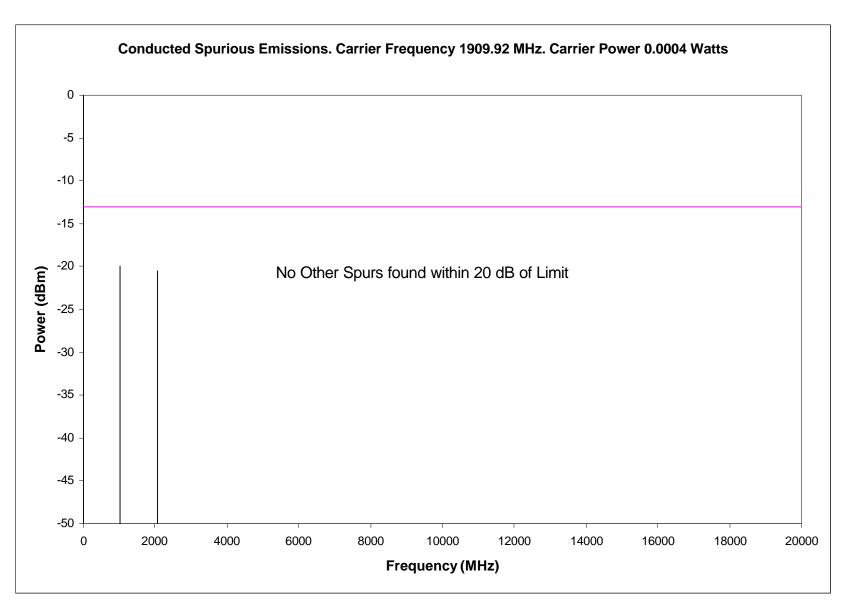


EXHIBIT 6K1

1900 MHz: SPURIOUS EMISSIONS. RADIATED

Para: 2.993 and Part 24

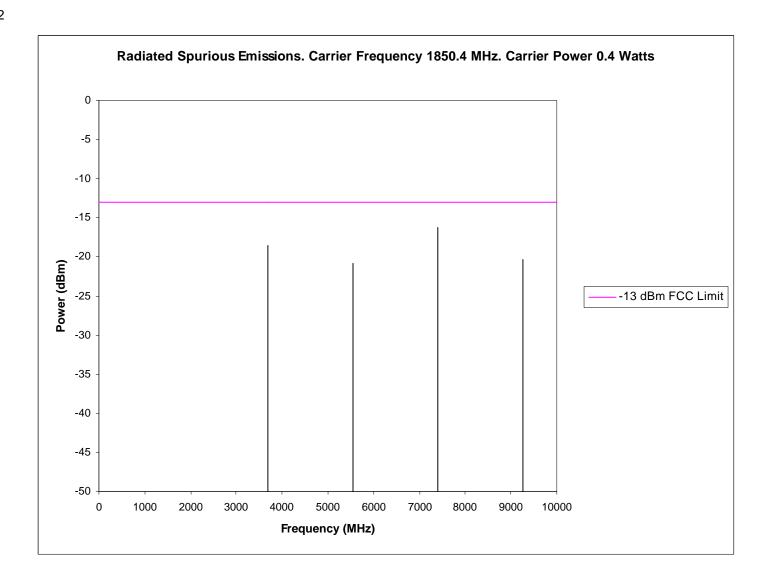
Per 2.993 and Part 24, field strength of spurious radiation was measured at Underwriters Laboratories Inc. Research Triangle Park, NC site. Underwriter Laboratories Inc. Research Triangle site is NVLAP and FCC registered. The measurement procedure is per EIA IS-137 conducted on a 3 meter test site. Results are shown on the following Exhibits.

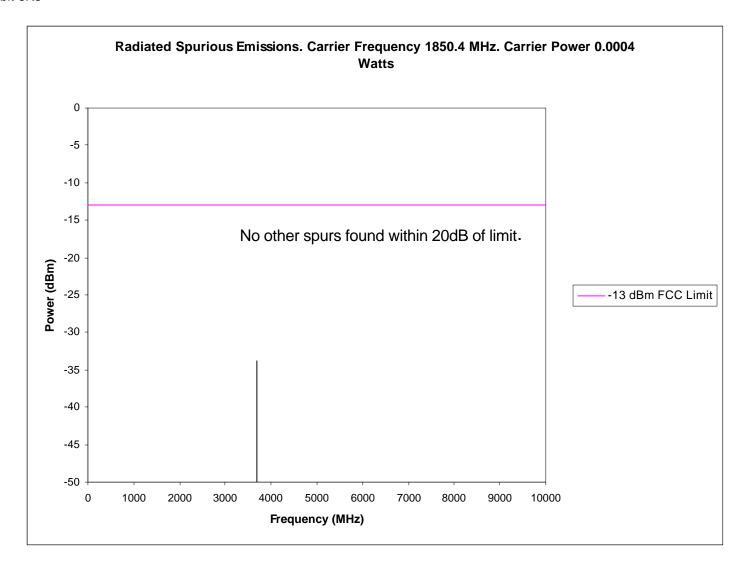
Note: The spectrum was examined through the 10th harmonic of the carrier. Measurements recorded are peak measurements.

Exhibit	Frequency (MHz)	Output Power (W)
6K2	1850.4	.4
6K3	1850.4	.0004
6K4	1909.92	.4
6K5	1909.92	.0004

The measurements were made using the following equipment:

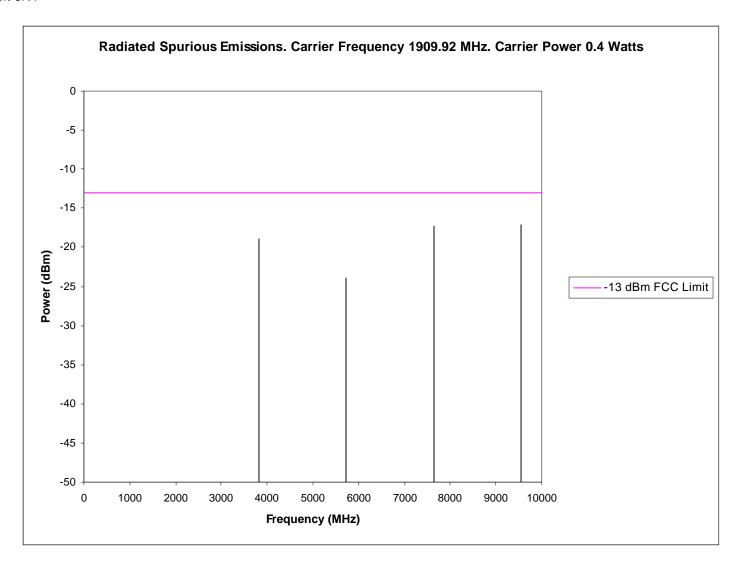
8566B Spectrum Analyzer 8559A Spectrum Analyzer





FCC ID NO:

AXATR-392-A2



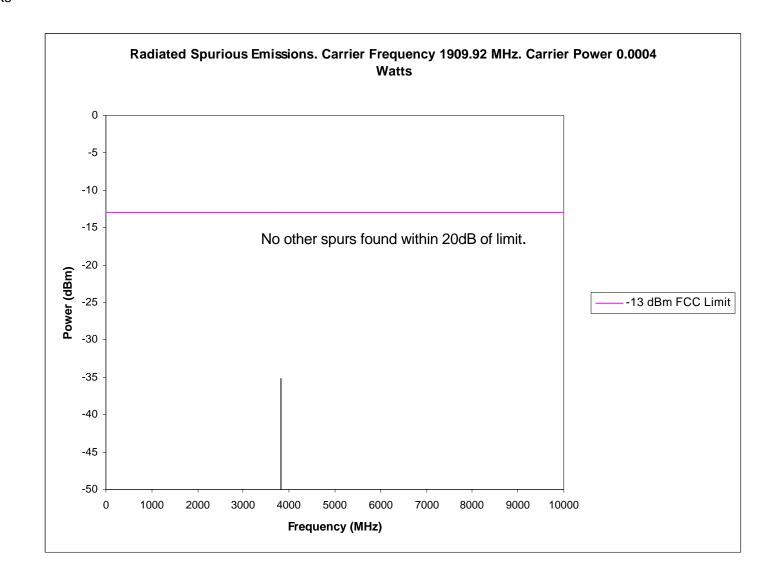


EXHIBIT 6L1

1900 MHz: FREQUENCY STABILITY

Per 2.995 (a)(1),(b),(d)(1)

Per 2.995 (a)(1),(b),(d)(1), variation of output frequency as a result of Varying either voltage or temperature is shown in Exhibit 6F2 and 6F3 respectively.

EXHIBIT #	Voltage	<u>Temperature</u>
6L2	4.3 to 5.3 Volts (varied)	+25 C
6L3	4.8 Volts	Varied

Note: The manufacturers rated voltage for the battery is 4.3 VDC to 5.3 VDC.

The measurements were made per IS-137A using a Hewlett Packard 8953DT North American Dual Mode Cellular Test System which includes the following equipment:

HP8958A Cellular Interface HP 6623A DC Power Supply HP 8596E Spectrum Analyzer HP 437B RF Power Meter HP 8901B Modulation Analyzer HP 8903B Audio Analyzer Thermotron SM-8C Temperature Chamber Exhibit 6L2

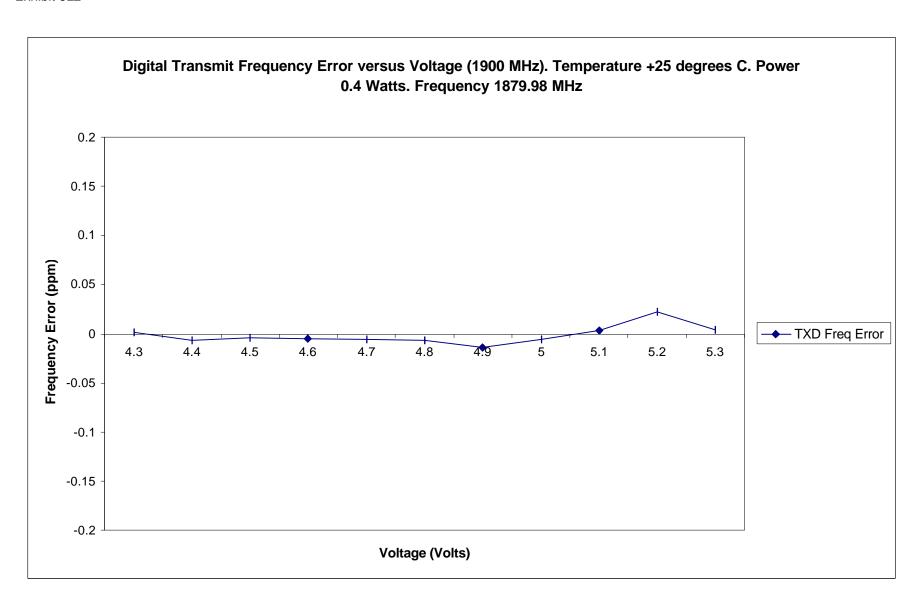


Exhibit 6L3

