FCC ID: A3LSMF721U

Power Density Simulation Report

Revision A

June 10, 2022

SAMSUNG ELECTRONICS

1. Simulation methodology for Power Density (PD)

1.1 Simulation tool

1.1.1 Tool description

For the simulation approach to calculating power density (PD) evaluation for mobile phone with mmWave antenna modules, ANSYS Electromagnetics suite version 2021.R2 (HFSS) is used. ANSYS HFSS is one of several commercial tools for 3D full-wave electromagnetic simulation used for antenna and RF structure design of high frequency component. ANSYS Electromagnetics suite version 2021.R2 (HFSS) is implemented based on Finite Element Method (FEM), which operates in the frequency domain.

1.1.2 Mesh and Convergence criteria

To solve the PD analysis using FEM, volume area containing simulated objects should be subdivided into electrically small parts that are called finite elements as the unknown functions. To subdivide system, the adaptive mesh technique in ANSYS Electromagnetics suite version 2021.R2 (HFSS) is used. ANSYS Electromagnetics suite version 2021.R2 (HFSS) starts to refine the initial mesh based on wavelength and calculate the error to iterative process for adaptive mesh refinement. The determination parameter of the number of iteration in ANSYS Electromagnetics suite version 2021.R2 (HFSS) is defined as convergence criteria, delta S, and the iterative adaptive mesh process repeats until the delta S is met. In ANSYS Electromagnetics suite version 2021.R2 (HFSS), the accuracy of converged results depends on the delta S. Figure 1 is an example of final adaptive mesh of the device (cross-section of top view).

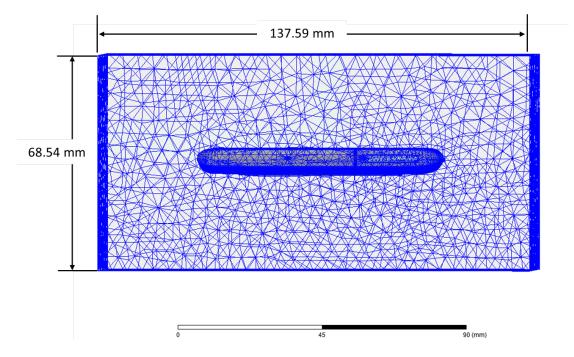


Figure 1 Example of the adaptive mesh technique (Top view)

1.1.3 Power density calculation

After solving 3D full-wave electromagnetic simulation, various kinds of physical quantities can be obtained. To calculate PD evaluation, two physical quantities, an electric field (\vec{E}) and a magnetic field (\vec{H}) are needed. The actual consumption power can be expressed as the real term of the Poynting vector (\vec{S}) from the cross product of \vec{E} and complex conjugation of \vec{H} as shown below:

$$\langle \vec{S} \rangle = \text{Re} \left(\frac{1}{2} \vec{E} \times \vec{H}^* \right)$$

 $\langle \vec{S} \rangle$ can be expressed as point power density based on a peak value of each spatial point on mesh grids, and obtained directly from ANSYS Electromagnetics suite version 2021.R2 (HFSS).

From the point power density $\langle \vec{S} \rangle$, the spatial-averaged power density (PD_{av}) on an evaluated area (A) can be derived as shown below:

$$PD_{av} = \frac{1}{A} \int_{A} \langle \vec{S} \rangle \cdot ds = \frac{1}{2A_{av}} \iint_{A_{av}} ||Re\{ExH^*\}|| dA$$

, where the spatial-averaged power density (PD_{av}) is total power density value considering on x, y and z components of point power density $\langle \vec{S} \rangle$ and the evaluated area (A) is 4cm².

1.2 Simulation setup

1.2.1 3D modeling

Figure 2 shows the simulation model which is mounted one mmWave antenna module. The simulation modeling includes most of the entire structure of device itself such as PCB, metal frame, battery, cables, and legacy antennas as well as mmWave antenna module called as Ant K. For a folder open status (Fig. 2-1), Ant K is placed on the left side and antennas are facing the left side. For a folder closed status (Fig. 2-2), Ant K is placed same of the folder open status.

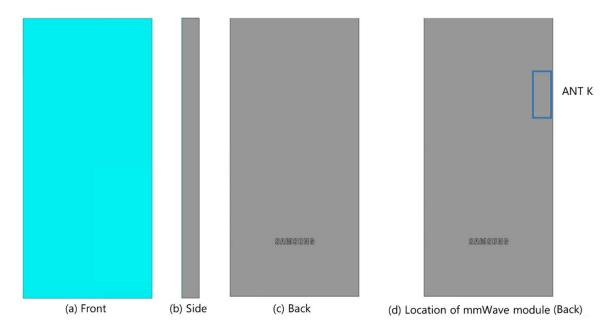


Figure 2-1. Simulation model which is mounted one mmWave antenna module (Folder Open Status)

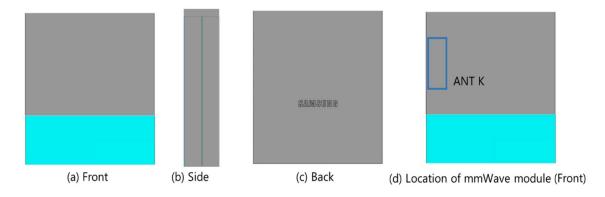


Figure 3-2. Simulation model which is mounted one mmWave antenna module (Folder Closed Status)

1.2.2 PD evaluation planes

Table 1 shows the PD evaluation planes for mmWave antenna module and Figure 3 shows the PD evaluation planes and whole area of the simulation model to find worst case of beamforming cases.

Please note that the "right" and "left" edge of mentioned in this report are defined from the perspective of looking at the device from the front side.

Table 1. PD evaluation planes

Module	Front	Back	Left From Front View	Right From Front View	Тор	Bottom
	S1	S2	S3	S4	S5	S6
Ant K	О	О	О	0	О	0

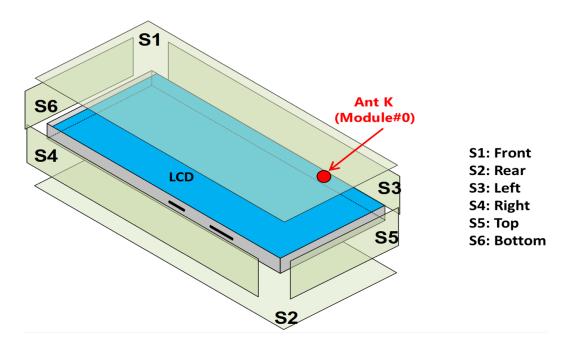


Figure 4. PD evaluation planes

1.2.3 Boundary condition

To simulate electromagnetic tool based on FEM, the boundary condition allows electromagnetic waves to be electrically open at the boundary and radiated far away without reflection. ANSYS Electromagnetics suite version 2021.R2 (HFSS) can support the absorbing boundary condition (ABC) for radiation boundary and make normally a quarter wave length from the radiating structure. In this report, to cover all beamforming cases of mmWave antenna module, 40 mm spacing from each surfaces of the device were used.

1.2.4 Source excitation condition

The number of antenna ports of ANT K for source excitation are the same. The antenna port of ANT K is divided into 10 ports for n261 1 x 5 patch array antennas, 10 ports for n260 1 x 5 patch array

antennas. In the 10 ports included in each patch antenna, 5 ports are divided into vertical polarization feeding, and the other 5 ports are divided into horizontal polarization feeding.

Figure 4 shows the ANT K module structure and surrounding structure. The ANT K module is encrypted in the ANSYS Electromagnetics suite (HFSS) and can only check the feeding position.

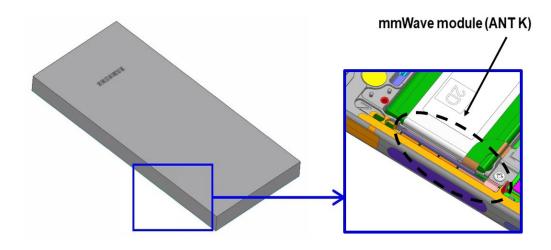


Figure 5. mmWave module (ANT K)

After finishing 3D full wave electromagnetic simulation of modeling structure, the magnitude and phase information can be loaded for each port by using "Edit Sources" function in ANSYS Electromagnetics suite (HFSS). Figure 5 shows an example of antenna port excitations.

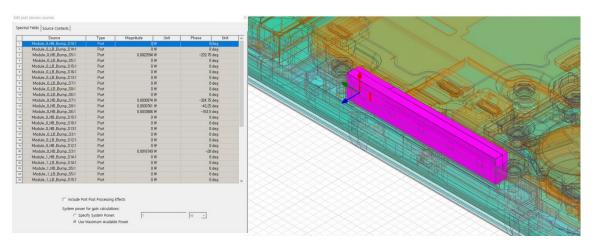


Figure 6. An example of port excitation (ANT K)

Since ANSYS Electromagnetics suite (HFSS) uses FEM solver based on frequency domain analysis method, the input source for the port excitation applies sinusoidal waveform for each frequency.

1.2.5 Condition of simulation completion

The simulation completion condition of ANSYS Electromagnetics suite (HFSS) is defined as delta S. The ANSYS Electromagnetics suite (HFSS) calculates the S-parameter for the mesh conditions of each step and determines whether to proceed with the operation of the next step by comparing the difference between the S-parameters in the previous step. A difference between the previous step and the current step of S-parameter is expressed as delta S, and the delta S generally sets 0.02. The simulation result of this report is the result of setting delta S to 0.02.

2. Simulation verification

2.1 Spatial-averaged power density

As mentioned in the previous chapter, the Poynting vector (\vec{S}) can be obtained through cross product of an electric field (\vec{E}) and complex conjugate of a magnetic field (\vec{H}) . The real term of the Poynting vector can be described as the point power density or peak power density. Using the point power density, the spatial-averaged power density can be obtained by the integral of 4 cm² at 2.5 mm intervals of the point power density result. Figure 6 shows examples of the distribution plot of point power density and the averaged power density.

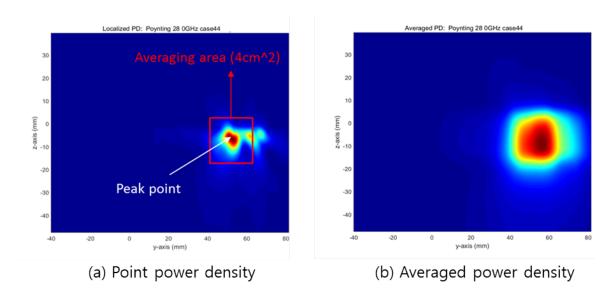


Figure 7. Power density distribution (Example)

2.2 Comparison between simulation and measurement

In this section, the simulated-power density distributions and measured-power density distributions are compared to each mmWave antenna.

Based on comparison of power density distributions, simulated power density and measured power density have a good correlation. The discrepancy in amplitude between simulated 4cm² averaged power density and measured 4cm² averaged power density is considered as housing influence and used in determining input power limit for each beam for RF exposure compliance.

The input powers per each active port are listed below for both Simulation and Measurement validation and power density characterization. For Simulation, these values were entered directly into HFSS model. For measurement, FTM S/W was used to input these values for each active port also.

Mode/Band	Antenna	Input Power (dBm) SISO	Input Power (dBm) MIMO
5G NR n261	K Patch	6.0	6.0
5G NR n260	K Patch	6.0	6.0
5G NR n258	K Patch	6.0	6.0

^{*} The below simulation and measurement result were performed at 2mm evaluation distance and 28GHz / 39GHz / 24GHz. The *input.power.limit* was determined based on below results in RF Exposure Part 0 Report.

					4cm² avg.P	$D(mW/cm^2)$
Band	Beam ID	Antenna	Surface	Channel	Meas.	Sim
	17		Front (S1)	Mid	0.365	1.244
	1 /		Left (S3)	Mid	0.866	2.238
n261	141	K (patch)	Front (S1)	Mid	0.608	0.668
	143		Rear (S2)	Mid	0.59	0.969
	148		Left (S3)	Mid	0.594	1.276
	15	K (patch)	Left (S3)	Mid	0.605	1.623
n260	20		Rear (S2)	Mid	0.446	0.871
	144		Left (S3)	Mid	0.491	1.346
	15		Front (S1)	Mid	0.582	1.030
n258	13	TZ (1)	Left (S3)	Mid	0.827	1.946
11238	141	K (patch)	Rear (S2)	Mid	0.698	1.036
	147		Left (S3)	Mid	0.8	1.269

(a) Measured PD for Folder Open Status

					4cm ² avg.P	$D(mW/cm^2)$
Band	Beam ID	Antenna	Surface	Channel	Meas.	Sim
	17		Left (S3)	Mid	0.957	2.313
n261	143	K (patch)	Front (S1)	Mid	0.349	0.947
	148		Left (S3)	Mid	0.639	1.305
	15	K (patch)	Left (S3)	Mid	0.53	1.652
n260	20		Front (S1)	Mid	0.391	0.856
11200	141		Front (S1)	Mid	0.231	0.684
	144		Left (S3)	Mid	0.575	1.362
	19		Left (S3)	Mid	1.2	2.011
n258	141	K (patch)	Front (S1)	Mid	0.596	1.002
	147		Left (S3)	Mid	0.918	1.285

(b) Measured PD for Folder Closed Status

[Folder Open Status]

• Table 2-1, n261 ANT K-Patch: Mid Channel, Beam ID 17 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD
17	S1 (Front)	ANT K		
17	S3 (Left)	ANTK	4	

Table 2-2, n261 ANT K-Patch: Mid Channel, Beam ID 141, 143 and 148 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD
141	S1 (Front)	ANTK		8
143	S2 (Rear)	ANT K	•	
148	S3 (Left)	AMTK	•	

• Table 2-3, n260 ANT K-Patch: Mid Channel, Beam ID 15 and 20 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD
15	S3 (Left)	ANTK	•	
20	S2 (Rear)	ANT K		

• Table 2-4, n260 ANT K-Patch: Mid Channel, Beam ID 144 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD
144	S3 (Left)	ANTK		

• Table 2-5, n258 ANT K-Patch: Mid Channel, Beam ID 15 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD
15	S1 (Front)	ANT K		
	S3 (Left)	ANTK	To the second	

• Table 2-6, n258 ANT K-Patch: Mid Channel, Beam ID 141 and 147 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD
141	S2 (Rear)	ANT K.		
147	S3 (Left)	ANTK	4	

[Folder Closed Status]

• Table 2-7, n261 ANT K-Patch: Mid Channel, Beam ID 17 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD
17	S3 (Left)	ANT K	**	

• Table 2-8, n261 ANT K-Patch: Mid Channel, Beam ID 143 and 148 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD
143	S1 (Front)	ANT K		
148	S3 (Left)	ANT K	•	

• Table 2-9, n260 ANT K-Patch: Mid Channel, Beam ID 15 and 20 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD
15	S3 (Left)	ANT K		
20	S1 (Front)	ANT K		

• Table 2-10, n260 ANT K-Patch: Mid Channel, Beam ID 141 and 144 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD
141	S1 (Front)	ANT K	***	
144	S3 (Left)	ANT K		

Table 2-11, n258. ANT K-Patch: Mid Channel, Beam ID 19 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD
19	S3 (Left)	ANTK	•	

Table 2-12, n258 ANT K-Patch: Mid Channel, Beam ID 141 and 147 for selected surfaces

Beam ID	Surface	View	Simulated PD	Measured PD
141	S1 (Front)	ANT K	•	
147	S3 (Left)	ANT K	0	

3 Simulation results

This section shows the PD simulation results of Ant K at 28GHz, 39GHz and 24GHz for each evaluation plane specified in Table 1 at two separation distances of 2mm and 10mm for open condition and 2mm and 5mm for closed condition. The ratio of PD exposure from front surface to the worst surface at 2mm, and the ratio of PD exposure from 2mm to 10mm (open) or 2mm to 5mm (closed) evaluation distance for each beam are also reported in this section to support RF exposure analysis for simultaneous transmission scenarios performed in the Part 1 Near Field PD report.

The relative phase between beam pairs is not controlled in the chipset design. Therefore, the relative phase between each beam pair was considered mathematically to identify the worst case conditions. The below MIMO results represent the highest reported MIMO simulation results after sweeping across the relative phase between beams a 5° step interval from 0° to 360° .

The worst-case simulated PD determined from the tables in this section were used for conservativeness in *input.power.limit* determination in RF Exposure Part 0 Report.

$3.1\ PD$ for Low/Mid/High Channel at $28GHz\,/\,39GHz\,/\,24GHz$

3.1.1 Ant K-Patch Antenna

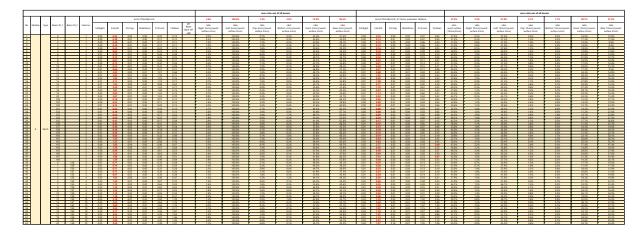
Table 3 to 5 show the PD simulation evaluation of Ant K patch antenna at 28GHz / 39GHz / 24GHz for the corresponding evaluation planes specified in Table 1.

Table 3. PD of Ant K – patch antenna (28GHz – n261)

[Folder Open Status]

K–patch Low CH

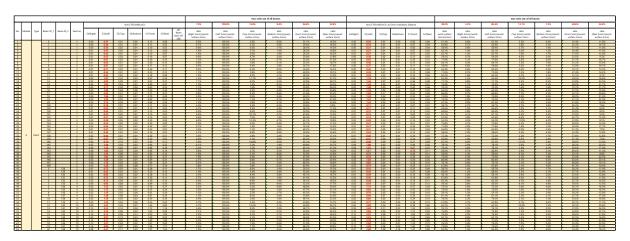


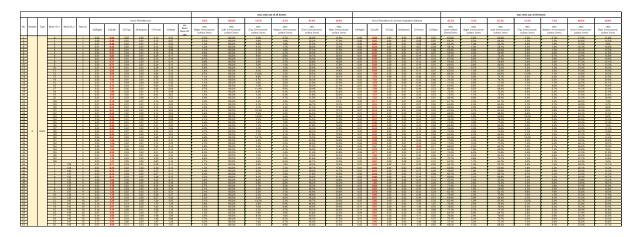


														max ratio ou	t of all beams									ı			max ratio out of all b	eams		
\Box							-	cm2 PDywwyc	ond)			2.8%	100.0%	7.2%	12%	73.6%	85.5%		6on2 PD)	nw(cn2) at 1	tonn eakat	ion distance		67%	210.8%	21.7%	2.1%	127.6%	103.8%	42.0%
No. M	dule Type	Beam ID	bj Benaibj	Feed no.	Septigen	S3(seb)	SS(Top)	Sirjkotom)	Stylvano	S2(Read)	per Beam Back-off (dit)	ratio (Right 2mm)/(worst- outlace 2mm)	ratio (Left 2mm)/(worst- curface 2mm)	(Top 2mm)/jeors- surface 2mm)	ratio (Bottom Jmm)/worst- surface Jmm)	ratio (Forst 2mm)/(worst- surface 2mm)	(Rear Jimm) (Nearch surface Jimm)	Strikght	SHARE	\$\$(Top)	Sé(Bottom)	\$1(Frant)	S2(Rear)	ratio worz-surface (12mm/2mm)	ratio (Right 15mm),r/word- surface 2mm)	ratio (Left 10mm)/(word- surface 2mm)	ratio (Top 10mm)/(worst- ourbor 2mm)	ratio (Rottom 15mm),/(worst- surface 2mm)	ratio (Font 10mm)/jwant- outlace 2mm)	ratio (Rear 10mm)/(worst- ourface 2mm)
1		0	_	- 1	4.00	0.40	0.00	0.00	0.19	0.12		0.5%	100.0%	1.0%	6.2%	47.0% 43.2%	32.6% 31.3%	4.00	0.15	4.00	630	0.07	034	0.2%	15.0%	4.2%	0.1%	7.0%	41%	11.2%
à		2		1	1.00	0.17	0.01	0.00	0.15	0.11		1.5%	100.0%	1.6%	0.5% 0.2%	41.6%	28.5%	4.00	0.12	0.01	0.00	0.0%	0.04	0.2%	12.1%	0.5% 0.5%	0.1%	52% 52%	35%	9.5%
-		4	_	1	1.00	0.41	0.01	0.00	0.17	0.52		97%	100.0%	1.2%	0.2%	53.0%	26.5%	4.00	0.12	0.01	0:33	0.0%	0.24	0.2%	17.5%	4.5%	0.0%	8.6%	18%	9.5%
6		- 1		-	0.00	0.62	0.01	0.00	0.25	0.19		0.6% 1.5%	100.0%	2,2% 0,7%	0.5%	40.1%	28.4% 27.2%	0.00	81.0	2.01	630	0.10	0.07	0.2%	17.9% 34.7%	1.1%	0.2%	5.9% 56.7%	7.1% 10.7%	11.4% 14.8%
		1		2	0.00	0.70	0.02	0.00	0.34	0.24		0.6%	100.0%	2.1%	0.7%	48.5% 28.6%	24.5% 26.8%	4.00	0.11	0.01	0.00	0.14	0.29	0.2%	31.3% 22.4%	11%	0.2%	13.7%	9.0%	12.9%
10		- 9	_	1	2.01	0.64	02.0	0.00	0.22	0.19	-	0.6%	100.0%	12%	0.6%	47.3%	32.9%	1.00	0.25	0.01	0.00	0.10	0.27	0.2%	25.4%	9.7%	0.2%	12.1%	1.9%	13.0%
11		10		-	0.01 0.01	0.69	0.61	0.00	6.25	0.25		67% 18%	100.0%	1,6%	0.1%	\$1.1% 49.1%	36.7% 31.6%	1.00	0.32	2.01	630	0.14	0.11	0.4%	22.4%	2.0%	0.1%	12.9%	10.6% 5.2%	15.4%
12		12		- 6	2.01	1.92	62.0	0.01	637	2.66		0.5%	100.0%	1.1%	0.5%	50.3%	34.2%	4.01	0.88	4.01	031	2.46	0.28	0.6%	22.4%	14%	0.8%	45.9%	27.7%	14.6%
56		13		- 5	0.02	1.86	0.61	0.00	1.54	0.62	+	10%	100.0%	0.2%	0.1%	61.2% \$7.6%	23.5% 28.2%	0.01	0.92	4.00	0.00	0.59	0.29	1,3%	98.2% 86.8%	125	0.1%	59.1% 49.2%	29.1%	15.7% 17.0%
		15	_	- 5	0.01	2.03	60.0	0.00	1.19	0.67	-	0.6% 0.2%	100.0% 100.0%	1.5%	0.2%	56.4%	22.8% 22.4%	0.01	1.05	4.03	0.00	0.66	0.28	0.9%	105.2% 85.7%	2.6% 7.8%	0.1%	66.3% 42.1%	27.5% 20.4%	13.5%
19		17		-	4.01	2.02	0.02	0.00	1.16	2.64		0.6%	100.0%	1.0%	0.2%	62% 97.6%	31.6%	0.01 0.01	1.05	102	0.00	4.07	0.82	0.9%	165.1%	16%	0.2%	\$7.0%	26.5%	13.1%
19		19	_		0.02	1.52	0.61	0.00	0.90	2.60	_	15%	100.0%	0.5%	0.1%	\$7.5% \$1.2%	28.2%	0.02	0.78	1.00	0.00	0.49	0.28	1.8%	22,7% 106,2%	175	0.1%	48.1% 59.1%	26.2%	18.0%
21		20		- 6	0.02	2.04	6.63	0.00	107	2.69		67%	120.0%	24%	0.1%	52.2%	22.9%	0.01	0.97	1.06	6:20	8.56	631	1.0%	96.5%	57%	0.2%	49.7%	20.6%	15.0%
23		129		1	0.00	0.17	0.01	0.00	0.11	0.12	_	2.1%	120,0%	245	0.4%	44.2% 45.1%	47.2%	1.00	0.09	0.01	0.00	0.02	034	0.4%	845	165	0.1%	24%	195	16.5%
24		130		1	1.00	0.24	0.01	0.00	0.10	0.12		12% 22%	100.0%	2.9%	0.4%	40.1% 40.1%	52.5% 64.0%	4.00	0.00	0.01	630	4.03	034	0.2%	8.1% 7.8%	4.6%	0.1%	245	46%	18.2% 22.9%
26		132		-	0.01	0.21	0.00	0.00	0.00	0.16		23%	100.0%	2.9%	0.5%	27.6%	76.1%	4.00	0.00	0.01	6:30	0.02	0.25	0.3%	7.6%	0.5%	0.1%	27%	5.4%	26.76
27		122		2	0.01	0.14	0.02	0.00	0.18	0.22	+	25%	100.0%	0.6%	12% 02%	\$1.9% 42.6%	64.7%	0.01 0.01	0.09	1.02	0.00	0.06	0.15	0.9%	E.P% 22.0%	125	0.2%	5.6%	7.9%	22.4%
29		125		- 2	0.01	0.17	0.01	0.00	0.17	0.25		27% 21%	100.0%	2.7%	0.2% 0.2%	41.7%	68.2% 62.0%	0.01 0.01	0.16	0.01	0.00	2.07	0.14	0.8%	16.0%	1.0%	0.1%	7.0% 6.8%	13.6%	28.7%
21				2	0.01	0.16	62.0	0.00	0.18	0.17		2.2%	100.0%	6.7%	0.6%	51.3%	47.9%	0.01	0.12	0.01	6:30	0.06	0:26	0.5%	11.6%	13%	0.2%	5.9%	57%	15.9%
22	K Patch	128		-	2.01	0.15	0.01	0.00	0.17	0.24	-	2.1%	100.0%	24%	0.3%	48.2%	67.0%	0.01	0.16	0.01	630	2.09	0.13	0.9%	15.8%	0.6%	0.1%	7.6% 6.8%	12.6%	28.5%
24		140		- 5	4.02	0.72	60.0	0.01	0.28	8.55		27%	100.0%	1.6%	1.5% 0.2%	\$3.2% \$5.1%	27.4% 45.2%	0.01 0.03	0.23	4.02	621	0.18	0.22	1.4% 2.8%	23.2% 57.0%	1.8%	0.7%	17.6% 20.9%	22.2%	21.0% 25.5%
26		142			0.04	1,10	0.00	0.00	0.59	0.74	+	3.2%	100.0%	0.8%	0.2%	47.8%	59.5%	0.02	0.65	0.01	0.00	0.30	0.41	2.4%	65.1%	0.6%	0.2%	29.6%	40.8%	32.9%
27		143		- 6	2.03	1.03	0.04	0.00	0.48	0.88		2.4%	100.0%	4.2%	0.1%	46.7% 46.1%	85.5% 54.6%	4.02	65.0	4.03	0.00	0.22	0.43	1.6%	29.6% 50.0%	24%	0.1%	21.9%	43.0%	42.0% 19.6%
39		145		- 3	4.03	0.90	0.03	0.00	0.56	2.47		2.8%	100.0%	32%	0.4%	62.1%	52.6%	403	0.40	102	0:00	0.26	026	2.8%	29.6%	16%	0.2%	25.6%	25.6%	28.5%
41		547	_	- 6	0.03	1.05	0.00	0.00	0.51	0.59	+	22%	100.0%	2.0%	0.1%	49.0%	49.5% 77.6%	0.02	0.67	0.02	0.00	0.30	0.42	12%	46.9%	155	0.1%	26.1%	41.7%	27.7%
42		149	120	5	2.03	132	0.09	0.00	0.59	0.78	=	21%	100.0%	20%	62%	43.9% 45.7%	59.5% 43.1%	2.02	0.50	0.06	6:00	0.21	632	1.9%	50.4% 22.7%	62%	0.2%	21.4%	22.1% 12.8%	24.65
44		1	129	2	0.01	0.68	0.02	0.00	0.31	0.27		15%	100.0%	2.8%	0.2%	6.8%	42.1%	0.01	0.36	0.01	0.00	0.12	0.11	0.9%	25.9%	13%	0.2%	11.9%	10.7%	15.9%
46		1	120	1 1	1.01	0.59	62.0	0.00	6.22	0.24	-	19%	120.0% 120.0%	2.9%	0.6%	47.6%	35.2% 36.2%	0.01 0.01	0.12	0.02 0.01	0:30 0:30	0.12 0.12	0.29	0.7%	21.9% 24.8%	1.6%	0.2%	12.0%	125	12.9%
47		-	132	- 2	0.01	0.71	0.02	0.00	0.36	0.29	=	12%	100.0%	2.2%	0.2%	50.6% 44.0%	41.2%	0.01	0.30	4.01	630	0.14	0.14	0.8%	30.4%	1.2%	0.2%	13.7% 21.3%	13.7%	13.4% 13.0%
49			124		2.02	1.26	0.00	0.00	674	2.66		2.1%	100.0%	0.7%	62%	59.1%	\$2.5%	4.02	0.61	0.01	630	0.36	6.20	1.6%	61.1%	17%	0.2%	25.6%	29.5%	23.7%
50		1	135	1	4.02	1,22	0.02	00.00	0.59	0.56	+	15%	100.0%	1.9%	0.5%	\$7.7% \$0.5%	45.5%	4.02	0.97	0.02	0:00	0.29	0.28	1.6%	56.7% 51.9%	17%	0.2%	23.9%	29.1%	22.9%
52		9	127	4	4.02	1.17	0.04	0.01	6.74	0.42		1.6%	100.0% 100.0%	1.5%	0.5% 0.2%	62.6% 61.4%	27.0% 45.9%	4.01	0.46	4.02	031	0.32	0.16	1.1%	45.7%	2.2%	0.5%	21.5% 21.7%	16.1%	13.7% 23.7%
54		11	139	1	4.02	1.17	0.06	0.00	0.64	0.54		1.6%	100.0%	5.0%	0.2%	94.7%	45.8%	0.01	0.51	0.05	0:20	0.24	0.25	1.2%	50.7%	45%	0.4%	24.3%	24.7%	21.1%
55		12	140	10	0.04	216	0.06	90.0	2.06	1.49		1.5%	100.0%	1,8%	0.8% 0.2%	65.4% 72.6%	41.4% 44.7%	4.03	į	0.04	632	1.05	0.55	2,8% 5,7%	122.7%	125	2.1%	1045%	54.6% 82.2%	17.2% 24.7%
57		14	142	10	0.10	255	60.0	0.61	2.12	1.65		2.9%	100.0%	0.7%	0.2%	60.0% 65.9%	46.5%	0.06	1.97	0.01	0.21	1.07	0.85	6.1%	166.9%	1.2%	0.5%	107.4%	99.1%	26.8%
59		15	143	10	0.07	429	0.08	93.0	2.69	1.95	-	15%	100.0% 100.0%	2.1% 6.5%	0.5%	57.1%	44.0%	1.04	1.99	0.06	030 031	1.05	104	4.0% 5.2%	196.5%	21.1%	0.2%	123.9%	123.8% 92.6%	25.4%
60		17	145	10	1.06	2.29	60.0	0.01	2.54	1.27		12%	100.0%	1.9%	0.3%	63.0% S6.6%	41.3%	4.04	1.68	4.04	621	1.11	0.74	42%	168.0%	126	0.8%	111.2%	75.8%	22.4%
62		19		10	2.06		60.0	0.00	2.62	1.77		1.6%	100.0%	0.9%	0.1%	67.2%	45.5%	0.04	2.11	0.02	0.00	1.28	1.01	2.9%	211.8%	2.2%	0.2%	127.5%	121.0%	25.9%
63		- 20	148	16	0.06	4.17	0.22	0.00	262	197	_	14%	100.0%	5.1%	0.1%	59.9%	42.8%	0.04	2.67	0.16	6:00	113	697	43%	207.0%	16.0%	0.4%	113,3%	96.5%	22.1%

[Folder Closed Status]

- K-patch Low CH





														max ratio ou	t of all beares												max ratio out of all b	eares		
								dow2 PD(wW	(on2)			69%	100.0%	16.1%	8.1%	80.0%	22.2%		4cm2 PD	(nW(on2) at	Sono evaluatio	n distance		81.2%	49%	81.2%	13.0%	7.8%	\$7.0%	26.2%
Acclude Type	e fea	m D,1	ilena 10,2	Feed no.	Septigne)	Skijurkij	SS(Tap)	Sirjiumor		e) S2(Rea	per Beam Back-off (SR)	ratio (Kight 2mm)/(worst- outace 2mm)	ratio (Left 2mm)/(worz- surface 2mm)	ratio (Top 2mm(//word- ourface 2mm)	ratio (Rotton Jimm)/(worth- surface Jimm)	ratio (Fant Jann)/(word- surface Jann)	ratio (Rear 2mm)/(worst- surface 2mm)	Se(Right)	Sajueti	SS(Top)	Sé(katan)	\$1(Foxe)	S2(Next)	stio worz-suface (Smm/2mm)	ratio (Right Smm)/(worst- ourface Jmm)	ratio (Left Smm)/(worth surface 2mm)	ratio (Top Smm)/worz- curtace 2mm)	ratio (Rotton: Smin)/(world- ourface 2mm)	ratio (Front Smin)/(worst- ourbox 2mm)	ratio (Rear Smort)/w surface 2min
	=	0		-1-	4.00	0.42	0.01	0.00	0.12	62.6	_	1.0% 0.7%	100.0% 100.0%	19%	1.0%	29.6%	17.1%	0.00	0.27	93.0 93.0	4.00		4.05	63.9%	0.7%	62.9%	2.6% 1.7%	1.0%	17.5%	12.5%
		2 2		- 1	0.00	0.29	0.02	0.01	0.12	0.06		1.0%	100.0% 100.0%	425	1.8%	29.2%	11.7%	0.00	0.25	0.01	0.01	60.0	0.02	62.4% 59.1%	0.8%	62.4% 59.1%	2.6%	1.8%	17.0%	8.6%
		4		-	4.00	0.42	0.01	0.00	0.12	93.0		0.9%	100.0%	2.4%	1.5%	25.4%	17.8%	0.00	0.20	93.0	0.01	50.0	0.06	66.2%	0.7%	66.2%	2.2%	1.5%	14.5%	13.2%
		5		2	0.01 0.01	0.66	0.03	0.02	0.19	0.12		0.8%	100.0%	51% 35%	2.7%	200	14.9%	0.00	0.36	90.00	0.02	0.12	0.09	54.8% 74.7%	0.9%	54.8% 74.7%	4.5%	2.6%	17.5%	11.63
		2 8		3	4.00	0.75	0.01	0.62	0.25	0.15	_	0.5% 0.7%	100.0% 100.0%	15%	2.0%	22.4%	19.6%	0.00	051	90.01	4.01	0.17	0.11	69.3% 53.9%	0.4%	68.2% 53.9%	12%	5.7% 2.5%	22.4% 17.5%	15.2
		ý.		-5-	0.01	0.74	4.03	0.00	0.24	0.12		0.7%	100.0%	43%	1.6%	32.3%	17.9%	0.00	0.47	90.0	0.01	0.16	0.10	62.8%	0.5%	62.8%	3.9%	15%	21.3%	13.57
	-	10 11	_		2.01	0.78	2.02	0.65	9.27	0.16	_	0.6%	100.0%	195	1.4%	34.2%	20.1%	0.00	457	0.61	2.01	0.18	0.12	72.6%	0.5%	72.6% 61.9%	15%	13%	23.0%	15.0
		12		-3-	0.01	2.00	0.25	0.00	3.65	0.45		0.6%	100.0%	12.4%	12%	22.5% 32.4%	22.5% 36.6%	0.01	124	0.22	4.02	0.45	426	67.0%	0.6%	67.0% 22.4%	11.0%	115	22.4% 13.3%	17.9
				- 6	1.02	1.91	0.01	0.01	2.68	0.53		12%	100.0%	4.7%	0.2%	25.8%	27.8%	0.02	148	0.07	0.01	0.47	0.66	74.7%	1.0%	747%	0.5%	125	25.1%	24.01
	=	15		=	4.03	2.12	1.02	0.04	0.67	0.58	_	12%	100.0%	1.0%	1.6%	21.7%	27.5%	0.02	151	0.02	4.03	0.43	249	70.6%	0.9%	21.9% 64.0%	0.8%	14%	20.2%	22.6
		17		_	4.02	214	6.22	0.02	2.67	0.55		0.7%	100.0%	10.1%	1.0%	21.4%	25.7%	93.0	151	0.18	4.02	0.45	2.45	70.5%	0.6%	71.5%	3.4%	1.9%	21.0%	212
		18 19	-	-	0.02	2.10	0.01	0.01	2.68	0.50	_	1.7%	100.0%	1.0%	0.4%	22.4%	27.3%	0.02	136	0.01	0.00	0.48	152	73.7%	1.5%	72.7% 72.7%	4.7% 4.9%	12%	26.2% 21.7%	23.1 24.6
	=	20 128		=	4.02	2.14	4.03	93.0	0.67	62.6		1.1% 2.5%	100.0%	1.4% 2.5%	25%	21.1% 26.1%	24.7%	0.02	1.66	6.03	4.07	0.46	2.62	69.1%	0.8%	68.1%	12%	21%	21.2%	19.0
				-	0.01	0.35	0.01	0.00	9.11	9.03		2.4%	100.0%	2.6%	44%	46.2%	12.0%	0.00	0.16	22.0	0.01	0.06	4.02	65.1%	2.0%	65.1%	2.0%	3.6%	25.7%	621 831
		132	_	1	0.01	0.35	0.01	0.01	0.12	60.0		24%	100.0%	4.0%	2.2%	50.0% 65.0%	11.2%	93.0	0.15	0.01	0.01 0.01	0.07	1.02	61.3%	2.0%	65.5%	12%	2.8%	29.0% 40.2%	11.
		132		- 5	4.01	0,31	0.01	0.01	0.16	60.0		4.2% 6.0%	100.0% 100.0%	6.7% 10.5%	2.2% 5.7%	34.2% 64.2%	11.9%	0.01	0.14	0.01	4.01	0.09	4.02	67.6% 52.6%	2.9%	67.6% 52.0%	57% 87%	2.9%	44.2% 26.6%	9.5
		124		- 2	0.02	0.47	2.01	0.00	0.31	9.00	_	4.4%	100.0%	2.7%	0.6%	64.2%	16.2%	0.01	0.26	0.01	4.00	0.23	2.06	74.9%	2.0%	74.9% 77.6%	2.2%	2.4%	47.9%	12
		136			0.01 0.01	0.17	0.00 0.01	0.00	4.27	0.06		2.0%	100.0%	1.6%	42%	62.0%	16.2%	93.0	0.27	0.00	0.01 0.02	0.19	0.05	72.6% 66.6%	2.7%	56.6%	12%	1.9%	52.0% 42.4%	12.
w	. =	122		3	0.01	0.18	0.02	0.62	0.18	0.06		2.9%	100.0%	44%	4.4%	6.75	12.0%	0.01	022	0.02	4.02	0.12	0.04	59.8% 73.2%	2.8%	59.8% 73.2%	4.2%	2.05	25.2% 50.8%	97
A Paul	_	122		- 1	0.01	0.43	0.01	0.02	0.27	0.06		2.1%	100.0%	14%	42%	62.0%	13.7%	0.01	0.29	0.01	4.02	0.18	0.05	66.6%	1.6%	66.6%	12%	37%	42.4%	10
		143	-	- 5	0.02	0.78	0.09	0.03	0.56	0.17	_	2.1%	100.0%	10.4%	2.7% 1.6%	72.6% 44.5%	21.4%	0.02	0.49	9.67	0.03	0.38	013	62.2% 22.6%	2.7%	62.2% 27.0%	125	32%	48.9% 24.0%	17.
		142		- 3	0.05	135	4.02	0.65	0.72	0.29	_	2.8%	100.0%	14%	0.8% 4.1%	58.4% 80.0%	22.4%	0.64	0.99	0.02	0.01	0.55	0.24	79.3%	2.1%	78.2% 66.9%	13%	16%	43.8% 56.9%	19
				\rightarrow	0.04	1,87	4.05	0.04 0.11	0.70	0.18	_	2.7%	100.0%	175	81%	90.0% S2.0%	14.8%	9.03	9.71	0.02	0.10	0.44	0.16	62,8%	245	62.8%	125	7.85	22.7%	12.
		145		-	1.06	0.86	0.04	0.02	0.47	0,22		2.0%	100.0%	415	2.7%	6.75	23.0%	0.04	961	0.03	0.02	0.36	55.5	71.7%	4.9%	71.7%	3.0%	185	41.6%	19
		147		=	4.6%	1.03	4.02	0.00	0.81	0.21		5.2%	100.0%	15%	2.0%	28.1% 56.2%	20.0%	0.64	0.75	93.0	4.02	0.59	0.16	72,2%	1.9%	72.2%	12%	1.6%	\$2.6% \$2.4%	- 15
		0	128	-	0.04	0.67	2.02	0.09	0.79	0.11	_	17%	100.0%	225	1.7%	41.7%	54.8% 56.1%	93.0	0.89	0.02	0.09 0.01	0.19	0.16	61.1%	146	63.2%	1.8%	155	28.4%	11.
		1	129	-	0.01	0.79	4.02	9.02	0.29	0.14		1.1%	100.0%	2.2% 4.1%	2.8%	25.9%	19,2%	10.0	051	0.02	4.02	0.18	0.11	64.7%	0.9%	64.7%	1.9%	2.4%	23.2% 18.4%	12.
		ì	131	- 2	4.03	0.72	4.03	0.02	0.27	0.12		2.8%	100.0% 100.0%	45%	2.2%	20.4%	14.1%	0.02	0.65	0.00	4.02	0.16	0.09	61.5%	3.2%	61.5%	4.0% 3.0%	2.1%	22.3% 25.0%	10.
	\vdash		133	4	0.02	1.14	0.01	02.0	453	0.13		2.6%		8.1%	6.1%		19.2%	93.0	262	0.09	0.02	0.18	0.10	69.2% 54.1%	2.6%	68.2% 54.1%	7.2%	5.6%	32.6%	
		-	134	-	0.04	134	0.05	0.01	2.67	0.28		2.1%	100.0% 100.0%	3.9%	0.7% 1.9%	50.3% 46.2%	21.0%	93.0	0.98	0.64	0.01	0.47	120	22.2%	2.5%	72.2% 31.5%	3.2% 1.4%	1.6%	35.5% 34.7%	15.
		ž.	136	-	4.02	1.44	4.0%	0.06	0.61	0.28		1.5%	100.0%	3.2%	3.9%	42.4% 20.7%	19.4%	0.62	0.00	0.64	4.0%	0.42	0.21	60.8%	1.1%	60.8%	2.8%	12%	29.2%	14 17
		10	132	4	4.02	1,22	0.06	62.0	0.49	0.28	-	1.6%	100.0% 100.0%	50% 21%	2.5%	47.2%	22.7%	0.02	0.75	0.06	4.02	0.43	0.22	61.2% 73.8%	1.2%	61.2% 72.8%	1.7%	13%	25.6% 25.1%	17.
		11	129	4	102	124	0.04	0.67	8.51	0.24	_	1.6%	100.0%	13%	5.2%	41.0% 40.5%	19.1%	0.02	0.83	0.04	106	0.34	0.19	67.1%	1.6%	62.1%	2.8%	47%	27.6%	14
	<u></u>	12	141	10	0.11	249	0.10	62.0	159	1.12		2.2%	100.0%	2.9%	0.8%	45.2%	32.2%	0.08	262	0.08	403	120	192	25.1%	2.65	75.1%	2.1%	47%	24.5%	24
	\vdash	16	142	10	0.12	471	0.03	0.02	166	1.12		32%	100.0%	185	25%	625	20.1%	0.10	2.05	0.69	0.02	129	100	27.8%	2.8%	77.2% 22.0%	4.7%	14%	24.9%	25
		16	144	10	0.09	435	0.09	0.21	197	1.13		1.6%	100.0%	1.9%	65%	20.4%	23.9%	93.0	3.11	93.0	0.27	135	0.88	65.5%	1.4%	65.5%	1.5%	262	28.4%	- 19
		18	145	10	0.10	1.10	2.03	9.04	1,27	0.90	_	2.0%	100.0% 100.0%	2.5%	1.2%	20.6%	29.3% 27.8%	90.09	2.45	0.03	0.04 0.02	0.95	0.81	70.6%	2.1%	75.6% 75.4%	6.1% 0.7%	1.0%	21.5%	22.
		19	147	10	0.12	4.06	0.04	60.0	175	126		2.8%	100.0%	11%	0.8%	40.2% 20.1%	31.1%	0.09	105	0.04	4.03	1.36	1.06	75.2%	2.2%	75.2%	1.9%	4.7%	23.5%	26.5

Table 4. PD of Ant K – patch antenna (39GHz – n260)

[Folder Open Status]

- K-patch Low CH

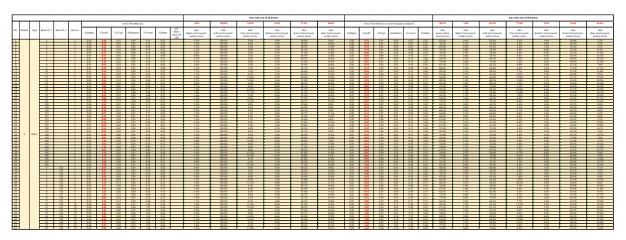
-														max ratio eu	t of all beams									ı			max ratio out of all b	eams		
								dow2 POgwwyi	onů)			62%	100.0%	7.2%	25%	\$7.8%	9.6		60n2 PD)	nW(on2) at 1	tünin evaluati	on distance		64.9%	42%	64.9%	53%	2.4%	25.0%	26.1%
No. Mo	dule Type	Beam ID.	5 Berna 10,2	Feed no.	Septigen	Shipeto	SS(Top)	Sicketton	S1(Frant)	S2(Rear)	per Beam Back-off	ratio (Right 2mm)/(worst- outlace 2mm)	catio (Left 2mm)/(wontr- curface 2mm)	ratio (Top 2mm)/(worst- surface 2mm)	ratio (Ration 2mm)/(worz- surface 2mm)	ratio (Forst Zimm)/(worst- surface Zimm)	(Rear Jimm)/(waren surface Jimm)	Strikgte	stude	SS(Sop)	Séciliamoni	\$1(Frant)	S2(Rear)	usio worz-surface (10mm/Qmm)	ratio (Kight 15mm),/worz- surface 2mm)	ratio (Left 10mm)/(ecoro- surface 2mm)	ratio (Top 10mm)/(worst- surface 2mm)	ratio (Rottom 10mm),/(worst surface 2mm)	otio (Fort t0mm)/(word- outlor 2mm)	ratio (Rear 10mm)/(word- ourface 2mm)
-	_	0				0.37	0.00	0.00	0.10	0.11	100	0.4%	100.0%	1.5%	1.5%	34.9%	29.7%			1.00		4.03		34.6%	0.4%	24.6%	1.1%	67%	10.7%	14.7%
2		1 2	+	1	0.00 0.01	0.25	0.00		0.19	0.11	_	12% 22%	100.0% 100.0%	1.6%	0.6%	27.6% 49.0%	43.6% 23.9%	1.00	0.10	1.00	0.00	0.03	034	41.2%	0.8% 1.2%	41.2% 43.0%	1.2%	0.6%	10.0%	16.4%
4		- 3	=	1	0.01	0.35	0.00	0.00	0.10	0.11		22%	100.0%	0.8%	0.4%	20.2% 40.7%	45.7% 23.7%	1.00	0.11	4.00	0.00	0.02	0.23	45.2%	12% 12%	45.2%	0.8%	0.4%	11.1%	11.5% 12.7%
-		- 1	+	1 2	0.00	0.63	0.00	0.00	0.12	0.25		98%	100.0%	22%	1.1%	32.6%	41.75	1.00	0.12	0.00	0.00	0.04	0.29	26.7%	0.5%	26.7%	1.6%	1.1%	13.1%	13.7%
-		-		1	0.01	0.43	0.00	0.00	0.25	0.19		2.1%	100.0% 100.0%	0.7% 1.4%	62% 62%	57.8% 28.6%	41.7%	0.01	22.0	0.00 0.01	0.00	0.10	0.28	46.7%	1.6% 0.6%	43.9% 46.7%	0.5%	0.2% 0.2%	22.4%	19.2% 19.0%
9				2	0.01	0.54	0.01	0.00	0.20	0.24		1.9%	100.0%	2.4%	67%	36.9%	45.2%	0.01	0.19	0.01	0.00	0.06	0.28	34.9%	1.1%	24.9%	1.9%	0.6%	11.7%	15.2%
10		10	+	- 2	0.01	0.48	0.01	0.00	617	0.19	_	29% 17%	100.0%	12%	0.2%	41.4%	27.9% 47.2%	0.01	0.30	0.01	0.00	0.09	0.05	40.8%	18%	40.8% 59.8%	0.8%	0.8%	15.4% 19.5%	9.8%
11 12 12 14 15		- 11	-	- 2	0.01	0.53	0.61	0.00	019	0.25	=	15%	100.0%	15%	0.6%	26.0%	47.5%	0.01	0.20	0.01	0.00	0.06	0.10	28.0%	0.9%	28.0%	1.1%	0.6%	12.1%	18.1%
24		12	_	- 2	0.06	0.93	60.0	0.02	0.50	0.28	-	62%	100.0%	21%	16%	St.1% 54.2%	63.4% 41.5%	0.04	0.52	0.02	031	0.22	0.15	56.2%	15%	36.2% 56.2%	2.6%	1.6% 1.5%	13.5%	20.5% 16.2%
15		- 14		- 5	0.02	0.86	0.01	0.00	0.45	0.42		1.8%	100.0%	1.1%	62% 64%	0.6% 6.8%	e), e);	0.01	954	0.01	0.00	0.20	0.19	632%	1.2%	63.2%	0.6%	0.2%	23.2%	21.6%
16		16			0.01	1.35	0.04	0.00	0.50	2.74		67%	120.0%	22%	0.5%	27.4%	56.1%	2.01	0.60	2.04	0.21	9.22	0.34	44.5%	0.6%	44.5%	2.6%	0.6%	15.2%	25.6%
19		17		-	0.05	1,31	0.05	9.00	0.47	0.57		3.8%	100.0%	24%	2.1%	6.0	43.2% 51.9%	2.03	98	4.03	0.02	0.22	0.17	20.6%	24%	20.6% 62.2%	2.1%	18%	16.6%	12.7% 22.1%
20		19		'n	0.01	0.83	0.02	0.00	0.63	0.37		1,2%	100.0%	2.1%	0.4%	52.1%	44.5% C1.5%	2.01	0.54	0.01	0.00	0.19	0.17	64.9%	6.7% 6.6%	64.9%	1.1%	0.4%	22.4%	22.6%
21		129	+	- 1	0.01	0.24	60.0	0.00	0.49	0.65	_	0.8%	100.0% 100.0%	27% 17%	0.6%	20.6%	47.9%	0.01	0.61	4.00	0.00	0.22	0.22	49.4% 27.9%	0.6%	27.9%	13%	0.6%	10.8%	25.7%
22		129		1	4.00	0.36	0.61	0.00		0.52		0.8%	100.0%	27%	0.6%	28.7% 21.2%	45.7%	4.00	90.0	0.01	6.50	4.02	635	21.8%	0.8%	21.8%	1.9%	0.4%	9.2% 10.4%	17.8%
25		131	_	1	1.00	0.12	0.61	0.00	0.11	0.50		1.5%	100.0%	3.5%	12%		41.7%	0.00	0.12	0.01			0.23	20.2%	12%	25.2%	2.5%	12%	11.4%	12.4%
26		122	_	-	4.00	0.11	0.01	0.00	0.10	0.58		0.6%	100.0%	2.1%	62%	20.7% 27.4%	53.2% 24.2%	1.00	0.13	0.01	0.00	0.04	0.04	29.5%	0.2%	29.5%	1.8%	62% 62%	13.1%	17.9% 15.0%
28		124		2	4.00	0.59	0.01	0.00	0.17	0.34		0.5%	100.0%	2.0%	0.7%	29.6%	60.5%	4.00	0.36	0.01	0.00	0.07	0.12	46.6%	0.7%	66.6%	1.9%	0.2%	12.2%	22.2%
29		135	_		0.00	0.51	0.02	0.00	0.20	0.19		0.8% 1.2%	100.0% 100.0%	2.5%	0.4% 0.7%	20.0%	27.8% 24.0%	4.00	0.21	0.01	0.00	0.07	647	40.7%	0.6%	40.7% 27.2%	2.1%	0.4%	13.9%	13.7%
21		127		- 2	0.00	0.55	0.02		0.16	0.25		62% 12%	100.0%	2.7%	03%	21.0% 28.7% 43.1%	45.6%	1.00	0.22	0.01	031	0.06	0.11	41.5%	0.7% 0.4% 0.7%	41.5%	2.2% 1.2%	63% 62%	10.7%	19.8% 25.5%
21 22 23 24 24 25	K 1920	129		- 1	0.01	0.42	0.01	0.00	0.19	0.19	-	12h 62h	100.0% 100.0%	3.7%	0.5%	46.1% 32.7%	22.8%	1.00	0.21	0.01	0.00	0.06	0.11	24,2%	0.5%	24.2%	27%	0.5%	10.6%	23.5%
34		140	_	-	0.01	1.51	0.09	0.01	0.40	0.74		12%	100.0%	62% 2.1%	03%	20.0%	48.9% 54.2%	0.01	050	0.08	0.31	0.12	627	47.8%	0.6%	33.5% 47.8%	5.2% 1.4%	0.8%	8.2% 17.2%	18.1% 28.6%
36		142		-	0.01	111	0.65	0.00	0.38	0.27		0.6%	100.0%	0.5%	0.2%	34.6%	69.4%	0.01	0.60	0.00	0.00	0.18	0.39	53.9%	0.5%	\$3.9%	0.4%	0.2%	16.2%	25.1%
37		143	+	- 5	0.01	158	0.03		636	0.40	_	12%	100.0%	2.8%	05%	43.4%	47.5%	0.01	0.41	0.02	0.00	0.16	0.17	48.9% 20.6%	10%	49.9%	2.5% 4.4%	0.4%	18.9%	22.8% 15.2%
20		545		- 5	0.01	1.15	0.67	0.02	0.30	0.65		62%	100.0%	5.9%	14%	25.7%	56.5%	0.01	0.54	105	0.22	0.11	0.31	47.0%	0.6%	47.0%	42%	14%	16%	26.8%
41		146	_	1	0.01	1.12	0.01	0.00	0.45	0.76	_	0.6%	100.0%	0.4%	62% 62%	20.8%	67.6% 53.2%	0.01	0.66	0.00 0.01	0.00	0.22	0.29	59.7%	0.6%	58.7% 51.7%	0.4%	62% 62%	19.7%	24.7%
42		148		- 1	4.02	1.46	0.11	93.0	0.60			1.2%	150.0%	73%	0.6%	41.0% 23.2%	26.1%	0.01		0.09		0.24	621	49.6%	6.7% 6.5%	49.6%	5.2%	0.2% 1.0%	16.2%	14.6%
66		1	129	1	0.01	0.59	0.01		0.22	0.24		15%	120.0%	2.0%	0.5%	27.7%	42.2%	3.01	0.22	2.01	0.22	2.07	0.10	37.6%	125	27.9%	1.4%	0.5%	11.2%	16.9%
		- 2	120	1	0.01	0.68	0.01	0.00	0.30	0.25		0.9%	100.0%	1.5%	0.6%	40.2%	16.9%	0.00	15	0.01	0.00	1.09	0.10	46.7%	0.6%	41.2%	12%	0.6%	12.8%	14.1%
47		4	132	ž	0.01	0.74	0.01		0.32	0.39		1.2%	100.0%	1.9%	0.2%	6.6%	\$2.8%	0.01	0.30	0.01	0.00	0.14	0.13	41.4%	6.7%	41.4%	1.6%	63%	19.2%	18.1%
		- 5	122	4	0.01	135	9.04	0.02	0.41	0.52		0.8% 1.2%	100.0%	2.8%	15%	22.4% 45.7%	41.2% 60.0%	0.01	0.50	0.01 0.01	632	0.16	0.19	40.1% 52.1%	0.6%	40.1% 52.1%	2.2%	1.5%	12.9%	15.2%
50		7	125	4	0.01	1.03	60.0	0.61	0.41	0.66		0.8%	100.0%	2.8%	0.5%	26.2%	42.5%	0.01	0.42	0.02	0.21	0.16	0.19	41.8%	0.5%	41.8%	2.1%	65%	15.1%	18.6%
52		-	127	1	0.02	131	90.0	0.02	0.40	0.60		18%	100,0%	2.0%	12%	40.5%	41.8% 21.5%	2.02	0.41	1.02	031	0.16	023	34.0%	11%	24.0% 46.6%	1.7%	12%	12.9%	17.1%
52		10	128	4	0.01 0.01	0.94	0.02	0.01	0.22	0.52		12%	100.0%	1.8%	0.5%	40.0%	55.0% 27.7%	0.01 0.01	0.49	2.01	031	0.16	0.26	\$2,0% 43,9%	0.9% 0.6%	\$2.0% 40.9%	1.1% 2.4%	0.5%	16.6%	28.1% 14.2%
55		12	140	10	0.04	2.94	0.18	0.06	1.11	1.50		1.5%	100.0% 100.0%	6.1%	0.7% 2.2%	28.2% 27.8%	51.0%	203	1.02	0.15	0.26	2.16	0.65	34.8%	1.5%	24.8%	5.1%	1.9%	12.1%	22.0%
56 56		12	141	10	0.11	2.50	9.00	0.04	1.17	1.28	\vdash	43%	100.0%	2.9%	1.8%	46.9%	\$1.3% \$5.8%	4.07	141	4.05	034	0.54	0.69	56.3%	27%	56.3% 56.4%	1.8%	15%	21.4%	27.6%
59		15	143	10	0.02	2.16	0.06	0.01	1.24	0.99		0.8%	100.0%	2.0%	0.5%	52.5%	41.8%	0.01	1.26	4.03	0.21	0.59	0.47	53.5%	0.6%	53.5%	1.4%	0.4%	25.0%	19.8%
60		12	166	10	0.02	2.08	0.18	9.00	1.19	1.59	_	0.8%	100.0%	5.8%	25%	3.04	\$1.7% 45.0%	0.02	1.35	0.14	033	0.49	0.78	40.7%	67% 15%	44.0%	4.5%	24%	15.8%	25.2%
61		19	166	10	203	2.75	0.02	0.01	125	181		12%	100.0%	0.6%	62%	6.6%	65.8%	102	1.76	0.01	0.21	0.54	031	63.9%	0.8%	63.9%	0.4%	0.2%	19.6%	22.9%
63		20	147	10	0.02	2.10	0.03	0.01	132	1.60	-	10%	100.0%	1.2% 5.4%	02%	47.0%	\$1.4% 48.7%	4.02	1.32	0.02	031	0.60	0.60	55.2% 52.4%	0.7% 0.5%	50.3% 52.4%	0.9% 4.1%	0.2% 0.2%	22.2% 18.2%	25.7%

														max ratio ou	t of all beams												max ratio out of all t	eams		
П							-	don2 POynte	(cn2)			66%	100.0%	66%	25%	\$3.0%	64.0%		60n2 PD)	nW(ox2) at 1	Ones evaluated	n distance		66.0%	47%	66.0%	5.2%	2.4%	26.2%	22.5%
No. M	idule Typ	e Beam ID	5 Berra 10,2	Feed no.	Sepligan	Skipario	SS(Top)	Séjkomo	m) StiFran	52(Read)	per Beam Back-off	ratio (Right 2mm)/(worst- ourface 2mm)	ratio (Left 2mm)/(wonz- curface 2mm)	ratio (Sop Jennij/jeons- surface Jenni)	ratio (Bottom Jmm)/worst- surface Jmm)	ratio (Forst 2mm)/(worst- surface 2mm)	(Rear Jimm) (Nearch surface Jimm)	Skillight	Siture	SS(Top)	Sé(Bottom)	\$1(Fram)	S2(Rear)	ratio worst-surface (15mm/(2mm)	ratio (Right 15mm),/(worst- surface 2mm)	ratio (Left 10mm)/(ecro- surface 2mm)	ratio (Top 12mm)/(worst- surface 2mm)	ratio (Rottom 15mm),/(worst- surface 2mm)	ratio (Figet 10mm)/(worst- ourface 2mm)	ratio (Rear 10mm)/(worst- ourface 2mm)
1			_	1	1.00	0.11	0.00	0.00	0.12	0.17		6.2% 6.6%	100.0%	1.2%	6.2%	27.7% 40.1%	55.4% 44.9%	4.00	0.12	4.00	0.00	0.04	0.27	42.6% 50.6%	0.2%	42.6% 50.6%	1.0%	6.2%	12.1%	22.0% 15.1%
à		2		-	0.01	0.22	0.00	0.00	0.12	0.15		1.5%	100.0%	12%	6.7%	28.1%	45.5%	4.00	0.15	4.00	6:33	0.04	034	45.5%	12%	45.5%	0.9%	0.2%	10.8%	13.2%
4		- 4	+	1	0.01	0.31	0.00	0.00	0.12	0.15	+	22% 12%	100.0%	0.7%	0.2%	29.0% 40.2%	51.7% 28.8%	1.00	0.16	1.00	0.00	0.04	0.25	50.8% 50.1%	1.2%	50.8% 50.1%	0.7%	0.2%	12.1%	16.1%
6		- 5		- 2	4.00	0.63	0.01		622			0.6% 2.5%	100.0%	1.6%	0.8%	31.9% 51.9%	\$2.1% \$2.2%	0.00	0.25	4.01	0.21	0.09	0.09	29.8%	0.5%	29.8%	0.9%	0.8% 0.2%	14.7%	14.4% 21.9%
· i		7		2	1.00	0.62	0.01	0.00	0.24	0.34		0.5%	100.0%	1.0%	0.2%	29.1%	54.7%	1.00	0.21	0.01	0.00	0.10	0.17	49.8%	625	49.8%	0.8%	0.2%	15.6%	26.5%
9		-	_		0.01	0.69	0.01	0.00	622	0.22	-	1.2% 2.2%	100.0%	1.5%	0.6%	22.4%	45.8% 28.7%	0.01	0.36	10.0	0.00	0.09	0.13	42.9%	14%	28.1% 42.9%	1.2%	0.4% 0.6%	11.0%	18.9% 12.2%
11		10		- 2	0.01	0.59	0.00	0.00	0.2k	0.30		12%	100.0%	0.5%	0.2%	47.9% 32.4%	\$1.4% 46.9%	1.00	0.16	4.00	0.00	0.11	0.14	60.5% 42.2%	6.7% 1.7%	60.5%	0.2%	62% 62%	19.2%	23.2%
13		12	+	- 6	0.02	1.28	0.05	0.02	0.45	0.71	+	1.6%	100.0%	35%	13%		55.6%	0.01	0.48	0.01 0.02	0:31	0.18	0.29	37.8%	1.1%	27.8%	2.6%	1.1%	14.3%	22.8%
54		12	_	5	0.07	1.03	0.03	0.01	0.55	0.56		66%	100.0%	25%	1.2%	\$3.6% #6.7%	\$4.7% \$1.3%	0.05	55	0.02	021	0.24	622	60.2%	42%	60.2% 63.8%	1.7%	12%	22.9%	21.0%
16		15		-	0.01	162	0.65	0.00	625	4.25		0.6%	100.0%	0.4%	62%	46.1%	46.2%	0.01	0.96	0.01	0.00	0.32	0.37	59.1%	0.6%	59.1%	0.2%	02%	19.7%	22.5%
17		12	+	1	0.01	1.44	0.04	0.01	0.47	0.93	+	0.2%	100.0%	2.6%	0.2%	22.4%	\$2.7% 42.1%	0.01	0.67	4.02	6.00	0.22	0.41	49.1%	0.4%	46.1%	2.4%	18%	15.0%	28 2% 15 0%
19		19		-	4.02	1,30	0.61	0.00	0.64	0.69		2.1%	100.0%	0.5%	62%	6.7%	\$2.0% 46.6%	1.02	0.83	4.00	0.00	0.27	629	63.7%	1.5%	63.7%	0.2%	62%	20.8%	22.76
21		20	_	-	0.01	1,59	60.0	0.00	0.55	2.87	_	0.6%	100.0%	1.6%	0.7%	34.7%	54.9%	0.01	0.80	2.02	0.00	0.24	0.47	50.6%	0.7%	50.6%	12%	0.1%	15.1%	23.5%
22		129		-	1.00	0.78	0.00	0.00	0.10	0.11		15%	100.0%	2.8%	0.5%	34.2%	27.1% 41.4%	100	110	10.0	0.00	0.04	023	29.6%	0.7%	29.6%	25%	0.7% 0.4%	13.8%	11.6% 18.6%
24		130		-	1.00	0.29	0.01	0.00	012	0.09		12%	120.0%	1.7%	0.7%	427%	23.4%	0.00	0.11	0.00	0.00	0.04	0.23	28.6%	0.7%	28.6%	1.0%	0.7%	14.3%	2.9%
25		131		1	1.00		0.00	0.00	0.11	0.16	+	12%	100.0%	12%	0.8%	40.9% 6.2%	64.0% 43.1%	1.00	0.11	0.00	0.00	0.05	0.04	42.5%	0.8%	42.5%	1.7%	0.8%	18.2%	17.0% 15.8%
27		122	_	- 2	0.01	0.56	0.01	13.0	620	0.19		1.1%	100.0%	1.6%	1.2%	26.1% 28.1%	34.2% 55.5%	4.00	0.18	0.01	0.21	0.06	0.04	22.4%	0.7%	22.4%	1.2%	1.5%	11.5%	11.8% 21.6%
29		135		2	0.01	0.55	0.01	0.00	0.25	0.29		1.1%	100.0%	1.5%	0.6%	6.8%	52.7%	0.00	0.27	0.01	0.00	0.11	0.29	ekelli	0.5%	49.4%	1.1%	0.2%	19.7%	17.0%
30		127		2	0.01	0.58	0.02	0.01	0.17		+	0.9% 1.2%	100.0%	24% 12%	0.9% 1.6%	29.1%	28.2% 26.1%	1.00	0.11	0.02	0:00 0:01	4.07	0.29	34.3%	0.5%	36.3% 36.0%	2.6%	67% 12%	14.5%	15.8%
22	K Patr	h 128	-	- 2	0.01	0.47	0.01	0.00	6.25 6.24		_	1.2%	100.0%	1.5%	6.2%	\$2.2%	59.0% 42.2%	4.00	0.35	0.01	633	0.12	0.10	52.2%	0.8%	52.2%	1.1%	62%	26.3% 16.2%	22.4%
24		140		- 1	0.02	1,21	90.0		0.41	0.53	_	1.6%	100.0%	6.6%	12%	32.2%	41.5%	0.01	0.49	2.07	0.31	0.12	0.22	28.5%	0.8%	28.5%	5.2%	12%	9.7%	17.1%
25		141			0.01	1.05	9.02	13.0	0.40	0.64		13%	100.0%	1.8%	15%	47.2%	61.4% 51.6%	0.01	50	500	621	0.17	0.29	60.5% 53.1%	12%	60.5% 53.1%	1.5%	15%	16-4% 23.5%	27.6%
47		143		- 1	4.01	1.05	60.0	0.00	0.51	0.54		1.2%	120.0%	2.8%	0.2%	49.0%	\$1.9% 41.5%	0.01	0.62	4.02	0.00	0.22	627	59.9% 43.2%	0.8%	58.9% 43.2%	2.2% 5.2%	0.2% 0.2%	22.2% 12.2%	22.7% 26.0% 15.0%
29		145	+		0.01	125	0.04	9.08	0.42	0.62	+	0.2%	100.0%	24%	2.1%	22.9%	48.9%	0.01	0.68	0.02	032	0.16	0.29	56.4%	0.5%	54.4%	18%	18%	12.6%	23.1%
41		146	_	5	0.01	1.13	0.62	0.00	653	0.54	_	10%	100.0%	2.0%	0.2%	47.2% \$2.1%	47.9%	0.01	95.0	0.01	6.00	0.28	624	49.6% C4.3%	0.7% 0.6%	49.6% C4.3%	12%	02%	24.9%	21.3% 19.2%
42		149		- 2	4.02	129	0.02	0.01	0.59	0.61		16%	100.0%	5.5%	0.6%	6.7%	47.2%	4.01	0.75	2.05	0:00	0.22	025	57.8%	0.8%	\$7.8%	41%	0.2%	18.1%	19.1%
- 66		- 0	129		0.01	0.66	0.02	0.01	0.24	1.25	+	12% 12%	100.0%	23%	0.8% 0.7%	20.7% 40.5%	0.2% 47.8%	0.01 0.01	0.12	0.01	0.01	1.09	0.12	46.0% 53.6%	0.8%	66.0% 53.6%	1.8%	0.8%	12.2%	18.5%
45			130	7	0.01	0.66	0.61	0.01	629	128	_	1.6%	100.0%	1.8%	0.8%	625	41.5% C7.0%	0.01	0.78	0.01	631	1.09	0.29	41.8%	0.9%	41.8%	12%	0.8%	12.4%	14.0%
47		-	122	1	2.01	0.82	0.01	0.00	0.31	2.26		1.2%	100.0%	17%	62%	27.6%	44.0%	2.01	0.19	0.01	0.22	0.12	0.12	47.2%	62%	47.2%	1.6%	62%	14.1%	15.0%
48		- 1	122	,	0.01	1.18	60.0	0.02	0.44	0.54		12% 14%	100.0%	2.1%	1.9%	27.6% 44.8%	45.2% 56.2%	0.01	950	50.0	632	4.17	0.18	47,2%	12%	47.2% 56.1%	1.6%	1.6%	14.7%	15.5% 22.8%
50		7	135	4	0.01	1.13	0.00	0.00	0.56	0.59		1.1%	100.0%	1.9%	0.6%	49.4%	52.4%	0.01	0.56	4.02	0:30	0.22	0.24	49.5%	0.6%	49.9%	1.6%	0.2%	19.8%	23.4%
52		- 8	127	1	4.02	1.39	9.04	93.0	0.40	0.63	-	1.6%	100.0%	1.5%	1.5%	30.9% 46.7%	41.6% 36.9%	0.01 0.02	0.62	4.03	0.01	0.12 0.22	0.19 0.19	40,2%	1.7%	40.2% 46.4%	2.4%	12%	10.4% 16.2%	21.5% 14.1%
5.0		10	138	4	4.02	1.16	62.0	0.00	0.60	0.59	=	1.6% 1.6%	100.0%	1.4%	0.2%	\$1.4% 34.4%	\$2.2% \$1.2%	0.01	0.66	4.01	633	4.26	625	56.6% 49.9%	12%	56.6% 49.9%	0.8%	62%	22.3% 13.2%	21.6%
55		12	140	10	1.06	2.18	0.18	0.06	120	1.65		12%	100.0%	5.6%	18%	27.7%	\$1.9%	0.04	1.31	0.15	0.0%	0.64	0.73	41.2%	12%	41.2%	4.6%	16%	13.9%	22.8%
56		12	141	10	1.09	2.85	93.0	0.04	1.27	1.69	+ =	15%	100.0%	1.6%	1.6%	47.9%	58.7% 55.4%	4.07	1.87	403	034 931	0.61	6.7%	65.6% 57.4%	2.2% 1.7%	65.6% 57.4%	1.0%	12%	21.5%	26.65
58		15	143	10	0.02	2.13	0.06	0.01	1.26	1.21		0.8%	120.0%	1.8%	0.4%	43.5% 86.6%	\$4.6% \$5.9%	402	1.84	0.05	0.21	0.63	0.84	59.8% 49.2%	0.5%	58.8% 49.2%	1.4%	0.2% 6.2%	20.1%	27.3% 28.2%
60		17	145	10	0.09	134	0.11	0.09	1.02	1.45		23%	100.0%	32%	2.5%	41.8%	43.5%	106	1.72	0.06	032	0.52	0.68	51.7%	18%	51.7%	1.9%	2.4%	16.2%	22.4%
61		19	146	10	4.07	2.72	0.04	0.01	1.26	1.43	+ =	2.4% 12%	100.0%	1.6%	0.2% 0.2%	49.5%	50.6% 50.6%	4.05	1.62	0.02 0.04	031 031	0.66	0.62	59.5% 59.3%	12% 02%	59.5% 59.3%	12%	0.2% 0.2%	24.4%	22.8%
63		20	148	10	4.03	2.16	0.16	0.01	130	2.02		10%	100.0%	47%	0.3%	26.7%	60.2%	0.02	1.94	0.12	0.31	0.57	1.09	57.8%	0.2%	57.8%	25%	02%	17.0%	22.5%

														max ratio eu	of all beams			ı —						I			max ratio out of all b	eams		$\overline{}$
П	$\neg \Gamma$	-		П			4	on2 POsnikyo	ona))			10.7%	100.0%	72%	25%	64.3%	72.7%		6on2 PD;	nM(on2) at	tūnin evaluat	on distance		63.8%	7.7%	an	5.6%	22%	25.6%	34.0%
No. 1	odule Type	Beam IC	5,5 Sema10,2	Feed no.	Sepligito	Skipario	SS(Top)	Séléotori	\$1(Frant)	52(Read)	Beam Rack-off	ratio (Right 2mm)/(worst- outsce 2mm)	ratio (Left 2mm)/(wonz- curface 2mm)	ratio (Top 2mm)/(word- surface 2mm)	ratio (Ration Zmm)/(worst- surface Zmm)	ratio (Forst 2mm)/(worst- surface 2mm)	(Rear Zimm) (Nearch surface Zimm)	Strilights	Siste	SS(Sop)	Si(Bottom)	\$1(Frant)	S2(Rear)	stio wortz-surface (15mm/2mm)	ratio (Right 15mm),r(word- surface 2mm)	ratio (Left 10mm)/(worth- surface 2mm)	ratio (Top 10mm)/(worz- surface 2mm)	ratio (Rottom 10mm),/(worst- surface 2mm)	ratio (Fiore 10mm()/(word- ourface 2mm)	ratio (Rear 10mm)/(word- ourface 2mm)
1		0		- 1	4.00	0.30	0.00	0.00		0.19		67% 27%	100.0%	1.2%	0.2%	43.4%	59.6% 54.1%	4.00	0.15	4.00	6.00	0.04	025	50.7%	0.7% 1.9%	50.7% 42.0%	1.0%	0.2% 0.4%	13.6%	17.5% 23.7%
à		2		1	0.01	0.27	0.00	0.00	0.10	0.15		2.2% 2.6%	100.0%	1.5%	0.6%	27.4%	\$3.5% \$3.6%	1.00	0.12	4.00	6:30	0.04	025	45.4% 53.6%	1.5%	45.4% 53.6%	0.7%	0.6%	13.2%	18.2%
-		4		1	0.01	0.24	0.00	0.00	0.14	0.14		2.1%	100.0%	1.4%	0.4%	49.1%	42.7%	4.00	0.12	1.00	0.00	0.01	025	43.5%	1.6%	43.5%	1.1%	0.4%	16.5%	16.1%
- 6		1	_	2	0.01	0.55	0.01	0.00	0.22	0.22	+	24% 22%	100.0%	2.0%	0.6%	40.0% \$7.9%	62.0% 52.9%	0.01 0.01	0.22	0.01	0.00	0.09	0.11	41.8%	12% 22%	41.8%	0.9%	0.6%	15.4%	19.4% 22.0%
-		7	_	- 2	0.01	0.57	0.01	0.00	622	0.32	-	12%	100.0%	1.7%	62% 62%	27.5%	55.4% 43.0%	0.00 0.01	0.37	0.01	6.00	1.09	0.15	66.8%	2.2%	6.1%	1.4%	0.2% 0.5%	14.0%	26.7% 21.6%
10		9		- 1	0.03	0.49	0.02	0.00	622	0.24		\$1% 18%	100.0%	3.5% 1.6%	0.8% 0.2%	62%	48.5% 52.8%	0.02 0.01	0.17	4.01	0.00	0.07	0.29	33.6% 59.4%	15% 12%	23.6% 59.4%	1.8%	0.8% 0.2%	14.9%	18.1% 24.1%
12		11		- 2	0.01	0.60	0.01	0.00	0.17	0.26	+	2.6%	100.0%	1.6%	0.4%	22.7%	52.9%	0.01	0.23	0.00	0.00	4.05	0.11	45.7%	1.8%	45.7%	1.0%	0.6%	10.8%	22.2%
12		12		- 5	0.04	1.11	60.0	93.0	0.29	0.59		12%	100.0%	2.9%	12%	62%	\$2.9%	0.02	0.27	4.02	0.21	0.17	0.28	22.9% C0.4%	22%	22.9% GLAN	1.7%	1.1%	15.7%	25.0%
15		- 19		- 3	102	126	0.61	0.00	0.55	0.72		12%	100.0%	0.9%	0.1%	49.5%	\$7.2% C.2.10	202	0.71	2.01	0.00	0.22	630	56.1% 56.4%	125	56.1% 56.4%	0.7%	0.7%	17.6%	24.5%
17		16			0.01	129	0.05	0.00	0.36	0.69		0.2%	100.0%	23%	0.6%		\$1.1% \$5.9%	0.01	0.72	4.01	0.00	0.16	0.40	41.9%	0.5%	41.9%	1.8%	0.4%	13.1%	32.0%
19		17	_	- 5	0.09	0.97	0.66	0.02	0.47	0.51	_	825 125	100.0%	62%	19%	60.2%	Q 9% Q 2%	2.05	0.42	0.03	0.02	0.16	021	eželi. Comi.	25%	43.4% C4.6%	24%	18%	18.8% 00.0%	21.4%
20		19		- 3	4.02	128	0.61	0.00	0.61	2.64		12%	100.0%	1.0%	6.2%	47% 28.7%	52.4%	0.01	0.77	0.01	6:30	0.27	628	60.4%	0.8%	60.4%	0.8%	0.2%	21.2% 12.2%	21.9% 24.0%
22		128	_	1	1.00	0.11	0.04	0.00	0.28	0.76	_	10%	100.0%	2.6%	0.2% 0.7%	20.8%	56.9% 44.6%	0.01	0.12	0.00	0:20	0.16	0.65	41.7%	0.7%	41.7%	2.0%	0.2% 0.2%	15.6%	11.7%
24		129		1	1.00	0.27	0.00	0.00	0.10	0.12	-	0.7% 0.8%	120.0%	1.6%	0.7% 0.8%	34.8% 36.2%	47.8%	1.00	0.11	1.00	0.00	0.04	034	40.7%	0.6%	40.7%	1.5%	0.4%	16.4%	13.2% 12.2%
25		131	_	1	1.00	0.23	0.00	0.00	637	0.17		12%	100.0%	1.7%	0.2%	29.0%	72.7% 34.9%	1.00	0.10	4.00	6.50	4.03	034	42.0% A1.0%	0.9%	42.0% 40.5%	13%	0.2%	12.6%	18.0%
27		122		- 2	0.00	0.52	0.01	92.0	0.15	0.26		1.7%	100.0%	23%	12%	29.0%	\$1.0%	2.01	0.18	0.01	0.21	0.05	0.28	35.1%	12%	26.1%	1.9%	12%	175	14.7%
29		134		2	0.01	0.51	0.01	0.00	0.17	0.29	+	1.6%	120.0%	13%	0.8% 0.2%	22.5% 26.7%	\$2.5% \$8.2%	0.01 0.00	0.35	0.01	0.00	1.09	0.10	49.0%	1.0% 0.8%	49.0% 50.5%	1.0%	0.8% 0.2%	17.6%	19.8% 22.1%
20		122		2	0.01	0.67	0.02	0.01	0.17	0.29		67% 18%	100.0%	2.1%	67% 12%	2.00	42.8%	0.00 0.01	0.23	4.02	6.00	1.06	0.29	22.5%	0.6% 1.2%	22.5%	2.4%	125	10.6%	13.6%
22	K Patri	138		- 1	0.01	0.45	0.00	0.00	0.19	0.31		1.1%	100.0%	0.9%	0.4%	41.8%	72.6%	0.00	0.36	4.00	0.00	0.09	0.13	59.7%	0.7%	58.7%	0.4%	0.2%	20.4%	28.5%
24		139		- 6	0.02	1.12	0.07	93.0	0.36	0.30	+	12% 12%	120.0%	2.3% 6.5%	0.8% 1.5%	21.5%	60.5% 50.9%	0.00 0.01	0.49	0.01	0:33 0:31	0.12	0.28 0.21	42.2%	0.8% 1.0%	42.2%	1.8%	12%	13.6%	16.4%
25		141		-	0.02	0.97	60.0	0.02	0.25	2.60		16%	100.0%	2.8%	25%	82% 46.8%	62.1%	2.01	0.53	4.02	0.02	0.14	0.24	54.4%	1.5%	54.4%	2.2%	22% 02%	14.0%	22.8%
27		543		- 5	4.02	1.12	0.02	0.00	0.59	0.65	-	12%	100.0%	1.4%	0.2%	\$3.0% 33.5%	58.4% 45.9%	0.01	0.64	0.01	6.00	0.29	0.29	\$7.3% 29.7%	0.9%	\$7.2% 36.7%	1.0%	0.2%	25.6%	25.9%
29		545		- 1	4.01	131	0.03	0.09	0.40	0.57		0.8%	100.0%	24%	2.1%	20.7%	43.9%	0.01	0.52	4.02	0.23	0.12	0.20	29.8%	0.5%	29.8%	1.8%	18%	3.1%	15.1%
41		146		- 5	0.02	1.00	0.03	0.00	0.44	2.63	+	12%	100.0%	26%	0.2%	40.8%	58.7% 59.4%	0.01	0.62	0.02	0.00	8.20	0.29	57.3% 59.0%	0.9%	57.2% GENN.	1.5%	0.2%	18.6% 23.6%	25.7%
42		149	476	- 1	0.01	1,22	0.09	0.00	0.43	2.64	-	175	100.0%	6.6%	62%	X 0% 42.8%	52.3%	0.01	0.53	0.06	0.00	0.15	023	43.9%	0.2%	43.9%	5.3%	0.2%	12.2%	18.7%
44		1	129	2	0.01	0.59	0.01	0.00	0.24	0.31		15%	100.0%	15%	0.2%	40.0%	928	0.01	0.27	0.01	0.00	0.11	0.54	45.2%	125	6.2%	1.0%	02%	18.1%	23.2%
		- 1	120	- 1	0.01 0.01	0.63	0.01	0.00	0.24	0.32	_	2.4%	100.0%	1.1%	0.8%		\$2.1% \$1.4%	0.01 0.01	0.22	0.01	0:21 0:20	0.10	0.12	41.8%	15%	48.8%	0.9%	0.5%	15.8%	18.5% 24.2%
47		1	132	- 2	4.01	0.76	0.02	0.00	0.22	0.30	=	1.65 2.85	100.0%	2.1%	0.6%	0.6% 0.2%	23.9%	2.01	0.13	4.01	633	0.10	631	42.6%	0.9%	42.8%	1.7%	125	12.8%	12.8% 22.2%
49			124	1	0.03	1.09	0.02	0.01	0.49	0.61		2.4%	100.0%	14%	0.6%	6.65	\$7.0%	1.02	0.63	0.01	621	0.17	621	59.2%	12%	58.2%	0.9%	0.5%	16.2%	13.9%
51		- 7	135	1	4.02	1.03	62.0	0.00	0.44	0.63	-	19% 22%	100.0%	2.0%	0.2%	49.1% 20.2%	65.6%	0.01	0.48	0.01 0.03	631	0.19	0.27	29.1%	1.2%	46.6% 29.1%	1.6%	0.2%	18.1%	26.7% 20.2%
52		10	127	4	4.05	1,24	0.03	9.02	0.50	0.49	+	12% 18%	120.0%	23%	12%	40.5% 47.1%	23.2%	0.03 0.01	0.46	0.01 0.01	631 631	0.21	0.20	27.1% 54.6%	2.4%	27.1% 54.6%	1.1%	1.5% 0.5%	16.9%	16.4% 23.6%
54		11	139	4	1.02	1,31	0.02	0.01	0.36	0.78	-	1.5%	100.0%	1.7%	0.6%	27.5%	59.6% 59.6%	0.01 0.04	0.69	1.02	6.01	0.12	0.22	\$2,3% 42,4%	1.0%	\$3.3% 42.4%	1,2%	0.5% 1.2%	9.2% 14.4%	25.1%
56		12	141	10	0.14	2.31	0.09	0.06	1.18	1.53		6.1%	100.0%	3.7%	2.2%	69.2%	66.5%	0.10	1.45	0.05	0.25	2.49	0.58	62.7%	4.2%	62.7%	2.1%	22%	21.2%	25.0%
57		14	142	10	0.04	2.44	90.04	0.01	124	1.52	+ =	15%	100.0%	1.8%	02% 02%	50.8% 45.0%	62.5% 52.3%	403	1.48	4.02	0.01	0.56	0.71	60.8% 59.5%	10%	60.8% 59.5%	1.1% 0.7%	0.2% 0.2%	22.6% 20.8%	21.25
59		16	144	10	0.04	2.17	0.16	0.61	1.17	1.79		1.1%	100.0%	5.2% 2.6%	0.6% 2.4%	32.9% 82.5%	54.5% 45.7%	4.02	1.59	0.12	0.21	0.41	0.95	\$0.0% 47.6%	0.7% 2.1%	50.0% 47.6%	3.8%	0.2% 2.2%	12.6%	29.8% 17.9%
61		17	146	10	0.09	231	0.05	93.0	1.19	1.49		3.2%	100.0%	2.0%	0.7%	49.7%	55.0%	1.06	1.58	4.03	0.21	4.65	0.61	59.2%	2.2%	58.3%	1.1%	0.3%	24.0%	22.6%
62		20	147	10	0.02	3.04	0.04	0.01	1.30	1.52	+	1.1%	100.0%	1.6%	0.2%	40.5% 20.7%	60.6%	4.02	1.61	0.02	0.21	0.60	0.76	\$1.9% \$8.6%	0.7%	61.6% 58.6%	1.1%	0.2%	23.0%	28.8%

[Folder Closed Status]

- K-patch Low CH



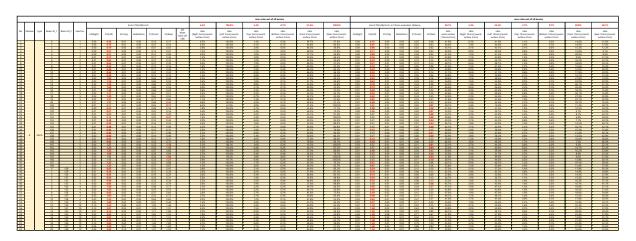
														max ratio ou	t of all bears									i –			max ratio out of all b	nams		$\overline{}$
П		Т						dow2 PD(wW/s	m2)			2.9%	100.0%	19.1%	7.6%	62.7%	25.9%		4cm2 PD	(Circipani)	Smm evaluati	on distance		85.5%	2.5%	85.0%	17.5%	69%	466%	21.1%
No.	Andule Typ	ie liear	on ID_1 Sens ID_2	Feed no.	S4(Kight)	Slipato	SS(Top)	Siciloton	S1(Frant)	S2(Reat)	per Beam Back-off (db)	ratio (Kight 2mm)/(wonz- outlace 2mm)	ratio (Left 2mm)/(worst- curface 2mm)	ratio (Top 2mm)/(worst- ourface 2mm)	ratio (Rotton Jimm)/(worst- surface Jimm)	ratio (Forst Jimm)/(worst- surface Jimm)	ratio (Rear Zmm)/(worst- surface Zmm)	S4(Right)	Skijueltij	SS(Top)	Sé(katan)	St(Frant)	SI(Next)	ratio worz-surface (Serre/Zenn)	ratio (Right Smm),(worst- outsce 2mm)	ratio (Left Smm)/(scorp- ourface 2mm)	ratio (Top Smm)/(worst- curface 2mm)	ratio (Acesans Sminit/)worle- ourface 2mm)	ratio (Frant Smis)/(worz- ourface Zmin)	ratio (Rear Sminity/worst- surface 2 min)
1 2			0	1	1.00	0.31	0.01	0.61	0.17	0.04		1.0%	100.0% 100.0%	2.6%	1.6%	56.1% 46.6%	11.9%	0.00	0.22	0.01	4.00	0.12	4.03	69.7% 76.5%	0.6%	69.7% 76.5%	2.2%	1.2%	27.1%	9.2% 50.1%
2		=	į.	- 1	4.00	0.22	0.01	0.00	0.15	0.04		1.2%	100.0% 100.0%	15%	0.9%	44.8% 50.0%	112%	0.00	0.24	0.01	4.00	90.0 90.0	4.03	72.7% 77.7%	0.9%	22.7% 22.7%	2.0% 2.5%	1.9%	26.1% 20.2%	8.5% 10.0%
S					0.01	0.18	4.02	0.00	0.16	0.04		1.6%	100.0%	5.0%	0.8%	28.5%	164%	0.00	0.20	0.02	4.00	0.09	0.04	28.2%	1.0%	28.2%	42%	45%	23.2%	10.5%
6		-	2	- 2	0.00	0.64	0.03	0.00	0.22	0.09		0.6%	100.0%	44%	2.0%	\$1.0% \$1.3%	54.0%	0.00	0.44	0.09	2.01	0.19	0.07	69.3% 95.5%	0.5%	69.2%	19%	17%	28.9%	10.8%
8			7	- 1	0.01	969	4.02	0.65	0.24	0.13		0.9%	100.0%	30%	1.1%	02.0% 44.5%	15.1%	0.00	146	0.02	0.01	0.25	4.07	72.2%	0.6%	22.2% 64.6%	2.5% 4.6%	19%	28.1%	11.7%
10				-	2.01	0.63	203	020	122	92.0		17%	100.0%	47%	1.6%	28.6%	13.9%	92.0	6.6	0.03	0.01	0.13	2.07	71.5%	1.1%	715%	4.2%	13%	13.9%	10.4%
11			10	- 2	0.01	0.60	0.01	0.00	0.20	0.12	-	1.2%	100.0% 100.0%	125	0.5% 1.2%	50.0% 46.2%	20.5% 12.2%	0.01	0.48	0.01	0.00	0.21	1.09	80,2% 69,0%	1.0%	92.2% 93.0%	105	12%	25.2%	15.7%
12			12	-	4.02	1.31	0.17	93.0	0.72 A C6	0.19		1,2%	100.0%	13.2%	4.4%	\$4.5% \$6.1%	54.2% 35.6%	0.01	***	0.15	0.05	0.46	0.15	67.4%	0.8%	62.4%	11,7%	18%	35.2% 35.2%	11.7%
15			14		0.03	1.54	0.02	0.00	0.77	0.16		2.2%	100.0%	1.1%	0.5%	50.1%	22.4%	9.08	1,29	0.01	0.01	0.51	0.20	83.0%	1.6%	82.0%	1.9%	0.4%	23.2%	19.4%
17			16	-	0.01	1.45	0.05	0.04	0.75	0.22		0.8%	100.0% 100.0%	3.1% 14.0%	0.4% 2.9%	45.1% 56.8%	20.2%	93.0	1.09	0.18	0.01	0.62	0.17	82.1% 72.1%	0.6%	92.1% 72.1%	12.0%	24%	22.5% 42.4%	11.9%
19		=	17	-	0.03	1.19	0.17	20.0	0.55	0,22		2.2%	100.0% 100.0%	14.2% 2.0%	2.8%	56.8% 46.0% 50.9% 46.5%	18.9%	0.02	1112	0.16	0.04	0.32	0.19	84.7%	1.6%	69.7% 84.7%	12.7% 1.7%	12%	25.4% 22.9%	15.6% 19.5% 20.1%
20			19 20	-	0.01 0.01	1.43	0.03	0.01	0.65	0.34		1.0%	100.0% 100.0% 100.0%	2.0% 11.7%	0.5% 0.7% 1.8%	6.5%	23.9%	0.01 10.0	1,22	0.09	4.01	0.46	4.29	\$4.8% 75.3%	0.9%	5185	1.7%	175	21.2%	20.1% 12.7%
22			128	,	0.00	0.29	0.01	0.00	0.11	0.04		1.4%	100.0%	3.8%	2.1%	27.2%	13.0%	0.00	0.19	93.0	0.01	0.06	4.02	63.7%	0.7%	63.7%	2.4%	2.7%	22.5%	10.6%
24			129	- 1	0.01	0.15	0.01	0.00	0.12	0.02		2.0%	100.0% 100.0%	475	1.6%	48.6% 32.6%	13.3%	0.00	0.18	0.01	4.00	90.0	0.02	72.1% 66.1%	1.6%	22.1% 66.1%	4.0%	1.0%	31.3% 11.6%	6.8% 10.0%
25			121	-	0.01	0.36	0.02	0.00	0.16	90.0		276	100.0% 100.0%	195	12%	62.7% 66.2%	19.5%	10.0	0.17	0.02	0.00	0.09	0.04	66.6%	1.9%	66.9%	42% 10%	12%	25.2% 23.1%	14.6% E2%
27		-	133	- 2	0.01	0.56	0.06	0.01	0.20	0.05		2.1%	100.0%	10.0%	2.0%	25.6%	9.1%	0.01	0.34	0.05	0.01	0.12	0.04	59.8% 69.7%	1.6%	58.9% 68.7%	9.1%	18%	25.6%	72%
29		-	134	2	0.01 0.01	0.66	4.03	0.00	0.27	0.11		2.0%	100.0% 100.0%	48%	1.6%	56.2% 55.0%	56.0% 20.0%	0.01	9.66	0.02	0.01 0.01	0.19	1.09	67.7%	1.6%	62.7%	4.2%	12%	36.4%	16.2%
35		-	136	- 2	0.01	0.61	2.03	0.60	0.24	0.04		1.2%	100.0%	10.6%	2.8%	20.0% 26.2%	7.2%	10.0	0.22	0.09	0.02	0.17	0.04	61.0%	0.8%	61.0%	1.9%	11%	22.4% 20.0%	52% 10.5%
32	K Fan	a 🗔	123	7	0.01	0.51	0.01	0.01	129	0.13		22%	100.0%	2.2%	1.0%	97.9% 46.7%	25.9%	0.61	9.86	0.61	1.00	0.18	9.11	21.3%	1.6%	71.2% 63.6%	2.0% 5.5%	1.6%	25.8% 27.6%	21.1%
24			142	1	403	1.31	0.17	0.12	453	0.12		2.4%	100.0% 100.0%	13.0%	74%	40.1%	7.7% 15.2%	0.02	0.82	0.15	1.09	0.35	1.09	62.2%	17%	622%	11.6%	685 175	26.65	5.9%
25			142	- 3	0.02	1,10	2.03	0.00	2.62	0.32		15%	100.0%	27%	1.1%	0.2% 90.6%	24.0%	0.02	0.91	0.02	0.02	0.45	0.14	78.8%	1.0%	72.5%	2.1%	1.0%	36.4%	12.6% 20.4%
27			162	-	4.02	1.07	0.0%	0.03	4.57	0.14		2.1%	100.0% 100.0%	4.6% 14.6%	2.9% 7.6%	52.4% 41.9%	21.1%	0.02	0.82	9.17	0.03	0.41	0.18	76.6%	1.6%	76.4% 64.0%	12.6%	27% 69%	28.2%	17.0% 8.1%
29			145	-	4.01	1,28	0.21	90.04	0.61	0.13		1.0%	100.0% 100.0%	16.5%	2.1% 1.5%	47.7% 46.4%	10,2%	9.01	0.91	0.20	4.03	0.44 0.43	0.10	70.6%	0.7%	71.6%	15.2%	2.6% 1.2%	24.0% 22.8%	7.7% 20.4%
41			147	- :	0.02	1.17	0.04	02.0	0.56	0.29		1.7%	100.0%	3.7%	1.5%	47.9%	24.9%	0.02	0.86	93.0	4.02	0.36	0.22	72.7%	1.2%	23.7%	2.8%	15%	35.2%	19.9%
42		-	148 0 128	5	0.04	0.68	0.17	92.0	0.63	0.00		2.6%	100.0% 100.0%	12.6%	6.6% 2.5%	47.4% 52.6%	14.9%	93.0	0.47	0.12	0.09	0.42	0.16	75.2% 70.1%	2.0% 1.0%	75.2% 72.1%	9.5% 4.4%	6.0% 2.4%	35.8% 35.4%	12.0% 10.2%
44			1 129	2	0.01 0.01	0.62	2.04	0.01	0.20	93.0		1.6%	100.0% 100.0%	455	1.3%	47.6% 42.8%	12.9%	10.0	0.49	0.02	2.01	0.18	4.06	78.6% 68.6%	1.2%	78.6% 68.6%	19% 52%	5.1% 5.2%	28.8%	9.2% 9.2%
46		=	2 131	- 2	0.01 0.01	0.68	4.05	0.61	0.29	0.09		1.8%	100.0% 100.0%	6.8% 5.7%	1.0%	\$7.8% 46.2%	12.2%	0.01	0.51	0.64	4.01	0.24	2.07	75.2%	1.2%	75.2% 73.2%	4.9%	1.6%	36.0%	10.5%
49			5 123	4	4.02	120	0.14	0.03	8.55	0.18		1.5%	100.0%	11.5%	2.1%	6.7%	14.6%	0.01	0.89	0.13	4.02	0.22	0.12	73.2%	1.2%	742%	10.7%	18%	27.2% 25.9%	11.1%
69		-	6 134 7 135	4	4.03	1.32	0.06	0.65	0.79	0.36		2.3%	100.0% 100.0%	45% 57%	1.0%	9.7% 9.5%	19.2%	0.02	106	0.05	0.01	0.51	0.22	77.6% 22.6%	1.7%	77.9%	4.0%	1.0%	27.4% 27.0%	15.8%
51			8 136	4	0.02	1.33	0.10	9.04	2.64	0.13		16%	100.0% 100.0%	7.5%	21%	48.0% 26.6%	10.0%	0.01	0.92	0.09	0.04	0.45	0.11	69.2%	1.1%	61.2%	5.8%	27%	23.9% 21.2%	7.9% 11.9%
4.1 (1.1 (1.1 (1.1 (1.1 (1.1 (1.1 (1.1 (10 128	-	2.02	- 13	2.03	020	0.59	0,35		15%	100.0%	2.2%	0.8%	49.0%	21.6%	0.02	192	0.02	0.01	632	0.20	77.6%	1.9%	77.6%	1.9%	125	21.4%	16.9%
54		=	11 129	10	1.02	2.03	0.1k	0.03	1.69	0.18	$\vdash \exists$	1.1%	100.0% 100.0%	9.1%	21%	92.1% 92.7%	12,2%	0.01	1.05	0.11	0.02	1.17	0.14	72.6%	0.8%	72.0% 69.9%	7.6%	1.9% 5.1%	28.1%	53% 10.6%
56		=	12 141	10	0.08	2.97	0.31	0.04	175	0.69		2.6%	100.0% 100.0%	10.9%	1.2%	60.8% 52.7%	23.9% 24.5%	0.05	2.44	0.29	4.03	1.11	0.56	85.1% 20.0%	1.8%	85.1% 24.0%	10.2% 2.2%	1.1%	24.7%	19.5%
58		=	15 143	10	0.04	2.15	0.14	93.0	1.70	0.62		1.2%	100.0%	45%	1.8%	54.1%	19.8%	9.08	2.50	0.09	0.05	128	0.50	79.5%	1.0%	79.5%	2.7%	1.6%	41.7%	16.0%
60		\vdash	15 144	10	0.06	151	2.67	0.12	1.89	0.52		1.6%	100.0% 100.0%	17.2%	5.9% 2.9%	\$5.0% 42.2%	15.2% 54.7%	0.64	2.54	0.52	0.18	1.45 0.55	0.42	72.9% 68.1%	1.1%	72.9% 68.1%	15.1%	5.2% 2.4%	42.2% 26.9%	12.2%
61		=	18 146 19 147	10	0.09 0.05	2.61	0.06	0.05				2.7% 1.7%	100.0% 100.0%	2.2%	1.2%	90.7% 49.2%	25.2%	0.05	2.24	90.0		1.00	0.59	29.6% 29.1%	1.7%	79.6% 79.1%	2.1%	1.2%	25.4% 25.4%	20.9%
62		╼	20 148	10	0.06	2.41	0.51	0.22	2.01	0.52		1.8%	100.0%	14.8%	5.9%	\$9.0%	15.2%	0.05	2.69	0.41	0.18	1.59	0.43	79.0%	1.2%	71.0%	11.9%	5.4%	46.6%	12.7%

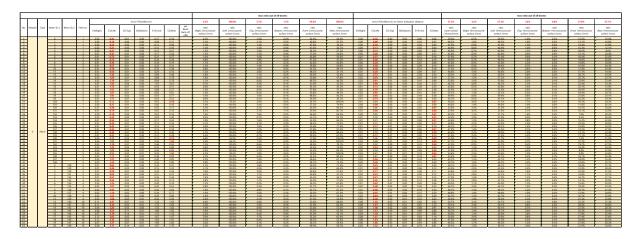
															max ratio ou	t of all beares												max ratio out of all b	eares		
								4cm2 PDs	(mW/cn2)				7.7%	100.0%	17.6%	7.7%	70.0%	25.7%		4cm2 PD	nW(cn2) a	g Soom evaluati	in distance		83.1%	\$2%	82.1%	15.6%	696	485	20.91
Module	Туре	isan D	1 (Remail)	Feed no.	S4(Kight)	\$3(14%)	SS(Top	56(8	uton)	S1(Frant)	S2(Reat)	per Beam Back-off (58)	ratio (Right 2mm)/(wont- surface 2mm)	ratio (Left 2mm)/(worz- surface 2mm)	ratio (Top 2mm(y/word- ourface 2mm)	ratio (Rotton Jimm)/(worth- surface Jimm)	ratio (Farst Zenny) worst- surface Zenny	ratio (Rear Zmm)/(worst- curtice Zmm)	S4(Kight)	Sajueti	SS(Tap)	Sé(Batton)	\$1(Foot)	S2(Rear)	stio word-surface (Sensyllenn)	ratio (Right Smm)/(worst- ourface Jmm)	ratio (Left Smm)/(worth surface 2mm)	ratio (Top Smm)/worz- curtace 2mm)	ratio (Rotton Smin(/)word- ourface 2mm)	ratio (Frant Smin)/worst- surface 2mm)	(Rear Smort) surface 2
		- 0	+	1	0.00	0.31	0.01	0	1.00	0.18	90.0		1.3%	100.0% 100.0%	2.2%	1.2%	\$7.9% \$2.6%	12.6%	0.00	0.24	0.01	1.00	0.12	0.02	77.3% 66.2%	1.0%	77.2% 66.2%	1.9%	1.2%	22.0% 27.2%	9.4%
		- 2		1	4.00	0.27	0.01			0.14	90.04		1.5%	100.0% 100.0%	49%	1.1%	\$2.8% \$1.2%	13.1%	0.00	0.19	0.01	1.00	90.0	4.03	71.5% 78.2%	1.1%	71.5% 78.2%	4.1%	0.7% 0.4%	22.2% 22.4%	10.11
		ŧ		1 2	0.01	0.29	0.01			0.14	0.06		2.4%	100.0%	41%	1.4%	49.3% 59.4%	15.9%	0.01	6.20	0.01	0.00	0.09	0.04	69.2%	2.8%	69.2%	3.4%	1.4%	29.2%	12.
		- 6	_	2	0.02	0.44	2.01	0	1.00	4.25	0.12		2.9%	100.0%	2.1%	1.6%	96.7%	222%	0.01	0.27	93.0	0.01	0.15	0.08	88.1%	3.2%	83.1%	1.6%	119	24.9%	19.
		7		-	0.01	0.58	4.01	9		0.22	93.0		1.7%	100.0%	24%	1.7%	\$5.1% 49.0%	12.4%	93.0	0.42	0.01	0.01	0.22	1.06	71.9% 65.1%	1.2%	71.9% 65.1%	1.9%	1.5%	22.4%	10
		- 10		- 2	0.02	0.49	2.02	-	165	0.24	0.67		2.0%	100.0%	13%	1.6%	47.8% Ca 1%	12.2%	0.01	0.21	0.02	0.01	0.15	4.05	63.6% 20.6%	2.0%	62.6%	4.5%	12%	29.7%	- 10
		10		- 5	0.01	0.52	0.04		165	0.26	0.05		16%	100.0%	7.4%	1.0%	\$2.8%	10.6%	0.01	9.27	0.09	4.00	0.19	0.04	74.0%	1.0%	740%	62%	1.8%	37.0%	
		12	+	- 5	0.02	1.12	0.14	- 0	163	0.60 0.50	0.15		1.7%	100.0%	12.4%	2.8%	C) 5%	13.0%	0.02	0.72 0.71	0.12	4.03	0.42	0.11	63.7% 91.5%	1.2%	63.7%	10.9%	24%	22.4% 16.2%	-
		14		- 1	0.03	1,22	0.02	0	1.01	0.72	0.24		2.3%	100.0%	13%	0.9%	56.6% 50.7%	19.9%	0.02	0.95	0.01	0.01	0.49	4.20	25.1%	1.9%	25.1% 21.6%	1.1%	18%	28.9%	
		16		-	0.02	128	0.14		103	2.69	0.15		1.6%	100.0%	11.1%	24%	90.7% 96.1%	12.1%	93.0 93.0	0.87	0.12	2.03	0.69	0.11	70,2%	1.1%	712%	1.7%	23%	44.7%	-
		17		-	1.05	0.97	0.12	9	103	454	0.15		5.0%	100.0%	13.2%	2.7%	95.2%	15.6%	0.04	964	0.11	4.02	0.35	0.12	27.4%	2.6%	22.4%	11.6%	2.0%	25.6%	
		19		- 1	4.02	1.12	0.04		160	4.65	0.92		17%	100.0%	2.7% 3.6%	1.1%	49.2% \$7.2%	22.0%	0.02	1.04	0.03	4.01	0.64	0.2%	79.4% 33.5%	1.2%	79.4% 73.5%	2.4%	1.0%	23.6%	=
		128		1	0.01	0.22	0.12			0.74	0.05		1.9%	100.0%	2.5%	2.8%	46.5%	162%	0.00	0.21	0.01	0.00	90.0	0.12	66.6%	1.2%	66.6%	2.2%	2.5%	24.6%	=
		129		1	4.00	0.79	0.01	90	1.60	0.14	90.0		1.0%	100.0% 100.0%	41%	1.7%	47.1%	12.1%	0.00	0.19	0.01	1.00	90.0	4.03	65.5%	1.0%	65.5%	125	1.6%	27.2% 23.2%	=
		131		1	0.01	0.24	4.02	ó	1.00	0.17	60.0		2.5% 1.2%	100.0% 100.0%	43%	1.7%	69.6% 36.7%	10.4%	0.00	0.15	0.01	0.00	0.09	0.02	642%	1.7%	64.2%	5.4% 3.2%	5.7% 2.6%	27.1%	
				- 2	0.01	0.14	0.01	0		0.12	0.04		2.0%	100.0%	10.6%	2.9%	49.4%	2.7%	0.01	0.22	0.05	0.01	0.14	4.02	53.9%	1.5%	\$3.9%	3.4%	2.4%	25.5%	_
		134		-	0.01	0.51	4.03	9	160	0.20	93.0		2.4%	100.0% 100.0%	485	1.0%	58.4% 68.1%	19%	0.01	0.26	9.09	0.01	0.18	0.04	71.6% 69.3%	1.8%	71.6% 69.2%	5.9% 42%	1.0%	26.1% 42.5%	=
		136		- 2	0.01	0.71	102	- 0	160	0.20	0.06		1.1%	100.0% 100.0%	2.8% 46.5%	2.2%	6.75	14%	0.01	0.41	0.02	4.02	0.18	4.0%	60.1% 52.6%	0.8%	60.1% 52.6%	3.4% 9.2%	2.7%	25.9% 25.1%	
	Feach	138		- 1	0.01	0.47	0.01	0	1.00	0.24	90.0		1.7%	100.0%	2.0%	0.6%	69.6%	19.2%	0.01	0.75	0.04	1.00	0.23	0.07	74.7%	1.2%	747%	2.6%	0.6%	48.8%	+
		129		2	0.01	953	0.05	9	165	0.32	52.0		1.7%	100.0%	195	2.7%	60.2%	12.9%	0.01	0.23	0.64	0.01	0.18	0.05	62.5%	1.1%	62.5%	7.8%	23%	22.2%	₽
		141		ŝ	4.02	100	0.12	ő	103	0.64	0.14		2.2%	100.0%	12.4%	3.2%	64.0%	16,0%	0.02	2.69	0.11	4.03	0.42	0.12	68.4%	1.7%	68.4%	112%	3.0%	41.6%	1
		142		5	0.02	125	0.01	- 0	160	0.72	0.22		24%	100.0%	26%	1.0%	27.7%	19.6%	0.02	931	0.02	0.01	0.49	126	77.2%	1.8%	77.2% 72.1%	1.0%	1.0%	25.0%	-
		144		-	4.02	133	4.17		122	160	0.12		1.8%	100.0%	12.4%	7.7%	6.45	1.0%	0.02	0.85	0.15	1.09	0.36	1.09	642%	1.2%	642% 54.8%	10.9%	67%	27.2%	⇇
		146			8.02	134	2.02		103	0.68	0.22		1.8%	100.0%	24%	2.2%	59.5%	19.0%	0.01	6.85	6.02	4.02	0.50	0.19	74.2%	1.2%	742%	2.0%	1.9%	43.4%	
		147		- 1	0.02	1.13	0.02	- 0	103	168	0.25		2.0%	100.0%	125	2.6%	60.5% 52.0%	21.8%	0.02	0.85	0.01	1.03	0.50	0.21	75.4% 59.2%	1.5%	75.4% 58.2%	1.1%	2.2% 4.9%	44.2% 21.6%	┰
		0	128	-	4.02	0.70	4.02	0	160	0.41	0.11		2.7%	100.0%	125	2.2%	99.1% 92.8%	15.7%	93.0	451	0.02	0.01	6.22	1.09	76.3% 69.1%	1.9%	76.2% 69.1%	2.6%	2.0%	21.6%	=
		- 2	132	- 5	0.01	0.64	0.04	0	1.60	0.24	0.12		17%	100.0% 100.0%	65% 81%	13%	93.2% 61.1%	15.6%	93.0	0.65	0.64	0.01	0.21	0.09	71.3% 73.5%	1.1%	71.2% 71.5%	57% 7.0%	1.1%	22.7% 41.0%	
		4	122	- 2	0.01	0.78	0.04	0	102	0.24	0.12		2.6%	100.0%	45%	1.9%	40.0%	12.2%	0.02	0.61	90.08	0.01	0.19	2.07	66.8%	2.0%	66.8%	3.8%	1.8%	24.2%	t
		- 5	122	4	0.03	1.07	0.10	9	103	4.67	0.16		2.8%	100.0% 100.0%	475	2.9%	\$3.7% \$8.8%	14,7%	0.02	0.70	0.09	0.03	0.37	0.12	26.3%	2.0%	28.2%	4.5%	24% 12%	34.2%	_
		7	135	4	4.02	1.05	0.06	0	62	0.64	0.16		2.2%	100.0% 100.0%	5.6%	2.2%	60.7% 67.8%	15.5%	0.02	0.74	0.06	4.02	0.43	0.12	70.2%	1.7%	71.2%	4.8%	1.9%	41.2% 21.9%	⊨
				-4	0.04	1.26	0.09	- 0	1.02	0.69	0.15		1.5%	100.0%	9.1%	2.6%	40.0%	10.2%	9.02	0.79	0.10	0.02	0.46	0.14	62.8%	1.1%	62.9% 62.4%	7.6%	12%	24.6%	_
		10	122	4	4.03	1.14	4.02	0	165	4.56	0.21		2.4%	100.0% 100.0%	2.9%	1.1%	57.4% 59.3%	18.8%	0.62	0.85	6.03	4.01	0.43	4.17	74.8%	1.8%	74.8%	2.6%	1.0%	27.7%	Е
		12	140	10	2.07	3.04	0.51	, i	114	171	0.29		2.2%	100.0%	16.7%	4.6%	96.3%	12.9%	0.06	216	0.46	0.12	1.22	0.31	71.2%	1.7%	71.2%	15.0%	3.9%	40.1%	ŧ
		13	141	10	0.12	2.12	0.91	- 0	109	1.63	920		5.2% 2.6%	100.0%	13.4%	1.1%	20.0% 62.1%	22.1%	0.08	1.99	0.09	0.05	1.01	0.45	81.2% 78.0%	2.6%	81.2% 78.0%	125%	22%	41.6%	
		15	143	10	2.08	115	0.08	- 0	163	193	0.69		2.3%	100.0%	2.2%	1.0%	97.6% 97.6%	20.7%	0.05	2.57	0.06	4.03	148	457	26.2%	1.6%	76.7% 74.0%	18%	0.8% 5.1%	44.2%	
		12	145	10	2.07	150	855	-	(6)	150	0.50		225	100.0%	17.6%	2.2%	67.6%	15.9%	0.05	201	0.49	106	0.54	1.0	63.9%	1.6%	63.9%	15.6%	2.0%	22.0%	Н
		18	146	10	0.10	2.86	0.06	0.0	166	152	0.64		2.2%	100.0%	226	1.1%	9.7% 97.8%	24.0%	93.0	2.22	0.06	0.02	1.03	0.54	77.6% 79.0%	2.4%	77.6% 79.0%	2.2%	169	15.9%	=
		20	148	10	0.06	3.08	2.62	- 0	117	1.97	0.40		2.6%	100.00	13.6%	5.6%	60.7%	12.6%													

Table 5. PD of Ant K- patch antenna (24GHz-n258)

[Folder Open Status]

- K-patch Low CH

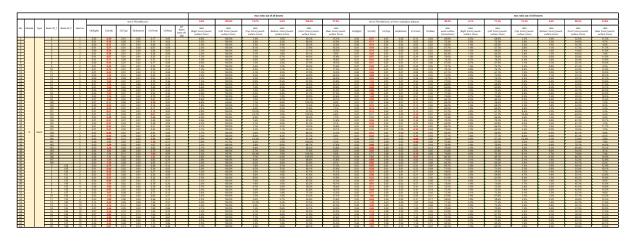




														max ratio eu	of all beams									1			max ratio out of all b	eams		$\overline{}$
П	$\neg \Gamma$	-					-	cm2 PDynratys	oni)			49%	100.0%	5.0%	0.8%	\$8.7%	86.0%		6on2 PD;	nM(on2) at	tūnin evaluat	ion distance		55.1%	2.6%	55.9%	2.7%	0.7%	28.2%	4EX
No. 1	odule Type	Beam IC	d Bena 10,3	Feed no.	SHRight)	Slipeto	SS(Top)	Sélkottoni	\$1(Frant)	52(Read)	per Beam Back-off	ratio (Right 2mm)/(worst- ourface 2mm)	ratio (Left 2mm)/(wonz- curface 2mm)	ratio (Top 2mm)/(word- surface 2mm)	ratio (Ration Zmm)/(worst- surface Zmm)	ratio (Forst 2mm)/(worst- surface 2mm)	(Rear Zimm) (Nearch surface Zimm)	Septigen	Siste	SS(Sop)	Si(Bottom)	Stifram	S2(Rear)	otio worth-surface (15mm/(2mm)	ratio (Right 15mm)/(worst- surface 2mm)	ratio (Left 10mm)/(worth- surface 2mm)	ratio (Top 10mm)/(worz- surface 2mm)	ratio (Rottom 10mm),/(worst- surface 2mm)	ratio (Fiore 10mm()/(word- ourface 2mm)	ratio (Rear 10mm)/(word- ourface 2mm)
1		. 0		- 1	4.00	0.45	0.61	0.00		0.58		0.6%	100.0%	1.1%	0.2%	44.7%	21.2%	4.00	0.18	4.00	6.50	0.09	0.28	40.9%	0.2% 0.8%	40.9% 42.5%	0.9%	0.2% 0.4%	16.7%	17.8%
à		2		1	4.00	0.30	0.00	0.00	0.14	0.08		62% 65%	100.0%	1.2%	6.2% 9.2%	47.2% 47.0%	27.8% 30.5%	1.00	0.11	4.00	6:30	0.04	0.23	27.5% 40.2%	0.2%	27.5% 40.2%	1.2%	0.2% 0.2%	14.4%	11.7% 12.7%
5		4		1	0.00	0.12	0.00	0.00	0.17	2.29		1.6%	100.0%	1.2%	0.7%	54.4%	28.0%	4.00	0.16	1.00	0.00	0.06	033	44.2%	1.7%	44.2%	0.9%	0.2%	18.9%	9.1%
- 6		1	_	2	0.01	0.60	0.00	0.00	0.25	0.25	+	0.8%	100.0%	0.7%	0.5%	41.8%	41.2%	1.00	0.35	1.00	0.00	0.09	0.12	41.1%	6.7% 6.5%	41.1% 50.2%	0.5%	0.7%	14.5%	11.25
		7		- 2	0.01	0.90	0.61	0.00	0.40	0.32	-	0.8%	100.0%	1.8%	0.2% 0.2%	46.7%	41.2% 36.7%	4.00	0.40	0.01	6.00	0.17	0.54 0.28	50.2% 46.4%	0.5%	50.2% 66.4%	1.3%	0.0% 0.2%	21.0%	16.9%
10		9		- 1	0.01	0.72	0.00	0.00	0.22	9.22		62% 62%	100.0%	0.4%	62% 62%	44.2%	44.1% 41.7%	100	0.22	4.00	0.00	0.10 0.11	0.15	46.6% 50.7%	0.4%	66.6% 50.7%	0.4%	0.2% 0.2%	15.8%	22.4% 11.2%
12		11		- 1	0.01	0.56	0.00	0.00	0.27	0.17	+	0.9%	100.0%	2.7%	0.2%	49.6%	21.5%	4.00	0.45	0.01	0.00	0.10	0.28	40.1%	0.5%	40.1%	2.2%	0.2%	18.2%	13.7%
12		12	_		0.01	1.76	0.01	0.00	105	0.54	_	04%	100.0%	0.5%	62%	90.7% 95.1%	32.9% 43.7%	0.01	0.88	0.01	0.00	0.52	0.26	\$0.3% \$4.7%	0.4%	50.2% G4.7%	0.5%	02%	29.3%	15.0%
		- 19	1	- 5	102	211	0.61	0.00	103	0.98		0.8%	100.0%	0.4%	02%	48.9%	46.7%	201	1.16	2.01	0.00	2.69	0.47	\$5.1%	0.6%	55.1% 47.1%	0.2%	02%	22.1%	22.5%
17		16		è	0.01	1.91	0.00	0.00	1.07	0.50		0.6%	100.0%	47%	62%	62% 02%	26.25	0.01 0.01	0.85	407	0.00	0.45	621	412%	0.6%	44.2%	24%	0.1%	23.4%	11.2%
19		17	_	1	0.02	2.11	0.01	0.00	1.09	0.66	+	1.1%	100.0%	0.5%	0.1%	\$2.8% \$2.8%	44.9%	0.02	1.16	0.00	0.00	0.54	0.46	\$1.6% \$4.9%	0.2%	\$1.6% \$4.9%	0.4%	0.1% 0.2%	26.6%	17.2% 22.0%
20		19	_	- 5	0.01	2.19	0.02	0.00	197	0.87	=	0.5%	100.0%	1.0%	02% 02%	6115 SL45	26.5%	2.01	1.12	4.02	6:30	0.49	0.62	\$1,2% ALCO	0.6%	51.2% 44.6%	0.7% 2.4%	0.2% 0.1%	21.9%	11.2%
22		129		-	3.01	0.13	0.01	0.00	0.26	0.11		13%	120.0%	2.9%	0.8%	6.6%	86.2%	1.00	0.04	4.00	0.00	1.02	0.25	29.5%	22%	34.1%	2.1%	0.2%	15.5%	29.5%
24		129		-	1.00	0.39	0.01	0.00	0.25	0.15	_	1.5%	100.0%	2.5%	0.5%	28.5% 22.7%	23.5% 66.8%	1.00	0.07	1.00	0:33	1.02	027	24.1%	1.0%	26.5%	2.0%	0.5%	12.0%	23.9%
25		132	-	1	0.01	0.19	00.0	0.00	0.25	0.16	_	25%	100.0%	2.0%	0.5%	26.7%	73.9%	1.00	0.07	1.00	0.00	1.02	0.26	25.1%	2.1%	25.1%	1.5%	0.5%	10.2%	23.4%
27		122		- 1	0.01	0.42	0.01	0.00	0.10	0.22	_	2.9% 1.6%	100.0% 100.0%	1.7%	67% 62%	23.1% 23.7%	76.4% 71.2%	0.01 0.00	0.17	4.00	0.00	0.04	0.16	41.0%	12% 0.8%	41.0% 44.2%	1.0%	0.5% 0.2%	145	27.6% 27.7%
29		135		2	0.01	0.50	0.00	0.00	0.15	0.34		2.4%	100.0%	24%	0.4%	30.1%	68.9%	0.01	0.19	0.01	6:30	0.06	0.16	37.3%	1.6%	27.2%	1.6%	0.2%	11.8%	22.5%
31		136		1	0.01	0.42	0.01	0.00	0.12	0.35	+	1.2% 1.2%	100.0%	2.2%	0.7% 0.2%	22.7% 20.9%	63.5% 71.0%	1.00	0.17	0.01	0:00	1.06	0.11	43.4%	12% 12%	43.4%	1.8%	0.2% 0.2%	14.9%	23.2%
22	K Patri	128		-	0.01	0.42	0.01	0.00	0.13	0.32		12% 22%	100.0%	2.6%	0.2%	2076	77.8% 67.2%	0.01 0.01	0.18	0.01	6.00	4.06	0.16	42.7%	12%	42.7%	1.7%	0.0% 0.4%	13.4%	27.0% 27.5%
às		140		- 3	4.03	0.68	60.0	0.01	0.19	0.52		4.9% 2.7%	100.0%	4.0%	6.7% 0.5%	26.5%	77.6% 84.4%	4.02	0.80	4.02	631	4.07	629	44.9% 48.0%	2.2%	44.9% 45.2%	2.8%	6.7% 0.5%	10.8%	43.0%
26		142		-	0.01	1.19	0.00	0.00	0.48	0.82		0.8%	100.0%	0.8%	0.1%	40.4%	68.4%	4.01	0.54	4.01	633	0.24	0.49	44.9%	0.7%	44.9%	0.4%	0.1%	19.8%	41.2%
37		542		- 5	4.03	1.29	0.04	0.00	0.42	0.95	+	25%	100.0%	24%	0.2%	32.4% 34.7%	23.5% 63.2%	0.02	0.60	0.03	0.00	0.21	0.44	46.5%	12%	46.5% 35.6%	2.4%	02%	15.9%	32.8%
39		145		5	0.03	0.95	0.02	0.01	627	0.76	-	24%	100.0%	23%	0.5%	26.1%	61.7%	0.02	0.45	0.01	0.00	0.12	0.42	49.0%	21%	48.0%	1.2%	0.4%	12.3%	44.7%
41		147		- 3	4.03	129	0.03	0.00	0.48	2.89		22%	120.0%	22%	02%	X 25	68.2%	402	0.61	4.02	0:00	0.24	0.45	47.2%	14%	47.2%	1.5%	0.2%	18.2%	34.6%
43		0	129	2	0.03	0.70	0.06	0.00	0.34	0.93		20%	100.0%	1.4%	0.2%	S0.0%	41.4%	0.02 0.01	0.55	0.05 0.01	0.01	0.16	0.41	40.0%	0.8%	40.0%	0.9%	0.2%	18.6%	25.25
44		-	129	-	0.01	0.56	0.61	0.00	0.22	0.27	_	1.6%	100.0%	22%	0.4%	40.2% 27.5%	49.2% 27.8%	0.01	0.22	0.01	0.00	1.07	0.11	29.8%	1.1%	20.8%	1.4%	02%	12.8%	20.2%
46		- 3	131	- 2	0.01	0.69	0.61	0.00	629	4.29	_	22%	100.0%	1.2%	0.4%		62.2%	0.01	0.36	0.01	6.50	0.10	0.54	37.6%	12%	27.6%	0.9%	0.2%	14.0%	11.5%
47			122	- 4	1.02	1.09	0.01	0.00	0.27	0.70		22%	100,0%	13%	0.5%	46.7% 36.2%	61.7%	4.02	0.52	0.01	0:30 0:31	0.11	0.31	47.5%	1/8	47.5%	1.1%	0.5%	12.8%	22.8%
50		- 5	134	+	4.02	1.16	92.0	0.00	0.70	0.82	+	12% 18%	100.0%	12%	0.1% 0.2%	\$1.1% 44.5%	62.2%	0.01	0.69	0.01	0.00	0.29	0.41	50.8% 49.7%	0.P% 1.7%	50.8% 49.7%	0.7%	0.1% 0.2%	20.5%	22.5%
51		- 1	126		0.01	1.06	62.6	0.00	0.44	4.59	=	12% 12%	120.0%	23% 12%	0.2% 0.2%	41.2%	56.0% 58.5%	0.01 0.01	0.48	4.02	6.00	0.19	622	45.8%	0.7% 0.8%	45.8%	1.6%	0.7%	18.2%	26.0% 21.6%
53		10	128	1	1.02	153	92.0	0.00		4.74		12%	120.0%	1.6%	0.1%	47.4%	43.9%	0.01	0.69	4.02	0.00	4.25	0.34	44.9%	0.8%	44.9%	1.0%	0.1%	16.6%	22.4%
55		11	139	10	4.02	2.78	0.03	0.00	1.55	1.54	_	1.9% 2.5%	100.0%	2.6%	0.2%	66.5% 55.7%	56.1% 55.5%	0.01	1.40	0.02	0:30 0:31	0.79	0.85	50.3%	1.0% 1.8%	29.1% 50.2%	1.9%	0.2%	20.7%	24.5% 31.7%
56		12	141	10	4.07	2.70	60.0	0.01	190	2.11	-	19%	100.0% 100.0%	0.9%	0.2% 0.1%	\$1.5% \$0.9%	\$7.1% \$1.6%	4.05	1.91	4.02	6.01	0.95	1.56	\$1.7%	1.6%	\$1.7% \$1.0%	0.4%	0.2% 0.1%	24.6%	21.2%
58		15	143	10	1.07	4.17	0.10	0.01	2.54	2.15		1.2%	100.0%	2.2%	62% 92%	51.2%	\$1.5% 46.5%	105	1.83	0.07	631	1.00	0.99	43.8%	1.1%	43.8%	1.7%	0.2%	23.9%	23.8%
60		17	145	10	0.06	240	0.14	93.0	181	1.90		1.5%	100.0% 100.0%	1.2%	0.7%	45.5% 52.7%	55.2%	0.04	1.72	0.02	0.21 0.21	0.91	1.05	50.3%	0.9% 1.2%	28.4% 50.3%	0.6%	0.2% 0.2%	19.8% 26.5%	21.7% 31.7%
62		19	147	10	1.06	411	0.02	0.00	212	1.90	+	15%	100.0%	0.4%	0.1%	47.7% 51.2%	\$1.0% \$2.2%	0.04 0.04	1.92	2.01		1.03	104	48.9%	1.5%	51.9% 48.9%	0.8%	0.1%	22.9%	21.75
63		20	148	10	0.05	2.90	0.14	0.01	191	1.87		1.6%	100.0%	2.6%	0.4%	49.0%	48.1%	0.04	1.62	0.10	0.21	0.95	0.84	41.5%	10%	41.5%	2.7%	0.4%	21.9%	21.6%

[Folder Closed Status]

- K-patch Low CH



														max ratio ou							max ratio out of all beams									
П		Т		4cm2 PD(mWycn2)								82%	100.0%	13.2%	5.4%	100.0%	29.6%	4cm2 PD(nRE(cm2) at Some evaluation distance						77.6%	66%	77.2%	11.5%	48%	77.6%	24.8%
No.	Andule Ty	pe ša	sam ID_1 Berna ID_2	Feed no.	Saylight	Silpario	SS(Top	Sic(Rotton	St(Frant)	S2(Reat)	per Bean Back-off (db)	ratio (Kight 2mm)/(wonz- ouface 2mm)	nzio (Left 2mm),(worz- surface 2mm)	ratio (Top 2mm)/(worst- ourface 2mm)	issio (koton žmn)/(eoro- suface žmn)	ratio (Fant Janny)word- surface Janny	ratio (Rear Zmm)/(worst- surface Zmm)	S4(Right)	Skijueltij	SS(Top)	Sé(katan)	St(Frant)	S2(New)	ratio worz-surface (Serre/Zenn)	ratio (Right Smm),(worst- outsce 2mm)	ratio (Left Smm)/(scorp- ourface 2mm)	ratio (Top Smm)/(worst- curface 2mm)	ratio (Rotson Smin(/)world- surface Zmin)	ratio (Frant Smire)/worst- ourface Jimm)	ratio (Rear Smm)/(wonz- surface 2 mm)
1 2		_	0	1	0.00 0.01	0.43	0.01	0.00	0.18	0.03		0.7% 2.8%	100.0% 100.0%	1.6%	2.8%	42.0% 54.2%	12.6%	0.00	0.29	0.01	4.00	0.13	4.05	67.1%	0.5% 2.8%	62.1%	2.85	2.8%	23.4%	12.0% 10.2%
2		⊨	į.	1	4.00	0.22	0.01	0.61	4.06	0.03		18%	100.0% 100.0%	2.2% 1.9%	32% 12%	36.8%	15.5%	0.00	0.14	0.01	4.01	6.63	2.03	64.5% 70.5%	1.4%	645% 715%	2.2% 3.2%	2.7% 4.9%	14.5%	11.4% 12.0%
5			1	-	4.00	0.26	0.01	0.00	4.07	0.04		12%	100.0%	31%	12%	25.6%	17.1%	0.00	0.18	0.01	4.00	0.04	4.03	69.4%	1.2%	68.4%	2.7%	12%	14.2%	12.4%
6		- 1-	2	3	0.01	0.50	0.02	0.61	435	0.03	-	1.8%	100.0%	4.0%	1.0%	50.9% 45.9%	14.0%	0.01	0.22	0.02	2.00	0.18	0.05	64.1% 24.0%	1.4%	641% 745%	14%	185	36.1%	10.6%
8		⊨	7	- 3	0.01	0.71	0.01	0.61	0.32	0.14		10%	100.0%	47% 17%	13%	44.9% 34.9%	20.1%	0.01	852	0.00	0.01	0.21	0.11	72.7% 67.4%	0.8%	22.7% (2.4%	0.4%	16%	35.2%	15.4%
10		_	10	- 5	2.01	0.61	2.02	0.00	0.21	0.12		13%	100.0%	3.2%	0.7%	50.0%	15.7%	92.0	6.41	0.02	1.00	6.22	4.07	70.1%	1.0%	72.1%	2.8%	8.5%	15.6%	11.8%
11			10	- 3	0.01	0.60	0.01	0.01	0.25	0.15		0.8%	100.0% 100.0%	25%	0.8%	43.9% 34.0%	19.2%	93.0 93.0	0.60	0.01	0.01	0.04	0.12	74.7% 59.8%	0.6%	747% 59.8%	2.2%	15%	32.5% 15.6%	12.8%
12		− =	12	-	0.04	1.66	0.12	0.61	0.47	0.43		2.5%	100.0%	125	0.9%	22.5%	27.9%	92.0	1.05	0.11	0.01	0.35	0.32	73.0% 27.1%	2.1%	72.0%	7.5%	100	24.5%	22.0%
15		⊨	14	- 3	4.02	1.77	0.02	0.61	0.74	0.45		1.1%	100.0% 100.0%	1.9%	0.5%	42.0%	25.5% 23.8%	0.02	122	0.01	0.01	0.53	0.28	75.2% 68.0%	0.9%	75.2% 68.0%	1.8%	0.4%	31.2% 21.4%	21.4% 18.7%
27			16	-	4.02	1.62	4.02	0.09	0.42	0.27		1.0%		13%		27.8%	22.5%	93.0	1.05	0.02	0.08	0.31	0.29	645%		64.5%	1.0%	48%		
19		⊢	17 18	- 5	0.03	1.51	0.10	0.01	0.67	0.41		2.2% 2.6% 0.7%	100.0% 100.0% 100.0%	6.9% 5.1%	0.7%	27.6% 42.2% 26.4%	24.9%	93.0	1.11	90.0	0.01 0.01	0.42	0.32	73.8% 77.3%	1.9%	72.8% 77.8%	1.0%	0.6%	28.0%	21.4% 24.8% 18.8%
20		E	19 20	- 5	4.02	2.01	0.01	60.0	0.72	0.47		0.7% 1.0%	100.0% 100.0%	125	1.6%	2.0	23.3% 22.5%	0.01 10.0	1.66	0.01	4.02	0.52	0.29	71.5% 64.7%	0.6%	71.5% 64.7%	0.4% 1.1%	1.4%	26.1%	17.6%
22			128	- 1	0.01	0.12			0.17	0.00		5.4%	79.9%	2.4%	2.4%	100.0%	12.0%	93.0	0.09	0.00	4.00	0.11	4.02	62.9%	4.8%	45.8%	5.8%	1.8%	63.9%	9.6%
24			129	1	0.01 0.01	0.22	0.01	0.01	0.16	0.02		2.2%	100.0% 100.0%	4.0%	2,2% 2,8%	30.2% 34.5%	10.2%	0.00	0.16	93.0	4.01	0.12 0.11	4.01	70.2% 62.5%	1.2%	31.2% 62.5%	2.5% 3.7%	1.8% 2.8%	\$1.6% \$2.3%	8.0% 5.6%
25			121	1	4.02	0.18				0.02	-	8.2% 2.8%	100.0% 100.0%	13.7%	17%	6.65	10.4%	0.00	0.12	0.02	1.00	0.13	0.01 0.01	64.5% 58.5%	1.7%	64.5% 58.5%	11.5%	1.6%	54.6% 58.0%	72% 52%
27			133	2	0.02	0.44	0.03	0.00	0.27	0.03		46%	100.0% 100.0%	7.1% 1.6%	0.7%	56.4% 91.6%	7.8%	0.02	630	0.09	4.00	0.28	4.03	68.0% 23.5%	2.0%	68.0% 73.5%	52% 136	47%	64.4%	52% 53%
29			135	- 5	402	0.45	2.03	0.65	0.24	0.05		47%	100.0%	62%	2.0%	25.2% 21.5%	11.0%	0.02	0.29	0.02	2.01	0.25	2.04	65.2%	4.0%	65.2%	426	185	55.2% 61.4%	£2% 11.0%
31			136	- 3	0.01 0.01	0.42	0.01	0.00	0.30	0.06		2.2%	100.0%	41%	0.9%	84.0%	16.1%	13.0	0.29	0.01	0.01	0.31	0.06	73.2%	1.7%	73.2%	3.0%	17%	64.2%	7.8%
22	K Fac	sch	123	- 3	2.01	0.46	0.01	0.61	0.40	90.0		2.8%	100.0%	19%	23%	85.5% 34.1%	11.9%	0.01	0.22	0.64	0.01	0.29	0.04	69.0%	2.6%	61.9%	1.5%	195	92%	9.5%
24		⊨	142		0.04	0.79	0.10	0.02	0.64	0.05		4.9%	100.0% 100.0%	12.6%	23%	81.5% 99.7%	6.2% 12.4%	6.69	0.58	0.09	4.02	0.50	0.04	73.5% 77.6%	4.1% 3.2%	72.5% 75.1%	10.9%	1.9%	63.0% 77.6%	43%
26		_	142	-	2.02	1,22	2.03	0.61	192	0.24		16%	100.0% 100.0%	2.1%	0.7%	75.0%	19.2%	0.02	0.89	0.02	0.01	6.75	0.19	73.2%	1.2%	73.2%	1.7%	145	61.4%	15.7% 15.7%
27			163	-	0.04	1.00	1.0%		0.89	90.0		22%	100.0%	17% 59%	2.0%	30.8% 86.7%	8.1%	9.02	0.92	0.09	0.04	0.65	0.14	72.8% 64.7%	2.1%	72.8% 64.7%	2.7% 4.8%	2.5% 1.5%	\$1.9% 64.6%	6.1%
29		− Ε	145	-	4.05	0.96	0.09	9.02	193	93.0		4.7%	100.0% 100.0%	2.6%	1.7%	67.1% 88.6%	16%	93.0	0.70	93.0	0.01	0.71	0.07	73.5%	2.9%	72.0%	7.0% 2.2%	1.2% 0.4%	73.5% 73.0%	6.9% 12.8%
41			147	- 1	0.02	129	0.04	60.0	0.86	0.11		24%	100.0%	3.4%	2.0%	67.2%	16.6%	0.62	0.95	6.09	4.02	0.65	0.17	73.9% 69.4%	1.9%	72.9% 69.4%	2.5%	5.7% 3.7%	50.6% 53.1%	12.4% 8.5%
42			0 128	- 2	0.02	0.71	4.02	0.01	2.46	0.14		2.1%	100.0% 100.0%	24%	1.6%	34.6% 64.7%	19.7%	93.0	0.45	0.02	0.01		0.11	64.2%	1.8%	64.0%	2.5%	13%	44.8%	15.2% 9.1%
44		⊢	1 129	2	0.02 0.01	0.46	1.02	0.01	0.31	90.0	\vdash	2.2%	100.0% 100.0%	4.2%	2.8% 1.9%	49.4%	11.9%	13.0	0.22	0.02	0.01	0.16	0.04	70.9%	1.9%	71.9% 61.8%	3.4% 3.8%	2.6% 1.5%	45.5% 31.2%	9.9%
46		− Ε	2 121 A 123	2	0.02	0.67	0.04	0.61	0.29	0.10		4.9%	100.0% 100.0%	43% 41%	1.2%	41.1% 41.0%	14.1%	90.0	0.46	9.09	0.01	0.19	4.07	64.0%	1.6%	66.6%	12%	195	27.8%	10.2% 10.2%
48		⊨	\$ 122	- 4	0.09	0.96	0.07	0.61	0.69	0.13		53%	100.0%	63%	12%	72.0%	12.1%	0.66	9.66	0.09	0.01	6.53	0.10	69.5%	4.0%	68.5%	5.6%	4.9%	54.4%	10.0%
69		E	6 134 7 135	4	1.04	0.98	2.05	0.00	0.76	0.18		1.9%	100.0% 100.0%	23% 52%	1.0%	61.1% 54.9%	17.4% 18.5%	0.02	970	0.02	4.01	0.56	0.16	75.6% 71.6%	1.5%	75.6% 71.6%	1.7% 4.1%	2.9%	45.2% 28.4%	13.2% 54.7%
51		- 1	6 122	4	403	0.96	0.02	0.03	0.61	0.18	-	2.8%	100.0%	16%	27%	65.5%	19.0%	0.02	0.70	0.61	0.03	0.42	0.14	72.1% 21.2%	2.4%	73.1%	2.8%	2.6%	43.5% 50.2%	54.2% 52%
53		=	10 138	- 1	4.03	154	4.03	0.02	4.97	0.36		18%	100.0%	18%	14%	92.5%	16.8%	6.02	106	0.02	4.02	0.61	4.20	69.0%	1.6%	68.0%	1.4%	1.2%	22.4%	12.7%
55		E	12 142	10	0.14	253	0.05	0.04	154	0.52		53%	100.0% 100.0%	15%	1.4%	60.8%	20.6%	0.12	191	0.18	4.02	1.18	0.40	25.2%	4.7%	15.2%	2.1%	1.1%	46.5%	15.9%
57			14 141	10	0.10	1.12	0.12	0.03	1.77	0.92		1.1%	100.0%	16%	JFR.0 JFR.0	\$1.9% \$1.5%	24.8% 24.8%	90.08	2.43	0.09	4.02	1,60	0.67	71.6%	2.4%	72.8% 71.6%	2.8% 1.2%	0.7% 0.5%	48.2% 36.7%	20.2%
58		E	15 143	10	0.09	2.62	0.09	0.12	1.71	0.92		2.2%	100.0% 100.0%	2.6%	2.6% 5.2%	60.8% 54.2%	23.8% 17.4%	0.06	2.21	6.07	0.12	121	2.66	67.4% 61.2%	1.7%	62.4% 61.2%	1.9%	24% 47%	35.2% 41.7%	19.2%
60		F	17 145	10	0.15	139	0.21	0.65	1.95	0.74		4.8%	100.0%	6.6% 1.6%	14%	62.2% 90.5%	22.7% 27.6%	0.12	224	0.16	0.04	152	0.60	71.2%	4.0%	71.2% 71.0%	5.2% 1.2%	115 125	41.7% 21.5%	19.0% 19.0%
4.1 (1.1 (1.1 (1.1 (1.1 (1.1 (1.1 (1.1 (19 147	10	0.05	2.51	1.06	0.06	1.98	0.92		1.5%	100.0%	1.8%	1.6%	56.2%	26.1%	0.04	2.48	0.06	0.05	1.36	4.75	70.5%	1.1%	72.5%	1.6%	15%	28.7%	21.5%
62			20 148	10	1.09	2.15	0.10	0.15	1.55	0.63		2.7%	100.0%	3.1%	4.7%	49.0%	20.1%	93.0	2.01	0.08	0.14	1.16	0.51	64.2%	2.2%	64.2%	2.6%	4.2%	16.9%	16.1%

														max ratio out of all beams												wax ratio out of all beams							
П								4cm	až PD(mW/cr	n2)			25%	100.0%	122%	5.9%	92.9%	28.2%	4cm2 PD(n88/on2) at Snow evaluation distance					75.8%	60%	75.8%	11.7%	SAS	63.7%	23.8%			
No.	Module 1	lype fina	m ID_1 Sens	10,2 Feed	54(G)	gito Silpa	es s	iS(Top)	Sé(Rotton)	\$1(Frant)	Sirker	Beam Back-off (db)	ratio (Right 2mm)/(worst- ouflace 2mm)	ratio (Left 2mm)/(worsz- surface 2mm)	ratio (Top 2mm)/(word- ourface 2mm)	ratio (Rotton Jimm)/(worth surface Jimm)	ratio (Forst 2mm)/(worst- surface 2mm)	ratio (Rear Zmm)/(wont- curface Zmm)	S4(Right)	Skijudij	SS(Tap)	Sé(katan)	\$1(Foot)	S2(Rear)	stio worz-suface (Smm/2mm)	ratio (Right Smm),(worst- ourface 2mm)	ratio (Left Smm)/(worth- oufface 2mm)	ratio (Top Smm)/worth- surface 2mm)	ratio (Rottom Smm(//word- surface Jmm)	ratio (Front Smm)/(worz- surface Jmm)	ratio (Near Smm)/(worst- surface 2 mm)		
1 2		=	0		4.0	0 0.41		0.01	0.01	0.17	92.0		6.7% 1.6%	100.0% 100.0%	1.5% 2.5%	1.1%	20.2%	16.9%	00.0		93.0	4.00	0.13	4.06	66.2% 67.2%	0.4% 1.2%	6225	1.5%	129	22.7%	12.0% 10.2%		
2		=	2		4.0	1 02		0.01	0.01	0.09	60.0		2.7% 1.0%	100.0% 100.0%	15%	2.1% 1.0%	22.2% 22.2%	14.6%	93.0	0.14	0.04	0.01	0.04	4.02	62.8% 66.1%	2.2%	62.8% 66.1%	2.5% 2.2%	2.7% 1.0%	19.0%	10.6% 11.8%		
- 5			4		4.0	0.1		0.01	0.61	0.09	0.06		1.5%	100.0% 100.0%	12%	1.5%	27.3% 43.7%	15.9%	0.00	0.22	0.01	0.01	0.06	0.04	67.0% 64.1%	1.2%	67.0% 64.1%	2.0% 2.7%	1.5%	15.2% 22.5%	11.4%		
2			2		4.0	0.9		102	0.00	4.27	0.18		1.0%	100.0% 100.0%	195	0.4%	20.5% 20.1%	19.2%	0.01	0.67	0.02	4.00	0.36	0.14	71.7% 72.7%	0.6%	71.7% 22.7%	16%	6.2% 1.6%	28.7%	14.7% 15.7%		
-			ž .		40	0.4		0.01	0.00	0.16	0.16		1.5%	100.0%	2.6%	3.9%	34.1%	20.0%	93.0	0.30	0.00	4.02	0.19 0.11	4.07	65.7%	1.2%	66.7%	2.4%	3.5%	35.2% 22.8%	15.0%		
10			10	_	40	0.7		0.01	0.00	0.22	0.13		1.0%	100.0% 100.0%	24% 51%	0.4%	43.0% 27.1%	17.2%	0.01	0.51	0.02	0.00 0.01	0.24	0.10	69.5% 72.6%	0.8%	68.5% 72.6%	10%	1.9%	21.8% 25.7%	12.0%		
12			11		40	0.51		0.01	0.02	0.17	90.0		2.0%	100.0%	2.2%	27%	34.2%	56.2% 34.4%	0.01	633	0.01	4.02	0.12	106	64.8%	1.6%	64.8%	1.8%	12%	24.2% 16.6%	12.4%		
24			13		4.0	2.0		105	0.61	0.84	0.58		14%	100.0%	22%	0.2%	41.0%	282%	0.02	149	0.09	0.01	0.62	0.49	72.6%	1.0%	72.6% 33.5%	126	125	20.1% 16.2%	23.3%		
16			10		10	2.0		102	0.00	160	0.47		0.9%	100.0%	115	26%	29.0%	23.1%	0.01	148	0.02	0.07	0.41	0.27	72.0%	0.7%	72.0%	195	12%	21.0%	18.0%		
17			16	_	4.0	1.7		0.04	0.12	0.47	0.49		1.2%	100.0% 100.0%	2.2% 6.1%	5.9% 0.5%	35.9% 27.0%	21.8% 25.5%	0.02		0.08	0.09	0.32	0.40	67.9% 71.3%	0.6%	67.9% 71.2%	525	5.4%	17.4% 27.5%	56,3% 30,5%		
22			16	\pm	40	2 2.1		0.02	02.0	130	0.56	_	1.7%	100.0%	11%	0.2%	27.8%	23.3%	93.0	1.60	0.02	0.01 0.02	0.53	0.47	71.1%	1.4%	71.1% 72.9%	15%	1.0%	27.4% 25.5%	22.8%		
21		=	20 (28 (29		4.00	1.3		2.04	0.12	0.45	0.27	=	1.2%	160.0% 160.0%	2.2%	245	26.5% 92.9%	21.8%	0.02	1.17	6.03	1.09	0.30	0.29	69.2%	1.1%	61.0%	1.8% 2.4%	165	17.7%	16.2%		
2.2		=	129		4.0	0.31		0.01	0.61	0.15	62.0		2.4%		2.4%	2.2%	30.2% 64.9%	10.0%	0.00	0.14	0.00	0.01	0.11	4.02	69.4% 66.2%	1.9%	66.2%	1.9%	12%	\$1.2% 46.0%	7.7% 6.9%		
25			130		4.0	0.31		4.02	0.00	0.16	62.0		2.4%	100.0% 100.0% 100.0%	1.05	2.0%	77.0% 66.8%	13%	0.00	0.12	0.02	4.00	0.10	0.02	64.2%	2.0% 2.5%	642%	7.4%	2.5% 2.0%	47.5%	7.4%		
26			133	_	4.0	0.40		1.02	0.00	0.13	0.02	_	5.5% 4.0%	100.0%	10.6%	1.5%	30.4%	9.0% 50.1%	10.0	0.12	0.02	4.00	0.09	0.01 0.03	62.8% 72.6%	2.5%	62.8% 72.6%	5.2%	1.5%	44.7% 52.7%	6.5% 7.8%		
29			134	_	4.0	1 0.4		0.01	0.01	0.24	0.00		1.8%	100.0% 100.0%	1.8%	1.0%	59.4% 70.5%	11.8%	0.01		0.01	0.01 0.01	0.36	1.05	75.2% 68.0%	1.4%	75.2% 68.0%	1.6%	1.0% 1.7%	\$2.7% \$2.2%	10.8% 8.9%		
20					40	0.40		0.01	0.01	425	0.06		1.5%	100.0%	1.5%	2.5%	62.7% 67.9%	14.0%	0.01	0.28	0.01	0.01	0.17	0.04	71.2%	1.2%	71.2%	2.85	2.2%	43.4% 52.6%	10.8% 9.5%		
22	K R	nech	122		40			0.01	0.61	0.22	0.06		2.4%	100.0% 100.0%	17%	2.6%	29.2%	122%	0.01		0.61	0.01	0.24	2.04	71.0%	1.9%	71.0% 62.2%	1.4%	24%	54.8% 47.1%	10.1%		
34			140		20	0.61		1.09	60.0	2.47	0.07		8.5%	100.0%	13.7%	6.6%	68.5%	1.0%	0.64	0.51	0.08	403	0.36	0.06	22.6%	6.0%	23.6%	11.7%	3.8%	52.2%	82%		
36			145		100	1.2		4.02	0.61	0.91	0.15		3.7%	100.0%	5.0% 1.7%	1.2%	82.0% 67.2%	15.1%	0.03	9.72	0.66	0.01 0.01	0.65	0.12	73.5%	2.0%	23.5% 23.8%	4.1%	11%	\$4.5% \$4.5%	12.1% 15.7%		
32			144	_	40	1.31	,	0.04	0.05	1.99	0.12	_	3.2% 4.1%	100.0%	15%	3.5% 5.0%	72.2% 88.0%	14.8%	0.64	0.61	0.00	0.04	0.62	0.16	22.6% 63.2%	24%	72.8% 62.4%	2.9%	11%	63.2%	12.0% 8.5%		
29		=	146	==	4.0	0.6		109	0.60	8.70	0.11	=	6.0%	100.0% 100.0%	14%	2.2%	36.1% 77.6%	11.9%	0.04	2.69	0.06	4.02	652	0.09	75.1% 73.1%	4.8%	25.1% 22.1%	1.4%	2.0%	56.1% 63.7%	9.5%		
41			(4)		4.0	1.0		0.04	6.63	8.92	0.23		2.8%	100.0%	2.8%	2.4%	0.2%	16.7%	9.03	102	6.00	4.03	0.68	0.19	74.6%	2.2%	746%	2.1%	21%	41.7% C) 46	12.5%		
42			0 1	9	4.0	0.61		0.02	0.01	0.97	0.12		27% 12%	100.0% 100.0%	2.0%	12% 12%	51.4% 61.4%	17.7%	93.0 13.0	9.44	0.02	0.01	0.27	4.09	62.4%	1.0%	62.4%	2.7%	125 125	32.5% 32.5%	13.2%		
44			2 1	ia i	4.00	0.54		4.03	0.01	6.27	0.03		3.0%	100.0%	2.9% 5.2%	24%	47.4%	142%	0.01	0.30	0.01	0.01 0.01	0.19	0.0%	45.2% 41.8%	2.4%	65.2% 61.8%	2.5% 4.7%	2.0%	23.7%	10.6%		
47			4 1		4.00	2 0.11		403	0.01	0.22	0.12		2.5%	100.0% 100.0%	40%	1.4%	46.6% 41.5%	12.7%	0.01	0.47	0.02	0.01 0.01	0.19	4.07	66.2%	1.8%	64.2% 65.1%	126	12%	22.4% 27.9%	10.2%		
ek			5 1 6 1					4.07	0.01	0.65	0.14		2.2%	100.0%	6.4% 13%	1.2%	59.1% 54.6%	12.5%	90.0		0.06	0.01	0.49	0.10	69.4% 74.6%	2.4%	69.4% 74.0%	5.1%	1.1%	44.5%	9.2%		
50			7 1	is e				4.02	60.0	0.55	0.23		2.4%	100.0%	1.8%	2.4%	46.6% Gr.E.S.	19.8%	0.02		0.02	4.03	0.28	0.18	70.8%	1.8%	71.8%	1.4%	2.2%	32.4%	15.5%		
52					40			104	0.01	2.54	0.22		2.2%	100.0%	15%	1.1%	92.7%	16.2%	0.02	0.00	0.04	0.01 0.01	0.51	0.12	69.5%	1.7%	69.5%	3.0%	11% 5.1%	23.1%	11.9%		
54		╒	10 1	9 3	100	1.50	F	0.02	0.02	0.75	034	-	1.4%	100.0% 100.0%	12%	1.5%	47.8% 57.2%	16.9% 20.0%	9.02	0.72	0.02	4.02	0.52	0.18	69.4%	1.1%	68.6% 61.7%	1.0%	1.2% 2.8%	22.4% 29.0%	12.8% 15.5%		
66			12 1	10 1	0 010	2.7		0.29	0.05	1.55	0.66		4.0% 2.4%	100.0%	10.2%	1.8%	\$7.0% \$8.1%	242%	0.08	202	0.22	0.04 0.03	120	853	74.0%	2.9%	740%	225	16%	44.5% 44.5%	19.5%		
57		=	14 1	12 1	0 10	1 16		0.05	60.0	193	0.94		12%		125	0.7%	50.0%	258%	0.64	2.62	0.64	102	135	0.79	71.6%	1.0%	21.6% 68.9%	1.1%	4.6%	36.8%	21.4%		
				14 1	0 0.11	10		109	0.12	1.66	0.63		2.9%	100.0% 100.0%	25%	22% 54%	C2.6% S0.6%	22.5% 19.2%	90.0	2.04	93.0	0.12	124	0.51	62,2%	1.9% 2.1%	62.2%	2.1%	2.9% 5.1%	27.8%	15.4%		
		=	12 1		0 010	12	-	0.04	0.05	1.91	0.76	-	21% 12%	100.0%	125	1.5%	92.6%	23.3%	0.08		0.18	0.04 0.01	1.67	0.63	71.8%	246	71.8% 71.5%	1.0%	13%	24.9%	19.3% 20.2%		
62			19 1		0 40	4.0		4.07	0.66	2.29	1.02	-	12%	100.0%	17%	12%	S8.4% S1.6%	24.8%	93.0	2.00	0.06	0.04	124	0.84	73,2%	1.8%	222%	126	11%	42.6%	20.5%		
										- 183						-/5		44.575	2.60	2.41	- 24				44/7			-/3		40.55			