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Power Density Simulation Report

Revision A

May 11, 2023

SAMSUNG ELECTRONICS

1. Simulation methodology for Power Density (PD)

1.1 Simulation tool

1.1.1 Tool description

For the simulation approach to calculating power density (PD) evaluation for mobile phone with mmWave antenna modules, ANSYS Electromagnetics suite version 2022.R2 (HFSS) is used. ANSYS HFSS is one of several commercial tools for 3D full-wave electromagnetic simulation used for antenna and RF structure design of high frequency component. ANSYS Electromagnetics suite version 2021.R2 (HFSS) is implemented based on Finite Element Method (FEM), which operates in the frequency domain.

1.1.2 Mesh and Convergence criteria

To solve the PD analysis using FEM, volume area containing simulated objects should be subdivided into electrically small parts that are called finite elements as the unknown functions. To subdivide system, the adaptive mesh technique in ANSYS Electromagnetics suite version 2021.R2 (HFSS) is used. ANSYS Electromagnetics suite version 2021.R2 (HFSS) starts to refine the initial mesh based on wavelength and calculate the error to iterative process for adaptive mesh refinement. The determination parameter of the number of iteration in ANSYS Electromagnetics suite version 2021.R2 (HFSS) is defined as convergence criteria, delta S, and the iterative adaptive mesh process repeats until the delta S is met. In ANSYS Electromagnetics suite version 2021.R2 (HFSS), the accuracy of converged results depends on the delta S. Figure 1 is an example of final adaptive mesh of the device (cross-section of top view).

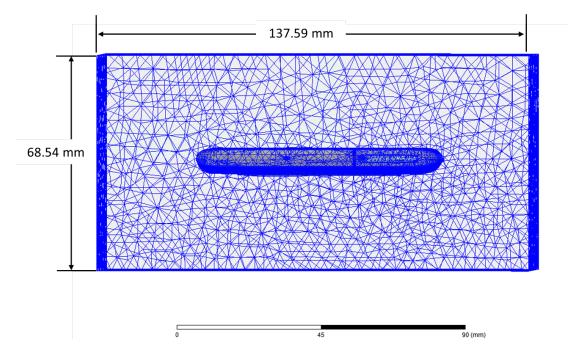


Figure 1 Example of the adaptive mesh technique (Top view)

1.1.3 Power density calculation

After solving 3D full-wave electromagnetic simulation, various kinds of physical quantities can be obtained. To calculate PD evaluation, two physical quantities, an electric field (\vec{E}) and a magnetic field (\vec{H}) are needed. The actual consumption power can be expressed as the real term of the Poynting vector (\vec{S}) from the cross product of \vec{E} and complex conjugation of \vec{H} as shown below:

$$\langle \vec{S} \rangle = \text{Re} \left(\frac{1}{2} \vec{E} \times \vec{H}^* \right)$$

 $\langle \vec{S} \rangle$ can be expressed as point power density based on a peak value of each spatial point on mesh grids, and obtained directly from ANSYS Electromagnetics suite version 2020.R1 (HFSS).

From the point power density $\langle \vec{S} \rangle$, the spatial-averaged power density (PD_{av}) on an evaluated area (A) can be derived as shown below:

$$PD_{av} = \frac{1}{A} \int_{A} \langle \vec{S} \rangle \cdot ds = \frac{1}{2A_{av}} \iint_{A_{av}} ||Re\{ExH^*\}|| dA$$

, where the spatial-averaged power density (PD_{av}) is total power density value considering on x, y and z components of point power density $\langle \vec{S} \rangle$ and the evaluated area (A) is 4cm².

1.2 Simulation setup

1.2.1 3D modeling

Figure 2 shows the simulation model which is mounted two mmWave antenna modules. The simulation modeling includes most of the entire structure of device itself such as PCB, metal frame, battery, cables, and legacy antennas as well as mmWave antenna modules called as Ant K and Ant M. For a folder open status (Fig. 2-1), Ant M is placed on the right side and antennas are facing the right side, and Ant K is placed on the back side and antennas are facing the back side of the device. For a folder close status (Fig. 2-2), Ant K and Ant M are placed same of the folder open status.

Folder Open

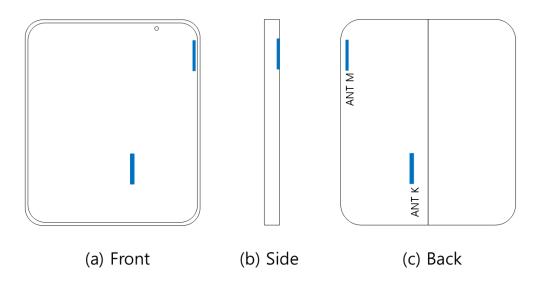


Figure 2-1. Simulation model which is mounted two mmWave antenna modules (Folder Open Status)

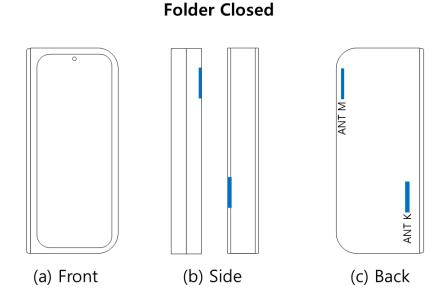


Figure 3-2. Simulation model which is mounted two mmWave antenna modules (Folder Closed Status)

1.2.2 PD evaluation planes

Table 1 shows the PD evaluation planes for each mmWave antenna module and Figure 3 shows the PD evaluation planes and whole area of the simulation model to find worst case of beamforming cases.

Please note that the "right" and "left" edge of mentioned in this report are defined from the perspective

of looking at the device from the front side.

Table 1. PD evaluation planes

Module	Front	Back	Left From Front View	Right From Front View	Тор	Bottom
	S1	S2	S3	S4	S5	S6
Ant K	О	О	О	0	0	0
Ant M	О	0	0	0	0	0

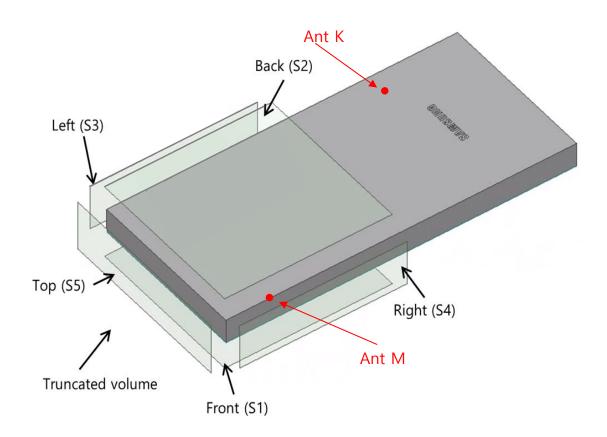


Figure 4. PD evaluation planes

1.2.3 Boundary condition

To simulate electromagnetic tool based on FEM, the boundary condition allows electromagnetic waves to be electrically open at the boundary and radiated far away without reflection. ANSYS

Electromagnetics suite version 2022.R2 (HFSS) can support the absorbing boundary condition (ABC) for radiation boundary and make normally a quarter wave length from the radiating structure. In this report, to cover all beamforming cases of mmWave antenna modules, 40 mm spacing from each surfaces of the device were used.

1.2.4 Source excitation condition

The number of antenna ports of ANT K and ANT M for source excitation are the same. The antenna port of ANT K and M is divided into 10 ports for n261 1 x 5 patch array antennas, 10 ports for n260 1 x 5 patch array antennas. In the 10 ports included in each patch antenna, 5 ports are divided into vertical polarization feeding, and the other 5 ports are divided into horizontal polarization feeding.

Figure 4 shows the ANT K module structure and surrounding structure. The ANT K module is encrypted in the ANSYS Electromagnetics suite (HFSS) and can only check the feeding position.

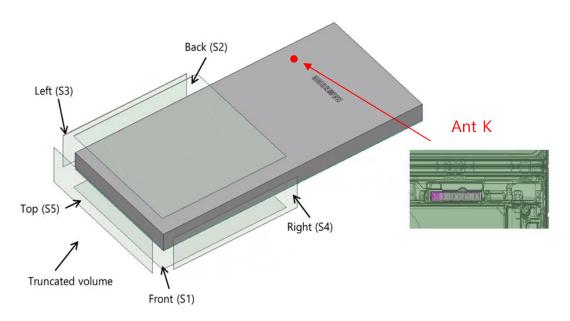


Figure 5. mmWave module (ANT K)

After finishing 3D full wave electromagnetic simulation of modeling structure, the magnitude and phase information can be loaded for each port by using "Edit Sources" function in ANSYS Electromagnetics suite (HFSS). Figure 5 shows an example of antenna port excitations.

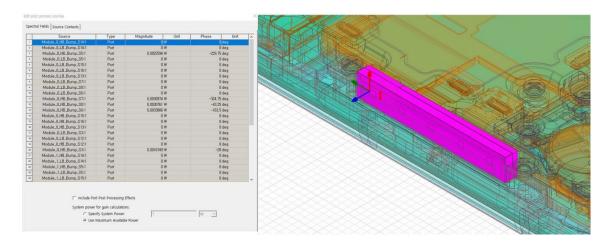


Figure 6. An example of port excitation (ANT M)

Since ANSYS Electromagnetics suite (HFSS) uses FEM solver based on frequency domain analysis method, the input source for the port excitation applies sinusoidal waveform for each frequency.

1.2.5 Condition of simulation completion

The simulation completion condition of ANSYS Electromagnetics suite (HFSS) is defined as delta S. The ANSYS Electromagnetics suite (HFSS) calculates the S-parameter for the mesh conditions of each step and determines whether to proceed with the operation of the next step by comparing the difference between the S-parameters in the previous step. A difference between the previous step and the current step of S-parameter is expressed as delta S, and the delta S generally sets 0.02. The simulation result of this report is the result of setting delta S to 0.02.

2. Simulation verification

2.1 Spatial-averaged power density

As mentioned in the previous chapter, the Poynting vector (\vec{S}) can be obtained through cross product of an electric field (\vec{E}) and complex conjugate of a magnetic field (\vec{H}) . The real term of the Poynting vector can be described as the point power density or peak power density. Using the point power density, the spatial-averaged power density can be obtained by the integral of 4 cm² at 2.5 mm intervals of the point power density result. Figure 6 shows examples of the distribution plot of point power density and the averaged power density.

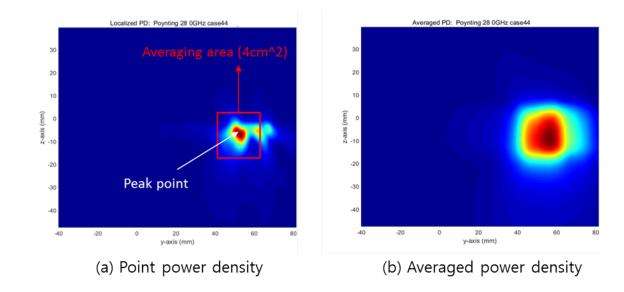


Figure 7. Power density distribution (Example)

2.2 Comparison between simulation and measurement

In this section, the simulated-power density distributions and measured-power density distributions are compared to each mmWave antenna.

Based on comparison of power density distributions, simulated power density and measured power density have a good correlation. The discrepancy in amplitude between simulated 4cm² averaged power density and measured 4cm² averaged power density is considered as housing influence and used in determining input power limit for each beam for RF exposure compliance.

The input powers per each active port are listed below for both Simulation and Measurement validation and power density characterization. For Simulation, these values were entered directly into HFSS model. For measurement, FTM S/W was used to input these values for each active port also.

Mada/Band	Antonno	Input Power (dBm)	Input Power (dBm)
Mode/Band	Antenna	SISO	MIMO
5G NR n261	K Patch	6.0	6.0
SG INK NZOT	M Patch	6.0	6.0
5G NR n260	K Patch	6.0	6.0
SG INK IIZOU	M Patch	6.0	6.0
5G NR n258	K Patch	6.0	6.0
3G INK 11230	M Patch	6.0	6.0

^{*} The below simulation and measurement result were performed at 2mm evaluation distance and 28GHz / 38.5GHz. The *input.power.limit* was determined based on below results in RF Exposure Part 0 Report.

Condition	Band	Channel	Module	Side	Beam ID	Sim. PD (mW/cm2)	Meas. PD (mW/cm2)
			V	Door	26	1.06	0.682
			K	Rear	165	2.12	1.65
	264	Mid		Right	44	1.17	0.572
	n261	Ch. 2077915 (27924.96 MHz)		Rear	41	0.92	0.253
		(27324.30 1011.2)	M	Right	166	2.06	0.642
				Rear	166	1.38	0.609
			V	Door	34	1.00	0.623
		Mid	К	Rear	154	0.87	0.721
Folder Closed	n260	Ch. 2254165		Right	31	1.95	0.708
Ciosea		(38499.96 MHz)	М	Rear	40	1.25	0.403
				Right	160	1.85	0.832
[Left	26	0.46	0.306
			К	Poor	26	0.87	0.686
	n258	Mid Ch. 2025833		Rear	165	1.75	1.51
	11230	(24800.04 MHz)		Right	29	1.10	0.631
		(2 100010 1 111112)	М	Nigiit	169	2.31	0.519
				Rear	169	1.91	0.653
Condition	Band	Channel	Module	Side	Beam ID	Sim. PD (mW/cm2)	Meas. PD (mW/cm2)
	n261	Mid Ch. 2077915 (27924.96 MHz)	K	Rear	26	1.03	0.582
				Real	165	2.16	1.48
				Front	31	0.92	0.61
				Right	33	1.31	0.523
				Right	159	1.02	0.718
				Rear	169	1.41	0.923
			К	Rear	34	1.00	0.683
			K	Near	154	0.86	0.676
		201		Rear	38	0.75	0.295
Foldor	n260	Mid Ch. 2254165		Right	39	1.46	0.745
Folder Open	11200	(38499.96 MHz)	М	Front	39	0.77	0.241
Open		,	141	Right		1.75	0.851
				Front	160	0.91	0.241
				Rear		0.89	0.303
			К	Rear	34	0.76	0.522
			IX.	Near	165	1.79	1.36
	n258	Mid 8 Ch. 2025833 (24800.04 MHz)		Rear	39	0.75	0.329
			М	Front	40	0.88	0.492
				Right	41	1.14	0.965
				Rear	169	1.21	0.649
				Right	100	1.04	0.411

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• Table 2-1, n258 ANT K-Patch: Mid Channel, Beam ID 34 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
34	S2 (Rear)	ANT K			Section

• Table 2-2, n258 ANT K-Patch: Mid Channel, Beam ID 165 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
165	S2 (Rear)	ANT M.			•

• Table 2-3, n258 ANT M-Patch: Mid Channel, Beam ID 39,40,41 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
39	S2 (Rear)	ANT C			- 1
40	S1 (Front)	W IMW			
41	S4 (Right)	WINY			

• Table 2-4, n258 ANT M-Patch: Mid Channel, Beam ID 169 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
160	S2 (Rear)	ANT K			
169	S4 (Right)	ANTM			

• Table 2-5, n260 ANT K-Patch: Mid Channel, Beam ID 34 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
34	S2 (Rear)	ANT K.			

• Table 2-6, n260 ANT K-Patch: Mid Channel, Beam ID 154 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
154	S2 (Rear)	ANT K.			

• Table 2-7, n260 ANT M-Patch: Mid Channel, Beam ID 38,39 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
38	S2 (Rear)	ANT K			
39	S4 (Right)	WINT			
39	S1 (Front)	WLDW			

• Table 2-8, n260 ANT M-Patch: Mid Channel, Beam ID 160 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
	S1 (Front)	ANT K			
160	S2 (Rear)	ANT K			1
	S4 (Right)	ANI M			•

• Table 2-9, n261 ANT K-Patch: Mid Channel, Beam ID 26 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
26	S2 (Rear)	ANT K			

• Table 2-10, n261 ANT K-Patch: Mid Channel, Beam ID 165 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
165	S2 (Rear)	ANT K			•

• Table 2-11, n261 ANT M-Patch: Mid Channel, Beam ID 31,33 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
31	S1 (Front)	ANT K			8
33	S4 (Right)	MINA		8	1

Table 2-12, n261 ANT M-Patch: Mid Channel, Beam ID 159,169 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
159	S4 (Right)	W IW			1000
169	S2 (Rear)	ANT K			6

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• Table 2-13, n258 ANT K-Patch: Mid Channel, Beam ID 26 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
26	S2 (Rear)	ANT K			•
20	S3 (Left)	NAT K			

• Table 2-14, n258 ANT K-Patch: Mid Channel, Beam ID 165 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
165	S2 (Rear)	ANT M.	9		•

• Table 2-15, n258 ANT M-Patch: Mid Channel, Beam ID 29 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
29	S4 (Right)	ANTM			<u> </u>

• Table 2-16, n258 ANT M-Patch: Mid Channel, Beam ID 169 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
	S2 (Rear)	ANT K			
169	S4 (Right)	ANT M			

• Table 2-17, n260 ANT K-Patch: Mid Channel, Beam ID 34 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
34	S2 (Rear)	ANT K		63	4.

• Table 2-18, n260 ANT K-Patch: Mid Channel, Beam ID 154 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
154	S2 (Rear)	WHI K		B	•

• Table 2-19, n260 ANT M-Patch: Mid Channel, Beam ID 31,40 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
31	S4 (Right)	MALIN			TO THE PERSON NAMED IN COLUMN TO THE
40	S2 (Rear)	ANT K			1

• Table 2-20, n260 ANT M-Patch: Mid Channel, Beam ID 160 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
160	S4 (Right)	WILW TWO			**

• Table 2-21, n261 ANT K-Patch: Mid Channel, Beam ID 26 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
26	S2 (Rear)	ANT K.——		B	

• Table 2-22, n261 ANT K-Patch: Mid Channel, Beam ID 165 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
165	S2 (Rear)	ANT M			

• Table 2-23, n261 ANT M-Patch: Mid Channel, Beam ID 41 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
41	S2 (Rear)	ANT K			
41	S4 (Right)	WILW			4

• Table 2-24, n261 ANT M-Patch: Mid Channel, Beam ID 166 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD	Print out from Qualcomm MG Script
166	S2 (Rear)	ANT K			
166	S4 (Right)	WINW			•

3 Simulation results

This section shows the PD simulation results of Ant K and Ant M at 24GHz, 28GHz and 39GHz for each evaluation plane specified in Table 1 at two separation distances of 2mm and 10mm for open condition and for closed conditions. The ratio of PD exposure from front surface to the worst surface at 2mm, and the ratio of PD exposure from 2mm to 10mm (open and closed) evaluation distance for each beam are also reported in this section to support RF exposure analysis for simultaneous transmission scenarios performed in the Part 1 Near Field PD report.

The relative phase between beam pairs is not controlled in the chipset design. Therefore, the relative phase between each beam pair was considered mathematically to identify the worst case conditions. The below MIMO results represent the highest reported MIMO simulation results after sweeping across the relative phase between beams a 5° step interval from 0° to 360° ,

The worst-case simulated PD determined from the tables in this section were used for conservativeness in *input.power.limit* determination in RF Exposure Part 0 Report.

3.1 PD for Low/Mid/High Channel at 24GHz / 28GHz / 39GHz

3.1.1 Ant K-Patch Antenna

Table 3 & Table 4 & Table 5 show the PD simulation evaluation of Ant K patch antenna at 24GHz / 28GHz / 39GHz for the corresponding evaluation planes specified in Table 1.

Table 3. PD of Ant K – patch antenna (24GHz – n258)

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- K-patch Low CH

													1		max ratio ou	t of all beams												max ratio out of all	Dearts		
\vdash			Г	Т .	т			4cm2 F	PD(mW/on	v2)			26.2%	10.4%	7.0%	25.1%	12.1%	100.0%		iom2 PD(ml	W/on2)	rt 10mm evalu	uation dist	whore	76.2%	16.9%	0.5%	5.5%	18.5%	5.4%	76.2%
No. 1	fodule Typ	e Beam ID_1	Sema ID	2 Feed no.	-	\neg	Т	т	\neg		П	per	ratio	ratio	ntio	ratio	ratio	ntio		Т	П	1	Т .	Т	ratio	ratio	ntio	ntio	ratio	ntio	ntio
					54/Rig	pht) S3(Left	t) \$5(To	(B)	(Bottom)	\$1(Front)	S2(Rear	Beam Back-of	(Right 2mm(/(wont- surface 2mm)	(Left 2mm)/(worst- surface 2mm)	(Top 2mm)/(wonst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	54(Right)	S3(Left)	SS(Top)	SS(Bottom)	\$1(Front	(S2)Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(wont- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Bottom 10mm(/(worst surface 2mm)	(Front 10mm)/(wonst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
1		0	-	1	0.01	0.00	0.00		0.01	001	0.09	(dB)	14.0%	435	1.7%	12.9%	7.5%	1000%	001	0.00	0.00	0.01	0.00	0.04	41.9%	97%	12%	1.1%	86%	12%	412%
2		2		1	0.00		0.00		0.01	0.00	0.10		13.7%	5.3%	12%	11.6% 11.2%	12% 56%	100.0%	001	0.00	0.00	0.01	0.00	0.04	38.9% 38.2%	8.4% 5.6%	42% 67%	21%	8.4% 7.9%	1.1%	31.9% 31.2%
4		6		1	0.00				0.01	001	0.12		7.4%	3.3% 5.1%	4.7%	5.0%	41%	1000%	001	0.00	0.00	0.01	0.00	0.04	34.7%	41%	25%	33%	41%	17%	34.7%
5 6 7		10		2	0.00	0.00	0.01		0.03	0.01	0.12		64%	6.4%	6.9%	15.0%	2.9%	100.0%	001	0.01	0.00	0.02	0.00	0.05	30.1%	4.0%	46%	52%	11.0%	17%	30.1%
8 9		11	-	2	020		0.00		0.02	001	0.18	-	94%	5.0%	2.8%	12.5% 4.2%	19%	100.0%		001		0.01	0.00	0.06	31.5% 42.2%	6.6% 9.0%	19% 85%	12%	7.7%	1.7%	31.5% 40.2%
10		13		2	0.00		0.01	1	0.04	601	0.18		11.1%	5.0%	2.8%	20.6% 10.5%	50% 19%	100.0%	601	001	0.00	0.03	0.00	0.05	29.4% 31.5%	6.7% 6.6%	19%	22% 17%	14.4%	22%	22.4%
11		19		2	0.00	2 0.00	0.01	1	0.01	001	0.24		99%	4.1%	2.1%	29%	4.5%	100.0%	002	001	0.00	0.01	0.01	0.10	42.2%	62%	13%	1.6%	21%	2.1%	40.3%
13		20		5	0.00		0.03	2	0.00	001	0.21		66%	6.1% 3.4%	1.0%	6.6% 18.5%	2.8% 1.6%	100.0%	001	001	0.01	0.01	0.00	0.07	32.1%	3.3% 5.0%	18% 25%	52% 23%	47% 13.0%	1.6%	32.1% 30.1%
14		25		5	0.00				0.06	002	0.40		5.0% 8.5%	4.6% 9.2%	2.0%	11.8% 4.1%	4.0%	100.0%		002	0.00	0.04	0.01		38.8%	44% 59%	17% 7.7%	23%	8.7% 2.5%	15% 1.8%	38.8%
111 122 133 144 155 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35		27		5	0.13				0.02	0.06	0.50		26.2%	9.5%	2.4%	42% 80%	12.1%	100.0%		0.04	0.00	0.01	0.03	0.24	48.6% 25.1%	16.9%	8.1% 6.0%	14%	2.8%	5.4% 1.7%	48.6% 25.1%
10		34		5	0.00	0.00	0.02	2	0.14	002	0.56		5.7%	2.2%	1.0%	25.1%	4.1%	100.0%	003	0.01	0.02	0.10	0.01	0.10	32.6%	45%	1.0%	27%	18.5%	1.0%	32.6%
19		35	-	5	0.04		0.01		0.04	0.02	0.55	-	7.4%	8.7% 8.6%	1.8%	7.4% 3.7%	4.0%	100.0%	003	0.04	0.00	0.02	0.01	0.24	42.7%	45% 14.6%	6.7% 7.4%	13%	14% 23%	2.4%	42.7% 47.4%
21		128		5	0.00				0.03	0.04	0.36		20.3%	7.8%	44%	8.1% 9.4%	10.0%	1000%	005	0.02			0.02	0.19	53.6% 45.6%	12.5%	6.7%	3.6%	5.6%	47%	51.6% 45.6%
23		130		i.	0.00	0.00	0.00	0	0.02	0.00	0.22		03%	0.9%	0.9%	97% 54%	0.9%	1000%	0.00	0.00	0.00	0.02	0.00	0.09	41.9% 42.5%	05%	05% 09%	0.5%	78% 45%	05%	41.9% 42.5%
25		134	-	1	0.00	0.00	0.00	0	0.01	000	0.22	-	05%	1.0%	1.0%	34%	0.5%	100.0%	000	000	0.00	0.01	0.00	0.09	53.6%	0.5%	0.5%	1.0%	2.9%	05%	\$3.6%
26		136		1 2	0.00				0.01	0.00	0.17		12%	10%	1.8%	30% 15.2%	0.6%	100.0%	000	0.00	0.00	000	0.00	0.08	47.9% 48.2%	12%	1.8%	1.8%	1.8%	06% 08%	47.9% 48.2%
28		139		2 2	0.00			0	0.03	000	0.43		07%	1.2%	0.5%	73% 12%	0.9%	100.0%	000	0.00	0.00	0.03	0.00	0.25	57.6% 55.9%	0.5%	09% 06%	0.2%	5.9% 0.6%	0.5%	57.6% 55.9%
30		141		2	0.00	0.00	0.01	_	0.04	0.00	0.34		15%	1.2%	1.5%	12.3%	1.2%	100.0%	000	000	0.00	0.03	0.00	0.15	42.5%	0.9%	09%	12%	9.4%	09%	42.5%
31	K Patr	146 h 147	-	2	0.00				0.06	0.00	0.41	-	12%	1.0%	0.5%	14.6%	1.5%	100.0%		0.00	0.00	0.05	0.00		42.2% 56.5%	1.0%	0.7%	02%	11.2%	0.7%	42.2% 56.5%
33		146		2	0.00		0.01		0.02	0.00	0.52		14%	125	1.2%	4.1% 16.1%	0.6%	100.0%	000	0.01	0.00	0.02	0.00	0.27	51.8% 41.7%	0.8%	1.0%	1.0%	3.1% 12.7%	02%	51.8% 41.7%
35		153		5	0.00				0.14	001	1.11		15%	1.6%	0.3%	12.7%	1.2%	100.0%	001	0.02	0.00	0.10	0.01	0.54	48.1% 75.2%	1.0%	13%	02%	92% 20%	05% 02%	48.1% 75.2%
37		155		5	0.00	0.02	0.00		0.01	0.01	1.21		0.7%	1.7%	0.2%	0.8%	0.4%	100.0%	001	0.01	0.00	0.01	0.00	0.14	70.9%	0.4%	12%	0.2%	0.4%	0.2%	70.9%
38		156		5	0.00		0.03		0.01	0.01	1.50		13%	2.1%	1.7%	0.8% 16.4%	0.7% 1.9%	100.0%	002	0.02	0.02	0.01	0.01	0.78	52.1% 42.2%	1.0%	14%	1.4%	0.5% 12.9%	05% 08%	52.1% 42.2%
40		163		- 3	020	0.02	0.00		0.04	0.01	0.94		16%	1.7%	0.3%	40% 12%	0.5%	100.0%	001	0.01	0.00	0.02	0.00	0.67	70.4% 76.2%	1.1% 0.6%	13%	0.3%	22%	0.3%	70.4% 76.2%
42		165		ŝ	0.00	0.03	0.02	2	0.01	001	1.54		0.8%	1.8%	1.0%	0.4%	0.6%	100.0%	001	0.02	0.00	0.00	0.01	0.97	62.8%	0.6%	1.4%	0.7%	0.3%	0.4%	62.8%
43		2	128	2	0.00				0.04	001	0.35	-	5.5% 4.5%	2.8%	0.9%	11.5% 13.1%	2.9%	100.0%	001	001	000	0.03	0.00	0.16	45.2% 42.7%	3.7% 3.0%	1.7% 2.0%	0.6%	8.6% 10.1%	1.2%	45.2% 42.7%
45		4	132	2	0.00		0.01		0.04	001	0.20		12% 28%	3.7% 1.0%	2.4%	12.0% 5.2%	1.6%	100.0%		001	0.01	0.03	0.00		41.7%	21% 17%	29% 12%	18%	7.7%	0.8%	41.7% 23.9%
47		8 10	136		0.00				0.01	001	0.35		17%	5.6%	42%	34%	1.7%	100.0%		0.01	0.01	0.01	0.00		53.7% 29.1%	1.7%	40%	34%	2.8%	0.8%	\$3.7%
49		11	139	4	0.00	0.02	0.01		0.09	001	0.64		2.4%	3.1%	1.0%	17.4% 13.9%	25% 1.9%	100.0%	001		002	0.11	0.01	0.34	53.1%	1.7% 2.3%	2.3% 2.7%	2.4%	11.2%	1.1%	29.1% 53.1%
50		12	140	4	0.04		0.02	2	0.01	0.02	0.05		49%	42% 12%	1.0%	1.6% 21.7%	2.0%	100.0%	003	003	0.01	0.10	0.01	0.45	52.9% 44.0%	11% 10%	2.4%	13%	1.2% 16.2%	0.8% 1.2%	52.9% 44.0%
38 39 40 41 41 42 43 44 45 46 47 46 49 50 51 51		16	146	4	0.00	0.02	0.01		0.13	0.02	0.79		3.3% 5.5%	2.2%	1.0%	17.0%	1.9%	100.0%	002	0.02	001	0.10	0.01	0.22	40.3% 52.2%	23%	19%	0.8%	13.2%	09%	40.7% 52.2%
54		20	148		0.00	0.03		1	0.06	001	0.00		2.3%	2.9% 3.5%	1.0%	69%	15%	100.0%		002			0.01	0.39	41.4%	14%	2.3%	28%	5.4%	0.9%	41.4%
54 55 56 57 58		24 25	152 153	10	0.00		0.03		0.41	0.06	2.31	H	2.2% 1.9%	2.3% 3.0%	1.2%	17.9% 14.6%	24%	100.0%	005	0.04	002	0.32	0.03	1.00	37.4% 46.7%	2.0% 1.4%	1.6% 2.5%	0.7%	13.6% 10.6%	12%	37.4% 46.7%
57		26 27	154 155	10	0.10				0.07	0.04	2.04		19%	4.8% 5.3%	1.1%	18%	21%	100.0%	005	0.08	0.02	0.05	0.02	1.44	70.6% 70.4%	2.6% 5.6%	40% 42%	0.8%	25% 1.1%	1.0%	70.6% 70.4%
59		26	156	10	0.00	0.13	0.10	,	0.06	0.05	2.52		11%	5.2%	19%	22%	1.0%	100.0%	006		0.08	0.04	0.03	1.16	45.9%	2.3%	2.4%	3.1%	1.7%	1.1%	45.9%
59 60 61		34 35	162 163	10	0.00	0.10	0.02	2	0.55	0.08 0.04	2.37		15% 19%	1.7% 4.9%	1.3%	23.3% 3.6%	15% 20%	100.0%		0.08			0.04		12.5% 63.2%	2.9% 2.5%	1.4% 1.8%	1.0%	18.2% 2.1%	1.5% 1.2%	32.5% 63.2%
62		36	164 165		0.11		0.00		0.03	008	2.12		80% 50%	44% 47%	0.5% 2.6%	18%	19% 28%	100.0%		007 007		0.02	0.04		63.4%	47% 13%	13% 13%	0.3% 2.1%	1.1%	1.6%	69.4% 63.8%
		- 80	70.5	10	0.11	0.10	0.00	_		00	-114		20%																		

- K-patch Mid CH

																	max ratio ou	et of all beams													max ratio out of all	beams		
П		Т			Т				4cm2 F	PD/mW/c	m2)			13.01		15.6%	7.4%	32.8%	6.2%	100.0%	4	iom2 PD(n	rW/cm2)	at 10mm	evaluatio	on distan	CIP .	75.1%	8.7%	12.9%	6.0%	21.0%	3.2%	75.1%
No.	Module Typ	pe Sea	m ID_1 Sema	D_2 Feed	10.				Т				per Sean	ratio		ratio	ratio	ratio	ratio	ratio				Т				ratio	ratio	ratio	ratio	ratio	ntio	ratio
					54	(Right)	S3(Left)	SS(Top	SE()	Bottom)	\$1(Front	\$2(Rea	Back-o			(Left 2mm)/(worst- surface 2mm)	(Top 2mm)/(worst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	S4(Right)	\$3(Left)	SS(Top	\$6(Bo	ttom) S	1(Front)	S2(Rear)	wont-surface (10mm/2mm)	(Right 10mm)/(wont- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Sottom 10mm)/(wont- surface 2mm)	(Front 10mm(/(worst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
1		+	0	1	+	000	0.00	0.00	٠	0.03	0.01	0.14	(49)	5.0%		16%	0.7%	20.1%	4.2%	100.0%	000	000	0.00	0.0	02	0.00	0.06	25.2%	2.9%	29%	0.7%	12:9%	1.4%	35.2%
2 3 4 5 6 7 8 9 10 11 12		F	2	1	Ŧ	000	0.00	0.00		002	001	0.15	Е	7.9%	=	6.0% 4.8%	2.0%	11.9%	40%	100.0%	001	001	0.00	01		0.00	0.06	29.1% 21.0%	53% 48%	46%	20% 12%	7.3% 8.7%	13%	29.1% 31.0%
4		⊨	6	1	#	000	0.00	0.01		0.01	000	0.12		6.0%		6.0%	3.8%	83%	10%	100.0%	001	001	0.00	0.0	01	0.00	0.04	33.1%	3.0%	5.3%	30%	5.3%	0.8%	33.1%
6			10	1 2	+	000	0.00	0.01	_	0.01	0.01	0.15	+	55% 41%		4.0%	4.8% 7.4%	48% 184%	14% 17%	1000%	000	001	0.01	0.0	03	0.00	0.06	40.7% 33.2%	28%	14%	4.1% 6.0%	2.8% 13.8%	21%	40.7% 31.2%
7		⊏	11	2			0.02	0.00	F	0.04	0.01			7.3%		5.8% 7.1%	0.7% 1.8%	15.0%	2.6%	100.0%	001	001				0.00	0.10	34.7% 38.7%	47%	44% 55%	0.7% 1.5%	10.2% 1.5%	11%	347% 34.7%
9			13	2	#	000	0.00	0.00		0.07	001	0.29		48%		145	2.4%	25.1%	14%	1000%	001	001	0.00	0.1	05	0.01	0.09	32.6%	2.7%	2.4%	21%	16.2%	17%	32.6%
10		\vdash	16	2	+	0.02	0.02	0.00		0.04	001	0.27	+	7.3%	-	5.8% 8.1%	0.7% 2.4%	15.0% 4.1%	2.6% 4.7%	100.0%	001	0.01	0.00			0.00	0.10	34.7% 51.2%	47%	44%	0.7% 1.2%	10.2% 2.7%	1.1%	34.7% 51.2%
12			20 24	2		000	0.01	0.01		0.02	0.01	0.24	-	5.0% 6.1%		545 145	5.4% 1.0%	8.7% 19.1%	2.1% 2.5%	100.0%	001		0.01			0.00	0.00	32.2% 32.0%	41%	2.7% 2.7%	4.1%	62% 11.6%	12%	32.2% 32.0%
1.6		-	25	s	_	0.05	0.03	0.01	+	0.08	0.02	0.67		7.8%	\neg	4.5%	1.7%	12.3%	2.3%	100.0%	004	0.02	0.00	0.0	06	0.01	0.29	43.5%	53%	16%	0.8%	8.7%	1.1%	41.5%
15			26	5	+	0.09	0.09	0.02		003 40.0	004	0.60	+	13.09		11.0%	2.4%	44% 65%	6.2% 5.7%	1000%	006	0.07	0.01	0.0		0.02	0.36	52.5% 45.2%	8.7% 7.9%	10.5%	1.8%	28%	12% 25%	52.5% 45.2%
16 17 18 19 20		F	28 34	5	1	0.03	0.06	0.04	Ŧ	0.05	002	0.62	Е	5.0% 2.9%		9.4%	6.8% 2.9%	7.3% 32.8%	2.6% 5.2%	100.0%	002	003	0.03	0.0		0.01	0.20	31.8% 27.0%	19%	55%	55% 24%	6.2% 21.0%	1.0%	31.8% 27.0%
19		-	25	- 5		0.05	0.06	0.02	+	0.04	0.03	0.60		7.9%	\neg	9.8%	1.3%	63%	5.6%	100.0%	003	0.04	0.02	0.0	02	0.02	0.30	50.0%	55%	7.3%	25%	15%	25%	50.0%
20			36 37	5		0.06	0.12	0.01	+	200	0.05	0.74	+	87%		15.6%	1.1%	33% 12.8%	62% 52%	1000%	003		0.01	0.0		0.02	0.39	53.3% 49.5%	62%	12.9% 4.8%	0.8%	20%	22%	51.9% 49.5%
22			128	1		0.00	0.00	0.00		0.02	000	0.20		1.5%		1.0%	0.5%	83% 82%	1.0%	100.0%	000	000	0.00	0.0		0.00	0.09	45.1% 44.1%	1.0%	05% 08%	0.5%	5.9%	05%	45.1% 44.1%
24			132	1		0.00	0.00	0.00		0.01	600	0.26		0.8%		1.2%	0.8%	54%	0.8%	100.0%	000	000	0.00	o:	01	0.00	0.11	44.4%	0.4%	0.8%	0.8%	42%	0.4%	44.4%
25			134	1		0.00	0.00	0.00		0.01	000	0.25	+	0.4%		0.8%	1.2%	36% 24%	1.2%	1000%	000	000				0.00	0.14	54.4%	0.4%	0.8%	0.8%	2.8%	0.4%	54.4% 51.6%
27			136	2		000	0.00	0.00		300	001	0.43		1.2% 0.8%		12%	0.7%	14.7% 65%	2.1%	1000%	001	000	0.00			0.00	0.23	52.8% 59.4%	12%	09%	0.7%	11.5% 5.3%	09%	52.8% 59.4%
29			140	2	_	0.00	0.01	0.00	+	0.01	000	0.51		0.5%	\neg	1.0%	0.7%	1.0%	0.3%	100.0%	000	000	0.00	0.0	00	0.00	0.72	55.9%	0.5%	0.7%	0.5%	0.7%	0.2%	55.9%
30			141	2		0.00	0.00	0.01		205	0.01	0.44	+	0.7%		1.6%	1.1%	11.2%	1.4%	100.0%	000	001	0.00			000	0.19	43.2%	0.7%	1.1%	0.9%	87%	07%	41.2% 47.0%
32	K Pas	ich i	147	2		000	0.01	0.00		0.03	000	0.55		0.7% 0.8%		0.9%	0.4%	46% 15%	0.2%	1000%	000	0.00	0.00			0.00	0.32	57.8% 52.0%	0.6%	06% 08%	02%	29%	02%	57.8% 52.0%
34			152	5		0.02	0.01	0.00	_	31.0	002	1.19		1.9%	\neg	1.3%	0.2%	13.0%	1.9%	100.0%	001	0.01	0.00	0.1	13	0.01	5 55	45.0%	1.1%	1.0%	0.1%	10.6%	0.8%	45.0%
35			153 154	5		0.02	0.02	0.00		31.0	0.01	1,23	-	19%		1.5%	0.3%	11.2% 2.4%	1.1% 0.3%	1000%	002	002	0.00			100	0.63	51.0% 75.1%	12%	1.3%	02%	10.0% 1.8%	05% 02%	51.0% 75.1%
37			155	5				0.00		0.01	0.01	1.44		0.5%		1.9%	0.2%	0.9%	0.6%	100.0%	001		0.00		01	0.01	1.02	71.1%	0.3%	1.3%	0.1%	0.7%	0.3%	71.1% 54.5%
39			156	5	_	0.02	0.02		+	0.17	002	1.16	+	1.0%	\neg	2.8%	2.1% 0.2%	0.9% 14.2%	1.1%	1000%	001	0.01	0.00	0.1	13	0.01	0.52	54.5% 45.4%	0.7%	1.9%	1.8%	0.7% 10.9%	0.6%	45.4%
40			163	5	-	0.02	0.02	0.00	Ŧ	0.04	0.01	1.12	-	2.0%		1.9%	0.4%	35% 13%	0.6% 0.4%	100.0%	002	002	0.00	0.0		000	0.80	71.4%	1.4%	1.9%	0.3%	21%	0.4%	71.4% 75.1%
42			165	5	1	000	0.04	0.02	#	0.01	001	1.79		08% 10%		2.2%	1.3%	0.6%	0.7%	1000%	001	003	0.02	0.0		0.01	1.12	63.4% 44.0%	0.6%	16%	1.0%	0.4%	04%	63.4% 44.0%
44			2 13	2	_	0.02	0.01	0.01	_	0.07	0.01	0.40		3.7%	\neg	2.5%	1.7%	14.1%	21%	100,0%	001	0.01	0.00	0.0	05	0.00	0.19	41.0%	23%	2.1%	15%	10.6%	0.8%	41.0%
45		F	4 13 6 13		-	0.02	0.00	0.01	Ŧ	0.04	0.01	0.44	-	19%		2.5% 2.2%	2.8%	10.1% 7.4%	1.0%	100.0%	001	001	001	0.0		900	0.17	29.2% 43.0%	23%	1.0%	23%	7.6% 5.8%	09%	29.2% 41.0%
47			8 13	2		0.02	0.02	0.02		0.01	0.01	0.29		44%		575	5.4%	135	2.6%	100.0%	001	0.01	0.02	0.0	01	0.01	0.21	\$1.7%	21%	16%	19%	23%	1.3%	\$1.7%
48			10 13 11 12			0.02	0.03	0.03		0.18	003	0.96	+	2.2% 4.1%	-	1.9%	1.7% 0.9%	18.4% 17.2%	2.9%	100.0%	001	001	002	0.1		0.01	0.42	44.0% 56.6%	13%	15%	2.5%	14.2%	1.2%	44.0% 56.6%
50			12 14			0.04	0.03	0.01		0.02	002	1.00		3.2%		2.7%	1.2%	21% 25.7%	22% 14%	100.0%	002	602	0.01			0.01	0.54	50.1% 44.2%	22%	2.0%	1.0%	15%	0.0%	50.1% At 7%
21 22 22 22 23 24 25 24 25 25 26 25 26 25 26 25 26 25 26 25 26 25 26 25 26 25 26 25 26 25 26 25 26 25 26 25 26 25 26 25 26 25 26 26 26 26 26 26 26 26 26 26 26 26 26			18 14	4		0.03	0.03	0.01		0.18	002	0.94		3.2%		2.8%	0.8%	11.6%	2.4%	100.0%	002	0.02	001	0.1	13	0.01	0.37	38.7%	1.8%	2.1%	0.6%	13.5%	1.1%	38.7%
53		\vdash	19 14 20 14		+	0.03	0.03	0.01	+	0.04 70.0	002	0.71	+	2.2%		4.0% 3.2%	15%	5.1% 7.3%	24%	100.0%	002	003	0.01	0.0		0.01	0.40	55.8% 45.5%	2.4%	18% 21%	1.1%	37% 59%	11%	55.8% 45.5%
55			24 15	10		0.09	0.07	0.02		0.53	007	2.83		13%		25%	05%	11.6%	25%	1000%	006	006		0.3	29	0.03	1.07	37.9% 46.2%	21%	21%	0.4%	11.7%	11%	37.9% 46.2%
57			26 15	10		0.14	0.12	0.03	_	0.08	006	2.22		6.2%		5.2%	1.3%	3.7%	2.8%	100.0%	0.09	0.09	0.02	0.0	96	0.03	1.50	67.5%	40%	42%	1.0%	2.7%	1.2%	67.5%
58			27 15 28 15			0.11	0.09	0.00		0.07	0.06	2.36	ΗΞ	44% 23%	\exists	1.0%	05% 46%	28% 27%	25% 22%	100.0%	005	0.06	0.01			003	1.66	70.1% 47.1%	32%	2.7% 19%	0.3%	19%	11%	70.1% 47.1%
60			34 16.	10		0.09	0.04	0.03		0.72	0.12	2.72		3.2%		1.5%	1.2%	26.4%	43%	100.0%	006	003	003	0.5	54	0.05	0.97	35.8%	2.0%	12%	1.0%	19:9%	1.7%	35.8%
62			35 16 36 16	10		0.10		0.04		0.06	005		+	46% 42%		4.5% 6.4%	1.8%	37% 18%	2.1% 2.2%	100.0%	007	0.12	0.03	0.0	03	0.02	1.62	70.2%	2.9%	3.4% 5.2%	1.4%	2.4% 1.2%	1.0%	70.2%
63		\blacksquare	37 10	10	_	0.09	0.13	0.08	т	0.10	0.04	2.50	_	3.3%	=	5.1%	10%	38%	1.6%	100.0%	005	0.09	0.06	0.0	07	0.03	1.59	61.7%	1.7%	2.4%	22%	27%	10%	61.7%

- K-patch High CH

															max ratio ou	t of all beams												max ratio out of all	beams		
Н		1	1	Т	т			4cm2 PD)	nW/on2)				20.2%	12.25	7.5%	25.25	14.6%	100.0%	-	Kom2 PD(m	W/cm2) a	rt 10mm evalu	uation dist	ance	74.0%	11.0%	11.1%	5.6%	25.0%	535	74.0%
No. I	lodule Typ	e Seam ID_1	Sema ID 2	2 Feed no.		1	Т	T	Ť			per	ratio	ratio	ntio	ratio	ratio	ntio					T	т —	ratio	ratio	ntio	ntio	ratio	ntio	ntio
					54/Righ	s) S3(Left)	\$5(Top	(S6(Bott	(more)	(Front)	S2(Rear)	Beam Back-off	(Right 2mm)/(wonst- surface 2mm)	(Left 2mm)/(wonst- surface 2mm)	(Top 2mm)/(worst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	54(Right)	S3(Left)	SS(Top)	SS(Bottom)	\$1(Front	(S2)Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(wont- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Sottom 10mm)/(worst- surface 2mm)	(Front 10mm)/(wonst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
1		0		1	0.00	0,01	0.00	0.00		000	0.15	(d0)	8.6%	13%	1.2%	18.4%	2.6%	100.0%			0.00	0.02	0.00	0.06	41.4%	19%	26%	0.7%	11.8%	1.3%	41.4%
2		4		-	0.01	0.01	0.00			001	0.15		60% 11.2%	4.6% 5.6%	2.0%	13.2% 12.0%	4.0%	100.0%	001	001	0.00	0.01	0.00	0.06	38.4%	13%	13% 48%	13%	8.6%	1.3%	38.4% 37.6%
4		6		1	0.00	0.01	0.00			001	0.14		80% 58%	6.6%	10%	66%	5.8%	1000%	601		0.00	0.01	0.00		29.9%	44%	5.1%	29%	51%	29%	29.9%
6		10		2	0.00	0.01	0.02	0.0		001	0.21		65%	2.8%	7.5%	20.6%	17%	100.0%	001	000	0.00	0.03	0.00	0.00	36.0%	42%	1.9%	5.6%	15.9%	1.9%	36.0%
8 9		12	-	2	0.02	0.01	0.00	0.01		002 002	0.27		7.4%	4.0%	1.1% 2.6%	33%	5.5% 7.4%	100.0%		001	0.00	0.03	0.01		42.2%	4.0% 7.4%	17% 52%	19%	10.3%	22% 10%	36.8% 42.2%
10		13		2	0.03	0.00	0.00			0.01	0.31		8.0% 7.4%	2.5%	2.2%	25.5% 17.2%	2.9%	100.0%	002	001	0.00	0.05	0.00	0.09	29.6%	48%	19%	19%	16.9% 10.3%	13%	29.6% 36.8%
11 12 13 14		19		2	0.03	0.02	0.00	0.01		003	0.26		10.0%	9.2%	15%	42% 69%	10.0%	100.0%	001	0.02	0.00	0.01	0.01	0.12	46.5% 30.7%	54% 13%	7.3% 2.6%	12% 29%	31% 55%	18%	46.5% 30.7%
13		24		5	0.05	0.03	0.01	0.10		002	0.69		7.7%	1.6%	1.2%	23.4%	2.5%	100.0%	003	0.02	0.00	0.11	0.01	0.25	35.0%	19%	2.9%	0.9%	15.2%	1.2%	36.0%
15		25	1	5	0.05	0.03	0.01			002	0.76		16.0%	4.5% 13.3%	1.2%	9.3% 7.7%	3.2% 10.2%	100.0%	003	003	0.01	0.06	0.01	0.32	42.6% 54.6%	16% 72%	3.3% 11.1%	0.8%	7.4%	12%	42.6% 54.6%
15 16 17 18 19 20 21 22 23 24 25 26 27 28		27 28		5	0.11	0.06	0.01			0.05	0.63		17.7%	9.5%	1.6%	54% 56%	78% 2.1%	100.0%		0.05	0.00	0.02	0.02	0.31	48.3% 36.5%	11.2%	7.8%	13%	13% 37%	15%	41.2% 36.5%
18		34 35		5	0.02	0.01	0.02			004	0.78		2.7% 9.3%	0.8% 12.2%	2.5% 2.0%	35.2% 9.3%	5.7% 5.1%	100.0%		001		0.19	0.02		27.7% 50.2%	1.9%	06%	19% 14%	25.0% 5.4%	25% 19%	27.7% 50.2%
20		36		Š	0.11	0.06				008	0.53		20.3%	11.6%	0.9%	47%	14.6%	100.0%	006	005		0.02	0.03		50.8%	11.8%	86%	0.8%	10%	5.3%	50.8%
21		37 128	+	1	0.07	0.04	0.01	0.00		002	0.57		12.9%	6.3%	1.9%	12.6% 12.8%	40% 1.3%	100.0%	005	003	0.00	0.04	0.01	0.10	49.0%	8.7% 0.9%	47% 04%	1.6%	7.5% 7.8%	19%	49.0% 43.1%
23		130		1	0.00	0.00	0.00	0.00		000	0.28		07% 1.1%	1.1% 0.7%	0.7%	85% 53%	1.4%	100.0%	600	000	0.00	0.02	0.00	0.12	42.9% 44.4%	0.7%	0.7% 0.4%	0.7% 0.7%	64% 42%	0.7% 0.4%	42.9% 44.4%
25		134		1	0.00	0.00	0.00	0.00		000	0.28		04%	1.1%	1.1%	32% 24%	0.7% 1.2%	1000%	000	000	0.00	0.01	0.00	0.15	51.7% 51.6%	0.4%	0.7% 2.4%	0.7%	25%	04%	51.7% 51.6%
26		135		2	0.00	0.01	0.00	0.00		000	0.17		1.2%	1.0%	0.8%	15.1%	2.7%	100.0%	000	000	0.00	0.00	0.01	0.09	51.9%	0.8%	0.8%	0.0%	11.4%	1.2%	51.9%
28		139 140	1	2	0.00	0.01	0.00	0.0		000	0.56		1.1%	1.1%	0.5% 0.8%	63% 1.1%	0.3%	100.0%	000		0.00	0.03	0.00	0.33	59.2% 56.7%	0.7%	09% 08%	0.4%	5.0%	0.4%	59.2% 56.7%
30		141		2	0.00	0.00				001	0.50		06% 12%	1.4% 0.8%	1.8% 0.8%	11.0%	1.8%	100.0%	000	001	0.00		0.00	0.22	43.7% 42.9%	0.4%	10%	14%	9.6% 11.2%	08% 10%	41.7% 42.9%
	X Pass	n 147		2	0.00	0.00		0.00		000	0.61		07% 1.1%	1.1%	0.2%	435	0.2%	1000%	000	001		0.02	0.00	0.35	57.4% 52.0%	05%	08% 08%	0.2%	2.8%	0.2%	57.4% 52.0%
24		152		5	0.00	0.02	0.00	0.20		003	1.34		1.0%	1.4%	0.2%	15.0%	2.3%	100.0%	001	0.02	0.00	0.14	0.01	0.59	43.8%	0.7%	1.1%	0.1%	10.7%	0.9%	43.8%
35		153	-	5	0.00	0.03				002	1.37		12%	1.7%	0.1%	12.2% 3.0%	1.4% 0.5%	100.0%	001		0.00	0.13	0.00	0.68	49.7% 74.0%	0.9%	1.4%	0.1%	9.7% 2.2%	05% 02%	49.7% 74.0%
37		155		5	0.00	0.03				001	1.59		08% 12%	2.0%	0.2% 2.5%	12%	0.7% 1.2%	100.0%	001	002	0.00	0.01	0.01		70.4% 56.6%	0.6%	15%	0.1%	0.8%	0.4% 0.8%	72.4% 56.6%
39		162		5	0.01	0.02		0.20	,	003	1.21		1.1%	1.4%	0.2%	15.4%	2.4%	100.0%		0.02		0.14	0.01		44.1% 72.2%	0.8%	1.1%	0.2%	11.0%	0.0%	44.1% 72.2%
41		164		5	0.00	0.04	0.00	0.00		001	1/1		0.8%	2.5%	0.3%	12%	0.4%	100.0%	001	003	0.00	0.01	0.00	1.04	73.2%	0.6%	1.8%	0.2%	0.8%	0.2%	73.2%
32 33 34 35 36 37 38 39 40 41 41 42 43 44 45 46 47 46		165	128	2	0.02	0.04	0.03			002	0.45		1.1%	2.3%	1.2%	0.7% 19.5%	27%	100.0%	001	003	0.02	0.01	0.01	0.20	65.2% 43.4%	20%	1.7% 1.5%	1.0%	0.5%	05% 1.1%	65.2% 41.4%
44		2	130	2	0.00	0.01	0.01	0.00		001	0.52		27% 47%	1.7%	1.0%	15.1%	21%	100.0%	001		601	0.05	0.01	0.21	41.6% 40.2%	1.7%	1.4%	12%	10.1%	10%	41.6% 40.2%
46		6	134	2	0.01	0.00	0.01	0.00		001	0.47		28%	10%	2.3%	68% 39%	23%	100.0%	001	001	0.00	0.02	0.01	0.21	43.6% 55.4%	1.7%	23%	19%	5.1% 2.8%	1.1%	43.6% 55.4%
45		10	138	4	0.03	0.02	0.03	0.21		004	0.98		2.0%	1.5%	1.5%	21.8%	16%	100.0%	0.02	0.01	003	0.16	0.02	0.45	45.0%	1.0%	1.1%	27%	16.2%	1.5%	45.0%
50 51		11	139		0.03	0.03	0.01			002	1.06		19% 45%	13% 24%	0.8%	15.5%	25% 27%	100.0%		602 602		0.09	0.01	0.42	49.9% 51.7%	21%	25%	0.7%	11.0%	12%	49.9% 51.7%
51		13	141	4	0.04	0.03	0.02			003	0.91		41%	3.1%	2.6%	28.1% 21.8%	16%	1000%	002	0.02	002	0.18	0.02	0.40	43.5% 38.6%	24%	2.0%	19%	19.2%	16%	43.5%
52 53		19	147	- 4	0.04	0.05	0.01	0.00		003	0.78		46%	6.4%	0.9%	60%	41%	100.0%	0.02	0.04	0.00	0.04	0.01	0.44	54.5%	24%	5.1%	0.6%	45%	1.4%	94.5%
54 55		20	148	10	0.03	0.03	0.03	0.60		002 008	2.09		25%	2.9%	1.1% 0.7%	7.8% 20.7%	1.6%	100.0%	005	002 005	0.03	0.06	0.01	1.11	44.6% 38.4%	1.7% 1.7%	2.1% 1.8%	23%	5.9% 13.8%	08% 1.1%	44.6% 38.4%
56		25	153	10	0.10	0.10	0.02			005	2.94		14%	125 425	05%	13.1% 57%	15%	100.0%	006	008	001	0.31	0.03	1.34	45.5% 69.6%	19%	26%	0.4%	10.5%	15%	45.5% 69.6%
57 58 59 60 61		27	155		0.15	0.14	0.02			008	2.56		60% 27%	5.0%	0.0%	10%	12%	100.0%	010	011	0.01	0.05	0.03	1.00	70.5% 47.2%	18% 20%	44% 16%	0.5%	1.9%	1.3%	70.5% 47.2%
60		34	162	10	0.07	0.04	0.03	0.8		0.14	2.00		2.3%	1.4%	1.1%	30% 30.0%	23% 51%	100.0%	004	003	003	13.0	0.06	1.00	35.0%	15%	1.1%	32%	21.9%	2.1%	35.0%
62		35	163		0.09	0.09		0.13		0.05	2.28		38% 58%	3.7% 5.0%	1.0%	5.6% 2.0%	22% 51%	100.0%		0.07	0.02	0.07	0.02		65.0% 70.7%	23% 15%	2.9% 1.9%	0.7%	32% 14%	17%	65.0% 70.7%
63		37	165	10	0.12	0.10	0.07	0.10		0.04	2.80		42%	15%	2.4%	35%	13%	100.0%	007	007	0.05	0.07	0.02	1.77	63.2%	2.4%	2.4%	12%	2.4%	0.8%	63.2%

[Folder Closed Status]

- K-patch Low CH

																max ratio ou	t of all beams											max ratio out of all b	HAPTS		
								40	m2 PD(m)	N/on2)				23.0%	61.6%	8.2%	31.9%	4.4%	100.0%	4cm2 PD/m	W/cm2)	at 10mm eva	eluation di	dance	76.4%	15.5%	42.1%	6.4%	23.1%	2.5%	76.4%
No. M	odule Typ	se Seam ID_1	Sema ID_2	Feed no.			ei ss		SS/Somo	Τ	Smath	Citiane	per Seam	ratio	ratio (Left 2mm)/(worst-	ratio	ratio	ratio (Fomt 2mm)/(worst-	ratio				n) S1(Fro	nti S2/Rear	ratio worst-surface	ratio	ratio	ratio	ratio	ratio	ratio (Rear 10mm)/(worst-
					S4/Rig	10) 53(58	(t) 55	(lop)	sejecto	210	Hone	22(4881)	Back-off	(Right 2mm)/(wonst- surface 2mm)	surface 2mm)	(Top 2mm)/(wonst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	S4(Right) S3(Left)	33(10)	p) sejection	10) S1(HO	al Phiens	(10mm/2mm)	(Right 10mm)/(wont- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Sottom 10mm(/(word- surface 2mm)	(Front 10mm)/(worst- surface 2mm)	surface 2mm)
1		. 0		1	0.00			0.00	0.01		000	0.10	(All	17.7%	35.4%	1.0%	11.5%	42%	1000%	001 002			0.00		37.5%	11.5%	17.7%	1.0%	10.4%	2.1%	37.5%
2		- 2	-	1	0.00			000	0.01		000	0.12	-	10.4%	35.7% 36.0%	2.6% 5.6%	11.2%	2.6%	100.0%	001 003			0.00		36.5% 29.2%	7.8% 6.7%	215% 19.1%	12% 45%	7.8% 10.1%	09%	36.5% 29.2%
4		- 6		1		0.00			0.01		000	0.11		8.0%	22.8%	15%	7.1%	1.8%	100.0%	601 602		0.01			31.0%	53%	19.5%	27%	44%	03%	31.0%
6		10		2	0.00	0.04		0.01	0.01		000	0.12		8.5% 7.6%	30.8% 24.6%	5.7% 8.2%	6.8% 20.5%	1.7%	100.0%	001 002 001 002		0.01	0.00		29.2% 28.1%	43%	16.2%	4.2% 6.4%	4.3% 14.0%	0.9% 1.8%	29.2% 28.1%
7 8		11 12			0.00				0.02		001	0.20		11.5%	42.0% 42.7%	1.5%	11.0%	10% 25%	100.0%	002 005		0.02	0.00		32.0% 36.8%	85%	23.5%	15%	75% 21%	2.0%	32.0% 36.8%
9		13		2	020	0.00		000	0.04	ľ	000	0.20		86%	32.0%	1.0%	22.3%	2.0%	100.0%	001 003	0.00	0.03	0.00	0.06	21.4%	5.6%	16.2%	25%	16.2%	1.0%	28.4%
10		16	-	2	0.00			000	0.02		001	0.20		11.5% 10.8%	40.0% 55.2%	1.5%	11.0%	10%	100.0%	002 005	0.00		0.00	0.06	32.0% 47.4%	85% 65%	21.5%	15%	75% 26%	2.0%	32.0% 47.4%
12		20			0.00			0.01	0.02		000	0.21		6.2% 5.6%	30.3% 41.6%	6.2%	9.5% 22.9%	1.9%	100.0%	001 003	0.00		0.00	0.07	32.2% 34.5%	47%	13.7%	57%	7.1% 16.2%	09%	32.2% 34.9%
13		25	_			0.20			0.11			0.48	_	5.6% 8.2%	41.6%	1.2%	22.9% 14.8%	2.5% 1.7%	100.0%	002 011					34.5%	42% 59%	22.5%	1.0%	16.2%	15%	34.5%
15		26		5	0.00	0.11		0.01	0.03		002	0.54		13.4%	61.6% 36.7%	2.0%	485	14%	1000%	005 023		0.02	0.01	0.30	55.6% A4.8%	9.9%	42.1%	15%	32% 10%	19%	56.6% 44.8%
17		20		5	0.00			0.03	0.03		001	0.49		66%	27.4%	6.8%	6.0%	2.3%	1000%	007 012			0.01	0.12	23.7%	41%	17.9%	5.1%	62%	12%	21.7%
18		34		5	0.00			0.02	0.18		002	0.56		45% 10.3%	28.1% 50.6%	1.9%	31.9% 6.3%	12% 12%	100.0%	002 007			0.01		29.7% 45.2%	2.9%	11.8% 32.7%	30% 1.3%	23.1% 4.2%	20%	29.7% 45.2%
20		36		ŝ	0.13	0.34	4 1	0.01	0.02	-	003	0.56		23.8%	60.1%	1.6%	3.7%	4.4%	100.0%	0.09 0.23	0.00	0.01	0.01	0.30	53.4%	15.5%	40.6%	12%	23%	25%	53.4%
21		128	-	5	0.00			0.01	0.04		001	0.36	_	16.3%	33.2% 21.2%	13% 08%	11.1% 8.8%	2.5%	100.0%	004 006	0.00	0.03	0.01	0.18	49.0%	10.5%	17.7%	2.8%	56%	14%	49.0% 46.2%
23		130			0.00		5	000	0.02		000	0.22		09%	21.8% 21.4%	0.9%	10.2% 55%	0.9%	1000%	000 002		0.02	0.00	0.09	41.2% 42.7%	0.9%	10.2%	0.5%	7.9%	05%	41.2%
25		132		1	0.00			000	0.01	+	000	0.22		0.9%	21.4%	1.4%	55% 33%	0.5%	100.0%	000 003	0.00	0.01	0.00	0.09	42.7% 53.6%	0.5%	14.8%	0.9%	45% 29%	05%	42.7% 53.6%
26		136		1	0.00			000	0.00		000	0.17		18%	26.3% 27.5%	2.4%	24% 15.9%	1.2%	100.0%	000 002	0.00	0.00	0.00		46.7% 46.9%	12%	12.6%	24%	1.0%	08%	45.7% 45.9%
28		139		2	0.00	0.11	5	000	0.03	-	000	0.43		1.2%	34.0%	0.2%	72%	0.7%	100.0%	000 007		0.03	0.00		58.0%	0.7%	16.3%	0.2%	6.1%	05%	58.0%
30		140		2 2	0.00	0.34	,	000	0.01		000	0.46		0.6% 1.4%	28.5% 19.2%	0.6% 1.2%	13%	0.4%	100.0%	000 007	0.00		0.00	0.27	55.4% 42.7%	0.6%	13.8%	0.4%	0.6% 8.9%	0.2%	55.4% 42.7%
31		146			0.00			000	0.06		001	0.40		1.3%	22.4% 31.1%	0.5%	14.0%	1.3%	100.0%	000 004	0.00		0.00		41.2% 07.9%	1.0%	8.0%	0.3%	11.3%	0.8%	41.2%
33	X Pat	th 147				0.14			0.02		000	0.45		0.7% 1.1%	23.3%	0.2% 1.3%	44%	0.4%	100.0%	000 007					\$7.1% \$1.1%	0.4%	14.9%	1.0%	27%	0.2%	57.1% 51.1%
34		152 153		5	0.00	0.20		000	0.17		002	1.00		2.0%	25.8%	0.4%	16.0%	1.5%	100.0%	002 013			0.01	0.44	40.5% 46.9%	1.6%	12.2%	0.2%	11.0%	03%	40.5% 46.9%
36		154		5	0.00	0.52	2 1	000	0.03	ľ	000	0.98		0.6%	53.0%	0.3%	2.6%	0.3%	100.0%	001 030	0.00	0.02	0.00		75.2%	0.6%	30.2%	0.2%	1.9%	0.2%	75.2%
37		155	-	5	0.00			0.00	0.01		001	1.20		0.7% 1.5%	41.6% 23.2%	0.1% 2.3%	0.7%	0.7%	100.0%	001 029			0.01		70.7% 51.8%	0.5%	24.2% 11.3%	0.1%	0.4%	0.4%	70.7% 51.8%
39		162		5	020	0.29		000	0.16		002	1.06		2:0%	27.0%	0.2%	16.5%	1.5%	100.0%	002 013	0.00	0.14	0.01	0.43	40.0%	1.4%	12.3%	0.1%	13.3%	0.8%	42.0%
40		163		5	0.00	0.50	5 1	000	0.03	-	000	1.04	\vdash	1.7%	46.2% 53.4%	0.4%	37% 12%	0.5%	100.0%	001 032			0.00		70.9%	12%	25.6%	0.1%	2.4%	0.3%	70.9% 76.4%
42		165	128		0.00			10.0	0.01		001	1.55		61%	31.4% 32.2%	0.7%	0.4%	0.8% 1.7%	100.0%	001 0.25 002 005	0.00	0.00	0.01		62.5% 44.5%	43%	164%	0.6%	0.3% 8.1%	05%	62.5% 44.5%
44		2	130	2	023	0.11		0.01	30.0	-	001	0.42		48%	25.4%	1.9%	13.2%	12%	100.0%	001 006	001	0.04	0.00	0.17	41.1%	33%	13.1%	1.4%	10.2%	0.7%	41.1%
45		- 4	132	2	0.00			0.01	0.04		000	0.38		45% 10%	29.9%	14%	11.3% 7.0%	1.0%	100.0%	001 006		0.03	0.00		38.8% 42.4%	2.9%	14.4%	2.5%	8.7% 5.2%	0.8%	38.8% 42.4%
47			136	2	0.00			0.02	0.02	- 3	001	0.25		5.1%	34.1%	5.7%	425	2.0%	100.0%	001 005	0.02	0.01	0.00		52.8%	2.8%	15.1%	45%	31%	1.1%	52.8%
40		10	138	4	020			003	0.17		002	0.66	-	14% 43%	25.6% 42.7%	15%	20.0%	21%	100.0%	002 011	002	0.13	0.01	0.33	38.0% 52.2%	22%	12.3%	27%	15.2%	12% 07%	38.0% 52.3%
50		12	140	4	0.00		9 1	0.02	0.02		001	0.90		52%	33.3% 25.1%	2.1%	2.0%	12%	100.0%	004 017			0.01		52.4% 41.0%	4.0%	18.5%	1.6%	1.5% 15.4%	07%	50.4% 41.0%
52		15	141		0.00	0.24	4 1	0.02	0.14	-	001	0.65		42%	31.8%	1.2%	17.6%	1.6%	100.0%	002 011	001	0.10			29.1%	3.1%	14.2%	0.9%	13.3%	09%	29.1%
53		19	147	4	0.00	0.21		0.01	0.03		001 001	0.59	F	5.6% 2.4%	36.1% 21.6%	1.2%	57% 91%	1.7%	100.0%	002 012		0.03	0.01	0.32	54.0% 41.4%	12%	20.6%	10%	42% 7.1%	10%	54.0% 41.4%
55		24	152	10	0.00	0.80		000	0.46	-	005	2.37		13%	37.4%	05%	20.2%	21%	1000%	006 041	001	0.37	0.03	0.92	38.7%	2.7%	17.4%	0.5%	15.5%	1.2%	38.7%
56		25	153	10	0.11			000	0.35		004	1.99	⊨	46% 53%	40.1% 50.2%	05% 12%	147% 12%	15%	100.0%	008 047			0.02		45.0% 63.4%	13% 17%	19.4%	0.4%	10.4% 2.4%	03%	45.0% 68.4%
58		27	155	10	0.13	0.80		0.02	0.05		003	2.00		6.7%	44.4%	0.8%	23%	1.4%	100.0%	0.09 0.50	0.00	0.04	0.02	1.38	68.7%	45%	24.9%	0.6%	1.7%	0.8%	63.7%
60		26 34	156 162		0.00	0.64		0.12	0.06			2.72	\vdash	2.9% 3.6%	27.8% 27.3%	44% 13%	2.1% 27.6%	1.6%	100.0%	006 035 006 027	0.09		0.01		44.6% 33.0%	2.3% 2.5%	12.9%	3.4% 1.0%	1.7% 21.6%	1.1% 1.5%	44.6% 33.0%
61		35 36	163	10	0.11			0.02	0.07		003 004	2.00		5.3% 7.7%	\$1.7% \$5.7%	1.1%	33% 14%	15%	100.0%	006 059 010 070				1.25	62.5% 68.0%	28%	29.6% 34.5%	0.9%	21%	08% 11%	62.5%
63		37	165			0.71					003	2.00		46%	34.1%	1.8%	25%	12%	100.0%	0.10 0.70			0.00		62.7%	25%	17.5%	12%	1.6%	07%	62.3%

- K-patch Mid CH

															max ratio o	t of all beams									1			max ratio out of all	beams		
\vdash		т —	Г	т —	_			4cm2	PD/mW/on	m2)			10.9%	56.1%	7.0%	24.05	455	100.0%	4	Kom2 PD/m	Witn2) a	rt 10mm evalu	uation dist	ance	75.1%	7.5%	10.2%	55%	25.7%	215	75.15
No. M	dule Type	Beam ID_1	Serva ID 3	2 Feed no.	\vdash	$\overline{}$	Т	Ť		_	_	per	ratio	ratio	mio	ratio	ratio	ntio		T	_	T		$\overline{}$	ratio	ratio	ntio	ntio	ratio	ntio	ntio
				1	54/Rig	he) S3(Left	t) \$5(To	p) S6((Bottom)	\$1(Front)	S2(Rear)	Beam Back-of		(Left 2mm)/(worst- surface 2mm)	(Top 2mm)/(wonst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Forst 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	S4(Right)	S3(Left)	SS(Top)	SS(Bottom)	\$1(Front	(S2(Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(wont- surface 2mm)	(Left 10mm)/(wonst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Sottom 10mm)/(worst- surface 2mm)	(Front 10mm(/(wonst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
1	_	0	-	1	0.01	0.06	0.00	0	0.03	0.00	0.16	(dB)	7.1%	36.0%	1.2%	17.4%	2.6%	1000%	001	003	0.00	0.02	0.00	0.06	34.0%	45%	16.7%	06%	11.6%	13%	3485
2		2		1	0.00	0.05			0.02	000	0.15		75%	31.6% 32.3%	2.7%	11.0%	2.1%	100.0%	001	003	0.00	0.01	0.00	0.06	42.4% 36.8%	48%	19,2%	21%	75% 75%	1.4%	40.4% 36.8%
4		6		į.	020	0.05	0.00		0.01	000	0.15		67%	30.2%	2.0%	81%	20%	1000%	001	0.03	0.00		0.00	0.06	36.9%	47%	17.4%	13%	6.0%	13%	35.9%
6		10		2	0.02	0.04	0.00		0.04	0.00	0.14		7.5%	21.1%	7.0%	13.6%	2.0%	100.0%	001	0.02	0.00	0.03	0.00	0.06	12.2%	55%	11.6%	55%	15.0%	1.0%	32.2%
7 8 9		11		2	0.02				0.04	001	0.31		6.0% 7.0%	42.9% 35.9%	1.2%	11.9%	2.6% 2.4%	100.0%	002	007		0.03	0.01		32.9% 45.2%	48%	23.9%	10%	9.0%	1.6%	12.9% 45.2%
10		13		2	0.00				0.07	601	0.27		49%	27.0% 42.3%	2.0%	25.8% 11.9%	2.6%	100.0%	001	004	0.00	0.05	0.01	0.00	28.8% 32.9%	3.7% 48%	14.6%	19%	18.0%	19%	28.8% 12.9%
11 12 13 14		19		2	0.00	0.16	0.00		0.01	001	0.30		8.3%	51.7%	1.2%	425	2.6%	100.0%	002	0.09	0.00	0.01	0.01	0.12	44.0%	5.6%	30.8%	1.0%	10%	1.7%	44.0%
13		20	-	5	0.02	0.25			0.03	000	0.62	-	67% 7.1%	28.3% 40.3%	1.4%	12.4% 21.5%	1.7% 1.0%	100.0%	001	013	0.01	0.10	0.00	0.19	36.3% 31.0%	18% 45%	13.8%	33%	8.3% 16.5%	1.8%	36.3% 31.0%
14		25		5	0.04				0.08	001	0.63		65%	48.1%	1.4%	12.3%	21% 45%	100.0%	003	015	0.00	0.07	0.01	0.28	43.4%	44%	23.2%	1.4%	10.3% 2.9%	13%	41.4%
15 16 17 18 19 20 21 22 23 24 25 26 27 28		27		5	0.00				0.03	602	0.74		10.9%	36.5% 31.4%	1.9%	39% 81%	2.9%	1000%		018	0.01	0.03	0.01	0.37	52.4% 31.7%	75% 45%	24.5% 15.8%	15% 53%	14%	18%	52.4% 31.7%
18		34		Š	0.00	0.22	0.02	2	0.25	003	0.72		40%	30.2%	13%	34.0%	16%	100.0%	002	0.09	0.02	0.19	0.02	0.20	27.0%	33%	12.1%	25%	25.7%	2.1%	27.0%
20		35	1	5	0.06				0.05	003	0.72	-	80% 85%	54.4% 49.1%	0.7%	75% 27%	19%	100.0%		0.30	0.01	0.03	0.02		49.0% 48.9%	6.6%	36.3%	0.8%	4.0%	2.5%	49.0% 45.9%
21		37 128		5	0.05	0.17	0.02	2	0.08	0.01	0.51		95%	11.9% 30.9%	2.9%	14.9% 8.4%	2.2% 0.5%	100.0%	003	0.09	0.00	0.06	0.01	0.27	52.8% #5.0%	6.7%	17.2%	25% 05%	11.2% 5.9%	14%	52.8% 45.0%
23		130		1	0.00		0.00		0.02	000	0.25		12%	22.8% 23.1%	0.8% 0.8%	8.8% 62%	0.8%	100.0%	000	003	0.00	0.02	0.00	0.11	43.6% 44.2%	0.8%	10.8%	0.8%	64% 46%	0.4% 0.4%	41.6% 44.2%
25		134		i	0.00	0.08	0.00		0.01	000	0.25		0.4%	31.7%	1.2%	4.1%	0.4%	100.0%	000	004	0.00	0.01	0.00	0.12	54.5%	0.4%	15.0%	0.8%	33%	0.4%	54.5%
26		136	+	2	0.00	0.13			0.00	000	0.17	-	23%	26.9% 26.8%	1.8%	2.3% 15.8%	1.2% 1.3%	100.0%	000	0.02	0.00	0.00	0.00	0.09	\$1.5% \$1.1%	12%	12.9%	12%	1.0%	06% 09%	\$1.5% \$1.1%
28		139		2	0.00		0.00		0.04	000	0.51		0.8%	35.5% 20.2%	0.4%	75%	0.6%	100.0%	000			0.03	0.00		58.8% 56.0%	0.6%	17.4%	0.4%	5.9%	0.4%	58.8% 56.0%
30		141		2	000		0.01		0.05	000	0.42		17%	20.0% 21.7%	1.4% 0.6%	11.0% 13.1%	0.7% 1.1%	100.0%	001	004	0.00	0.04	0.00		43.0% 46.0%	12%	9.4% 9.5%	12%	8.7% 9.2%	05% 06%	41.0% 46.0%
	C Past	147		2	0.00	0.17	0.00		0.02	000	0.55		05%	31.1%	0.2%	44%	0.4%	100.0%	000	008	0.00	0.02	0.00	0.31	57.0%	0.5%	14.6%	0.2%	2.7%	0.2%	57.0%
33		146	1	5	0.00				0.02	000	1.23	-	1.0%	24.9% 26.6%	1.2%	3.8% 13.7%	0.5% 1.3%	100.0%	000	0.15	0.00	0.02	0.00	0.31	52.5% 44.2%	0.7% 1.3%	10.9%	12%	2.8% 10.4%	0.3% 0.7%	52.5% 44.2%
35		151 154		5	0.02				0.15	001	1.10	Н	17%	28.9% 54.0%	0.2%	12.1%	0.9%	100.0%	002	0.18	0.00	0.11	0.01	0.63	49.8% 74.4%	12%	14.4% 31.1%	0.2%	8.7% 1.6%	05% 02%	49.8% 74.4%
37		155		5	0.00	0.65	0.00		0.01	001	1.42		13%	45.5% 26.5%	0.1%	0.8%	0.7%	1000%	001	0.36		0.01	0.01		70.7% 54.5%	0.4%	25.3% 12.7%	0.1%	0.7%	0.4%	70.7% 54.5%
39		162		5	0.02	0.32	0.00		0.17	0.02	1.71		19%	26.7%	0.3%	14.1%	1.3%	100.0%	0.02	0.15	0.00	0.13	0.01	0.53	44.6%	1.3%	12.4%	0.2%	10.8%	0.7%	44.6%
40		163	1	5	0.00			0 0	0.02	000	1.11	-	19%	47.3% 53.3%	0.4%	3.3% 1.2%	0.5%	100.0%	002	0.29	0.00	0.02	0.00		70.6% 75.1%	1.4%	26.0% 30.5%	0.3%	1.9%	0.3% 0.2%	70.6% 75.1%
32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48		165	128	5	0.02				0.01	002	1.75	F	40%	33.8% 27.7%	0.7%	0.6% 16.1%	0.9% 1.3%	100.0%	001	0.31	0.01	0.01	0.01		63.6% 42.4%	0.7% 2.7%	17.4%	0.7%	05%	05% 09%	61.6% 42.4%
44		2	130	2	0.02				0.07	001	0.47		41%	27.0% 29.7%	2.1%	15.0%	15%	100.0%	001	006	001	0.05	0.00	0.20	43.3%	10% 27%	12.2%	15%	11.2% 7.5%	09%	43.2% 42.5%
46		- 6	134	2	0.00	0.12	0.01		0.04	001	0.46		29%	25.9%	2.2%	7.9%	1.1%	100.0%	001	006	0.01	0.03	0.00	0.19	43.0%	2.0%	12.7%	1.8%	6.4%	0.4%	43.0%
40		10	136	4	0.03	0.25	0.03	3	0.02	0.02	0.37	-	7.4%	32.8% 26.3%	2.7%	55% 20.4%	2.2% 2.1%	100.0%	001	0.12	0.01	0.01	0.00	0.21	56.8% 42.0%	16% 24%	15.6%	22%	3.0% 15.8%	11%	56.8% 42.0%
49 50 51		11	139		0.00				0.15	601	0.03		19%	42.6% 31.0%	1.4%	17.7%	1.0%	100.0%		018	0.01	0.11	0.01	0.45	53.7% 51.9%	2.9%	21.5%	1.1%	13.5%	1.0%	51.7% 51.0%
51		13	141	4	0.00	0.79	0.02	2	0.22	0.02	0.77		35% 34%	25.0% 31.0%	17%	28.3% 19.0%	23%	1000%	0.02	0.09	002	0.16	0.01	0.35	44.6%	25%	11.6%	22%	20.4%	16%	44.6%
52 53		19	147	- 4	0.00	0.25	0.01	1	0.19	002	0.98		43%	32.4%	0.6%	585	1.6%	100.0%	003	0.15	0.00	0.03	0.01	0.41	35.3% 53.4%	12%	19.5%	0.9%	43%	0.9%	53.4%
54		20	148	10	0.00				0.08	001	2.79	H	2.0%	20.8% 36.4%	2.4%	8.7% 13.6%	1.1%	100.0%	001	010	0.03	0.07	0.01	1.04	46.3% 37.3%	1.4%	98% 16.5%	28%	6.8%	0.7% 1.2%	46.3% 37.3%
56		25	153		0.11	1.16	0.02	2	0.37	004	2.71		19%	42.6%	06%	13.7%	1.6%	100.0%	007	054	0.02	0.28	0.03	1.23	45.2% 85.9%	2.0%	20.0%	0.6%	10.1%	1.0%	45.2% 65.9%
58		27	155	10	0.11	1.33	0.02	2	0.07	004	2.40		46%	47.0%	0.8%	27%	1.6%	100.0%	0.00	0.66	0.02	0.05	0.02	1.70	70.9%	13%	27.4%	0.7%	1.9%	0.9%	70.9%
60		28 34	156		0.00				0.09	006	2.98	-	2.6%	29.7% 27.7%	13%	3.1% 27.9%	1.8%	100.0%		0.39		0.07	0.03		47.3% 35.2%	1.7%	13.0%	3.0%	22%	1.0%	47.3% 35.2%
57 58 59 60 61		35	163		0.12				0.09	004	2.28		52%	\$2.7% \$1.5%	0.7%	40%	1.7%	100.0%		0.71		0.06	0.03		61.5%	32% 11%	31.2%	0.6%	27%	12%	61.5% 62.8%
63		27	165		0.09		0.00			003	2.57		14%	34%	12%	42%	13%	100.0%				0.00			61.3%	22%	18.3%	1.1%	10%	0.7%	61.2%

- K-patch High CH

															max ratio ou	t of all beams												max ratio out of all	beams		
\Box	П		П	Т	Г			4cm2	2 PD/mW/c	m2)			18.5%	50.6%	7.5%	37.2%	4.0%	100.0%	4	ion2 PD(m	W/cm2) a	rt 10mm evalu	uation dista	nce	73.5%	12.6%	18.9%	\$7%	26.6%	2.3%	73.5%
No. Module	Туре	Seam ID_1	Sera ID,	2 Feed no.	SAJRSq	pht) S3(Le	et) SS(To	lap) Si	6(Bottom)	\$1(Front)	S2(Rea	per Bean Back o		ratio (Left 2mm)/(worst- surface 2mm)	ratio (Top 2mmi/(worst- surface 2mm)	ratio (Bottom 2mm)/(wont- surface 2mm)	ratio (Fornt 2mm)/(worst- surface 2mm)	ratio (Rear 2mm)/(wont- surface 2mm)	S4(Right)	S3(Left)	SS(Top)	S6(Bottom)	\$1(Front)	S2(Rear)	ratio worst-surface (10mm/2mm)	ratio (Right 10mm)/(wont- surface 2mm)	ratio (Left 10mm)/(worst- surface 2mm)	ratio (Top 10mm)/(worst- surface 2mm)	ratio (Bottom 10mm)/(wont- surface 2mm)	ratio (Front 10mm(//wonst- surface 2mm)	ratio (Rear 10mm)/(worst- surface 2mm)
1		0		-	0.0				0.03	000	0.17	_	48%	37.1% 21.6%	1.8%	19.2% 16.8%	1.8% 1.8%	100.0%		003		0.02	0.00	0.07	41.9%	10%	19.8%	12%	12.0%	12%	41.9% 40.7%
3		4	+	+ +	0.0	0.00	5 0.0	01	0.02	000	0.17	+	8.3%	33.8%	4.5%	12.0%	2.3%	100.0%		002			0.00	0.05	36.1%	45%	18.0%	30%	9.0%	15%	36.1%
4		6	_	-	0.0		5 00		10.0	000	0.15		7.2% 5.9%	29.6% 34.1%	12%	53% 44%	2.0% 1.5%	100.0%		003		0.01	0.00	0.05	32.2% 40.7%	46% 17%	17.1%	26%	19% 17%	13%	32.2% 40.7%
5		10	_	1 2	0.0		5 00		0.01	000	0.14	+	59% 62%	34.1% 21.1%	7.5%	4.4% 17.2%	1.5%	100.0%		0.02			0.00	0.06	40.7% 11.0%	3.7% 40%	16.3%	22% 57%	13.7%	0.7% 1.3%	40.7% 31.0%
7		- 11		2	0.0	2 0.12	2 0.0	80	0.05	0.01	0.32		64%	34.8%	0.6%	16.4%	1.6%	100.0%	0.02		0.00	0.04	0.00	0.12	36.0%	47%	20.4%	0.6%	11.0%	1.3%	36.8%
8		12	-	2	0.0				0.01	001	0.31	+	10.8%	29.2% 36.0%	1.2% 2.2%	11%	2.6%	100.0%	0.02	0.04	0.00	0.01	0.01	0.12	42.6%	72%	14.1%	23%	2.0%	1.6%	42.6%
6 7 8 9 10 11 12 13 14		10		2	0.0		2 0.0		0.05	0.01	0.32		66%	MAN	0.6%	16.4%	1.6%	100.0%		0.07			0.00	0.12	36.0%	47%	20.4%	0.6%	11.0%	1.3%	36.0%
11		19	-	2	00		0.0			0.01	0.28	+	98% 60%	41.4% 25.6%	1.8%	3.6% 4.9%	2.9% 1.5%	100.0%		008			0.01	0.12	42.9% 32.7%	10%	28.0%	15%	25% 34%	1.0%	42.9% 32.7%
13		24		5	0.0	5 0.30	0.0	23	0.19	0.02	0.72		7.4%	42.2%	1.4%	26.9%	2.9%	100.0%	003	0.17	0.00	0.14	0.01	0.24	33.8%	45%	23.3%	1.0%	18.9%	1.7%	33.8%
14		25	-	5	00		2 00		0.06	0.01	0.79	+	7.3%	41.5% 49.9%	1.3%	9.8%	1.8% 1.3%	100.0%		0.18	0.00	0.06	0.01	0.32	40.8%	47% 7.1%	23.2%	0.9%	7.9%	1.0%	40.8% 51.7%
16		27	+	5	0.0				0.03	002	0.67	+	13.2%	41.5%	4.5%	50%	2.9%	100.0%	005		0.02	0.02	0.01	0.32	41.0%	9.6%	29.1%	15%	10%	18%	41.0%
17		26 34		5	0.0				0.09	601	0.74	F	£9% 25%	28.7% 36.2%	4.7%	11.9% 37.2%	1.6%	100.0%	003	011	0.03	0.06	0.01	0.27	35.7% 28.1%	18%	14.7%	34% 25%	7.8% 26.6%	09% 23%	25.7% 28.1%
10		35	_	5	0.0		0.0	23	30.0	002	0.60	+	7.3%	55.8%	1.5%	85%	2.2%	100.0%		0.27	0.00	0.04	0.01	0.38	55.5%	5.3%	38.9%	1.0%	5.1%	1.5%	55.5%
20		36		5	0.1				0.03	003	0.64		18.5%	49.1%	2.0%	425 510%	40%	100.0%		0.22	0.00	0.02	0.01	0.32	50.2% 47.8%	12.6%	33.5% 22.0%	1.6%	28%	22%	50.2% 47.8%
21 22 23		128	_	1	0.0		5 00		0.02	000	0.61	+	12%	21.2%	0.8%	10.2%	0.0%	1000%		0.14		0.02	0.00	0.10	47.0%	98%	97%	0.0%	68%	04%	47.0%
23		130		1	0.0				0.02	000	0.28		1.1%	23.3%	1.7%	8.0%	1.1%	100.0%		003		0.02	0.00	0.12	43.6%	0.7%	10.5%	0.7%	5.8%	0.4%	43.6%
24 25 26 27 28		132	+	1	0.0				0.02	000	0.28	+	04%	24.7% 32.0%	1.1%	57% 36%	0.7%	100.0%	000	003	0.00	0.01	0.00	0.12	44.9% 53.2%	0.7%	11.3%	0.7%	42%	04%	44.9% 51.2%
26		136		i	0.0		5 00	10	0.01	000	0.16		1.8%	28.2%	1.2%	3.1%	1.2%	100.0%	000	002	0.00	0.00	0.00	0.09	54.6%	12%	14.1%	12%	1.0%	06%	54.6%
27		135		2	0.0		0.0		0.07 0.04	0.00	0.47		15%	12.0% 17.0%	1.2% 0.5%	14.8% 6.9%	1.7% 0.7%	100.0% 100.0%	001	010	0.00	0.05	0.00	0.25	53.8% 59.0%	1.1%	15.0%	1.1%	11.0% 5.4%	0.8% 0.4%	51.8% 59.0%
		140		2	0.0	0.20	0.0	0	0.01	000	0.64		06%	33.9%	0.6%	0.9%	0.3%	100.0%	000	0.09	0.00	0.00	0.00	0.36	56.9%	0.5%	14.3%	0.5%	0.6%	0.2%	54.9%
30		141	_	2	0.0				0.06	0.01	0.50	-	0.0%	21.2% 24.7%	1.6% 0.6%	12.0% 14.6%	1.0%	100.0%		0.05	0.00	0.04	0.00	0.22	41.9% 46.5%	12%	10.0%	1.4%	10.7%	0.6%	41.9% 46.5%
30 31 32 K 33 34	Pasch	147		2	0.0	0.20	0.0	00	0.02	0.00	0.61	_	1.0%	32.8%	0.2%	42%	0.3%	100.0%	000	0.09	0.00	0.02	0.00	0.35	57.8%	0.7%	15.2%	0.2%	25%	0.2%	57.8%
33		146		2	0.0				0.03	000	0.66	_	12%	25.4%	1.4%	3.8%	0.5% 1.6%	100.0%		007	0.00	0.02	0.00	0.35	52.6% 45.0%	12%	11.3%	1.1%	2.7% 10.2%	0.3%	52.6% 45.0%
35		153	+	5	0.0				0.16	001	1.36	+	2.4%	31.6%	0.2%	11.7%	0.9%	100.0%		0.21	0.00	0.14	0.01	0.69	45.0% 50.4%	15%	15.4%	0.1%	8.8%	05%	43.0% 52.4%
16		154		5	0.0		2 0.0	00	0.04	0.00	1.20		11% 08%	55.2% 47.7%	0.2%	29%	0.9%	100.0%	001	0.41	0.00	0.03	0.00	0.95	73.5% 70.7%	0.6%	31.7%	02%	22%	0.2%	73.5%
37		155	_	5	0.0		5 00	13	0.02	001	1.57	+	12%	47.7% 30.0%	1.7%	13%	1.2%	100.0%	001		0.00		0.01	1.11	70.7% 56.0%	0.6%	26.8%	0.1%	0.8%	0.4%	70.7% 56.0%
39		162		5	00		1 00		0.19	0.02	1.29		2.0%	29.6% 49.4%	0.4%	145% 115	1.6%	100.0%	002			0.14	0.01	0.58	45.1% 71.2%	12%	13.7% 27.3%	02%	10.0%	09%	45.1% 71.2%
40		164	_	5	0.0				0.02	001	1/41	+	02%	49.4% 54.8%	0.7%	1.1%	0.4%	1000%		0.945		0.02	0.00	1.02	73.4%	06%	27.3%	0.7%	0.7%	0.2%	73.4%
42		165		5	0.0				0.01	0.02	1.00		0.8%	36.2%	0.7%	0.7%	1.0%	100.0%	001	0.35			0.01	1.21	64.3%	0.5%	18.8%	0.6%	0.5%	05%	64.3%
43		2	128	2	00		0.0		900	001	0.46	+	15%	28.8%	1.7%	18.6% 17.5%	1.7% 1.9%	100.0%	001			0.06	0.01	0.21	45.0% 42.7%	22%	13.8%	0.9%	12.7% 12.5%	1.1%	45.0% 42.7%
29 40 41 42 43 44 45 46 47 46 47 48 50 51 53		- 4	132	2	0.0	2 0.14	4 0.0		30.0	601	0.47		40%	30.5%	2.8%	12.3%	1.3%	100.0%	001	007	001	0.04	0.00	0.19	40.5%	23%	15.3%	2.1%	9.3%	06%	40.5%
46		- 6	134		0.0				0.03	0.00	0.49	+	29%	26.9%	2.2%	59% 15%	1.9%	100.0%	001	0.07	0.00	0.02	0.00	0.22	41.9% 51.0%	27%	13.3%	18%	45%	0.6%	41.9% 58.0%
46		10	135	- 4	0.0	0.21	0.0	34	0.20	0.02	0.96		10%	28.8%	1.8%	21.2%	2.4%	100.0%	0.02	013	003	0.15	0.01	0.44	45.0%	22%	13.7%	29%	16.0%	1.4%	45.0%
49		11	129				0.0			0.02	0.90		19%	29.3%	1.0%	16.7% 2.0%	1.8% 1.0%	100.0% 100.0%		018			0.01	0.44	49.4%	2.7% 2.8%	20.0%	0.7%	11.9%	1.0%	49.4%
51		13	141				9 00			003	0.92	-	11%	31.6%	2.4%	30.3%	2.8%	100.0%		0.13			0.02	0.41	44.5%	21%	13.8%	12%	21.3%	1.6%	44.5%
52		18	146		0.0		0.0		0.21	0.02	1.04	\mathbf{I}	50% 19%	35.0% 34.7%	0.8%	20.5% 5.8%	2.2% 1.6%	100.0%		0.15	001	0.14	0.01	0.40	38.3% 51.2%	34% 27%	14.8%	0.6%	13.9%	1.4%	34.3% 51.2%
5.6		20	147						0.05	001	1.06	+	19%	34.7%	2.9%	585	1.6%	100.0%		0.15	0.01		0.01	0.43	53.2% 46.1%	2.7%	18.6%	0.7% 2.4%	43%	1.0%	53.2% 46.1%
55		24	152	10	0.1	1.10	1 00		0.63	607	2.98		43%	29.7%	0.8%	21.3%	2.3%	100.0%	008		002	0.47	0.04	1.12	38.1%	2.8%	18.5%	0.5%	15.0%	1.3%	38.1%
56 57		25	153	10	0.1				0.37	005	2.01	-	49%	42.6%	0.7%	12.4% 5.3%	1.7%	100.0%		064	0.01	0.29	0.03	1.34	44.4%	3.1% 1.7%	21.3%	0.5%	96%	10%	44.4%
58		27	155	10	0.1	1.25	5 0.0	14	0.06	0.04	2.50		5.4%	48.7%	1.7%	3.1%	1.7%	100.0%	0.10	0.73	0.03	0.06	0.03	1.82	70.0%	3.7%	28.4%	1.3%	2.1%	1.0%	70.8%
59		25	156		00		0.00	29	0.16	0.07	2.70	+=	22%	30.1%	2.7%	4.4% 30.6%	1.9%	100.0%	006			0.10	0.04	1.67	47.7% 17.5%	1.7%	14.4%	22%	2.9%	1.1%	47.7% 17.9%
61	I	35	163	10	0.0	1.20	0.0	12	0.12	0.02	2.70		19%	55.2%	0.9%	5.1%	1.0%	100.0%	007	0.76	0.02	0.07	0.02	151	65.3%	2.8%	32.7%	0.7%	2.9%	0.6%	65.3%
62		36	164	10					30.0	0.04	2.45	+	11%	54.5% 36.1%	0.7% 1.2%	24% 34%	1.6%	100.0%	0.12	0.79			0.02	1.73	70.3% 62.6%	47% 17%	32.1%	05% 1.1%	15%	0.9%	70.3% 62.6%
4.5	•		193	10	0.0	155	0.0	~	4.00	-04	2.84	-	41%	ps.17h	1,376	.45t	1,376	100/0%	-03	V30	V03	020	302	/8	44.6%	1.7%	19555	6.1%	43%	vd7h	44.6%

Table 4. PD of Ant K – patch antenna (28GHz – n261)

[Folder Open Status]

- K-patch Low CH

No. No.														T		max ratio ou	t of all beams			Г									max ratio out of all	Dearts		
Column C	\vdash		T	Т .	т —	Т			4cm2	2 PD(mW/o	m2)			12.9%	24.2%	4.6%	12.7%	9.2%	100.0%		iom2 PD(mi	N/cm2) a	rt 10mm evalu	ation distr	nce	61.6%	10.1%	18.2%	15%	9.5%	425	61.6%
Column C	No. In	Indula Turu	Saum ID 1	Same ID	2 East no	Н		Т	Ť		_	Т	per	ratio	ratio	min	ratio	ratio	min					T		ntio	ratio	ratio	retin	ratio	ratio	netio
1						54/86	pht) S3(Le	e) SS(S	opi Si	6(Bottom)	\$1(Front)	S2(Rea	Back-o		(Left 2mm)/(worst-	(Top 2mm)/(worst-	(Bottom 2mm)/(wont-	(Fornt 2mm)/(worst-	(Rear 2mm)/(wont-	S4(Right)	S3(Left)	SS(Top)	SS(Bottom)	S1(Front)	S2(Rear)	worst-surface	(Right 10mm)/(wont-	(Left 10mm)/(worst-	(Top 10mm)/(worst-	(Ecttom 10mm)/(wont	(Front 10mm)/(wond-	(Rear 10mm)/(worst- surface 2mm)
The column The	1	_	0	-	1	0.0	0.00	1 00	10	0.02	001	0.14	(40)							001	001	0.00	0.01	0.00	0.05							36.0%
The color of the	2				1			1 01				0.15	=	5.3%		1.3%	73%	4.0%	100.0%						0.07			46%	0.7%	6.0%	2.0%	43.7%
The column The	4		- 6		-	0.0	0.00	0.0	00	0.01	001	0.15		5.3%	8.6%	1.2%	33%	19%	100.0%	001	001	0.00	0.00	0.00	0.06	42.1%	46%	59%	0.7%	2.6%	2.0%	42.1%
The column The	6		10		2	0.0	0.00	2 02	00	0.03	0.01	0.12	+	7.4%	7.4%	1.2%	12.1%	2.2%	100.0%	001	001	0.00	0.02	0.00	0.05	17.2%	52%	5.2%	1.2%	9.5%	1.2%	17.2%
The color of the	7			_	2						601	0.35	-						100.0%						0.15							41.6% 41.8%
The color of the	9				2	0.0	0.00			0.02	001	0.22		5.1%	5.1%	1.8%	8.8%	4.1%				000	0.02		0.11	41.4%	3.7%	41%	1.4%	6.9%	1.8%	48.4% 37.0%
The column The	11		19		2	0.0	0.00	1 01	00	0.01	002	0.35		7.8%	7.5%	0.6%	35%	6.4%	100.0%			000	0.01	0.01	0.12	46.5%	46%	5.5%	0.6%	23%	29%	46.5%
The column The	12			+	5						002	0.24	+												0.11							45.4% 41.2%
The column The	14				5							0.77													0.34							41.9% 45.2%
The column The	16		27		Ś	0.0	7 0.00	5 02	00	0.02	006	0.02		8.2%	7.6%	0.5%	2.0%	6.7%	100.0%	0.04	005	0.00		0.03	0.42	50.8%	5.4%	5.5%	0.4%	1.3%	3.2%	50.8% 44.5%
The column The	10		34	+	5	0.0	2 0.00	1 01	10	0.05	001	0.52	+	2.4%	4.5%	0.7%	8.1%	2.1%	100.0%	0.02	0.02	0.00	0.03	0.01	0.25	43.2%	2.6%	2.4%	0.5%	62%	1.2%	41.2%
The column The	19			+	5						0.04	0.79	+	12.0%		0.5%	19%	9.2%	100,0%				0.01		0.35	45.9%	8.7%	8.7%	0.4%	1.1%	40%	44.4% 46.9%
The column The	21											0.74													0.39							52.0% 41.7%
The column The	23		130		- 1	0.0	0.00	0.0	00	0.02	0.00			1.1%	0.8%	0.8%	42%	0.8%	100.0%	000	000	0.00	0.01	0.00	0.15	42.1%	0.8%	96%	0.6%	31%	0.2%	42.1%
The column The	25		134	+	1	0.0	0.00	0.0	10	0.01	000	0.35	+	1.1%	1.1%	1.7%	29%	0.8%	100.0%	000	000	0.00	0.01		0.16	42.0%	0.8%	0.8%	0.8%	1.8%	0.3%	41.8% 42.0%
The column The	26			_	1 2				10		000	0.20	-								000		0.01		0.00							29.0% 49.6%
The column The	28											0.78				0.1%	33%	0.4%	100.0%						0.41	52.3%	0.9%	06%		24%	0.3%	52.3% 41.6%
The column The	30		141		2	0.0	0.00	0.0	01	0.04	001	0.74		1.4%	2.5%	2.1%	9.1%	1.6%	100.0%	000	001	0.00	0.03	0.00	0.20	40.7%	0.8%	1.4%	14%	6.0%	06%	40.7%
The column The	31	K Pand		+								0.64	+												0.30							47.5% 50.4%
The column The	33		146		2						001	0.80						0.9%			001				0.38							47.8% 50.2%
The column The	35		153		- 3						0.01	1.76	=	2.3%		0.5%	35%	0.4%	100.0%						0.96	54.6%	1.6%	1.4%	0.3%	2.0%	0.2%	54.6% 57.4%
2	37		155			0.0	5 0.00	5 02	12	0.01		2.05		2.7%	2.5%	0.8%	0.7%	0.9%	100.0%	0.04	003	000	0.01	0.01	1.07	61.4%	1.7%	1.6%	0.6%	0.5%	0.5%	61.4%
2	38		156	-	5						003	1.94	+												0.92							47.4% 51.2%
Z	40				5			1 01	00	0.02	601	1.00	-								003	0.00			1.03							56.9% 59.6%
Z	42		165		ŝ	0.0	5 0.00	7 01	34	0.02	002	2.07		2.7%	12%	1.9%	0.9%	1.2%	100.0%	0.04		0.03	0.01	0.02	1.14	55.4%	1.7%	2.0%	1.4%	0.6%	0.7%	55.4%
Z	43				2						001	0.44	+												0.19							44.4% 43.6%
Z	45				2						601	0.52	Е												0.22							41.6% 41.2%
2	47											0.36	=			1.1%	42%	1.9%	100.0%						0.15	41.9%	3.3%	2.5%	22%	31%	0.8%	41.9% 45.5%
Z	49		11	122	4	0.0	5 0.00				002	1.09		47%	43%	0.4%	3.6%	12%	100.0%	0.04	003			0.01	0.57	52.7%	33%	10%	0.3%	2.5%	0.6%	52.7%
Z	50		12	141	4			1 01	12		602 602	0.07	ŧΞ	2.9%	3.8%	2.8%	12.9%	21%	100.0%			0.01	0.01		0.48	44.2%	21%	2.6%	21%	72%	0.9%	45.2% 44.2%
Z	52											1.06	-												0.47							44.4% 54.1%
22 23 15 15 15 15 15 15 15 1	54					0.0	5 0.00			0.10		0.96		5.2%		2.2%	9.9%	15%	100.0%						0.49	\$1.0%	3.3%	1.7%	1.7%	6.8%	1.9%	\$1.0%
20 28 154 159 159 150	55		24 25			0.1	0.00			0.12		2.50		50%		0.5%	4.0%	1.5%				0.00	0.15	0.01	1.33	58.7%	4.0%	2.7%	0.3%	10%	0.8%	51.4% 58.7%
20 28 154 159 159 150	57		26 27						9	0.05		2.02	-								019				1.49				0.4%	1.1%	1.5%	52.9% 61.6%
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	59			156	10	0.1	0.00	0.1	14	0.10	005	2.98	1	13%	3.0%	46%	35%	1.6%	100.0%	0.06		0.10	0.06	0.03	1.34	45.0%	1.9%	19%	35%	2.1%	1.0%	45.0%
62 M 164 10 0.20 0.18 0.02 0.05 0.16 1.05 65% 5.8% 0.5% 1.8% 5.2% 100.0% 0.15 0.13 0.07 1.10 53.0% 4.7% 4.2% 0.3% 1.1% 2.2% 56.	61			163	10	0.1	0.13	5 01	12	0.05		2.60		5.7%	5.5%	0.7%	19%	2.0%	100.0%	012	0.11	0.00	0.03	0.03	1.41	51.7%	44%	40%	0.5%	12%	1.1%	55.6% 51.7%
63 37 MS 10 0.06 0.02 0.06 0.05 0.07 1.30 4.8% 1.6% 1.7% 1.6% 2.0% 100.0% 0.09 0.08 0.04 0.04 0.03 1.87 56.8% 2.7% 2.5% 1.2% 0.9% 56	63		32								016	1.05	F	65% 48%			1.6%								1.00					1.1% 1.2%		51.9% 54.8%

- K-patch Mid CH

															max ratio ou	t of all beams													max ratio out of all I	beares		
П							-	4cm2 PD(n	nW/on2)				10.5%	12.4%	4.0%	12.7%	6.1%	100.0%	4	om2 PD(ml	W/cm2) a	t 10mm ev	valuation	distance		61.5%	7.6%	9.9%	2.8%	8.9%	2.0%	61.5%
No. M	odule Type	Beam II	d Sema ID.	Feed no.						Т	\neg	per leam	ratio	ratio	ratio	ratio	ratio	ratio								ratio	ratio	ntio	ratio	ratio	ratio	ratio
					54/Right	(f) \$3(Left)	SS(Top)	SE(Both	(mo	tont) S2	(Rear) D.	ck-off	(Right 2mm(/(wonst- surface 2mm)	(Left 2mm)/(wonst- surface 2mm)	(Top 2mm)/(worst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	S4(Right)	S3(Left)	SS(Tap)	SS/Botto	om) \$1(i	ront) S2/R		est-surface mm/2mm)	(Right 10mm)/(worst- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Bottom 10mm(//worst- surface 2mm)	(Front 10mm)/(worst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
1		0		1	0.00		0.00				.17	(30)	52%	5.8%	0.0%	11.6%	2.9%	100.0%	001		0.00			00 01		45.1%	2.9%	40%	0.6%	75%	12%	45.1%
3		4		1	000		0.00	0.01		30 6	1.19	_	54% 55%	5.4% 4.9%	1.1%	7.6%	2.2% 1.8%	1000%	001 001	001	0.00	0.01		00 01		41.1%	38% 43%	18% 17%	0.5% 1.2%	5.4% 5.5%	1.1%	41.1% 43.9%
4		- 6	_	1	0.00	0.00	0.00	0.01	- 0	31 6	1.21		49% 78%	4.9% 5.2%	0.5%	34% 60%	24%	1000%	001	001	0.00	0.01		00 01		43.9% 42.2%	14%	3.4% 4.2%	05%	29% 14%	10%	419% 42.2%
6		10		2	0.00	0.01	0.00	0.03			1.35		14%	3.7%	1.1%	92%	1.4%	1000%	001	001	0.00	0.00		.00 0.1	15	42.5%	2.6%	2.9%	1.1%	75%	09%	42.5%
7 8		11	_	2 2	0.03	0.02	0.00	0.02		31 (1.29	\rightarrow	5.7% 7.0%	5.0%	0.2%	41% 28%	2.5%	100.0%	002	002	0.00	0.02		00 03		45.7% 42.0%	43% 52%	16%	02%	34% 21%	09% 15%	45.7% 42.0%
9		13		2	0.00	0.00	0.00	0.02		31 6	1.21		42%	45% 7.3%	1.9%	61%	2.6%	1000%	001	001	0.00	0.01	. 0			49.5% 41.6%	29%	12% 49%	1.6%	45% 57%	12%	49.5% 41.6%
11		19		2	0.02		0.00	0.02	- 0	22 (1.29		6.1%	5.6%	0.8%	43%	3.0%	100.0%	002	002	0.00	0.01	0	.01 0.2	20	50.3%	3.8%	4.1%	0.5%	25%	1.8%	50.3%
12		20	+	5	0.02		0.00	0.04		21 6	1.02	_	10%	15% 11%	1.3%	13.7% 7.8%	1.5% 1.4%	100.0%	001		0.00	0.03		.01 0.1		41.6% 50.5%	15% 23%	2.5%	1.0%	8.9% 5.0%	1.6%	41.6% 50.5%
14		25 26		5	0.06		0.01	0.04		33 (1.95		65% 98%	8.0% 8.2%	0.8%	435 135	2.6% 1.9%	100.0%	004	006	0.00	0.02		01 0		45.2% 52.3%	40%	5.9%	05%	23%	14%	48.2% 52.3%
16		27		5	0.06		0.00	0.03			1.94		6.4%	6.2%	0.4%	33%	42%	100.0%	004		0.00	0.02		02 0/	49	\$1.9%	43%	42%	0.4%	2.4%	21%	51.9%
2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18		28 34		5	0.03	0.01	0.01	0.06	0	21 6	1.64	-	49% 11%	1.7%	2.4% 0.7%	13.9% 7.4%	1.9%	1000%	002	001	0.00	0.04		.01 0.2	42	42.8% 50.2%	2.6% 2.3%	1.0%	1.9%	7.1% 4.6%	1.0%	42.8% 50.2%
19		35 36	_	5	0.10		0.00	0.02	- 0	34 6	1.97		10.5%	13.1%	0.3%	22%	1.0% 6.1%	100.0%	007	0.09	0.00	0.01		02 0		50.3% 50.5%	6.9% 7.6%	94%	02%	1.1%	2.0%	50.3% 50.5%
21		37		5	0.06	0.04	0.01	0.04	- 0	32 (.87		6.4%	4.0%	0.6%	43%	2.0%	100.0%	003	0.02	0.00	0.03		.01 0.4	45	\$1.6%	15%	2.8%	0.5%	10%	13%	51.6%
22		128		1	0.00		0.00	0.01	01	30 6	1.29	\rightarrow	14%	14%	1.0%	31% 22%	0.7% 0.5%	1000%	000	000	0.00	0.01		.00 0.1		41.0%	1.0%	1.0%	0.7% 1.1%	24% 14%	0.3%	41.0% 29.6%
24		132		1	000		0.01	0.01		00 6	1.36		14%	0.8%	14%	28%	0.6%	1000%	000	000	0.00	0.01		00 0.1		41.1% 39.7%	0.8%	06%	0.8%	1.7%	0.3%	41.1% 33.7%
26		136		i	0.00		0.00	0.01	01	30	.20		1.5%	3.0%	2.5%	45%	1.0%	100.0%	000	000		0.01	-	.00 0.1	00	40.1%	1.0%	2.0%	15%	35%	05%	40.1%
27		135		2 2	000	0.01	0.01	0.03	0		1.57		2.1% 1.7%	1.4%	2.1%	54% 29%	1.2%	100.0%	001	001	0.00	0.02	. 0			41.9% 51.9%	1.8%	1.1%	14%	35% 20%	07%	41.9% 51.9%
29		140		2 2	000	0.00	0.01	0.00	0		1.77		1.6%	1.7%	1.2%	05% 32%	0.6%	100.0%	001	001 001	0.01	0.00		00 0		45.5% 38.9%	1.0%	1.0%	0.9% 2.1%	0.3% 2.1%	0.4%	45.5% 38.9%
31		146		2	0.00	0.00	0.01	0.03	0	31 (1.65		19%	1.1%	1.2%	53%	1.1%	100.0%	001	0.01	0.01	0.02		.00 0.3	30	45.9%	1.5%	0.9%	0.9%	16%	05%	46.9%
32	K Pasch	147	_	2 2	0.02		0.00	0.01		20 0	1.90	\rightarrow	17%	0.8%	0.3%	0.7% 2.5%	0.3%	100.0%	001		0.00	0.00		00 0		52.4% 44.5%	1.1%	05%	02% 15%	0.4% 1.6%	0.2%	52.4% 44.5%
34		152 153		5	0.04		0.01		- 0	21	.67		22%	1.8%	0.5%	92% 32%	0.8%	100.0%	003	002 002	0.01	0.10		01 01		41.2% 51.0%	1.7%	10%	0.3%	61% 19%	05%	48.2% 51.0%
26		154		5	0.06	0.03	0.01	0.02	- 0	21 1	.92		13%	1.6%	0.3%	0.8%	0.4%	100.0%	005	0.02	0.00	0.01	0	.00 14	07	55.7%	2.4%	12%	0.2%	0.5%	0.2%	55.7%
37		155 156		5	0.06		0.01	0.01		32 3	1.05	_	27%	1.9%	2.0%	0.6%	1.7%	1000%	004	003	0.01	0.01		.01 1.2 .02 0.1		59.3% 46.2%	1.9% 1.2%	1.4% 2.7%	0.5% 2.8%	0.5% 0.5%	05% 09%	59.3% 46.2%
39		162		5	0.03	0.03	0.00	0.12	- 0	21	1.72		20%	1.5%	0.2%	62%	0.6%	100.0%	003	002	0.00	0.06		01 01		50.7% 56.2%	1.6% 2.5%	12%	02%	44%	0.3% 0.2%	50.7% 56.2%
41		164		5	0.06	0.04	0.00	0.01	0		.92		31%	1.8%	0.2%	0.4%	0.7%	100.0%	005	0.03	0.00	0.01	0	.01 1.1	12	58.0%	2.4%	1.4%	0.2%	0.3%	0.4%	58.0%
43		165		5 2	0.06		0.04	0.01	01		1.16	_	27% 16%	2.8% 3.2%	1.9%	0.5% 7.6%	1.0%	100.0%	004		0.03	0.01			21	55.7% 42.4%	1.7% 2.2%	19%	14%	0.4% 5.0%	0.6%	55.7% 42.4%
44		2	130	2	0.02		0.01	0.03	- 0	21 (1.50		27%	2.1%	1.5%	53% 48%	15% 12%	100.0%	001 001	001	0.01	0.02		01 03		42.4% 41.2%	1.9%	1.5%	1.0%	18% 12%	09% 07%	42.4% 41.2%
46		- 6	134	2	0.02		0.01	0.02	- 0	21 6	1.60		10%	2.0%	1.3%	32%	1.7%	100.0%	001	001	0.00	0.01	0	00 02	20	45.1%	23%	15%	1.0%	2.3%	0.7%	46.1%
40		10	136	4	0.02	0.01	0.01	0.02	- 0	32 1	1.06	-	5.0% 2.7%	2.9%	1.2% 2.1%	4.4% 6.7%	2.6%	100.0%	001	001	0.01	0.01		.00 0.1		50.3% 51.0%	15% 23%	2.1%	24%	15% 47%	12%	50.3% 51.0%
49		11		4	0.05		0.00	0.04	- 0		1.17		19%	10%	0.3%	34% 12%	15%	100.0%	004	603	0.00	0.03		01 01		55.1% 45.6%	11%	22%	02% 13%	2.6% 1.0%	0.7% 1.0%	56.1% 45.6%
51		13	141	4	0.03	0.04	0.03	0.05		32	.02		10%	4.0%	2.7%	49%	1.0%	100.0%	002	0.02	0.02	0.04		.01 0.4	47	45.4%	22%	2.3%	2.0%	3.7%	0.8%	45.4%
53		18	146	4	0.04	0.03	0.01	0.09	0		.11	-	12% 43%	2.8%	1.0%	83% 20%	1.9%	100.0%	003	0.02	0.01	0.07		.01 0.1	69	43.9% 57.1%	2.3% 2.7%	1.9%	0.6% 203.0	61% 13%	1.0%	41.9% 57.1%
22 22 23 38 38 39 39 30 30 30 30 30 30 30 40 40 40 40 40 40 40 40 40 40 40 40 40		20	148	4 10	0.05		0.03	0.09		32	1.01	=	54%	2.5%	2.5%	9.1% 8.7%	24%	100.0%	003	0.02	0.02	0.06		01 01	S1 S7	50.2% 54.5%	12% 26%	16%	1.7%	63%	12%	50.2% 54.9%
56		25	153		0.13	0.09	0.03	0.11	0	25	.02		46%	3.3%	02%	3.0%	1.7%	100.0%	0.09	007	0.02	0.12		03 14	68	59.6%	32%	2.4%	0.6%	24%	09%	59.6%
57		25	154 155	10	0.20		0.00	0.03		10	1.08	-	6.3% 4.0%	4.5%	05%	1.1%	23%	100.0%	014	010	0.01	0.02		03 11		\$3.2% \$1.5%	46% 14%	13%	0.3%	1.0%	14%	53.2% 61.5%
59		28 34	156	10	0.12		0.13	0.12		36	.22		17%	4.9%	40%	38% 75%	1.0%	100.0%	007	0.09	0.09	0.06		01 1		48.7%	22% 25%	28%	28%	25% 44%	1.0%	48.7% 56.6%
61		35	163	10	0.14	0.16	0.01	0.05	- 0	25	.00		5.0%	5.4%	0.4%	1.8%	1.7%	100.0%	0.11	0.11	0.01	0.03		03 14	65	57.2%	19%	40%	0.2%	1.0%	0.9%	57.2%
63		32	164	10	0.22		0.01	0.03	0	13 27	1.21	\dashv	%02 %02	5.9% 3.3%	0.4%	1.0%	19%	100.0%	017		0.01	0.02		06 11		59.2% 58.1%	5.2% 2.7%	42% 22%	1.1%	1.0%	1.8%	59.2% 58.1%

- K-patch High CH

_													1			t of all beams			_										max ratio out of all I			
\vdash		_	_	_	_				PD/mW/c	_									Η.	Nom2 PD/n					-							
					┝			4cmz	V LIJTINO C	2002)		- ner	12.0%	12.5%	2.8%	11.4%	6.5%	100.0%	_	NOTE PLUT	IW(CILZ)	at sames	evanuation	n distance	•	62.5%	9.9%	9.2%	2.8%	9.0%	2.9%	62.5%
No. I	Module Type	e Beam ID,	1 Berra ID,2	Feed no.	54 Right	Salver	55/50	e 56	Sottom)	\$1/Fronti	Chillenn	Bean	ratio (Right 2mm)//worst-	ratio (Left 2mm\/\womt-	ratio (Top 2mm)//wont-	ratio (Sottom 2mmi//wont-	ratio (Fornt 2mm)//worst-	ratio (Rear 2mm)/(wont-	CATUM	Salver	SS/Ton	SS/Bott	tom) St	(Front)	S2/Rear)	ratio worst-surface	ratio (Right 10mm)/(wont-	ratio (Left 10mm)/(wonst-	ratio (Top 10mm)/(worst-	ratio (Sottom 10mm)//wont	ratio (Front 10mm)//wont-	ratio (Rear 10mm)//wont-
							33,13	-				Back-o	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)				-		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	-,,	(10mm/2mm)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)
1 2		0	_	1	0.00	0.00	0.00		0.02	000	0.19	-	12% 67%	3.8% 5.5%	0.5%	10.2% 6.1%	2.2% 1.8%	100.0%	000	0.01	0.00	0.00	0 1	200	0.00	45.2% 25.2%	22% 42%	27% 16%	0.5%	45% 42%	1.1%	45.2% 35.2%
3 4		4		1	0.00	0.00	0.00		0.01	000	0.18		6.0%	43%	1.6%	7.1%	2.2%	100.0%	001	001	0.00	0.01		200	0.07	38.0%	43%	3.3%	1.1%	49%	1.1%	38.0%
5		-	+	1	0.01	0.01	0.00		000	001	0.10	+	6.1% 12.2%	3.6% 11.2%	1.0%	46%	16% 61%	100.0%	001		0.00	0.00	0 1	200	0.09	45.4%	41% 92%	2.6% 7.1%	10%	41%	15%	45.4% 44.9%
5 6 7		10		2	0.00	0.00	0.00		0.04	0.00	0.35		15%	3.8% 4.9%	1.7%	11.0%	1.2% 1.2%	100.0%	0.01	0.01	0.01	0.00		0.00	0.15	41.9% 46.5%	23%	2.6%	14%	9.0%	06%	41.9% ac oc.
8		12		2	0.03		0.00	_	0.01	0.02	0.35		94%	6.0%	0.9%	2.6%	54%	100.0%	003	0.02	0.00	0.01	0 1	0.01	0.15	42.0%	7.4%	48%	0.6%	2.0%	2.6%	42.0%
9		13	+	2	0.01	0.01	0.00	+	0.03	001	0.32	+	44% 52%	4.4% 6.8%	2.5% 0.5%	85% 79%	22% 2.7%	1000%	001	0.01	0.00	0.00	2 1	200	0.16	46.7% 44.3%	12%	32% 49%	1.9%	5.4%	1.1%	46.7% 44.2%
11		19 20		2	0.02	0.02	0.00		9 9	001	0.39		52% 17%	425 435	0.8%	3.4% 11.4%	2.6% 2.5%	100.0%	001	001	0.00	0.00		0.01	0.17	44.9% 37.2%	14% 22%	29%	0.5%	2.1% 7.7%	13%	44.9% 37.2%
13		24		5	0.02	0.06	0.01		0.07	002	0.90		2.5%	6.4%	0.9%	7.6%	1.9%	100.0%	002	004	0.00	0.00	5 1	0.01	0.43	47.8%	2.0%	45%	0.7%	5.1%	1.0%	47.8%
13 14 15 16 17 18		25	_	5	0.06	0.09	0.01		300	003	1.03	+	6.4% 10.4%	9.2%	0.7%	64% 1.6%	2.8% 5.7%	100.0%	004	0.06	0.00	0.04		0.01	0.43	46.0%	40% 7.7%	6.2% 5.0%	0.5%	37%	1.3%	44.4% 48.0%
16		27 28		5	0.06	0.08	0.01		0.02	003	0.92		60% 42%	9.1% 2.0%	07% 3.1%	2.6% 9.1%	14%	100.0%	0.04	006	0.00	0.00		0.02	0.45	49.6%	43%	62% 15%	05%	1.7%	19%	49.6% 45.4%
18		34		ŝ	0.02	0.06	0.01		0.07	0.02	0.92		2.6%	6.0%	0.9%	72%	2.0%	100.0%	002	004	0.01	0.04	4	0.01	0.43	45.9%	2.0%	47%	0.7%	47%	1.1%	45.9%
19		35	+	5	0.12	0.10	0.00	-	0.02	0.05	0.92	+	13.0%	11.0%	0.3%	2.0%	5.0% 6.5%	100.0%	0.03	0.07	0.00	0.01		0.02	0.43	46.7%	83% 99%	80% 92%	0.2%	1.1%	2.2%	46.7% 47.3%
20 21 22 23 24 25 26 27 28 29		37 128		5	0.04	0.04	0.01		0.02	0.02	0.05		42% 1.2%	4.7% 1.0%	0.0%	2.1% 2.9%	2.6%	100.0%	002	003	0.00	0.00		0.01	0.44	\$1.8% #5.1%	25%	11%	0.5%	1.6%	1.4%	51.8% 45.1%
23		130		1	0.00	0.00	0.00		0.01	0.00	0.31		1.3%	1.3%	1.1%	22%	0.5%	100.0%	000	0.00	0.00	0.00	0 1	0.00	0.16	29.0%	1.1%	0.8%	0.8%	13%	0.3%	29.0%
24		132	+	1	0.00	0.00	0.00	-	0.01	000	0.36	+	14%	1.1%	1.1%	25% 21%	0.6% 0.5%	100.0%	000	000	0.00	0.01		000	0.15	40.7%	1.1%	06% 08%	0.8%	1.7%	0.3% 0.3%	40.7% 29.7%
26		136		1 2	0.00	0.00	0.01		0.01	000	0.20		20%	1.0%	2.5% 1.7%	40% 53%	1.0%	100.0%	000	000	0.00	0.00		0.00	0.07	34.7% 46.9%	15%	15%	15%	15% 16%	05% 07%	34.7%
28		139	_	2	0.01	0.01	0.00	,	0.02	0.00	0.78	+	1.0%	0.8%	0.1%	10%	0.1%	100.0%	001	0.01	0.00	0.00	2 1	0.00	0.42	51.9%	13%	06%	0.0%	1.9%	0.1%	51.9%
29 30		140		2	0.00	0.00	0.01		300	601	0.78	-	15%	1.4%	1.0%	0.8% 3.2%	0.6%	100.0%	001	001	0.00	0.00		000	0.37	47.8% 42.8%	13%	09% 16%	0.8%	05%	0.4%	47.8% 42.8%
31		146 h 147	1	2	0.00	0.00	0.01		0.03	001	0.63		22%	0.9%	1.1%	44%	0.9%	100.0%	001	0.01	0.00	0.00		0.00	0.29	45.5%	17%	0.8%	0.8%	33%	0.5%	45.5%
33	K Pass	140	+	2	0.02	0.01	0.00		0.02	000	0.90	+	1.8%	0.7%	1.5%	24%	0.8%	100.0%	001	001	0.00	0.00	0 1	0.00	0.46	50.7% 43.5%	12%	12%	12%	1.5%	0.2%	50.7% 41.5%
34		152	_	5	0.04	0.02	0.01		0.14	601	1.66		24%	14%	0.5%	84%	0.8%	100.0%	003	0.02	0.00	0.00		0.01	0.81	41.9%	2.0%	1.1%	0.4%	57%	0.4%	45.9%
26		154		Ś	0.07	0.03	0.01	Н	0.01	001	1.95		15%	1.5%	0.3%	0.6%	0.6%	100.0%	0.05	0.02	0.00	0.00	1	0.01	1.00	55.5%	2.6%	1.2%	0.2%	0.4%	0.3%	55.5%
32 33 34 35 36 37 38		155		5	0.06	0.04	0.01		0.02	0.02	1.09	+	10%	2.0%	16%	0.5%	1.0%	100.0%	004		0.01	0.01		0.01	0.87	57.4% 45.9%	1.9%	14%	0.4% 2.5%	0.4%	05% 1,0%	57.4% 45.9%
39		162		5	0.04				0.11	601	1.74		2.1% 1.7%	1.6%	0.3%	61%	0.6%	100.0%	003		0.00			0.01	0.89	50.9% 55.9%	18%	13%	0.2%	38%	0.3% 0.2%	53.9% 55.9%
40 41 42		164		ś	0.06	0.03	0.01		0.01	0.02	1.91		13%	1.0%	0.3%	0.5%	0.8%	100.0%	0.05	003	0.00	0.01	9 1	0.01	1.10	57.4%	2.6%	1.4%	0.2%	0.4%	0.4%	57.4%
42		165	128	2	0.00	0.07	0.04	-	0.02	002	0.52	+	3.8% 2.9%	3.6%	2.0%	0.7% 5.8%	1.2% 1.3%	100.0%	005	0.04	0.03	0.00		0.02	0.22	55.2% 43.4%	24% 1.9%	21%	15%	05% 19%	0.7% 0.6%	55.2% 41.4%
43 44 45 46 47 48 49		2	130	2	0.02	0.01	0.01		0.03	601	0.60	F	29% 10%	2.2% 2.5%	1.2%	44% 15%	15%	100.0%	001	001	0.01	0.00		0.01	0.24	29.0%	18%	15%	0.8%	32% 26%	08%	22.0% 23.0%
46		- 6	134	2	0.02	0.00	0.01		0.02	001	0.62		2.9%	1.8%	1.3%	32%	1.9%	100.0%	001	0.01	0.01	0.00	2 1	0.01	0.29	45.4%	21%	1.3%	1.0%	2.6%	0.8%	46.4%
40		10	136	4	0.02	0.01	0.01	-	0.01	001	1.11	+	5.9% 2.8%	3.8% 2.3%	2.0%	64% 62%	13%	100.0%	001	001	0.00	0.01	6 1	0.01	0.15	45.9% 50.4%	44% 24%	2.8%	28%	14% 50%	16%	45.9% 50.4%
49		11	139	4	0.05	0.03	0.01		0.05	002	1.23	_	19%	2.2%	0.4%	17%	1.8%	100.0%	0.04	002		0.00		0.01	0.66	53.9% 44.2%	31% 10%	16%	0.3%	24%	0.7%	51.9% 44.2%
51		13	141	- 4	0.04	0.04	0.03		0.05	0.02	1.07		2.4%	3.3%	2.4%	44%	1.4%	100.0%	0.02	0.02	0.02	0.04	4 1	0.01	0.49	45.4%	22%	2.0%	12%	33%	0.7%	45.4%
52		18	146	4	0.03	0.03	0.01	F	800	002	1.10	ΗΞ	11% 12%	2.6%	1.0%	7.4%	21%	100.0%	003	002	0.01	0.00		0.01	0.67	42.5% 56.2%	26%	1.0%	0.7%	54%	10%	42.5% 56.2%
53 54 55 56 57		20	148	4	0.05	0.03	0.02		0.09	0.02	1.03		44%	2.6%	2.2%	84%	22%	100.0%	003	0.02	0.02	0.00		0.01	0.50	48.6% 54.9%	2.7%	17%	1.5%	5.7%	12%	48.6%
56		24 25	153	10	0.08		0.03		0.26	004	2.92		27% 46%	1.0%	0.9%	9.0% 3.6%	12% 15%	100.0%	0.11	007	0.02	0.11	6 1	0.02	1.69	57.9%	24% 16%	2.1%	0.6%	5.7% 2.1%	06% 07%	54.9% 57.9%
57		2£	154 155	10	0.21	0.13	0.01	F	0.03	0.11	3.12	F	43%	425	0.4%	1.0%	16% 24%	100.0%	0.16	0.09	0.00	0.00		0.05	1.65	52.9% 62.5%	51% 24%	10%	0.3%	0.7%	15%	52.9% 62.5%
58 59		28	156	10	0.10		0.12		0.11	0.06	2.31		10%	42%	15%	3.4%	1.8%	100.0%	0.06	0.08	0.08	0.00	6	203	1.63	49.2%	1.9%	25%	24%	23%	1.0%	49.2%
61		34	163	10	0.09	0.12	0.02		90 PD	003	2.83		2.9% 6.3%	12% 43%	0.7%	7.5% 1.3%	1.1% 2.1%	100.0%	0.14			0.15	2 1	0.02	1.59	56.9% 56.4%	2.4% 4.9%	2.3% 3.2%	0.5%	48%	06%	56.9% 56.4%
63		36			0.27				0.03	013		-	8.7% 5.1%	5.4% 19%	0.4% 1.2%	0.8%	42% 20%	100.0%	0.19	012	0.01			206	1.01	52.1% 60.0%	62% 10%	19%	03%	0.6%	19%	59.1% 60.0%
6.0					0.19	9.13	0.04		_03	100	4.12	-	2170	250	147	1375	200	TAKE OF THE PARTY	4.11	200	well	Ja	- 1			W.U.R	202	47.0	0.5%	470	10%	won

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- K-patch Low CH

														max ratio ou	t of all beams											max ratio out of all I	bearts		
П							4	cm2 PD(mW	(on2)			11.0%	47.2%	428	14.2%	CIN	100.0%	4cm2 PD(ml	W/cm2)	at 10mm evalu	uation dista	nce	61.6%	7.0%	29.1%	2.1%	10.2%	2.4%	61.6%
No. I	fodule Typ	e Beam ID_1	Sema ID,	2 Feed no.							per Seam	ratio	ratio	ratio	ratio	ratio	ntio						ratio	ratio	ratio	ratio	ratio	ratio	ratio
					S4(Right)	S3(Left)	SS(Top)	S6(Bottom	\$1(Fron	t) S2(Rea	Back-of	(Right 2mm)/(wont- surface 2mm)	(Left 2mm)/(wonst- surface 2mm)	(Top 2mm)/(worst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	S4(Right) S3(Left)	SS(Top)	SS(Bottom)	\$1(Front)	S2(Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(worst- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Bottom 10mm)/(worst surface 2mm)	(Front 10mm)/(wont- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
1		0		- 1	0.00	0.05	0.00		000		((31)	41%	34.0%	0.7%	14.2%	2.0%	100.0%	000 003			0.00	0.06	29.5%	2.7%	17.7%	0.7%	10.2%	1.4%	29.5%
2		2		1	0.00	0.04	0.00	0.01	600			44%	25.3% 30.5%	0.0%	70% 92%	1.9%	100.0%	001 002			0.00	0.00	47.5% 45.8%	32% 46%	14.6%	0.6%	51% 61%	13%	47.5% 45.8%
4		- 6	_	1				0.01			+	40%	28.7%	2.0%	13%	2.7%	100.0%	000 002			0.00	0.07	48.7%	2.7%	16.0%	13%	2.7%	13%	48.7%
5		10		1	0.00	0.04		0.00	000	0.12		67% 62%	36.7% 22.1%	2.5%	3.3% 11.9%	1.7% 2.2%	100.0%	001 002	0.00		0.00	0.05	41.7% 40.3%	50%	20.0%	17% 22%	2.5% 9.3%	0.8% 1.3%	41.7% 40.2%
7		- 11	_	2	0.03	0.13			001	0.35	+	7.1%	35.5%	0.6%	40%	3.7%	100.0%	002 007		0.01	0.01	0.17	49.1%	45%	19.6%	0.6%	11%	2.0%	49.1%
8		12	-	2	0.02	0.12	0.00	0.01	001	0.32	+-	62% 57%	37.8% 24.1%	2.6%	19%	11%	100.0%	002 007			0.01	0.16	49.5%	46%	22.3% 12.7%	0.6%	1.2%	15%	49.5%
10		10		2	0.02	0.11	0.00	0.03	001	0.22		46%	34.5%	0.9%	95%	1.8%	100.0%	001 006	0.00	0.02	0.00	0.12	40.5%	10%	10.6%	0.6%	7.0%	03%	40.5%
11		19	-	2	0.02	0.11	0.00	0.01	0.01	0.36	+-	5.0% 6.3%	31.7% 20.6%	0.8% 1.2%	3.6% 14.2%	2.2%	100.0%	001 007	0.00		0.01	0.19	51.7% 47.2%	15%	18.1%	12%	2.5% 9.5%	1.4%	51.7% 47.2%
13		24		ŝ	0.02	0.16	0.01	0.05	001	0.56		4.1%	27.9%	1.4%	84%	1.1%	100.0%	002 009	0.00	0.04	0.00	0.25	44.2%	3.4%	16.6%	0.9%	6.6%	0.7%	44.2%
14		25 26	+	5	0.05		0.00	0.03	0.02		+-	6.5% 10.6%	35.9% 47.2%	0.5%	40% 25%	21%	100.0% 100.0%	003 019	0.00		0.01	0.38	46.5% 57.2%	3.8% 6.9%	23.2% 27.8%	0.2%	2.8%	11%	46.5% 57.2%
16		27		Š	0.05	0.27	0.01	0.02	002	0.06		53%	31.0%	0.6%	22%	2.0%	100.0%	003 016	0.00	0.01	0.01	0.46	52.9%	3.4%	20.4%	0.6%	1.4%	12%	52.9%
4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20		28 34	1	5	0.05	0.08		0.05	001	0.52	+	8.9% 4.0%	15.4% 29.1%	2.7%	92%	1.0%	100.0%	003 004	0.00	0.03	0.00	0.24	46.6% 44.2%	54% 33%	7.3%	2.1% 0.7%	5.6% 5.9%	0.6% 0.7%	46.6% 44.2%
19		35		5	0.09			0.02	004	0.02		11.0%	45.7%	0.7%	23%	4.6%	100.0%	0.06 0.22			0.02	0.42	52.6%	7.0%	27.3%	0.4%	1.6%	2.4%	52.6%
20		36	1	5	0.07	0.29	0.01	0.01	003	0.85	+-	80% 7.7%	31.6% 22.2%	0.7%	14%	17%	100.0%	004 018	0.00		0.02	0.45	53.0%	49%	21.4%	05%	0.9% 2.2%	21% 08%	51.0% 52.9%
21 22 23 24 25 26 27 28		128		1	0.00	0.07	0.00	0.01	000	0.20		1.1%	23.6%	0.7%	4.6%	0.7%	100.0%	000 003	0.00		0.00	0.12	40.0%	0.7%	10.6%	0.7%	12%	0.4%	42.0%
23		130	+	1	0.00	0.09	0.00		000	0.36	+	11%	25.5% 24.7%	1.1%	425 455	0.8%	100.0%	000 004			0.00	0.15	41.7%	0.9%	11.2%	0.8%	16%	06%	41.7% 41.8%
25		134		1	0.00	0.10	0.01	0.01	000	0.30		1.1%	25.1%	1.3%	29%	0.5%	100.0%	000 005	0.00	0.01	0.00	0.16	41.2%	0.8%	12.4%	0.8%	21%	0.3%	41.2%
26		136	+	2	0.00	0.04	0.00	0.01	000	0.56	+-	2.0%	19.9%	2.0%	5.1% 11.1%	1.0%	100.0%	000 002	0.00		0.00	0.00	38.8% 48.7%	1.5%	92%	1.0%	3.1% 8.4%	05%	38.8% 48.7%
28		139		2	0.00	0.25	0.00	0.02	000	0.70		1.4%	32.3%	0.0%	3.1%	0.4%	100.0%	001 012	0.00	0.02	0.00	0.40	52.1% #1.7%	1.0%	15.5%	0.0%	22%	0.3%	52.1%
30		140	1	2	0.00	0.14	0.01	0.01	001	0.74	+	1.4%	32.0% 27.9%	1.1% 2.6%	15% 93%	0.7%	100.0%	000 007	0.01	0.01	0.00	0.36	40.1%	1.0%	14.7%	0.8%	1.0%	0.4%	48.3% 40.1%
31		146 ch 147		2	0.00	0.79	0.01	0.04	601	0.63		16%	29.2% 30.8%	1.1%	6.6%	1.1%	100.0%	001 009	0.00	0.03	0.00	0.30	45.0% 50.9%	13%	13.7%	0.6%	49%	05%	45.0% 50.9%
33		146	+	2				0.03		0.00	+	15%	29.7%	2.1%	35%	0.9%	100.0%	001 012				0.46	46.6%	0.9%	15.0%	14%	2.5%	0.5%	46.6%
34		152 153		5	0.03	0.59	0.00	0.15	0.02	1.69		2.0%	35.0% 41.8%	0.2%	9.1% 3.3%	0.9%	100.0%	003 031	0.00		0.01	0.83	49.1% 54.0%	1.6%	18.1%	0.2%	65% 2.0%	05% 0.2%	49.1% 54.0%
36		154		ś	0.06	0.85	0.00	0.02	001	1.07		11%	45.2%	0.2%	0.9%	0.3%	100.0%	004 050	0.00	0.01	0.00	1.00	57.5%	2.2%	26.9%	0.1%	0.6%	0.2%	57.5%
3.7		155	-	5	0.05	0.90	0.00	0.02	0.02	2.02	_	2.3%	44.5% 31.4%	0.2%	0.7% 1.2%	0.9%	100.0%	003 050	0.00		0.01	1.22	60.9% 46.2%	1.4%	24.9%	0.1% 2.7%	0.5%	05% 1.1%	60.9%
32 33 34 35 36 37 38 39		162		ŝ	0.03	0.67	0.00	0.13	001	1.74		2.0%	38.5%	0.1%	7.3%	0.7%	100.0%	0.03 0.36	0.00	0.09	0.01	0.92	52.6%	1.6%	20.8%	0.1%	49%	05%	52.6%
40		163	-	5	0.06	0.80	0.00	0.02	001	1.00	-	13%	44.2% 46.0%	0.2%	1.1%	0.3%	100.0%	004 046	0.00	0.01	0.00	1.03	56.9% 50.7%	2.1%	26.6%	0.1%	0.8%	0.2%	56.9% 50.7%
42		165		5	0.04	0.29	0.03	0.02	003	2.07		19%	34.2%	1.2%	1.0%	14%	100.0%	0.02 0.40	0.02		0.02	1.12	54.3%	12%	19.5%	1.1%	0.6%	0.7%	54.7%
43		2	128		0.00	0.15	0.00	0.06	001	0.45	+	27%	34.3% 25.0%	0.9%	13.1% 7.2%	1.8%	100.0%	001 007	0.00		0.01	0.20	44.7%	1.8%	16.5%	0.7% 1.1%	9.8%	1.1%	44.2% 44.7%
45		- 4	132		0.02	0.14	0.01		0.01	0.53		2.0%	25.7%	2.1%	72%	1.1%	100.0%	001 006			0.00	0.22	43.2%	1.9%	11.9%	13%	49%	0.8%	43.2%
46		- 6	134	2	0.00	0.14	0.01	0.02	000	0.54	+	2.2% 4.2%	25.9% 26.1%	2.6%	37% 46%	1.1%	100.0%	001 007	0.01		0.00	0.15	48.2%	13%	12.2%	1.8%	2.6%	06%	41.2% 41.0%
46		10	138		0.03	0.26	0.03	0.12	0.02	0.91		2.0%	28.7%	3.6%	13.2%	2.0%	100.0%	002 014	0.02		0.01	0.42	45.8%	23%	15.4%	24%	24%	1.2%	45.0%
50		12	139		0.04	0.34	0.00		002	1.00	+	17%	31.5% 31.0%	0.4%	3.1% 1.4%	1.6%	100.0%	003 017	0.00		0.01	0.58	53.8% 47.1%	2.5%	15.6%	0.3% 1.3%	2.3%	0.8%	53.8% 47.1%
51		13	141		0.02		0.04	0.10	001		F	2.6%	28.2%	4.0% 1.2%	11.2% 11.7%	14%	100.0%	002 012			0.01	0.41	45.6% A4.7%	1.8%	13.3%	27%	8.0% 8.9%	0.8% 1.1%	45.6% 44.7%
53		19	147	4	0.04	0.35	0.01		002	1.07		10%	21.3%	0.5%	20%	0.9%	100.0%	003 036	0.00		0.01	0.60	44.2% 55.4%	2.0%	16.3%	0.3%	13%	0.7%	55.4%
41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 55		20	148		0.04	0.31	0.03	0.11	0.02	0.97	ŧΞ	40%	32.1% 36.6%	2.7%	11.4% 8.1%	1.6%	100.0%	003 015	0.02		0.01	120	49.5%	27%	15.5%	1.9%	54%	0.9%	49.5% 50.6%
56		25	153	10	0.12	123	0.00	0.11	003	2.62		44%	46.0%	05%	40%	1.1%	100.0%	0.10 0.72	0.01	0.06	0.02	151	57.6%	3.7%	27.4%	0.3%	2.9%	0.6%	57.6%
57		26	154			1.32			007	2.85	-	55% 42%	46.3% 40.1%	0.4%	15%	25% 17%	100.0%	0.11 0.81	0.00		0.04	2.00	55.5% 61.6%	19% 26%	28.2% 22.2%	0.3%	1.0%	1.3%	55.5% 61.6%
59		26	156	10	0.11	0.83	0.13	0.11	004	2.90		16%	27.9%	42%	3.8%	1.4%	100.0%	007 035	0.09	0.06	0.03	1.36	45.5%	24%	11.9%	3.1%	2.6%	09%	45.5%
61		34	162	10	0.08	1.08	0.01	0.19	002	2.51	-	12% 47%	42.9% 46.8%	05%	7.4% 1.2%	0.8%	100.0%	0.06 0.61			0.01	1.36	54.3% 54.1%	25%	24.2% 29.1%	0.3%	45% 12%	05%	54.7% 54.1%
62		36	164	10	0.16	1.30	0.01	0.04	006	3.07		53%	42.2%	0.4%	14%	1.9%	100.0%	0.11 0.76	0.00	0.03	0.04	1.85	60.1%	16%	24.7%	0.3%	1.0%	1.3%	60.1%
63	_	37	165	10	0.12	1.13	0.54	0.07	0.04	3.30	_	17%	34.3%	1.1%	22%	12%	100.0%	007 060	0.03	0.05	0.02	1.60	54.9%	22%	18.1%	0.9%	1.4%	0.7%	54.9%

- K-patch Mid CH

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Ь.															max ratio ou	t of all beams												max ratio out of all I			
					L			4cm2	PD/mW/o	m2)			10.5%	48.2%	4.9%	14.9%	4.6%	100.0%	4cm	n2 PD(mV	W/cm2) a	t 10mm evalu	uation dista	nce	62.2%	7.2%	29.1%	12%	10.9%	2.8%	62.2%
No.	Module Typ	oe Beam I	0,1 Sema ID	2 Feed no.	54/8	ght) S3(Le	n 55/7e		(Sottom)	\$1/Pronti	SZIRear	per Seam	ratio (Right 2mml/Iworst-	ratio (Left 2mm)/(wont-	ratio (Top 2mml/lwont-	ratio (Bottom 2mml/Iwont-	ratio (Fornt 2mm)/(worst-	ratio (Rear 2mm)/(wont-	S4(Right)		SS(Top)	SS(Bottom)	S1/Front)		ratio worst-surface	ratio (Right 10mmi/(wont-	ratio (Left 10mm)//worst-	ratio (Top 10mm)/(wont-	ratio (Sottom 10mm)//worst	ratio (Front 10mm)//wont-	ratio (Rear 10mm)/(wonst-
					5490	get) Saja	11) 55(10	ipi sa	(ectors)	21(HORE)	SZORRE	Back-of (dB)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)	S40kight	Salrest)	30(100)	Se(somon)	3 ((Hone)	52(9000)	(10mm/2mm)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)
1 2		0 2		1	0.0		0.00	0	0.02	0.00	0.16		44%	36.3% 25.1%	0.6%	12.5% 7.8%	1.9%	1000%	000	003	0.00	0.02	0.00	0.07	45.0% 40.2%	25% 34%	19.4%	0.6%	9.4% 5.6%	1.3%	45.0% 41.2%
3 4		- 4		1	0.0	0.04	0.00	-	0.01	000	0.16		6.3%	26.6%	1.2%	82%	1.2%	100.0%	001	0.02	0.00	0.01	0.00	0.06	38.6%	44%	13.9%	1.3%	6.3%	06%	31.6%
5		6		1	01		0.00		0.01	000	0.20	-	40%	20.8% 48.2%	1.0%	15% 15%	15%	100.0%	001		0.00	0.01	0.00	0.10	47.0% 42.1%	10%	11.4% 25.4%	05%	25%	1.0%	47.0% 42.1%
6		10		2	01				0.04	0.00	0.34		18% 58%	23.0% 29.9%	1.2%	10.2% 42%	0.9%	100.0%	001	004	0.00	0.03	0.00	0.14	41.7% 46.1%	23% 42%	12.2%	0.9%	82% 33%	05%	41.7% 45.1%
8		12		2	02	22 0.34	0.00	,	0.01	001	0.20		63%	35.4%	0.8%	23%	2.6%	100.0%	0.02		0.00	0.01	0.01	0.17	44.0%	49%	18.5%	0.5%	1.6%	1.3%	44.0%
10		13		2	0.0				0.02	0.00	0.29	-	41%	22.8% 40.7%	2.0%	75% 81%	1.4%	100.0%		003	0.00	0.02	0.00	0.14	49.0%	31% 31%	11.2%	17%	5.8% 6.4%	0.7% 1.1%	49.0% 42.6%
11		19		2	0.0			0	0.02	0.01	0.38		47% 46%	29.6% 23.2%	0.5% 1.0%	47% 14.9%	1.6% 2.0%	100.0%	001	007	0.00	0.01	0.00	0.19	49.5%	2.9%	17.8%	0.5%	2.9%	1.0%	49.5% 41.4%
13		24		5	0.0	0.20	0.00		0.07	001	0.84		12%	11.7%	1.0%	7.9%	1.1%	100.0%	002	0.16	0.01	0.05	0.01	0.41	48.7%	2.7%	18.9%	0.7%	5.7%	0.6%	48.7%
14		25		5	01				0.04	0.02	1.06	-	49%	41.2% 38.1%	0.4%	40% 12%	2.2% 2.3%	100.0%	003		0.00	0.02	0.01	0.45	48.3% 51.5%	33% 69%	25.2%	0.3%	2.6%	1.3%	48.2% 51.5%
5 6 7 8 9 10 11 12 13 14 15 16		27		5	0.0	5 0.31	0.00	1	0.03	0.02	0.09		58% 46%	34.2% 18.1%	09% 27%	3.4% 11.9%	25%	100.0%	0.04	0.19	0.00	0.02	0.01	0.46	51.6% 43.7%	4.0%	20.9%	0.8%	22% 81%	1.3%	51.6% 41.7%
18		34		5	0.0	0.30	0.00		0.06	0.01	0.05		1.2%	34.7%	0.8%	7.4%	1.2%	100.0%	002	0.17	0.01	0.04	0.01	0.41	48.6%	2.6%	19.6%	0.6%	51%	06%	41.6%
19		35		5	0.1				0.02	002	0.87	+	10.5%	42.1% 39.8%	0.2%	19%	2.4%	100.0%	006	0.29	0.00	0.01	0.02	0.48	48.5% 48.0%	6.0% 7.2%	29.1%	0.2%	12%	2.0%	41.5% 41.0%
21		37		5	0.0		0.00		0.03	0.01	0.84		55%	26.2% 21.0%	1.0%	18% 11%	1.4%	100.0%	003	013	0.00	0.02	0.01	0.43	\$1.4% 41.6%	12%	15.2%	0.8%	25%	1.0%	51.4% 41.6%
20 21 22 23 24		130	_	i	0.0	00 0.00	0.00		0.01	0.00	0.36		1.1%	22.8%	1.4%	22%	0.5%	100.0%	000	0.04	0.00	0.01	0.00	0.15	29.0%	0.8%	11.0%	1.1%	1.4%	0.3%	29.0%
25		132		1	01	0.00	0.00	+	0.01	000	0.35	+	14%	23.2% 22.8%	1.6%	28% 27%	0.6% 0.5%	100.0%	000	004	0.00	0.01	0.00	0.15	41.4%	1.1%	11.0%	1.1%	2.0%	0.3%	41.4% 20.8%
26		136		1	0.0	0 0.54		1	0.01	0.00	0.21		1.4%	20.3% 11.2%	2.9% 2.3%	43% 55%	1.0%	100.0%	000	0.02	0.00	0.01	0.00	0.00	29.1% 48.1%	1.0%	9.7% 17.7%	1.9%	19% 17%	05% 05%	20.1% 48.1%
25 26 27 28 29 30		139		2	0.0	0.24	0.00		0.02	000	0.76		1.7%	31.7%	0.1%	2.8%	0.1%	100.0%	001	0.12	0.00	0.01	0.00	0.41	53.6%	12%	15.3%	0.0%	1.7%	0.1%	53.6%
30		140		2	0.0				0.00	001	0.76	+	1.6%	26.2%	1.2%	0.5% 3.1%	0.7%	100.0%	001		0.01	0.00	0.00	0.15	46.0% 29.6%	13%	13.0%	0.8%	22%	0.4%	46.0% 29.6%
31		146		2	0.0				0.03	0.01	0.64		19%	28.2% 29.1%	1.4%	50%	0.8%	1000%	001		0.00	0.02	0.00	0.30	46.6% 50.2%	1.6%	12.9%	0.9%	14%	05%	46.6% 50.3%
33		140		2	0.0	0 0.22	0.00	2	0.02	0.01	0.78		17%	27.8%	2.4%	27%	0.9%	100.0%	001	0.11	0.01	0.01	0.00	0.35	44.6%	1.2%	14.0%	15%	1.8%	05%	44.6%
35		152		5	01	5 0.70	0.00		0.14	001	1.76	+	23%	34.2% 29.6%	0.4%	8.2% 2.9%	0.8%	100.0%		0.40	0.00	0.09	0.01	0.93	47.0% 52.0%	1.9%	18.3%	0.3%	5.2% 1.6%	0.4%	47.6% 52.6%
26		154		5	01				0.01	601	1.93		13% 28%	41.3% 42.2%	0.1%	0.7%	0.9%	100.0%	005	0.46	0.00	0.01	0.00	1.00	55.9% 58.8%	2.4%	24.8% 23.4%	0.1%	0.5%	0.2%	55.9% SLIPS
32 33 34 35 36 37 38 40 41 42 43 44 45 46 47 48 49 50 51		156		Š	0.0	03.0	0.00	7	0.02	003	1.95		1.3%	30.8%	1.4%	1.0%	1.5%	100.0%	002	0.26	0.05	0.02	0.02	0.90	46.2%	0.9%	13.3%	2.6%	0.8%	1.1%	46.2%
40		162		5	01	6 0.73	0.00		0.02	000	1.72	+	2.4%	35.7% 40.2%	0.2%	6.3%	0.6%	100.0%	003	0.44	0.00	0.01	0.01	1.03	50.1% 56.3%	2.0%	20.4%	0.1%	19%	0.3%	50.1% 56.3%
41		164		5	0.0		0.00		0.01	0.01	1.93		11%	41.4% % PK	0.2%	05%	0.4%	1000%			0.00	0.01	0.01	1.12	57.9% 55.2%	24%	26.0%	0.2%	0.4%	0.3%	57.9% 55.2%
43		0	128		0.0				0.04	001	0.40		29%	30.2%	0.E% 1.0%	8.1%	12%	100.0%		007	0.00	0.03	0.00	0.21	42.6%	2.1%	143%	0.6%	5.8%	06%	42.6%
45		4	132	2	01				0.03	001	0.56	+	14%	23.3% 23.8%	1.8%	55% 47%	0.9%	100.0%		000	0.01	0.02	0.00	0.23	42.2% 43.9%	25%	12.4%	13%	41% 32%	05%	42.2% 40.9%
46 47		6	134		0.0				0.02	0.01	0.61		26%	22.7% 35.2%	1.8%	13%	0.8%	100.0%	001	007	0.00	0.01	0.00	0.29	47.1% 49.7%	1.8%	10.7%	12%	23%	05%	47.1% 40.7%
40		10	138	- 4	0.0	0.31	0.00	3	0.07	0.01	1.05		2.9%	29.9%	2.6%	6.6%	1.0%	100.0%	002		0.02	0.05	0.01	0.53	50.5%	22%	16.6%	1.6%	51%	06%	50.5%
50		11			0.0				0.04	001	1.16	+	40%	32.7% 28.8%	1.8%	34% 13%	1.0%	100.0%	004		0.00	0.03	0.01	0.64	55.1% 45.6%	31% 31%	17.4%	12%	2.7% 0.7%	05%	55.1% 45.6%
51		13			0.0				0.05	0.01	1.00		33% 29%	27.4% 34.2%	10%	48%	1.3%	100.0%	003		0.02	0.04	0.01	0.46	45.5% 44.1%	25%	12.3%	20%	3.7% 7.0%	0.7%	45.5% 44.1%
53		19	147	- 4	0.0	9 0.39	0.00	0	0.03	001	1.20		11%	32.2%	0.3%	23%	0.8%	100.0%	003	0.20	0.00	0.02	0.01	0.69	57.1%	22%	16.8%	0.3%	1.6%	0.7%	57.1%
54 55 56		20		10	0.1	1.12	0.00	2	0.10	002	2.87	-	17%	30.8% 29.1%	2.2% 0.8%	12.0% 8.3%	1.5%	100.0%	008	0.15	0.01	0.07	0.01	1.55	50.1% 54.1%	2.7% 2.7%	15.1% 21.5%	1.4%	7.0%	0.6%	50.1% 54.1%
56		25			0.1				0.11	003	2.01		44%	47.0% 40.2%	0.5%	41%	12%	100.0%	010	0.78	0.00	0.07	0.02	1.66	59.1% 53.9%	3.7% 5.0%	27.8%	0.4%	2.6%	0.7%	59.1% 51.9%
58		27	155	10	0.3	5 1.40	0.00	2	0.05	0.06	2.47		43%	41.8%	0.5%	14%	1.6%	100.0%	0.11	0.79	0.02	0.04	0.03	2.16	62.2%	11%	22.7%	0.4%	1.0%	09%	62.2%
60		26			01				0.14	004	2.84	-	27%	24.8% 41.5%	17%	43% 74%	1.4%	100.0%	005		0.00	0.10	0.03	1.62	48.1% 56.8%	1.7%	11.8% 24.5%	25%	12% 44%	09%	48.1% 56.8%
61		35	163	10	0.1			1	0.05	003	2.00		46%	42.2% 41.9%	0.3%	1.0%	12%	100.0%	010		0.00	0.04	0.03	1.66	57.5% 59.9%	33%	26.7%	0.2%	12%	09%	57.5% 59.9%
63		37	165			12 121			0.05	0.05	3.72		32%	345%	0.8%	13%	13%	100.0%	0.15		0.03	0.04	0.03	2.10	50.5%	2.0%	18.2%	0.7%	1.0%	08%	58.5%

- K-patch High CH

																max ratio ou	t of all beams												max ratio out of all	beams		
	Т		T					40	cm2 PD/m	W/ora2	0			12.0%	\$3.8%	4.2%	12.4%	2.4%	100.0%	4cm2 l	PD(nW)	(cm2) at	10mm evalu	ation distan	nce	62.0%	9.1%	28.6%	2.7%	9.1%	2.2%	62.0%
No. Mc	dule Typ	e Seam ID_1	Sema ID 2	Feed no.		Т	т			Т			per Beam	ratio	ratio	ntio	ratio	ratio	ntio	-						ratio	ratio	ntio	ntio	ratio	ntio	ntio
	- 1				54/Rig	ht) 53(1	eft) S	S(Top)	S6(Botto	rm) S1	(Front)	S2(Rear)	Back-off	(Right 2mm)/(wont- surface 2mm)	(Left 2mm)/(worst- surface 2mm)	(Top 2mm)/(wont- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Forst 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	S4(Right) S3	(Left) 1	S(Top)	SS(Bottom)	S1(Front)	S2(Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(wont- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Sottom 10mm)/(word- surface 2mm)	(Front 10mm(/(wont- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
1	_	0		1	0.00	0.0	06	0.00	0.02	+	000	0.20	(dB)	16%	32.0%	0.5%	12.7%	1.5%	100.0%	000 0	003	0.00	0.02	0.00	0.09	43.7%	2.0%	16.2%	0.5%	7.6%	1.0%	43.7%
2		2		1	020			000	0.01		000	0.17		58% 49%	24.4% 21.0%	1.2%	70% 7.1%	1.7%	100.0%	001 0		0.00	0.01	0.00	0.07	29.5% 40.4%	15% 18%	12.2%	0.6%	52% 55%	1.2% 0.5%	33.5% 42.4%
4		- 6		1	0.00	0.0	04	0.00	0.01	-	000	0.19		5.3%	19.5%	1.1%	42%	1.1%	100.0%	001 0	002	0.00	0.01	0.00	0.00	42.1%	3.7%	10.0%	1.1%	3.7%	1.1%	42.1%
5		8 10	-		0.00			0.00	0.00		000	0.09		99% 17%	51.8% 22.8%	2.2%	44% 124%	1.7% 0.8%	100.0%	001 0			0.00	0.00	0.04	45.1% 42.4%	7.7% 2.2%	28.6%	1.1%	33% 81%	2.2% 0.6%	45.1% 42.4%
7		11		2 2	0.00	0.1		0.00	0.02		001 001	0.44		56% 84%	28.7% 38.4%	0.5%	41% 28%	1.1%	100.0%	002 0	007	0.00	0.02	0.00	0.21	47.0% 41.3%	43% 72%	15.6%	05%	34% 19%	0.7% 1.2%	47.0% 41.2%
9		13			0.02	0.0	07	000	0.02		0.00	0.34		45%	21.1%	2.7%	7.1%	1.2%	100.0%	001 0	004	0.00	0.02	0.00	0.17	49.3%	10%	10.7%	21%	5.0%	09%	49.3%
10		18	-	2	0.02		16	000	0.03		001	0.39	-	6.2% 5.0%	42.1% 21.2%	0.3%	79%	2.6% 1.5%	100.0%	001 0 001 0		0.00	0.02	0.01	0.18	44.9% 50.9%	11%	23.1%	0.3%	5.9% 2.5%	1.5%	44.9% 50.9%
12		20 24			0.02		09 32	0.01	0.04		001	0.33		5.4% 15%	26.3% 11.5%	1.5%	12.4% 7.1%	1.5%	100.0%	601 0			0.03	0.00	0.12	29.6% 47.2%	33% 25%	15.4%	12%	9.1% 46%	09% 09%	22.0% 47.2%
14		25		5	0.05	o.	45	000	0.04		0.04	1.04		47%	41.0%	0.4%	40%	3.4%	100.0%	003 0	0.27	0.00	0.02	0.02	0.40	46.3%	33%	25.7%	0.2%	2.0%	19%	46.3%
15		26 27	-	5	0.10			0.01	0.01		002	0.94		10.6%	30.2% 36.2%	0.8%	13%	1.8%	100.0%	007 0 004 0			0.01	0.01	0.49	52.6% 50.8%	7.8% 45%	20.2%	0.4%	1.0%	1.2% 1.8%	52.6% 50.8%
17		28 34			0.02			0.02	0.06		001	0.63		18% 15%	21.1% 34.2%	1.0%	61%	1.1%	100.0%	002 0		0.02	0.04	0.00	0.30	47.5% 46.4%	24%	10.9%	24%	58% 44%	06%	47.5% 46.4%
19		35		5	0.10	0.3	12	0.00	0.02	-	0.02	0.97		11.2%	35.4%	0.3%	1.9%	2.6%	100.0%	0.07 0	0.21	0.00	0.01	0.02	0.46	53.2%	7.8%	23.8%	0.3%	1.1%	1.0%	53.2%
20		36	-		0.10			0.01	0.02		003	0.87		12.0%	38.6% 26.7%	0.7%	23%	11%	100.0%	008 0		0.00	0.01	0.02	0.44	50.8% 52.6%	9.1% 2.9%	24.6%	05%	1.1%	2.2% 1.0%	50.8% 52.6%
22		126			0.00			000	0.01		000	0.31		1.3%	21.9%	10%	26% 19%	0.3%	100.0%	000 0		0.00	0.01	0.00	0.14	44.4% 20.4%	1.0%	95%	0.7%	20%	03%	44.4% 22.4%
24		132		1	020	0.0	00		0.01		000	0.36		1.4%	22.1%	1.7%	22%	0.6%	100.0%	000 0	004	0.00	0.01	0.00	0.15	41.1%	1.1%	10.6%	1.1%	1.7%	0.3%	41.1%
25		134	-	-	0.00		06	0.01	0.01		000	0.20		13%	21.9%	13%	27%	0.5%	100.0%	600 6	004	0.00	0.01	0.00	0.15	29.7% 34.7%	0.8%	10.7%	1.1%	19%	03%	29.7% 34.7%
27		138			0.00		18	0.01	0.03		000	0.58		2.2% 1.8%	31.3%	2.1%	52%	0.7%	100.0%	001 0		0.00	0.02	0.00	0.27	47.0% 51.6%	1.9%	16.2%	12%	16%	05%	47.0%
29		140	 	2			22		0.01		001	0.77	-	1.5%	30.9% 28.6%	0.1%	27%	0.1%	100.0%	001 0			0.01	0.00	0.37	47.4%	12%	15.1%	0.1%	1.8%	0.1%	53.6% 47.4%
30		141	-		0.00			0.01	0.02		001	0.55		1.8% 2.2%	27.0% 27.2%	2.4%	31% 43%	0.9%	100.0%	601 6		0.00	0.01	0.00	0.23	41.6%	13%	12.5%	18%	22%	05% 03%	41.6% 46.0%
31	E Pass	h 147		2	0.02	0.2		0.00	0.01		000	0.89		1.8%	28.1% 27.1%	0.2%	0.6%	0.2%	100.0%	001 0	012	0.00	0.00	0.00	0.45	50.8% 41.2%	12% 12%	13.7%	0.1%	0.3%	01% 05%	50.8% 41.2%
34		152	 	5	0.04	0.5	34	0.01	0.13	-	001	1.65	_	2.4%	11.9%	0.5%	7.8%	0.6%	100.0%	003 0	0.31		0.09	0.01	0.00	48.3%	2.1%	10.0%	0.4%	5.1%	0.4%	41.2%
35		153	-		0.06	0.0		0.01	0.05		001	1.74		13%	37.7% 38.9%	0.3%	29%	0.2%	100.0%	004 0		0.00	0.03	0.01	0.91	52.3% 55.4%	23%	22.3% 23.5%	0.3%	15%	03% 02%	52.9% 55.4%
37		155			0.06	0.1	15	0.01	0.01			2.00		2.8%	42.2% 12.1%	0.3%	0.5%	0.6%	100.0%	004 0	0.46	0.00	0.01	0.01	1.15	57.6% 44.6%	19%	23.8%	02%	0.4%	0.4%	57.6% 44.6%
39		162	 	5	0.05	- 0.1	£2	0.01	0.10	\neg	001	1.72	-	2.7%	35.8%	0.3%	55%	0.5%	100.0%	002 0	0.35	0.00	0.06	0.01	0.87	52.4%	22%	20.5%	0.2%	16%	0.3%	52.4%
40		163	-	٥.	0.07	01	22	0.01	0.02		000	1.01		16% 14%	38.1% 41.4%	0.3%	0.9%	0.2%	100.0%	005 0		0.00	0.01	0.00	1.02	56.0%	2.6%	21.6%	0.2%	0.8%	01% 04%	56.0% 57.2%
42		165	128		0.06		76	0.02	0.02		0.02	2.01		2.9%	37.7%	1.0%	0.7%	1.1%	100.0%	004 0 001 0		0.02	0.01	0.01	1.10	54.6%	1.8%	19.2%	0.8%	0.5%	06%	54.6% 43.4%
44 45		2	130	2			13		0.03		001	0.60	_	10% 28%	28.5%	1.0%	65% 43%	0.9%	100.0%	001 0			0.03	0.00	0.24	42.4%	1.8%	14.2%	0.6%	48% 32%	05%	42.4%
45		4	132		0.02			0.01	0.02		001	0.61		26% 29%	21.1%	1.6%	38% 29%	0.8%	100.0%	001 0			0.02	0.00	0.25	41.2%	21%	10.4%	12%	10% 23%	05% 0.7%	41.2% 46.7%
47		8 10	136		0.02			0.01	0.02		000	0.21		5.1%	33.2% 27.9%	4.2%	7.0%	13%	100.0%	601 6	300	0.00	0.02	0.00	0.15	46.3% 51.0%	42%	18.8%	26%	48%	1.0%	46.2%
40		11	129		0.04	0.2	36	0.00	0.07	\neg	001	1.10	\vdash	11%	30.1%	2.3% 0.3%	63% 37%	0.7%	100.0%	004 0	019	0.00	0.03	0.01	0.66	54.5%	3.0%	14.9%	0.2%	25%	0.4%	\$1.0% \$4.5%
50		12	140	4	0.06			0.01	0.02		0.02	1.14		49%	29.3%	1.2%	14%	13%	100.0%	004 0		0.00	0.01	0.01	0.50	43.4%	37% 21%	15.0%	12%	0.8%	09%	43.4% 45.5%
52		10	146	4	0.04	0.7	36	0.01	0.06			1.11		19%	12.6%	0.9%	7.4%	13%	100.0%	003 0	019	0.00	0.06	0.01	0.47	42.1%	25%	17.3%	0.6%	5.8%	0.7%	42.1%
54		19	147	4	0.04	0.0		0.01	0.02		001	1.21	\vdash	13%	30.3% 29.4%	2.2%	1.8% 8.3%	1.1%	100.0%	003 0		0.00	0.02	0.01	0.70	57.7% 49.1%	22%	15.8%	0.3%	12%	08% 08%	57.7% 49.1%
55		24	152	10	0.11	1.7	16	0.02	0.25		004	2.15		15%	36.7% 41.9%	0.6%	79%	13%	100.0%		064	0.02	0.16	0.02	1.60	53.8% 57.9%	28%	20.4%	0.5%	5.1% 2.1%	06%	\$3.8% \$7.9%
57		26	154	10	0.19	1.0	29	0.00	0.03		004	2.00		6.2%	15.4%	0.3%	0.9%	12%	100.0%	0.15 0	067	0.00	0.02	0.03	1.69	54.9%	48%	21.7%	0.2%	0.6%	0.8%	54.9%
58		27	155	10	0.18		46 13		0.04		006	1.57	H	50% 26%	41.0% 24.8%	11%	12% 34%	1.7%	100.0%	013 0			0.03	0.04	1.65	62.0% 49.2%	17%	22.7%	0.3% 2.4%	0.9% 2.2%	11%	62.0% 49.2%
60		34	162	10	0.12	1.2	25	0.02	0.21		0.04	2.14		17%	29.7%	05%	6.7%	13%	100.0%	0.10 0	0.71	0.00	0.14	0.02	1.75	55.7%	31%	22.5%	0.3%	44%	06%	55.7%
62		35 36	163	10	0.23	1.7	17	000	0.04		006	2.00		5.1% 7.4%	37.3% 38.1%	0.3%	15%	1.0%	100.0%	012 0 017 0	069	0.00	0.03	0.02	1.62	54.5% 60.3%	4.0% 5.5%	23.4% 22.4%	0.2%	0.9%	0.7% 1.4%	94.5% 60.3%
63		227	165	10	0.13	1.2	27	0.03	0.06	T	005	3.78		15%	33.7%	0.8%	15%	13%	100.0%	0.09 0	068	0.03	0.04	0.03	2.26	59.8%	24%	18.0%	0.7%	1.1%	0.7%	59.8%

Table 5. PD of Ant K – patch antenna (39GHz – n260)

[Folder Open Status]

- K-patch Low CH

															max ratio ou	t of all beams												max ratio out of all	beams		
т	\neg	T		Т	Г			4cm2 P	PD(mW/on	n2)			6.9%	4.9%	2.2%	19.2%	2.2%	100.0%	4	iom2 PD(ml	W/cm2) a	at 10mm evalu	uation dista	nce	60.4%	4.4%	16%	1.9%	11.0%	125	60.4%
No. N	odule Typ	e Beam ID_1	Sema ID 2	2 Feed no.	Н	\top	Т	Т	\neg		П	per	ratio	ratio	ntio	ratio	ratio	ntio		Т	П				ntio	ratio	ratio	ntio	ratio	ntio	ntio
	,,,				54/Rig	ht) S3(Lef	t) SS(Top	96(0	Bottom)	\$1(Front)	S2(Rear	Beam Back-of	(Right 2mm)/(wont- surface 2mm)	(Left 2mm)/(wonst- surface 2mm)	(Top 2mm)/(worst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	S4(Right)	S3(Left)	SS(Top)	SS(Bottom)	\$1(Front)	S2(Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(wont- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Sottom 10mm)/(worst- surface 2mm)	(Front 10mm)/(wont- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
	_		-		0.00	0.00	0.00	-	0.00	000	A16	(40)	19%	13%	DATACH ZITER)	Surtace 27576 7.5%	126	100.0%	600	0.00	0.00	0.01	0.00	0.00	(10mm/2mm) 25.2%	13%	05%	numace zmm)	50%	95% 05%	15.2%
2		2		i	0.00	0.00			0.01	000	0.19		1.6%	1.6%	0.5%	67%	0.5%	100.0%				0.01		0.00	44.6%	1.0%	1.0%	0.5%	31%	05%	44.5%
3		4		1	0.00			-	0.02	000	0.22		1.8%	1.8%	0.5% 0.6%	6.8% 4.1%	0.5%	100.0%				0.01	0.00	0.09	41.4%	14%	14%	05%	45% 15%	00% 00%	41.4% 44.7%
1 4 5		-		1	0.00		0.00			000	0.15	_	2.7%	14%	0.0%	485	0.7%	100.0%				0.01	0.00	0.06	42.2%	2.0%	14%	0.0%	41%	00%	42.2%
6		10		2	0.00	0.01			0.03	000	0.41		1.7%	1.7%	0.5%	66% 45%	0.5%	100.0%	001	0.01	0.00	0.02	0.00	0.20	49.4%	12%	12%	05%	42%	0.2% 0.2%	49.4% 54.0%
8 9		12	_	2	0.01			1		000	0.49	-	17%	2.1%	0.2%	94%	1.7%	1000%		001		0.02	0.00	0.14	54.0% 47.0%	1.0%	17%	0.2%	59%	0.2%	54.0% 47.0%
9		13		2	0.00		0.00		0.05	000	0.36		19%	14%	0.0%	11.9%	0.8%	1000%		000		0.03	0.00	0.15	42.4%	1.7%	0.8%	0.0%	72%	0.6%	42.4%
10		18	-	2 2	0.01				0.00	000	0.39	+	23%	1.5%	0.5%	10%	0.5%	100.0%	001	000			0.00	0.18	45.6% 55.2%	1.0%	20%	03%	44%	0.3%	45.6% 55.2%
12		20		2	0.00				0.04	001	0.30		2.0%	1.7%	0.3%	12.5%	2.0%	1000%		0.00			0.00	0.12	43.9%	1.4%	14%	0.3%	8.4%	1.0%	43.9%
13		24	-	5	0.04				0.16	001	1.10	-	15% 10%	1.6%	0.7%	14.4% 2.1%	0.6%	100.0%	003	0.01		0.10	0.00	0.62	56.6% 60.0%	2.5% 2.2%	1.3%	0.6%	1.9%	0.3% 0.2%	56.6% 60.0%
12 13 14 15 16 17 18 19		26		ŝ	0.00	0.05	0.00	-	0.01	001	0.97		3.2%	4.9%	0.3%	13%	0.6%	100.0%	0.02	0.04	0.00	0.01	0.00	0.56	57.5%	25%	16%	0.2%	0.9%	0.3%	57.5%
16		27 28	\vdash	5	0.02				0.03	001	0.63	\vdash	2.7% 5.9%	4.3% 1.7%	0.3%	5.3% 8.1%	1.0%	1000%		0.02		0.02	0.00	0.35	55.5% 55.0%	21%	12%	0.2%	14%	05%	55.5% 55.0%
10		34		5	0.05	0.02	0.01	- 0	0.13	001	1.17		4.1%	2.0%	0.4%	12.9%	0.9%	100.0%	003	0.02	0.00	0.07	0.01	0.60	58.0%	2.8%	1.5%	0.3%	62%	0.4%	58.0%
19		35		5	0.00			,	0.01	001	0.96		29% 18%	4.7% 4.5%	0.4%	12%	0.6%	1000%		0.04	0.00		0.00	0.56	50.3% 50.5%	21%	16%	0.3%	0.9%	0.3%	58.3% 59.5%
21		37	_	5	0.02		0.00	-	0.06	001	0.50	_	18%	2.6%	0.4%	12.8%	2.2%	100.0%	001	001	0.00	0.04	0.01	0.26	51.1%	2.8%	22%	0.4%	8.4%	12%	51.1%
22 23 24 25 26 27 28 29 30 31 32 33		128		1	0.00		0.00		0.01	0.00	0.15		2.1%	2.7%	0.7%	6.0%	0.7%	1000%		000	0.00	0.01	0.00	0.06	41.1%	1.4%	21%	0.7%	48%	0.7%	41.1%
23		130	-	1	0.00		0.00		0.01	000	0.14	-	2.1% 1.5%	1.4%	0.7%	35% 42%	0.7%	100.0%				0.00	0.00	0.07	49.7% 46.5%	1.4%	0.7%	0.7% 0.7%	28%	0.7% 0.7%	49.7% 46.5%
25		134		1	0.00			-	0.01	000	0.13		2.4%	1.6%	0.8%	39%	0.8%	100.0%	000	000	0.00	0.00	0.00	0.06	48.0%	1.6%	0.8%	0.8%	2.4%	0.8%	48.0%
26		136		1	0.00	0.00			0.00	000	0.11	-	1.8% 5.3%	1.8%	0.9%	2.6% 7.4%	2.1%	100.0%	000	0.00	0.00		0.00	0.05	46.5% 36.2%	1.8%	09% 21%	0.9%	1.8%	00% 1.1%	46.5% 36.2%
28		139		2	0.00	0.00	0.00		0.01	000	0.37		1.9%	2.1%	0.3%	3.0%	0.5%	100.0%	001	0.01	0.00	0.01	0.00	0.20	52.5%	13%	1.3%	0.3%	24%	0.3%	52.5%
29		140		2	0.00		000	,		000	0.22		2.1%	1.8%	1.0%	30% 75%	2.0%	1000%				0.01	0.00	0.19	57.4% 42.0%	1.8%	12% 15%	0.3%	1.8%	0.3% 1.0%	57.4% 42.0%
31		146	_	2	0.01				0.01	000	0.20	_	10%	2.1%	1.3%	30%	0.9%	100.0%		000			0.00	0.11	46.4%	21%	13%	0.9%	2.6%	0.4%	46.4%
32	K Pass	h 147		2	0.00				0.02	0.00	0.39		1.0%	2.0%	0.3%	43%	0.5%	100.0%	001	0.01			0.00	0.20	\$1.4%	13%	1.3%	0.0%	2.8%	0.3%	51.4%
33		152	-	5	0.00				0.01	000	0.20	+	40%	25%	1.0%	19.2%	1.5% 2.2%	100.0%		000	0.00		0.00	0.10	50.3% 50.3%	25% 41%	2.0%	0.5%	4.0% 13.0%	05% 08%	50.3% 50.3%
35		153 154		5	0.00				0.02	0.00	0.49		2.8%	2.8%	1.0%	30% 23%	0.6%	100.0%	001	001		0.01	0.00	0.28	54.5% 59.7%	2.4%	22%	0.8%	2.4%	0.2%	56.5% 59.7%
36		154	-	5	0.00		0.00			001	0.92	-	17%	13%	0.2%	23% 65%	0.8%	100.0%				0.02	0.00	0.55	59.7% 58.9%	2.5%	2.3%	0.2%	17%	0.4%	59.7% 58.9%
37		156		5	0.54	0.02	0.00		0.04	0.01	0.55		6.9%	11%	0.7%	7.4%	1.6%	1000%	0.02	0.01	0.00	0.02	0.01	0.30	51.7%	4.0%	25%	05%	40%	03%	51.7%
39		162	-	5	0.02		0.01		0.05	001	0.40	-	45% 11%	1.0%	1.8% 0.5%	11.8% 2.3%	1.8%	100.0%	001	0.01	0.00		0.00	0.19	48.2% 57.4%	3.0% 2.1%	1.8%	1.8%	65% 1.7%	0.8%	41.2%
41		164		ś	0.00				0.04	001	0.93		16%	2.7%	0.2%	39%	0.8%	100.0%		002		0.03	0.00	0.54	57.7%	2.7%	1.7%	0.1%	2.8%	0.4%	57.7%
39 40 41 42 43 44 45 46 47 46		165	134	5	0.02				0.04	0.01	0.55	₽	42% 14%	15%	0.2% 0.6%	7.3%	1.7%	100.0%		002	0.00	0.03	0.00	0.33	59.6% 36.6%	2.8%	2.8%	02%	46%	0.7% 0.6%	59.6% 36.6%
44		2	130	2	0.00				0.02	000	0.25		1.7%	2.3%	0.6%	65%	1.1%	100.0%			0.00	0.02	0.00	0.17	45.9%	1.1%	1.4%	0.6%	48%	06%	46.9%
45		4	132	2	000	0.00	0.00	-	0.02	000	0.40		23%	2.0%	0.5% 0.6%	58%	0.8%	100.0% 100.0%	601	0.01	0.00		0.00	0.16	42.7%	15%	15% 12%	05%	45% 17%	05% 0.3%	40.7% 42.5%
4.7		-	136	2	0.01	0.01	0.00		0.01	0.00	0.32	_	1.6%	1.6%	0.6%	35%	0.6%	100.0%	000	0.00	0.00	0.01	0.00	0.11	34.2%	13%	1.2%	0.6%	22%	0.3%	34.2%
46		10	138		0.02				30.0	001	0.56		12%	2.0%	1.3%	9.9%	1.1%	100.0%		0.01		0.03	0.00	0.29	\$1.5% \$1.6%	18%	1.6%	0.9%	59%	05%	51.5%
50		12	139		0.02	0.02	000		0.04	001	0.65	-	2.2%	2.8%	0.2%	49%	0.7% 1.2%	100.0%	001	002	0.00		0.00	0.44	51.6% 57.6%	1.5%	1.0%	0.2%	16%	0.4%	51.6% 57.6%
51		13	141	- 4	0.02				0.07	001	0.65		2.8%	2.3%	0.9%	11.0%	12%	100.0%	001	0.01	001	0.05	0.00	0.22	33.0%	1.5%	1.7%	0.8%	7.7%	0.5%	33.8%
49 50 51 52 53 54 55 56		18	146		0.02				0.04	000	0.71	₽	2.7%	2.1%	0.9%	60% 4.1%	0.6%	100.0%	001	001	0.00		0.00	0.31	44.2% 53.5%	2.0%	16%	0.7%	43%	0.3%	44.3% \$1.5%
54		20	141	- 4	0.00	0.01	0.01	-	0.05	001	0.43		2.0%	13%	1.2%	12.1%	21%	100.0%	001	001	000	0.03	0.00	0.21	43.9%	23%	2.6%	0.9%	75%	09%	49.2%
55		24 25	152 153		0.06		0.03		0.29	0.02	1.71	₽	16%	2.8%	1.6%	17.1% 3.0%	12%	100.0%		0.04			0.01	1.00	58.3% 60.4%	25% 25%	22% 15%	13%	10.6%	05%	58.3% 60.4%
5.7		26	154	10	0.00	0.09	0.00	-	0.04	002	1.99	_	19%	45%	0.4%	22%	12%	100.0%	0.05	0.07	0.00	0.03	0.01	1.19	59.6%	2.7%	1.3%	0.3%	1.6%	0.6%	59.6%
58		27	155	10	0.05				0.09	0.02	1.75		2.6%	4.0%	0.2%	53%	1.1%	100.0%	004	0.05	0.00	0.06	0.01	1.03	58.7% 49.0%	21%	10%	0.1%	33%	05%	58.7%
60		26	156	10	0.09	0.05	0.02	-	0.22	0.02	1.01	+	40%	2.9%	10%	7.9% 12.3%	12%	100.0%		0.04	0.01		0.01	1.07	59.0%	11%	25%	0.5%	49% 67%	0.7% 0.6%	49.0% 59.0%
61		35	163	10	0.07	0.00	0.00	-	0.04	002	1.74		4.1%	4.6%	0.6%	20%	0.9%	100.0%				0.02	0.01	1.04	59.7%	2.9%	16%	0.5%	1.4%	0.5%	59.7%
63		36	164	10			0.00		0.06	002	1.93	+	40% 15%	19%	0.2%	32% 98%	0.8% 1.7%	100.0%		0.05			0.01		58.7% 53.9%	31% 23%	29% 11%	02%	21% 61%	0.4%	51.7% 51.9%

- K-patch Mid CH

														max ratio ou	t of all beams												max ratio out of all I	beams		
	П							lon2 PD(mil	N/cm2)			5.6%	5.5%	2.6%	19.2%	2.8%	100.0%	4cm2 PD(r	nW/cm2	at 10m	nn evalua	ation dista	nce	70.5%	42%	46%	2.1%	11.0%	1.4%	70.5%
No. Module T	Type I	leam ID_1	Sens ID,2	Feed no.						Т	per Bear	ratio	ratio	ratio	ratio	ratio	ntio			Т				ratio	ratio	ratio	ratio	ratio	ratio	ratio
					S4(Right)	S3(Left)	SS(Top)	S6(Botton	ri) S1(Pro	nt) 52(Re	Back-o	(Right 2mm)/(wont- surface 2mm)	(Left 2mm)/(worst- surface 2mm)	(Top 2mm)/(worst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	S4(Right) S3(Left)	\$5(Ta)	p) SS()	Bottom)	S1(Front)	S2(Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(worst- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Sottom 10mm)/(worst- surface 2mm)	(Front 10mm)/(worst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
1		0		1	0.00	0.00	0.00	0.01	000		(01)	19%	1.3%	0.6%	65%	0.6%	100.0%		0.00		0.01	0.00	0.06	43.9%	13%	1.3%	0.6%	52%	06%	40.9%
2	F	2 4		1	0.00	0.00	0.00	0.02	000		-	19%	1.9%	0.5% 0.5%	99% 86%	1.2% 0.5%	100.0% 100.0%		0.00		0.01	0.00	0.07	40.1% 43.2%	12%	12%	0.5%	43% 65%	05%	40.1% 43.2%
5	F	6		1	0.00	0.00	0.00	0.01	000	0.1		2.7%	2.1%	0.7%	62%	0.7%	100.0%	000 000	0.00	#	0.01	0.00	0.07	45.2%	21%	1.4%	0.7%	34% 17%	0.0%	45.2%
6	- 1-	10		2	0.00	00.00	0.00	0.01	000	0.1	+	1.0%	1.2%	0.8%	49% 90%	0.0%	100.0%	000 000	0.00	+	0.01	0.00	0.07	40.2% 40.5%	1.2%	06%	0.6%	42%	0.0%	40.2% 48.5%
7	F	11 12		2	0.00	0.00	0.00	0.03	600			27%	1.0% 2.1%	0.5%	7.7% 12.0%	0.5% 2.1%	100.0%	001 001	0.00		0.02	0.00	0.22	59.2% 58.1%	25% 21%	2.5% 1.7%	0.3%	41%	0.3%	59.2% 58.1%
9	F	13		2	0.00	0.00	0.00	0.06				2.4%	1.1%	0.8%	15.5%	0.8%	100.0%		0.00		0.04	0.00	0.15	40.5%	1.6%	0.8%	0.5%	9.3%	0.3%	40.5%
9 10 11 12 13 14 15 16	- 1-	18 19		2	0.00	0.00	0.00	0.03	000		+	2.2% 3.7%	1.7% 3.7%	0.6%	7.4% 4.8%	0.7%	100.0%	001 001 001 001	0.00		0.02	0.00	0.16	48.5% 57.6%	1.9%	14%	0.6%	47% 26%	0.3%	48.5% 57.6%
12	F	20 24		2 5	0.01	0.00	0.00	0.03	001			2.4% 16%	1.7%	0.7%	11.9%	1.7%	100.0%		0.00		0.03	0.00	0.14	50.0% 65.3%	1.7%	14%	0.3%	9.1% 9.9%	0.7% 0.2%	50.0% 65.2%
14	E	25		5	0.03		0.00					3.0%	5.1%	0.1%	20%	0.8%	100.0%		0.00		0.01	0.00	0.55	63.6%	31%	4.3%	0.1%	13%	0.3%	63.6%
15	- 1-	26 27		5	0.03	0.04	0.00	0.02	000	0.6	+	41%	5.5% 1.6%	0.5%	2.5% 19.2%	0.5% 2.8%	100.0%		0.00		0.01	0.00	0.38	59.4% 53.7%	33%	43% 10%	0.5%	17%	0.3%	59.4% 51.7%
17	F	28 34		5	0.04	0.02	0.00	0.05	001	0.0	+	45% 12%	2.6%	0.5%	65% 10.7%	1.2%	100.0%	003 002 002 002	0.00		0.04	0.00	0.51	63.9% 65.7%	16% 24%	2.1%	0.4%	46%	05% 02%	63.9% 65.7%
19	Ŀ	35		Š	0.03	0.04	0.00	0.01	0.01	0.71		16%	5.5%	0.4%	1.4%	0.8%	100.0%	002 004	0.00	_	0.01	0.00	0.46	61.7%	31%	46%	0.3%	1.1%	0.4%	61.7%
20	F	36		5	0.01	0.02	0.00	0.05	001		_	11%	5.0% 2.9%	0.5%	11.2% 7.3%	1.7% 1.2%	100.0%		0.00		0.03	0.00	0.23	54.4% 61.1%	24%	41%	0.5%	67% 48%	10%	54.4% 61.1%
22	- 1	128		1	0.00	0.00	0.00	0.01	000			2.0%	2.0%	0.7% 0.6%	60% 3.8%	1.3%	100.0%	000 000			0.01	0.00	0.07	43.6% 41.7%	2.0%	1.3%	0.7%	4.0%	0.7%	41.6%
22 23 24 25 26 27	Ŀ	132		-	0.00	0.00	0.00	0.01	000	0.11		19%	1.3%	1.2%	39%	1.2% 0.6%	100.0%	000 000	0.00		0.00	0.00	0.07	48.1%	1.3%	06%	0.6%	2.6%	06%	41.7% 48.1%
25	H	134		1	0.00	0.00	0.00	0.00	000		-	2.8%	14%	0.7%	28%	0.7%	100.0%		0.00		000	0.00	0.06	43.4%	1.4%	07%	0.7%	21%	60%	41.4% 51.6%
27	- 1	138		2	0.00	0.00	0.00	0.02	0.00	0.2		10%	1.3%	1.3%	72% 34%	1.2%	1000%	001 000	0.00		0.01	0.00	0.09	37.4% 52.9%	2.1%	09%	13%	5.1% 2.2%	0.4%	17.4% 52.9%
29	- 1-	140		2	0.00	0.00	0.00	0.01	0.00		+	1.0%	1.8%	0.6%	29%	0.6%	100.0%	000 001	0.00		0.01	0.00	0.19	56.0%	12%	1.5%	0.3%	1.8%	0.3%	56.0%
30	F	141		2	0.00	0.00	0.00	0.02	001			24%	1.6%	0.8%	77%	2.0%	100.0%	001 000	0.00		0.01	0.00	0.12	49.4%	2.0%	12%	0.8%	57%	0.8%	49.4%
32 K P	asch .	147		2	0.00	0.00	0.00	0.01	000			22%	1.6%	0.3%	13%	1.1%	1000%	001 000			0.01	0.00	0.19	51.1% 50.0%	1.6%	1.1%	0.3%	24%	05%	\$1.1% \$0.0%
33	- 1-	146 152		5	0.00	0.00	0.00	0.01	0.00	0.4	+	1.7% 4.7%	1.7%	0.8% 2.6%	5.0% 17.6%	1.2%	100.0%	000 000	0.00		0.01	0.00	0.12	57.1%	3.4%	1.3%	2.1%	3.8% 9.9%	0.4%	57.1%
35	F	153		5	0.02	0.00	0.00	0.02	000			12%	2.2% 2.5%	0.5%	3.6% 2.5%	0.5%	100.0%	001 001	0.00		0.01	0.00	0.34	57.9% 56.0%	2.4%	19%	0.5%	2.0%	0.2%	57.9% 54.0%
3.7	E	155		5	0.02	0.00	0.00	0.03	001	0.7		2.4%	1.9%	0.2%	445	1.2%	100.0%	001 001	0.00		0.02	0.01	0.49	65.3%	1.9%	1.6%	0.1%	24%	0.7%	65.2%
38	- 1-	156		5	0.02	0.02	0.00	0.03	001	0.6	+	15%	12% 22%	0.6% 1.5%	43% 93%	1.4%	100.0%		0.00		0.02	0.00	0.36	57.3% 58.0%	2.9%	27% 17%	05%	13% 17%	0.6%	57.3% 58.0%
40	F	163		5	0.02	0.00	0.00	0.01	000	0.7		13%	1.9%	0.4%	12%	0.6%	100.0%	002 001 002 001	0.00		0.01	0.00	0.43	59.8% 59.9%	25%	18%	0.4%	13%	0.3%	59.8% 59.9%
42	Ŀ	165		5	0.02	0.02	0.00	0.04	003			25%	2.8%	0.3%	53%	2.6%	100.0%	001 001	0.00		0.02	0.01	0.10	61.6%	21%	2.3%	0.2%	34%	1.0%	61.6%
31	F	2	128	2 2	0.01	0.01	0.00	0.02	001		+=	2.3%	2.3%	0.6%	66%	1.4%	100.0%		0.00		0.02	0.00	0.16	44.8%	1.7%	20%	0.6%	58% 19%	0.6%	44.8% 40.4%
45	þ	4	132	2	0.00	0.00	0.00	0.03	000			21%	1.3%	0.5%	6.6%	0.8%	100.0%	001 000			0.02	0.00	0.16	42.8% 42.5%	1.8%	1.0%	05%	50%	0.3%	42.8% 42.5%
47	E	8	136	2	0.00	0.00	0.00	0.01	000	0.2		15%	1.8%	0.6%	425	0.3%	100.0%	000 001	0.00	\pm	0.01	0.00	0.16	40.5%	12%	15%	0.6%	14%	0.3%	40.5%
46	F	10	138	4	0.02	0.00	0.01	0.06	001	0.9	$\overline{}$	2.8%	2.1% 1.6%	1.4% 0.4%	10.7% 6.2%	0.9%	100.0%		0.01		0.03	0.00	0.28	47.8% 57.8%	22%	17%	12%	52% 34%	0.3%	47.8% 57.8%
50	E	12	140	4	0.02	0.02	0.00	0.05	001	0.0		2.4%	2.3%	0.3%	73%	1.4%	100.0%	001 001	0.00		0.03	0.00	0.36	55.3%	2.0%	1.0%	0.3%	46%	05%	55.3%
51 52	Ŀ	13	146	4	0.02	0.01	0.01	0.09	000	0.6		25% 25%	2.6%	0.9%	13.4% 5.9%	1.6%	100.0%	001 001	0.00		0.03	0.00	0.35	41.3% 51.1%	1.9%	13%	0.6%	41%	0.7%	41.3% 51.1%
53	F	19	147	4	0.02	0.02	0.00	0.03	0.01	0.6		25%	2.4% 2.7%	0.1%	50%	1.0%	100.0%	001 002	0.00		0.03	0.00	0.37	544% 40.7%	2.0%	23%	0.1%	37% 86%	08%	544% 49.7%
53 54 55 56 57	E	24	152	10	0.06	0.04	0.00	0.31	0.01	1.6		16%	2.1%	1.6%	11.6%	0.7%	100.0%	005 003	002		0.17	0.01	1.15	68.4%	2.7%	1.7%	13%	10.2%	0.3%	68.4%
56	F	25	153 154	10	0.07	0.06	0.00	0.05	0.01	1.9	ΗΞ	45% 42%	4.0%	0.4%	33% 31%	0.7% 0.8%	100.0%	005 005	0.00		0.03	0.01	1.06	66.5% 64.0%	13% 16%	13% 14%	0.3%	21% 25%	0.3%	66.5% 64.8%
58 59 60	F	27 28	155	10	0.05	0.05	0.00	0.14	601	1.6		3.2%	2.9%	0.3%	84%	1.7%	100.0%	004 004			0.06	0.02	0.96	59.6%	25%	25%	0.2%	47%	1.0%	59.6%
60	E	34	156 162	10	0.07	0.07	0.02	0.19	001			44% 18%	4.0% 3.4%	06% 12%	50% 13.9%	1.9%	100.0%	005 005	0.01		0.10	0.01	1.03	57.5% 70.5%	10%	13% 27%	1.0%	44% 58%	0.8%	57.5% 70.5%
62	F	35 36	163	10	0.06	0.07	0.01	0.03	002		+=	17%	41%	0.4%	20%	0.9% 1.2%	100.0%		0.00		0.03	0.01	0.89	66.0% 57.0%	2.8% 2.6%	3.3% 2.8%	0.4%	16%	0.4%	66.0% 57.0%
63		37	165	10	0.07	0.07	0.00	0.12	004	1.0		45%	4.1%	0.2%	7.6%	2.2%	100.0%		0.00		000	0.02	0.94	58.4%	16%	13%	0.2%	47%	69%	51.4%

- K-patch High CH

															max ratio ou	et of all beams													max ratio out of all	beams		
П								4cm2 F	PD(mW/c	m2)			LIN	4.0%	2.0%	17.1%	1.7%	100.0%	4	Kom2 PD(n	rW/cm2) a	at 10mm e	evaluation	n distance	o	72.4%	7.0%	2.0%	1.7%	9.6%	0.6%	72.4%
No.	Andule Type	Seam ID	J Bena D.	2 Feed no.			П	Т			Citan	per Seam	ratio	ratio	ratio	ratio	ratio	ntio								ratio	ratio	ratio	ratio	ratio	ratio	ratio
					54/Righ	() S3(Left)	\$5(To	p) (S6)	Bottom)	\$1(Front)	S2(Rear	Back-of	(Right 2mm)/(wonst- surface 2mm)	(Left 2mm)/(wonst- surface 2mm)	(Top 2mm(//wonst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	54(Right)	S3(Left)	SS(Top)	SS(Bott	ton) S1	(Front) S	S2(Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(worst- surface 2mm)	(Left 10mm)/(wonst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Sottom 10mm)/(worst surface 2mm)	(Front 10mm)/(wonst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
1		0		1	0.00	0.00	0.00		0.01	000	0.19	-	12% 27%	1.6%	0.5%	48%	0.5%	100.0%	001	0.00	0.00	0.01		0.00	0.09	45.8% 47.9%	27%	11%	0.5%	17% 59%	05%	46.8% 47.9%
2 3 4 5 6 7 8 9 10 11 12		4		i	0.00	0.00	0.00		0.00	600	0.20		25%	1.0%	0.5%	5.9%	0.5%	100.0%	000	000		0.01	0 1	0.00	0.10	50.0%	2.0%	10%	0.5%	45%	90%	50.0%
5		- 6	+	1	0.00	0.00	0.00	+	0.01	000	0.18	+	2.8%	1.1%	0.5%	45% 32%	0.0%	100.0%	000	0.00	0.00	0.01		0.00	0.09	49.7%	22% 16%	1.1%	0.6%	2.8%	00%	49.7% 47.4%
6		10 11		2	0.02	0.00	0.00		0.04	000	0.39		19%	1.8%	0.8%	11.1% 46%	0.3%	100.0%	001	001	0.00	0.03		0.00	0.20	\$1.2% \$1.4%	21% 24%	15%	0.8%	67% 27%	0.3%	\$1.3% \$1.4%
á		12		2	0.02	0.00	0.00		0.02	600	0.34		44%	1.7%	0.3%	55%	12%	100.0%	001	0.01	0.00	0.01	0 1	0.00	0.22	63.1%	32% 17%	15%	03%	38%	0.6%	63.1%
10		13		2	000		0.00		300	000	0.41	+	22%	1.0%	0.7%	13.8%	0.7%	100.0%	001	000	0.00	0.04		0.00	0.16	38.2% 54.6%	1.7%	0.7%	0.5%	96% 19%	0.3%	38.2% 54.6%
11		19		2	0.02		0.00		0.01	000	0.36	-	47% 10%	1.7%	0.3%	19%	0.3% 1.1%	100.0%	001	0.01	0.00	0.01		0.00	0.25	68.0% 53.3%	16% 25%	14%	02%	1.4%	00% 05%	68.0% 53.2%
13		24		5	0.02		0.02		0.14	000	0.03		2.9%	1.0%	1.0%	17.1%	0.5%	100.0%	002		0.00	0.07		0.00	0.57	68.8%	23%	1.4%	14%	8.9%	0.2%	63.0%
15		25		5	0.07		0.00	+	0.02	000	0.78	+	7.3%	3.5% 3.8%	0.3%	1.8%	0.4%	100.0%	005	003	0.00	0.01		0.00	0.53	70.9%	5.5% 5.9%	2.8% 3.2%	0.3%	1.1%	0.2%	70.9% 68.1%
14 15 16 17		27		5	0.07		0.00		500 700	001	0.74	₽	88% 45%	14%	0.1%	43% 89%	0.8% 1.3%	100.0%	005	0.02	0.00	0.02		000	0.47	63.2% 66.0%	7.0% 14%	2.8%	0.1%	2.4%	0.3% 0.5%	63.2% 66.0%
18		34	$\overline{}$	3	0.03	0.02	0.01	_	300	001	0.83		35% 78%	28%	12%	6.7%	0.6%	1000%	0.02	002	0.00	0.03	3 1	000	0.59	71.4% 69.8%	26%	22% 24%	1.1%	31%	02%	71.4% 69.8%
20		36		5	0.06	0.03	0.00	+	0.03	000	0.70	+	82%	3.7%	0.1%	0.9% 4.0%	0.7%	100.0%	005	0.02	0.00	0.01	2 1	0.00	0.47	67.2%	65%	13%	0.1%	23%	0.3%	67.2%
21		37 128	_	5	0.05	0.02	0.00	-	0.03	0.01	0.77	-	19%	2.9%	0.4%	43% 83%	1.2%	100.0%	0.04	0.02	0.00	0.02		000	0.51	66.1% 38.5%	48% 19%	2.3%	0.4%	31% 58%	0.4% 0.6%	66.1% 38.5%
18 19 20 21 22 23 24 25 26 27 28		130			0.00		0.00		0.01	000	0.20		1.0%	1.0%	0.5% 1.0%	5.1% 5.2%	1.0%	100.0%	000		0.00	0.01	0 1	000	0.00	41.3% 40.6%	1.0%	10%	05%	31% 43%	05%	41.3% 42.6%
25		134	_	++	0.00	0.00	0.00		0.01	000	0.19	-	1.1%	1.1%	0.5%	32%	0.5%	100.0%	000	0.00		0.00	0 1	0.00	0.07	37.3%	1.1%	05%	0.5%	22%	0.0%	37.3%
26		136	-	1 2	0.00	0.00	0.00	-	0.00	000	0.15	-	14%	0.7%	0.7%	2.1% 7.2%	0.0%	100.0%	000	0.00	0.00	0.00		0.00	0.07	50.7% A4.5%	14%	0.7%	0.7%	14%	0.0%	50.7% 44.9%
28		139		2	0.00	0.01	0.00		0.01	000	0.32	=	19%	1.9%	0.3%	28% 28%	1.2%	100.0%	001	000	0.00	0.01		000	0.16	\$1.2% \$4.0%	16%	13%	03%	25%	0.3%	51.3% 54.9%
30		141	_	2	0.00	0.00	0.00	_	0.04	0.00	0.35		16%	0.8%	0.8%	12.0%	1.1%	100.0%	000	0.00	0.00	0.03	3 1	0.00	0.16	42.7%	1.1%	05%	0.5%	73%	0.3%	42.2%
31	K Page	146		2	0.00	0.00	0.00	+	10.0	000	0.33	+	21%	12%	0.3%	21%	0.3%	1000%	001	000	0.00	0.00		0.00	0.20	59.2% 51.5%	15%	09% 12%	0.3%	12%	0.3%	59.2% 51.5%
32 33 34		146 152		2	0.00		0.00		0.02	0.00	0.22		1.0%	0.9%	0.9%	46% 11.7%	0.5%	100.0%	001	000	0.00			0.00	0.15	45.1% 62.9%	1.5%	06% 12%	0.9%	37% 57%	0.3%	45.1% 62.9%
35 36		151		ŝ	0.02	0.02	0.00		0.02	000	0.00		25%	1.9%	0.3%	2.4%	0.2%	100.0%	002	001	0.00	0.01	0 1	0.00	0.51	58.2%	22%	1.6%	0.2%	13%	0.2%	58.2%
3.7		154		5	0.03	0.02	0.00		200	000	0.68	+	38% 27%	16% 21%	0.4%	28%	0.4% 1.5%	100.0%	002	0.02	0.00	0.01		0.00	0.37	55.0% 61.1%	28%	2.4%	0.3%	21%	0.1%	55.0% 61.1%
38		156 162		5	0.03	0.02	0.00		300	001	0.87		14%	2.1%	0.3% 1.2%	9.8% 62%	0.7%	100.0%	002	001	0.00	0.07		0.00	0.53	61.2% 62.4%	2.6% 2.6%	1.6%	0.2%	8.0% 3.6%	0.3%	61.3% 62.4%
40		163		Š	0.03	0.02	0.00		0.02	600	0.75		3.4%	2.5%	0.4%	2.4%	0.4%	100.0%	0.02	0.01	0.00	0.02	2 1	0.00	0.45	63.9%	25%	19%	0.4%	2.0%	0.1%	60.9%
41		164 165		5	0.02				0.02	001	0.65	+	2.0%	4.1%	0.9%	2.6% 4.0%	0.9% 1.0%	100.0%	001	0.02	0.00			0.00	0.59	56.0% 59.8%	2.1%	2.9%	0.8%	1.8%	0.3%	56.0% 59.8%
38 39 40 41 42 43 44 45 46 47		0		2	0.00	0.01	0.00		0.03	001	0.38	\mathbf{I}	11%	1.6%	0.5% 0.5%	65% 93%	1.6%	100.0%	001	0.01	0.00	0.02		000	0.16	42.2% #4.1%	2.6%	1.3%	0.5%	55% 51%	05%	42.2% #4.1%
45		4	132	2	0.00	0.00	0.00	Н	0.03	000	0.46		2.2%	1.1%	0.7%	7.4%	0.4%	100.0%	001	000	0.00	0.03	3	000	0.20	43.1%	15%	09%	0.7%	6.1%	0.2%	43.1%
46		- 6	136		0.00		0.00		0.02	000	0.37		25% 19%	1.8%	0.5%	43% 38%	0.5%	100.0%	001	0.01	0.00		9	0.00	0.18	44.2% 46.9%	18%	1.0%	0.5%	10%	0.3%	44.2% 46.9%
45 49		10	135	4	0.03	0.01	0.01		0.11	000	0.78	₽	12%	1.7%	1.2%	13.8% 5.2%	0.5% 0.8%	100.0%	0.02	0.01	001	0.07		000	0.40	\$1.0% \$8.2%	2.6%	14%	1.0%	2.4% 2.6%	0.3%	\$1.0% \$8.2%
50 51		12	140	4	0.03	0.02	0.00		0.04	0.01	0.75		19%	2.1%	0.3%	5.0%	0.9%	100.0%	0.02	001	0.00	0.03	3 1	0.00	0.42	56.1%	2.9%	1.6%	0.3%	41%	0.4%	56.1%
52		13	146	4	0.02	0.01	0.01		0.10	600	0.72		2.5%	1.6%	1.0%	11.9% 5.5%	12%	100.0%	002		0.01	0.07	3	000	0.42	43.4%	1.0%	1.0%	0.7%	8.7% 3.6%	0.5%	43.4%
53 54		19	147	4	0.03	0.02	0.00		0.02	0.01	0.72	F	45% 26%	2.5%	0.1%	32% 89%	1.1%	100.0%	003	0.01	0.00	0.02		0.00	0.41	57.8% 49.4%	15% 21%	18%	0.1%	22% 61%	0.4%	57.8% 49.4%
55		24	152	10	0.07	0.04	0.04	_	0.32	0.01	1.98		3.3%	1.9%	2.0%	16.0%	0.6%	100.0%	005	0.03	003	0.17	7 1	0.00	1.16	68.9%	23%	1.6%	1.7%	8.6%	0.2%	68.9%
55 56 57 58		25	153		0.10		0.01		0.04	001	1.51		48% 87%	3.2% 4.1%	0.5%	20%	0.6%	100.0%	010	005	0.01	0.04	4 1	0.00	0.94	68.2% 61.8%	16% 67%	2.6% 3.2%	0.4%	12%	0.3%	68.2% 61.8%
58 59		27	155 156	10	0.10	0.06	0.01		0.09	003	1.82	F	54% 19%	14%	0.3%	52% 88%	14%	100.0%	0.05	0.05	0.00	0.05		0.01	1.11	61.0% 61.2%	44%	2.8%	0.3%	28%	05% 05%	61.0% 63.2%
60		34		10	0.07	0.05	0.00	_	0.15	001	1.95	-	18%	25%	14%	7.4% 1.5%	06%	100.0%	005	0.04	0.02		9 1	0.01	1.42	72.4%	27%	19%	12%	46%	0.3%	72.4%
62		36	164	10	0.09	0.08	0.00	+	30.0	0.02			5.6%	4.0%	06%	38%	1.0%	100.0%	0.07	0.06	0.00	0.03	3 1	0.01	0.98	62.6%	43%	18%	0.5%	1.7%	0.4%	60.6%
63		37	165	10	0.09	0.07	0.00		0.12	0.04	2.09		4.1%	12%	0.3%	5.9%	1.7%	100.0%	007	0.05	0.00	0.09	0 1	0.01	1.25	59.7%	12%	25%	0.2%	41%	0.6%	59.7%

[Folder Closed Status]

- K-patch Low CH

															max ratio ou	t of all beams			l									max ratio out of all I	bearts		
П								4cm2 PD	D)mW/on	n2)			11.2%	45.8%	2.6%	19.7%	2.0%	100.0%	40	m2 PD(m)	W/cm2) a	t 10mm evalu	uation dista	nce	62.2%	6.9%	29.6%	2.3%	12.4%	12%	62.2%
No. M	odule Typ	e Seam ID_1	Sema ID,	2 Feed no.				Т				per Beam	ratio	ratio	ratio	ratio	ratio	ratio							ratio	ratio	ntio	ratio	ratio	ratio	ratio
1 1			1		S4/Righ	t) S3(Left)	SS(Top	p) S6(8a	ottom)	\$1(Front)	S2(Rear)	Back-off	(Right 2mm)/(worst- surface 2mm)	(Left 2mm)/(wonst- surface 2mm)	(Top 2mm)/(wonst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Forst 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	S4(Right)	S3(Left)	SS(Top)	SS(Bottom)	S1(Front)	S2(Rear)	wont-surface (10mm/2mm)	(Right 10mm)/(wont- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Bottom 10mm)/(worst surface 2mm)	(Front 10mm(/(worst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
1	_			1	0.00	0.04	0.00	0.0	.01	000	0.16	(d0)	1.9%	27.7%	0.6%	75%	0.6%	100.0%	000	0.02	0.00	0.01	0.00	0.06	25.0%	1.3%	13.2%	0.6%	50%	06%	25.0%
2		2		1	0.00	0.05	0.00			000	0.19		15%	24.2% 26.0%	0.5%	62% 59%	0.5%	100.0%	000	003		0.01	0.00	0.09	44.3% 42.0%	1.0%	13.4%	0.5%	16% 41%	05%	44.3% 42.0%
4		- 6	_	+ ;	0.00	0.06	0.00			000	0.17		24%	28.0%	0.5%	385	0.5%	1000%	000			0.01	0.00	0.00	45.2%	24%	15.5%	0.6%	10%	95%	45.2%
5		8 10		1 2	0.00	0.04	0.00			000	0.15		27%	24.3% 29.7%	0.0%	47% 58%	0.7%	100.0%	000			0.01	0.00	0.06	41.2% 41.9%	2.0%	13.5%	0.0%	41%	00%	41.2% 48.9%
7		11	_	2	0.01	0.12	0.00		02	000	0.41		2.2%	34.0%	0.2%	425	1.0%	1000%	901	010	0.00	0.02	0.00	0.26	544%	1.7%	20.0%	0.5%	21%	0.2%	48.9% 54.4%
8		12		2	0.00	0.10	0.00			000	0.29		1.0%	34.4% 22.7%	0.4%	95%	1.1%	100.0%	000	005	0.00	0.02	0.00	0.14	48.1%	1.4%	18.9%	0.4%	63%	0.7%	48.1%
10		10		2	0.00	0.11	0.00	0.0	02	000	0.39		16%	28.1%	0.5%	53%	0.8%	100.0%	001	0.06	0.00	0.02	0.00	0.15	45.9%	31%	15.1%	0.3%	41%	05%	45.9%
11		19		2	0.00	0.14	0.00	0.0		000	0.39		2.3%	36.0% 26.7%	0.0%	12.8%	0.8%	100.0%	001	0.09	0.00	0.00	0.00	0.22	56.6% 44.9%	1.8%	21.7%	0.0%	91%	0.3%	56.6% 44.9%
13		24		ŝ	0.04	0.33		0.1	15	002	1.11		16%	29.6%	0.0%	13.4%	1.4%	100.0%		018	0.00	0.09	0.01	0.62	55.7%	2.7%	16.1%	0.5%	8.0%	0.7%	55.7%
14		25			0.03		0.00	0.0		002	1.03		12% 12%	42.9% 29.1%	0.2%	15% 12%	1.5% 1.2%	100.0%		0.29		0.01	0.01	0.63	61.1% 59.1%	2.2% 2.5%	27.8% 25.9%	0.2%	0.9%	0.8% 0.6%	61.1% 59.1%
16		27		ŝ	0.02	0.26	0.00	0.1	03	000	0.62		2.6%	41.4%	0.2%	53%	0.6%	100.0%	001	017	0.00	0.02	0.00	0.35	54.9%	21%	28.1%	0.2%	16%	0.3%	54.9%
5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20		28 34	-	5	0.04	0.20		0.1	12	001	1.10		6.1% 4.4%	33.9% 31.9%	0.0%	8.3% 10.1%	0.8%	100.0%	003	0.12	0.00	0.04	0.00	0.38	57.2% 57.2%	45% 31%	18.0%	0.5%	53%	05% 0.7%	57.2% 57.2%
19		35		Š	0.03	0.42	0.00	0.1	.01	0.02	0.95		3.2%	44.4%	0.4%	0.7%	1.7%	100.0%	002	0.28	0.00	0.01	0.01	0.57	59.6%	22%	29.6%	0.3%	0.5%	0.9%	59.6%
20		36	-	5	0.03	0.34	0.00	0.0		001	0.90		16%	38.2% 34.4%	0.1%	0.7%	0.7% 1.4%	100.0%	003	0.23	0.00	0.00	0.00	0.55	61.0% 52.7%	29%	25.7%	0.1%	0.3% 8.7%	0.3%	61.0% 52.7%
21 22 23 24 25 26 27 28		126		1	0.00	0.04	0.00	0.1		000	0.15		14%	25.0%	0.7%	7.4%	14%	100.0%	000	0.02	0.00	0.01	0.00	0.06	40.5% 47.6%	2.0%	14.2%	0.7%	47%	0.7%	40.5%
23		130	-	1	0.00	0.03	0.00			000	0.15	_	28%	23.4%	0.7%	34% 35%	0.7%	100.0%	000		0.00	0.00	0.00	0.07	47.6% 47.2%	21%	11.7%	0.7%	2.8%	0.7%	47.0% 47.2%
25		134		1	0.00	0.03	0.00	- GI	.01	000	0.12		4.1%	23.6%	0.8%	4.1%	0.8%	100.0%	000	0.02	000	0.00	0.00	0.06	43.6%	24%	13.8%	0.8%	2.4%	0.0%	49.6%
26		136	-	1 2	0.00	0.03	0.00			000	0.12	-	35% 7.3%	27.8% 29.2%	1.7%	26% 7.3%	1.7%	100.0%	000	0.02	0.00	0.00	0.00	0.05	44.3% 37.6%	1.7%	15.7%	12%	1.7% 51%	1.1%	44.2% 37.6%
28		139		2	0.00	0.09		- ai	.01	000	0.20		2.4%	24.5%	0.3%	32%	0.8%	100.0%	001	005	0.00	0.01	0.00	0.19	50.9% 55.7%	1.8%	13.2%	0.0%	2.1%	05%	50.9%
30		140	-	2	000	0.06	0.00	01	.02	000	0.34		2.4%	24.1% 28.0%	1.0%	3.3% 85%	0.9%	100.0%	001	003	0.00	0.01	0.00	0.19	55.7% 43.5%	1.8% 3.0%	14.0%	0.3% 1.0%	2.1% 7.0%	0.3% 0.5%	55.7% 43.5%
31		146		2	000	0.07	0.00			000	0.23		15%	28.8%	0.9%	3.1%	0.9%	100.0%		0.04	0.00	0.01	0.00	0.10	45.1%	2.7% 1.5%	16.8%	0.9%	2.7%	0.4%	45.1%
32	X Pas	th 147 146	-	2	0.01	0.10	0.00			000	0.40		2.3% 7.1%	25.0% 28.9%	0.0%	35% 61%	0.8%	100.0%	001	005	0.00	0.01	0.00	0.10	50.0% 51.3%	15%	13.4%	0.0%	25% 16%	05% 05%	50.0% \$1.3%
32 33 34 35 36 37		152		5	0.03	0.13				0.01	0.35		7.4% 1.2%	23% 23%	2.0%	13.7% 2.4%	1.4%	100.0%	002	000	0.00	0.05	0.00	0.18	52.3% 55.5%	49%	16.3%	23%	13.4%	0.9%	52.3% 55.5%
36		154	_	5	0.04			0.0		000	0.94	-	40%	30.7%	0.2%	20%	1.1%	100.0%	001			0.01	0.01	0.54	57.8%	2.8%	20.5%	0.2%	1.5%	0.5%	57.8%
37		155		5	0.03	0.21	0.00			0.01	0.76		16%	27.0% 35.7%	0.7%	63% 72%	12%	100.0%	002	0.13	0.00	0.03	0.01	0.43	57.0% 54.0%	10%	17.5% 22.2%	0.1%	41%	0.7% 0.7%	57.0% SAII%
39 40		162	_	5	0.03	0.12	0.01	0.1	.04	001	0.38	-	65%	32.1%	1.6%	10.7%	1.6%	100.0%	002	0.07	0.01	0.02	0.00	0.19	50.1%	47%	17.8%	13%	6.3%	0.8%	50.1%
40		163		5	0.02	0.79	0.00			601	0.66		16%	29.1% 28.9%	0.0%	185	1.1%	100.0%	002	0.12	0.00	0.01	0.00	0.37	55.7% 55.7%	2.6%	18.5%	0.6%	12%	06%	55.7% 55.7%
42		165		ŝ	0.03	0.16	0.00	a)	.04	001	0.54		47%	29.1%	0.2%	7.2%	0.9%	100.0%	002	0.10	0.00	0.02	0.00	0.32	60.1%	14%	19.2%	0.2%	43%	0.7%	60.1%
43		0	128		0.00	0.10				000	0.35	H	2.0%	28.7%	0.6%	69% 59%	1.1%	100.0%		005	0.00	0.02	0.00	0.13	36.5% 45.8%	14%	15.5%	0.6%	52% 19%	06%	36.5% 45.8%
45		- 4	132	2	0.00	0.13	0.00	ä		000	0.40		25%	31.3%	0.5%	4.0%	1.0%	100.0%	001	000		0.01	0.00	0.16	43.1%	1.0%	15.8%	0.5%	15%	05%	43.1%
46		- 6	134	2	0.00	0.09	0.00	0.0	02	000	0.33	_	2.4% 2.2%	26.9% 27.0%	0.6%	49%	0.9%	100.0%	001	0.05	0.00	0.01	0.00	0.14	41.2% 34.6%	2.4%	14.4%	0.3%	37% 31%	0.6%	41.2% 34.6%
46		10	135		0.02	0.79				001	0.55		16%	34.4%	1.3%	89%	1.3%	100.0%	002		0.00		0.00	0.29	52.0%	2.7%	19.5%	1.1%	5.3%	0.7%	52.0%
49		11	129		0.02	0.27				601	0.85		2.6% 2.2%	32.0% 28.6%	0.2%	4.1% 7.0%	13%	100.0%	002	016	0.00	0.03	0.01	0.45	52.7% 58.9%	1.6%	16.3%	0.1%	10%	0.7% 0.6%	52.7% 51.9%
51		13	141	- 4	0.02	0.21	0.01	Q1	.07	001	0.67		3.1%	31.3%	1.0%	9.9%	12%	100.0%	002	012	0.00	0.04	0.01	0.21	31.9%	22%	18.6%	0.7%	6.6%	0.7%	31.9%
52		18	146		0.02					601	0.71		21%	31.2% 32.7%	0.7%	58% 36%	1.0%	100.0%		012	0.00	0.03	0.00	0.32	45.0%	24%	16.9%	0.6%	19%	05%	45.0%
54		20	148	- 4	0.02	0.36	0.00	0.0	30	0.01	0.43		5.1%	38.1%	0.7%	12.0%	1.4%	100.0%	001	0.10	000	0.04	0.00	0.22	50.9%	33%	22.1%	0.7%	9.1%	09%	50.9%
41 42 43 44 45 46 47 48 49 50 51 51 52 53 54 55		24	152	10	0.08		0.02			003	1.66	-	50% 45%	42.0% 43.1%	13%	16.7% 2.1%	2.0%	100.0%	006		0.02	0.16	0.02	0.97	58.1% 62.2%	17% 13%	24.3% 27.3%	1.1%	9.7%	11%	58.1% 62.2%
57		26	154	10	0.09	0.70	0.00	Q1	.04	0.04	1.98		4.3%	35.5%	0.4%	1.0%	1.0%	100.0%	006	0.46	0.00	0.03	0.02	1.20	60.6%	31%	23.3%	0.4%	1.3%	1.0%	62.6%
58		27	155	10	0.05	0.65	0.00	01		002	1.75	_	2.8%	36.9% 41.5%	0.2%	5.1% 6.4%	1.1%	100.0%	004	0.42	0.00	90.0	0.01	0.00	59.4% 50.5%	2.3% 40%	24.2% 24.9%	0.2%	12% 46%	06%	59.4% 50.5%
60		34	162		0.10				20	003	1.78		5.3%	45.8%	0.9%	11.4%	1.8%	100.0%	007	050	001	0.11	0.02	1.06	59.1%	3.8%	28.1%	0.7%	63%	1.0%	59.1%
61		35	163		0.00					004	1.72	⊨	48% 19%	41.5% 35.9%	05%	17%	2.0%	100.0%		0.49	0.00	0.02	0.02	1.06	\$1.4% \$9.1%	34% 31%	28.7%	0.6%	12%	12% 07%	61.4% 59.1%
63		37	165	10						002	1.47		4.1%	29.5%	0.2%	12.4%	12%	100.0%				0.09		0.82	55.8%	2.9%	24.7%	0.2%	6.4%	0.8%	55.8%

- K-patch Mid CH

															max ratio ou	at of all beams													max ratio out of all	beams		
								4cm2 P	D(mW/o	m2)			6.1%	29.1%	2.2%	17.2%	1.9%	100.0%	4	Kom2 PD(n	rW/cm2) a	at 10mm e	evaluation	distance		70.2%	\$3%	26.9%	1.0%	9.9%	1.2%	70.2%
No.	Module Typ	e Beam D	D_1 Sema ID,	2 Feed no.				Т				per Beam	ratio	ratio	ratio	ratio	ratio	ntio								ratio	ratio	ratio	ratio	ratio	ratio	ratio
					54/Righ	s) S3(Left)	\$5(7a)	p) SB(I	Bottom)	\$1(Front)	S2(Rear	Back-of	(Right 2mm)/(wonst- surface 2mm)	(Left 2mm)/(worst- surface 2mm)	(Top 2mm)/(wonst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	S4(Right)	S3(Left)	SS(Top)	SS/Both	ton) 51	Front) 52(nt-surface nm/2mm)	(Right 10mm)/(wonst- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Bottom 10mm(/(wont) surface 2mm)	(Front 10mm(/(worst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
1		0		1	0.00		0.00		0.01	0.00	0.15	(0.00)	2.6%	23.8%	0.7%	60%	0.7%	100.0%	0.00		0.00	0.01		200 0		41.0%	2.0%	12.6%	0.7%	40%	0.7%	41.0%
3		4	+-	1	0.00		0.00		0.01	000	0.16	+	1.9%	23.3%	0.5%	8.8% 8.2%	1.1%	100.0%	000	0.02	0.00	0.01		200 0	.00	22.6% 42.9%	1.5%	13.8%	0.5%	3.8% 6.0%	05%	29.6% 42.9%
4		6	_	1	0.00	0.04	0.00		0.01	0.00	0.14	-	2.0%	27.1% 18.9%	0.7%	5.6% 4.9%	1.4%	100.0%	000	0.02	0.00	0.01		100 0		46.5% 41.5%	21% 12%	15.3% 8.5%	0.0%	15% 17%	0.7% 0.0%	46.5% 41.5%
2 3 4 5 6 7 8 9 10 11 12		10		2	0.01		0.00		0.03	000	0.37		2.4%	27.7% 31.8%	0.8%	7.9%	0.8%	100.0%	001	0.06	0.00	0.01	0 (100 0	:10	49.5%	1.9%	16.6%	0.5%	18% 13%	05% 08%	49.5% 59.1%
4		11		2	0.00	0.06	0.00		2.03	0.00	0.24		2.9%	26.9%	0.4%	12.9%	0.8%	100.0%	001	0.04	0.00	0.02	2 1	2.00	:14	50.4%	21%	16.0%	0.4%	7.6%	0.4%	58.4%
10		13		2	0.01		0.00		0.05	000	0.37	+	25%	22.2% 24.1%	0.5%	14.2% 6.8%	1.1% 0.8%	100.0%	001	0.04	0.00	0.03		100 0		40.5% 40.8%	22% 1.9%	11.6%	0.8%	7.6% 4.7%	05% 05%	40.5% 40.8%
11		19		2	0.01		0.00		0.01	0.00	0.27		41%	32.6% 22.3%	0.0%	52% 10.8%	1.5%	100.0%	001	006	0.00	0.01		100 0		58.1% 50.7%	3.3% 1.8%	21.1%	0.0%	3.0% 7.9%	07% 07%	58.1% 50.7%
13		24		5	0.04	0.26	0.00		0.16	001	0.96		41%	26.8%	1.1%	16.2%	1.4%	100.0%	003	0.16	0.00	0.09	9	201 0	63	65.6%	10%	17.0%	0.9%	9.1%	0.7%	65.6%
14		25		5	0.04		0.00		0.01	0.02	0.63	+	43%	31.6%	0.5%	0.8% 2.6%	1.9%	100.0%	003	0.23	0.00	0.01		201 0		60.9%	16%	26.9%	0.1%	1.6%	1.3%	64.4%
14 15 16 17		27		5	0.02		0.00		0.06	001	0.17		45% 47%	36.4%	05% 05%	17.1% 5.8%	1.9%	1000%	001	0.09	0.00	0.04		101 0	20	53.5% 65.5%	17% 17%	24.3% 17.0%	0.5%	9.9%	1.3%	\$1.5% 65.5%
18		34		ŝ	0.03	0.30	0.01		0.09	0.01	1.00		3.4%	32.4%	0.8%	9.4%	1.2%	100.0%	0.03	0.20	0.00	0.05	5 1	2.01	65	65.5%	2.7%	20.4%	0.7%	51%	0.7%	65.5%
19		35		5	0.03	0.29	0.00		0.01	001	0.78	+	43%	36.9% 17.9%	0.4%	14%	1.7% 1.4%	100.0%	003	0.21	0.00	0.01		201 0		61.0% 54.7%	16% 11%	26.5%	0.3%	62%	12% 07%	61.0% 54.7%
21		37 128		5	0.04	0.79	0.00		0.04	600	0.64		57% 26%	29.2% 17.2%	0.2%	66%	0.6%	100.0%	003	0.11	0.00	0.03		200 0		62.1% 41.0%	44% 20%	17.6% 86%	0.2%	41% 46%	0.3% 0.7%	62.1% 43.0%
23		130		i	0.00		0.00		0.01	0.00	0.16		1.9%	19.2%	0.6%	37%	0.6%	100.0%	000	0.02		0.00	0 1	2.00	.07	41.0%	1.9%	12%	0.0%	25%	96%	41.0%
18 19 20 21 22 23 24 25 26 27 28 29		132		1	0.00	0.03	0.00		0.00	000	0.16	+	32% 28%	15.9% 20.7%	0.0%	3.8% 2.8%	0.6%	100.0%	000	0.01	0.00	0.01		100 0		47.1% 42.1%	1.9%	8.3% 11.0%	0.6%	32% 21%	06% 07%	47.1% 42.1%
26		136		1 2	0.00	0.02	0.00		0.00	0.00	0.13		1.6%	17.8% 18.1%	0.8%	3.1% 7.2%	0.8%	100.0%	000	0.01	0.00	0.00		100 0	07	51.2% 35.9%	1.6%	10.9%	0.8%	23%	0.8%	51.2% 15.9%
28		129	_	2	0.00	0.08	0.00		0.01	0.00	0.36		25%	23.3%	0.3% 0.6%	3.1%	0.0%	100.0%	001	0.04	0.00	0.01	0 1	200 0	10	50.6% 54.6%	22%	11.9%	0.3%	25%	03%	50.6% G/ 0%
30		140		2	0.01	0.08			0.01	000	0.26	+	15%	20.4%	0.8%	32% 82%	0.8%	100.0%	001		0.00		2 1	200 0	12	45.9%	1.7%	10.6%	0.3%	1.4%	04%	45.9%
31	v 0	146 th 147		2	0.00	0.07	0.00		0.01	0.00	0.29		27%	25.0% 23.3%	0.7%	24% 33%	0.7%	1000%	001	0.04	0.00	0.01		200 0		49.0% 48.5%	2.4% 2.2%	14.2%	0.7%	1.7%	0.3%	49.0% 48.5%
32 33 34		146		2	0.00		0.00		0.01	0.00	0.24		10%	20.3%	0.8%	5.1%	0.4%	100.0%	000	003	0.00			200 0	:12	50.0%	1.7%	11.0%	0.8%	42%	0.4%	50.8%
34 35 36		151	_	5	0.03	0.08	0.01		0.08	001	0.49	+	17%	16.1% 24.5%	0.7%	16.1% 2.9%	1.0%	100.0%	003	0.05	0.00	0.05		200 0	.22	58.7% 56.4%	5.3% 2.7%	10.2%	1.8%	9.4%	06% 07%	58.7% 56.4%
36		154		5	0.04		0.00		0.02	0.01	0.87	-	44%	29.4% 26.2%	0.3%	24% 42%	1.1%	100.0%	003	0.17	0.00	0.02	2 1	201 0		52.9% 64.8%	16% 21%	20.0%	0.3%	1.7%	0.7% 0.4%	52.9% 64.8%
36		156		5	0.03	0.79	0.00		2.03	0.01	0.61		5.6%	33.9%	0.5%	53%	1.6%	100.0%	0.02	0.12	0.00	0.02	2 1	101 0	35	57.6% 57.4%	3.3%	19.5%	0.3%	19%	1.0%	57.6% 57.4%
40		163		5	0.03	0.20	0.00		0.04 0.01	001	0.55		45% 42%	21.2% 27.9%	1.4%	7.6%	1.1% 0.7%	100.0%	0.02		0.00		0 1	200 0	.41	57.4%	42% 29%	13.0%	0.4%	42% 14%	05% 04%	57.4%
41		164		5	0.03				0.03	001	0.82	-	18%	28.8% 26.0%	0.7%	33% 63%	0.7% 1.2%	100.0%	003	0.16	0.00	0.02		100 0		57.4% 61.6%	12% 10%	19.2%	0.6%	2.4%	0.4%	57.4% 61.6%
37 38 39 40 41 42 43 44 45 46		0	128	2	0.00		000		0.02	000	0.34		2.6%	23.0%	0.6%	67%	0.9%	100.0%	001	0.05	0.00	0.02		200 0	:15	44.5% 31.9%	2.0%	13.7%	0.6%	55% 13%	06% 05%	44.5% 38.9%
45		- 4	132	2	0.00	0.00	0.00		203	000	0.39		22% 34%	20.9%	0.5% 0.5%	70%	1.0%	100.0%	001	0.04	0.00	0.02	2	200 0	16	42.4%	21%	10.3%	0.5%	54%	05%	42.4%
46		- 6			0.01		0.00		0.01 0.01	000	0.33	+	2.8%	26.9% 24.6%	0.0%	40% 43%	1.5%	100.0%	001		0.00			200 0		43.4% 41.0%	2.1% 1.2%	15.6%	0.6%	2.8% 3.3%	0.9%	43.4% 41.0%
45 49		10	138	4	0.03	0.16	0.01		0.06	001	0.55		45%	28.0% 26.7%	1.2%	10.2% 5.7%	0.9% 1.5%	100.0%	0.02	0.10	001	0.03		200 0		50.0%	14% 24%	10.1%	1.1%	6.0% 3.2%	05%	50.0% 57.0%
50		12	140	4	0.02	0.20	0.00		0.05	001	0.66		2.9%	30.3%	0.5%	6.8%	0.8%	100.0%	0.02	0.12	0.00	0.03	3 1	200 0	.27	55.4%	24%	18.8%	0.3%	19%	0.5%	55.4%
51 52		13	141	4	0.03	0.19	0.01		0.06 0.04	001	0.69	+	17% 27%	26.9% 29.4%	0.7%	12.0%	1.0%	100.0%	002	0.10	0.00	0.05		200 0		40.3% 51.0%	2.0%	13.8%	0.7%	72%	06% 07%	40.3% 51.0%
53 54		19	147	4	0.02	0.17	0.00		0.03	001	0.69		29%	25.1%	0.1%	49%	15%	100.0%	002	0.11	0.00	0.02		201 0	.27	53.4% 50.2%	2.5% 2.8%	16.1%	0.1%	15% 70%	09% 06%	51.4% 50.2%
55		24	152	10	0.29		0.00	_	0.29	0.02	1.66		5.4%	31.9%	1.6%	17.2%	1.4%	100.0%	008	0.33	002	0.16	c 1	201	.14	68.6%	45%	20.0%	1.3%	9.4%	0.8%	68.6%
55 56 57 58		25	153	10	0.08		0.01		0.04	002	1.57	+	5.3% 5.3%	35.2% 36.9%	05%	24%	15%	100.0%	006	0.37	0.01	0.02		102		67.6%	40%	23.5%	0.4%	13%	10%	67.6% 65.1%
58 59		27	155	10	0.06		0.01		0.13	0.02	1.61		18%	30.2% 29.1%	0.4%	8.1% 5.9%	1.0%	100.0%	0.05	0.33	0.00	0.07	σ .	101 0 102 1	.94	58.5% 58.7%	10%	20.3%	0.3%	45% 45%	06%	51.5% 51.7%
60		34	162	10	0.07	0.06	0.02	_	0.17	0.03	1.71		41%	38.7%	12%	9.9%	1.6%	100.0%	0.06	0.44	0.02	0.00	6 1	102	20	70.2%	3.3%	25.4%	1.1%	4.0%	1.0%	70.2%
61		35	164		0.08		0.01	_	0.03	003	1.66	+ =	46%	32.5% 33.1%	0.4%	21% 59%	1.6% 1.2%	100.0%	0.05	0.36		0.03	6	102 1		67.0% 54.2%	16% 11%	21.9% 22.8%	0.4%	1.6%	1.1%	67.0% 54.2%
63		37	165	10	0.08	0.56	0.00		0.12	0.02	1.50		49%	35.5%	0.3%	73%	1.0%	100.0%	007		0.00		σ 1	2.01 0	.94	59.5%	41%	22.8%	0.1%	42%	06%	59.5%

- K-patch High CH

																max ratio ou	t of all beams												max ratio out of all b	Hams		
								4cm	n2 PD(mill	(/cm2)				8.7%	13.8%	2.0%	15.2%	1.5%	100.0%	4om2 PD	(nW/cm	2) at 10mm	evaluatio	n distanc	2	72.5%	7.1%	22.4%	1.7%	8.8%	0.9%	72.5%
No. M	oclule Typ	e Beam ID,1	Sema ID_2	Feed no.		Т	Т	П			Т		per Seam	ratio	ratio	ratio	ratio	ratio	ratio							ratio	ratio	ratio	ratio	ratio	ratio	ratio
			l		54/Rig	ht) S3(Lef	55(7	lop)	S6(Botton	9 \$1(Fn	ont) S	(2(Rear)	Back-off	(Right 2mm)/(wont- surface 2mm)	(Left 2mm)/(worst- surface 2mm)	(Top 2mm)/(worst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	S4(Right) S3(Le	n) SS(T	op) SS(Bot	tom) S1	(Front)	S2(Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(worst- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Sottom 10mm(/(worst surface 2mm)	(Front 10mm)/(wont- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
1	_	0		1	0.00	0.03	0.0	00	0.01	0.0	10	0.19	(d0)	12%	17.6%	0.5%	48%	0.5%	100.0%	001 002	0.0	00 00	1	0.00	0.09	47.2%	2.7%	10.6%	0.5%	3.7%	0.0%	47.3%
2		2 4			0.00		01		0.02			0.19		27% 25%	14.6% 17.0%	0.5%	92% 50%	0.5%	100.0%	000 001				000	0.09	48.1% 50.5%	22%	7.6% 8.5%	0.5%	49%	05% 05%	48.1% 50.5%
4		6		1	0.00		01		0.01			0.18		2.8%	16.2%	0.6%	45%	0.6%	100.0%	000 000				0.00	0.09	50.3% 40.1%	22%	89%	0.6%	2.8%	0.6%	50.3%
6		10		2	0.00	0.07	0.0		0.01			0.19		2.1% 1.9%	16.4% 17.1%	0.5%	3.7% 9.9%	0.5%	100.0%	001 004				0.00	0.09	51.2%	31%	9.5%	0.5%	2.6% 6.0%	0.3%	48.1% 51.2%
7		11		2	0.00				0.02	00		0.41		12% 41%	20.1% 11.8%	0.5% 0.3%	42% 56%	0.7%	100.0%	001 005	01			000	0.25	61.4% 61.0%	25% 32%	11.8%	0.5%	25% 18%	05% 0.3%	61.4% 61.0%
9		13		2	0.00	0.07			0.05			0.40		25% 22%	18.5% 16.2%	0.8%	12.4%	0.8%	100.0%	001 004 001 004				0.00	0.15	38.2% 54.5%	2.0%	10.1%	0.8%	84% 19%	05%	38.2% 54.5%
10		18		2		0.07	0.0		0.01	00		0.36		47%	20.1%	0.3%	12%	0.3%	100.0%	001 005	0.0			0.00	0.20	68.9%	16%	13.2%	0.0%	1.1%	0.3%	68.9%
12		20 24		2 5	0.00	0.06		00	0.02	60		0.36		11% 29%	17.8% 22.3%	0.6% 1.2%	64% 15.2%	1.2%	100.0%	001 004		00 00		0.00	0.19	53.5% 68.1%	2.5% 2.4%	9.7% 15.3%	0.3% 1.5%	42% 82%	0.3%	53.5% 68.1%
14		25			0.07				0.01			0.98		7.4%	21.2%	0.3%	13%	1.0%	100.0%	0.05 0.10				0.01	0.70	71.1%	5.7%	16.0%	0.2%	0.5%	0.6%	71.1%
16		26 27		5	0.00	0.16			0.03	00		0.79		7.4% 8.7%	19.9% 20.8%	0.4%	1.8% 4.1%	0.5%	100.0%	005 012 005 011	0.0	0.0	2	0.00	0.54	63.7%	5.8% 7.1%	15.2% 14.8%	0.3%	1.3% 2.4%	0.1%	63.7%
17		26 34		5	0.00	0.20	01	00	0.06			0.74		46% 18%	27.3% 23.4%	0.3% 1.2%	87% 57%	12%	100.0%	003 013		0.0		0.01	0.49	66.0% 71.0%	17% 29%	16.2%	0.1%	6.6% 2.8%	0.7% 0.7%	66.0% 71.0%
19		35		Š				00	0.01	60	i	0.97		7.0%	19.3%	0.2%	0.8%	0.8%	1000% 1000%	006 014		0.0	-	0.01	0.60	70.3%	6.0%	14.6%	0.2%	0.7%	05%	70.2%
20		36	 	5	0.06		0.0		0.03	0.0		0.75		7.8% 6.3%	23.6% 20.6%	0.1%	40% 4.1%	0.4%	100.0%	004 013 004 011	0.0			0.00	0.48	67.7%	62% 52%	17.2%	0.1%	2.3% 2.9%	0.3% 0.4%	67.7% 67.0%
22		126			0.00		01		0.01			0.16		25%	16.3% 34.8%	0.6%	49%	0.6%	100.0%	000 000				000	0.06	31.0% 41.4%	1.9%	9.4% 79%	0.6%	63%	00%	31.0%
24		132		1			0.1	00	0.01	0.0	10	0.22		1.0%	146%	0.5%	5.0%	0.5%	100.0%	000 000				0.00	0.09	40.2%	1.4%	7.0%	0.5%	41%	0.5%	40.2%
25		134	+	1	0.00		0.0	00	0.01	00	10	0.15		15%	15.7% 18.5%	0.5%	30%	0.5%	100.0%	000 000		00 00		0.00	0.07	36.9% 49.0%	1.0%	7.6%	0.5%	25%	00%	36.9% 49.0%
27 28		135		2	0.00		01	00	0.03	0.0		0.43		19%	14.8% 23.3%	0.9%	63% 23%	0.5%	100.0%	001 004 001 004		00 00		0.00	0.18	42.1%	14%	85% 11.4%	0.7%	5.9% 2.2%	0.2% 0.6%	42.1% 50.0%
29		140		2	0.00	0.09	01	00	0.01	60	10	0.37		1.6%	25.3%	0.5%	27%	0.5%	100.0%	001 005	- 01	00 00	-	0.00	0.20	53.9%	13%	14.0%	0.3%	1.6%	0.3%	53.9%
30 31 32		141	+	2	000	0.06	0.0	00	0.04	00	10	0.38		2.3%	15.1% 23.0%	0.8%	10.2%	0.5%	100.0%	001 003	0.0	00 00	1	0.00	0.16	40.9% 57.7%	1.8%	8.3% 13.4%	0.5%	73% 14%	0.3%	40.9% 57.7%
32	X Pat	th 147		2	0.00	0.08	01	00	0.01	0.0	9	0.33		27% 17%	23.6%	0.3%	30% 48%	0.9%	100.0%	001 005 001 003	0.0	0.0	1	0.00	0.17	50.3% 44.2%	21%	13.9%	0.3%	2.1% 4.0%	0.6%	50.3% 44.2%
34		152		5	0.00	0.17	0.0	02	0.09	0.0	10	0.88		2.9%	19.7%	1.9%	10.2%	0.5%	1000% 1000%	002 010	0.0	2 0.0	4	000	0.55	62.5%	22%	11.2%	1.2%	49%	0.3%	62.5%
35		153	+		0.00			00	0.01			0.09		10%	24.3% 32.8%	0.3%	15%	1.3%	100.0%	002 014				0.00	0.50	56.0% 54.0%	2.4% 3.2%	15.5% 22.6%	0.3%	1.9%	0.3%	54.0% 54.0%
37		155 156	_	5	0.02	0.19		00	0.03			0.76		10%	25.1% 24.2%	0.4%	40% 10.1%	0.4%	100.0%	002 012				0.00	0.46	60.4%	22%	15.9%	0.3%	21% 81%	0.3%	60.4% 60.7%
39 40		162			0.00	0.22	01		0.05	60		0.96		2.0%	23.2%	1.4%	48%	0.6%	100.0%	002 013	0.0	0.0	1	0.00	0.59	61.0%	2.1%	13.6%	1.1%	2.7%	0.4%	61.0%
41		163	-	5	0.00			00	0.02			0.76		18% 14%	27.2% 31.8%	0.3%	24%	0.7% 1.2%	100.0%	002 014				0.00	0.45	59.1% 55.3%	25%	18.3%	0.3%	2.0% 1.7%	0.4%	59.1% 55.3%
42		165	128	5	0.00	0.27	01	00	0.04		2 21	1.00		28%	27.1% 17.9%	0.2%	4.1% 7.0%	0.6%	100.0%	002 017 001 004				0.00	820	57.8% 41.0%	22%	17.2%	0.1% 0.5%	2.6% 5.4%	0.3%	57.8% 41.0%
44		2	130	2	0.01	0.06		00	0.04			0.41		27%	15.4%	0.5%	8.8%	0.5%	100.0%	001 003	0.0	0.0	2	0.00	0.10	45.0%	1.7%	8.1%	0.5%	44%	0.2%	45.0%
45 46 47		- 4	132	2	0.01	0.08	0.0	00	0.03	00	10	0.46		2.4%	16.4% 16.9%	0.5%	70% 43%	0.7%	100.0%	001 004		00 00		0.00	0.20	44.0%	15%	90% 97%	0.7%	5.7% 3.1%	0.4%	44.0% 44.0%
47 48		8 10	136		0.00		0.0		0.01			0.37		22%	17.7%	0.5%	3.8% 12.8%	0.3%	100.0%	001 004				0.00	0.17	47.2% 51.5%	1.6%	10.1%	0.5%	10%	0.3%	47.3% 93.9%
40		11	129		0.02	0.79	0.0	00	0.03	00		0.73		13%	25.2%	0.4%	47%	0.8%	100.0%	002 011	01	00 00	2	0.00	0.42	58.9%	25%	15.2%	0.4%	25%	05%	58.9%
50		12	140	4	0.00		0.0	00	0.04	0.0	10	0.76		17%	24.6% 20.9%	0.3%	5.4% 11.9%	05%	100.0%	002 011	0.0	00 00	7	0.00	0.42	56.1% 42.1%	2.9%	14.9%	0.3%	40%	0.3%	56.1% 42.1%
52		18	146	4	0.02		0.0		0.04			0.74		29%	23.4%	0.7%	54% 30%	0.8%	100.0%	002 010		00 00		0.00	0.45	60.5% 50.2%	22% 14%	13.5%	0.5%	15% 15%	04%	60.5% 50.2%
54		20	143	4	0.02	0.11	01	01	0.05	60		0.59		29%	19.3%	0.9%	85%	0.9%	100.0%	001 001	- 0	00 00	4	0.00	0.28	48.0%	2.4%	11.8%	0.7%	6.3%	05%	41.0%
55		24	152	10	0.06	0.47	01	04	0.29	60	12	2.01		11% 54%	21.2% 26.1%	2.0%	14.2%	1.1%	100.0%	005 025	00	0.1	2	0.01	1.39	69.2% 68.8%	27%	14.5%	17%	78% 08%	0.7% 0.7%	69.2% 68.8%
5.7		26	154	10	0.13	0.39	0.0	00	0.04		11	1.52		14%	25.9%	06%	28%	0.9%	100.0%	010 028		0.0		0.01	0.97	63.8%	6.7%	18.1%	05%	22%	0.6%	63.8%
59		26	155		0.10	0.57	0.0	00	0.09	0.0		1.97		5.7% 4.9%	23.3% 29.2%	0.3%	49% 85%	05% 15%	100.0%	008 030	0.0	00 0.1	4	0.02	1.14	61.0% 64.6%	45% 43%	16.1%	0.3%	2.6% 7.1%	0.3%	61.8% 64.6%
60		34	162		0.00	0.54			0.13			1.98		40%	27.2% 21.6%	1.3%	63% 15%	14%	100.0%	006 034				0.02	1.43	72.5% 69.2%	2.8% 52%	17.3%	1.1%	10%	0.9%	72.5% 69.2%
62		36	164	10	0.09	0.47	0.0	00	0.06	0.0		1.64		5.6%	28.5%	0.6%	15%	1.0%	100.0%	007 034	0.0	0.0	2	0.01	1.02	62.3%	44%	20.9%	0.5%	1.5%	0.5%	62.3%
63	_	37	165	10	0.09	0.53	0.0	00	0.12	00	2	2.07		44%	25.8%	0.3%	53%	1.0%	100.0%	007 035	- 01	0.0	9	0.01	1.24	59.9%	15%	17.1%	0.2%	41%	06%	59.9%

3.1.2 Ant M – Patch Antenna

Table 5 & Table 6 & Table 7 show the PD simulation evaluation of Ant M patch antenna at 24GHz / 28GHz / 39GHz for the corresponding evaluation planes specified in Table 1. As shown, a per beam back-off for TER analysis is added to Table 5 (28 GHz Ant. M). This back-off is originated by the 2mm/10mm PD worst ratio which is used for TER calculation of 'Hotspot' condition of folder closed status. If the ratio is large, the *input.power.limit* of this model should be decreased large enough to meet the TER analysis. To avoid the large back-off, therefore, the per beam back-off is adopted and the back-off are applied to several beam IDs in Table 5 to meet the worst surface conditions that satisfying the 'Hotspot' TER analysis.

Table 5. PD of Ant M – patch antenna (24GHz – n258)

[Folder Open Status]

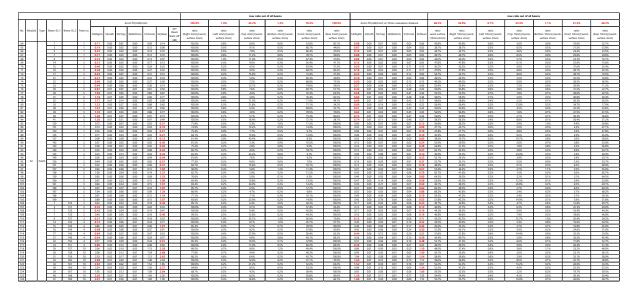
- M-patch Low CH

																max ratio ou	t of all beams											max ratio out of all b	ears s		
П								4cm	n2 PD(mW	(/cm2)				100.0%	1.6%	49.4%	12%	78.5%	100.0%	4cm2 PD(m	W/cm2)	at 10mm evalu	ation distan	nce	66.8%	60.5%	1.4%	25.4%	1.1%	41.7%	66.8%
No.	Andule Ty	pe Seam ID_1	Sema ID_2	Feed no.			Т	П		Т	Т		per Seam	ratio	ratio	ratio	ratio	ratio	ntio						ratio	ratio	ratio	ratio	ratio	ratio	ratio
			l		54/Rig	ht) S3(Let	t) \$5(5	lop)	SE(Bottom	\$1(Pro	ont) 52	(Rear)	Back-off	(Right 2mm)/(wont- surface 2mm)	(Left 2mm)/(worst- surface 2mm)	(Top 2mm)/(worst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Forst 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	S4(Right) S3(Left)	SS(Top)	SS(Bottom)	S1(Front)	S2(Rear)	wont-surface (10mm/2mm)	(Right 10mm)/(worst- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Sottom 10mm(/(wont- surface 2mm)	(Front 10mm(/(worst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
64	_	-		1	0.00	0.00	0.0	01	0.00	0.04	4	0.10	(dB)	69.2%	1.0%	87%	0.0%	36.5%	100.0%	003 000	0.01	0.00	0.01	0.04	42.2%	30.8%	1.0%	585	90%	13.5%	42.2%
65		3			0.1		0.0		0.00			30.0		100.0%	0.7%	90% 74%	0.7%	62.7%	43.3%	0.05 0.00			0.03	0.03	22.6% A1.0%	39.6% 40.9%	00%	60%	0.0%	21.6% 34.8%	23.9%
67		- 5	-			0.00			0.00			0.07		100.0%	0.0%	7.4% 9.3%	0.7%	68.5% 73.8%	49.0% 75.7%	0.06 0.00				0.04		40.9%	02%	47% 58%	0.0%	24.8%	24.8%
68		9		1	0.11	0.00	0.0		0.00	601	7	0.06		100.0%	1.1%	15.8%	1.1%	72.0%	86.3%	0.05 0.00	001	0.00	0.03	0.04	48.4%	45.4%	1.1%	6.3%	0.0%	29.5%	44.2%
69		14	_	2	0.2			00	0.00	0.11		0.09		100.0%	0.5%	63% 74%	0.5%	51.7% 61.2%	44.4% 83.6%	0.09 0.00		0.00	0.03	0.03	42.0%	42.0%	00%	44%	0.5%	16.1% 24.6%	34.6% 35.2%
71		16		2	0.21	0.00	0.0	02	0.00		5 1	0.26		79.7%	1.1%	9.2%	0.4%	57.5%	100.0%	010 000	0.02	0.00	0.06	0.12	50.6%	36.4%	0.8%	57%	0.0%	22.6%	50.6%
72		17		2	0.21	0.00			0.00	0.15		0.11		100.0% 100.0%	0.4%	14.1%	0.4%	70.7% 56.6%	43.7% 53.9%	0.14 0.00	002	0.00	0.08	0.05	\$1.3% A46%	51.3% 44.6%	0.4%	72%	0.0%	29.7%	17.5% 19.0%
74		22		2	0.24	0.00	0.0		0.00	0.10	6 1	0.26		91.5%	125	85%	0.4%	62.3%	100.0%	011 000	0.00	0.00	0.07	0.12	48.1%	42.3%	08%	54%	0.4%	25.0%	48.1%
75		23		2	0.21	0.00		03	0.00	0.22		0.14		100.0%	0.7%	11.6%	0.3%	73.0%	47.3%	0.15 0.00	0.02	0.00	0.09	0.07	52.1%	52.1%	0.7%	5.8%	0.0%	31.8%	22.3%
76		29	-	5	0.51		01		0.01			0.35		100.0% 100.0%	0.7%	10.0%	0.9%	61.6% 76.2%	62.9% 86.2%	0.26 0.00			0.14	0.13	46.6% 54.8%	46.0% 54.8%	05% 08%	53%	0.7%	24.8% 38.4%	24.2% 44.1%
78		31		5	0.60				0.00			0.70		97.9%	1.4%	6.4%	0.1%	78.5%	100.0%	0.41 0.01			0.29	0.43	61.0%	58.0%	1.1%	3.0%	0.1%	41.7%	61.0%
79		32	_	5	0.7	0.00	01		0.00	0.53		0.48		100.0% 100.0%	0.5%	12.1%	0.3%	72.0% 69.8%	62.2% 31.1%	0.45 0.00		0.00	0.29	0.26	58.3% CON.	58.3% 52.9%	0.5%	55%	0.1%	37.2% 31.9%	31.6% 16.0%
81		38		Ś	0.6				0.00	0.35		0.39		100.0%	0.7%	7.6%	0.7%	63.4%	63.9%	0.29 0.00		0.00	0.17	0.17	47.0%	47.8%	05%	3.8%	0.5%	27.3%	27.3%
82		39 40		5	0.60		01		0.00			0.71		92.9% 100.0%	1.6% 0.8%	50%	0.1%	75.4% 77.6%	100.0%	0.38 0.01 0.44 0.01			0.29	0.41	57.7% 60.5%	53.2%	14%	24%	0.1%	40.3% 41.4%	57.7% 54.0%
84		40			0.7		0.1		0.00			0.83		100.0%	0.4%	16.0%	0.1%	77.0%	88.2% 47.1%	0.45 000			0.10	0.20	56.7%	56.7%	04%	80%	0.1%	37.4%	25.6%
85		129		1	0.10				0.00	003		0.18		88.6%	0.5%	12.5%	0.5%	14.2%	100.0%	0.06 0.00		0.00	0.01	0.10	\$3.8%	30.4%	05%	87%	0.5%	54%	53.8%
86		131	-	- 1	0.11		0.0		0.00			0.20		75.9%	0.0%	12.3%	10%	10.8%	100.0%	005 000			0.01	0.09	43.6%	27.2% 27.6%	00%	72%	05%	16%	41.0%
86		135		1	0.17	0.00	0.0	05	0.00	602		0.22		79.7%	0.5%	23.0%	05%	10.7%	100.0%	006 000	0.03	0.00	0.01	0.09	40.6%	25.8%	05%	13.0%	0.5%	41%	40.6%
89		117		1	0.00	0.00	0.0	07	0.00	001	-	0.15		56.4% 83.2%	0.7%	43.6%	0.7%	6.7% 10.7%	100.0%	002 000	0.03	000	0.01	0.07	45.0%	16.1% 31.5%	0.7% 0.2%	17.4% 3.5%	0.7% 0.7%	24% 42%	45.0% 49.9%
91		143			0.40	0.00			0.00			0.50		80.9%	0.2%	10%	0.6%	8.0%	100.0%	017 000	0.01		0.02	0.21	57.4%	34.2%	0.2%	20%	0.4%	10%	46.9% 57.4%
92		144		2	0.20	0.00			0.00			0.43		89.5% 62.4%	0.2%	93%	02%	13.7% 8.0%	100.0%	015 000 009 000	0.03	0.00	0.02	0.22	52.6% 46.8%	35.8% 21.4%	0.2% 0.5%	60% 25.4%	0.0%	47% 11%	52.6% 46.8%
94		149		2	0.30				0.00	003		0.44		82.3%	0.5%	7.0%	0.7%	66%	1000%	012 000			0.01	0.20	46.0%	28.0%	02%	34%	0.7%	12%	45.0%
94 95 96	M Pa	sch 150		2	0.42				0.00	003		0.56		75.9%	0.2%	11.3%	0.0%	5.4%	100.0%	0.18 0.00			0.01	0.27	48.7%	32.0%	0.2%	7.0%	0.0%	1.8%	48.7%
96		151	_	2 5	0.40		01		0.00			0.47		85.3% 86.4%	0.2%	16.5%	0.4%	9.2%	100.0%	0.16 0.00			0.02	0.21	44.4%	33.2% 35.0%	02% 02%	9.8% 2.8%	0.2% 1.0%	16% 47%	44.4% 53.1%
98		158		5	1.10	0.00	0.0		0.00	013		1.20		86.2%	0.2%	2.7%	0.2%	10.2%	100.0%	053 000	0.02	0.00	0.06	0.00	62.5%	41.7%	0.1%	1.6%	0.2%	47%	62.5%
99		159	-	5	1.00			07	0.00	000		1.07		76.8%	0.2%	6.2% 27.9%	0.2%	4.2%	100.0%	045 000		000	0.02	0.67	63.0% 51.0%	41.7%	0.2% 0.2%	2.5% 17.2%	0.2%	21%	63.0% 51.9%
101		160		5	1.10	0.00	0.5		0.00			1.32		89.3%	0.2%	39.1%	0.2%	13.8%	100.0%	056 000			0.07	0.66	50.1%	42.3%	0.2%	23.3%	0.2%	51%	50.1%
102		166 167		5	1.05		01		0.00			1.20		88.1% 82.3%	0.2%	5.9% 7.4%	0.4%	11.7% 6.6%	100.0%	0.47 0.00 0.50 0.00			0.06	0.68	56.8% 66.8%	38.9% 42.9%	0.2% 0.2%	3.8% 3.7%	0.4%	54% 28%	56.8% 66.8%
104		160		5	0.91				0.00	0.10		1.11		82.2%	0.2%	87%	0.2%	9.0%	1000%	0.50 0.00			0.03	0.64	57.6%	44.2%	02%	40%	0.7%	19%	57.6%
105		169			1.13		0.4		0.00			1.22		84.9%	0.2%	31.4%	0.1%	10.8%	100.0%	056 000	0.25		0.06	0.67	50.6%	41.8%	0.1%	19.1%	0.1%	44%	50.6%
106		1	129	2	0.1	0.00	01		0.00	000		0.29		82.9% 100.0%	0.5%	9.9%	0.8%	23.0%	100.0% 93.2%	012 000		000	0.03	0.19	47.2% 38.7%	30.4%	05%	7.1%	0.5%	8.2% 15.2%	47.2% 34.7%
108		- 5	133	2	0.31	0.00	0.0	05	0.00	0.14	4	0.20		95.0%	0.5%	13.0%	0.5%	36.0%	100.0%	014 000	0.03	0.00	0.05	0.16	41.5%	36.0%	0.3%	7.9%	0.5%	12.7%	41.5%
110		7 9	135	2	0.32				0.00			0.29	_	82.2% 76.3%	0.5%	16.0%	0.3%	29.8% 35.7%	100.0%	012 000			0.05	0.19	47.6% 50.0%	31.6% 29.2%	05%	9.4% 16.2%	0.3%	11.5%	47.6% 50.0%
111		14	142	4	0.50	0.00	02	07	0.01	0.21		0.60		85.3%	0.3%	9.5%	12%	30.1%	100.0%	023 000	0.04	0.01	0.08		46.0%	33.9%	0.3%	59%	0.9%	11.7%	46.0%
112		15	143	4	0.82				0.01	0.20		1.05		78.4%	0.4%	5.1%	0.5%	24.8%	100.0%	0.31 0.00			0.11	0.51	48.6%	29.5%	0.4%	38%	0.4%	10.0%	41.6%
113		16	144	4	0.6		0.2		0.00	0.37		0.63		100.0% 100.0%	0.5%	10.6%	0.2%	42.4% 44.2%	92.3% 92.7%	0.36 0.00			0.14	0.37	42.8% 46.2%	41.0% 46.2%	0.3%	72% 13.9%	0.1%	16.4%	42.8% 43.4%
115		21	149	4					0.01	0.21		0.57		91.4%	0.5%	10.7%	1.1%	36.2%	100.0%	0.19 0.00	0.04	0.01	0.09	0.28	48.3%	33.7%	0.4%	63%	1.1%	15.5%	48.2%
116		22	150	4	0.64	0.00	0.1		0.00	0.21		0.82		77.3% 100.0%	0.5%	11.9%	0.1%	25.4% 43.9%	100.0%	0.30 0.00		000	0.10	0.42	51.3% 47.2%	36.1% 47.2%	0.4%	72%	0.1%	12.0%	51.3% 37.8%
110	- 1	29	157	10	1.53	0.00	0.1	19	0.03	0.67	7 .	2.22		70.7%	0.5%	16%	12%	30.2%	100.0%	0.72 0.01	0.11	0.03	0.31	1.04	46.9%	32.6%	0.3%	50%	1.1%	13.8%	46.9%
119		30	158 159	10	1.60	0.02	0.1	90	0.00		3	2.65 2.34	_	61.6% 72.3%	0.6%	16% 62%	02%	31.2% 30.1%	100.0%	0.85 0.01			0.41	1.48	56.0% 57.9%	32.0% 38.0%	0.4%	23% 28%	0.2% 0.2%	15.6%	56.0% 57.9%
121		32	160	10	2.61	0.00	0.1		0.00	1.11		2.10		100.0%	0.3%	18.6%	0.1%	42.9%	81.0%	1.46 0.01			0.54	1.09	57.9% 56.2%	56.2%	0.3%	11.8%	0.1%	20.7%	57.9% 42.0%
122		33	161	10	2.6		0.7		0.01	1.12		1.64		100.0% 70.4%	0.2%	26.5%	0.2%	42.2%	69.1%	1.35 001	0.43	0.00	0.52	0.93	50.8% 50.0%	50.8% 12.1%	0.2%	16.2%	0.2%	19.4%	35.0%
123		38	166	10			0.1		0.01			2.32		70.4%	0.3%	7.8% 5.8%	0.0%	33.6% 27.0%	100.0%	0.75 0.01			0.16	1.16	50.0% 59.8%	32.3% 33.4%	03%	49%	0.6%	15.6%	50.0% 59.8%
125		40	168	10	2.20	0.00	0.1	14	0.00	1.01		2.28		96.4%	0.6%	6.1%	0.1%	44.4%	100.0%	1.22 0.01	0.07	0.00	0.52	1.24	54.3%	53.6%	05%	29%	0.1%	22.9%	54.3%
126		43	169	10	2.6	0.00	0.5	54 T	0.00	1.16		2.06		100.0%	0.3%	21.7%	0.1%	44.2%	77.0%	1.44 001	0.37	0.00	0.57	1.06	51.9%	53.9%	0.3%	13.8%	0.1%	21.2%	42.4%

- M-patch Mid CH

$\overline{}$		-	-	-	-		-			_					max ratio ou	t of all beams					-							max ratio out of all	beams		
\vdash	Т	Т	т	$\overline{}$	т -			4cm2 PD(r	rM/om2)				100.0%	1.1%	47.2%	128	84.0%	100.0%		iom2 PD(ml	W/cm2) a	at 10mm evalu	uation distr	ance	68.2%	93.4%	1.15	25.65	1.1%	44.2%	64.2%
No.	Applied Tv	pe Seam ID	1 Sema ID	2 Feed n	. –	1	T	T	Ť			per	ratio	ratio	ntio	ratio	ratio	ntio					1	т —	ntio	ratio	ntio	ratio	ratio	ntio	ntio
					54/Rigit	sa(Left)	SS(Top)	\$6(800)	(m) \$1(R	Front) S	2(Rear)	Beam lack-off	(Right 2mm)/(wont- surface 2mm)	(Left 2mm)/(wonst- surface 2mm)	(Top 2mm)/(worst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	54/Right	S3(Left)	SS(Top)	S6(Bottom)	S1(Front)	(S2)Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(wont- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Sottom 10mm)/(worst- surface 2mm)	(Front 10mm)/(wonst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
64	-	1		1	0.12	0.00	0.01	0.00	0	107	0.13	(dB)	95.4%	0.8%	8.5%	0.0%	50.8%	100.0%	0.05	0.00	0.01	0.00	0.02	0.06	43.1%	41.5%	0.8%	54%	0.0%	18.5%	43.1%
65		5	_	1	0.17	0.00	0.02	0.00	- 0	114	0.07		100.0% 100.0%	0.6%	8.7% 7.5%	0.6%	66.3%	37.8% 44.8%		000		0.00	0.04	0.04	40.7% 41.8%	40.7% 41.8%	00% 05%	58% 50%	0.0%	23.3% 25.4%	21.5% 21.9%
67		7 9		1	0.14	0.00					0.09		100.0% 100.0%	0.7%	11.1%	0.0%	79.2% 71.8%	\$1.8% \$2.0%	0.07	000		0.00	0.04		45.0% 44.2%	45.8% 44.2%	0.7% 0.6%	63% 51%	0.0%	30.6%	31.9% 24.4%
69		14		2	0.26	0.00	0.02	0.00			0.12		100.0% 100.0%	0.4%	86% 72%	0.4%	53.5% 64.2%	44.9% 63.0%	0.11	0.00	0.01	0.00	0.05		43.5%	43.8%	00%	55% 47%	0.4%	20.3%	17.2% 26.5%
71		16		2	0.33		0.04	0.00	0.	124	0.29		100.0%	0.6%	10.8%	0.3%	71.5% 74.6%	87.1% 28.4%			003	0.00	0.10 0.11	0.15	48.3% 51.1%	48.2% 51.1%	06%	75% 7.1%	0.0%	29.15 29.85	45.6% 12.8%
66. 66. 67. 68. 69. 77. 77. 77. 77. 78. 79. 81. 82. 83. 85. 86. 87. 87. 88. 89. 99. 99. 99. 99. 99. 99. 99. 99		21		2	0.32	0.00	0.02	0.00			0.16		100.0%	0.3%	6.3%	0.3%	59.2%	50.3%	0.15	000	0.02	000	0.08	0.05	47.2%	47.2%	0.3%	47%	0.3%	24.7%	15.5%
75		22		2	0.16	0.00	0.03	0.00		132	0.28		100.0% 100.0%	0.6%	9.1% 12.0%	0.3%	68.6% 76.5%	77.1% 30.9%	0.18	0.00	002		0.10	0.06	49.0% 51.6%	49.0% 51.6%	0.6% 0.5%	6.1%	0.0%	28.7% 31.9%	31.0% 13.4%
76		29	_	5	0.66	0.01	0.07				0.45		100.0% 100.0%	0.8%	10.6%	0.8%	65.3% 78.4%	68.3% 71.3%	0.32	000	004		0.19		483% 548%	48.7% 54.8%	06% 04%	58% 18%	0.6%	29.4% 39.3%	27.2% 36.5%
78		31		5	1.05	0.00	0.05			100	0.70		100.0% 100.0%	1.1%	43% 12.2%	0.1%	84.0% 73.3%	66.4% 46.2%		601	002		0.46		57.8% 51.6%	57.8% 58.6%	1.1%	23%	0.1%	44.3% 38.0%	40.1% 24.0%
80		33		5		0.00		0.00	- 0		0.32		100.0% 100.0%	0.4%	20.4%	02%	69.3% 67.3%	28.9% 64.7%	0.59	0.00	013	0.00	0.37	0.17	53.8% 49.1%	53.8% 49.7%	0.3% 0.5%	11.5%	0.1%	34.2%	15.2% 28.0%
82		39		- 5	0.90	0.00	0.03	0.00	0.0	182	0.75		100.0%	1.0%	2.4%	0.1%	83.1%	76.1%	0.55	0.01	002	0.00	0.43	0.43	55.6%	55.0%	0.8%	1.7%	0.1%	40.2%	43.6%
83		40		5	1.14	0.01	0.06	0.00	0		0.63		100.0%	0.8%	5.3% 16.4%	0.1%	81.9% 72.7%	58.4% 36.9%	0.65	0.00	0.10	0.00	0.46	0.38	59.4% 57.1%	59.4% 57.1%	0.7%	25% 84%	0.1%	42.9% 37.5%	35.2% 20.2%
85		129		1	0.17	0.00	0.02		0	102	0.20		84.6% 76.4%	0.5%	10.8%	10%	13.8%	100.0%	0.05	000	0.01	0.00	0.01	0.11	57.4% 45.1%	29.7%	00% 00%	72% 7.1%	05%	62% 18%	57.4% 45.1%
87		133		1	0.16	0.00	0.02		01	102	0.21		77.3% 83.6%	0.0%	8.1% 18.8%	05% 05%	9.5% 12.1%	100.0%	006	000	0.01	0.00	0.01	0.10	47.4% 42.5%	28.4% 27.5%	00% 00%	52% 12.1%	05%	18%	47.4% 42.5%
89		137		1 2	0.08	0.00	0.06	0.00	01	101	0.14		54.2% 82.9%	0.0%	45.1% 4.0%	0.7%	7.7%	100.0%	002	0.00	0.03	0.00	0.01	0.06	43.0% 51.7%	15.5% 28.9%	00% 02%	19.0% 2.4%	0.7%	15% 18%	41.0%
91		141	_		0.29		0.02	0.00	- 0	005	0.40		80.3%	0.2%	1.1%	0.7% 0.6% 0.2%	9.2%	1000%	0.17	0.00	0.01	0.00		0.28	58.1%	34.2% 34.2%	0.2%	21%	0.6%	15% 7.1%	58.1%
93		145	_	2	0.24	0.00	0.18	0.00	0.	104	0.41		62.1%	0.2%	6.6% 47.2%	0.3%	18.6% 9.7%	100.0%		0.00		0.00	0.01	0.17	60.3% 44.6%	22.1%	0.2% 0.3%	4.4% 25.6%	0.0%	1.2%	60.3% 44.6%
94	M Pa	149 sch 150		2	0.43	0.00		0.00	- 0	103	0.42		82.5% 77.0%	0.2%	8.9% 9.4%	0.5%	7.5% 6.6%	100.0%		0.00	0.03	0.00	0.01	0.21	50.2% 52.0%	28.8% 33.0%	0.2% 0.2%	48% 59%	0.5%	1.4% 2.0%	50.2% 52.0%
96		151 157	_	2 5	0.35					106	1.03	_	85.9% 91.6%	0.2%	15.3% 7.6%	0.2% 1.2%	14.1%	100.0%	0.14	000	0.04		0.02		47.9% 54.6%	34.1%	0.2% 0.2%	98% 14%	02% 1.1%	52% 56%	47.9% 54.0%
98		158 159	=	5	1.01		0.04	0.00	- 0	114	1.19		85.0% 77.8%	0.3%	14% 60%	0.2% 0.2%	11.2% 5.2%	100.0%	0.49	000	0.02	0.00	0.06		64.2% 63.4%	41.3% 41.2%	0.2% 0.2%	19%	0.2%	54% 25%	61.2%
100		160		- 5	1.02	0.00	0.29	0.00	0	116	1.10		86.7% 85.7%	0.3%	24.4%	0.1%	13.3%	100.0%	052	000	0.18	0.00	0.06	0.63	53.4% 50.0%	43.9%	0.2%	15.3%	0.1%	5.3%	\$3.4% \$0.0%
102		166		5	0.95	0.00	0.06	0.00	0	224	1.07		89.1%	0.2%	7.0%	02%	13.2% 13.2%	100.0%	0.42	0.00	0.05	0.00	0.07	0.62	57.0%	39.3%	0.2% 0.3%	23.6% 4.6%	0.4%	5.9% 6.5%	57.8%
101		167		5	0.29	0.00	0.09	0.00	0	108	1.12		82.1% 79.9%	0.2%	4.8% 8.2%	0.2% 0.2%	10.1%	100.0%	0.48	0.00	0.04		0.04	0.65	68.2% 58.4%	43.4% 42.7%	0.2% 0.2%	24% 3.6%	0.2%	29% 48%	68.2% 58.4%
105		169	129	- 5	0.41	0.00	0.35			016	0.45		91.4%	0.2%	28.6%	0.2%	13.2%	100.0%		000	0.22		0.06		51.7% 50.2%	42.1% 33.3%	0.2% 0.2%	17.8% 6.7%	0.1%	5.3% 11.8%	51.7% 50.3%
228		3	131	2	0.35	0.00	0.04			119	0.30		100.0% 100.0%	0.6%	10.2%	0.6%	52.8% 43.4%	85.5% 96.3%	0.13	000	003	0.00	0.07	0.12	375% 41.9%	37.5% 39.0%	0.3% 0.2%	7.1%	0.6%	20.5%	34.9% 41.9%
122		- 7	135	2	0.37	0.00	0.05	0.00	- 0	216	0.39		96.1% 100.0%	0.5%	13.7%	03%	41.0% 57.2%	100.0%	0.14	0.00	0.03	0.00	0.06	0.18	46.9% 47.4%	37.1% 38.9%	0.3% 0.7%	80% 154%	0.3%	16.5%	46.9% 47.4%
110 111 112		14	142	- 4	0.62	0.00	0.07	0.01	0.	126	0.67		92.7%	0.6%	9.7%	0.9%	29.2%	100.0%	0.24	0.00	0.04	0.01	0.11	0.29	43.7%	35.7%	0.4%	61%	0.9%	15.8%	41.7%
113		15		- 4	1.00	0.00	0.10	0.00	0:	253	0.80	_	85.4% 100.0%	0.4%	6.9% 9.5%	0.5%	36.2% 53.6%	100.0% 80.2%	0.44	0.00	007		0.16	0.44	47.6% 43.9%	33.3% 43.6%	0.3%	49% 67%	0.4%	15.4% 22.4%	47.0% 43.9%
113 114 115 116 117		17	145			0.00	0.25				0.54	_	100.0% 100.0%	0.6%	30.7% 12.4%	0.3%	53.2% 42.6%	67.7% 95.5%	0.38		013	0.00	0.18 0.11		47.6%	47.6% 37.1%	05% 03%	15.9% 7.1%	0.3%	22.3% 19.1%	33.7% 48.4%
116		22	150			0.01	0.11			130	0.00		84.1% 100.0%	0.6%	12.0%	0.1%	33.9% 56.6%	100.0% 74.8%	0.35	0.00			0.14	0.46	52.2% 44.4%	40.2% 44.4%	05% 05%	74%	0.1%	15.9% 24.8%	52.2% 34.0%
118 119		29	157	10		0.01	0.25	0.00	6	134	2.21		74.0%	0.6%	11.3%	10%	38.2% 41.6%	100.0%		001	0.12	0.02	0.41 0.56	1.03	46.7% 56.2%	28.8% 30.3%	05% 04%	53% 25%	0.9% 0.2%	16.4%	45.7% 56.2%
120		31	159	10	1.91	0.02	0.19	0.00	1	1.09	2.29		79.8%	1.0%	7.7%	0.1%	45.5%	100.0%	093	0.02	0.10	0.00	0.57	1.29	57.9%	39.0%	0.8%	40%	0.1%	23.9%	57.9%
121		32 33	160 161	10	1.02	0.01	0.43	0.01	1-	141	2.02		100.0% 100.0%	0.4%	14.7% 23.1%	0.2%	46.2% 46.2%	68.2% 60.0%	1.51	0.01 0.01		0.00	0.73	0.94	55.5% 49.9%	55.5% 49.9%	0.4% 0.2%	9.4% 14.4%	0.1%	24.5%	36.6% 31.1%
123		38	166				0.23				2.34		80.0% 63.3%	0.6%	9.7% 4.0%	05% 02%	42.8% 38.0%	100.0%		0.01	0.11		0.49		49.0% 60.0%	33.2% 32.9%	0.4% 0.6%	47% 18%	0.4%	21.0%	49.8% 60.0%
120 121 122 123 124 125		40			2.47	0.02	0.18	0.00	1.		2.19 1.98		100.0% 100.0%	0.6%	7.2% 17.8%	0.2%	58.5% 49.2%	88.9% 64.5%			0.09	0.00	0.76	1.23	543% 535%	54.3% 51.5%	06% 03%	35% 11.4%	0.1%	30.7% 24.7%	49.6% 35.1%
120		41	199	10	1.07	0.01	935	dbi			1.000	_	rus/2%	0.85	17,875	W/5	9.05	V437h	1.04	201	VJ5	350	3.76	100	44376	as 37h	v.J7h	11.40%	41%	24.75	AA.17h

- M-patch High CH

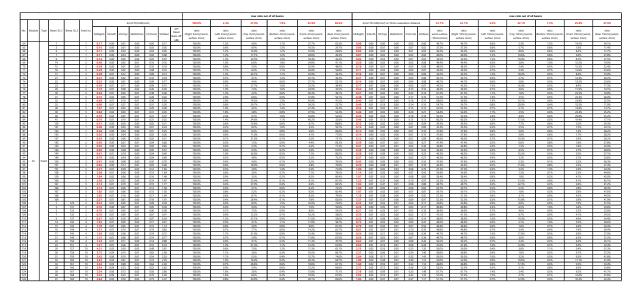


[Folder Closed Status]

- M-patch Low CH

		-			_			-			_		· ·		max ratio ou	t of all beams								-				max ratio out of all	bearts		
\vdash		1						lcm2 PD(n	nW(on2)				100.0%	2.8%	41.5%	1.0%	44.8%	88.7%	4	Kom2 PD	(nW/cm2)	at 10mm eva	lustion die	tance	59.0%	59.0%	2.4%	22.0%	2.0%	24.9%	52.7%
No. M	odule Type	Beam ID_1	Sens D ₂ 2	Feed no.		T	Т		Т			per Seam	ratio	ratio	ratio	ratio	ratio	ratio		Т	Т		Т	Т	ratio	ratio	ratio	ratio	ratio	ratio	ratio
					54/Right	t) S3(Le	ft) SS(Top)	S6(Both	om) \$1()	Front)	S2(Rear)	Back-off	(Right 2mm(/(worst- surface 2mm)	(Left 2mm)/(worst- surface 2mm)	(Top 2mm)/(worst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	54(Right)	53(Le	ft) SS(Top)	SS/Bottom	n) S1(From	r) S2(Rear)	wont-surface (10mm/2mm)	(Right 10mm)/(wont- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Sottom 10mm)/(worst- surface 2mm)	(Front 10mm(y/(worst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
64		1 1		1	0.11	0.00		0.00			0.09	(00)	100.0% 100.0%	1.8%	8.3% 10.8%	0.9%	19.3%	83.5% 27.5%	0.06		000	0.00	0.01		50.5% 35.0%	50.5% 35.0%	09% 08%	37% 50%	0.9%	92% 92%	41.2% 11.7%
66		5		-	0.12	0.00	0.01	0.00		002	0.04		100.0%	1.7%	12.0%	12%	20.5%	32.5%	0.05	000	0.01	0.00	0.01	0.02	38.5%	38.5%	0.9%	6.0%	0.9%	6.0%	15.4%
67		7		-	0.10	0.00	0.02	0.00	- 0		0.06		100.0%	2.0%	21.8%	30%	19.8%	545%	0.04		001	0.00	0.01		40.6% 25.4%	40.0% 25.4%	20%	11.9% 22.0%	20%	79%	27.7%
69		14		2	0.28	0.00		0.00		007	0.12		100.0% 100.0%	0.7%	89% 50%	1.1%	24.8% 27.7%	41.8% 542%	0.14	0.00	001	0.00	0.03		41.6% 46.2%	48.6% 46.2%	0.7% 0.4%	50% 38%	0.7% 0.4%	12.1%	13.8% 24.4%
71		16		2	0.17	0.00	0.00	0.00		004	0.13		100.0%	1.2%	8.1%	0.6%	23.1%	77.5%	0.11	000	0.01	0.00	0.02	0.07	41.6%	37.6%	12%	64%	0.6%	12.1%	41.6%
72		21		2 2	0.27	0.00		0.00		006 007	0.09		100.0% 100.0%	1.9%	36.1% 6.2%	15%	22.3% 25.7%	342% 442%	0.10	001	005		0.02		38.3% 46.4%	38.3% 46.4%	19%	19.7%	0.7%	82% 12.7%	15.6%
74 75		22 23		2	0.19	0.00		0.00			0.13		100.0% 100.0%	1.0%	62%	05% 13%	27.5%	69.4% 17.7%	0.09	000	001	0.00	0.03		44.0% 38.4%	44.0% 38.4%	05% 19%	52% 17.5%	05%	13.0%	347%
76		29		5	071	0.00	0.06	0.02		017	0.27		100.0%	1.0%	8.7%	2.1%	23.3%	37.4%	0.34	001	002	0.01	0.07	0.11	47.5%	47.5%	0.7%	34%	1.1%	10.3%	15.3%
78		30		5	0.53	0.01		0.01			0.35		100.0%	1.5%	62% 11.4%	13%	37.7% 44.8%	49.0% 59.0%	0.31		002		0.11		58.6% 55.4%	58.6% 55.4%	1.1%	30% 53%	0.6%	21.1%	23.7% 34.0%
79 80		32 33		5	0.43	0.00		0.01		018	0.25		100.0% 100.0%	28%	18.7% 32.4%	12%	41.7% 35.7%	56.5% 27.3%	0.26	601	0.05	0.00	0.09		58.8% 54.9%	58.8% 54.9%	21% 12%	12.0% 19.9%	0.5%	20.3% 16.2%	33.6% 15.2%
81		38		5	0.67	0.01	0.05	0.02		018	0.13		100.0%	1.0%	7.0%	22%	26.8%	37.6%	0.34		0.02	0.01	0.09	0.10	50.6%	50.0%	0.7%	2.4%	1.0%	13.1%	14.9%
63		40		5	0.51	0.01		0.00			0.34		100.0% 100.0%	2.0%	5.3% 15.6%	0.6%	43.1%	67.0% 56.7%	0.28	001		0.00	0.13		55.1% 57.9%	55.1% 57.9%	16%	30% 7.1%	0.4%	24.9% 22.8%	41.5% 30.3%
84		41 129		5	0.46	0.00		0.00			0.20		100.0% 100.0%	2.0%	28.4%	0.9%	38.8% 7.6%	43.8%	0.27	001	0.09	0.00	0.08		59.0% 40.3%	59.0% 40.2%	15%	18.4% 8.2%	0.4%	17.8% 3.8%	36.2% 31.2%
06		131		1	0.24	0.00	0.03	0.00		001	0.22		100.0%	0.3%	7.4%	0.6%	15%	65.5%	0.12	0.00	0.02	0.00	0.01	0.09	38.1%	38.1%	0.2%	47%	0.6%	18% 12%	25.1%
87		133			0.35		0.04	0.00		001	0.26		100.0%	0.9%	8.0% 12.7%	0.9%	17% 16%	74.1% 74.9%	0.13	000	0.02	0.00	0.01	0.10	35.6% 36.4%	35.6% 36.4%	06%	4.8% 6.5%	0.6%	15%	23.9%
89		117		, ,	0.28		0.05	0.00			0.22		100.0% 100.0%	0.7%	18.3%	0.4%	47% 46%	77.3% 74.0%	0.11		0.02		0.01		17.8% 43.6%	37.8% 43.6%	0.7% 0.3%	83%	0.4%	22% 21%	33.9% 33.5%
91		143		2	0.84	0.00	0.00	0.01	- 0	004	0.62		100.0%	0.4%	1.5%	0.6%	42%	74.1%	0.37	000	0.00	0.01	0.02	0.29	44.1%	44.1%	0.2%	0.8%	0.6%	1.0%	34.6%
92 93 94		144		2	0.73	0.00	0.17	0.00		003	0.50		100.0% 100.0%	0.4%	£9% 29.7%	0.3%	6.1% 5.5%	69.3% 84.6%	0.32		0.08	0.00	0.02		44.2% 46.0%	44.2% 46.0%	0.3%	5.9% 14.0%	0.1%	2.7% 2.6%	30.3% 43.2%
94	M Part	149		2	0.73			0.00			0.58		100.0%	0.7%	5.4% 96%	0.4%	48% 50%	79.0%	0.33		0.02		0.01		44.0% 46.0%	44.8% 46.8%	0.7% 0.7%	29% 54%	03%	19%	35.0% 38.7%
96 97		151		2	0.57	0.00		0.01			0.44		100.0% 100.0%	0.7%	16.9%	0.9%	44%	77.3%	0.25		0.06		0.01		43.4% 48.1%	43.4%	0.7%	12.4%	0.9%	1.9%	34.6%
98		157		5	2.02	0.00	0.07	0.00		013	1.60		100.0%	0.4%	13%	12%	54% 65%	77.0% 79.4%	1.00	0.01	0.03	0.00	0.06	0.90	53.4%	48.1% 53.4%	0.3% 0.5%	2.1% 1.7%	1.1% 0.1%	25% 11%	37.7% 44.7%
100		159		5	2.16	0.00		0.00		013	1.65		100.0% 100.0%	0.9%	15% 25.0%	0.2%	78% 73%	83.8% 84.9%	0.95	002	0.03	0.00	0.07		55.1% 52.3%	55.1% 52.3%	09% 04%	17% 14.5%	02%	19% 18%	48.7% 44.5%
101		161 166		5	1.98	0.00		0.00			1.69		100.0% 100.0%	0.5%	37.9% 5.5%	02% 08%	7.0% 5.8%	85.2% 75.9%	0.93		0.42		0.07		47.0% 49.0%	47.0% 49.8%	05% 03%	21.0% 32%	0.1%	2.4% 2.7%	43.1% 29.1%
323		167		5	1.00	0.00	0.05	0.00		0.14	1.51		100.0%	0.9%	2.0%	0.2%	7.6%	83.8%	1.02	0.01	0.03	0.00	0.07	0.91	56.6%	56.0%	0.7%	1.6%	0.2%	17%	52.4%
104		168		5	2.10	0.00	0.17	0.00	- 6		1.53		100.0% 100.0%	0.7%	20.9%	0.1%	86% 72%	846%	1.00		0.07	0.00	0.08		55.2% 50.9%	55.2% 50.9%	06% 04%	40% 16.6%	01%	46% 18%	47.7% 44.1%
106		1	129	2	0.49	0.00		0.00			0.16		100.0%	1.0%	13.6%	0.8%	12.2%	73.8% 60.0%	0.21		004		0.03		43.1% 40.2%	43.1% 40.2%	1.0%	87% 59%	0.4%	58% 16%	31.1% 24.2%
108		5	123	2	0.59	0.00	0.05	0.01	-	005	0.40		100.0%	0.7%	7.9%	12%	9.1%	68.0%	0.22	000	0.03	0.01	0.02	0.18	35.9%	36.9%	0.7%	5.1%	1.0%	17%	32.3%
110		9	135	2	0.56	0.00	0.06	0.01			0.40		100.0% 100.0%	1.6%	14.1% 26.8%	1.3%	8.5% 10.0%	72.6% 69.7%	0.23	001			0.02		40.5% 35.2%	40.5% 35.2%	14%	7.6%	0.7%	14% 41%	31.9% 30.1%
111		14	142	4	1.35	0.00		0.01		015	0.88		100.0%	0.6%	10%	1.0%	10.7% 9.7%	64.7% 34.0%	0.64	001	003	0.01	0.07		47.5% #5.8%	47.5% 45.4%	05%	185	0.8%	50%	27.1% 32.4%
113		16	144	4	1.10			0.01			0.75		100.0% 100.0%	0.7%	7.4%	0.5%	13.2%	68.3%	0.52		0.05	0.00	0.07		46.0%	46.0%	05%	47%	0.2%	6.2%	32.0%
115		21	145	4	0.98			0.01	-		0.65		100.0%	1.6%	2.7%	12% 0.6%	12.8%	66.6% 73.8%	0.43		016	0.01	0.05	0.34	43.6%	43.6% 43.9%	13%	16.3% 4.2%	0.7% 0.6%	54% 52%	37.1% 35.0%
116		22 23	150	4	1.05	0.00	0.10	0.00		012	0.65		100.0% 100.0%	1.1%	9.2%	0.3%	11.0%	83.3% 65.8%	0.50	001	006	0.00	0.06		47.4% 37.4%	47.4% 37.4%	1.0%	52% 11.6%	0.2%	58% 48%	41.2% 29.2%
118		29	157	10	159	0.00	0.25	0.04		0.36	2.62		100.0%	0.7%	6.9%	1.1%	10.7%	72.9%	1.82	003	0.12	0.04	0.17	1.27	50.6%	50.8%	0.4%	35%	1.1%	46%	35.4%
119		30	158 159	10	2.81	0.00	0.20	0.01	-		2.60 2.47		100.0% 100.0%	1.0%	46% 7.2%	0.3%	13.5%	78.9% 87.9%	1.60	001	0.10	0.01	0.24	1.43	57.1% 54.6%	57.1% 54.6%	16%	22% 36%	0.2%	7.3% 9.9%	42.7% 51.0%
121		32 33	160	10	259	0.00		0.01			2.29 1.84		100.0% 100.0%	1.0%	19.0%	0.3%	16.9%	74.2% 71.0%	1.58	003	0.35	0.01	0.27		51.1% 46.1%	51.1% 46.1%	08%	11.2%	02%	87% 91%	37.0% 34.7%
123		38	166		2.31 2.01		0.20	0.03	- 0	0.40	2.44		100.0% 100.0%	0.6%	60% 38%	0.8%	12.0% 14.8%	716% 88.7%	1.77	0.02	012	0.02	020	1.22	53.5% 57.6%	53.5% 57.6%	05% 12%	15% 21%	06% 02%	59% 84%	36.9% 52.7%
124		40	168	10	2.92	0.04	0.22	0.01	-	060	2.35		100.0%	1.5%	7.4%	0.2%	20.5%	80.3%	1.59	0.04	0.10	0.00	0.32	1.30	543%	54.3%	1.3%	35%	0.1%	11.0%	44.2%
126		41	169	10	1.01	0.00	0.70	0.01	_ 0	051	2.17		100.0%	1.1%	23.2%	0.2%	17.1%	72.2%	1.51	0.03	0.41	0.00	0.27	1.05	50.1%	50.1%	0.9%	11.6%	0.1%	8.0%	34.8%

- M-patch Mid CH



- M-patch High CH

						-	_	-	-					max ratio ou	t of all beams			Г		_	-		-				max ratio out of all	beams		
П			T	T			4	cm2 PD(mW	(on2)			100.0%	2.4%	15.5%	1.0%	38.1%	81.1%	4	Kom2 PD(m	W/cm2) a	rt 10mm evalu	uation dista	nce	64.3%	64.2%	2.4%	20.7%	12%	20.0%	44.9%
No. Mod	tule Type	e Beam ID_1	Sema ID,	Feed no.							per Seat	ratio	ratio	ratio	ratio	ratio	ntio							ratio	ratio	ratio	ratio	ratio	ratio	ratio
					54/Right	() S3(Left)	SS(Top)	S6(Bottom	\$1(Front	t) S2(Rea	Back-o	(Right 2mm(/(wont- surface 2mm)	(Left 2mm)/(worst- surface 2mm)	(Top 2mm)/(wonst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	S4(Right)	S3(Left)	SS(Top)	SS(Bottom)	\$1(Front)	S2(Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(worst- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Sottom 10mm)/(wont) surface 2mm)	(Front 10mm(/(wonst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
64		1		1	0.20	0.00	0.02	0.00	0.05	0.11		100.0% 100.0%	1.0%	81% 82%	15%	23.9%	57.4% 28.2%		0.00	0.01	0.00	0.02		50.3% #6.7%	50.3% 46.7%	10%	41% 62%	1.0%	12.2%	28.4% 10.2%
64 65 66 67 68 69		5	_	+ +	0.20			0.00	004			100.0%	0.9%	12.7%	0.9%	17.2%	30.1%				0.00	0.02		29,5%	29.8%	05%	8.7%	0.9%	68%	11.0%
6.7		7 9		1	0.21			0.00	0.05			100.0% 100.0%	1.4%	14.8%	14%	21.4%	37.6% 37.9%		000		0.00	0.02	0.03	43.3%	43.2% 40.8%	1.4%	12.0% 20.7%	05%	81% 82%	15.2% 15.4%
69		14	 	2	0.17	0.00	0.04		0.10	0.19		100.0%	1.15	82%	15%	21.0%	40.0%		000	002	0.00	0.05		40.0% 52.5%	40.0% 52.5%	09%	40%	0.9%	99%	13.4%
70		15		2	0.51	0.01	0.02	0.00	0.12	0.20		100.0%	1.0%	43%	0.8%	23.4%	29.5%	0.28	000	001	0.00	0.06	0.06	552%	55.2%	06%	2.6%	0.4%	11.4%	16.5%
71 72		16	_	2	0.37	0.01	0.04		0.08	0.15	+	100.0% 100.0%	1.3%	9.7% 29.9%	0.8%	22.0% 25.5%	41.1% 35.9%	0.17		003		0.03	0.07	44.9% 50.7%	44.9% 50.7%	11%	7.8% 17.0%	0.3%	9.1% 10.4%	17.5% 13.1%
73		21		2	0.52	0.00	0.03		012	0.21		100.0%	1.0%	52%	12%	22.9%	22.9%	0.29	000		0.00	0.06	0.09	55.6%	55.6%	0.8%	27%	0.6%	10.9%	17.4%
75		22	_	2	0.44	0.01	0.03	0.00	0.10	0.17	+	100.0%	1.1%	6.5% 24.1%	0.7%	22.8% 25.9%	31.6%	0.22	000	0.02		0.05	0.07	50.3% 50.7%	50.3% 50.7%	09% 14%	52% 11.5%	05% 05%	10.6%	14.9% 14.9%
76		29		5	1.20		0.10		0.36			100.0%	0.9%	7.6%	1.1%	26.2%	30.2%				0.01	0.17		51.3%	51.3%	09%	3.3%	0.9%	12.4%	11.9%
73. 74. 75. 76. 77. 78. 91. 92. 92. 93. 94. 96. 96. 97. 99. 99. 99. 99. 99. 99.		30	+	5	1.04	0.02	0.05		0.36	0.35	+	100.0% 100.0%	1.4%	75% 50%	0.6%	34.0% 25.8%	34.0% 49.6%	0.61	001	005		0.22		58.9% 64.1%	58.9% 64.1%	12% 19%	435 325	0.3%	20.8%	15.8% 25.7%
79		32		5	0.96	0.02	0.14	0.01	0.36	0.13		100.0%	1.6%	14.3%	0.9%	38.7%	344%	0.54		0.07	0.01	0.20	0.16	56.9%	54.9%	14%	75%	0.5%	20.5%	16.5%
80		33	+	5	1.15	0.00	0.28		0.37	0.26		100.0% 100.0%	0.7%	24.6%	1.0%	31.9%	22.7%		0.01		0.01	0.17	0.10	55.0%	55.0% 52.3%	0.7%	17.6% 2.2%	05%	14.5%	8.7%
82		39		5	1.10	0.02	0.05	0.01	0.30	0.55		100.0%	1.7%	47%	0.5%	27.1%	49.9%	0.69	0.02	003	000	0.18		625%	62.5%	1.5%	27%	0.3%	16.0%	26.7%
83		40	+	5	0.97	0.02	0.09	0.01	0.30	0.46	+-	100.0% 100.0%	2.2%	9.3%	0.9%	31.2% 37.8%	47.9% 25.8%	0.60		0.05	0.00	0.17	023	\$1.9% \$7.9%	61.9% 57.9%	2.0%	54%	0.4%	17.4%	23.4% 11.4%
85		129		í	0.34	0.00	0.03		0.02	0.23		100.0%	0.6%	12%	0.9%	44%	66.1%	0.14	000	0.03	000	0.01	0.09	29.5%	39.5%	0.6%	7.3%	0.6%	2.0%	25.1%
86		131		1	0.42	0.00	0.04	0.00	602	0.24		100.0% 100.0%	0.2%	8.3% 9.1%	0.9%	40% 37%	56.0% 67.0%	0.15	000	0.02		0.01	0.09	36.2% 40.2%	36.2% 40.2%	0.2% 0.6%	57% 60%	0.7% 0.6%	17% 14%	21.0% 26.8%
86		135	_	1	0.37	0.00	0.03		0.02	0.23		100.0%	0.3%	10%	05%	44%	641%		000	0.02		0.01	0.10	29.5%	39.5%	0.3%	49%	0.5%	19%	27.1%
89		137		1 2	0.10	0.00	0.05	0.00	0.02	0.21		100.0% 100.0%	0.7%	18.2% 2.7%	0.3% 1.0%	54% 45%	69.7% 66.2%	0.13	0.00	0.03	0.00	0.01	0.08	42.4% 42.6%	42.4% 42.6%	0.3%	9.1% 1.5%	0.3%	2.4%	25.2% 27.5%
91		140	_	2				0.01		0.66		100.0%	0.3%	2.0%	0.7%	45%	69.0%				0.01				45.2%	0.3%	0.9%	0.7%	1.0%	27.5%
92		144		2	0.09		0.08		005			100.0%	0.3%	8.4% 27.0%	0.2%	55%	67.2% 75.9%		000			0.02	0.26	48.0%	48.0% 49.9%	0.3% 0.7%	6.1% 13.7%	0.1%	24%	28.8% 37.1%
94		149	+	2	0.82	0.00	0.16	0.00	0.05		+-	100.0%	0.4%	46%	0.4%	56%	69.3%		000			0.02		47.0%	47.8%	0.2%	24%	0.4%	2.3%	31.4%
95 N	f Pasd	h 150		2	0.92		0.07		0.05			100.0%	0.4%	7.7% 17.7%	0.1%	5.6%	72.0%		000	0.04		0.02	0.31	49.0%	49.0%	0.4%	45%	0.1%	2.4%	31.7% 28.1%
96		151	1	5	2.41	0.00	0.12		0.14			100.0% 100.0%	0.4%	17.7%	13%	4.9% 5.8%	72.6% 69.6%	1.17	0.00	0.08		0.02	0.19	45.2%	45.2% 48.7%	0.4% 0.2%	11.8% 15%	0.7% 1.2%	2.2% 2.6%	34.6%
98		158 159		5	2.13			0.00	017			100.0% 100.0%	0.6%	3.8% 2.0%	0.1%	81% 93%	74.5% 77.0%		0.01			0.08	0.88	56.2% 51.7%	56.2% 58.7%	0.4% 0.6%	12%	0.1% 0.2%	18% 46%	41.1% 42.2%
100		160	_	5				0.00	0.19			100.0%	0.7%	21.8%	0.1%	83%	77,0%		001		0.00	0.10		54.7%	54.7%	0.3%	12.6%	0.1%	42%	42.2%
101		161		5	2.14		0.71		0.15			100.0%	0.4%	23.1%	0.3%	6.9%	41.1%		0.01		0.00	0.07		49.0%	49.8%	0.3%	20.4%	0.2%	11%	29.5%
333		166	+	5	1.86	0.01	0.07		0.16	1.62		100.0% 100.0%	0.3%	11%	0.0%	7.1% 8.9%	71.9%		001	0.04	0.01	0.07		52.9% 53.6%	52.9% 59.6%	0.2% 0.4%	19%	0.5%	12% 42%	37.8% 44.9%
104		168		5	2.04	0.00	0.15	0.00	0.19	1.58		100.0%	0.6%	75%	0.0%	92%	77.5%	1.21	0.01	0.07	0.00	0.09	0.86	59.3%	59.3%	06%	13%	0.0%	46%	41.9%
105		169	129	2	0.57	0.01	0.57		0.19	1.85		100.0% 100.0%	0.4%	24.3% 9.2%	02% 12%	8.0% 11.0%	79.7% 65.3%	0.26		0.33	0.00	0.09	0.93	53.6% 45.5%	53.6% 45.5%	0.3% 0.7%	14.2% 5.4%	0.1%	19% 52%	29.9% 27.2%
105 106 107 108 109 110		3	131	2	0.77				006			100.0%	0.5%	9.3%	1.3%	8.1%	49.4%		000		0.01	0.02	0.15	42.0%	42.0%	0.5%	6.0%	12%	10%	19.8%
108		- 5	133	2	0.76	0.01	0.00	0.01	0.06			100.0%	0.7%	9.8% 11.5%	12%	8.4% 10.6%	49.5% 50.6%	0.32	000	0.05		0.03	0.15	42.1% 44.1%	42.1% 44.1%	05%	63%	0.9%	24% 45%	19.0% 21.2%
110		9	137		0.61	0.00	0.17		0.07	0.33		100.0%	1.5%	27.3%	0.7%	11.0%	519%	0.26			0.00	0.03		42.0%	42.0%	1.3%	15.3%	0.3%	48%	19.8%
111		14	142	4	1.57	0.01	0.09	0.02	0.17	0.92		100.0% 100.0%	0.6%	5.7% 3.6%	1.1%	10.0%	58.4% 60.6%	0.76	0.01	004		0.07	0.42	48.7% 48.0%	46.7% 46.0%	0.5% 0.4%	26%	1.1%	45% 46%	26.7% 24.0%
113		16	144		1.38	0.00	0.12	0.01	0.17	38.0	_	100.0%	0.8%	8.0%	0.5%	12.6%	62.3%		001	0.08	0.00	0.07	0.36	49.1%	49.1%	0.6%	60%	0.3%	5.1%	25.7%
114		17	145		122	0.02	0.37	0.01	0.19	0.72		100.0% 100.0%	1.5%	30.0% 7.9%	0.9%	15.4%	58.7% 60.1%	0.60	002	0.22	0.01	0.09	0.34	49.3%	49.2%	13%	17.6%	05%	7.3% 64%	27.8% 28.8%
116		22	150	4	1.19	0.01	0.11	0.00	0.17	0.85		100.0%	0.8%	7.0%	0.3%	11.8%	60.9%	0.75	0.01	007	0.00	0.08	0.41	54.0%	54.0%	06%	52%	0.3%	55%	29.2%
112 113 114 115 116 117		23	151	4 10	133	0.01	0.27	0.01	0.18	0.80		100.0% 100.0%	1.0%	20.2% 5.8%	0.9%	13.5%	60.3%		0.01	018	0.01	0.08	0.30	43.9%	43.9% 50.2%	08% 05%	13.5%	0.6%	61% 59%	22.7% 29.8%
119		30	150	10	4.01	0.04	0.25	0.01	066	2.51		100.0%	0.9%	6.2%	0.3%	16.5%	62.6%	2.41	003	0.14	0.01	0.37	1.34	60.1%	60.1%	0.7%	3.4%	0.1%	9.1%	11.4%
119 120 121 122		31	159	10	195	0.06	0.15	0.01	0.60	2.69		100.0% 100.0%	1.6%	3.8% 16.0%	0.3%	15.1%	68.0%	2.48	0.05	0.09		0.31	153	62.7% 53.7%	62.7% 51.7%	14%	23%	0.2%	7.9%	38.8% 20.5%
122		33	161	10	2.72	0.03	1.02	0.03	0.65	2.52		100.0%	0.8%	27.2%	0.8%	17.5%	67.0%	1.77		064	0.01	0.31	1.19	47.3%	47.3%	06%	17.0%	0.4%	8.4%	33.5%
123 124 125 126		35	166	10	433 359	0.03	0.22		0.66			100.0% 100.0%	125	5.0% 3.7%	0.6%	15.2% 15.8%	60.1% 69.3%	2.16		012	0.03	031	133	544% 643%	544% 643%	06% 10%	28%	0.6%	7.2% 8.5%	32.7% 23.7%
125		40	168	10	2.92	0.06	0.25	0.01	0.69	2.54		100.0%	1.6%	6.3%	0.3%	17.4%	64.7%	2.40	0.06	013	0.01	0.37	1.37	61.1%	61.1%	1.5%	34%	0.2%	95%	34.9%
126		41	169	10	116	0.03	0.77	0.02	0.81	2.46	_	100.0%	0.7%	20.0%	0.5%	20.9%	63.7%	2.02	003	0.45	0.01	0.43	1.22	52.1%	52.1%	06%	11.7%	0.3%	11.0%	31.7%

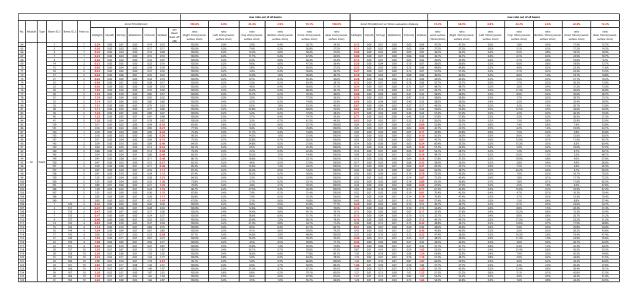
Table 6. PD of Ant M- patch antenna (28GHz - n261)

[Folder Open Status]

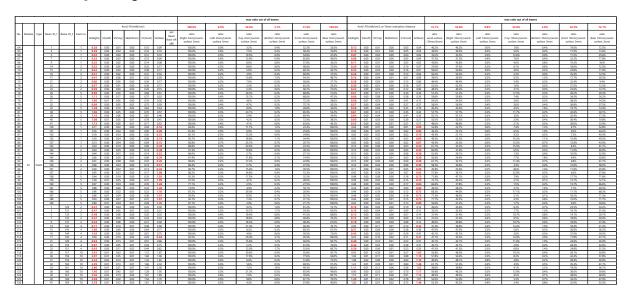
- M-patch Low CH

	-					-	-	_		-	_					max ratio ou	t of all beams					_							max ratio out of all I	bearts		
								40	m2 PD(mil	N/on2)				100.0%	0.8%	14.4%	2.0%	74.6%	100.0%	4	om2 PD(n	W/cm2) a	t 10mm evalu	ation dista	nce	71.4%	59.2%	0.6%	20.9%	2.3%	27.1%	71.4%
No. Mor	dule Typ	e Seam ID_1	Sema ID_2	Feed no.		Т	Т			Т			per Seam	ratio	ratio	ratio	ratio	ratio	ratio							ratio	ratio	ratio	ratio	ratio	ntio	ratio
				1 1	54/Rig	phe) S3(Li	e) ss	(Top)	S6(Botton	n) 51((Front)	S2(Rear)	Back-off	(Right 2mm)/(worst- surface 2mm)	(Left 2mm)/(worst- surface 2mm)	(Top 2mm)/(wonst- surface 2mm)	(Bottom 2mm)/(wont-	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont-	S4(Right)	\$3(Left)	SS(Top)	SS(Bottom)	\$1(Front)	S2(Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(worst- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Bottom 10mm)/(wont- surface 2mm)	(Front 10mm)/(worst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
-	+	٠.	-		0.21	6 60	٠.	0.01	0.00	+	013	0.10	(d0)	100.0%	0.0%	10%	0.0%	47.9%	29.2%	011	0.00	001	000	0.04	0.05	49.4%	49.4%	00%	19%	00%	16.0%	18.2%
65		3				6 00		0.02	0.00		0.14	0.11		100.0% 100.0%	0.4%	8.7%	0.8%	52.9%	40.7%	0.10	0.00	0.02	0.00	0.04	0.04	37.3%	37.3% 37.3%	0.0%	6.1% 5.5%	0.4%	15.6%	14.4%
67		7			0.2	2 0.0	-		0.00		0.14	0.09		100.0%	0.5%	9.1% 11.5%	0.5%	61.4% 66.8%	43.0% 48.4%	0.07		001	0.00	0.05	0.04	34.1%	34.1%	05% 05%	55%	0.5%	23.0%	18.6% 22.1%
68		9		1	0.21	0.0			0.00		016			100.0%	0.4%	10%	0.8%	61.7%	241% 41.5%	0.11			0.00		0.02		43.7%	0.4%	34%	0.8%	19.2%	7.7%
70		14		2 2	0.4			0.05	0.00		0.22	0.20	\vdash	100.0% 100.0%	0.2%	10.9%	0.6%	45.9% 54.5%	41.5% 30.6%	0.17	000		0.00	0.08	0.07	35.2% 48.3%	35.2% 48.3%	0.2% 0.0%	7.6%	0.6%	16.2%	14.7% 13.4%
71		16 17		2 2	0.4			0.02	0.00		0.27	0.17		100.0% 100.0%	0.2%	19%	0.4% 1.1%	56.0% 50.4%	35.1% 41.6%		000		0.00	0.10	0.08	50.6% 40.7%	50.6% 40.7%	0.2% 0.2%	25% 64%	0.2% 1.1%	20.9%	16.9% 14.9%
73		21		2	0.5	6 0.0		0.05	0.00	-	0.29	0.19		100.0%	0.2%	9.1%	0.4%	52.0%	341%	0.24	0.00	004	0.00	0.11	0.07	42.9%	42.9%	0.2%	63%	0.4%	19.1%	12.0%
74		22	_	2 2			_		0.00		0.32	0.19		100.0% 100.0%	0.2%	28%	0.2%	57.5% 54.2%	33.1% 37.8%		000		0.00	0.13	0.08	532% 482%	53.2% 48.2%	0.2% 0.2%	20%	0.2%	22.6% 19.8%	14.9%
76		29		5	10	1 02		0.30	0.00	ľ	0.73	0.43		100.0%	0.3%	29.4%	0.4%	72.7%	41.0%	0.50	0.00	0.17	0.00	0.33	0.24	50.0%	50.0%	0.2%	17.0%	0.3%	33.1%	24.2%
77		30		5			1		0.00		082	0.56		100.0%	0.4%	15.6%	03%	69:9% 71.2%	47.7% 34.1%	0.66			0.00	0.41	0.32	56.4% 59.2%	56.4% 59.2%	0.3%	80% 12%	0.2%	34.05	27.2% 19.0%
79		32		5		2 0.0	3 1	90.0	0.00	- 0	0.83	0.60		100.0%	0.4%	5.4%	0.2%	74.7%	541%	0.64	0.00	004	0.00	0.19	0.32	57.5%	57.5%	0.4%	34%	0.2%	35.1%	29.0%
80		33	 	5	1.0	0.0		0.10	0.02		088	0.44	-	100.0% 100.0%	0.3%	8.2% 23.4%	1.6%	57.9% 74.6%	37.0% 52.4%		000		0.02	0.26	0.13	47.0% 54.1%	47.0% 54.2%	0.3%	3.6% 12.5%	1.4%	22.3% 37.1%	11.0% 29.2%
82		39		5	1.1	4 02	9 1	90.0	0.00		0.78	0.53		100.0%	0.3%	5.1%	0.2%	67.8%	46.0%	0.67	0.00	004	0.00	0.19	0.29	58.7%	58.7%	0.3%	3.1%	0.2%	33.9%	25.1%
83		40		5	13	9 02		004	0.00		0.85	0.54		100.0% 100.0%	0.4%	10%	0.2%	70.9% 64.8%	45.5% 43.3%		000		0.00	0.42	0.30	57.8% 49.2%	57.8% 49.2%	0.3% 0.2%	19%	03%	25.0% 27.6%	25.2% 18.8%
85		129			0.10			0.01	0.00			0.16		64.8% 72.8%	0.0%	63% 92%	0.6%	16.4%	1000%		000		0.00	0.01	0.09	54.1% 44.7%	25.2% 20.6%	00%	3.8%	0.6%	69% 92%	541% 447%
8.7		133			0.17	0.0	2 1	0.03	0.00			0.25	_	67.0%	0.0%	96%	0.8%	14.0%	100.0%	0.05	000	0.01	0.00	0.02	0.10	44.0%	20.6% 19.9%	0.0%	6.1%	0.8%	42%	44.0%
89		135		1	0.13		, ,	0.03	0.00			0.21		80.8% 60.5%	0.0%	12.1%	0.9%	24.3% 17.9%	100.0%		000		0.00	0.02	0.11	52.3% 49.4%	26.6%	0.0%	7.0% 11.6%	05%	52% 55%	52.3%
90		142			0.11			0.09	0.00			0.16	\vdash	85.0%	0.2%	22.1%	0.2%	20.1%	1000%	0.14	0.00	0.06	0.00	0.03	0.25	60.0%	35.0%	0.2%	13.5%	0.2%	7.6%	60.0%
91		143		2	0.44			0.04	0.00		0.09	0.59		75.0% 72.3%	0.2%	7.3% 2.2%	0.2%	15.8%	100.0%		000		0.00	0.04	0.32	54.2% 55.0%	27.0% 26.8%	0.2% 0.2%	42% 03%	0.2%	59%	54.2% 55.0%
93		145		2	0.23	3 0.0		002	0.01	-	300	0.29		58.9%	0.3%	5.6%	1.8%	14.5%	100.0%	0.09	0.00	0.01	0.01	0.02	0.20	49.7%	22.4%	0.3%	3.6%	1.3%	5.9%	49.7%
94 95 M 96		149 h 150	_	2	0.42			0.07	0.01		0.09	0.50		82.3% 74.4%	0.2%	14.1%	1.0%	16.9%	100.0%	0.15	0.00		0.00	0.03	0.29	56.7% 51.2%	30.2% 30.0%	0.2% 0.2%	93%	0.8%	60% 7.5%	96.7% 98.2%
96		151		2	0.33	7 0.0	2 1	90.0	0.01	- 0	0.00	0.49		74.9%	0.2%	11.9%	12%	16.6%	100.0%	0.11	0.00	0.04	0.01	0.03	0.22	47.0%	22.4%	0.2%	72%	1.0%	66%	47.0%
97		157		5	0.95		2		0.00			1.07	_	89.3% 83.6%	0.2%	344%	0.4%	13.5%	100.0%		000		0.00	0.07	0.58	54.5% 71.1%	36.2% 45.2%	0.2% 0.1%	20.9%	0.3%	61%	54.5%
99		159		5	1.12	2 0.0	9 1	0.04	0.00	-	0.20	1.27		81.6%	0.2%	25%	0.1%	14.4%	100.0%	058	0.00	0.02	0.00	0.10	0.98	71.3%	42.4%	0.2%	1.6%	0.1%	7.4%	71.2%
101		160	-		0.89			0.04	0.00		0.28	1.40		71.7%	0.3%	2.8%	02%	20.3%	100.0%		000		0.00	0.15	0.62	64.7% 47.7%	35.0% 25.9%	0.3%	19%	0.2% 1.8%	10.6%	64.7% 47.7%
102		166		- 5	1.00			028	0.00		0.21	1.22		85.6%	0.1%	22.9%	0.3%	17.0%	100.0%		000		0.00	0.10	0.81	65.9% 70.2%	41.7% 41.4%	0.1%	12.1%	0.2%	85%	65.9% 31.2%
104		167		5	100			0.10	0.00		0.24	1.27		81.7% 81.6%	0.2%	8.7% 4.6%	0.1%	19:0% 17:4%	100.0%		000		0.00	0.13	0.90	70.2%	43.4% 41.8%	0.2% 0.2%	4.1% 3.0%	0.1%	10.4%	70.2% 71.4%
305		169	129	5	0.95			003	0.01		0.23	0.12		67.0% 100.0%	0.2%	1.8%	0.5%	16.1%	100.0%		000	662	0.01	0.11	0.81	56.9% 50.1%	29.1%	0.2%	12%	0.6%	7.9%	56.9% 17.2%
107		3	131		0.4	6 0.0		0.06	0.01	-	0.23	0.37		100.0%	0.2%	12.0%	22%	50.4%	81.0%	0.15	000	004	0.01	0.08	0.16	43.0%	31.9%	0.2%	8.1%	1.7%	16.8%	40.0%
108		5 7	133		0.42	9 00		005	0.00			0.42		99.3% 100.0%	0.5% 0.5%	12.2%	0.7% 0.7%	46.2% 56.2%	100.0% 92.7%		000		0.00	0.07	0.18	43.1%	31.6% 32.3%	0.2% 0.2%	8.1% 7.8%	0.7% 0.7%	16.7%	43.1%
110		9	137	2	07	0.0		000	0.00	-	0.23	0.31		100.0%	0.8%	20.4%	1.1%	61.4%	81.7%	0.15	0.00	004	0.00	0.09	0.13	40.7%	40.7%	05%	11.6%	0.8%	22.5%	34.1%
111		14	142		0.7	9 00	_		0.01			0.67		100.0% 100.0%	0.3%	19.4%	1.0%	43.8% 52.4%	87.2% 72.1%		000		0.01	0.14	0.36	46.2% 41.6%	36.3% 43.6%	0.3% 0.2%	12.7%	0.8%	18.0%	46.2% 36.1%
113		16	144	4	1.00	2 0.0		0.04	0.01	-	054	0.91		100.0%	0.3%	17%	0.6%	52.7%	88.6%	0.41	0.00	0.03	0.01	0.24	0.52	52.6%	40.1%	0.2%	24%	0.5%	23.1%	50.6%
114		17	145	4	0.54		2 1	0.13	0.02		0.36	0.70		91.4% 100.0%	0.6%	19.3%	26%	51.7% 55.2%	100.0%		000		0.02	0.14	0.33	47.6% 42.6%	37.0% 38.2%	0.4%	9.4%	22% 12%	20.1%	47.0% 42.6%
116		22	150	- 4	0.90	0.0	3 1	90.0	0.01	Ü	0.52	0.80		100.0%	0.2%	5.6%	0.7%	52.7%	80.9%	0.44	0.00	003	0.01	0.23	0.44	44.4%	44.3%	0.2%	3.1%	0.5%	23.5%	44.4%
117		23	151	10				0.09	0.02		1.21	1.87	-	100.0% 100.0%	0.3%	10.5%	12%	43.7% 59.8%	80.5% 92.3%		0.00		0.01	0.17	1.06	41.0% 52.5%	41.0% 41.5%	0.3%	11.6%	1.4%	19.4%	22.4% 52.5%
119		30	158	10	2.31	9 02		0.35	0.01		1.60	2.15		100.0%	0.3%	14.8%	0.4%	66.7%	89.9%	1.12	0.01	018	0.01	0.86	1.22	55.4%	46.7%	0.3%	7.4%	0.3%	36.0%	55.4%
120		31	159	10		0.0	Η		0.01			2.64	-	100.0% 98.6%	0.4%	19% 57%	0.3%	53.0% 66.5%	91.4% 100.0%		0.01		0.01	0.63	1.35	53.9% 63.5%	49.0% 48.3%	0.3%	23% 39%	0.3%	27.8% 33.5%	59.9% 63.5%
122		33	161			0.0			0.07			2.52		98.7%	0.4%	7.7%	28%	52.8%	100.0%				0.06	0.51	1.07	42.4%	38.3%	0.3%	34%	23%	20.1%	42.4%
123		38	166 167		21			0.46	0.02		1.51 1.46	2.12	\vdash	100.0% 100.0%	0.2%	19.7% 80%	0.6%	64.3% 63.2%	92.4% 92.3%	1.13	0.00	0.10	0.00	0.81	1.29	55.0% 55.2%	45.7% 48.8%	0.2% 0.3%	13.9% 4.2%	0.5% 0.1%	34.4% 34.3%	55.0% 55.2%
125		40	168	10				0.15	0.02		1.46	2.25		100.0% 100.0%	0.4%	62% 31%	0.7%	63.3% 57.4%	95.9% 95.0%		001			0.74	1.46	62.3% 52.5%	50.8% 41.8%	0.3%	4.1% 1.6%	0.6%	31.4% 25.8%	62.9% 52.5%
129		- 41	199	10	10	- 00		U-29	uol		1.74	7.00		100.0%	0.4%	A1%	03%	57.4%	35,0%	127	cut	005	002	0.76	1.59	34.5%	41.8%	0.3%	1.6%	0.8%	- 45	34.3%

- K-patch Mid CH



- M-patch High CH



[Folder Closed Status]

- M-patch Low CH

No. Section Processing	
	40.5%
	ratio
1	
The column The	19.5%
The color of the	20.1% 38.6%
The column The	31.4%
The column The	18.9% 19.1%
The color of the	25.2% 19.5%
The color of the	28.5%
The column The	24.1% 18.2%
The column The	19.8% 35.8%
1	36.5%
The column 1	36.8% 27.0%
The column The	30.1%
## 1	36.8% 35.3%
1	30.2% 38.5%
TO 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	24.2%
The column The	18.9% 20.7%
The column The	19.3% 22.6%
The column The	26.0%
No.	27.7%
1	28.6%
The column The	24.9% 28.6%
The column The	27.4% 31.6%
The column The	23.9%
	29.2%
	30.1%
The column The	29.5%
1	40.5% 36.3%
T	23.8%
TO UT 1 12 12 13 14 15 15 15 15 15 15 15 15 15 15 15 15 15	15.8% 18.2%
17 18 18 18 18 18 18 18	17.7% 17.2%
\$\begin{array}{cccccccccccccccccccccccccccccccccccc	28.4%
15 27 16 4 17 56 66 17 18 18 18 18 18 18 18	25.4%
2 19 1 10 10 10 10 10 10 10 10 10 10 10 10 1	31.9%
118 29 157 10 247 050 059 050 059 050 059 050 059 050 059 050 050	26.7% 27.0%
	27.2% 11.0%
119 20 158 10 153 004 034 030 061 063 222 1000% 1.1% 97% 04K 180% C80% 214 003 016 001 035 120 005% 068 07% 44% 02% 100	34.0%
132 13 15 15 15 15 15 15 15	33.3% 30.1%
122 33 Mt 59 3.19 568 568 568 527 19685 185 1978 227 1968 1878 227	12.5% 11.6%
124 29 167 10 1.43 054 0.77 0.07 067 2.04 100.0% 1.78 4.8% 0.3% 19.6% 59.6% 2.21 0.04 0.10 0.01 0.39 1.30 64.5% 64.5% 1.0% 2.8% 0.1% 11.4	32.2%
135 40 568 109 1244 568 510 524 568 510 507 577 1578 5058 5178 5178 5178 5178 5178 5178 5178 51	31.6% M.7%

- M-patch Mid CH

$\overline{}$					_						-					max ratio ou	t of all beams					-							max ratio out of all	beams		
\vdash	Т		Т	Т	Т			-	lcm2 PD(m	nW/on2)				100.0%	1.0%	\$2.1%	1.0%	11.7%	100.0%	-	Tom2 PD(m	W/cm2) a	rt 10mm evalu	uation distr	ance	69.7%	69.7%	225	29.5%	1.9%	19.0%	49.63
No. 1	Applied Ty	pe Seam S	o_1 Sema	ID_2 Fe	red no.				П	Т	Т		per Seam	ratio	ratio	ratio	ratio	ratio	ntio			П			Т	ratio	ratio	ratio	ratio	ratio	ntio	ratio
	- 1				- 1	S4/Right)	S3(Left)	SS(Top)	S6(Botto	om) \$1()	Front)	S2(Rear)	Back-off	(Right 2mm)/(worst- surface 2mm)	(Left 2mm)/(wonst- surface 2mm)	(Top 2mm)/(wonst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	54/Right	S3(Left)	SS(Top)	SS(Bottom)	S1(Front)	(\$2(Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(wont- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Sottom 10mm)/(wont- surface 2mm)	(Front 10mm(/(wonst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
64	_	1		#	1	0.27	0.00	0.01	0.00		106	0.10	(dB)	100.0%	0.8%	41%	0.4%	22.2%	38.7%	0.14		001	0.00	0.03	0.05	541%	54.1%	04%	19%	0.4%	10.9%	17.3%
65		5		_		0.12	000	0.02	0.00	-		0.12		100.0% 100.0%	1.3%	8.4% 36.6%	0.9%	15.4% 21.6%	51.1% 78.4%		000		0.00	0.02	0.05	45.4% 51.5%	45.4% 51.5%	13%	5.3% 17.9%	0.4%	7.0%	17.6% 38.1%
66 67 68 69 70 71 72		7		-		0.14	0.00	0.03				0.12		100.0% 100.0%	2.2%	21.2%	22% 16%	26.3% 15.6%	83.9% 46.4%	0.07	000	001	0.00	0.02		41.9% 31.5%	48.9% 38.5%	2.2% 1.0%	10.2% 16.1%	0.7%	12.4% 7.8%	37.2% 19.8%
69 70		14		7		0.41	0.01	0.04	0.01		106	0.20		100.0%	1.7%	92%	12%	15.5% 25.2%	41.0%	0.16	0.01	003	0.00	0.03		29.6% 56.1%	29.6% 56.2%	14%	60% 43%	0.5%	7.0%	20.0% 16.8%
71		16	_			0.53	0.00	0.03	0.00			0.24		100.0% 100.0%	0.8% 2.2%	5.3% 46.4%	0.4%	23.5% 16.0%	45.8% 62.3%	0.31	000		0.00	0.06		58.5% 36.6%	58.5% 36.6%	06% 22%	19%	02% 19%	12.0%	21.4%
73		21		_	2	0.44	65	0.04	0.00	- 0	:08	0.21		100.0%	1.6%	8.2%	0.9%	19.0%	47.6%	0.18	0.01	003	0.00	0.04		41.9%	41.9%	1.1%	59%	0.5%	19%	20.6%
72. 74. 75. 76. 77. 77. 78. 90. 80. 81. 82. 83. 84. 85. 86. 87. 88. 89. 90. 90. 90. 90. 90. 90. 90. 90. 90. 9		22		_	2	0.56	0.00	0.02	0.00		112	0.25		100.0% 100.0%	0.5%	1.4% 6.4%	0.4%	25.1% 22.9%	45.5% 46.0%	0.36		001	0.00	0.07		642% 55.9%	64.2% 55.9%	0.4%	22% 25%	02%	12.0%	18.8% 22.5%
76		29 30	-	7		0.45	0.01	0.25	0.02		128	0.48		93.9% 100.0%	2.3%	53.1% 17.4%	3.8%	21.5% 31.5%	100.0%	0.49	0.01	0.14		0.16		49.1% 55.2%	48.0% 55.2%	19%	29.5% 11.5%	1.7%	9.3% 17.7%	49.1% 45.0%
76		31		=	5	1.00	0.03	0.06	0.01		128	0.53		100.0% 100.0%	2.3%	5.8% 8.2%	0.6%	30.3% 26.9%	49.4%		0.02	003	0.00	0.20		69.1% 56.1%	69.1% 56.2%	19%	27% 42%	0.4%	16.6%	28.1% 31.7%
80		33		_		0.92	0.02	0.27	0.02		110	0.60		100.0%	1.8%	29.2% 28.1%	20%	10.4% 25.6%	65.4% 100.0%	0.27	602	0.08	0.02	0.04	0.32	40.1% 49.6%	40.1% 44.2%	17%	9.1% 18.5%	1.6%	47% 14.2%	34.5%
82		39			5	1.07	0.03	0.00	0.01		0.36	0.62		100.0%	2.3%	7.0%	0.6%	33.7%	57.9%	0.73	0.02	004	000	0.20	0.37	68.1%	68.1%	1.8%	3.7%	0.3%	19.0%	34.0%
83		40		\pm	5	1.17	0.02	0.10	0.01	- 6	131	50 00		100.0%	1.0%	9.7% 15.3%	0.5%	31.2% 12.6%	50.0% 78.7%	0.62	001	005	0.01	0.18	0.27	61.8% 45.9%	61.8% 45.9%	12%	47% 53%	0.3%	18.2% 7.0%	26.6% 44.2%
85		129		-	1	0.29	0.00	0.02	0.00		102	0.19		100.0% 100.0%	0.3%	64%	0.7%	55% 52%	65.7% 50.0%	0.11	000	0.01	0.00	0.01	0.07	22.4% 41.2%	39.4% 41.2%	0.3%	45%	0.7%	2.4%	24.6% 17.8%
8.7		133		-	1	0.16	0.00	0.03	0.00		102	0.20		100.0% 100.0%	0.3%	7.8% 11.3%	0.0%	53%	549% 543%	0.16	000	0.02	000	0.01	0.07	45.1% 45.8%	45.1% 46.8%	0.3%	53% 64%	0.3%	22% 26%	20.1% 20.5%
89		137		#	1 2	0.28	0.00	0.05	0.00	- 0	102	0.17		100.0%	0.4%	18.0%	0.4%	63% 73%	58.1% 63.6%	0.12	000	0.02	0.00	0.01	0.07	45.8% 53.4%	45.8% 53.4%	00% 02%	85% 10.1%	0.4%	25% 11%	22.9%
91		143		_	2	0.81	0.00	0.05	0.00	- 6	106	0.52		100.0%	0.1%	6.0%	0.1%	7.7%	63.3%	0.46	000	0.03	0.00	0.03	0.22	57.1%	57.1%	0.1%	41%	0.0%	1.2%	27.3%
92		145	_	-	2	0.03		0.05	0.01	-	104	0.54		100.0% 100.0%	0.1%	1.7% 9.0%	02% 12%	7.9%	64.9%		000	0.01	0.01	0.03	0.14	58.6% 45.8%	58.6% 45.8%	0.1%	0.8% 5.7%	12%	14% 24%	28.9% 23.9%
94	M Pa	149 nch 150				0.72	0.00	0.09				0.44		100.0% 100.0%	0.1%	12.3%	0.4%	6.4%	61.7%	0.37	000	0.06		0.02		\$1.8% \$7.6%	51.8% 57.6%	01%	77%	0.3%	26%	25.5% 28.4%
96		151		-	2	1.95	0.00	0.07			104	0.38		100.0% 100.0%	0.3%	10.8%	0.8% 0.2%	6.7% 7.5%	61.7% 65.6%	0.30	000	0.04		0.02		49.4% 51.8%	49.4% 53.8%	0.2% 0.2%	64% 17.4%	0.7%	29% 14%	26.8% 31.6%
98		150	-	=	5	1.94	655	0.21	0.00	-	123	1.35		100.0% 100.0%	0.3%	11.0%	0.1%	11.9% 12.4%	69.6% 68.6%	1.26	000	007		0.11	0.76	64.8% 65.1%	64.8% 65.1%	0.2%	36%	0.1% 0.1%	5.7% 7.0%	29.1% 38.2%
100		160	\neg	\neg	5	1.74	0.00	0.03	0.00	ľ	20	1.26		100.0%	0.2%	1.7%	0.1%	11.4%	72.5%	1.14	0.00	0.02	0.00	0.12	0.70	65.9%	65.9%	01%	1.0%	0.1%	5.6%	40.2%
101		161 166				1.81 2.06	0.01	0.38	0.00		20	1.10		100.0% 100.0%	0.3%	65% 18.5%	1.5%	9.7%	60.6%	1.23		0.18	0.02	0.06	0.74	48.3% 59.7%	48.2% 59.7%	0.3%	34% 88%	13%	11% 45%	26.6% 35.7%
101		167			5 5	1.79	0.00	0.05			122	1.22		100.0% 100.0%	0.3%	47% 13%	0.1%	12.5%	68.2% 70.9%		000	002	0.00	011 011		664%	64.4% 66.4%	0.2%	1.1%	0.1%	6.3% 6.7%	37.9% 40.2%
105		169	12		5	1.83	0.00	0.09				1.25		100.0% 100.0%	0.2%	46% 60%	0.5%	8.7% 14.1%	68.3% 55.5%		000	0.04	0.01	0.08		57.2% 46.4%	57.2% 46.4%	01%	24%	0.4%	42% 66%	34.1% 24.0%
107		3	13		2	0.69	0.00	0.05				0.32		100.0%	0.7%	7.9%	0.6%	9.6% 10.8%	46.6% 53.3%	0.30	000	0.03		0.03	0.11	44.1%	44.1% 49.4%	00%	50% 10.6%	0.4%	44%	15.8% 16.2%
322		7	12	5	2	0.50	0.00	0.07	0.01	-	006	0.29		100.0%	0.8%	11.4%	0.8%	12.5%	41.4%	0.29	0.01	004	0.00	0.03	0.12	48.2%	48.2%	0.8%	60%	0.5%	5.5%	19.4%
110 111 112		14		2		0.57	0.00	0.11	0.00	-	110	0.26		100.0% 100.0%	0.5% 1.4%	18.3%	0.7% 1.1%	11.5%	49.6% 62.2%	0.42		0.06	0.00	0.03	0.27	41.0% 46.2%	41.0% 46.2%	05% 12%	12.7%	0.5%	56%	16.6% 29.9%
112		15				1.16	0.01	0.11				0.71		100.0%	0.7%	8.3% 3.5%	0.3%	16.3%	52.6% 55.8%	0.81	001		000	0.11		59.8% 58.0%	59.8% 58.0%	05%	55% 16%	0.1%	80% 66%	23.8%
114		17	14	5		0.86	0.01	0.18	0.02			0.58		100.0% 100.0%	1.0%	20.4%	20%	92%	67.6% 59.0%	0.42	0.01	0.08	0.02	0.04	0.25	49.0% 50.6%	49.0% 50.0%	1.0%	8.9% 10.5%	1.7%	45% 7.1%	29.1%
113 114 115 116 117		22	15	2		1.44	0.00	0.17	0.00	- 0	123	0.63		100.0%	0.3%	42% 92%	02%	15.7% 15.0%	58.9% 58.9%	0.91	000	004	0.00	0.11	0.37	63.3% 55.0%	63.3% 53.0%	0.7% 0.2% 0.4%	24% 48%	0.1% 0.6%	7.5% 7.8%	25.8% 27.4%
		29	15	,	10	2.65	0.02	0.72	0.03	-	126	1.72		100.0%	0.8%	27.3%	0.9%	10.4%	65.1%	1.40	0.02	0.46	0.01	0.12	0.89	53.0%	53.0%	0.6%	17.2%	0.5%	45%	33.0%
119		30	15		10	2.16 2.40	0.05	0.31	0.01		158 173	2.00	_	100.0% 100.0%	1.6%	99% 12%	0.2%	18.2% 21.5%	63.4% 62.1%	1.95	004	017	0.01	0.32	1.14	61.6%	61.6%	12%	53% 14%	0.2%	10.1%	11.9% 11.2%
121		32 33				2.45 2.16	0.03	0.19	0.01			2.10		100.0% 100.0%	0.8%	5.4% 16.3%	02% 18%	17.8% 7.2%	60.8% 71.3%		002	0.10	0.01	0.34		64.9% 41.0%	64.9% 43.0%	05%	29%	0.2% 1.7%	10.0%	31.2% 34.1%
123		35				2.10	0.04	0.49	0.01	ľ		2.03		100.0% 100.0%	125	15.7%	0.4%	15.1%	65.5% 60.1%		003	0.28	0.01	025	1.05	55.7% 65.9%	55.7% 65.9%	09%	90%	02%	7.9% 12.0%	34.0% 32.5%
120 121 122 123 124 125 126		40	16		10	1.05	622	0.18	0.01	ľ	566	1.66		100.0%	0.7%	59%	0.4%	21.0%	61.6%	2.12	0.02	0.09	0.01	0.37	0.96	69.5%	69.5%	06%	2.8%	0.3%	12.2%	32.0%
126		- 41	16	_	10	1.15	0.02	0.36	0.02		136	2.52		100.0%	0.6%	10.8%	07%	10.9%	75.1%	1.87	602	u17	0.02	0.19	1.36	55.9%	55.9%	05%	5.1%	06%	58%	40.5%

- M-patch High CH

	2.3% 26.3% 22.3% 2	io natio natio natio nm//wont- (Front 10mm//wont- (Rear 10mm//wont-
	Left 30mm /(worst- surface 3mm)	nni//worst- (Front 10mm)//worst- (Rear 10mm)//worst-
Second Column Second Colum	surface 2mm) surface 2mm) surface 2 0.4% 2.6% 0.4% 1.5% 6.4% 0.5% 2.1% 12.1% 0.7% 2.2% 13.2% 0.7%	
	04% 2.6% 0.4% 1.5% 6.4% 0.5% 2.1% 12.1% 0.7% 2.2% 11.2% 0.7%	
The color of the	21% 12.1% 0.7% 22% 13.2% 0.7%	
The color of the	22% 13.2% 0.7%	
1		% 14.7% 29.0%
The color of the	15% 69% 05%	
1	10% 39% 02%	5 11.05 17.25
1	04% 19% 02% 23% 229% 19%	
1	14% 55% 05% 04% 17% 02%	
1	06% 5.1% 0.4%	% 11.1% 23.9%
The column The	20% 35.3% 2.2% 1.9% 12.0% 0.3%	
The column The	13% 22% 03%	% 19.9% 21.2%
2	14% 42% 0.4% 17% 119% 1.6%	
## Company Com	2.3% 15.3% 0.7% 1.3% 1.9% 0.3%	
1	16% 59% 04%	5. 16.6% 27.4%
THE	13% 58% 0.7% 0.2% 46% 0.7%	
10	03% 43% 05%	% 2.1% 18.5%
TO THE PARTY OF TH	0.7% 45% 0.6% 0.7% 60% 0.3%	
1	0.0% 9.5% 0.4%	% 2.6% 22.6%
1	02% 10.5% 0.3% 0.1% 4.1% 0.1%	% 2.4% 26.6%
THE THE PROPERTY OF THE PROPER	01% 1.1% 0.2% 0.3% 5.8% 1.0%	
FF 12 3 113 500 514 505 155 155 155 155 155 155 155 155 155	01% 7.7% 0.4%	% 2.7% 25.8%
FF 12 3 113 500 514 505 155 155 155 155 155 155 155 155 155	01% 18% 0.1% 0.2% 6.2% 0.8%	
99 150 5 160 000 002 000 022 114 10005 0.25 145 0.15 1145 6815 100 000 001 000 012 064 6505 6505	01% 16.4% 0.2% 0.3% 3.8% 0.1%	
	0.1% 0.7% 0.1%	% 7.0% 37.9%
1001 101 1 101 1 101 1 101 1 101 1 101 1 101 1 101 1 101 1 101 1 101 1 101 1 101 1 101 1 101 1 101 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	01% 18% 01% 02% 32% 1.2%	
102 166 5 2,00 0.01 0.09 0.00 0.19 1.36 100.0% 0.4% 19.5% 0.1% 9.5% 68.0% 1.19 0.01 0.19 0.00 0.09 0.72 59.4% 59.4%	0.3% 9.5% 0.1%	% 44% 36.2%
154 168 5 1.00 0.00 0.06 0.01 0.21 1.12 10.0% 0.2% 1.7% 0.4% 11.2% 66.6% 1.06 0.00 0.03 0.01 0.11 0.03 66.0% 66.0%	02% 10% 0.1% 0.2% 2.1% 0.3%	
95 196 5 1.78 600 121 601 617 122 1000 107 122 1000 10 107 122 1000 108 618 618 648 648 648 648 648 648 648 648 648 64	02% 15% 04% 05% 17% 05%	
137 3 131 2 065 001 005 000 006 0.33 100.0% 1.1% 84% 0.6% 8.7% 52.6% 0.29 0.01 0.03 0.00 0.03 0.12 45.4% 45.4%	09% 50% 0.6%	% 4.3% 18.6%
55 133 2 0.57 0.01 0.57 0.00 0.05 0.03 100.05 0.08 13.05 0.09 0.07 10.05	07% 77% 0.7% 11% 67% 0.5%	
110 9 137 2 055 007 011 007 006 029 1000% 09% 197% 13% 114% 522% 022 000 006 000 003 010 406% 406%	05% 11.1% 0.7%	
111 14 142 4 0.01 0.01 0.01 0.07 0.02 100.00 0.02 100.00 115 100.00 0.02 115 100.00 100 0.00 0.00 0.00 0.00 0.00	1.0% 12.9% 0.7% 0.6% 5.2% 0.2%	
113 16 144 4 144 001 008 001 010 005 1000 005 1000 100 005 1000 100 005 1000 105 100	03% 31% 02% 11% 114% 22%	% 67% 26.1%
115 21 149 4 1.00 001 0.16 0.01 0.14 0.72 100.0% 1.2% 14.9% 0.8% 12.8% 66.5% 0.55 0.01 0.10 0.01 0.08 0.30 52.8% 50.8%	09% 9.1% 0.7%	% 7.1% 27.4%
115 22 150 4 1.59 000 005 000 027 0.50 1000% 006 478 0.50 1000% 006 027 0.50 1000% 006 028 4.7% 0.2% 15.7% 15.6% 0.2% 0.04 001 0.07 0.07 0.00 0.01 0.08 0.08 0.07 0.08 0.09 0.00 0.00 0.00 0.00 0.00 0.00	0.3% 2.2% 0.2% 0.4% 6.4% 0.6%	
118 29 157 10 247 002 066 003 030 187 1000% 0.7% 268% 1.3% 12.1% 75.9% 1.31 001 041 002 0.15 088 51.2% 53.2%	05% 16.5% 0.6%	% 60% 35.9%
220 27 280 29 20 27 280 29 20 27 280 29 20 20 20 20 20 20 20 20 20 20 20 20 20	12% 64% 0.1% 0.7% 16% 0.2%	
121 22 160 10 129 003 023 0.01 0.57 2.01 100.0% 0.8% 6.8% 0.3% 17.2% 61.3% 2.15 0.03 0.12 0.01 0.32 1.07 65.4% 65.4%	08% 37% 02%	
122 38 166 10 2.81 0.94 0.48 0.02 0.46 2.13 10.0% 1.5% 17.2% 0.6% 16.4% 75.7% 1.59 0.03 0.29 0.01 0.26 0.07 56.4% 56.4%	0.9% 7.4% 1.6% 1.1% 90.5% 0.3%	
124 99 147 10 133 004 015 007 074 147 1009% 138 44% 03% 227% 557% 1218 003 004 000 004 157 657% 657% 138 44% 03% 227% 557% 1218 003 004 000 004 157 657% 657% 1048 207% 657% 044% 207% 657% 657% 1048 207% 657% 657% 1048 207% 657% 1048 207% 657% 1048 207% 657% 1048 207% 657% 1048 207% 104		
125 40 584 10 140 200 021 025 021 025 100 100 100 100 100 100 100 100 100 10	08% 23% 01% 07% 13% 03%	% 11.5% 31.6% % 5.8% 44.6%

Table 7. PD of Ant M – patch antenna (39GHz – n260)

[Folder Open Status]

- M-patch Low CH

_				-	_	-			-					max ratio ou	t of all beams	-		_		-			-				max ratio out of all	beams		
H		T	Г	Т			- 4	cm2 PD(mW)	(cm2)			100.0%	0.8%	19.9%	2.6%	\$4.3%	66.5%	١.	4cm2 PD/m	W/cm2) a	rt 10mm evalu	uation distr	whore	60.9%	61.9%	0.7%	27.2%	2.2%	26.2%	34.9%
No. Mo	dule Type	Seam ID_1	Sema ID,	2 Feed no.			Г			П	per Seam	ratio	ratio	ratio	ratio	ratio	nsio		Т	Г			Т	ratio	ratio	ntio	ratio	ratio	ntio	ratio
					S4(Right)	S3(Left)	SS(Top)	S6(Bottom)	\$1(Front	S2(Rear	Back-off	(Right 2mm)/(wont- surface 2mm)	(Left 2mm)/(wont- surface 2mm)	(Top 2mm)/(wonst- surface 2mm)	(Sottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	S4(Right	53(Left)	SS(Top)	SS(Bottom)	\$1(Front)	(52(Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(wont- surface 2mm)	(Left 10mm)/(wonst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Sottom 10mm(/(worst- surface 2mm)	(Front 10mm(/(wont- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
64	_	1		1	0.26	0.00	0.02	0.00	0.10	0.10	(dil)	100.0%	0.4%	65%	0.8%	39.5%	29.8%	0.11	0.00	001	0.00	0.03	0.04	42.9%	42.9%	00%	425	0.8%	12.6%	15.7%
66		5		1	0.29		002	0.00	0.11			100.0% 100.0%	0.3%	6.5% 10.4%	0.7%	38.4% 37.3%	46.9% 51.3%				0.00		0.07		41.2% 41.2%	0.3% 0.0%	44% 68%	0.7%	12.2%	19.4% 23.4%
66 66 66 771 772 774 775 775 775 86 86 87 88 88 88 88 88 88 88 88 88 88 88 88		7 9	-	1	0.10	0.00	0.04		011	0.14	-	100.0% 100.0%	0.3%	13.1%	0.7% 1.1%	37.2% 37.0%	48.0% 25.2%	0.12	000		0.00	0.04		42.6%	40.6% 44.2%	0.3% 0.0%	8.1% 4.4%	0.3%	11.7%	22.8% 11.2%
69		14 15		2	0.60	0.00	0.13	0.00	0.18	0.26		100.0%	0.3%	22.0% 7.6%	0.7%	30.6% 37.0%	46.9% 45.5%	0.18	000	0.09	0.00	0.06		29.9% 29.4%	29.9%	0.3% 0.0%	54.2% 5.1%	0.7%	10.4%	19.9% 21.0%
71		16		2	0.54	0.00	0.03	0.00	0.24	0.28		100.0% 100.0%	0.6%	6.3% 12.0%	0.2%	45.3% 31.6%	51.7% 42.6%		000		0.00	0.09	0.15	55.0% 33.3%	55.0% 33.2%	0.4% 0.4%	32% 81%	02%	17.5%	28.2% 19.2%
72		21		2	0.66	0.00	0.11	0.01	0.26	0.34		100.0%	0.2%	17.1%	0.9%	38.9%	52.0%		000	0.07	0.01	0.10	0.16	41.0%	43.0%	0.2%	11.2%	0.8%	15.6%	23.9%
74		22	-	2	0.60	0.00	0.02	0.00	0.27	0.28	-	100.0% 100.0%	0.0%	19%	0.5%	44.8% 36.7%	45.6% 43.8%	0.30	000	002	0.00	0.11		50.7% 41.6%	50.7% 43.6%	0.0%	27% 83%	0.5%	17.8%	25.0% 22.4%
76 77		29 30		5	1.12	0.00	0.45	0.02	0.39	0.74		100.0%	0.3%	39.9% 14.5%	12%	35.2% 46.1%	665% 452%		000		0.02	0.17		29.6% 52.9%	29.6% 52.9%	0.2%	27.3% 85%	1.4%	15.2% 22.0%	32.3% 28.2%
78		31 32		5	1.42	0.00	0.04	0.01	0.70	0.77		100.0% 100.0%	0.1%	2.6% 6.0%	0.4%	48.7% 47.4%	542% 45.7%		000	002	000	0.31		56.6% 52.7%	56.6% 52.7%	0.1% 0.5%	12% 33%	0.3%	21.7%	29.4% 27.5%
80		33		Š	1.12	0.00	0.35	0.01	0.37	0.59		100.0%	0.4%	31.4% 26.5%	05%	32.4% 39.2%	52.7% 60.3%	0.48	000	0.25	0.01	0.16	0.34	42.6% 45.7%	42.6% 45.7%	0.4%	21.9% 17.9%	0.4% 2.1%	14.5%	30.1% 34.9%
82		39		5	1.38	0.00	0.16	0.00	0.75	0.74		100.0%	0.1%	10.2%	0.1%	48.3%	47.6%	0.63	000	0.06	0.00	0.26	0.45	53.1%	53.7%	0.1%	37%	0.1%	21.7%	29.3%
83 84		40		5	1.19	0.01	0.03	0.01	0.59	0.62	-	100.0% 100.0%	0.5%	18.6%	0.5%	50.0% 42.0%	52.5% 47.5%	0.68	001	0.02		0.28		57.0% 50.4%	57.0% 50.4%	0.4% 0.7%	1.5%	0.4%	23.3%	29.7% 30.1%
85		129		1	0.21	0.00	0.00	0.00	0.09	0.09		100.0%	0.0%	5.2% 4.7%	0.5%	40.8%	29.9% 42.5%	0.11	0.00	001	0.00	0.03		50.2% 51.2%	50.2% 51.2%	00%	33% 30%	0.0%	14.1%	15.0%
8.7		133		1	0.19	0.00	0.04		013	0.16		100.0% 100.0%	0.0%	10.0%	0.3%	34.1%	29.7% 21.3%	0.18	000	0.02		0.03	0.07	47.2% 46.1%	47.2% 46.1%	00% 00%	59% 58%	0.3%	85% 11.9%	18.2%
89		137		1	0.10	0.00	0.02	0.00	013	0.12		100.0%	0.3%	7.0%	0.3%	44.5%	38.9%	0.15	0.00	001	0.00	0.04	0.05	43.5%	48.8%	0.0%	33%	0.3%	14.0%	15.9%
91		142		2	0.72	0.00	0.09	0.00	0.24	0.20	_	100.0% 100.0%	0.1%	12.6%	0.4%	32.5% 42.9%	28.0%	0.28		005		0.08		29.3% 54.9%	39.3% 54.9%	01%	75% 9.1%	0.4%	10.9%	12.0%
92		144		2	0.64	0.00	0.02	0.00	0.23	0.37		100.0% 100.0%	0.2%	18% 65%	0.2%	15.8% 31.7%	57.5% 17.1%	0.38	000	002	0.00	0.09		59.5% 43.1%	59.5% 43.1%	0.2% 0.2%	24%	0.2%	13.5%	26.5% 18.8%
94	d Page	149		2	0.78	0.00	0.13	0.01	0.23			100.0% 100.0%	0.1%	17.1%	0.8%	29.3%	30.7% 47.0%	0.30	0.00	607	0.01	0.07		38.9%	38.9% 66.2%	01% 02%	95% 45%	0.6%	9.0% 19.7%	13.3% 23.2%
96	742	151		2	0.31	0.00	0.03	0.00	0.33	0.28		100.0%	0.1%	45%	0.6%	46.0%	29.7%	0.38	000	0.02	0.00	0.11	0.12	53.1% 58.5%	53.7%	0.1%	28%	0.6%	15.0%	16.5%
98		157		5	1.50	0.00	0.34	0.01	0.71	0.76		100.0% 100.0%	0.2%	14.8% 22.5%	0.8%	44.8% 47.2%	42.4% 52.4%	1.03	0.00	0.14	0.01	0.25	0.37	68.9%	58.5% 68.9%	01%	9.6%	0.5%	17.2%	20.7%
100		159	-	5	1.04	0.00	0.07	0.00	0.54	0.46	-	100.0% 100.0%	0.5%	6.4% 2.6%	0.3%	52.2% 44.6%	46.8% 60.0%		0.00	004	0.00	0.25		56.2% 66.9%	56.2% 66.9%	0.4% 0.2%	37% 13%	0.3%	24.0%	23.6% 33.8%
101		161		5	1.53	0.00	0.25	0.01	0.67	0.62		100.0%	0.1%	16.1%	0.7%	43.5% 44.2%	40.5% 37.4%	0.86	0.00	0.15	0.01	0.25		56.3% 51.4%	56.3% 51.4%	01%	9.7% 12.0%	0.7%	16.2%	20.0% 18.9%
103		167		5	1.40	0.00	0.09		062	0.69		100.0% 100.0%	0.2%	64% 52%	0.1%	44.0% 46.0%	49.6% 50.9%	0.85	0.00	005		023	0.38	60.7% 59.5%	60.7% 59.5%	01% 03%	36% 27%	0.1%	16.8%	27.0%
103 104 105 106 107 108 109 110		169		Š	1.50	0.00	0.09	0.01	0.74	0.73		100.0%	0.2%	60%	0.5%	49.0%	48.9%	1.00	000	0.05	0.01	0.10	0.38	66.9%	66.9%	0.1%	35%	0.4%	19.9%	25.4%
106		3	129 131	2	0.58	0.00		0.00	0.25	0.21		100.0% 100.0%	0.2%	6.2% 6.7%	0.5%	42.4% 38.9%	36.9% 42.5%	0.27			0.00	0.09		45.6% 45.3%	46.0% 46.3%	0.2% 0.3%	45% 45%	0.5%	14.7% 11.9%	16.2% 15.9%
108		7	133	2	0.76	0.00	0.09	0.00	0.31	0.31		100.0% 100.0%	0.3%	11.2%	0.4%	41.4% 29.6%	41.0% 41.7%	0.34	000	0.05	0.00	0.10	0.14	412%	44.9% 43.2%	01%	7.4% 7.1%	0.4%	12.7%	18.5% 17.7%
110		9 14	137	2	1.50	0.00	0.06		0.27	0.24		100.0% 100.0%	0.3%	9.6%	1.1%	42.5% 34.0%	37.7% 35.8%	0.31	000			0.09		50.2% 32.9%	50.2% 32.9%	0.3% 0.2%	5.1% 12.1%	1.0%	14.2%	15.5% 14.5%
112		15	143		1.29	0.00	0.17	0.02	0.58	0.54		100.0%	0.2%	13.2%	12%	44.7%	41.7%	0.62	0.00	0.10	0.01	0.23	0.28	41.0%	48.0%	0.2%	78%	1.1%	17.5%	21.5%
113		16	144	- 4	1.24	0.00	0.08		0.50	0.59		100.0% 100.0%	0.4%	6.7% 10.2%	0.2% 0.7%	40.4% 35.8%	48.0% 36.3%	0.52	0.00	0.10	0.00	0.18	0.25	53.5% 40.1%	53.5% 40.1%	0.3% 0.2%	3.6% 7.4%	0.2% 0.7%	14.6%	24.5% 18.5%
115		21	149	4	1.56	0.00	0.25	0.02	0.70	0.72 0.57	+ ≡	100.0% 100.0%	0.2%	18.0% 7.2%	1.4%	44.5% 47.9%	45.9% 46.6%		000	0.17	0.02	0.26		43.6% 57.8%	43.6% 57.8%	0.2% 0.1%	11.1%	12%	16.3%	20.8% 24.9%
112 113 114 115 116 117		23	151	4 10	1.52	0.00	0.17	0.02	0.66	0.61	-	100.0% 100.0%	0.5%	11.1%	12%	43.2% 43.6%	40.2% 40.9%	0.76	001	0.10	0.01	0.22	0.27	50.0% 45.0%	50.0% 46.0%	0.3% 0.2%	68% 18.2%	0.8%	14.7%	17.5% 20.2%
119		30	158	10	119	0.01	83.0	0.04	1.85	1.70		100.0%	0.1%	20.0%	1.0%	54.0%	50.2%	2.01	001	0.34	0.03	0.76		59.4%	59.4%	0.1%	9.9%	0.9%	22.9%	28.8%
120 121		31 32	159	10	2.64 2.98	0.01	0.11	0.00	141	1.37		100.0% 100.0%	0.5%	42% 52%	0.3%	54.1% 49.6%	48.5% 46.1%	1.55	001	0.09	0.00	0.64	0.82	58.8% 60.5%	58.8% 60.5%	0.2% 0.4%	21% 29%	0.3%	24.3%	25.9% 27.5%
122		33	161	10	1.45	0.00	0.89	0.06	1.44	1.52	+ =	100.0% 100.0%	0.4%	25.7%	26%	41.7%	441% 465%	1.66	0.00	051	0.07	0.57	0.80	48.2% 38.4%	46.2%	0.3%	17.7% 16.6%	22%	16.5%	23.3% 25.2%
123 124 125 126		39	167			0.00	0.34	0.01	1.61	1.56		100.0%	0.2%	10.4%	0.2%	48.0%	47.5% 49.1%		001	0.14	0.01	0.69		55.9%	55.9% 50.3%	0.2%	41%	02%	20.9%	30.1%
126		41	169						153			100.0%	0.5%	12.6%	0.4%	56.3% 47.5%	43.7%		001					58.9%	52.9%	0.4%	83%	0.3%	19.2%	25.1%

- M-patch Mid CH

														max ratio ou	t of all beams												max ratio out of all I	beares		
П							- 4	lcm2 PD(mW	(rom2)			100.0%	1.2%	11.7%	2.7%	61.2%	65.5%	4	om2 PD(mi	W/cm2) at	10mm evalu	ation distan	ice	66.1%	66.1%	1.1%	22.5%	2.2%	29.2%	39.0%
No. Modu	de Type	Seam ID_1	Sema ID_2	Feed no.		Т			Т		per Seam	ratio	ratio	ratio	ratio	ratio	ratio							ratio	ratio	ratio	ratio	ratio	ratio	ratio
					54/Right	() S3(Left)	SS(Top)	S6(Botton	S1(Fro	rt) S2(Rea	Back-of	(Right 2mm)/(wont- surface 2mm)	(Left 2mm)/(worst- surface 2mm)	(Top 2mm)/(worst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm)/(wont- surface 2mm)	S4(Right)	S3(Left)	SS(Top)	SS(Bottom)	\$1(Front)	S2(Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(worst- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Bottom 10mm(//worst- surface 2mm)	(Front 10mm(/(worst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
64	+	1		1	0.24	0.00		0.00	010			100.0%	0.4%	8.3%	0.4%	40.8%	46.3%				0.00	0.03		43.3%	43.2%	0.4%	58%	0.4%	12.1%	19.2%
66		3 5		-	0.25	0.00		0.00	011			100.0% 100.0%	0.4%	57% 97%	0.4%	44.5% 40.7%	543% 57.6%	0.12			0.00	0.04	0.06	\$1.0% 42.1%	51.0% 42.1%	0.4%	36% 66%	0.4% 0.7%	15.4%	25.1% 30.7%
65 66 67 68		7 9		1	0.28	0.00	0.03		012			100.0%	0.4%	10.3%	0.7%	43.4%	548%		000	002	0.00	0.04	0.07	445% 41.7%	44.5%	0.4%	64%	0.4%	14.6%	25.6%
60		14		2	0.59	0.00	0.03		0.10		+	100.0% 100.0%	0.4%	10.9%	1.0%	36.6% 39.2%	42.8% 50.9%	0.12	000	001		0.03	0.12	41.7% 28.4%	41.7% 28.4%	0.4%	5.1% 11.2%	0.4%	12.3%	14.5% 19.5%
70		15 16		2	020	0.00		0.01	0.23			100.0% 100.0%	0.2% 0.6%	60% 60%	0.9%	41.3% 43.9%	50.4% 50.4%	0.25		003	0.00	0.09	0.14	43.9% 55.1%	43.9% 55.1%	0.2%	54% 10%	0.7%	16.1%	25.5% 31.6%
72		17		2	0.45	0.00	0.06	0.00	0.16	0.24		100.0%	0.7%	13.5%	0.7%	39.9%	\$1.6%	0.15	0.00	004	0.00	0.05	0.11	33.0%	33.0%	0.7%	9.0%	0.4%	11.4%	23.5%
70 71 72 73 74 75 76 77 78 79 80		21	_	2	0.66	0.00	0.08		0.28		+	100.0% 100.0%	0.2%	11.8%	1.1% 0.6%	43.0% 48.1%	51.4% 48.1%	0.25	0.00	005		0.12	0.16	37.7% 58.1%	37.7% 58.1%	0.2% 0.2%	7.4%	0.6%	17.4%	24.2% 26.2%
75		23 29		2	0.48	0.00	0.06	0.00	017			100.0% 100.0%	0.6%	11.8%	0.4%	36.7% 45.8%	55.6% 59.1%	0.19			0.00	0.06	0.13	40.0% 35.6%	40.0% 15.6%	0.6%	64% 20.9%	0.4% 1.2%	12.0%	27.8% 25.7%
77		30		5	1.37	0.00	0.18	0.01	068	0.71		100.0%	0.3%	13.2%	1.0%	49.4%	52.0%	0.71	0.00	0.09	0.01	0.29	0.38	53.5%	53.5%	0.2%	6.0%	0.8%	21.4%	27.9%
78		31		5	1.19		0.04		0.73		-	100.0% 100.0%	0.2%	10%	0.2%	52.9% 45.0%	52.6% 54.6%		0.00		0.00	0.33	0.43	61.4% 54.7%	61.4% 54.2%	0.2%	1.6% 5.7%	0.1%	24.0%	32.9% 31.8%
80		33		5	0.99	0.01	0.33	0.01	0.37	0.65		100.0% 100.0%	0.8%	33.4% 24.8%	0.7% 2.7%	37.2% 42.5%	655% 612%	0.38	0.01	0.22	0.01	0.15	0.37	38.7% 45.0%	38.7% 45.0%	06% 02%	22.5% 16.0%	0.6% 2.2%	14.8% 22.2%	37.0% 34.4%
82		29		5	1.46	0.01	0.09	0.00	0.77	0.69	_	100.0%	0.3%	60%	0.2%	52.8%	47.4%	0.87	0.00	003	0.00	0.35	0.29	59.5%	59.5%	0.3%	2.0%	0.2%	23.7%	26.7%
83		40 41		5	1.02	0.00	0.05		0.47			100.0%	0.2%	46% 15.8%	0.4%	46.0% 41.3%	63.4%	0.60	000	003		0.20	0.40	58.9% 48.2%	58.9% 48.2%	02%	25%	0.3%	20.1% 17.5%	39.0% 38.8%
84 85 86 87 88 89 90		129		í	0.21	0.00	0.01	0.00	0.07	0.10		100.0%	0.0%	1.3%	0.5%	34.4%	48.1%	0.10	0.00	0.01	0.00	0.03	0.05	49.1%	49.1%	0.0%	24%	0.5%	11.8%	22.2%
86		131	-	1	0.32	0.00			0.14			100.0% 100.0%	0.3%	5.4% 11.0%	0.3%	44.0% 42.8%	35.4%	0.16	0.00	001	0.00	0.05	0.05	50.3% 47.9%	50.3% 47.9%	00% 00%	38% 62%	0.3%	15.8%	16.8% 19.0%
88		135		1	0.35	0.00			015			100.0%	0.3%	11.9% 5.0%	0.6%	42.1% 44.9%	37.3% 36.8%		0.00		0.00	0.05	0.05	46.9% 0.1%	46.9% 52.3%	0.0%	65%	0.3%	14.1%	14.4% 14.6%
90		142		2	0.61	0.00	0.10	0.00	0.22	0.16		100.0%	0.2%	17.0%	0.7%	35.0%	25.9%	0.21	0.00	007	0.00	0.06	0.05	347%	34.7%	0.2%	11.1%	0.5%	98%	7.7%
92		143		2	0.72	0.00	0.11		032			100.0% 100.0%	0.1%	14.5%	0.6% 0.1%	44.2% 44.2%	39.2% 50.8%	0.39		0.06	0.00	0.13		53.5% 60.3%	53.5% 60.2%	01%	84% 24%	0.4%	17.5%	18.9% 27.9%
93		145		2	0.53		0.03	0.00	0.19			100.0%	0.2%	6.1% 19.0%	0.6%	36.9% 35.2%	32.9%	0.22		0.02		0.05	0.00	41.1%	41.1% 42.7%	02%	4.0% 10.9%	0.4%	10.1%	16.0%
95 M	Pasch	150		2	0.64	0.00		0.00	0.25	0.31		100.0%	0.2%	6.1%	0.5%	54.0%	31.2% 49.2%	0.41	0.00	0.02	0.00	0.15	0.15	642%	64.2%	0.2%	3.1%	0.3%	23.6%	21.9%
96		151		2	0.73		0.07		0.34	0.24	_	100.0%	0.3%	10.1%	0.7%	46.0% 37.9%	33.2% 11.0%		000		0.00	0.13		51.0% A4.0%	51.0% 44.9%	0.1%	57% 21.7%	0.5%	17.2%	15.3% 15.6%
98		158		ś	1.21	0.00	0.23	0.01	063	0.59		100.0%	0.2%	19.1%	0.6%	52.5%	49.0%	0.76	0.00	0.10	0.01	0.29	0.31	63.3%	63.3%	0.2%	8,0%	0.6%	23.9%	25.5%
95 M 96 97 98 99 199 190 191		159	 	5	1.24	0.00		0.01	0.70			100.0%	0.2%	2.4%	0.4%	51.9% 52.4%	46.8% 51.1%	1.12		002	0.01	0.31	0.34	59.8% 64.7%	59.8% 64.7%	0.2%	12%	0.4%	23.4%	25.0% 30.0%
101		161		5	1.23	0.00		0.01	0.46			100.0% 100.0%	0.3%	31.5% 33.7%	0.4%	37.4% 41.2%	32.4% 33.1%	0.52		0.25	0.00	0.16		42.5% 47.6%	42.5% 47.6%	0.3% 0.2%	20.0% 21.5%	0.5%	12.8%	14.0% 15.7%
222		167		ś	1.53	0.00	0.07	0.00	0.73	0.82		100.0%	0.2%	4.7%	0.1%	47.8%	53.5%	0.99	0.00	0.02	0.00	0.31	0.45	645%	64.5%	0.1%	1.6%	0.1%	20.4%	29.7%
334		168	-	5	1.35	0.00	0.02		0.69	0.60		100.0%	0.2%	1.2%	0.3%	51.0% 52.6%	50.9% 47.4%	0.83	0.00	001	0.00	0.31	0.38	65.1%	61.4%	01%	60%	0.3%	23.2%	28.4%
104 105 106 107	1	1	129	2	0.51			0.00	0.23			100.0%	0.2%	7.8% 5.9%	0.6%	45.2% 50.4%	41.5% 41.9%		000			0.08		51.9% 51.2%	51.9% 51.2%	0.2%	5.7% 19%	0.6%	15.8%	16.6% 17.1%
108	1	3 5	133	2	0.71	0.00	0.06	0.01	0.36	0.33		100.0%	0.1%	11.1%	0.8%	50.1%	46.1%	0.31	000	0.05	0.01	0.11	0.15	44.1%	44.1%	0.1%	6.6%	0.7%	15.9%	21.6%
109 110 111 111 112 113		7 9	135	2	0.68	0.00	0.09		0.37	0.32		100.0%	0.3%	12.6%	0.7%	53.4% 41.2%	473% 372%	0.33		005	0.00	0.12	0.14	47.0% 45.5%	47.6% 45.5%	0.3%	70% 45%	0.6%	17.4%	20.1% 34.5%
111		14	142	- 4	1.29	0.00	0.23	0.01	0.64	0.51		100.0%	0.4%	18.0%	1.1%	49.7%	29.2%	0.45	000	0.14	0.01	0.23	0.20	345%	34.5%	0.3%	11.1%	1.0%	17.7%	15.5%
112		15 16	143	4	1.23	0.00	0.13		054			100.0% 100.0%	0.2%	10.9%	13%	44.0% 45.0%	45.0% 45.9%		000	008	0.01	0.23	0.34	48.7% 51.8%	48.7% 51.8%	0.2%	67% 29%	1.1% 0.2%	18.8%	19.6% 26.6%
114		17 21	145	4	1.07	0.00	0.13		0.47	0.44		100.0% 100.0%	0.4%	12.0%	0.7% 1.2%	43.8% 57.5%	40.7% 40.9%	0.46		0.09	0.01	0.17	0.15	42.9% 45.8%	42.9% 45.8%	0.4% 0.2%	82% 10.1%	0.7% 1.0%	15.5% 21.5%	16.4% 13.1%
116	1	22	150		1.16	0.00	0.06	0.01	0.61	0.57	_	100.0%	0.3%	5.0%	0.9%	52.3%	40.0%	0.70	000	003	0.01	0.25	0.27	60.6%	60.6%	0.2%	29%	0.8%	21.6%	23.6%
117	1	23 29	151	10	1.44	0.01	0.19		063			100.0% 100.0%	0.4%	13.1%	0.8%	43.7% 51.6%	37.6% 44.5%	0.70	001	011		0.24	0.25	48.8% 27.9%	48.8% 37.9%	0.3% 0.5%	78%	0.6% 0.7%	16.6%	17.6% 20.8%
118 119 120	1	30	158	10	2.94	0.01	0.48	0.04		1.42		100.0% 100.0%	0.2%	16.5%	13%	63.2% 58.0%	41.4% 41.6%		001	0.23	0.03	0.86	0.80	58.5% 60.1%	58.5%	0.2%	79%	1.1%	29.3%	27.3%
120	1	32	159	10	2.88 3.21	0.02		0.00	1.67			100.0% 100.0%	0.5%	13%	0.2%	58.0% 49.8%	45.0% 45.0%		0.00	005	000	0.77	0.73	60.1%	60.1% 60.9%	0.1%	19%	0.2%	26.7% 22.8%	25.4%
122	1	33	161					0.02	1.29			100.0%	0.9%	32.1%	0.6% 2.1%	48.5%	42.5% #1.0%	1.24	0.02	056	0.01	0.50	0.63	45.6% 44.0%	46.6% 44.0%	0.7% 0.2%	21.1% 14.6%	0.5% 1.7%	18.9%	23.6%
124	1	39	167	10	120	0.01	0.21	0.01	1.73	1.73		100.0%	0.2%	66%	0.2%	53.9%	541%	2.01	0.01	007	0.01	0.79	0.96	63.3%	63.2%	0.2%	2.1%	0.2%	24.6%	30.1%
125	1	40	168		2.52			0.02	1.31	1.32		100.0% 100.0%	0.4%	10%	0.0%	51.8% 51.5%	524% 448%		0.01		0.01	0.58		\$1.0% \$8.0%	61.8% SA.8%	0.3% 0.7%	15%	0.5%	23.1%	29.3% 21.0%

- M-patch High CH

_		-	_		_			_			_		_		-	may ratio ou	t of all beams			_		_	_	_	_	1			max ratio out of all I	hanna		
\perp		1						des	m2 PD/mili	80(nm2)				100.0%	1.5%	40.6%	1.0%	62.7%	71.7%	40	w2 SUIM	Mirm 7: a	10mm evalu	ation distan	200	71.1%	71.1%	1.15	26.15	1.7%	29.4%	41.65
l., l.	odule Tvo	e Seam ID_1	Sema ID_2	Court on		_	$\overline{}$	Ť		1	\neg		per	ratio	ratio	ntio	ratio	ratio	ntio						Ī	ratio	ratio	ntio	ntio	ratio	ntio	ratio
1000	- iyy		anna ibi,a	Peed III.	54/Rigit	nt) \$3(14	nt) SS	(Top)	S6(Botton	10 S1(F	Front)	S2(Rear)	Seam Back-off	(Right 2mm)/(wont-	(Left 2mm)/(worst-	(Top 2mm)/(worst-	(Bottom 2mm)/(wont-	(Fornt 2mm)/(worst-	(Rear 2mm)/(wont-	S4(Right)	S3(Left)	SS(Top)	SS(Bottom)	S1(Front)	S2(Rear)	worst-surface	(Right 10mm)/(worst-	(Left 10mm)/(worst-	(Top 10mm)/(worst-	(Ecttom 10mm)/(wont	(Front 10mm)/(worst-	(Rear 10mm)/(worst-
-	_	٠.			430	0.0		0.02	0.00	٠.	108	0.11	(dB)	surface 2mm) 100.0%	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm) 38.6%	surface 2mm) 52.5%	010	0.00	001	0.00	0.03	0.04	(10mm/2mm) 515%	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm)	surface 2mm) 13.4%	surface 2mm)
65		3		1	0.20	0.0	0 0	0.02	0.00	- 0	009	0.11		100.0%	0.5%	90%	0.5%	42.3%	67.2%	0.11	0.00	001	0.00	0.03	0.07	53.2%	53.2%	00%	55%	0.5%	15.9%	34.0%
67		7	-	1	0.29	0.0	0 0	0.03	0.00	- 0	009	0.16	-	100.0% 100.0%	0.3%	8.7% 13.7%	0.3%	39.6% 41.6%	542% 71.7%	0.14	0.00	0.02	0.00	0.04	0.06	48.5% 46.6%	45.2% 46.6%	0.3% 0.5%	59% 82%	0.5%	12.2%	21.5% 32.4%
68		9		1	0.25	0.0	0 0	0.03	0.00		120	0.11		100.0% 100.0%	0.4%	11.6%	0.4%	39.0% 39.2%	45.0% 63.1%	0.12	000	002	0.00	0.03	0.04	50.2% 26.5%	50.2% 26.5%	0.4%	60%	0.4%	12.4%	15.1%
70		15			0.43	0.0	0 0	0.03	0.00	- 0	227	0.28		100.0%	0.2%	65%	0.7%	39.8%	63.9%	0.21	0.00	0.02	0.00	0.07	0.14	49.5%	49.5%	0.2%	4.6%	0.7%	15.7%	33.2%
71		16		2	0.41	0.0	0 0	0.04	0.00	0	213	0.28		100.0% 100.0%	0.5%	14.3%	0.2%	43.7% 36.8%	67.4% 62.9%	0.26	0.00	0.03	0.00	0.08	0.15	61.8% 37.6%	61.8% 37.6%	0.5%	5.6% 9.1%	0.5%	10.1%	35.0% 26.6%
73		21		2	0.56	0.0		0.07	0.00		123	0.36		100.0%	0.4%	11.9%	0.7%	40.5% 46.5%	64.7% 59.1%	0.21	000	004	0.00	0.09	0.16	41.1%	41.7%	0.4%	74%	0.7%	15.5%	29.2% M/6%
75		23		2	0.43	0.0		0.07	0.00		117	0.23		100.0% 100.0%	0.5%	16.3%	0.7%	40.1%	51.6%	0.20	000	0.04	0.00	0.06	0.09	45.7% 34.4%	45.7%	05%	9.3%	0.7%	13.3%	21.9%
77		29 30		5	1.00	0.0	0 0	0.16	0.01		151	0.67		100.0%	0.5%	14.4%	0.8%	47.0%	61.5%	0.69	001	0.00	0.01	0.21	0.35	63.3%	63.2%	0.5%	6.9%	0.7%	19.1%	32.2%
78 79		31	-	5 5	0.90	0.0		0.04	0.00		156	0.77	\vdash	100.0% 100.0%	0.3%	13%	0.2%	49.2% 45.2%	68.0% 54.7%	0.80	000	002	0.00	0.19	0.47	71.1% 59.2%	71.1% 59.2%	0.3%	17% 32%	02%	21.6%	41.6% 31.3%
80		33		5	0.80			0.36	0.01		130	0.59		100.0% 100.0%	1.4%	40.6%	0.7%	33.9% 43.8%	66.9% 59.1%	0.33			0.00	0.11	0.29	37.3% 45.9%	37.3% 45.0%	1.0%	26.1% 34.1%	0.5%	12.0%	12.4% 29.7%
82		39		5	1.12	0.0	0 0	0.00	0.00		253	0.74		100.0%	0.5%	7.3%	0.2%	47.1%	65.2%	0.76	0.01	0.03	0.00	0.22	0.43	67.7%	67.7%	0.4%	25%	0.2%	19.8%	31.4%
83		40	-	5 5	0.93	0.0		0.06	0.00	- 0	1.13	0.55	\vdash	100.0% 100.0%	0.3% 1.5%	59% 3615	0.4%	49.1%	59.5% 60.9%	0.58	000	0.03	0.00	0.21	0.31	62.9% 544%	62:9% 54:4%	0.2% 1.1%	30% 22.6%	0.3%	22.7% 16.8%	32.9% 34.7%
85		129		1	0.24	0.0		0.00	0.00	0	110	0.10		100.0% 100.0%	0.0%	21%	0.4%	43.7% 42.9%	41.2% 23.4%	0.12		0.00	0.00	0.03	0.04	542% 440%	54.2% 44.0%	0.0%	12%	0.4%	14.3%	16.8% 12.6%
86		133		1	0.34	0.0	0 0	0.03	0.00		116	0.11		100.0%	0.3%	7.9%	0.6%	45.0%	11.0%	0.15	000	002	0.00	0.06	0.05	44.4%	44.4%	0.3%	5.0%	0.6%	16.7%	14.0%
88		135	-	1	0.33	0.0	0 0	0.04	0.00	- 0	115	0.10	\vdash	100.0% 100.0%	0.3%	12.9%	0.3%	43.8% 51.5%	28.5%	0.15	000	002	0.00	0.04	0.04	45.9% 49.5%	45.9% 49.5%	0.0% 0.3%	6.9% 4.0%	0.3%	12.9%	10.8% 14.1%
90		142		2	0.50	0.0	0 0	900	0.00			0.17		100.0%	0.2%	15.2%	0.5%	34.7%	29.8%	0.19			0.00	0.05	0.06	32.6% 51.3%	32.6% 51.3%	0.2%	10.3%	05%	9.1%	12.0%
92		144		2	0.64	0.0	0 0	0.04	0.00		335	0.27		100.0%	0.3%	65%	0.2%	54.3%	41.9%	0.38	0.00	003	0.00	0.14	0.13	60.3%	60.3%	0.3%	43%	0.2%	22.0%	20.6%
93 94		145		2	0.55	0.0		0.04	0.00		121	0.15	_	100.0% 100.0%	0.2%	17.8%	0.4%	38.3% 38.1%	26.3% 24.1%	0.21	000	007	0.00	0.07	0.06	17.6% 17.5%	37.6% 37.5%	0.0%	45% 10.1%	0.4%	12.2% 11.6%	10.7% 9.3%
95 96	M Pas	n 150		, ,	0.59	0.0		0.04	0.00		136	0.22		100.0% 100.0%	0.3%	14.1%	0.5%	61.3% 49.2%	37.9% 25.8%	0.39	000		0.00	0.15	0.11	65.1% 47.2%	65.1% 47.2%	0.3%	2.7% 7.4%	0.3%	24.5% 19.2%	18.1% 11.1%
9.7		157		5	1.10	0.0	0	0.40	0.00	0	158 158	0.40		100.0% 100.0%	0.3%	34.0%	0.3%	49.5%	13.5% 17.9%	0.55	000	025	0.00	0.22	0.18	46.6%	46.0% 64.0%	0.3%	21.4%	0.3%	18.3%	15.3%
99		159		5	1.06	0.0	0 0	0.05	0.01	- 0	154	0.46		100.0%	0.8%	44%	0.8%	60.0%	45.1%	0.55	001		0.01	0.27	0.23	66.5%	66.0%	0.6%	2.0%	0.7%	25.7%	21.6%
100		160			1.65			0.03	0.00		198	0.73		100.0%	0.2%	19%	0.1%	59.0% 46.4%	446% 30.1%	1.10			0.00	0.46	0.44	67.0% 44.2%	67.0% 44.2%	0.2% 0.2%	0.8% 20.3%	0.1%	27.6% 17.6%	26.5% 11.4%
102		166		5	1.25		0 0	0.39	0.01		158	0.35		100.0% 100.0%	0.2%	31.3% 46%	0.4%	46.3% 58.9%	27.9% 46.3%	0.55			0.00	0.22	0.16	41.6%	43.0%	0.2%	19.6%	0.3%	17.2% 27.5%	12.5% 25.7%
104		168		5	1.19	0.0	0 0	0.04	0.01	0	068	0.56		100.0%	0.6%	17%	0.6%	57.3%	46.5%	0.78	001	0.02	0.01	0.30	0.30	65.7%	65.7%	05%	1.7%	0.4%	25.4%	25.0%
105		169	129	5	1.03	0.0		0.16	0.00		126	0.47	\vdash	100.0% 100.0%	0.3%	15.3% 5.2%	0.3%	60.7% 46.8%	45.6% 37.7%	0.67			0.00	0.27	0.22	65.3% 56.8%	65.3% 56.8%	0.2% 0.2%	93%	0.3%	26.3%	20.9% 15.1%
107		3	131	2	0.52	0.0	0 0	0.04	0.00		129	0.24		100.0% 100.0%	0.4%	7.9%	0.6%	55.2% 50.3%	45.8% 44.9%	0.27			0.00	0.11	0.10	52.3% 47.7%	52.3% 47.2%	0.2%	56%	0.6%	21.6%	19.2% 18.2%
109		7	135	2	0.61	0.0	0 0	000	0.00		3.32	0.29		100.0%	0.3%	13.2%	0.5%	53.5%	48.2%	0.27	0.00	004	0.00	0.10	0.12	44.6%	44.0%	0.2%	6.9%	0.5%	16.8%	19.0%
110		14	137		1.00	0.0	0 0	0.05	0.01		128	0.21	\vdash	100.0% 100.0%	0.5%	18.0%	10%	47.5% 50.6%	348% 49.7%	0.29	001		0.01	0.09	0.09	48.7% 35.4%	46.7% 35.4%	0.3%	49% 11.7%	0.8%	15.0%	15.5% 21.7%
112		15	143		1.00		0 0	0.13	0.01	0	346	0.50		100.0% 100.0%	0.3%	11.8%	1.0%	44.9% 52.4%	46.0% 47.2%	0.55			0.01	0.20	0.25	50.7% 59.3%	50.7% 59.3%	0.3%	6.0%	0.8%	18.1%	22.8% 22.6%
114		17	145	- 4	1.02	0.0	0 0	0.10	0.01		0.46	0.43		100.0%	0.4%	10.0%	0.8%	45.0%	41.6%	0.45	0.00	0.07	0.01	0.17	0.18	44.0%	44.0%	0.3%	65%	0.7%	16.6%	17.8%
115		21	149	4 4	0.90			023	0.02		173	0.62	⊢=	100.0% 100.0%	0.3%	16.9%	1.1%	53.6% 56.9%	453%	0.55	000		0.01	0.26	0.12	40.1%	40.1% 62.3%	0.2% 0.3%	9.8%	0.9%	19.1%	23.5% 25.7%
117		23	151	4	1.30	0.0	0 0	0.16	0.01	0	65	0.46		100.0% 100.0%	0.5%	12.4%	0.6%	50.0%	355% 413%	0.60	001	0.09	0.01	0.23	0.19	46.4% 46.1%	46.4%	0.5%	69%	0.5%	17.6%	14.6%
119		29 30	158	10	2.44	0.0	0	0.74	0.02	1	150	1.12		100.0%	0.4%	17.8%	12%	57.9% 62.7%	49.3%	1.61	0.01	0.19	0.02	0.64	0.62	66.0%	66.0%	05% 0.3%	7.7%	1.4%	26.1%	24.0% 27.5%
120		31	159	10	2.41	0.0		0.10	0.01		142	1.26	⊢=	100.0% 100.0%	0.5%	41% 17%	0.5%	58.7% 58.0%	52.9% 44.1%	1.66	001	0.05	0.01	0.63	0.64	60.5%	68.7% 60.5%	0.4%	19%	0.4%	26.2%	26.4% 24.8%
122		33	161		2.51		9 0	0.76	0.01		26	1.04		100.0% 100.0%	1.1%	30.2% 25.0%	0.6%	50.3% 56.4%	41.6% 45.6%	1.15			0.01	0.51	0.57	45.9% 45.4%	45.9% 45.4%	0.2%	19.2% 15.5%	0.4% 1.1%	20.4%	22.7% 21.3%
123		39	167	10	2.66	0.0	0 0	023	0.01	1	1.60	1.46		100.0%	0.4%	86%	0.2%	60.1%	55.7%	1.76	0.01	0.09	0.01	0.73	0.78	66.1%	66.7%	0.3%	32%	0.2%	27.5%	29.5%
125		40	168	10			0 0		0.01		129	1.23	⊢=	100.0% 100.0%	0.4%	5.8% 22.6%	0.6%	60.9% 56.4%	52.1% 47.6%	1.45			0.01	0.69	60.0	63.7%	61.4% 63.7%	0.3%	2.7% 15.1%	0.5%	29.4% 25.0%	26.5% 30.3%
					_			_													-											

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- M-patch Low CH

					-												max ratio ou	t of all beams												max ratio out of all I	Hams		
March Marc		Т				Π			40	m2 PD(mW	N/on2)				100.0%	0.7%	44.1%	1.2%	27.9%	65.3%	40	n2 PD/mV	N/cm2) at	10mm evalua	tion distan	ICP	69.6%	69.6%	0.6%	31.2%	12%	24.1%	22.7%
Company Comp	No. Modu	de Type	Seam ID_1	Sema ID_2	Feed no.	Г	Т	Т	П		Т	П		per Seam																			ratio
The color of the			1			54/8	ght) S3(Le	n) ss	(Top)	S6(Botton	(i) \$1(Fe	hont) S	S2(Rear)								S4(Right)	S3(Left)	SS(Top)	SS(Bottom)	\$1(Front)	S2(Rear)						(Front 10mm(/(worst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
The column The	64	+	1		1	0.2	7 0.00		0.02	0.00	00	03	0.16	((31)	100.0%	0.4%	6.6%	0.4%	9.2%		0.12	000	0.01	0.00	0.01	0.06		45.8%	00%	42%	0.4%	17%	20.5%
The color of the	65				-																												17.0%
The column The	67		7		i					0.00	8	04	0.19				15.5%				0.19	000	0.04	0.00	0.02		47.6%						16.0%
The color of the	68			1	2																												17.1% 15.8%
The column The	70				2																					0.15							22.5% 25.4%
The column The	72					0.0	2 0.00		30.0	0.00	0.0	04	0.28		100.0%	0.3%	10.2%	0.6%	65%	45.1%	0.20	0.00	0.04	0.00	0.02	0.11	32.5%	32.5%	0.2%	7.1%	0.6%	3.2%	18.1%
The column The	73		21	-	2										100.0% 100.0%	0.1%													0.1%		0.4%		20.8% 27.5%
TO 1 1 12 30 15 15 16 15 15 15 15 15 15 15 15 15 15 15 15 15	75				2																			0.00									19.1% 27.9%
The column The	77			 	5									-							1.07	0.00	0.14										30.2%
The column The	78 79																																31.9% 30.0%
The column The	80		33			12									100.0%	0.4%	42.7%	0.4%	9.7%	61.8%	0.66	0.00	0.29	0.00		0.22		52.3%	0.3%	31.2%	0.3%	48%	30.7%
## 1 10 20 20 20 20 20 20 20 20 20 20 20 20 20	81			_	5	12																											33.7% 31.1%
The column The	83				5																												32.3% 30.8%
The column The	85		129		1	0.2	4 0.00	ľ	000	0.00	- 60	03	0.05		100.0%	0.4%	5.5%	0.4%	13.0%	22.6%	0.12	000	001	0.00	0.01	0.02	50.6%	50.0%	0.4%	3.8%	0.4%	60%	8.1%
The color of the	87			-										_																			9.7% 7.5%
## Company 1	88		135		1		7 0.00		0.03	0.00	- 60	29	0.07			0.3%	92%	0.5%	24.0%	17.8%	0.18	000	0.02	0.00	0.04	0.02	40.5%	48.8%	0.3%	43%	0.5%	11.1%	59%
The color of the	90		142	_	2		5 0.00		2.12	0.00	0.1	13	0.13		100.0%	0.3%		0.4%		17.1%				0.00	0.07	0.03	342%	34.2%		9.8%		8.0%	75% 56%
1	91																																89%
1	93		145		2	0.5	9 000		300	0.00		29	0.12		100.0%	0.3%	10.8%	0.7%	14.2%	19.5%	0.20	000	004	0.00	0.04		33.7%	33.7%	0.2%	7.1%	0.5%	7.3%	7.6%
1	94 95 M	Pasd		-	2	0.0	9 0.00	1 6	0.13		0.2	18 24		\vdash								000	007			0.05							6.2% 10.0%
The column The	96																																75%
The column The	98		158		5	1.6	6 0.00		3.45	0.01	- 00	51	0.42		100.0%	0.4%	27.1%	0.5%	36.9%	25.5%	1.07	0.01	0.25	000	0.40	0.20	64.5%	64.5%	0.3%	14.0%	0.2%	24.1%	12.0%
The column The	300			+	- 5									_																			92%
1	101		161		5		9 0.00		3.43	0.02	ä	25	0.45		100.0%	0.3%	26.7%	1.1%	23.5%	30.1%		0.00	0.26	0.01	0.19	0.21	543%	54.3%	0.3%	17.7%	0.9%	12.9%	14.4%
1	103																																14.7%
1	104			_																													95%
1	106				2	0.5	7 0.00			0.00		G7	0.23		100.0%	0.2%	7.3%	0.5%	12:9%	42.3%				000		0.09	49.7%	49.7%	0.2%	5.6%	0.5%	5.2%	15.0%
TO US 1 40 12 11 12 12 13 12 12 13 12 13 12 13 13 13 13 13 13 13 14 15 15 15 15 15 15 15 15 15 15 15 15 15	108		5	133	2	0.5	0 000		2.13	0.00	0.1	17	0.37		100.0%	0.3%	14.3%	0.3%	19.2%	41.4%	0.42	000	008	0.00	0.08	0.11	46.5%	46.0%	0.3%	92%	0.3%	90%	16.6%
1	129		7		2																												12.8% 11.0%
TO U. H. I. 12 20 10 10 20 22 22 22 25 25 30 30 30 30 30 30 30 30 30 30 30 30 30	111		14		4		2 0.00		3.44	0.01	0.2	25	0.65		100.0%	0.3%	25.4%	0.6%	14.5%	37.5%	0.68	0.00	0.29	10.0	0.13	0.24	22.4%	39.4%	0.2%	16.6%	0.5%	7.3%	13.0%
11	112		15		4																												16.7% 20.7%
15 2 15 4 15 15 15 15 15 15 15 15 15 15 15 15 15	114	1	17		4					0.01		16	0.55						13.7%			000		0.01	0.08								16.4%
118 29 157 10 137 000 118 0.04 0.70 158 1000% 0.03 407% 10% 1177% 499% 2.20 001 112 0.03 0.37 0.09 555% 555% 0.0% 282% 0.0% 52%	115	1	22	150	4	13	4 0.00		2.11	0.01	0.7	25	0.64		100.0%	0.5%	84%	0.4%	26.3%	47.9%	0.85	0.01	007	0.00	0.16	0.25	63.5%	63.5%	0.4%	5.1%	0.3%	13.4%	16.5% 21.1%
	117	1												⊢=																			15.8% 22.5%
	119	1		158	10	44	0 0.01		392	0.03	11	19	1.61		100.0%	0.3%	22.9%	0.7%	29.9%	45.3%	2.47	0.01		0.03	0.75	0.97	61.0%	61.8%	0.3%	9.6%	0.7%	18.6%	24.3%
125 27 19 10 1.10 0.10 0.10 0.20 0.00 1.00 1.10 1.1	120	1		160	10				229	0.01		04	1.65	<u> </u>	100.0%	0.4%	80%	0.2%	28.3%	44.0%	2.49	001		0.01	0.62		67.7%	67.7%	0.4%	2.6%	0.2%	16.9%	25.7% 22.3%
122 33 Mt 10 10 422 601 144 605 671 177 1505F 678 578 678 178 178 178 178 178 178 178 178 178 1	122	1																															20.3% 22.8%
124 29 167 10 2.30 001 0.29 001 1.09 1.96 190.0% 0.2% 0.2% 0.2% 0.2% 0.2% 0.2% 0.2%	124	1	39	167	10	2.7	0 0.00		229	0.01	1.0	09	1.96		100.0%	0.3%	7.8%	0.3%	29.4%	52.9%	2.14	0.01	0.09	0.01	0.70	1.00	63.2%	63.2%	0.2%	25%	0.2%	19.0%	27.0%
135 40 168 10 1247 608 605 500 110 150 15025 6075 1558 6175 1558 6175 6175 6175 6175 6175 6175 6175 6175	125	1	40											\vdash							2.15	0.02	0.20	0.00									20.1% 21.5%

- M-patch Mid CH

															max ratio ou	t of all beams												max ratio out of all	beams		
П								4cm2 P	D)mW/on	v2)			100.0%	0.6%	42.5%	1.5%	31.2%	69.0%	*	iom2 PD(r	nW/cm2)	at 10mm eva	luation dis	tance	70.4%	70.4%	0.6%	32.5%	1.2%	22.0%	36.2%
No. Mi	dule Type	Seam ID_1	Sema ID,	2 Feed no.	54/Right	S3(Lef	t) SS(Top	56(8	lottom)	\$1(Frant)	S2(Rear)	per Seam Sack-oft (dS)	ratio (Right 2mm)/(wont- surface 2mm)	ratio (Left 2mm)/(worst- surface 2mm)	ratio (Top 2mm)/(worst- surface 2mm)	ratio (Bottom 2mm)/(wont- surface 2mm)	ratio (Fornt 2mm)/(worst- surface 2mm)	ratio (Rear 2mm(/(wont- surface 2mm)	54/Right	S3(Left)	t) SS(Top	S6(Botton	() S1(From	t) 52/Read	ratio wont-surface (10mm/2mm)	ratio (Right 10mm)/(worst- surface 2mm)	ratio (Left 10mm)/(worst- surface 2mm)	ratio (Top 10mm)/(worst- surface 2mm)	ratio (Sottom 10mm)/(wont) surface 2mm)	ratio (Front 10mm(/(wonst- surface 2mm)	ratio (Rear 10mm)/(worst- surface 2mm)
64 65 66 67 68 69 70 71		1		1	0.28	0.00	0.03		100	0.02	0.16		100.0% 100.0%	0.4%	10.7%	0.4%	8.5% 12.8%	57.3% 51.4%		0.00		0.00	0.01		38.1%	38.1%	0.4% 0.0%	75% 40%	0.4% 0.5%	19% 58%	20.6%
66		5 7		1	0.43	0.00	0.05	-	100	0.05	0.24		100.0%	0.2%	12.2%	0.2%	11.5%	56.2% 51.8%	0.18		0.04	000	0.02		41.7% 42.4%	41.7% 42.4%	0.2%	84%	0.2%	52% 48%	25.1%
68		9	_	1	0.19	0.00	0.06			005	0.22	-	100.0% 100.0%	0.3%	16.6%	0.2%	11.5%	52.6%		000		0.00	0.02		443%	44.3%	0.2%	92%	0.0%	62%	22.0% 20.5%
69		14		2	0.79	0.00			100	0.07	0.35		100.0% 100.0%	0.3%	27.9%	0.4%	9.0%	45.0% 58.2%	0.28	000	0.14		0.03		36.1% 51.1%	36.1% 51.1%	0.3%	18.3%	0.3%	19% 62%	14.9% 25.6%
71		16		2	0.78	0.00	0.06	-	100	0.14	0.50		100.0%	0.4%	7.0%	0.1%	17.4%	641%	0.44	000	004	0.00	0.07	0.25	56.0%	56.0%	0.3%	55%	0.1%	90%	31.3%
		17		2	0.70	0.00			100	0.05	0.31	+	100.0% 100.0%	0.3%	12.8%	0.4%	6.4% 13.4%	447% 52.9%	0.25	000	0.06		0.02		36.1% 45.0%	36.1% 45.0%	01% 02%	79% 11.2%	0.3%	10% 62%	16.0% 22.5%
74 75 76 77		22		2	0.62	0.00	0.03		100	0.10	0.42		100.0% 100.0%	0.2%	40%	0.6%	16.7%	67.4% 52.6%	0.35	0.00	002	000	0.05		55.5% 45.2%	55.5% 45.2%	0.2% 0.4%	24% 11.5%	0.6%	80% 56%	32.9% 22.9%
76		29	_	5	1.01	0.00	0.72	-	1.01	0.21	0.98	+	100.0%	0.3%	39.5%	0.7%	11.3%	54.0%	0.86	000	0.50	0.01	0.10	0.47	47.6%	47.6%	0.2%	27.5%	0.6%	5.5%	25.7%
77		30		5	1.63	0.00	0.38		101	0.27	1.13		100.0% 100.0%	0.3%	23.5%	0.7%	16.6% 21.8%	63.5%	0.98	000	0.14	0.01	0.15		60.0% 57.2%	60.0% 57.2%	0.2% 0.2%	16%	0.6%	8.9% 12.7%	36.2% 32.5%
78 79 80 81 82 83 84 85 86 87 88 89 90 90 91 92		32		ś	1.76	0.01	0.09	- 0	1.00	0.29	1.10		100.0%	0.4%	5.2%	0.1%	16.6%	67.0%	1.05	0.01	0.06	0.00	0.16	0.58	59.7%	59.7%	0.3%	12%	0.1%	9.3%	32.7%
80		33	_	5	1.16	0.01	0.59		100	0.11	0.71	-	100.0% 100.0%	0.4%	41.5%	0.3%	84%	52.1% 59.6%	0.56	000		0.00	0.05	0.35	41.1%	41.1%	0.3%	32.5% 22.9%	0.2%	16%	25.7%
82		39		5	1.75	0.01	0.16	-	2.01	0.34	1.14		100.0%	0.3%	9.1%	0.3%	19.4%	65.2%	0.99	0.00	0.05	0.01	0.19	0.59	56.4%	56.4% 56.2%	0.2%	29%	0.3%	11.0%	11.6%
83		40	_	5	124	0.01	0.11		100	0.35	1.25	-	100.0%	0.3%	5.8% 27.9%	0.1%	19.0%	68.0%	0.69	000	0.04		0.20		54.3% 56.0%	56.3% 56.0%	0.2% 0.5%	21%	0.1%	10.8%	35.5% 34.8%
85		129		1	0.25	0.00	0.02		100	0.05	0.05		100.0%	0.4%	64%	0.4%	18.1%	18.9% 24.5%				000	0.02		52.6% 51.6%	50.0% 53.0%	0.4%	40% 30%	0.4%	80% 10.0%	60%
87		133		1	0.43	0.00	0.03	-	100	0.09	0.09		100.0%	0.5%	7.7%	0.2%	20.4%	21.1%	0.22	0.00	0.02	0.00	0.04	0.03	52.3%	52.3%	0.2%	47%	0.2%	8.5%	80%
88		135		1	0.19	0.00	0.04		100	0.09	90.0		100.0% 100.0%	0.5%	10.9%	05%	23.4%	16.1% 21.3%	0.19	000	002		0.04		48.6% 53.4%	48.6% 53.4%	0.3% 0.2%	62%	0.5%	10.9%	57% 74%
90		142		2	0.74	0.00	0.09	-	201	0.13	0.13		100.0%	0.4%	11.8%	0.7%	18.0%	17.9%	0.25	0.00	006	0.01	0.07	0.05	342%	34.2%	0.3%	7.6%	0.7%	10.0%	64%
91		143 144	-	2	0.75	0.00			100	0.21	0.16	-	100.0% 100.0%	0.4%	13.9%	0.7%	27.9%	21.1% 33.2%	0.41	000			0.11		55.3% 65.4%	55.3% 65.4%	0.3%	7.9% 2.4%	0.5%	14.6%	8.4% 15.4%
93 94		145 149		2	0.58	0.00			100	0.09	0.11		100.0% 100.0%	0.3%	8.8% 17.9%	0.7%	14.7% 20.2%	19.2% 20.3%	0.20	000	004		0.04		34.1% 40.6%	34.1% 40.6%	0.3% 0.3%	6.1% 10.2%	0.7%	7.1% 10.4%	7.3% 6.1%
95	M Pasch	150		2	0.76	0.00	0.05	ľ	100	0.24	0.18		100.0%	0.5%	7.0%	0.3%	31.5%	23.1%	0.49	000	002	0.00	0.13	0.07	64.9%	64.9%	0.4%	29%	0.1%	16.8%	8.7%
96		151		2	1.16	0.00			101	0.21	0.14	_	100.0% 100.0%	0.4%	16.6%	0.8%	25.2% 26.2%	16.9% 25.7%	0.39	000			0.11		46.3% 55.3%	46.2% 55.2%	0.2% 0.3%	9.5%	0.5%	13.4%	57% 88%
98		158		5	1.40	0.00	0.42	-	2.01	053	0.33		100.0%	0.5%	28.3%	0.5%	35.8%	22.4%	0.99	0.01	0.18	0.01	0.33	0.15	66.7%	66.7%	0.4%	12.0%	0.5%	22.6%	12.0%
95 96 97 98 99 100 100 100 100 100 100 100 100 100		159		5	1.45	0.01			100	0.50	0.39	+	100.0% 100.0%	0.6%	7.9%	0.2%	34.6% 37.8%	27.2%		001		0.00	0.29		69.6%	69.6%	0.4%	32% 18%	0.1%	20.1%	11.0%
101		161		5	1.31	0.00			102	0.29	0.36		100.0% 100.0%	0.3%	35.2% 34.7%	12% 15%	21.9%	29.1% 26.4%		0.00			0.17		50.2% 47.7%	50.2% 47.7%	0.3% 0.2%	22.7% 22.0%	1.1%	13.0%	10.5%
102		167		5	1.70	0.01	0.12	-	2.01	0.57	0.54		100.0%	0.5%	6.9%	0.3%	33.5%	31.6%	1.20	0.01	004	0.00	0.35	0.22	70.4%	70.4%	0.4%	22%	0.2%	20.3%	12.7%
334		168		5	1.56	0.01			100	0.56	0.45	-	100.0%	0.6%	7.0%	0.2%	35.9% 36.2%	29.2%		0.01		0.00	033		70.2% 65.2%	70.2% 65.2%	0.5%	3.1% 7.2%	0.1%	21.4%	11.6%
106		1	129	2	0.56	0.00			100	0.09	0.23		100.0%	0.4%	99%	0.4%	15.0%	40.3%		000			0.04		47.0% 48.5%	47.0%	0.2%	7.0%	0.4%	6.2%	15.4%
107		3 5	131	2	0.76	0.00	0.05		2.01	0.16	0.34	+	100.0% 100.0%	0.4%	6.3%	0.8%	20.4%	41.5%		000	004		0.07		48.5% 50.5%	48.5% 50.5%	0.4%	44% 85%	0.8%	87% 81%	18.2%
129		7	135	2	0.83	0.01			100	0.18	0.36		100.0% 100.0%	0.6%	18.9%	05%	21.1%	42.7% 42.3%		000	0.10		0.09		45.8% 49.9%	45.8% 49.9%	05%	11.8%	0.4%	10.2%	15.8%
111		14	142	4	1.50	0.01	0.40		2.01	0.28	0.62		100.0%	0.4%	25.0%	0.8%	17.2%	29.1%	0.65	0.01	0.27	0.01	0.14	0.20	41.4%	41.4%	0.3%	16.9%	0.7%	8.7%	12.7%
112		15	143	4	154	0.00	0.23		100	0.35	0.58		100.0% 100.0%	0.3%	7.9%	0.8%	22.7%	37.5% 51.0%	0.84	0.00	0.15	0.01	0.19		54.3% 59.8%	54.3% 59.8%	0.2% 0.4%	9.8%	0.7%	12.2%	17.1% 25.7%
113		17	145	1	129	0.01	0.18	- 0	2.01	0.16	0.51		100.0%	0.4%	13.7%	0.8%	12.0%	29.6%	0.55	000	012	0.01	0.08	0.20	42.9%	42.9%	0.3%	9.4%	0.7%	5.9%	15.3%
115 116 117		21	149	4	1.91	0.00	0.44		201	0.43	0.79	+	100.0% 100.0%	0.2%	23.1% 58%	0.7%	22.6% 26.5%	41.5%	0.96	000	0.29		0.21		50.3% 59.2%	50.3% 59.2%	0.2% 0.3%	14.9%	0.6%	11.2%	16.1% 20.7%
117		23	151	4 10	1.76	0.01			2.01	0.39	0.72		100.0% 100.0%	0.6%	27.1%	0.6%	22.1%	41.5% 47.8%	0.95	001		0.01	0.21	0.29	541% 486%	54.1% 48.6%	0.4%	16.0%	0.5%	11.8%	16.5%
119		30	157 158	10	4.02	0.02	0.17	-	204	1,20	1.80		100.0%	0.5%	21.5%	0.9%	29.7%	44.0%	2.46	0.02		0.03	0.31	0.92	61.2%	61.2%	0.3% 0.4%	28.0% 8.6%	0.8%	7.6% 17.7%	22.3% 22.8%
120		31	159	10	142	0.02	0.28		100	1.03	1.65		100.0%	0.6%	8.1% 4.2%	0.2%	30.0% 29.4%	48.2%	2.11			0.01	0.63		61.5%	61.5%	0.4% 0.5%	2.1% 2.5%	0.2%	18.3%	23.2% 25.8%
122		32	161	10	1.10	0.02	1.45	-	2.03	0.58	1.59		100.0%	0.4%	42.9%	0.8%	17.2%	46.9%	1.02	0.01	1.05	0.02	0.28	0.73	53.7%	53.7%	0.4%	31.1%	0.7%	8.3%	21.4%
123		38	166	10	4.20	0.02			106	0.73	1.82	F	100.0%	0.4%	35.2% 6.7%	14%	17.4% 28.8%	43.4%	2.29	001	037		0.34		56.9% 62.4%	56.9% 60.4%	0.3%	21.0%	12%	8.1% 17.5%	12.4% 26.7%
118 119 120 121 122 123 124 125 126		40	168	10	2.57	0.02	0.24	-	2.01	1.06	1.85		100.0%	0.6%	6.0%	0.1%	29.8%	52.0%	2.18	0.02	0.10	0.00	0.61	0.95	61.0%	61.0%	0.4%	29%	0.1%	17.2%	26.7%
126		41	169	10	151	0.02	0.72		2.01	035	1.55	_	100.0%	0.6%	20.5%	0.2%	27.0%	443%	2.21	602	0.51	0.01	0.55	0.80	63.4%	63.4%	0.6%	144%	0.2%	15.6%	22.6%

- M-patch High CH

			-										-			max ratio ou	t of all beams												max ratio out of all	beams		
П		1			Г			-	4cm2 PD	(mW/on	n2)			100.0%	0.9%	41.7%	1.1%	31.2%	68.3%	4on	2 PD(mV	W/cm2) at	10mm evalu	ation dista	nce	74.7%	74.7%	0.9%	21.2%	0.9%	22.8%	42.4%
No. Mo	dule Typ	e Seam ID_1	Sema ID_2	Feed no.	П	Т			Т	П			per Seam	ratio	ratio	ratio	ratio	ratio	ratio							ratio	ratio	ratio	ratio	ratio	ratio	ratio
					54/8	ghe) Sã	(Left)	\$5(Top)	\$6(Bo	ttom)	\$1(Front)	S2(Rear	Back-of	(Right 2mm)/(worst- surface 2mm)	(Left 2mm)/(worst- surface 2mm)	(Top 2mm)/(wonst- surface 2mm)	(Bottom 2mm)/(wont- surface 2mm)	(Fornt 2mm)/(worst- surface 2mm)	(Rear 2mm(/(wont- surface 2mm)	S4(Right)	S3(Left)	SS(Top)	SS(Bottom)	S1(Front)	S2(Rear)	worst-surface (10mm/2mm)	(Right 10mm)/(wont- surface 2mm)	(Left 10mm)/(worst- surface 2mm)	(Top 10mm)/(worst- surface 2mm)	(Sottom 10mm)/(wont- surface 2mm)	(Front 10mm(/(worst- surface 2mm)	(Rear 10mm)/(worst- surface 2mm)
64	_	+	 	-	0.2		0.00	0.02	0.0	00	0.04	0.16	(d0)	100.0%	0.25	61%	0.7%	112%	514%	0.11	0.00	001	0.00	0.02	0.07	36.8%	265	0.3%	47%	97%	64%	23.0%
65		3		1	0.4		0.00	0.02	0.0		005	0.21		100.0% 100.0%	0.2%	5.6%	0.2%	12.2% 10.6%	52.2% 50.7%	0.14		002	0.00	0.03	0.11	35.1% 35.7%	35.1% 35.7%	0.2% 0.0%	39% 70%	02%	6.1% 4.0%	27.3% 25.0%
67		7	 		0.4	9 0	0.00	0.07	0.0	00	0.04	0.23	+	100.0%	0.2%	15.1%	0.2%	9.5%	52.4%	0.15	0.00	0.04	0.00	0.02	0.11	35.7%	35.7%	0.2%	9.3%	0.2%	42%	26.2%
68		9			0.1	6 0	0.00	0.06		00	0.05	0.19		100.0%	0.6%	15.9%	0.3%	13.4%	52.8% 33.9%	0.14			0.00	0.02	0.09	23.9% 12.7%	39.9% 12.7%	0.3%	95%	03%	54%	24.3%
70		15		2	0.6	7 0	0.00	0.05	0.0	27	0.10	0.36		100.0%	0.3%	6.9%	0.7%	15.2%	53.4%	0.28	0.00	003	0.00	0.05	0.21	42.4%	42.4%	0.3%	45%	0.6%	7.6%	30.7%
71		16	-		62		0.00	0.10		90	0.11	0.50	+	100.0% 100.0%	0.3%	13.2%	0.1%	14.4%	65.1% 49.2%	0.35			0.00	0.06	0.30	46.1% 29.5%	46.1% 29.5%	01%	89% 7.1%	0.1%	76%	38.7% 18.2%
73		21		2 2	0.5	6 0	0.00	0.15	0.0		0.12	0.49		100.0%	0.1%	15.4%	0.3%	12.3%	50.8% 61.2%	0.40	0.00	0.09	0.00	0.05	0.24	41.6% 48.0%	41.6%	0.1%	9.3%	0.3%	54%	24.8% 38.2%
76		22	 	2	0.0	9 0	0.00	0.19	0.0	00	012	0.39	+	100.0% 100.0%	0.2%	35% 26.7%	0.1%	19.5% 10.4%	50.1%	0.26			0.00	0.06	0.18	37.5%	48.0% 37.5%	0.2%	1.7%	0.5%	99% 49%	26.4%
76		29		5				0.63			0.17			100.0%	0.4%	35.9%	0.5%	95%	46.5% 85.0%	0.84			0.01		0.38	47.6% 54.1%	47.0%	03%	23.7%	05%	44%	21.7%
76		31		5	1.5	2 0	0.00	0.07	0.0	30	043	1.20		100.0%	0.2%	16%	0.2%	22.3%	62.7%	0.94	0.00	0.03	0.00	0.26	0.77	40.0%	48.8%	0.2%	14%	0.2%	13.3%	40.1%
79		32	-	5				0.17 0.62		9	023	0.76	+	100.0% 100.0%	0.4%	11.1%	0.3%	14.9%	68.3% 48.9%	0.71			0.00	0.13	0.66	46.7% 44.8%	46.7% 44.8%	0.3%	7.6% 28.8%	02%	84% 16%	43.4% 23.8%
81		38		5	11	2 0	92.0	0.55	0.0	32	0.32	0.97		100.0%	0.3%	30.3%	0.9%	17.6%	53.3%	1.02	0.01	0.33	0.02	0.17	0.51	56.4%	56.4%	0.3%	18.2%	0.8%	95%	28.2%
82		40	 	5	2.6			0.20	0.0	00	0.33	1.16	+-	100.0% 100.0%	0.2%	10.9%	0.3%	18.4% 17.6%	65.4%	0.91		004	0.00	0.19	0.75	50.7% 46.3%	50.7% 46.2%	01%	22% 30%	0.2%	10.8%	41.4% 42.9%
85		41 129			1.1			0.50		00	0.12	0.73	_	100.0%	0.5%	41.7%	0.3%	10.4%	60.8% 17.4%	0.61			0.00	0.06	0.40	50.7% 53.1%	50.7% 53.1%	0.4%	31.2% 2.9%	0.2%	5.1% 8.2%	11.6% 71%
BG		131		1	0.3	2 0	0.00	0.02	0.0	00	0.06	0.08		100.0%	0.3%	47%	0.3%	24.5%	26.1%	0.16	0.00	001	0.00	0.04	0.03	51.3%	51.3%	0.3%	3.1%	0.3%	11.6%	8.8%
87		133		-	83		0.00	0.03	0.0	00	0.07	0.07	_	100.0% 100.0%	0.6%	13.1%	0.6%	20.1%	20.1%	0.18			0.00	0.03	0.03	51.0% 44.1%	51.0% 44.1%	06% 03%	5.1%	0.6%	8.2% 7.8%	7.6%
89		137		1	0.3			0.06		00	0.00	0.06		100.0%	0.3%	15.7%	0.3%	19.0%	22.9%	0.16			0.00	0.03	0.03	94.1% 50.7%	94.7% 50.7%	0.3%	7.7%	0.3%	85%	7.7%
90 91		142		2 2	0.0			0.07	0.0	00	012	0.17		100.0% 100.0%	0.3%	10.6%	0.4%	18.1% 26.3%	24.7% 17.0%	0.22		005	0.00	0.06	0.06	32.1% 49.9%	32.1% 49.9%	0.3%	67% 72%	0.4%	8.8% 13.4%	63%
92		144		2			0.00		0.0		0.22	0.20		100.0%	0.3%	7.0%	0.2%	33.3%	29.8%	0.45			000		0.00	68.7%	68.7%	0.3%	44%	0.2%	16.8%	12.7%
93		145	 		0.5		0.00	0.04		00	0.10	0.14	+	100.0% 100.0%	0.2%	7.3% 17.0%	0.3%	16.7% 19.5%	245% 17.3%	0.21		003	0.00	0.04	0.06	36.1% 35.3%	36.1% 35.2%	0.2%	4.6% 9.5%	0.3%	7.5% 8.7%	10.5% 6.4%
94 95 96	M Pass	n 150		2	0.5		0.00	0.05	0.0	00	0.16	0.12		100.0%	0.9%	8.4% 19.5%	0.3%	31.4% 21.9%	20.0%	0.39	001	0.02	0.00	0.09	0.05	66.9% 44.0%	66.9% 44.0%	09%	3.6% 11.5%	0.3%	15.9%	83% 65%
97		157		ŝ	14	0 0	0.00	0.43	0.0	00	0.39	0.40		100.0%	0.3%	30.9%	0.3%	28.1%	28.6%	0.75	000	0.27	0.00	0.22	0.17	53.7%	53.7%	0.3%	19.3%	0.2%	15.5%	12.5%
98		158	_	5	12			0.31	0.0		0.43	0.26	+	100.0%	0.6%	24.9%	0.9%	34.5%	21.9%	0.79	001	012	0.01	0.26	0.11	62.8% 74.1%	62.8% 74.2%	05%	9.4%	0.8%	20.7%	89% 99%
100		160		5	1.6			0.07	0.0	00	0.64	0.51		100.0%	0.4%	44%	0.1%	38.2%	30.5%		0.01	003	0.00	0.36	023	72.6% 48.0%	72.6%	0.4%	2.0%	0.1%	22.8%	11.9%
101		161	_	5	1/4	9 0	0.00	0.47	0.0	21		0.42	+	100.0% 100.0%	0.2%	33.9%	0.4%	24.4%	29.8%		0.00	0.29	0.00			46.0%	48.9% 46.0%	01%	21.6%	0.3%	13.4%	12.3%
103		167		5	1.4		0.00	0.12		20	054	0.42		100.0% 100.0%	0.8%	7.9%	0.3%	36.8% 35.9%	29.0% 21.1%	1.07			0.00	0.10	0.18	73.2% 74.7%	73.2%	0.7%	34% 47%	02%	20.3%	12.5% 13.1%
105		169		5	1.2	9 0	0.00	0.20	0.0	00	0.46	0.34		100.0%	0.7%	15.2%	0.3%	35.4%	25.4%	0.77	0.01	0.13	0.00	0.26	0.14	60.1%	60.1%	05%	10.2%	0.2%	19.8%	10.5%
106		-	129	2	0.0			0.04		00	013	0.22		100.0%	0.3%	67%	0.7%	21.0%	35.1% 47.3%	0.30			0.00	0.06	0.09	48.6%	48.6% 44.7%	0.2%	50% 46%	0.7%	9.4%	14.2% 23.2%
108		- 5	133	2	0.5			0.11	0.0		0.14	0.37		100.0%	0.3%	12.1%	0.3%	16.0%	41.6%	0.38			0.00	0.06	0.16	42.4%	42.4%	0.3%	7.7%	0.2%	6.0%	17.4%
110		7 9	135		0.7			0.14		30	013	0.33	+	100.0% 100.0%	0.5%	18.6%	0.5%	16.4%	41.0% 38.1%	0.32			0.00	0.06	0.14	41.7%	41.7% 46.2%	0.4%	12.2% 9.6%	0.4%	7.9%	18.6%
111		14	142	4		3 0	0.00	0.37	0.0	21	0.28			100.0%	0.2%	22.8%	0.6%	17.0%	36.4%	0.62			0.01	0.13		37.7%	37.7%	0.2%	14.8%	0.6%	80%	15.0%
112		15	141	4	14			0.16		00	0.36	0.54	+-	100.0% 100.0%	0.6%	11.6%	0.8%	25.6% 23.4%	38.2% 48.6%	0.74				0.20	0.29	52.3% 57.4%	52.3% 57.4%	05%	7.3% 9.5%	0.7%	14.0%	20.8% 26.3%
114		17	145	4	11			0.15	0.0		0.20	0.56		100.0% 100.0%	0.3%	11.3%	0.6%	15.7% 20.2%	41.6% 42.4%	0.56		0.11	0.01	0.09	0.20	43.4%	43.4% 48.8%	0.3%	82% 11.8%	05%	7.0%	15.0% 18.5%
115		21	150	4	1.2	9 0	90.0	0.10	0.0	21	0.36	0.56	ᆂ	100.0%	0.8%	7.9%	0.5%	28.2%	41.6%	0.77	001	005	0.01	0.19	0.35	60.5%	60.5%	0.7%	40%	0.4%	14.9%	27.5%
117		23 29	151 157		14			1.42	0.0		0.31	152	F	100.0% 100.0%	0.5%	28.5% 37.8%	0.4% 0.5%	18.9% 17.4%	38.5% 42.4%	0.00 2.15			0.01	0.16	0.30	48.1% 57.6%	48.1%	0.4%	17.7% 25.1%	0.4%	98%	18.1%
119		30	158	10	46	6 0	920	0.81	ac	33	123	1.73	=	100.0%	0.3%	20.0%	0.8%	30.2%	42.7%	2.56	001	0.31	0.03	0.72	0.89	63.0%	63.0%	0.2%	7.2%	0.7%	17.7%	22.0%
120		31	159	10	2.1			0.32		21	1.00	1.49	+	100.0%	0.5%	10.1%	0.3%	30.1% 27.4%	45.6% 48.2%	1.86			0.01	0.55	0.90	58.3% 62.4%	58.3% 62.4%	0.4%	43% 42%	0.3%	17.4%	28.2% 26.2%
122		33	161	10	21	9 0	90.0	1.47	0.0	27	0.58	1.69	=	100.0%	0.3%	37.9%	0.3%	15.0%	43.4%	2.04	0.01		0.01	0.32	0.83	52.5%	52.5%	0.3%	26.6%	0.2%	8.2%	21.4%
123		38	166	10	210		0.00	1.09	0.0	22	1.14	1.65	+	100.0% 100.0%	0.3%	28.0%	1.1%	21.5% 31.0%	42.3% 51.3%	2.36	0.01	0.67	0.04	0.19	1.10	49.8%	49.2% 64.1%	0.2%	17.2% 2.6%	0.9%	10.1%	22.0% 29.9%
125		40	168	10				0.27		01	034			100.0%	0.5%	8.3% 30.1%	0.2%	28.8% 27.8%	56.4% 46.8%	1.00			0.00		1.13 0.77	55.1% 62.9%	55.1% 62.9%	0.4%	4.8% 22.8%	0.1%	16.6%	347% 252%
140		- 41	309	10			rare	0.82	- 01		vili	1.43	_	130,0%	U.9%	av.176	UJ3	27.875	74.87h	1.42	www	470	021	u45	0.77	ta.9%	su.3%	w/%	42.0%	V.37h		