# Ossia, Inc. 

TEST REPORT FOR<br>Cota WPT Source<br>Model: Cota Tx203

## Tested to The Following Standards: <br> FCC Part 15 Subpart C Section(s)

15.207 \& 15.247
(DTS 2400-2483.5 MHz)

Report No.: 103895-3

Date of issue: July 8, 2020


This test report bears the accreditation symbol indicating that the testing performed herein meets the test and reporting requirements of ISO/IEC 17025 under the applicable scope of testing for CKC Laboratories, Inc.

We strive to create long-term, trust based relationships by providing sound, adaptive, customer first testing services. We embrace each of our customers' unique EMC challenges, not as an interruption to set processes, but rather as the reason we are in business.

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# ADMINISTRATIVE INFORMATION 

## Test Report Information

## REPORT PREPARED FOR:

Ossa, Inc.
1100 112th Ave NE Suite 301
Bellevue, WA 98004

Representative: Bob McDonald
Customer Reference Number: 13172

DATE OF EQUIPMENT RECEIPT:
DATES) OF TESTING:

REPORT PREPARED BY:

Darcy Thompson
CKC Laboratories, Inc.
5046 Sierra Pines Drive
Mariposa, CA 95338

Project Number: 103895

June 13, 2020
June 13-29, 2020

## Report Authorization

The test data contained in this report documents the observed testing parameters pertaining to and are relevant for only the equipment provided by the client, tested in the agreed upon operational modes) and configurations) as identified herein. Compliance assessment remains the client's responsibility. This report may not be used to claim product endorsement by A2LA or any government agencies. This test report has been authorized for release under quality control from CKC Laboratories, Inc.


Steve Behm
Director of Quality Assurance \& Engineering Services CKC Laboratories, Inc.

## Test Facility Information



Our laboratories are configured to effectively test a wide variety of product types. CKC utilizes first class test equipment, anechoic chambers, data acquisition and information services to create accurate, repeatable and affordable test results.

TEST LOCATION(S):
CKC Laboratories, Inc.
22116 23rd Drive S.E., Suite A
Canyon Park, Bothell, WA 98021

## Software Versions

| CKC Laboratories Proprietary Software | Version |
| :--- | :---: |
| EMITest Emissions | 5.03 .12 |

## Site Registration \& Accreditation Information

| Location | *NIST CB \# | FCC | Japan |
| :---: | :---: | :---: | :---: |
| Canyon Park, Bothell, WA | US0081 | US1022 | A-0136 |
| Brea, CA | US0060 | US1025 | A-0136 |
| Fremont, CA | US0082 | US1023 | A-0136 |
| Mariposa, CA | US0103 | US1024 | A-0136 |

*CKC's list of NIST designated countries can be found at: https://standards.gov/cabs/designations.html

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## SUMMARY OF RESULTS

Standard / Specification: FCC Part 15 Subpart C - 15.247 (DTS)

| Test Procedure | Description | Modifications | Results |
| :--- | :--- | :--- | :--- |
| $15.247(\mathrm{a})(2)$ | 6dB Bandwidth | NA | Pass |
| $15.247(\mathrm{~b})(3)$ | Output Power | NA | Pass |
| $15.247(\mathrm{e})$ | Power Spectral Density | NA | Pass |
| $15.247(\mathrm{~d})$ | RF Conducted Emissions \& Band Edge | NA | Pass |
| $15.247(\mathrm{~d})$ | Radiated Emissions \& Band Edge | NA | Pass |
| 15.207 | AC Conducted Emissions | NA | Pass |

NA = Not Applicable

## ISO/IEC 17025 Decision Rule

The declaration of pass or fail herein is based upon assessment to the specification(s) listed above, including where applicable, assessment of measurement uncertainties. For performance related tests, equipment was monitored for specified criteria identified in that section of testing.

## Modifications During Testing

This list is a summary of the modifications made to the equipment during testing.

## Summary of Conditions

No modifications were made during testing.

Modifications listed above must be incorporated into all production units.

## Conditions During Testing

This list is a summary of the conditions noted to the equipment during testing.

## Summary of Conditions

None

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## EQUIPMENT UNDER TEST (EXT)

During testing, numerous configurations may have been utilized. The configurations listed below support compliance to the standards) listed in the Summary of Results section.

## Configuration 1

Equipment Tested:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Cora WPT Source | Usia, Inc. | Cota Tx203 | OR-001 |

Support Equipment:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| USB 2.0 Extension Cable | Blue Rigger | $32 \mathrm{ft}(10 \mathrm{~m})$ | NA |
| AC Adapter (for PoE Injector) | GlobTek, Inc. | GTM961808P18054-T3 | NA |
| PoE Injector | Usia, Inc. | OL-10282 | NA |
| Laptop | Apple | MacBook Pro A1398 | NA |
| USB Hub | AmazonBasics | B00DQFGJR4 | NA |
| Thunderbolt to Ethernet adapter | Apple | A1433 | NA |

## Configuration 2

Equipment Tested:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Cora WPT Source | Usia, Inc. | Cota Tx203 | OR-001 |

Support Equipment:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| USB 2.0 Extension Cable | Blue Rigger | $32 \mathrm{ft}(10 \mathrm{~m})$ | NA |
| AC/DC Switching Adapter | Mean Well | GST220A12 | NA |
| Laptop | Apple | MacBook Pro A1398 | NA |
| USB Hub | AmazonBasics | BOODQFGJR4 | NA |
| Thunderbolt to Ethernet adapter | Apple | A1433 | NA |

## General Product Information:

| Product Information | Manufacturer-Provided Details |
| :---: | :---: |
| Equipment Type: | Stand-Alone Equipment |
| Type of Wideband System: | Zigbee 802.15.4 |
| Operating Frequency Range: | $2405-2480 \mathrm{MHz}$ |
| Modulation Types): | OQPSK |
| Maximum Duty Cycle: | $100 \%$ tested as worst case |
| Number of TX Chains: | 1 |
| Antenna Types) and Gain: | External Dipole 2dBi |
| Beamforming Type: | NA |
| Antenna Connection Type: | External Connector |
| Nominal Input Voltage: | $120 \mathrm{VAC}, 60 \mathrm{~Hz}$ |
| Firmware / Software used for Test: | 0x2524CF1 |

Block Diagram of Test Setup(s)

Configuration 1
Test Setup Block Diagram


## Configuration 2

Test Setup Block Diagram


## FCC Part 15 Subpart C

### 15.247(a)(2) 6dB Bandwidth

| Test Setup/Conditions |  |  |  |
| :--- | :--- | :--- | :--- |
| Test Location: | Bothell Lab C3 | Test Engineer: | S. Pittsford |
| Test Method: | ANSI C63.10 (2013) <br> KDB 558074 (April 2, 2019) | Test Date(s): | $6 / 13 / 2020$ |
| Configuration: | 2 | Test Mode: Continuously Modulated. <br> The EUT's antenna port is connected directly to the spectrum analyzer through a RF cable <br> and an attenuator. |  |
| Test Setup: |  |  |  |


| Environmental Conditions |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Temperature (ㅇ) | 22 | Relative Humidity (\%): | 38 |  |


| Test Equipment |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Asset\# | Description | Manufacturer | Model | Cal Date | Cal Due |
| P06243 | Attenuator | Weinschel | $54 A-10$ | $1 / 27 / 2020$ | $1 / 27 / 2022$ |
| P06678 | Cable | Astrolab | $32026-29801-29801-144$ | $2 / 20 / 2020$ | $2 / 20 / 2022$ |
| 02673 | Spectrum Analyzer | Agilent | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |


| Test Data Summary |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Frequency <br> $(\mathbf{M H z})$ | Antenna <br> Port | Modulation | Measured <br> $\mathbf{( k H z )}$ | Limit <br> $\mathbf{( k H z )}$ | Results |
| 2405 | 1 | OQPSK | 1612 | $\geq 500$ | Pass |
| 2440 | 1 | OQPSK | 1505 | $\geq 500$ | Pass |
| 2480 | 1 | OQPSK | 1599 | $\geq 500$ | Pass |

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## Plot (s)

| Agilent |
| :--- |
| Ref 10 dBm <br> Peak <br> Log <br> 10 <br> dB |

Low Channel


Middle Channel


High Channel

Test Setup Photo(s)


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### 15.247(b)(3) Output Power

| Test Setup / Conditions |  |  |  |
| :--- | :--- | :--- | :--- |
| Test Location: | Bothell Lab C3 | Test Engineer: | S. Pittsford |
| Test Method: | ANSI C63.10 (2013) <br> KDB 558074 (April 2, 2019) | Test Date(s): | $6 / 13 / 2020$ |
| Configuration: | 2 | Test Mode: Continuously Modulated. <br> The EUT's antenna port is connected directly to the spectrum analyzer through a RF cable <br> and an attenuator. <br> Test Setup: <br> System losses are corrected for internal to the spectrum analyzer. <br> No change in power observed at extreme voltages. |  |


| Environmental Conditions |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Temperature (ㅇ) | 22 | Relative Humidity (\%): | 38 |  |


| Test Equipment |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Asset\# | Description | Manufacturer | Model | Cal Date | Cal Due |  |
| P06243 | Attenuator | Weinschel | $54 A-10$ | $1 / 27 / 2020$ | $1 / 27 / 2022$ |  |
| P06678 | Cable | Astrolab | $32026-29801-29801-144$ | $2 / 20 / 2020$ | $2 / 20 / 2022$ |  |
| 02673 | Spectrum Analyzer | Agilent | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |  |


| Test Data Summary - Voltage Variations |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Frequency <br> $(\mathbf{M H z})$ | Modulation / Ant Port | $\mathbf{V}_{\text {Minimum }}$ <br> $(\mathbf{d B m})$ | $\mathbf{V}_{\text {Nominal }}$ <br> $(\mathbf{d B m})$ | $\mathbf{V}_{\text {Maximum }}$ <br> $(\mathrm{dBm})$ | Max Deviation <br> from $\mathbf{V}_{\text {Nominal }}(\mathbf{d B})$ |
| 2405 | OQPSK | 3.69 | 3.69 | 3.69 | 0.00 |
| 2440 | OQPSK | 3.42 | 3.42 | 3.42 | 0.00 |
| 2480 | OQPSK | 2.91 | 2.91 | 2.91 | 0.00 |

Test performed using operational mode with the highest output power, representing worst case.

## Parameter Definitions:

Measurements performed at input voltage Vnominal $\pm 15 \%$.

| Parameter | Value |
| :--- | :--- |
| $\mathrm{V}_{\text {Nominal }}:$ | 85 Vrms |
| $\mathrm{V}_{\text {Minimum: }}:$ | 120 Vrms |
| $\mathrm{V}_{\text {Maximum: }}:$ | 276 Vrms |

## Power Output Test Data Summary - RF Conducted Measurement

Measurement Option: RBW > DTS Bandwidth

| Frequency <br> $(\mathbf{M H z})$ | Modulation | Ant. Type / <br> Gain $(\mathbf{d B i})$ | Measured <br> $(\mathbf{d B m})$ | Limit <br> $(\mathbf{d B m})$ | Results |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 2405 | OQPSK | Dipole 2dBi | 3.69 | $\leq 30$ | Pass |
| 2440 | OQPSK | Dipole 2 dBi | 3.42 | $\leq 30$ | Pass |
| 2480 | OQPSK | Dipole 2dBi | 2.91 | $\leq 30$ | Pass |

Plots


Low Channel

| Agilent |
| :--- |
| Ref 10 dBm <br> Peak <br> Log <br> 10 <br> dB 7 |

Middle Channel

| Agilent |
| :--- |
| Ref 10 dBm <br> FPeak <br> Log <br> 10 <br> dB7 |

High Channel

Test Setup Photo(s)


LABORATORIES, INC.

### 15.247(e) Power Spectral Density

| Test Setup / Conditions / Data |  |  |  |
| :--- | :--- | :--- | :--- |
| Test Location: | Bothell Lab C3 | Test Engineer: | S. Pittsford |
| Test Method: | ANSI C63.10 (2013) <br> KDB 558074 (April 2, 2019) | Test Dates): | $6 / 13 / 2020$ |
| Configuration: | 2 | Test Mode: Continuously Modulated. <br> The EUT's antenna port is connected directly to the spectrum analyzer through a RF cable <br> and an attenuator. |  |
| Test Setup: | System losses are corrected for internal to the spectrum analyzer. |  |  |


| Environmental Conditions |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Temperature (ㅇ) | 22 | Relative Humidity (\%): | 38 |  |


| Test Equipment |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Asset\# | Description | Manufacturer | Model | Cal Date | Cal Due |
| P06243 | Attenuator | Weinschel | $54 A-10$ | $1 / 27 / 2020$ | $1 / 27 / 2022$ |
| P06678 | Cable | Astrolab | $32026-29801-29801-144$ | $2 / 20 / 2020$ | $2 / 20 / 2022$ |
| 02673 | Spectrum Analyzer | Agilent | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |

## PSD Test Data Summary - RF Conducted Measurement

Measurement Method: PKPSD

| Frequency <br> $(\mathbf{M H z})$ | Modulation | Measured <br> $(\mathbf{d B m} / \mathbf{3 k H z})$ | Limit <br> $(\mathbf{d B m} / \mathbf{3 k H z})$ | Results |
| :---: | :---: | :---: | :---: | :---: |
| 2405 | OQPSK | -6.61 | $\leq 8$ | Pass |
| 2440 | OQPSK | -6.73 | $\leq 8$ | Pass |
| 2480 | OQPSK | -7.23 | $\leq 8$ | Pass |

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Plots


Low Channel


Middle Channel

| Agilent |
| :--- |
| Ref 10 dBm <br> FPeak <br> Log <br> 10 <br> dB7 |

High Channel

Test Setup Photo(s)


LABORATORIES, INC.

### 15.247(d) RF Conducted Emissions \& Band Edge

## Test Setup / Conditions / Data

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)

Customer:
Specification: Work Order \#: Test Type: Tested By: Software:

Usia, Inc.
15.247(d) Conducted Spurious Emissions 102446
Conducted Emissions
Steven Pittsford
EMITest 5.03.19

Date: 6/13/2020
Time: 09:00:20
Sequence\#: 1
115 V 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Test Conditions / Notes:

Test Mode: Continuously Modulated
EUT is transmitting on Low channel
The EUT's antenna port is connected directly to the spectrum analyzer through a RF cable and an attenuator.

Ossia, Inc. WO\#: 102446 Sequence\#: 1 Date: 6/13/2020
15.247 (d) Conducted Spurious Emissions High Test Lead: 115 V 60 Hz Antenna


Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | ANP06243 | Attenuator | $54 A-10$ | $1 / 27 / 2020$ | $1 / 27 / 2022$ |
| T2 | ANP06678 | Cable | $32026-29801-$ | $2 / 20 / 2020$ | $2 / 20 / 2022$ |
|  |  |  | $29801-144$ |  |  |
|  | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |


| Measurement Data: | Reading listed by margin. |  |  |  |  | Test Lead: Antenna |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \#Freq <br>  <br>  <br> MHz | $\begin{aligned} & \text { Rdng } \\ & \mathrm{dB} \mu \mathrm{~V} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | dB | dB | $\begin{gathered} \hline \text { Dist } \\ \text { Table } \end{gathered}$ | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} \end{gathered}$ | Spec $\mathrm{dB} \mu \mathrm{V}$ | $\begin{gathered} \text { Margin } \\ \mathrm{dB} \end{gathered}$ | Polar <br> Ant |
| $\begin{array}{cc} 1 & 24973.811 \\ & M \end{array}$ | 44.8 | +10.0 | +10.0 |  |  | +0.0 | 64.8 | 85.5 | -20.7 | Anten |
| $\begin{array}{cc} 2 & 23598.910 \\ M \end{array}$ | 43.0 | +10.2 | +9.7 |  |  | +0.0 | 62.9 | 85.5 | -22.6 | Anten |
| $\begin{array}{cc} 3 & 23520.345 \\ M \end{array}$ | 42.6 | +10.2 | +9.7 |  |  | +0.0 | 62.5 | 85.5 | -23.0 | Anten |
| $\begin{array}{cc} \hline 4 & 23206.082 \\ M \end{array}$ | 42.4 | +10.1 | +9.6 |  |  | +0.0 | 62.1 | 85.5 | -23.4 | Anten |
| $\begin{array}{cc} 5 & 23376.307 \\ M \end{array}$ | 42.2 | +10.2 | +9.7 |  |  | +0.0 | 62.1 | 85.5 | -23.4 | Anten |
| $\begin{array}{cc} \hline 6 & 24253.625 \\ M \end{array}$ | 41.8 | +10.0 | +9.9 |  |  | +0.0 | 61.7 | 85.5 | -23.8 | Anten |
| $\begin{array}{cc} \hline 7 & 24109.588 \\ M \end{array}$ | 41.9 | +10.0 | +9.8 |  |  | +0.0 | 61.7 | 85.5 | -23.8 | Anten |
| 84808.955 M | 48.0 | +9.8 | +3.8 |  |  | +0.0 | 61.6 | 85.5 | -23.9 | Anten |
| $\begin{array}{cc} \hline 9 & 24607.171 \\ M \end{array}$ | 41.1 | +10.0 | +10.0 |  |  | +0.0 | 61.1 | 85.5 | -24.4 | Anten |
| $\begin{array}{cc} \hline 10 & 24384.568 \\ & M \end{array}$ | 41.2 | +10.0 | +9.9 |  |  | +0.0 | 61.1 | 85.5 | -24.4 | Anten |
| $\begin{array}{cc} \hline 11 & 23886.985 \\ & M \end{array}$ | 41.1 | +10.0 | +9.7 |  |  | +0.0 | 60.8 | 85.5 | -24.7 | Anten |
| $\begin{array}{cc} 12 & 21516.918 \\ & M \end{array}$ | 41.2 | +10.2 | +9.2 |  |  | +0.0 | 60.6 | 85.5 | -24.9 | Anten |

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bethel, WA 98021 • 1-800-500-4EMC (4362)

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Usia, Inc.
15.247(d) Conducted Spurious Emissions

102446
Conducted Emissions
Steven Pittsford
EMIT est 5.03.19

Date: 6/13/2020
Time: 09:24:57
Sequence\#: 3
115 V 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Test Mode: Continuously Modulated
EUT is transmitting on Mid channel
The EUT's antenna port is connected directly to the spectrum analyzer through a RF cable and an attenuator.

Ossia, Inc. WO\#: 102446 Sequence\#: 3 Date: 6/13/2020
15.247 (d) Conducted Spurious Emissions High Test Lead: 115 V 60 Hz Antenna


|  | Sweep Data | - Readings |
| :--- | :--- | :--- |
| - | Peak Readings | $\times$ |
| QP Readings |  |  |
| * Average Readings | Ambient |  |
| Software Version: 5.03 .19 |  | $1-15.247$ (d) Conducted Spurious Emissions |

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | ANP06243 | Attenuator | $54 A-10$ | $1 / 27 / 2020$ | $1 / 27 / 2022$ |
| T2 | ANP06678 | Cable | $32026-29801-$ | $2 / 20 / 2020$ | $2 / 20 / 2022$ |
|  |  |  | $29801-144$ |  |  |
|  | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |


| Measu | rement Data: | Reading listed by margin. |  |  |  | Test Lead: Antenna |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | Freq MHz | $\begin{aligned} & \mathrm{Rdng} \\ & \mathrm{~dB} \mu \mathrm{~V} \end{aligned}$ | $\begin{aligned} & \hline \text { T1 } \\ & \text { dB } \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | dB | dB | $\begin{gathered} \hline \text { Dist } \\ \text { Table } \end{gathered}$ | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} \\ \hline \end{gathered}$ | Margin <br> dB | Polar Ant |
|  | $\begin{gathered} 24895.246 \\ \text { M } \end{gathered}$ | 44.9 | +10.0 | +10.0 |  |  | +0.0 | 64.9 | 85.5 | -20.6 | Anten |
|  | $\begin{gathered} 23677.476 \\ \mathrm{M} \end{gathered}$ | 43.8 | +10.1 | +9.7 |  |  | +0.0 | 63.6 | 85.5 | -21.9 | Anten |
|  | $\begin{gathered} 23546.533 \\ \mathrm{M} \end{gathered}$ | 43.3 | +10.2 | +9.7 |  |  | +0.0 | 63.2 | 85.5 | -22.3 | Anten |
|  | $\begin{gathered} 23926.268 \\ \text { M } \end{gathered}$ | 43.5 | +10.0 | +9.7 |  |  | +0.0 | 63.2 | 85.5 | -22.3 | Anten |
|  | $\begin{gathered} 23271.553 \\ \mathrm{M} \end{gathered}$ | 43.3 | +10.1 | +9.6 |  |  | +0.0 | 63.0 | 85.5 | -22.5 | Anten |
|  | $\begin{gathered} 23454.873 \\ \mathrm{M} \end{gathered}$ | 43.0 | +10.2 | +9.7 |  |  | +0.0 | 62.9 | 85.5 | -22.6 | Anten |
|  | $\begin{gathered} 23402.496 \\ \mathrm{M} \end{gathered}$ | 42.8 | +10.2 | +9.7 |  |  | $+0.0$ | 62.7 | 85.5 | -22.8 | Anten |
|  | $\begin{gathered} 24135.777 \\ \mathrm{M} \end{gathered}$ | 42.4 | +10.0 | +9.8 |  |  | +0.0 | 62.2 | 85.5 | -23.3 | Anten |
| 9 | 4878.960M | 47.3 | +9.8 | +3.9 |  |  | +0.0 | 61.0 | 85.5 | -24.5 | Anten |

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bethel, WA 98021 • 1-800-500-4EMC (4362)

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Usia, Inc.
15.247(d) Conducted Spurious Emissions

102446
Conducted Emissions
Steven Pittsford
EMIT est 5.03.19

Date: 6/13/2020
Time: 09:15:30
Sequence\#: 2
115 V 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Test Mode: Continuously Modulated
EUT is transmitting on High channel
The EUT's antenna port is connected directly to the spectrum analyzer through a RF cable and an attenuator.

Ossia, Inc. WO\#: 102446 Sequence\#: 2 Date: 6/13/2020
15.247 (d) Conducted Spurious Emissions High Test Lead: 115 V 60 Hz Antenna


Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | ANP06243 | Attenuator | $54 A-10$ | $1 / 27 / 2020$ | $1 / 27 / 2022$ |
| T2 | ANP06678 | Cable | $32026-29801-$ | $2 / 20 / 2020$ | $2 / 20 / 2022$ |
|  |  |  | $29801-144$ |  |  |
|  | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |


| Measurement Data: | Reading listed by margin. |  |  |  |  | Test Lead: Antenna |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# $\quad$Freq <br>  <br>  <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | dB | dB | Dist <br> Table | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} \end{gathered}$ | $\begin{gathered} \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} \end{gathered}$ | $\begin{gathered} \text { Margin } \\ \mathrm{dB} \end{gathered}$ | Polar <br> Ant |
| $\begin{array}{cc} 1 & 24986.906 \\ \text { M } \end{array}$ | 44.9 | +10.0 | +10.0 |  |  | +0.0 | 64.9 | 85.5 | -20.6 | Anten |
| $\begin{array}{cc} 2 & 24842.868 \\ & M \end{array}$ | 44.0 | +10.0 | +10.0 |  |  | +0.0 | 64.0 | 85.5 | -21.5 | Anten |
| 3 2483.754M | 51.2 | +9.8 | +2.7 |  |  | +0.0 | 63.7 | 85.5 | -21.8 | Anten |
| $\begin{array}{cc} 4 & 23598.910 \\ M \end{array}$ | 43.5 | +10.2 | +9.7 |  |  | +0.0 | 63.4 | 85.5 | -22.1 | Anten |
| $\begin{array}{cc} 5 & 24109.588 \\ M \end{array}$ | 42.6 | +10.0 | +9.8 |  |  | +0.0 | 62.4 | 85.5 | -23.1 | Anten |
| $\begin{array}{cc} \hline 6 & 24371.474 \\ M \end{array}$ | 41.9 | +10.0 | +9.9 |  |  | +0.0 | 61.8 | 85.5 | -23.7 | Anten |
| $\begin{array}{cc} \hline 7 & 21516.918 \\ M \end{array}$ | 41.3 | +10.2 | +9.2 |  |  | $+0.0$ | 60.7 | 85.5 | -24.8 | Anten |
| $\begin{array}{cc} 8 & 14406.716 \\ M \end{array}$ | 43.2 | +10.0 | +7.3 |  |  | +0.0 | 60.5 | 85.5 | $-25.0$ | Anten |
| $\begin{array}{cc} \hline 9 & 21372.880 \\ & M \end{array}$ | 41.2 | +10.1 | +9.2 |  |  | +0.0 | 60.5 | 85.5 | $-25.0$ | Anten |
| $10 \quad 4958.955 \mathrm{M}$ | 46.4 | +9.8 | +4.0 |  |  | +0.0 | 60.2 | 85.5 | -25.3 | Anten |
| $\begin{array}{cc} 11 & 22590.650 \\ & M \end{array}$ | 40.8 | +10.0 | +9.3 |  |  | +0.0 | 60.1 | 85.5 | -25.4 | Anten |
| $\begin{array}{cc} 12 & 20822.920 \\ & M \end{array}$ | 40.7 | +10.0 | +9.3 |  |  | $+0.0$ | 60.0 | 85.5 | $-25.5$ | Anten |

Band Edge

| Band Edge Summary |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Limit applied: Max Power/100kHz - 20dB. |  |  |  |  |  |
| Frequency <br> $(\mathrm{MHz})$ | Modulation | Measured <br> $(\mathrm{dB} \mu \mathrm{V})$ | Limit <br> $(\mathrm{dB} \mu \mathrm{V})$ | Results |  |
| 2400.0 |  | 56.8 | $<85.5$ | Pass |  |
| 2483.5 | OQPSK | 57.9 | $<85.5$ | Pass |  |

## Band Edge Plots




## Test Setup / Conditions / Data

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Usia, Inc.
15.247(d) Conducted Spurious Emissions High

102446
Conducted Emissions
Steven Pittsford
EMIT est 5.03.12

Date: 6/13/2020
Time: 09:08:11
Sequence\#: 2
115 V 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Test Conditions / Notes:

Test Mode: Continuously Modulated
EUT is transmitting on Low channel.
The EUT's antenna port is connected directly to the spectrum analyzer through a RF cable and an attenuator.
Test Location: Bothell Lab C3
Test Method: ANSI C63.10 (2013) KDB 558074 (April 2, 2019)
Temperature $\left({ }^{\circ} \mathrm{C}\right) 22$
Relative Humidity (\%): 38

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | ANP06243 | Attenuator | 54 A-10 | $1 / 27 / 2020$ | $1 / 27 / 2022$ |
| T2 | ANP06678 | Cable | $32026-29801-29801-144$ | $2 / 20 / 2020$ | $2 / 20 / 2022$ |
|  | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |



Test Setup Photo(s)


### 15.247(d) Radiated Emissions \& Band Edge

## Test Setup / Conditions / Data

Test Location: Customer: Specification: Work Order \#: Test Type: Tested By: Software:

CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362) Usia, Inc.
15.247(d) / 15.209 Radiated Spurious Emissions 103895 Date: 6/15/2020
Maximized Emissions
S. Pittsford/M. Atkinson

EMIT est 5.03.12

Time: 09:05:56
Sequence\#: 4

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Test Conditions / Notes:

Frequency range tested: $9 \mathrm{kHz}-25 \mathrm{GHz}$
Test Mode: Continuously Modulated
EUT is on a 0.8 m test bench below 1 GHz and a 1.5 m high Styrofoam test bench above 1 GHz .

EUT is investigated in Low, Middle, and High Channels, X, Y, \& Z Axis with only the worst case reported.
Vertical and Horizontal polarities investigated
EUT connected to support Laptop via USB cable.

No emissions observed within 20dB of limit from $18-25 \mathrm{GHz}$, values provided are noise floor.
EUT connected to AC adapter for power.
EUT connected to support Laptop via Ethernet cable.
Laptop is located remotely.

Test Location: Bothell Lab C3
Test Method: ANSI C63.10 (2013) KDB 558074 (April 2, 2019)
Temperature $\left({ }^{\circ} \mathrm{C}\right) 23$
Relative Humidity (\%): 33

Ossia, Inc. WO\#: 103895 Sequence\#\#: 4 Date: 6/15/2020
15.247 (d) / 15.209 Radiated Spurious Emissions Test Distance: 3 Meters Ground Para


[^0]O Peak Readings

* Average Readings

Software Version: 5.03.12

Test Equipment:

| ID | Asset \# | Description | Model | Calibration <br> Date | Cal Due <br> Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |
| T2 | ANP06540 | Cable | Heliax | $8 / 23 / 2019$ | $8 / 23 / 2021$ |
| T3 | ANP05305 | Cable | ETSI-50T | $9 / 6 / 2019$ | $9 / 6 / 2021$ |
| T4 | AN02307 | Preamp | $8447 D$ | $1 / 10 / 2020$ | $1 / 10 / 2022$ |
| T5 | ANP05360 | Cable | RG214 | $2 / 3 / 2020$ | $2 / 3 / 2022$ |
| T6 | ANP06123 | Attenuator | 18N-6 | $4 / 5 / 2019$ | $4 / 5 / 2021$ |
| T7 | AN03628 | Biconilog Antenna | $3142 E$ | $6 / 11 / 2019$ | $6 / 11 / 2021$ |
| T8 | AN03540 | Preamp | $83017 A$ | $5 / 13 / 2019$ | $5 / 13 / 2021$ |
| T9 | AN01467 | Horn Antenna-ANSI C63.5 | 3115 | $7 / 5 / 2019$ | $7 / 5 / 2021$ |
| T10 | ANP06515 | Calibration | Heliax | $6 / 29 / 2018$ | $6 / 29 / 2020$ |
| T11 | ANP07504 | Cable | CLU40-KMKM-02.00F | $1 / 17 / 2019$ | $1 / 17 / 2021$ |
| T12 | AN03116 | High Pass Filter | 11SH10-00313 | $1 / 22 / 2019$ | $1 / 22 / 2021$ |
| T13 | AN02741 | Active Horn Antenna | AMFW-5F-12001800-20-10P | $4 / 26 / 2019$ | $4 / 26 / 2021$ |
| T14 | AN02742 | Active Horn Antenna | AMFW-5F-18002650-20-10P | $10 / 16 / 2018$ | $10 / 16 / 2020$ |
| T15 | ANP06678 | Cable | $32026-29801-29801-144$ | $2 / 20 / 2020$ | $2 / 20 / 2022$ |
| T16 | AN02763-69 | Waveguide | Multiple | $4 / 28 / 2020$ | $4 / 28 / 2022$ |
| T17 | ANP07212 | Cable | $32026-29801-29801-18$ | $8 / 7 / 2019$ | $8 / 7 / 2021$ |
| T18 | ANP07211 | Cable | $32026-29801-29801-18$ | $8 / 7 / 2019$ | $8 / 7 / 2021$ |
| T19 | AN00052 | Loop Antenna | 6502 | $5 / 4 / 2020$ | $5 / 4 / 2022$ |

Measurement Data: $\quad$ Reading listed by margin. Test Distance: 3 Meters


| 4 4961.090M | 44.3 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.6 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.9 \\ & +0.0 \\ & +4.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -3.6 \\ +0.5 \\ +0.0 \end{array}$ | +0.0 |  | $\begin{array}{r} 54.0 \\ \operatorname{High} \text { Z } \end{array}$ | -4.7 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{cc} 5 & 12202.620 \\ \mathrm{M} \end{array}$ | 53.7 | $\begin{array}{r} \hline+0.0 \\ +0.0 \\ +0.0 \\ -12.8 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.4 \\ & +0.0 \\ & +6.9 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 49.2 | 54.0 Mid Y | -4.8 | Horiz |
| 6 4958.950M | 44.2 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.6 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +4.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.5 \\ +0.0 \end{array}$ | +0.0 | 49.2 | $\begin{gathered} 54.0 \\ \text { High Y } \end{gathered}$ | -4.8 | Horiz |
| $\begin{gathered} 7 \text { 4878.970M } \\ \text { Ave } \end{gathered}$ | 43.7 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.5 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +4.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.6 \\ +0.0 \end{array}$ | +0.0 | 48.8 | $\begin{gathered} 54.0 \\ \operatorname{Mid} Z \end{gathered}$ | -5.2 | Horiz |
| $\begin{aligned} & \hline 8 \text { 4878.886M } \\ & \text { Ave } \end{aligned}$ | 44.3 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.5 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +4.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 48.8 | $\begin{gathered} \quad 54.0 \\ \operatorname{Mid} X \end{gathered}$ | -5.2 | $\begin{gathered} \hline \text { Vert } \\ 201 \end{gathered}$ |
| ^ 4878.860M | 50.9 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.5 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.9 \\ & +0.0 \\ & +4.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 55.4 | $\begin{gathered} 54.0 \\ \operatorname{Mid} X \end{gathered}$ | +1.4 | $\begin{gathered} \hline \text { Vert } \\ 201 \end{gathered}$ |
| 10 4880.890M | 43.5 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.5 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +4.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.5 \\ +0.0 \end{array}$ | +0.0 | 48.5 | $\begin{gathered} \quad 54.0 \\ \operatorname{Mid} \mathrm{Y} \end{gathered}$ | -5.5 | Vert |
| 11 4808.930M | 43.3 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.4 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +4.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{gathered} \hline+0.0 \\ -33.6 \\ +0.6 \\ +0.0 \end{gathered}$ | +0.0 | 48.3 | $\begin{gathered} \quad 54.0 \\ \text { Low } \mathrm{Z} \end{gathered}$ | -5.7 | Vert |
| $\begin{aligned} & 12 \text { 4879.016M } \\ & \text { Ave } \end{aligned}$ | 42.3 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.5 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +4.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.6 \\ +0.0 \end{array}$ | +0.0 | 47.4 | $\begin{gathered} 54.0 \\ \operatorname{Mid} Y \end{gathered}$ | -6.6 | Horiz |
| ^ 4879.010M | 49.4 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.5 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.0 \\ & \hline+0.9 \\ & +0.0 \\ & +4.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.6 \\ +0.0 \end{array}$ | +0.0 | 54.5 | $\begin{gathered} \quad 54.0 \\ \operatorname{Mid} \mathrm{Z} \end{gathered}$ | +0.5 | Horiz |

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| $\wedge$ | 4879.054M | 48.8 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.5 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +4.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.6 \\ +0.0 \end{array}$ | +0.0 |  | $\begin{gathered} 54.0 \\ \operatorname{Mid} \mathrm{Y} \end{gathered}$ | -0.1 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 4879.040M | 41.3 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.5 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +4.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.6 \\ +0.0 \end{array}$ | +0.0 | 46.4 | $\begin{gathered} \quad 54.0 \\ \operatorname{Mid} Z \end{gathered}$ | -7.6 | Horiz |
| 16 | 4958.980M | 41.3 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.6 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +4.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.5 \\ +0.0 \end{array}$ | +0.0 | 46.3 | $\begin{gathered} 54.0 \\ \text { High Y } \end{gathered}$ | -7.7 | Vert |
| 17 | 4809.080M | 40.9 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.4 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +4.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.6 \\ +0.0 \end{array}$ | +0.0 | 45.9 | $\begin{gathered} 54.0 \\ \text { Low } \mathrm{Y} \end{gathered}$ | -8.1 | Vert |
| 18 | 4958.940M | 40.3 | $\begin{array}{r} +0.0 \\ +3.0 \\ +32.6 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +4.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.4 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} \hline+0.0 \\ -3.6 \\ +0.5 \\ +0.0 \end{array}$ | +0.0 | 45.3 | $\begin{gathered} 54.0 \\ \operatorname{High} Z \end{gathered}$ | -8.7 | Vert |
| 19 | $\begin{aligned} & \hline 4810.952 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 40.8 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.4 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +4.1 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 45.2 | $\begin{gathered} 54.0 \\ \text { Low X } \end{gathered}$ | -8.8 | $\begin{gathered} \hline \text { Vert } \\ 223 \end{gathered}$ |
| $\wedge$ | 4810.952M | 48.6 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.4 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +4.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 53.0 | $\begin{gathered} 54.0 \\ \text { Low X } \end{gathered}$ | -1.0 | $\begin{gathered} \hline \text { Vert } \\ 223 \end{gathered}$ |
| 21 | $\begin{aligned} & \hline 12022.420 \\ & \text { M } \\ & \text { Ave } \end{aligned}$ | 48.8 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ +13.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +1.4 \\ & +0.0 \\ & +6.8 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 44.0 | 54.0 Low Y | -10.0 | Horiz |
| 22 | $\begin{gathered} 12397.400 \\ \mathrm{M} \end{gathered}$ | 48.2 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +13.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +1.5 \\ & +0.0 \\ & +7.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 43.7 | $\begin{array}{r} \hline 54.0 \\ \text { High Z } \end{array}$ | -10.3 | Vert |
| 23 | $\begin{aligned} & \hline 12397.480 \\ & \text { M } \\ & \text { Ave } \end{aligned}$ | 48.0 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -13.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +1.5 \\ & +0.0 \\ & +7.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 43.5 | $\begin{array}{r} \hline 54.0 \\ \text { High Z } \end{array}$ | -10.5 | Horiz |


|  | $\begin{aligned} & \hline 12202.427 \\ & \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 46.8 | $\begin{gathered} +0.0 \\ +0.0 \\ +0.0 \\ -12.8 \\ +0.0 \end{gathered}$ | $\begin{aligned} & \hline+1.4 \\ & +0.0 \\ & +6.9 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 42.3 | 54.0 id Z | -11.7 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | 1378.000M | 50.1 | $\begin{array}{r} +0.0 \\ +0.0 \\ +25.1 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.5 \\ & +0.0 \\ & +2.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{gathered} \hline+0.0 \\ -35.6 \\ +0.0 \\ +0.0 \end{gathered}$ | +0.0 | 42.3 | 54.0 | -11.7 | Horiz |
| 26 | $\begin{aligned} & \hline 12397.480 \\ & \text { M } \\ & \text { Ave } \end{aligned}$ | 46.7 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & -13.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+1.5 \\ & +0.0 \\ & +7.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 42.2 | $\begin{array}{r} \hline 54.0 \\ \text { igh Y } \end{array}$ | -11.8 | Horiz |
| $\wedge$ | $\begin{gathered} \hline 12397.480 \\ \mathrm{M} \end{gathered}$ | 54.9 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & -13.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+1.5 \\ & +0.0 \\ & +7.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 50.4 | $\begin{gathered} \hline 54.0 \\ \text { igh Z } \end{gathered}$ | -3.6 | Horiz |
|  | $\begin{gathered} 12397.480 \\ \mathrm{M} \end{gathered}$ | 53.8 | $\begin{array}{r} \hline+0.0 \\ +0.0 \\ +0.0 \\ -13.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +1.5 \\ & +0.0 \\ & +7.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 49.3 | $\begin{array}{r} \hline 54.0 \\ \text { igh Y } \end{array}$ | -4.7 | Horiz |
| 29 | 1375.000M | 49.9 | $\begin{array}{r} +0.0 \\ +0.0 \\ +25.1 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.5 \\ & +0.0 \\ & +2.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -35.7 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 42.0 | 54.0 | -12.0 | Horiz |
| 30 | $\begin{aligned} & \text { 4960.852M } \\ & \text { Ave } \end{aligned}$ | 37.3 | $\begin{array}{r} +0.0 \\ +0.0 \\ +3.6 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +4.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -3.6 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 41.8 | $\begin{gathered} 54.0 \\ \text { igh } X \end{gathered}$ | -12.2 | $\begin{array}{r} \hline \text { Vert } \\ 181 \end{array}$ |
| $\wedge$ | 4960.852M | 47.5 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.6 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +4.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 52.0 | $\begin{gathered} 54.0 \\ \text { igh X } \end{gathered}$ | -2.0 | $\begin{array}{r} \hline \text { Vert } \\ 181 \end{array}$ |
| 32 | 1525.000M | 48.2 | $\begin{array}{r} +0.0 \\ +0.0 \\ +25.1 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.5 \\ & +0.0 \\ & +2.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -35.3 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 40.9 | 54.0 | -13.1 | Horiz |
| 33 | $\begin{gathered} 12022.351 \\ \mathrm{M} \end{gathered}$ | 45.5 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ +13.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +1.4 \\ & +0.0 \\ & +6.8 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 40.7 | $\begin{gathered} 54.0 \\ \text { ow Z } \end{gathered}$ | -13.3 | Vert |


| 34 | 240.000 M | 40.0 | $\begin{aligned} & +0.0 \\ & +0.9 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +5.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.8 \\ +11.8 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{gathered} -27.1 \\ +0.0 \\ +0.0 \\ +0.0 \end{gathered}$ | +0.0 | 32.4 | 46.0 | -13.6 | $\begin{gathered} \hline \text { Vert } \\ 100 \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 35 | $\begin{aligned} & 12202.440 \\ & \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 44.7 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -12.8 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.4 \\ & +0.0 \\ & +6.9 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 40.2 | $\begin{aligned} & 54.0 \\ & \text { id Y } \end{aligned}$ | -13.8 | Horiz |
| $\wedge$ | $\begin{gathered} 12202.480 \\ \mathrm{M} \end{gathered}$ | 43.9 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -12.8 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.4 \\ & +0.0 \\ & +6.9 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ |  |  | $\begin{aligned} & 54.0 \\ & \text { id Y } \end{aligned}$ | -14.6 | Horiz |
| 37 | $\begin{gathered} 12202.427 \\ \mathrm{M} \end{gathered}$ | 44.7 | $\begin{array}{r} \hline+0.0 \\ +0.0 \\ +0.0 \\ -12.8 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.4 \\ & +0.0 \\ & +6.9 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ |  |  | $\begin{aligned} & 54.0 \\ & i d Z \end{aligned}$ | -13.8 | Vert |
| 38 | 1223.000M | 48.5 | $\begin{array}{r} +0.0 \\ +0.0 \\ +25.1 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.4 \\ & +0.0 \\ & +1.8 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.1 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -36.1 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 39.8 | 54.0 | -14.2 | Vert |
| 39 | $\begin{gathered} 12397.580 \\ \text { M } \end{gathered}$ | 43.7 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -13.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.5 \\ & +0.0 \\ & +7.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ |  | $39.2$ | $54.0$ <br> gh Y | -14.8 | Vert |
| 40 | $\begin{gathered} 12202.423 \\ \mathrm{M} \end{gathered}$ | 43.6 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -12.8 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.4 \\ & +0.0 \\ & +6.9 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ |  |  | $\begin{aligned} & \hline 54.0 \\ & \text { id X } \end{aligned}$ | -14.9 | Vert |
| 41 | $\begin{gathered} 12022.420 \\ \mathrm{M} \end{gathered}$ | 43.9 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -13.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.4 \\ & +0.0 \\ & +6.8 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 |  | $\begin{aligned} & \hline 54.0 \\ & \text { w Y } \end{aligned}$ | -14.9 | Vert |
| 42 | $\begin{gathered} 12022.430 \\ \mathrm{M} \end{gathered}$ | 43.9 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -13.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.4 \\ & +0.0 \\ & +6.8 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ |  |  | $\begin{aligned} & 54.0 \\ & \text { w X } \end{aligned}$ | -14.9 | Vert |
| 43 | $\begin{aligned} & 12022.400 \\ & \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 43.9 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -13.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.4 \\ & +0.0 \\ & +6.8 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 39.1 | $\begin{aligned} & 54.0 \\ & \mathrm{w} \mathrm{Z} \end{aligned}$ | -14.9 | Horiz |


|  | $\begin{gathered} 12022.460 \\ \mathrm{M} \end{gathered}$ | 55.8 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -13.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +1.4 \\ & +0.0 \\ & +6.8 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $+0.0$ |  | $54.0$ <br> Low Y | -3.0 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | $\begin{gathered} 12022.400 \\ \mathrm{M} \end{gathered}$ | 51.9 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -13.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +1.4 \\ & +0.0 \\ & +6.8 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ |  |  | $54.0$ <br> Low Z | -6.9 | Horiz |
| 46 | 1225.000M | 47.6 | $\begin{array}{r} +0.0 \\ +0.0 \\ +25.1 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.4 \\ & +0.0 \\ & +1.8 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.1 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -36.1 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 38.9 | 54.0 | -15.1 | Horiz |
|  | $Q^{38.250 \mathrm{M}}$ | 33.5 | $\begin{aligned} & \hline+0.0 \\ & +0.3 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +5.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.3 \\ +12.9 \\ +0.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} -28.0 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 24.9 | 40.0 | -15.1 | $\begin{gathered} \hline \text { Vert } \\ 99 \end{gathered}$ |
| $\wedge$ | 38.250M | 44.0 | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +5.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.3 \\ +12.9 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{gathered} -28.0 \\ +0.0 \\ +0.0 \\ +0.0 \end{gathered}$ | $+0.0$ | 35.4 | 40.0 | -4.6 | $\begin{gathered} \hline \text { Vert } \\ 99 \end{gathered}$ |
|  | $\begin{gathered} 12397.100 \\ \mathrm{M} \end{gathered}$ | 42.6 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -13.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +1.5 \\ & +0.0 \\ & +7.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ |  | $38.1$ | $54.0$ <br> High X | -15.9 | Vert |
| 50 | 1073.000M | 47.9 | $\begin{array}{r} +0.0 \\ +0.0 \\ +24.6 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.4 \\ & +0.0 \\ & +1.8 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -36.8 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 38.0 | 54.0 | -16.0 | Vert |
|  | $\begin{gathered} \hline 19517.180 \\ \mathrm{M} \end{gathered}$ | 37.8 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.8 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -12.9 \\ +1.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +9.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +2.1 \end{aligned}$ | $+0.0$ | 37.8 | 54.0 | -16.2 | Vert |
|  | $7289.690 \mathrm{M}$ <br> Ave | 27.4 | $\begin{array}{r} +0.0 \\ +0.0 \\ +36.7 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.2 \\ & +0.0 \\ & +5.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{gathered} +0.0 \\ -34.6 \\ +0.0 \\ +0.0 \end{gathered}$ | $+0.0$ | 36.6 | $\begin{gathered} \quad 54.0 \\ \operatorname{Mid} X \end{gathered}$ | -17.4 | $\begin{array}{r} \hline \text { Vert } \\ 201 \end{array}$ |
| $\wedge$ | 7289.690M | 42.6 | $\begin{array}{r} +0.0 \\ +0.0 \\ +36.7 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.2 \\ & +0.0 \\ & +5.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -34.6 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 51.8 | $\begin{aligned} & \hline 54.0 \\ & \operatorname{Mid} X \end{aligned}$ | -2.2 | $\begin{array}{r} \hline \text { Vert } \\ 201 \end{array}$ |

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|  | $7451.190 \mathrm{M}$ Ave | 23.9 | $\begin{array}{r} +0.0 \\ +0.0 \\ +37.2 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +1.6 \\ & +0.0 \\ & +5.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.3 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -34.7 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 33.8 | $\begin{gathered} 54.0 \\ \text { High X } \end{gathered}$ | -20.2 | $\begin{array}{r} \hline \text { Vert } \\ 201 \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 7451.190M | 38.8 | $\begin{array}{r} +0.0 \\ +0.0 \\ +37.2 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.6 \\ & +0.0 \\ & +5.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -34.7 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 48.7 | $\begin{gathered} 54.0 \\ \operatorname{High} X \end{gathered}$ | -5.3 | $\begin{array}{r} \hline \text { Vert } \\ 201 \end{array}$ |
|  | $\begin{aligned} & 459.388 \mathrm{M} \\ & \text { QP } \end{aligned}$ | 52.3 | $\begin{aligned} & \hline+0.0 \\ & +1.4 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +5.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +1.0 \\ +18.1 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{array}{r} -27.9 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 50.9 | 73.7 | -22.8 | $\begin{array}{r} \hline \text { Vert } \\ 99 \end{array}$ |
| $\wedge$ | 459.388M | 54.0 | $\begin{aligned} & +0.0 \\ & +1.4 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +5.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +1.0 \\ +18.1 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{array}{r} -27.9 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 52.6 | 73.7 | -21.1 | $\begin{gathered} \hline \text { Vert } \\ 100 \end{gathered}$ |
|  | $\begin{aligned} & 153.126 \mathrm{M} \\ & \mathrm{QP} \end{aligned}$ | 58.8 | $\begin{aligned} & +0.0 \\ & +0.7 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +5.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.6 \\ & +9.4 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} -27.5 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 48.0 | 73.7 | -25.7 | $\begin{gathered} \hline \text { Vert } \\ 99 \end{gathered}$ |
| $\wedge$ | 153.080 M | 57.9 | $\begin{aligned} & +0.0 \\ & +0.7 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +5.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.6 \\ & +9.3 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} -27.5 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 47.0 | 73.7 | -26.7 | $\begin{gathered} \hline \text { Vert } \\ 100 \end{gathered}$ |
| 60 | 9926.390M | 35.2 | $\begin{array}{r} +0.0 \\ +0.0 \\ +37.5 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.3 \\ & +0.0 \\ & +6.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -33.9 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 |  | $\begin{gathered} 73.7 \\ \text { High X } \end{gathered}$ | -26.8 | $\begin{array}{r} \hline \text { Vert } \\ 201 \end{array}$ |
| 61 | $\begin{gathered} 14882.780 \\ \mathrm{M} \end{gathered}$ | 51.1 | $\begin{gathered} +0.0 \\ +0.0 \\ +0.0 \\ -14.4 \\ +0.0 \end{gathered}$ | $\begin{aligned} & +1.7 \\ & +0.0 \\ & +8.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ |  | $46.9$ | High Z | -26.8 | Horiz |
| 62 | $\begin{gathered} 14876.920 \\ \mathrm{M} \end{gathered}$ | 47.4 | $\begin{gathered} +0.0 \\ +0.0 \\ +0.0 \\ -14.4 \\ +0.0 \end{gathered}$ | $\begin{aligned} & +1.7 \\ & +0.0 \\ & +8.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ |  | $43.2$ | $\begin{array}{r} 73.7 \\ \text { High Y } \end{array}$ | -30.5 | Horiz |
| 63 | $\begin{aligned} & 19520.000 \\ & \text { M } \\ & \text { Ave } \end{aligned}$ | 23.4 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.8 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -12.9 \\ +1.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +9.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +2.1 \end{aligned}$ | +0.0 | 23.4 | 54.0 | -30.6 | Vert |


|  | $\begin{gathered} 14426.660 \\ \mathrm{M} \end{gathered}$ | 47.2 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -14.7 \\ +0.0 \end{array}$ | $\begin{aligned} & +1.4 \\ & +0.0 \\ & +8.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ |  |  | 73.7 <br> Low Z | -31.8 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 65 | $\begin{gathered} 14636.880 \\ \text { M } \end{gathered}$ | 46.6 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -14.7 \\ +0.0 \end{array}$ | $\begin{aligned} & +1.5 \\ & +0.0 \\ & +8.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ |  |  | $73.7$ <br> Mid Y | -32.1 | Horiz |
| 66 | 306.400M | 46.8 | $\begin{aligned} & +0.0 \\ & +1.1 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +5.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.9 \\ +13.4 \\ +0.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{array}{r} -27.1 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 41.1 | 73.7 | -32.6 | Horiz 141 |
| 67 | $\begin{gathered} 14426.820 \\ \text { M } \end{gathered}$ | 46.3 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -14.7 \\ +0.0 \end{array}$ | $\begin{aligned} & +1.4 \\ & +0.0 \\ & +8.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ |  | $41.0$ | $73.7$ <br> Low Y | -32.7 | Horiz |
| 68 | $\begin{gathered} 14642.950 \\ \mathrm{M} \end{gathered}$ | 45.0 | $\begin{array}{r} \hline+0.0 \\ +0.0 \\ +0.0 \\ -14.7 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +1.5 \\ & +0.0 \\ & +8.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $+0.0$ | $40.0$ | Mid Z | -33.7 | Horiz |
| 69 | 88.480M | 51.2 | $\begin{aligned} & +0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +5.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.4 \\ & +7.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{gathered} -27.8 \\ +0.0 \\ +0.0 \\ +0.0 \end{gathered}$ | $+0.0$ | 37.2 | 73.7 | -36.5 | $\begin{gathered} \hline \text { Vert } \\ 100 \end{gathered}$ |
| 70 | 624.800M | 35.0 | $\begin{aligned} & +0.0 \\ & +1.7 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.3 \\ & +5.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +1.2 \\ +21.4 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{array}{r} -28.2 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 37.2 | 73.7 | -36.5 | $\begin{gathered} \hline \text { Vert } \\ 100 \end{gathered}$ |
|  | $\begin{gathered} 21644.540 \\ \mathrm{M} \end{gathered}$ | 38.6 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +1.3 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -15.6 \\ +0.8 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +9.2 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +2.0 \end{aligned}$ | +0.0 | 36.3 | 73.7 | -37.4 | Horiz |
|  | $7215.505 \mathrm{M}$ <br> Ave | 27.4 | $\begin{array}{r} +0.0 \\ +0.0 \\ +36.5 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +1.1 \\ & +0.0 \\ & +5.3 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -34.5 \\ +0.0 \\ +0.0 \end{array}$ | $+0.0$ | 36.3 | $\begin{aligned} & 73.7 \\ & \text { Low X } \end{aligned}$ | -37.4 | $\begin{array}{r} \hline \text { Vert } \\ 223 \end{array}$ |
| $\wedge$ | 7215.505M | 42.3 | $\begin{array}{r} +0.0 \\ +0.0 \\ +36.5 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.1 \\ & +0.0 \\ & +5.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -34.5 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 51.2 | $\begin{aligned} & 73.7 \\ & \text { Low X } \end{aligned}$ | -22.5 | $\begin{array}{r} \hline \text { Vert } \\ 201 \end{array}$ |


|  | $\begin{aligned} & \text { QP } \\ & \hline 41.900 \mathrm{M} \\ & \hline \end{aligned}$ | 45.3 | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +5.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.3 \\ +11.2 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{gathered} -28.0 \\ +0.0 \\ +0.0 \\ +0.0 \end{gathered}$ | +0.0 | 35.0 | 73.7 | -38.7 | $\begin{array}{r} \hline \text { Vert } \\ 99 \end{array}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 41.900 M | 52.6 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 52.7 | 73.7 | -21.0 | $\begin{gathered} \hline \text { Vert } \\ 100 \end{gathered}$ |
| 76 | $\begin{gathered} 14636.898 \\ \text { M } \end{gathered}$ | 39.6 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -14.7 \\ +0.0 \end{array}$ | $\begin{aligned} & +1.5 \\ & +0.0 \\ & +8.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $+0.0$ | $34.6$ | $\begin{aligned} & \hline 73.7 \\ & \text { d X } \end{aligned}$ | -39.1 | Vert |
| 77 | 28.057 M | 37.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.3 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +5.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | 2.7 | 73.7 | -71.0 | Groun |
| 78 | 2.008 M | 32.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.1 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +9.5 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | 1.9 | 73.7 | -71.8 | Para |
| 79 | 28.415 M | 35.4 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +4.9 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | 0.7 | 73.7 | -73.0 | Groun |
| 80 | 2.305 M | 30.8 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +9.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | 0.4 | 73.7 | -73.3 | Para |
| 81 | 28.326M | 34.5 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.3 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +4.9 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -0.2 | 73.7 | -73.9 | Groun |
| 82 | 28.620 M | 33.6 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.3 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +4.8 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -1.2 | 73.7 | -74.9 | Groun |
| 83 | 2.062 M | 28.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.1 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +9.5 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $-40.0$ | -2.1 | 73.7 | -75.8 | Perp |


| 84 | 27.880M | 32.1 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +5.1 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -2.4 | 73.7 | -76.1 | Perp |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 85 | 26.780M | 31.4 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.3 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +5.6 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -2.6 | 73.7 | -76.3 | Para |
| 86 | 18.728M | 24.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +7.8 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -7.6 | 73.7 | -81.3 | Groun |
| 87 | 18.788M | 22.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline+0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +7.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -9.9 | 73.7 | -83.6 | Groun |
| 88 | 18.820M | 21.2 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +7.7 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $-40.0$ | -10.8 | 73.7 | -84.5 | Groun |
| 89 | 18.420M | 18.4 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline+0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.2 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +7.9 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -13.4 | 73.7 | -87.1 | Para |

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)
Customer:
Ossia, Inc.
Specification:
15.247(d) / 15.209 Radiated Spurious Emissions

Work Order \#:
Test Type:
Tested By: 103895

Date: 6/16/2020
Maximized Emissions
Time: 09:56:49
S. Pittsford/M. Atkinson

Sequence\#: 5
Software:
EMITest 5.03.12

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Test Conditions / Notes:
Frequency range tested: $9 \mathrm{kHz}-25 \mathrm{GHz}$
Test Mode: Continuously Modulated
EUT is on a 0.8 m test bench below 1 GHz and a 1.5 m high Styrofoam test bench above 1 GHz .

EUT is investigated in Low, Middle, and High Channels, X, Y, \& Z Axis with only the worst case reported.
Vertical and Horizontal polarities investigated
EUT connected to support Laptop via USB cable.
EUT connected to support PoE box with 2 x Ethernet cables for power.
Support laptop connected to PoE box with 1 x Ethernet cable.
PoE box and support
Laptop are located remotely.
No emissions observed within 20 dB of limit from $18-25 \mathrm{GHz}$, values provided are noise floor.
Test Location: Bothell Lab C3
Test Method: ANSI C63.10 (2013) KDB 558074 (April 2, 2019)
Temperature $\left({ }^{\circ} \mathrm{C}\right) 23$
Relative Humidity (\%): 33

Ossia, Inc. WO\#: 103895 Sequence\#: 5 Date: 6/16/2020
15.247 (d) / 15.209 Radiated Spurious Emissions Test Distance: 3 Meters Various


[^1]O Peak Readings

* Average Readings

Software Version: 5.03.12

Test Equipment:

| ID | Asset \# | Description | Model | Calibration <br> Date | Cal Due <br> Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |
| T2 | ANP06540 | Cable | Heliax | $8 / 23 / 2019$ | $8 / 23 / 2021$ |
| T3 | ANP05305 | Cable | ETSI-50T | $9 / 6 / 2019$ | $9 / 6 / 2021$ |
| T4 | AN02307 | Preamp | $8447 D$ | $1 / 10 / 2020$ | $1 / 10 / 2022$ |
| T5 | ANP05360 | Cable | RG214 | $2 / 3 / 2020$ | $2 / 3 / 2022$ |
| T6 | ANP06123 | Attenuator | 18N-6 | $4 / 5 / 2019$ | $4 / 5 / 2021$ |
| T7 | AN03628 | Biconilog Antenna | $3142 E$ | $6 / 11 / 2019$ | $6 / 11 / 2021$ |
| T8 | AN03540 | Preamp | $83017 A$ | $5 / 13 / 2019$ | $5 / 13 / 2021$ |
| T9 | AN01467 | Horn Antenna-ANSI | 3115 | $7 / 5 / 2019$ | $7 / 5 / 2021$ |
| T10 | ANP06515 | Cable |  |  |  |
| T11 | ANP07504 | Cable | Heliax | $6 / 29 / 2018$ | $6 / 29 / 2020$ |
| T12 | AN03116 | High Pass Filter | CLU40-KMKM-02.00F | $1 / 17 / 2019$ | $1 / 17 / 2021$ |
|  | AN02741 | Active Horn Antenna | AMFW-5F-12001800-20-10P | $4 / 26 / 2019$ | $4 / 26 / 2021$ |
|  | AN02742 | Active Horn Antenna | AMFW-5F-18002650-20-10P | $10 / 16 / 2018$ | $10 / 16 / 2020$ |
|  | ANP06678 | Cable | $32026-29801-29801-144$ | $2 / 20 / 2020$ | $2 / 20 / 2022$ |
|  | AN02763-69 | Waveguide | Multiple | $4 / 28 / 2020$ | $4 / 28 / 2022$ |
|  | ANP07212 | Cable | $32026-29801-29801-18$ | $8 / 7 / 2019$ | $8 / 7 / 2021$ |
|  | ANP07211 | Cable | $32026-29801-29801-18$ | $8 / 7 / 2019$ | $8 / 7 / 2021$ |
| T13 | AN00052 | Loop Antenna | 6502 | $5 / 4 / 2020$ | $5 / 4 / 2022$ |

Measurement Data: $\quad$ Reading listed by margin. Test Distance: 3 Meters


| $\begin{aligned} & 4 \text { 4878.947M } \\ & \text { Ave } \end{aligned}$ |  | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.5 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.9 \\ & +0.0 \\ & +4.2 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.5 \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.6 \end{array}$ | +0.0 | 49.2 | 54.0 | -4.8 | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ^ 4878.947M | 50.3 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.5 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.9 \\ & +0.0 \\ & +4.2 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.5 \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.6 \end{array}$ | +0.0 | 55.4 | 54.0 | +1.4 | Vert |
| ^ 4878.962M | 46.2 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.5 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +4.2 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.5 \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.6 \end{array}$ | +0.0 | 51.3 | 54.0 | -2.7 | Vert |
| $\begin{aligned} & \hline 7878.920 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 43.3 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.5 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.9 \\ & +0.0 \\ & +4.2 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.5 \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.6 \end{array}$ | +0.0 | 48.4 | 54.0 | -5.6 | Horiz |
| ^ 4878.950M | 49.5 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.5 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.9 \\ & +0.0 \\ & +4.2 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.5 \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.6 \end{array}$ | +0.0 | 54.6 | 54.0 | +0.6 | Horiz |
| 9120.200 M | 47.1 | $\begin{aligned} & +0.0 \\ & \hline+0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +5.8 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.5 \\ & +8.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-27.6 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 34.5 | 43.5 | -9.0 | Vert |
| $\begin{aligned} & 104810.954 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 39.5 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +4.1 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.6 \end{aligned}$ | $\begin{gathered} +0.0 \\ -33.6 \\ +0.6 \end{gathered}$ | +0.0 | 44.5 | 54.0 | -9.5 | Horiz |
| ^ 4810.970M | 45.7 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.4 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.9 \\ & +0.0 \\ & +4.1 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.6 \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -33.6 \\ +0.6 \end{array}$ | +0.0 | 50.7 | 54.0 | -3.3 | Horiz |
| ^ 4810.980M | 44.4 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.4 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+0.9 \\ & +0.0 \\ & +4.1 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.6 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -33.6 \\ +0.6 \end{array}$ | +0.0 | 49.4 | 54.0 | -4.6 | Horiz |
| $\begin{gathered} 13120.023 \mathrm{M} \\ \mathrm{QP} \end{gathered}$ | 45.3 | $\begin{aligned} & +0.0 \\ & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +5.8 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.5 \\ & +8.0 \\ & +0.0 \end{aligned}$ | $\begin{gathered} -27.6 \\ +0.0 \\ +0.0 \end{gathered}$ | +0.0 | 32.7 | 43.5 | -10.8 | Vert |
| 14 35.800M | 56.3 | $\begin{aligned} & +0.0 \\ & +0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +5.8 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.3 \\ +13.9 \\ +0.0 \end{array}$ | $\begin{array}{r} \hline-27.9 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 48.8 | 73.7 | -24.9 | Vert |
| 15 451.000M | 48.5 | $\begin{aligned} & +0.0 \\ & +1.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.2 \\ & +5.8 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +1.0 \\ +18.0 \\ +0.0 \end{array}$ | $\begin{array}{r} \hline-27.9 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 47.0 | 73.7 | -26.7 | Horiz |
| 16 451.000M | 47.9 | $\begin{aligned} & +0.0 \\ & +1.4 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.2 \\ & +5.8 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +1.0 \\ +18.0 \\ +0.0 \end{array}$ | $\begin{array}{r} -27.9 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 46.4 | 73.7 | -27.3 | Vert |

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| 17 | 63.000M | 54.9 | $\begin{aligned} & +0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +5.8 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.4 \\ & +7.6 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 41.5 | 73.7 | -32.2 | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 18 | 359.800 M | 39.3 | $\begin{aligned} & +0.0 \\ & +1.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +5.8 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.9 \\ +15.9 \\ +0.0 \end{array}$ | $\begin{array}{r} \hline-27.3 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 36.0 | 73.7 | -37.7 | Vert |
|  | $\mathrm{QP}^{68.800 \mathrm{M}}$ | 47.8 | $\begin{aligned} & \hline+0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +5.8 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.4 \\ & +7.4 \\ & +0.0 \end{aligned}$ | $\begin{gathered} \hline-27.8 \\ +0.0 \\ +0.0 \end{gathered}$ | +0.0 | 34.2 | 73.7 | -39.5 | Vert |
| $\wedge$ | 68.800 M | 54.9 | $\begin{aligned} & +0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +5.8 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.4 \\ & +7.4 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-27.8 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 41.3 | 73.7 | -32.4 | Vert |
| 21 | 30.000 M | 29.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +4.2 \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.3 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 33.7 | 73.7 | -40.0 | Perp |
| 22 | 2.014 M | 33.5 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +9.5 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.1 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | 3.1 | 73.7 | -70.6 | Para |
| 23 | 28.266 M | 36.6 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +5.0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.3 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | 2.0 | 73.7 | -71.7 | Groun |
| 24 | 28.445 M | 35.0 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +4.9 \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & +0.3 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | 0.3 | 73.7 | -73.4 | Groun |
| 25 | 18.728 M | 26.8 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +7.8 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.2 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -5.1 | 73.7 | -78.8 | Groun |


| Band Edge |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Band Edge Summary      <br> Frequency <br> $(\mathrm{MHz})$ Modulation Ant. Type Field Strength <br> (dBuV/m @sm)   <br> 2390.0 OQPSK Dipole 42.2   <br> (dBuV/m @sm)      | Results |  |  |  |  |
| 2400.0 | OQPSK | Dipole | 52.7 | $<54$ | Pass |
| 2483.5 | OQPSK | Dipole | 59.0 | $<74$ (PEAK) | Pass |
| 2483.5 | OQPSK | Dipole | 52.4 | $<54$ (AVE) | Pass |

## Band Edge Plots






## Test Setup / Conditions / Data

Test Location: CKC Laboratories • 2211623 rd Drive SE, Suite A • Bethel, WA 98021 • 1-800-500-4EMC (4362)

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Usia, Inc.
15.247(d) / 15.209 Radiated Spurious Emissions

102119 Date: 6/13/2020
Maximized Emissions Time: 16:27:01
Steven Pittsford
EMIT est 5.03.12
Sequence\#: 5

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

## Test Conditions / Notes:

Frequency range tested: Band Edge
Test Mode: Continuously Modulated
EUT is on a 0.8 m test bench below 1 GHz and a 1.5 m high Styrofoam test bench above 1 GHz .
EUT is investigated in Low, Middle, and High Channels, X, Y, \& Z Axis with only the worst case reported.
Vertical and Horizontal polarities investigated
EUT connected to support Laptop via USB cable.
EUT connected to AC adapter for power.
EUT connected to support Laptop via Ethernet cable.
Laptop is located remotely. (Configuration 2)
Also investigated EUT connected to support Laptop via USB cable.
EUT connected to support PoE box with 2 x Ethernet cables for power.
Support laptop connected to PoE box with 1 x Ethernet cable.
PoE box and support Laptop are located remotely. (Configuration 1)
Data collected is representative of worst case.
Test Location: Bothell Lab C3
Test Method: ANSI C63.10 (2013) KDB 558074 (April 2, 2019)
Temperature ( ${ }^{\circ} \mathrm{C}$ ) 23
Relative Humidity (\%): 33

Test Equipment:

| ID | Asset \# | Description | Model | Calibration <br> Date | Cal Due <br> Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |
| T1 | ANP06540 | Cable | Heliax | $8 / 23 / 2019$ | $8 / 23 / 2021$ |
|  | ANP05305 | Cable | ETSI-50T | $9 / 6 / 2019$ | $9 / 6 / 2021$ |
|  | AN02307 | Preamp | $8447 D$ | $1 / 10 / 2020$ | $1 / 10 / 2022$ |
|  | ANP05360 | Cable | RG214 | $2 / 3 / 2020$ | $2 / 3 / 2022$ |
|  | ANP06123 | Attenuator | $18 N-6$ | $4 / 5 / 2019$ | $4 / 5 / 2021$ |
|  | AN03628 | Biconilog Antenna | $3142 E$ | $6 / 11 / 2019$ | $6 / 11 / 2021$ |
| T2 | AN03540 | Preamp | $83017 A$ | $5 / 13 / 2019$ | $5 / 13 / 2021$ |
| T3 | AN01467 | Horn Antenna-ANSI C63.5 | 3115 | $7 / 5 / 2019$ | $7 / 5 / 2021$ |
|  |  | Calibration |  |  |  |
| T4 | ANP06515 | Cable | Heliax | $6 / 29 / 2018$ | $6 / 29 / 2020$ |
| T5 | ANP07504 | Cable | CLU40-KMKM- | $1 / 17 / 2019$ | $1 / 17 / 2021$ |
|  |  |  | $02.00 F$ |  |  |



## Test Setup Photo(s)



Configuration 1 - Below 1GHz


Configuration 1 - Above 1GHz


Configuration 2 - Below 1GHz


Configuration 2 - Above 1GHz


68.13.2020 15: 7

LABORATORIES, INC.

### 15.207 AC Conducted Emissions

## Test Setup / Conditions / Data

Test Location: Customer:
Specification: Work Order \#: Test Type: Tested By: Software:

CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362) Ossia, Inc.
15.207 AC Mains - Average

102119
Conducted Emissions
Michael Atkinson
EMITest 5.03.12

Date: 6/26/2020
Time: 09:26:08
Sequence\#: 60
115 VAC 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Test Conditions / Notes:

Temperature: $23^{\circ} \mathrm{C}$
Humidity: 34\%
Pressure: 101.6 kPa

Method: ANSI C63.10 (2013)
Frequency: $0.15-30 \mathrm{MHz}$

EUT connected to support Laptop via USB cable.
EUT connected to support laptop via USB cable.
EUT connected to support PoE box with 2 x Ethernet cables for power.
Support laptop connected to PoE box with 1 x Ethernet cable.
Support Laptop is located remotely.

Zigbee is continuously transmitting on mid-channel as representative of worst case.

Ossia. Inc. WO\#: 102119 Sequence\#: 60 Date: 6/26/2020 15.207 AC Mains - Average Test Lead: 115 VAC 60 Hz Line



Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |
| T1 | AN02611 | High Pass Filter | HE9615-150K-50-720B | $1 / 10 / 2020$ | $1 / 10 / 2022$ |
| T2 | ANP06540 | Cable | Heliax | Heliax | $8 / 23 / 2019$ |
| T3 | ANP06515 | Cable | $768-10$ | $6 / 29 / 2018$ | $8 / 23 / 2021$ |
| T4 | ANP06219 | Attenuator | $4 / 29 / 2020$ |  |  |
| T5 | AN01311 | 50uH LISN-Line1 (L) | $3816 / 2$ | $2 / 24 / 2020$ | $4 / 7 / 2022$ |
|  | AN01311 | 50uH LISN-Line2 (N) | $3816 / 2$ | $2 / 24 / 2022$ |  |

Measurement Data: Reading listed by margin. Test Lead: Line

| \# | Freq <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~T} 5 \\ & \mathrm{~dB} \end{aligned}$ | T2 $\mathrm{dB}$ | $\begin{array}{r} \mathrm{T} 3 \\ \mathrm{~dB} \\ \hline \end{array}$ | T4 <br> dB | Dist Table | $\begin{array}{r} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} \\ \hline \end{array}$ | Spec <br> $\mathrm{dB} \mu \mathrm{V}$ | Margin <br> dB | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 669.575 k | 34.9 | $\begin{array}{r} \hline+0.3 \\ -0.4 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 43.9 | 46.0 | -2.1 | Line |
| 2 | 1.159M | 34.7 | $\begin{array}{r} \hline+0.2 \\ -0.3 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 43.7 | 46.0 | -2.3 | Line |
| 3 | 208.372k | 42.7 | $\begin{gathered} \hline+0.2 \\ -1.1 \end{gathered}$ | +0.0 | +0.0 | +9.1 | +0.0 | 50.9 | 53.3 | -2.4 | Line |
| 4 | 990.470k | 34.6 | $\begin{array}{r} \hline+0.2 \\ -0.3 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 43.6 | 46.0 | -2.4 | Line |
| 5 | 499.938k | 34.5 | $\begin{array}{r} \hline+0.2 \\ -0.4 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 43.4 | 46.0 | -2.6 | Line |
| 6 | 1.055 M | 33.8 | $\begin{array}{r} \hline+0.2 \\ -0.3 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 42.8 | 46.0 | -3.2 | Line |
| 7 | 995.092k | 33.8 | $\begin{gathered} \hline+0.2 \\ -0.3 \end{gathered}$ | +0.0 | +0.0 | +9.1 | +0.0 | 42.8 | 46.0 | -3.2 | Line |
| 8 | 523.826k | 33.8 | $\begin{array}{r} \hline+0.2 \\ -0.4 \\ \hline \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 42.7 | 46.0 | -3.3 | Line |
| 9 | 1.012 M | 33.7 | $\begin{array}{r} \hline+0.2 \\ -0.3 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 42.7 | 46.0 | -3.3 | Line |
| 10 | 1.135 M | 33.6 | $\begin{array}{r} \hline+0.2 \\ -0.3 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 42.6 | 46.0 | -3.4 | Line |
| 11 | 1.125 M | 33.5 | $\begin{gathered} \hline+0.2 \\ -0.3 \end{gathered}$ | +0.0 | +0.0 | +9.1 | +0.0 | 42.5 | 46.0 | -3.5 | Line |
| 12 | 1.683 M | 32.9 | $\begin{array}{r} +0.2 \\ -0.3 \\ \hline \end{array}$ | +0.0 | +0.1 | +9.1 | +0.0 | 42.0 | 46.0 | -4.0 | Line |
| $13$ | $640.546 \mathrm{k}$ | 29.4 | $\begin{array}{r} +0.3 \\ -0.4 \\ \hline \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 38.4 | 46.0 | -7.6 | Line |
| $\wedge$ | 640.546k | 37.1 | $\begin{array}{r} \hline+0.3 \\ -0.4 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 46.1 | 46.0 | +0.1 | Line |
| $15$ | 1.356 M Ave | 28.1 | $\begin{gathered} \hline+0.2 \\ -0.3 \end{gathered}$ | +0.0 | +0.1 | +9.1 | +0.0 | 37.2 | 46.0 | -8.8 | Line |
| $\wedge$ | 1.356 M | 35.5 | $\begin{gathered} \hline+0.2 \\ -0.3 \end{gathered}$ | +0.0 | +0.1 | +9.1 | +0.0 | 44.6 | 46.0 | -1.4 | Line |
|  | $\begin{aligned} & \text { 937.565k } \\ & \text { Ave } \end{aligned}$ | 27.8 | $\begin{array}{r} \hline+0.2 \\ -0.3 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 36.8 | 46.0 | -9.2 | Line |
| $\wedge$ | 937.565k | 35.3 | $\begin{array}{r} +0.2 \\ -0.3 \\ \hline \end{array}$ | +0.0 | $+0.0$ | +9.1 | +0.0 | 44.3 | 46.0 | -1.7 | Line |
|  | $794.260 \mathrm{k}$ | 27.8 | $\begin{array}{r} \hline+0.2 \\ -0.3 \end{array}$ | +0.0 | $+0.0$ | +9.1 | $+0.0$ | 36.8 | 46.0 | -9.2 | Line |
| $\wedge$ | 794.259k | 35.1 | $\begin{array}{r} \hline+0.2 \\ -0.3 \end{array}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 44.1 | 46.0 | -1.9 | Line |
|  | $\begin{aligned} & 830.728 \mathrm{k} \\ & \text { Ave } \end{aligned}$ | $26.2$ | $\begin{gathered} +0.2 \\ -0.3 \end{gathered}$ | +0.0 | +0.0 | +9.1 | +0.0 | 35.2 | 46.0 | -10.8 | Line |
| $\wedge$ | 830.728k | 35.8 | $\begin{array}{r} \hline+0.2 \\ -0.3 \end{array}$ | +0.0 | $+0.0$ | +9.1 | $+0.0$ | 44.8 | 46.0 | -1.2 | Line |


|  | $\begin{aligned} & 978.143 \mathrm{k} \\ & \text { Ave } \\ & \hline \end{aligned}$ | 26.1 | $\begin{array}{r} \hline+0.2 \\ -0.3 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 35.1 | 46.0 | -10.9 | Line |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 978.142k | 35.2 | $\begin{gathered} +0.2 \\ -0.3 \end{gathered}$ | +0.0 | +0.0 | +9.1 | +0.0 | 44.2 | 46.0 | -1.8 | Line |
|  | $678.042 \mathrm{k}$ <br> Ave | 25.3 | $\begin{array}{r} \hline+0.3 \\ -0.4 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 34.3 | 46.0 | -11.7 | Line |
| $\wedge$ | 678.041k | 35.3 | $\begin{array}{r} +0.3 \\ -0.4 \\ \hline \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 44.3 | 46.0 | -1.7 | Line |
|  | $462.443 \mathrm{k}$ | 23.2 | $\begin{array}{r} +0.2 \\ -0.5 \\ \hline \end{array}$ | $+0.0$ | +0.1 | +9.1 | +0.0 | 32.1 | 46.6 | -14.5 | Line |
| $\wedge$ | 462.443k | 36.3 | $\begin{array}{r} +0.2 \\ -0.5 \end{array}$ | +0.0 | +0.1 | +9.1 | +0.0 | 45.2 | 46.6 | -1.4 | Line |

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)
Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:
Ossia, Inc.
15.207 AC Mains - Average

102119
Conducted Emissions
Michael Atkinson
EMITest 5.03.12

Date: 6/26/2020
Time: 09:15:32
Sequence\#: 59
115 VAC 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Temperature: $23^{\circ} \mathrm{C}$
Humidity: $34 \%$
Pressure: 101.6 kPa
Method: ANSI C63.10 (2013)

Frequency: $0.15-30 \mathrm{MHz}$
EUT connected to support Laptop via USB cable.
EUT connected to support laptop via USB cable.
EUT connected to support PoE box with 2 x Ethernet cables for power.
Support laptop connected to PoE box with 1 x Ethernet cable.
Support Laptop is located remotely.
Zigbee is continuously transmitting on mid-channel as representative of worst case.

Ossia, Inc. WO\#: 102119 Sequence\#: 59 Date: 6/26/2020 15.207 AC Mains - Average Test Lead: 115 VAC 60 Hz Neutral



Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |
| T1 | AN02611 | High Pass Filter | HE9615-150K-50-720B | $1 / 10 / 2020$ | $1 / 10 / 2022$ |
| T2 | ANP06540 | Cable | Heliax | $8 / 23 / 2019$ | $8 / 23 / 2021$ |
| T3 | ANP06515 | Cable | Heliax | $6 / 29 / 2018$ | $6 / 29 / 2020$ |
| T4 | ANP06219 | Attenuator | $768-10$ | $4 / 7 / 2020$ | $4 / 7 / 2022$ |
|  | AN01311 | 50uH LISN-Line1 (L) | $3816 / 2$ | $2 / 24 / 2020$ | $2 / 24 / 2022$ |
| T5 | AN01311 | 50uH LISN-Line2 (N) | $3816 / 2$ | $2 / 24 / 2020$ | $2 / 24 / 2022$ |



Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bethel, WA 98021 • 1-800-500-4EMC (4362)
Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:
Ossa, Inc.
15.207 AC Mains - Average

102119
Conducted Emissions
Michael Atkinson
EMITest 5.03.12

Date: 6/14/2020
Time: 15:40:00
Sequence\#: 37
115 VAC 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Test Conditions / Notes:
Temperature: $19-21^{\circ} \mathrm{C}$
Humidity: 29-32\%
Pressure: $102-103 \mathrm{kPa}$

Method: ANSI C63.10 (2013)
Frequency: $0.15-30 \mathrm{MHz}$
EUT connected to support Laptop via USB cable.
EUT connected to AC adapter for power.
EUT connected to support Laptop via Ethernet cable.
Laptop is located remotely.
Zigbee is continuously transmitting on mid-channel as representative of worst case.

Ossia, Inc. WO\#: 102119 Sequence\#: 37 Date: 6/14/2020 15.207 AC Mains - Average Test Lead: 115 VAC 60 Hz Line



Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |
| T1 | AN02611 | High Pass Filter | HE9615-150K-50-720B | $1 / 10 / 2020$ | $1 / 10 / 2022$ |
| T2 | ANP06540 | Cable | Heliax | Heliax | $8 / 23 / 2019$ |
| T3 | ANP06515 | Cable | $768-10$ | $6 / 29 / 2018$ | $8 / 23 / 2021$ |
| T4 | ANP06219 | Attenuator | $3816 / 2 N M$ | $4 / 7 / 2020$ | $4 / 7 / 2022$ |
| T5 | AN01492 | 50uH LISN-Line (L1) | 30.2020 |  |  |
|  | AN01492 | 50uH LISN-Neutral (L2) | $3816 / 2 N M$ | $10 / 14 / 2019$ | $10 / 14 / 2021$ |

Measurement Data: Reading listed by margin. Test Lead: Line

| \# | Freq <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~T} 5 \\ & \mathrm{~dB} \end{aligned}$ | T2 $\mathrm{dB}$ | $\begin{array}{r} \mathrm{T} 3 \\ \mathrm{~dB} \\ \hline \end{array}$ | T4 <br> dB | Dist Table | Corr $\mathrm{dB} \mu \mathrm{V}$ | Spec <br> $\mathrm{dB} \mu \mathrm{V}$ | Margin <br> dB | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 7.049M | 38.0 | $\begin{aligned} & \hline+0.1 \\ & +0.6 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 47.9 | 50.0 | -2.1 | Line |
| 2 | 10.337M | 37.9 | $\begin{array}{r} +0.1 \\ +0.5 \\ \hline \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.8 | 50.0 | -2.2 | Line |
| 3 | 8.939M | 37.8 | $\begin{aligned} & \hline+0.1 \\ & +0.6 \end{aligned}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.8 | 50.0 | -2.2 | Line |
| 4 | 4.651 M | 33.9 | $\begin{aligned} & +0.1 \\ & +0.5 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 43.7 | 46.0 | -2.3 | Line |
| 5 | 10.034 M | 37.8 | $\begin{aligned} & +0.1 \\ & +0.5 \end{aligned}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.7 | 50.0 | -2.3 | Line |
| 6 | 8.242M | 37.7 | $\begin{aligned} & +0.1 \\ & +0.6 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 47.6 | 50.0 | -2.4 | Line |
| 7 | 4.691 M | 33.6 | $\begin{aligned} & \hline+0.1 \\ & +0.6 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 43.5 | 46.0 | -2.5 | Line |
| 8 | 8.404M | 37.5 | $\begin{aligned} & +0.1 \\ & +0.6 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 47.4 | 50.0 | -2.6 | Line |
| 9 | 8.610M | 37.4 | $\begin{aligned} & +0.1 \\ & +0.6 \end{aligned}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.4 | 50.0 | -2.6 | Line |
| 10 | 8.075M | 37.6 | $\begin{aligned} & +0.1 \\ & +0.5 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 47.4 | 50.0 | -2.6 | Line |
| 11 | 14.923M | 37.2 | $\begin{aligned} & \hline+0.2 \\ & +0.5 \end{aligned}$ | +0.1 | +0.2 | +9.1 | +0.0 | 47.3 | 50.0 | -2.7 | Line |
| $12$ | 4.935M | 20.2 | $\begin{aligned} & +0.1 \\ & +0.5 \end{aligned}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 30.0 | 46.0 | -16.0 | Line |
| $\wedge$ | 4.935 M | 34.9 | $\begin{array}{r} +0.1 \\ +0.5 \\ \hline \end{array}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 44.7 | 46.0 | -1.3 | Line |
| $14$ | $4.832 \mathrm{M}$ | 19.6 | $\begin{aligned} & +0.1 \\ & +0.5 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 29.4 | 46.0 | -16.6 | Line |
| $\wedge$ | 4.832 M | 34.3 | $\begin{aligned} & \hline+0.1 \\ & +0.5 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 44.1 | 46.0 | -1.9 | Line |
| $16$ | $4.902 \mathrm{M}$ | 19.5 | $\begin{aligned} & \hline+0.1 \\ & +0.5 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 29.3 | 46.0 | -16.7 | Line |
| $\wedge$ | 4.902 M | 34.8 | $\begin{aligned} & \hline+0.1 \\ & +0.5 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 44.6 | 46.0 | -1.4 | Line |
|  | $\begin{aligned} & \text { ve } \\ & \text { ve } \end{aligned}$ | 20.8 | $\begin{array}{r} +0.1 \\ +0.5 \\ \hline \end{array}$ | +0.0 | +0.1 | +9.1 | +0.0 | 30.6 | 50.0 | -19.4 | Line |
| $\wedge$ | 6.976M | 38.2 | $\begin{aligned} & +0.1 \\ & +0.5 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 48.0 | 50.0 | -2.0 | Line |

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)
Ossa, Inc.
15.207 AC Mains - Average

102119
Conducted Emissions
Michael Atkinson
EMITest 5.03.12

Date: 6/14/2020
Time: 15:34:45
Sequence\#: 36
115 VAC 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Test Conditions / Notes:
Temperature: $19-21^{\circ} \mathrm{C}$
Humidity: 29-32\%
Pressure: $102-103 \mathrm{kPa}$
Method: ANSI C63.10 (2013)

Frequency: $0.15-30 \mathrm{MHz}$
EUT connected to support Laptop via USB cable.
EUT connected to AC adapter for power.
EUT connected to support Laptop via Ethernet cable.
Laptop is located remotely.
Zigbee is continuously transmitting on mid-channel as representative of worst case.

Ossia, Inc. WO\#: 102119 Sequence\#: 36 Date: 6/14/2020 15.207 AC Mains - Average Test Lead: 115 VAC 60 Hz Neutral



Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |
| T1 | AN02611 | High Pass Filter | HE9615-150K-50-720B | $1 / 10 / 2020$ | $1 / 10 / 2022$ |
| T2 | ANP06540 | Cable | Heliax | Heliax | $8 / 23 / 2019$ |
| T3 | ANP06515 | Cable | $768-10$ | $6 / 29 / 2018$ | $8 / 23 / 2021$ |
| T4 | ANP06219 | Attenuator | $3816 / 2 N M$ | $4 / 7 / 2020$ | $4 / 7 / 2022$ |
|  | AN01492 | 50uH LISN-Line (L1) | 30uH LISN-Neutral (L2) | $3816 / 2 N M$ | $10 / 14 / 2019$ |
| T5 | AN01492 | 50u | $10 / 14 / 2021$ |  |  |


| Measu | ment Data | Reading listed by margin. |  |  |  | Test Lead: Neutral |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | Freq | Rdng |  | T2 | T3 | T4 | Dist | Corr | Spec | Margin | Polar |
|  | MHz | $\mathrm{dB} \mu \mathrm{V}$ | dB | dB | dB | dB | Table | $\mathrm{dB} \mu \mathrm{V}$ | $\mathrm{dB} \mu \mathrm{V}$ | dB | Ant |
| 1 | 15.547M | 37.5 | +0.2 | +0.1 | +0.2 | +9.1 | +0.0 | 47.7 | 50.0 | -2.3 | Neutr |
|  |  |  | +0.6 |  |  |  |  |  |  |  |  |
| 2 | 13.993M | 37.5 | +0.2 | +0.0 | +0.2 | +9.1 | +0.0 | 47.5 | 50.0 | -2.5 | Neutr |
|  |  |  | +0.5 |  |  |  |  |  |  |  |  |
| 3 | 14.218M | 37.3 | +0.2 | +0.0 | +0.2 | +9.1 | +0.0 | 47.4 | 50.0 | -2.6 | Neutr |
|  |  |  | +0.6 |  |  |  |  |  |  |  |  |
| 4 | 16.281M | 37.0 | +0.2 | +0.1 | +0.2 | +9.1 | +0.0 | 47.1 | 50.0 | -2.9 | Neutr |
|  |  |  | +0.5 |  |  |  |  |  |  |  |  |
| 5 | 16.005M | 36.4 | +0.2 | +0.1 | +0.2 | +9.1 | +0.0 | 46.5 | 50.0 | -3.5 | Neutr |
|  |  |  | +0.5 |  |  |  |  |  |  |  |  |
| 6 | 16.092M | 36.2 | +0.2 | +0.1 | +0.2 | +9.1 | +0.0 | 46.3 | 50.0 | -3.7 | Neutr |
|  |  |  | +0.5 |  |  |  |  |  |  |  |  |
| 7 | 15.700M | 36.1 | +0.2 | +0.1 | +0.2 | +9.1 | +0.0 | 46.3 | 50.0 | -3.7 | Neutr |
|  |  |  | +0.6 |  |  |  |  |  |  |  |  |
| 8 | 16.034M | 35.9 | +0.2 | +0.1 | +0.2 | +9.1 | +0.0 | 46.0 | 50.0 | -4.0 | Neutr |
|  |  |  | +0.5 |  |  |  |  |  |  |  |  |
| 9 | 14.930M | 35.5 | +0.2 | +0.1 | +0.2 | +9.1 | +0.0 | 45.6 | 50.0 | -4.4 | Neutr |
|  | Ave |  | +0.5 |  |  |  |  |  |  |  |  |
| $\wedge$ | 14.930M | 39.3 | +0.2 | +0.1 | +0.2 | +9.1 | +0.0 | 49.4 | 50.0 | -0.6 | Neutr |
|  |  |  | +0.5 |  |  |  |  |  |  |  |  |
| 11 | 14.944M | 21.8 | +0.2 | +0.1 | +0.2 | +9.1 | +0.0 | 31.9 | 50.0 | -18.1 | Neutr |
|  | Ave |  | +0.5 |  |  |  |  |  |  |  |  |
| $\wedge$ | 14.944M | 39.0 | +0.2 | +0.1 | +0.2 | +9.1 | +0.0 | 49.1 | 50.0 | -0.9 | Neutr |
|  |  |  | +0.5 |  |  |  |  |  |  |  |  |
| 13 | 14.785M | 21.6 | +0.2 | +0.1 | +0.2 | +9.1 | +0.0 | 31.7 | 50.0 | -18.3 | Neutr |
|  | ve |  | +0.5 |  |  |  |  |  |  |  |  |
| $\wedge$ | 14.785M | 38.1 | +0.2 | +0.1 | +0.2 | +9.1 | +0.0 | 48.2 | 50.0 | -1.8 | Neutr |
|  |  |  | +0.5 |  |  |  |  |  |  |  |  |
| 15 | 15.119M | 21.4 | +0.2 | +0.1 | +0.2 | +9.1 | +0.0 | 31.6 | 50.0 | -18.4 | Neutr |
|  | ve |  | +0.6 |  |  |  |  |  |  |  |  |
| $\wedge$ | 15.119M | 38.8 | +0.2 | +0.1 | +0.2 | +9.1 | +0.0 | 49.0 | 50.0 | -1.0 | Neutr |
|  |  |  | +0.6 |  |  |  |  |  |  |  |  |
| 17 | 14.647M | 21.4 | +0.2 | +0.1 | +0.2 | +9.1 | +0.0 | 31.5 | 50.0 | -18.5 | Neutr |
|  | ve |  | +0.5 |  |  |  |  |  |  |  |  |
| $\wedge$ | 14.647M | 38.3 | +0.2 | +0.1 | +0.2 | +9.1 | +0.0 | 48.4 | 50.0 | -1.6 | Neutr |
|  |  |  | +0.5 |  |  |  |  |  |  |  |  |
| 19 | 14.465M | 21.3 | +0.2 | +0.0 | +0.2 | +9.1 | +0.0 | 31.3 | 50.0 | -18.7 | Neutr |
|  | ve |  | +0.5 |  |  |  |  |  |  |  |  |
| $\wedge$ | 14.465M | 39.2 | +0.2 | +0.0 | +0.2 | +9.1 | +0.0 | 49.2 | 50.0 | -0.8 | Neutr |
|  |  |  | +0.5 |  |  |  |  |  |  |  |  |
| 21 | 14.327M | 20.8 | +0.2 | +0.0 | +0.2 | +9.1 | +0.0 | 30.9 | 50.0 | -19.1 | Neutr |
|  | ve |  | +0.6 |  |  |  |  |  |  |  |  |
| $\wedge$ | 14.327M | 39.5 | +0.2 | +0.0 | +0.2 | +9.1 | +0.0 | 49.6 | 50.0 | -0.4 | Neutr |
|  |  |  | +0.6 |  |  |  |  |  |  |  |  |

## Test Setup Photo(s)



Configuration 1


Configuration 2

## Appendix A: Co-Location Testing

Co-Location testing was performed and no mixing products were observed within 15 dB of 15.209 limit.

The following configurations were tested as representative of worst case with channels available at time of test:

WPT $2.45 \mathrm{GHz}+$ Pi Wi-Fi 2.452 GHz
WPT $2.45 \mathrm{GHz}+$ Pi Wi-Fi $2.452 \mathrm{GHz}+$ Zigbee 2.455 GHz
Pi Wi-Fi $2.452 \mathrm{GHz}+$ Zigbee 2.45 GHz
Pi Wi-Fi 5.180GHz + Zigbee 2.480 GHz Zigbee
Pi Wi-Fi $5.180 \mathrm{GHz}+$ WPT 2.46 GHz

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)
Customer:
Specification:
Ossia, Inc.
15.207 AC Mains - Average

Work Order \#: 102119
Test Type:
Tested By:
Conducted Emissions

Software:
Michael Atkinson
Date: 6/26/2020
Time: 09:50:06
Sequence\#: 61
115 VAC 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Temperature: $20-25^{\circ} \mathrm{C}$
Humidity: 30-36\%
Pressure: $101-102 \mathrm{kPa}$

Method: ANSI C63.10 (2013)
Frequency range tested: $0.15-30 \mathrm{MHz}$
XYZ EUT orientations investigated, worst case reported.
Below $30 \mathrm{MHz}, 3 \mathrm{x}$ orthogonal axes investigated, above 30 MHz , Horizontal and Vertical Antenna polarities investigated, worst case reported.

Investigated Radiated Spurious Emissions of Integrated Raspberry Pi 4 module while running the $2.4 \mathrm{GHz} \mathrm{Wi-Fi}$ radio continuously. Customer was provided a worst case script of maximum power, running on Channel 1 $(2412 \mathrm{MHz})$ at worst case data rate for spurious emissions.

EUT connected to support laptop via USB cable.
EUT connected to support PoE box with 2 x Ethernet cables for power.
Support laptop connected to PoE box with $1 \times$ Ethernet cable.
PoE box and support Laptop are located remotely. (Configuration 1)
Integrated Module Info
Raspberry Pi 4B (FCC ID 2ABCB-RPI4B)

Ossia. Inc. WO\#: 102119 Sequence\#: 61 Date: 6/26/2020 15.207 AC Mains - Average Test Lead: 115 VAC 60 Hz Line



Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |
| T1 | AN02611 | High Pass Filter | HE9615-150K-50-720B | $1 / 10 / 2020$ | $1 / 10 / 2022$ |
| T2 | ANP06540 | Cable | Heliax | Heliax | $8 / 23 / 2019$ |
| T3 | ANP06515 | Cable | $768-10$ | $6 / 29 / 2018$ | $8 / 23 / 2021$ |
| T4 | ANP06219 | Attenuator | $4 / 29 / 2020$ |  |  |
| T5 | AN01311 | 50uH LISN-Line1 (L) | $3816 / 2$ | $4 / 7 / 2020$ | $4 / 7 / 2022$ |
|  | AN01311 | 50uH LISN-Line2 (N) | $3816 / 2$ | $2 / 24 / 2020$ | $2 / 24 / 2022$ |

Measurement Data: Reading listed by margin. Test Lead: Line

| \# | Freq <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{gathered} \mathrm{T} 1 \\ \mathrm{~T} 5 \\ \mathrm{~dB} \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \\ & \hline \end{aligned}$ | $\begin{array}{r} \mathrm{T} 3 \\ \mathrm{~dB} \\ \hline \end{array}$ | T4 dB | Dist <br> Table | Corr <br> $\mathrm{dB} \mu \mathrm{V}$ | Spec <br> $\mathrm{dB} \mu \mathrm{V}$ | Margin <br> dB | Polar Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 830.728k | 34.9 | $\begin{gathered} \hline+0.2 \\ -0.3 \end{gathered}$ | +0.0 | +0.0 | +9.1 | +0.0 | 43.9 | 46.0 | -2.1 | Line |
| 2 | 675.320k | 34.8 | $\begin{array}{r} \hline+0.3 \\ -0.4 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 43.8 | 46.0 | -2.2 | Line |
| 3 | 680.460k | 34.8 | $\begin{array}{r} \hline+0.3 \\ -0.4 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 43.8 | 46.0 | -2.2 | Line |
| 4 | 1.358M | 34.5 | $\begin{array}{r} +0.2 \\ -0.3 \\ \hline \end{array}$ | +0.0 | +0.1 | +9.1 | +0.0 | 43.6 | 46.0 | -2.4 | Line |
| 5 | 296.986k | 39.2 | $\begin{array}{r} \hline+0.1 \\ -0.7 \end{array}$ | +0.0 | $+0.0$ | +9.1 | +0.0 | 47.7 | 50.3 | -2.6 | Line |
| 6 | 411.983 k | 36.2 | $\begin{array}{r} \hline+0.2 \\ -0.5 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 45.0 | 47.6 | -2.6 | Line |
| 7 | 256.755 k | 40.4 | $\begin{array}{r} \hline+0.2 \\ -0.9 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 48.8 | 51.5 | -2.7 | Line |
| 8 | 792.718k | 34.2 | $\begin{array}{r} \hline+0.2 \\ -0.3 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 43.2 | 46.0 | -2.8 | Line |
| 9 | 227.550 k | 41.2 | $\begin{array}{r} \hline+0.3 \\ -1.0 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 49.6 | 52.5 | -2.9 | Line |
| 10 | 261.561 k | 40.0 | $\begin{array}{r} \hline+0.2 \\ -0.8 \end{array}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 48.5 | 51.4 | -2.9 | Line |
| 11 | 254.693 k | 40.1 | $\begin{array}{r} \hline+0.2 \\ -0.9 \end{array}$ | +0.0 | $+0.0$ | +9.1 | $+0.0$ | 48.5 | 51.6 | -3.1 | Line |
| 12 | 252.806k | 40.1 | $\begin{array}{r} \hline+0.2 \\ -0.9 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 48.5 | 51.7 | -3.2 | Line |
| 13 | 263.341k | 39.6 | $\begin{array}{r} +0.2 \\ -0.8 \\ \hline \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 48.1 | 51.3 | -3.2 | Line |
| 14 | 266.545k | 39.4 | $\begin{array}{r} +0.2 \\ -0.8 \\ \hline \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 47.9 | 51.2 | -3.3 | Line |
| 15 | 250.606k | 39.9 | $\begin{array}{r} \hline+0.2 \\ -0.9 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 48.3 | 51.7 | -3.4 | Line |
| 16 | 978.142k | 33.5 | $\begin{array}{r} \hline+0.2 \\ -0.3 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 42.5 | 46.0 | -3.5 | Line |
| $17$ | $\begin{aligned} & \text { 451.558k } \\ & \text { Ave } \end{aligned}$ | 32.6 | $\begin{array}{r} \hline+0.2 \\ -0.5 \end{array}$ | +0.0 | +0.1 | +9.1 | +0.0 | 41.5 | 46.8 | -5.3 | Line |
| $\wedge$ | 451.557k | 36.8 | $\begin{array}{r} \hline+0.2 \\ -0.5 \end{array}$ | +0.0 | +0.1 | +9.1 | +0.0 | 45.7 | 46.8 | -1.1 | Line |
|  | $\begin{aligned} & \text { 638.430k } \\ & \text { Ave } \end{aligned}$ | 31.6 | $\begin{array}{r} \hline+0.3 \\ -0.4 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 40.6 | 46.0 | -5.4 | Line |
| $\wedge$ | 638.429k | 35.7 | $\begin{array}{r} \hline+0.3 \\ -0.4 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 44.7 | 46.0 | -1.3 | Line |
|  | $\begin{aligned} & \text { 938.079k } \\ & \text { Ave } \end{aligned}$ | 28.2 | $\begin{array}{r} \hline+0.2 \\ -0.3 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 37.2 | 46.0 | -8.8 | Line |
| $\wedge$ | 938.078k | 35.2 | $\begin{array}{r} \hline+0.2 \\ -0.3 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 44.2 | 46.0 | -1.8 | Line |
| $23$ | $\begin{aligned} & \text { 208.268k } \\ & \text { Ave } \end{aligned}$ | 34.1 | $\begin{array}{r} +0.2 \\ -1.1 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 42.3 | 53.3 | -11.0 | Line |
| $\wedge$ | 208.267k | 44.0 | $\begin{array}{r} \hline+0.2 \\ -1.1 \\ \hline \end{array}$ | +0.0 | $+0.0$ | +9.1 | $+0.0$ | 52.2 | 53.3 | -1.1 | Line |

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Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)
Customer:
Specification:
Ossia, Inc.
15.207 AC Mains - Average

Work Order \#: 102119
Test Type:
Tested By:
Conducted Emissions

Software:
Michael Atkinson
Date: 6/26/2020
Time: 09:53:53
Sequence\#: 62
115 VAC 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Temperature: $20-25^{\circ} \mathrm{C}$
Humidity: 30-36\%
Pressure: $101-102 \mathrm{kPa}$
Method: ANSI C63.10 (2013)

Frequency range tested: $0.15-30 \mathrm{MHz}$
XYZ EUT orientations investigated, worst case reported.
Below $30 \mathrm{MHz}, 3 \mathrm{x}$ orthogonal axes investigated, above 30 MHz , Horizontal and Vertical Antenna polarities investigated, worst case reported.

Investigated Radiated Spurious Emissions of Integrated Raspberry Pi 4 module while running the $2.4 \mathrm{GHz} \mathrm{Wi}-\mathrm{Fi}$ radio continuously. Customer was provided a worst case script of maximum power, running on Channel 1 $(2412 \mathrm{MHz})$ at worst case data rate for spurious emissions.

EUT connected to support laptop via USB cable.
EUT connected to support PoE box with 2 x Ethernet cables for power.
Support laptop connected to PoE box with $1 \times$ Ethernet cable.
PoE box and support Laptop are located remotely. (Configuration 1)
Integrated Module Info
Raspberry Pi 4B (FCC ID 2ABCB-RPI4B)

Ossia, Inc. WO\#: 102119 Sequence\#: 62 Date: 6/26/2020 15.207 AC Mains - Average Test Lead: 115 VAC 60 Hz Neutral



Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |
| T1 | AN02611 | High Pass Filter | HE9615-150K-50-720B | $1 / 10 / 2020$ | $1 / 10 / 2022$ |
| T2 | ANP06540 | Cable | Heliax | Heliax | $8 / 23 / 2019$ |
| T3 | ANP06515 | Cable | $768-10$ | $6 / 29 / 2018$ | $8 / 23 / 2021$ |
| T4 | ANP06219 | Attenuator | $4 / 7 / 2020$ | $4 / 2020$ |  |
|  | AN01311 | 50uH LISN-Line1 (L) | $3816 / 2$ | $2 / 24 / 2020$ | $2 / 24 / 2022$ |
| T5 | AN01311 | 50uH LISN-Line2 (N) | $3816 / 2$ | $2 / 24 / 2020$ | $2 / 24 / 2022$ |



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Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)
Customer:
Specification:
Ossia, Inc.
15.207 AC Mains - Average

Work Order \#: 102119
Test Type:
Tested By:
Conducted Emissions
Michael Atkinson
Date: 6/26/2020
Time: 10:12:07

Software:
EMITest 5.03.12

Sequence\#: 64
115 VAC 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Temperature: $20-25^{\circ} \mathrm{C}$
Humidity: 30-36\%
Pressure: $101-102 \mathrm{kPa}$
Method: ANSI C63.10 (2013)

Frequency range tested: $0.15-30 \mathrm{MHz}$
XYZ EUT orientations investigated, worst case reported.
Below $30 \mathrm{MHz}, 3 \mathrm{x}$ orthogonal axes investigated, above 30 MHz , Horizontal and Vertical Antenna polarities investigated, worst case reported.

Investigated Radiated Spurious Emissions of Integrated Raspberry Pi 4 module while running the 5 GHz Wi-Fi radio continuously. Customer was provided a worst case script of maximum power, running on Channel 36 ( 5180 MHz ) at worst case data rate for spurious emissions. Also investigated Channel $140(5700 \mathrm{MHz})$ but no emissions observed within 20 dB of 15.209 limit.

EUT connected to support laptop via USB cable.
EUT connected to support PoE box with 2 x Ethernet cables for power.
Support laptop connected to PoE box with $1 \times$ Ethernet cable.
PoE box and support Laptop are located remotely. (Configuration 1)
Integrated Module Info
Raspberry Pi 4B (FCC ID 2ABCB-RPI4B)

Ossia, Inc. WO\#: 102119 Sequence\#: 64 Date: 6/26/2020 15.207 AC Mains - Average Test Lead: 115 VAC 60 Hz Line


|  | Sweep Data | Readings | Peak Readings |
| :--- | :--- | :--- | :--- |
| $\times$ | Q Readings | Average Readings | Ambient |
| Software Version: 5.03 .12 |  | -15.207 AC Mains - Average | $2-15.207$ AC Mains - Quasi-peak |

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |
| T1 | AN02611 | High Pass Filter | HE9615-150K-50-720B | $1 / 10 / 2020$ | $1 / 10 / 2022$ |
| T2 | ANP06540 | Cable | Heliax | $8 / 23 / 2019$ | $8 / 23 / 2021$ |
| T3 | ANP06515 | Cable | Heliax | $6 / 29 / 2018$ | $6 / 29 / 2020$ |
| T4 | ANP06219 | Attenuator | $768-10$ | $4 / 7 / 2020$ | $4 / 7 / 2022$ |
| T5 | AN01311 | 50uH LISN-Line1 (L) | $3816 / 2$ | $2 / 24 / 2020$ | $2 / 24 / 2022$ |
|  | AN01311 | 50uH LISN-Line2 (N) | $3816 / 2$ | $2 / 24 / 2020$ | $2 / 24 / 2022$ |

Measurement Data: $\quad$ Reading listed by margin.
Test Lead: Line

| $\#$ | Freq | Rdng | T 1 | T 2 | T 3 | T 4 | Dist | Corr | Spec | Margin | Polar |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | T 5 |  |  |  |  |  |  |  |  |
|  | MHz | $\mathrm{dB} \mu \mathrm{V}$ | dB | dB | dB | dB | Table | $\mathrm{dB} \mu \mathrm{V}$ | $\mathrm{dB} \mu \mathrm{V}$ | dB | Ant |
| 1 | 825.078 k | 34.7 | +0.2 | +0.0 | +0.0 | +9.1 | +0.0 | 43.7 | 46.0 | -2.3 | Line |
| 2 | 266.545 k | 40.2 | +0.2 | +0.0 | +0.0 | +9.1 | +0.0 | 48.7 | 51.2 | -2.5 | Line |


| 3 | 1.357 M | 34.4 | $\begin{array}{r} \hline+0.2 \\ -0.3 \end{array}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 43.5 | 46.0 | -2.5 | Line |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | 260.137k | 40.2 | $\begin{gathered} \hline+0.2 \\ -0.8 \end{gathered}$ | +0.0 | +0.0 | +9.1 | +0.0 | 48.7 | 51.4 | -2.7 | Line |
| 5 | 681.065 k | 34.3 | $\begin{gathered} \hline+0.3 \\ -0.4 \end{gathered}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 43.3 | 46.0 | -2.7 | Line |
| 6 | 793.232k | 34.3 | $\begin{gathered} \hline+0.2 \\ -0.3 \end{gathered}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 43.3 | 46.0 | -2.7 | Line |
| 7 | 296.808k | 39.0 | $\begin{gathered} \hline+0.1 \\ -0.7 \end{gathered}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 47.5 | 50.3 | -2.8 | Line |
| 8 | 227.864k | 41.3 | $\begin{gathered} +0.3 \\ -1.0 \end{gathered}$ | +0.0 | +0.0 | +9.1 | +0.0 | 49.7 | 52.5 | -2.8 | Line |
| 9 | 252.492k | 40.1 | $\begin{array}{r} +0.2 \\ -0.9 \\ \hline \end{array}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 48.5 | 51.7 | -3.2 | Line |
| 10 | 255.509k | 39.9 | $\begin{array}{r} +0.2 \\ -0.9 \end{array}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 48.3 | 51.6 | -3.3 | Line |
| 11 | 416.077k | 35.3 | $\begin{array}{r} \hline+0.2 \\ -0.5 \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 44.1 | 47.5 | -3.4 | Line |
| 12 | 171.693 k | 43.3 | $\begin{gathered} \hline+0.4 \\ -1.5 \end{gathered}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 51.3 | 54.9 | -3.6 | Line |
| 13 | 186.469k | 42.4 | $\begin{gathered} \hline+0.3 \\ -1.3 \end{gathered}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 50.5 | 54.2 | -3.7 | Line |
| 14 | 520.500k | 33.4 | $\begin{array}{r} \hline+0.2 \\ -0.4 \end{array}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 42.3 | 46.0 | -3.7 | Line |
| 15 | 1.050M | 33.2 | $\begin{array}{r} \hline+0.2 \\ -0.3 \\ \hline \end{array}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 42.2 | 46.0 | -3.8 | Line |
|  | $\begin{aligned} & \text { 451.860k } \\ & \text { Ave } \end{aligned}$ | 32.5 | $\begin{array}{r} \hline+0.2 \\ -0.5 \end{array}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 41.4 | 46.8 | -5.4 | Line |
| $\wedge$ | 451.860k | 36.7 | $\begin{array}{r} \hline+0.2 \\ -0.5 \end{array}$ | +0.0 | +0.1 | +9.1 | +0.0 | 45.6 | 46.8 | -1.2 | Line |
|  | $\begin{aligned} & \text { 639.337k } \\ & \text { Ave } \end{aligned}$ | 31.5 | $\begin{array}{r} \hline+0.3 \\ -0.4 \end{array}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 40.5 | 46.0 | -5.5 | Line |
| $\wedge$ | 639.336k | 35.9 | $\begin{array}{r} +0.3 \\ -0.4 \\ \hline \end{array}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 44.9 | 46.0 | -1.1 | Line |
|  | $\begin{aligned} & \text { 207.325k } \\ & \text { Ave } \end{aligned}$ | 34.0 | $\begin{array}{r} \hline+0.2 \\ -1.2 \end{array}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 42.1 | 53.3 | -11.2 | Line |
| $\wedge$ | 207.324k | 44.2 | $\begin{gathered} \hline+0.2 \\ -1.2 \end{gathered}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 52.3 | 53.3 | -1.0 | Line |
|  | $\begin{aligned} & \text { 673.808k } \\ & \text { Ave } \end{aligned}$ | 25.6 | $\begin{array}{r} \hline+0.3 \\ -0.4 \\ \hline \end{array}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 34.6 | 46.0 | -11.4 | Line |
| $\wedge$ | 673.808k | 35.2 | $\begin{array}{r} +0.3 \\ -0.4 \end{array}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 44.2 | 46.0 | -1.8 | Line |
|  | $944.756 \mathrm{k}$ | $23.5$ | $\begin{array}{r} +0.2 \\ -0.3 \end{array}$ | $+0.0$ | +0.0 | +9.1 | $+0.0$ | 32.5 | 46.0 | -13.5 | Line |
| $\wedge$ | 944.756k | 35.2 | $\begin{array}{r} +0.2 \\ -0.3 \\ \hline \end{array}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 44.2 | 46.0 | -1.8 | Line |

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)
Customer:
Specification:
Ossia, Inc.
15.207 AC Mains - Average

Work Order \#: 102119
Test Type:
Tested By:
Conducted Emissions
Michael Atkinson
Date: 6/26/2020
Time: 10:04:41

Software:
EMITest 5.03.12

Sequence\#: 63
115 VAC 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Temperature: $20-25^{\circ} \mathrm{C}$
Humidity: 30-36\%
Pressure: $101-102 \mathrm{kPa}$
Method: ANSI C63.10 (2013)

Frequency range tested: $0.15-30 \mathrm{MHz}$
XYZ EUT orientations investigated, worst case reported.
Below $30 \mathrm{MHz}, 3 \mathrm{x}$ orthogonal axes investigated, above 30 MHz , Horizontal and Vertical Antenna polarities investigated, worst case reported.

Investigated Radiated Spurious Emissions of Integrated Raspberry Pi 4 module while running the 5 GHz Wi-Fi radio continuously. Customer was provided a worst case script of maximum power, running on Channel 36 ( 5180 MHz ) at worst case data rate for spurious emissions. Also investigated Channel $140(5700 \mathrm{MHz})$ but no emissions observed within 20 dB of 15.209 limit.

EUT connected to support laptop via USB cable.
EUT connected to support PoE box with 2 x Ethernet cables for power.
Support laptop connected to PoE box with $1 \times$ Ethernet cable.
PoE box and support Laptop are located remotely. (Configuration 1)

Integrated Module Info
Raspberry Pi 4B (FCC ID 2ABCB-RPI4B)

Ossia, Inc. WO\#: 102119 Sequence\#: 63 Date: 6/26/2020 15.207 AC Mains - Average Test Lead: 115 VAC 60 Hz Neutral



Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |
| T1 | AN02611 | High Pass Filter | HE9615-150K-50-720B | $1 / 10 / 2020$ | $1 / 10 / 2022$ |
| T2 | ANP06540 | Cable | Heliax | Heliax | $8 / 23 / 2019$ |
| T3 | ANP06515 | Cable | $768-10$ | $6 / 29 / 2018$ | $8 / 23 / 2021$ |
| T4 | ANP06219 | Attenuator | $4 / 7 / 2020$ | $4 / 2020$ |  |
|  | AN01311 | 50uH LISN-Line1 (L) | $3816 / 2$ | $2 / 24 / 2020$ | $2 / 24 / 2022$ |
| T5 | AN01311 | 50uH LISN-Line2 (N) | $3816 / 2$ | $2 / 24 / 2020$ | $2 / 24 / 2022$ |



Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)
Customer:
Specification:
Ossia, Inc.
15.207 AC Mains - Average

Work Order \#: 102119
Test Type:
Tested By:
Conducted Emissions
Date: 6/26/2020
Michael Atkinson
Time: 14:13:25

Software:
EMITest 5.03.12

Sequence\#: 78
115 VAC 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Test Conditions / Notes:
Temperature: $20-25^{\circ} \mathrm{C}$
Humidity: 30-36\%
Pressure: $101-102 \mathrm{kPa}$

Method: ANSI C63.10 (2013)
Frequency range tested: $0.15-30 \mathrm{MHz}$
XYZ EUT orientations investigated, worst case reported.
Below $30 \mathrm{MHz}, 3 \mathrm{x}$ orthogonal axes investigated, above 30 MHz , Horizontal and Vertical Antenna polarities investigated, worst case reported.

Investigated Radiated Spurious Emissions of Integrated Raspberry Pi 4 module while running the $2.4 \mathrm{GHz} \mathrm{Wi}-\mathrm{Fi}$ radio continuously. Customer was provided a worst case script of maximum power, running on Channel 1 $(2412 \mathrm{MHz})$ at worst case data rate for spurious emissions.

EUT connected to support laptop via USB cable.
EUT connected to AC adapter for power.
EUT connected to support Laptop via Ethernet cable.
Laptop is located remotely. (Configuration 2)
Integrated Module Info
Raspberry Pi 4B (FCC ID 2ABCB-RPI4B)

Ossia, Inc. WO\#: 102119 Sequence\#: 78 Date: 6/26/2020 15.207 AC Mains - Average Test Lead: 115 VAC 60 Hz Line


|  | Sweep Data | Readings | Peak Readings |
| :--- | :--- | :--- | :--- |
| $\times$ | Q Readings | Average Readings | Ambient |
| Software Version: 5.03 .12 |  | -15.207 AC Mains - Average | $2-15.207$ AC Mains - Quasi-peak |

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |
| T1 | AN02611 | High Pass Filter | HE9615-150K-50-720B | $1 / 10 / 2020$ | $1 / 10 / 2022$ |
| T2 | ANP06540 | Cable | Heliax | $8 / 23 / 2019$ | $8 / 23 / 2021$ |
| T3 | ANP06515 | Cable | Heliax | $6 / 29 / 2018$ | $6 / 29 / 2020$ |
| T4 | ANP06219 | Attenuator | $768-10$ | $4 / 7 / 2020$ | $4 / 7 / 2022$ |
| T5 | AN01311 | 50uH LISN-Line1 (L) | $3816 / 2$ | $2 / 24 / 2020$ | $2 / 24 / 2022$ |
|  | AN01311 | 50uH LISN-Line2 (N) | $3816 / 2$ | $2 / 24 / 2020$ | $2 / 24 / 2022$ |

Measurement Data: $\quad$ Reading listed by margin.
Test Lead: Line

| $\#$ | Freq | Rdng | T 1 | T 2 | T 3 | T 4 | Dist | Corr | Spec | Margin | Polar |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  |  |  | T 5 |  |  |  |  |  |  |  |  |
|  | MHz | $\mathrm{dB} \mu \mathrm{V}$ | dB | dB | dB | dB | Table | $\mathrm{dB} \mu \mathrm{V}$ | $\mathrm{dB} \mu \mathrm{V}$ | dB | Ant |
| 1 | 9.050 M | 38.6 | +0.1 | +0.0 | +0.2 | +9.1 | +0.0 | 47.5 | 50.0 | -2.5 | Line |
|  |  |  | -0.5 |  |  |  |  |  |  |  |  |
| 2 | 10.051 M | 38.6 | +0.1 | +0.0 | +0.2 | +9.1 | +0.0 | 47.5 | 50.0 | -2.5 | Line |


| 3 | 8.939M | 38.3 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | $+0.0$ | 47.2 | 50.0 | -2.8 | Line |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | 10.068 M | 38.3 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.2 | 50.0 | -2.8 | Line |
| 5 | 9.273 M | 38.2 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.1 | 50.0 | -2.9 | Line |
| 6 | 9.798 M | 38.2 | $\begin{array}{r} \hline+0.1 \\ -0.5 \\ \hline \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.1 | 50.0 | -2.9 | Line |
| 7 | 17.029 M | 38.0 | $\begin{array}{r} \hline+0.2 \\ -0.7 \\ \hline \end{array}$ | +0.1 | +0.2 | +9.1 | $+0.0$ | 46.9 | 50.0 | -3.1 | Line |
| 8 | 8.747M | 38.0 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | $+0.0$ | 46.9 | 50.0 | -3.1 | Line |
| 9 | 9.486 M | 37.9 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 46.8 | 50.0 | -3.2 | Line |
| 10 | 11.044 M | 37.7 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | $+0.0$ | 46.6 | 50.0 | -3.4 | Line |
| 11 | 8.439M | 37.6 | $\begin{array}{r} +0.1 \\ -0.5 \\ \hline \end{array}$ | +0.0 | +0.2 | +9.1 | $+0.0$ | 46.5 | 50.0 | -3.5 | Line |
| 12 | 8.156M | 37.7 | $\begin{array}{r} \hline+0.1 \\ -0.5 \\ \hline \end{array}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 46.5 | 50.0 | -3.5 | Line |
| 13 | 9.324 M | 37.6 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | $+0.0$ | 46.5 | 50.0 | -3.5 | Line |
| 14 | 8.849M | 37.6 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 46.5 | 50.0 | -3.5 | Line |
| $15$ | $9.516 \mathrm{M}$ <br> ve | 22.0 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 30.9 | 50.0 | -19.1 | Line |
| $\wedge$ | 9.516 M | 39.4 | $\begin{array}{r} \hline+0.1 \\ -0.5 \\ \hline \end{array}$ | +0.0 | +0.2 | +9.1 | $+0.0$ | 48.3 | 50.0 | -1.7 | Line |
|  | $\begin{aligned} & \text { ve } \\ & \text { ve } \end{aligned}$ | 21.7 | $\begin{array}{r} \hline+0.1 \\ -0.5 \\ \hline \end{array}$ | +0.0 | +0.2 | +9.1 | $+0.0$ | 30.6 | 50.0 | -19.4 | Line |
| $\wedge$ | 9.905 M | 40.0 | $\begin{array}{r} \hline+0.1 \\ -0.5 \\ \hline \end{array}$ | +0.0 | +0.2 | +9.1 | $+0.0$ | 48.9 | 50.0 | -1.1 | Line |
|  | $9.610 \mathrm{M}$ | 21.1 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 30.0 | 50.0 | -20.0 | Line |
| $\wedge$ | 9.610 M | 39.4 | $\begin{array}{r} \hline+0.1 \\ -0.5 \\ \hline \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 48.3 | 50.0 | -1.7 | Line |
|  | $9.110 \mathrm{M}$ <br> ve | 20.6 | $\begin{array}{r} \hline+0.1 \\ -0.5 \\ \hline \end{array}$ | +0.0 | +0.2 | +9.1 | $+0.0$ | 29.5 | 50.0 | -20.5 | Line |
| $\wedge$ | 9.110 M | 39.1 | $\begin{array}{r} +0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | $+0.0$ | 48.0 | 50.0 | -2.0 | Line |
|  | $8.687 \mathrm{M}$ | $20.2$ | $\begin{array}{r} \hline+0.1 \\ -0.5 \\ \hline \end{array}$ | $+0.0$ | +0.2 | +9.1 | $+0.0$ | 29.1 | 50.0 | -20.9 | Line |
| $\wedge$ | 8.687M | 38.9 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.8 | 50.0 | -2.2 | Line |
|  | $10.702 \mathrm{M}$ | $20.2$ | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 29.1 | 50.0 | -20.9 | Line |
| $\wedge$ | 10.702 M | 39.2 | $\begin{array}{r} +0.1 \\ -0.5 \\ \hline \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 48.1 | 50.0 | -1.9 | Line |

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)
Customer:
Specification:
Ossia, Inc.
15.207 AC Mains - Average

Work Order \#:
Test Type:
Tested By:
102119
Conducted Emissions
Michael Atkinson
Date: 6/26/2020

Software:
EMITest 5.03.12

Time: 14:09:01
Sequence\#: 77
115 VAC 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Test Conditions / Notes:
Temperature: $20-25^{\circ} \mathrm{C}$
Humidity: 30-36\%
Pressure: $101-102 \mathrm{kPa}$

Method: ANSI C63.10 (2013)
Frequency range tested: $0.15-30 \mathrm{MHz}$
XYZ EUT orientations investigated, worst case reported.
Below $30 \mathrm{MHz}, 3 \mathrm{x}$ orthogonal axes investigated, above 30 MHz , Horizontal and Vertical Antenna polarities investigated, worst case reported.

Investigated Radiated Spurious Emissions of Integrated Raspberry Pi 4 module while running the $2.4 \mathrm{GHz} \mathrm{Wi}-\mathrm{Fi}$ radio continuously. Customer was provided a worst case script of maximum power, running on Channel 1 $(2412 \mathrm{MHz})$ at worst case data rate for spurious emissions.

EUT connected to support laptop via USB cable.
EUT connected to AC adapter for power.
EUT connected to support Laptop via Ethernet cable.
Laptop is located remotely. (Configuration 2)
Integrated Module Info
Raspberry Pi 4B (FCC ID 2ABCB-RPI4B)

Ossia, Inc. WO\#: 102119 Sequence\#: 77 Date: 6/26/2020 15.207 AC Mains - Average Test Lead: 115 VAC 60 Hz Neutral



Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |
| T1 | AN02611 | High Pass Filter | HE9615-150K-50-720B | $1 / 10 / 2020$ | $1 / 10 / 2022$ |
| T2 | ANP06540 | Cable | Heliax | Heliax | $8 / 23 / 2019$ |
| T3 | ANP06515 | Cable | $768-10$ | $6 / 29 / 2018$ | $8 / 23 / 2021$ |
| T4 | ANP06219 | Attenuator | $4 / 29 / 2020$ |  |  |
|  | AN01311 | 50uH LISN-Line1 (L) | $3816 / 2$ | $2 / 24 / 2020$ | $4 / 7 / 2022$ |
| T5 | AN01311 | 50uH LISN-Line2 (N) | $3816 / 2$ | $2 / 24 / 2020$ | $2 / 24 / 2022$ |


| Measu | ment Data: | Reading listed by margin. |  |  |  | Test Lead: Neutral |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | Freq | Rdng | T1 | T2 | T3 | T4 | Dist | Corr | Spec | Margin | Polar |
|  | MHz | $\mathrm{dB} \mu \mathrm{V}$ | dB | dB | dB | dB | Table | $\mathrm{dB} \mu \mathrm{V}$ | $\mathrm{dB} \mu \mathrm{V}$ | dB | Ant |
| 1 | 4.895M | 32.2 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 41.1 | 46.0 | -4.9 | Neutr |
|  |  |  | -0.4 |  |  |  |  |  |  |  |  |
| 2 | 3.427 M | 31.6 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 40.6 | 46.0 | -5.4 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 3 | 3.575 M | 31.6 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 40.6 | 46.0 | -5.4 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 4 | 3.563 M | 31.3 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 40.3 | 46.0 | -5.7 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 5 | 3.003 M | 31.0 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 40.0 | 46.0 | -6.0 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 6 | 2.113 M | 30.9 | +0.2 | +0.0 | +0.1 | +9.1 | +0.0 | 40.0 | 46.0 | -6.0 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 7 | 3.391 M | 31.0 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 40.0 | 46.0 | -6.0 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 8 | 3.258M | 31.0 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 40.0 | 46.0 | -6.0 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 9 | 2.403 M | 30.9 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 39.9 | 46.0 | -6.1 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 10 | 153.981k | 41.4 | +0.8 | +0.0 | +0.0 | +9.1 | $+0.0$ | 49.6 | 55.8 | -6.2 | Neutr |
|  |  |  | -1.7 |  |  |  |  |  |  |  |  |
| 11 | 3.501 M | 30.7 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 39.7 | 46.0 | -6.3 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 12 | 2.505 M | 30.7 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 39.7 | 46.0 | -6.3 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 13 | 6.613 M | 34.8 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 43.7 | 50.0 | -6.3 | Neutr |
|  |  |  | -0.4 |  |  |  |  |  |  |  |  |
| 14 | 3.777 M | 30.7 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 39.7 | 46.0 | -6.3 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 15 | 3.031 M | 30.6 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 39.6 | 46.0 | -6.4 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 16 | 6.189M | 34.7 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 43.6 | 50.0 | -6.4 | Neutr |
|  |  |  | -0.4 |  |  |  |  |  |  |  |  |
| 17 | 155.762k | 41.0 | +0.8 | +0.0 | +0.0 | +9.1 | +0.0 | 49.2 | 55.7 | -6.5 | Neutr |
|  |  |  | -1.7 |  |  |  |  |  |  |  |  |
| 18 | 3.689M | 30.5 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 39.5 | 46.0 | -6.5 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 19 | 3.458M | 30.4 | +0.1 | $+0.0$ | +0.1 | +9.1 | +0.0 | 39.4 | 46.0 | -6.6 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 20 | 489.658k | 18.0 | +0.2 | +0.0 | +0.0 | +9.1 | +0.0 | 26.9 | 46.2 | -19.3 | Neutr |
|  | Ave |  | -0.4 |  |  |  |  |  |  |  |  |
| $\wedge$ | 489.657k | 32.8 | +0.2 | +0.0 | +0.0 | +9.1 | +0.0 | 41.7 | 46.2 | -4.5 | Neutr |
|  |  |  | -0.4 |  |  |  |  |  |  |  |  |

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)
Customer:
Specification:
Ossia, Inc.
15.207 AC Mains - Average

Work Order \#: 102119
Test Type:
Tested By:
Conducted Emissions
Michael Atkinson
EMITest 5.03.12

Date: 6/26/2020<br>Time: 14:20:34<br>Sequence\#: 79<br>115 VAC 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Test Conditions / Notes:
Temperature: $20-25^{\circ} \mathrm{C}$
Humidity: 30-36\%
Pressure: $101-102 \mathrm{kPa}$
Method: ANSI C63.10 (2013)

Frequency range tested: $0.15-30 \mathrm{MHz}$
XYZ EUT orientations investigated, worst case reported.
Below $30 \mathrm{MHz}, 3 \mathrm{x}$ orthogonal axes investigated, above 30 MHz , Horizontal and Vertical Antenna polarities investigated, worst case reported.

Investigated Radiated Spurious Emissions of Integrated Raspberry Pi 4 module while running the $5 \mathrm{GHz} \mathrm{Wi-Fi}$ radio continuously. Customer was provided a worst case script of maximum power, running on Channel 36 ( 5180 MHz ) at worst case data rate for spurious emissions. Also investigated Channel $140(5700 \mathrm{MHz})$ but no emissions observed within 20 dB of 15.209 limit.

EUT connected to support laptop via USB cable.
EUT connected to AC adapter for power.
EUT connected to support Laptop via Ethernet cable.
Laptop is located remotely. (Configuration 2)

Integrated Module Info
Raspberry Pi 4B (FCC ID 2ABCB-RPI4B)

Ossia, Inc. WO\#: 102119 Sequence\#: 79 Date: 6/26/2020 15.207 AC Mains - Average Test Lead: 115 VAC 60 Hz Line



Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |
| T1 | AN02611 | High Pass Filter | HE9615-150K-50-720B | $1 / 10 / 2020$ | $1 / 10 / 2022$ |
| T2 | ANP06540 | Cable | Heliax | Heliax | $8 / 23 / 2019$ |
| T3 | ANP06515 | Cable | $768-10$ | $6 / 29 / 2018$ | $8 / 23 / 2021$ |
| T4 | ANP06219 | Attenuator | $4 / 29 / 2020$ |  |  |
| T5 | AN01311 | 50uH LISN-Line1 (L) | $3816 / 2$ | $2 / 24 / 2020$ | $4 / 7 / 2022$ |
|  | AN01311 | 50uH LISN-Line2 (N) | $3816 / 2$ | $2 / 24 / 2022$ |  |

Measurement Data: Reading listed by margin. Test Lead: Line

| \# | Freq <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~T} 5 \\ & \mathrm{~dB} \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \\ & \hline \end{aligned}$ | $\begin{array}{r} \mathrm{T} 3 \\ \mathrm{~dB} \\ \hline \end{array}$ | T4 dB | Dist <br> Table | Corr <br> $\mathrm{dB} \mu \mathrm{V}$ | Spec <br> $\mathrm{dB} \mu \mathrm{V}$ | Margin <br> dB | Polar Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 10.312 M | 38.9 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.8 | 50.0 | -2.2 | Line |
| 2 | 10.935 M | 38.8 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.7 | 50.0 | -2.3 | Line |
| 3 | 8.952M | 38.7 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.6 | 50.0 | -2.4 | Line |
| 4 | 9.080M | 38.7 | $\begin{array}{r} \hline+0.1 \\ -0.5 \\ \hline \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.6 | 50.0 | -2.4 | Line |
| 5 | 10.492M | 38.7 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.6 | 50.0 | -2.4 | Line |
| 6 | 9.897 M | 38.6 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.5 | 50.0 | -2.5 | Line |
| 7 | 10.218M | 38.6 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.5 | 50.0 | -2.5 | Line |
| 8 | 10.688M | 38.6 | $\begin{array}{r} \hline+0.1 \\ -0.5 \\ \hline \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.5 | 50.0 | -2.5 | Line |
| 9 | 9.452 M | 38.5 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.4 | 50.0 | -2.6 | Line |
| 10 | 10.042M | 38.5 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | $+0.0$ | 47.4 | 50.0 | -2.6 | Line |
| 11 | 10.615M | 38.5 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | $+0.0$ | 47.4 | 50.0 | -2.6 | Line |
| 12 | 9.401 M | 38.4 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.3 | 50.0 | -2.7 | Line |
| 13 | 10.136M | 38.3 | $\begin{array}{r} \hline+0.1 \\ -0.5 \\ \hline \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.2 | 50.0 | -2.8 | Line |
| 14 | 10.333M | 38.3 | $\begin{array}{r} \hline+0.1 \\ -0.5 \\ \hline \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.2 | 50.0 | -2.8 | Line |
| 15 | 9.760 M | 38.2 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 47.1 | 50.0 | -2.9 | Line |
| 16 | 9.957 M | 38.2 | $\begin{array}{r} +0.1 \\ -0.5 \\ \hline \end{array}$ | +0.0 | +0.2 | +9.1 | $+0.0$ | 47.1 | 50.0 | -2.9 | Line |
| $17$ | $10.448 \mathrm{M}$ <br> ve | 22.4 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 31.3 | 50.0 | -18.7 | Line |
| $\wedge$ | 10.448M | 39.6 | $\begin{array}{r} +0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 48.5 | 50.0 | -1.5 | Line |
|  | $\begin{aligned} & 9.743 \mathrm{M} \\ & \mathrm{ve} \end{aligned}$ | 22.1 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 31.0 | 50.0 | -19.0 | Line |
| $\wedge$ | 9.743 M | 40.2 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 49.1 | 50.0 | -0.9 | Line |
|  | ${ }^{9.563 \mathrm{M}}$ | $22.0$ | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 30.9 | 50.0 | -19.1 | Line |
| $\wedge$ | 9.563 M | 39.2 | $\begin{array}{r} \hline+0.1 \\ -0.5 \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 48.1 | 50.0 | -1.9 | Line |
| $23$ | $\begin{aligned} & 9.657 \mathrm{M} \\ & \hline \end{aligned}$ | $21.7$ | $\begin{array}{r} \hline+0.1 \\ -0.5 \\ \hline \end{array}$ | +0.0 | +0.2 | +9.1 | +0.0 | 30.6 | 50.0 | -19.4 | Line |
| $\wedge$ | 9.657 M | 39.0 | $\begin{array}{r} +0.1 \\ -0.5 \\ \hline \end{array}$ | +0.0 | +0.2 | +9.1 | $+0.0$ | 47.9 | 50.0 | -2.1 | Line |

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Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)
Customer:
Specification:
Ossia, Inc.
15.207 AC Mains - Average

Work Order \#: 102119
Test Type:
Tested By:
Conducted Emissions
Date: 6/26/2020
Michael Atkinson
Time: 14:23:41

Software:
EMITest 5.03.12

Sequence\#: 80
115 VAC 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Test Conditions / Notes:
Temperature: $20-25^{\circ} \mathrm{C}$
Humidity: 30-36\%
Pressure: $101-102 \mathrm{kPa}$
Method: ANSI C63.10 (2013)

Frequency range tested: $0.15-30 \mathrm{MHz}$
XYZ EUT orientations investigated, worst case reported.
Below $30 \mathrm{MHz}, 3 \mathrm{x}$ orthogonal axes investigated, above 30 MHz , Horizontal and Vertical Antenna polarities investigated, worst case reported.

Investigated Radiated Spurious Emissions of Integrated Raspberry Pi 4 module while running the 5 GHz Wi -Fi radio continuously. Customer was provided a worst case script of maximum power, running on Channel 36 ( 5180 MHz ) at worst case data rate for spurious emissions. Also investigated Channel $140(5700 \mathrm{MHz})$ but no emissions observed within 20 dB of 15.209 limit.

EUT connected to support laptop via USB cable.
EUT connected to AC adapter for power.
EUT connected to support Laptop via Ethernet cable.
Laptop is located remotely. (Configuration 2)

Integrated Module Info
Raspberry Pi 4B (FCC ID 2ABCB-RPI4B)

Ossia, Inc. WO\#: 102119 Sequence\#: 80 Date: 6/26/2020 15.207 AC Mains - Average Test Lead: 115 VAC 60 Hz Neutral



Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |
| T1 | AN02611 | High Pass Filter | HE9615-150K-50-720B | $1 / 10 / 2020$ | $1 / 10 / 2022$ |
| T2 | ANP06540 | Cable | Heliax | Heliax | $8 / 23 / 2019$ |
| T3 | ANP06515 | Cable | $768-10$ | $6 / 29 / 2018$ | $8 / 23 / 2021$ |
| T4 | ANP06219 | Attenuator | $3 / 29 / 2020$ |  |  |
| T5 | AN01311 | 50uH LISN-Line1 (L) | $3816 / 2$ | $4 / 7 / 2020$ | $4 / 7 / 2022$ |
|  | AN01311 | 50uH LISN-Line2 (N) | $3816 / 2$ | $2 / 24 / 2020$ | $2 / 24 / 2022$ |


| Measu | ement Data | Reading listed by margin. |  |  |  | Test Lead: Neutral |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# | Freq | Rdng | T1 | T2 | T3 | T4 | Dist | Corr | Spec | Margin | Polar |
|  | MHz | $\mathrm{dB} \mu \mathrm{V}$ | dB | dB | dB | dB | Table | $\mathrm{dB} \mu \mathrm{V}$ | $\mathrm{dB} \mu \mathrm{V}$ | dB | Ant |
| 1 | 150.000k | 42.1 | +2.5 | +0.0 | +0.0 | +9.1 | +0.0 | 51.9 | 56.0 | -4.1 | Neutr |
|  |  |  | -1.8 |  |  |  |  |  |  |  |  |
| 2 | 450.045k | 32.9 | +0.2 | +0.0 | +0.1 | +9.1 | +0.0 | 41.8 | 46.9 | -5.1 | Neutr |
|  |  |  | -0.5 |  |  |  |  |  |  |  |  |
| 3 | 4.771 M | 31.8 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 40.7 | 46.0 | -5.3 | Neutr |
|  |  |  | -0.4 |  |  |  |  |  |  |  |  |
| 4 | 435.833k | 32.6 | +0.2 | +0.0 | +0.1 | +9.1 | +0.0 | 41.5 | 47.1 | -5.6 | Neutr |
|  |  |  | -0.5 |  |  |  |  |  |  |  |  |
| 5 | 190.452k | 40.1 | +0.3 | +0.0 | +0.0 | +9.1 | +0.0 | 48.2 | 54.0 | -5.8 | Neutr |
|  |  |  | -1.3 |  |  |  |  |  |  |  |  |
| 6 | 212.459k | 39.0 | +0.3 | +0.0 | +0.0 | +9.1 | +0.0 | 47.3 | 53.1 | -5.8 | Neutr |
|  |  |  | -1.1 |  |  |  |  |  |  |  |  |
| 7 | 4.978M | 31.3 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 40.2 | 46.0 | -5.8 | Neutr |
|  |  |  | -0.4 |  |  |  |  |  |  |  |  |
| 8 | 173.684k | 40.8 | +0.4 | +0.0 | +0.0 | +9.1 | +0.0 | 48.8 | 54.8 | -6.0 | Neutr |
|  |  |  | -1.5 |  |  |  |  |  |  |  |  |
| 9 | 186.679k | 40.0 | +0.3 | +0.0 | +0.0 | +9.1 | +0.0 | 48.1 | 54.2 | -6.1 | Neutr |
|  |  |  | -1.3 |  |  |  |  |  |  |  |  |
| 10 | 197.368k | 39.2 | +0.2 | +0.0 | +0.0 | +9.1 | $+0.0$ | 47.3 | 53.7 | -6.4 | Neutr |
|  |  |  | -1.2 |  |  |  |  |  |  |  |  |
| 11 | 7.130M | 34.5 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 43.4 | 50.0 | -6.6 | Neutr |
|  |  |  | -0.4 |  |  |  |  |  |  |  |  |
| 12 | 192.443k | 39.1 | +0.3 | +0.0 | +0.0 | +9.1 | +0.0 | 47.2 | 53.9 | -6.7 | Neutr |
|  |  |  | -1.3 |  |  |  |  |  |  |  |  |
| 13 | 182.906k | 39.6 | +0.4 | +0.0 | +0.0 | +9.1 | +0.0 | 47.7 | 54.4 | -6.7 | Neutr |
|  |  |  | -1.4 |  |  |  |  |  |  |  |  |
| 14 | 3.295 M | 30.3 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 39.3 | 46.0 | -6.7 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 15 | 3.439 M | 30.3 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 39.3 | 46.0 | -6.7 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 16 | 3.400 M | 30.3 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 39.3 | 46.0 | -6.7 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 17 | 1.940M | 30.1 | +0.2 | +0.0 | +0.1 | +9.1 | +0.0 | 39.2 | 46.0 | -6.8 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 18 | 2.363 M | 30.2 | +0.1 | +0.0 | +0.1 | +9.1 | +0.0 | 39.2 | 46.0 | -6.8 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 19 | 3.406M | 30.1 | +0.1 | $+0.0$ | +0.1 | +9.1 | +0.0 | 39.1 | 46.0 | -6.9 | Neutr |
|  |  |  | -0.3 |  |  |  |  |  |  |  |  |
| 20 | 155.030k | 29.0 | +0.8 | +0.0 | +0.0 | +9.1 | +0.0 | 37.2 | 55.7 | -18.5 | Neutr |
|  | Ave |  | -1.7 |  |  |  |  |  |  |  |  |
| $\wedge$ | 155.030k | 46.2 | +0.8 | +0.0 | +0.0 | +9.1 | +0.0 | 54.4 | 55.7 | -1.3 | Neutr |
|  |  |  | -1.7 |  |  |  |  |  |  |  |  |

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)
Customer:
Specification:
Ossia, Inc.
15.209 Radiated Emissions

Work Order \#:
Test Type:
Tested By:
102119
Maximized Emissions
Date: 6/29/2020
Time: 11:03:14

Software:
Michael Atkinson
Sequence\#: 7
EMITest 5.03.12

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Temperature: $20-25^{\circ} \mathrm{C}$
Humidity: 30-36\%
Pressure: $101-102 \mathrm{kPa}$
Method: ANSI C63.10 (2013)

Frequency range tested: $9 \mathrm{kHz}-25 \mathrm{GHz}$
XYZ EUT orientations investigated, worst case reported.
Below 30MHz, 3 x orthogonal axes investigated, above 30 MHz , Horizontal and Vertical Antenna polarities investigated, worst case reported.

Investigated Radiated Spurious Emissions of Integrated Raspberry Pi 4 module while running the $2.4 \mathrm{GHz} \mathrm{Wi}-\mathrm{Fi}$ radio continuously. Customer was provided a worst case script of maximum power, running on Channel 1 $(2412 \mathrm{MHz})$ at worst case data rate for spurious emissions.

EUT connected to support laptop via USB cable.
EUT connected to support PoE box with $2 \times$ Ethernet cables for power.
Support laptop connected to PoE box with $1 \times$ Ethernet cable.
PoE box and support Laptop are located remotely.
The manufacturer declares the other power configuration is unlikely to affect the Radiated Spurious Emissions of the 2.4 GHz WiFi from the module, however, AC emissions will be run in both PoE and AC Adapter configurations.

No emissions observed above 18 GHz , values provided are noise floor.
Integrated Module Info
Raspberry Pi 4B (FCC ID 2ABCB-RPI4B)

> Ossia, Inc. WO\#: 102119 Sequence\#: 7 Date: 6/29/2020 15.209 Radiated Emissions Test Distance: 3 Meters Various


Test Equipment:

| ID | Asset \# | Description | Model | Calibration <br> Date | Cal Due <br> Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |
| T2 | ANP06540 | Cable | Heliax | $8 / 23 / 2019$ | $8 / 23 / 2021$ |
| T3 | ANP05305 | Cable | ETSI-50T | $9 / 6 / 2019$ | $9 / 6 / 2021$ |
| T4 | AN02307 | Preamp | $8447 D$ | $1 / 10 / 2020$ | $1 / 10 / 2022$ |
| T5 | ANP05360 | Cable | RG214 | $2 / 3 / 2020$ | $2 / 3 / 2022$ |
| T6 | ANP06123 | Attenuator | 18N-6 | $4 / 5 / 2019$ | $4 / 5 / 2021$ |
| T7 | AN03628 | Biconilog Antenna | $3142 E$ | $6 / 11 / 2019$ | $6 / 11 / 2021$ |
| T8 | AN03540 | Preamp | $83017 A$ | $5 / 13 / 2019$ | $5 / 13 / 2021$ |
| T9 | AN01467 | Horn Antenna-ANSI C63.5 | 3115 | $7 / 5 / 2019$ | $7 / 5 / 2021$ |
|  |  | Calibration | Heliax |  |  |
| T10 | ANP06515 | Cable | CLU40-KMKM-02.00F | $1 / 17 / 2019$ | $1 / 17 / 2021$ |
| T11 | ANP07504 | Cable | 11 SH10-00313 | $1 / 22 / 2019$ | $1 / 22 / 2021$ |
| T12 | AN03116 | High Pass Filter | AMFW-5F-12001800-20- | $4 / 26 / 2019$ | $4 / 26 / 2021$ |
| T13 | AN02741 | Active Horn Antenna | $10 P$ |  |  |
| T14 | AN02742 | Active Horn Antenna | AMFW-5F-18002650-20- | $10 / 16 / 2018$ | $10 / 16 / 2020$ |
|  |  |  | $10 P$ |  |  |
| T15 | ANP06678 | Cable | $32026-29801-29801-144$ | $2 / 20 / 2020$ | $2 / 20 / 2022$ |
| T16 | AN02763- | Waveguide | Multiple | $4 / 28 / 2020$ | $4 / 28 / 2022$ |
|  | 69 |  | $32026-29801-29801-18$ | $8 / 7 / 2019$ | $8 / 7 / 2021$ |
| T17 | ANP07212 | Cable | $32026-29801-29801-18$ | $8 / 7 / 2019$ | $8 / 7 / 2021$ |
| T18 | ANP07211 | Cable | 5502 | $10 / 2 / 2019$ | $10 / 2 / 2021$ |
| T19 | AN00052 | Loop Antenna | PE7004-6 |  |  |
|  | ANP07226 | Attenuator |  | $5 / 4 / 2022$ |  |



| $\begin{aligned} & 3454.728 \mathrm{M} \\ & \mathrm{QP} \end{aligned}$ |  | 45.7 | +0.0 | +0.2 | +1.0 | -27.9 | $+0.0$ | 44.3 | 46.0 | -1.7 | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | +1.4 | +5.8 | +18.1 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
|  | ^ 454.728 M | 48.1 | +0.0 | +0.2 | +1.0 | -27.9 | +0.0 | 46.7 | 46.0 | +0.7 | Vert |
|  |  |  | +1.4 | +5.8 | +18.1 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
|  | $\begin{aligned} & 5{ }_{\mathrm{QP}}{ }^{42.543 \mathrm{M}} \\ & \hline \end{aligned}$ | 45.8 | +0.0 | +0.1 | +0.3 | -28.0 | +0.0 | 35.2 | 40.0 | -4.8 | Vert |
|  |  |  | +0.3 | +5.8 | +10.9 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
|  | 6333.600 M | 45.1 | +0.0 | +0.2 | +0.9 | -27.1 | +0.0 | 40.8 | 46.0 | -5.2 | Vert |
|  |  |  | +1.2 | +5.8 | +14.7 | $+0.0$ |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | $+0.0$ |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| $\begin{aligned} & 7333.346 \mathrm{M} \\ & \mathrm{QP} \end{aligned}$ |  | 44.5 | +0.0 | +0.2 | +0.9 | -27.1 | +0.0 | 40.2 | 46.0 | -5.8 | Vert |
|  |  | +1.2 | +5.8 | +14.7 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 8 | 4897.000M |  | 42.8 | +0.0 | +0.9 | +0.0 | +0.0 | +0.0 | 47.8 | 54.0 | -6.2 | Vert |
|  |  |  |  | +0.0 | +0.0 | +0.0 | -33.6 |  |  |  |  |  |
|  |  |  |  | +32.5 | +4.2 | +0.5 | +0.5 |  |  |  |  |  |
|  |  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  | +0.0 |  | +0.0 | +0.0 |  |  |  |  |  |  |  |
| 9 | 451.000M | 41.0 | +0.0 | +0.2 | +1.0 | -27.9 | +0.0 | 39.5 | 46.0 | -6.5 | Vert |  |
|  |  |  | +1.4 | +5.8 | +18.0 | $+0.0$ |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | $+0.0$ |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | $+0.0$ |  |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |  |
| $\begin{gathered} 10 \quad 468.400 \mathrm{M} \\ \mathrm{QP} \end{gathered}$ |  | 39.2 | +0.0 | +0.3 | +1.1 | -28.0 | +0.0 | 38.0 | 46.0 | -8.0 | Horiz |  |
|  |  | +1.4 | +5.8 | +18.2 | $+0.0$ |  |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
|  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |  |
|  | ^ 468.400 M |  | 42.2 | +0.0 | +0.3 | +1.1 | -28.0 | +0.0 | 41.0 | 46.0 | -5.0 | Horiz |
|  |  |  |  | +1.4 | +5.8 | +18.2 | +0.0 |  |  |  |  |  |
|  |  |  |  | +0.0 | +0.0 | +0.0 | $+0.0$ |  |  |  |  |  |
|  |  |  |  | +0.0 | +0.0 | +0.0 | $+0.0$ |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |  |


| 124900.000 MAve |  | 40.8 | +0.0 | +0.9 | +0.0 | +0.0 | +0.0 | 45.8 | 54.0 | -8.2 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | +0.0 | +0.0 | +0.0 | -33.6 |  |  |  |  |  |
|  |  |  | +32.5 | +4.2 | +0.5 | +0.5 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| $\wedge$ | 4900.000M | 44.4 | +0.0 | +0.9 | +0.0 | +0.0 | $+0.0$ | 49.4 | 54.0 | -4.6 | Horiz |
|  |  |  | +0.0 | +0.0 | +0.0 | -33.6 |  |  |  |  |  |
|  |  |  | +32.5 | +4.2 | +0.5 | +0.5 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 14 | 125.100M | 47.5 | +0.0 | +0.1 | +0.5 | -27.6 | +0.0 | 34.8 | 43.5 | -8.7 | Vert |
|  |  |  | +0.7 | +5.8 | +7.8 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 15 | $Q^{41.600 \mathrm{M}}$ | 41.3 | +0.0 | +0.1 | +0.3 | -28.0 | +0.0 | 31.2 | 40.0 | -8.8 | Vert |
|  |  |  | +0.3 | +5.8 | +11.4 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| $\wedge$ | 41.600M | 50.0 | +0.0 | +0.1 | +0.3 | -28.0 | $+0.0$ | 39.9 | 40.0 | -0.1 | Vert |
|  |  |  | +0.3 | +5.8 | +11.4 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 17 | 30.000 M | 26.2 | +0.0 | +0.1 | +0.0 | +0.0 | +0.0 | 30.8 | 40.0 | -9.2 | Perp |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.3 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +4.2 |  |  |  |  |  |  |
| 18 | 4823.970M | 38.6 | +0.0 | +0.9 | +0.0 | +0.0 | +0.0 | 43.5 | 54.0 | -10.5 | Vert |
|  |  |  | +0.0 | +0.0 | +0.0 | -33.6 |  |  |  |  |  |
|  |  |  | +32.4 | +4.1 | +0.5 | +0.6 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 19 | 1530.000M | 47.7 | +0.0 | +0.5 | +0.0 | +0.0 | +0.0 | 40.5 | 54.0 | -13.5 | Horiz |
|  |  |  | +0.0 | +0.0 | +0.0 | -35.3 |  |  |  |  |  |
|  |  |  | +25.2 | +2.2 | +0.2 | $+0.0$ |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |
| 20 | 240.500M | 39.2 | +0.0 | +0.2 | +0.8 | -27.1 | +0.0 | 31.6 | 46.0 | -14.4 | Vert |
|  |  |  | +0.9 | +5.8 | +11.8 | $+0.0$ |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | $+0.0$ |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 | +0.0 |  |  |  |  |  |
|  |  |  | +0.0 | +0.0 | +0.0 |  |  |  |  |  |  |


| $\begin{aligned} & 21 \text { 3619.430M } \\ & \text { Ave } \end{aligned}$ | 30.3 | $\begin{array}{r} +0.0 \\ +0.0 \\ +3.4 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.8 \\ & +0.0 \\ & +3.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{gathered} +0.0 \\ -33.8 \\ +0.8 \\ +0.0 \end{gathered}$ | +0.0 | 32.7 | 54.0 | -21.3 | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ^ 3619.450M | 42.5 | $\begin{array}{r} +0.0 \\ +0.0 \\ +30.4 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.8 \\ & +0.0 \\ & +3.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.6 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ -33.8 \\ +0.8 \\ +0.0 \end{array}$ | +0.0 | 44.9 | 54.0 | -9.1 | Vert |
| $\begin{array}{cc} 23 & \begin{array}{c} 12060.000 \\ M \end{array} \end{array}$ | 36.7 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -13.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.4 \\ & +0.0 \\ & +6.8 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | +0.0 | 31.9 | 54.0 | -22.1 | Horiz |
| $\begin{aligned} & 24 \text { 4823.970M } \\ & \text { Ave } \end{aligned}$ | 24.9 | $\begin{array}{r} +0.0 \\ +0.0 \\ +32.4 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.9 \\ & +0.0 \\ & +4.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{gathered} +0.0 \\ -33.6 \\ +0.6 \\ +0.0 \end{gathered}$ | +0.0 | 29.8 | 54.0 | -24.2 | Horiz |
| 25 28.505M | 38.1 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +4.8 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | 3.3 | 29.5 | -26.2 | Groun |
| 26 1.984M | 32.8 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.1 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +9.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | 2.4 | 29.5 | -27.1 | Para |
| $\begin{gathered} 27 \begin{array}{c} 24119.900 \\ \mathrm{M} \\ \text { Ave } \end{array} . \end{gathered}$ | 25.9 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +1.0 \\ & \hline \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ +13.2 \\ +1.0 \\ \hline \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +9.8 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +1.9 \end{aligned}$ | $+0.0$ | 26.4 | 54.0 | -27.6 | Vert |
| 28 27.907M | 32.9 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.3 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +5.1 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | -1.6 | 29.5 | -31.1 | Perp |

$\left.\begin{array}{|cccccccccccc|}\hline 29 & 14472.000 & 26.8 & +0.0 & +1.3 & +0.0 & +0.0 & +0.0 & 21.4 & 54.0 & -32.6 & \text { Horiz } \\ & \text { M } & & +0.0 & +0.0 & +0.0 & +0.0 & & & & & \\ & \text { Ave } & & +0.0 & +8.1 & +0.0 & +0.0 & & & & \\ & & & -14.8 & +0.0 & +0.0 & +0.0 & & & & \\ & & & +0.0 & +0.0 & +0.0 & & & & & \\ \hline & & 14472.000 & 38.2 & +0.0 & +1.3 & +0.0 & +0.0 & +0.0 & 32.8 & 54.0 & -21.2\end{array}\right)$ Horiz 1

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)
Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:
Ossia, Inc.
15.209 Radiated Emissions

102119
Maximized Emissions
Michael Atkinson
EMITest 5.03.12

Date: 6/29/2020
Time: 10:26:37
Sequence\#: 8

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Temperature: $20-25^{\circ} \mathrm{C}$
Humidity: 30-36\%
Pressure: $101-102 \mathrm{kPa}$
Method: ANSI C63.10 (2013)
Frequency range tested: $9 \mathrm{kHz}-40 \mathrm{GHz}$
XYZ EUT orientations investigated, worst case reported.
Below $30 \mathrm{MHz}, 3 \mathrm{x}$ orthogonal axes investigated, above 30 MHz , Horizontal and Vertical Antenna polarities investigated, worst case reported.

Investigated Radiated Spurious Emissions of Integrated Raspberry Pi 4 module while running the 5 GHz Wi-Fi radio continuously. Customer was provided a worst case script of maximum power, running on Channel 36 ( 5180 MHz ) at worst case data rate for spurious emissions. Also investigated Channel $140(5700 \mathrm{MHz})$ but no emissions observed within 20 dB of 15.209 limit.

EUT connected to support laptop via USB cable.
EUT connected to support PoE box with $2 \times$ Ethernet cables for power.
Support laptop connected to PoE box with $1 \times$ Ethernet cable.
PoE box and support Laptop are located remotely.
The manufacturer declares the other power configuration is unlikely to affect the Radiated Spurious Emissions of the 5 GHz WiFi from the module, however, AC emissions will be run in both PoE and AC Adapter configurations.

No emissions observed above 18 GHz , values provided are noise floor.
Integrated Module Info
Raspberry Pi 4B (FCC ID 2ABCB-RPI4B)

Ossia, Inc. WO\#: 102119 Sequence\#\#: 8 Date: 6/29/2020 15.209 Radiated Emissions Test Distance: 3 Meters Various


Test Equipment:

| ID | Asset \# | Description | Model | Calibration <br> Date | Cal Due <br> Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02673 | Spectrum Analyzer | E4446A | $2 / 22 / 2019$ | $2 / 22 / 2021$ |
| T2 | ANP06540 | Cable | Heliax | $8 / 23 / 2019$ | $8 / 23 / 2021$ |
| T3 | ANP05305 | Cable | ETSI-50T | $9 / 6 / 2019$ | $9 / 6 / 2021$ |
| T4 | AN02307 | Preamp | $8447 D$ | $1 / 10 / 2020$ | $1 / 10 / 2022$ |
| T5 | ANP05360 | Cable | RG214 | $2 / 3 / 2020$ | $2 / 3 / 2022$ |
| T6 | ANP06123 | Attenuator | 18N-6 | $4 / 5 / 2019$ | $4 / 5 / 2021$ |
| T7 | AN03628 | Biconilog Antenna | $3142 E$ | $6 / 11 / 2019$ | $6 / 11 / 2021$ |
| T8 | AN03540 | Preamp | $83017 A$ | $5 / 13 / 2019$ | $5 / 13 / 2021$ |
| T9 | AN01467 | Horn Antenna-ANSI | 3115 | $7 / 5 / 2019$ | $7 / 5 / 2021$ |
| T10 | ANP06515 | C6able |  | $6 / 29 / 2018$ | $6 / 29 / 2020$ |
| T11 | ANP07504 | Cable | CLU40-KMKM-02.00F | $1 / 17 / 2019$ | $1 / 17 / 2021$ |
|  | AN03116 | High Pass Filter | $11 S H 10-00313$ | $1 / 22 / 2019$ | $1 / 22 / 2021$ |
| T12 | AN02741 | Active Horn Antenna | AMFW-5F-12001800-20-10P | $4 / 26 / 2019$ | $4 / 26 / 2021$ |
| T13 | AN02742 | Active Horn Antenna | AMFW-5F-18002650-20-10P | $10 / 16 / 2018$ | $10 / 16 / 2020$ |
| T14 | ANP06678 | Cable | $32026-29801-29801-144$ | $2 / 20 / 2020$ | $2 / 20 / 2022$ |
| T15 | AN02763-69 | Waveguide | Multiple | $4 / 28 / 2020$ | $4 / 28 / 2022$ |
| T16 | ANP07212 | Cable | $32026-29801-29801-18$ | $8 / 7 / 2019$ | $8 / 7 / 2021$ |
| T17 | ANP07211 | Cable | $32026-29801-29801-18$ | $8 / 7 / 2019$ | $8 / 7 / 2021$ |
| T18 | AN00052 | Loop Antenna | 6502 | $5 / 4 / 2020$ | $5 / 4 / 2022$ |
| T19 | ANP07226 | Attenuator | PE7004-6 | $10 / 2 / 2019$ | $10 / 2 / 2021$ |
| T20 | AN02743 | Active Horn Antenna | AMFW-5F-260400-33-8P | $4 / 26 / 2019$ | $4 / 26 / 2021$ |
| T21 | AN02764-70 | Waveguide | Multiple | $4 / 28 / 2020$ | $4 / 28 / 2022$ |



| $\begin{aligned} & 3451.000 \mathrm{M} \\ & \mathrm{QP} \end{aligned}$ | 42.9 | $\begin{aligned} & +0.0 \\ & +1.4 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +5.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +1.0 \\ +18.0 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{array}{r} -27.9 \\ +0.0 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 41.4 | 46.0 | -4.6 | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{cc} 4 & 13472.000 \\ M \end{array}$ | 45.9 | $\begin{array}{r} +0.0 \\ +0.0 \\ +40.5 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+1.3 \\ & +0.0 \\ & +7.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -33.7 \\ -14.5 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 48.0 | 54.0 | -6.0 | Vert |
| $\begin{aligned} & 5 \mathrm{QP}^{45.500 \mathrm{M}} \\ & \mathrm{Q}^{2} \end{aligned}$ | 45.4 | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +5.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.3 \\ & +9.4 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} -28.0 \\ +0.0 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 33.4 | 40.0 | -6.6 | Vert |
| 6 3106.000M | 41.8 | $\begin{array}{r} +0.0 \\ +0.0 \\ +29.3 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.8 \\ & +0.0 \\ & +3.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.4 \\ & +0.0 \\ & +5.9 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -34.0 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 47.2 | 54.0 | -6.8 | Vert |
| 7 2161.000M | 42.8 | $\begin{array}{r} +0.0 \\ +0.0 \\ +27.8 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.6 \\ & +0.0 \\ & +2.4 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.2 \\ & +0.0 \\ & +5.9 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -34.4 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 45.3 | 54.0 | -8.7 | Vert |
| $8 \quad 125.100 \mathrm{M}$ | 47.2 | $\begin{aligned} & +0.0 \\ & +0.7 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +5.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.5 \\ & +7.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} -27.6 \\ +0.0 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 34.5 | 43.5 | -9.0 | Vert |
| 9 1837.000M | 44.0 | $\begin{array}{r} +0.0 \\ +0.0 \\ +26.4 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.5 \\ & +0.0 \\ & +2.3 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.2 \\ & +0.0 \\ & +5.9 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -34.8 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 44.5 | 54.0 | -9.5 | Vert |
| $10 \quad 96.900 \mathrm{M}$ | 46.3 | $\begin{aligned} & +0.0 \\ & +0.6 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +5.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.5 \\ & +7.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline-27.7 \\ +0.0 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 33.4 | 43.5 | -10.1 | Vert |


| $\begin{aligned} & 11 \mathrm{QP}^{44.500 \mathrm{M}} \\ & \\ & \hline \end{aligned}$ | 41.2 | $\begin{aligned} & +0.0 \\ & +0.4 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +5.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.3 \\ & +9.9 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} -28.0 \\ +0.0 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 29.7 | 40.0 | -10.3 | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 1531.000M | 44.5 | $\begin{array}{r} +0.0 \\ +0.0 \\ +25.2 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.5 \\ & +0.0 \\ & +2.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.2 \\ & +0.0 \\ & +5.9 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -35.3 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 43.2 | 54.0 | -10.8 | Vert |
| 131108.000 M | 46.4 | $\begin{array}{r} +0.0 \\ +0.0 \\ +24.7 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & \hline+0.4 \\ & +0.0 \\ & +1.8 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.1 \\ & +0.0 \\ & +5.9 \end{aligned}$ | $\begin{gathered} +0.0 \\ -36.7 \\ +0.0 \\ +0.0 \\ +0.0 \end{gathered}$ | +0.0 | 42.6 | 54.0 | -11.4 | Horiz |
| $\begin{gathered} 14 \quad 13475.175 \\ \mathrm{M} \\ \text { Ave } \end{gathered}$ | 40.1 | $\begin{array}{r} +0.0 \\ +0.0 \\ +40.5 \\ +0.0 \\ +0.0 \\ +0.0 \end{array}$ | $\begin{aligned} & +1.3 \\ & +0.0 \\ & +7.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +1.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -33.7 \\ -14.5 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 42.2 | 54.0 | -11.8 | Vert |
| $15 \quad 120.200 \mathrm{M}$ | 43.7 | $\begin{aligned} & \hline+0.0 \\ & +0.6 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +5.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.5 \\ & +8.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{gathered} -27.6 \\ +0.0 \\ +0.0 \\ +0.0 \\ +0.0 \end{gathered}$ | +0.0 | 31.1 | 43.5 | -12.4 | Vert |
| $\begin{gathered} 16{ }_{\mathrm{QP}}{ }^{62.000 \mathrm{M}} \\ \hline \end{gathered}$ | 39.5 | $\begin{aligned} & +0.0 \\ & +0.5 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline+0.1 \\ & +5.8 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.4 \\ & +7.6 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{gathered} \hline-27.8 \\ +0.0 \\ +0.0 \\ +0.0 \\ +0.0 \end{gathered}$ | +0.0 | 26.1 | 40.0 | -13.9 | Vert |
| $\begin{array}{cc} \hline 17 & 15541.110 \\ \mathrm{M} \end{array}$ | 36.7 | $\begin{array}{r} +0.0 \\ +0.0 \\ +39.0 \\ +0.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.8 \\ & +0.0 \\ & +8.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.7 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{gathered} \hline+0.0 \\ -34.2 \\ -12.8 \\ +0.0 \\ +0.0 \end{gathered}$ | +0.0 | 39.4 | 54.0 | -14.6 | Horiz |
| $\begin{array}{cc} \hline 18 & 10360.560 \\ M \end{array}$ | 40.4 | $\begin{array}{r} +0.0 \\ +0.0 \\ +36.3 \\ +0.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.3 \\ & +0.0 \\ & +6.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.8 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} \hline+0.0 \\ -34.1 \\ -12.1 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 38.8 | 54.0 | -15.2 | Vert |


|  | $\begin{aligned} & \hline 28310.000 \\ & \text { M } \\ & \text { Ave } \end{aligned}$ | 19.3 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +1.1 \\ & +3.9 \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ +10.8 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +1.3 \\ & +2.2 \end{aligned}$ | +0.0 | 38.6 | 54.0 | -15.4 | Vert |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 20 | 27.518M | 46.8 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.1 \\ & +0.0 \\ & +0.3 \\ & +0.0 \\ & +5.3 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | 12.5 | 29.5 | -17.0 | Groun |
| 21 | 2.014 M | 39.5 | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.1 \\ & +0.0 \\ & +9.5 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | -40.0 | 9.1 | 29.5 | -20.4 | Groun |
|  | $\begin{aligned} & 15539.885 \\ & \text { M } \\ & \text { Ave } \end{aligned}$ | 25.4 | $\begin{array}{r} +0.0 \\ +0.0 \\ +39.0 \\ +0.0 \\ +0.0 \\ +0.0 \\ \hline \end{array}$ | $\begin{aligned} & \hline+1.8 \\ & +0.0 \\ & +8.2 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.7 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ -34.2 \\ -12.8 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 28.1 | 54.0 | -25.9 | Horiz |
|  | $\begin{aligned} & 20720.000 \\ & \text { M } \\ & \text { Ave } \end{aligned}$ | 25.9 | $\begin{array}{r} +0.0 \\ +0.0 \\ +0.0 \\ -13.9 \\ +0.9 \\ +0.0 \end{array}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +9.2 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +2.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +1.2 \\ & +0.0 \end{aligned}$ |  | 25.3 | 54.0 | -28.7 | Vert |
|  | $\begin{aligned} & \hline 11398.750 \\ & \text { M } \\ & \text { Ave } \end{aligned}$ | 28.9 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & \hline+1.4 \\ & +0.0 \\ & +6.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ -13.3 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 23.5 | 54.0 | -30.5 | Vert |
| $\wedge$ | $\begin{gathered} 11398.750 \\ \mathrm{M} \end{gathered}$ | 42.2 | $\begin{aligned} & \hline+0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +1.4 \\ & +0.0 \\ & +6.5 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{aligned} & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \\ & +0.0 \end{aligned}$ | $\begin{array}{r} +0.0 \\ +0.0 \\ -13.3 \\ +0.0 \\ +0.0 \end{array}$ | +0.0 | 36.8 | 54.0 | -17.2 | Vert |

## SUPPLEMENTAL INFORMATION

## Measurement Uncertainty

| Uncertainty Value | Parameter |
| :---: | :---: |
| 4.73 dB | Radiated Emissions |
| 3.34 dB | Mains Conducted Emissions |
| 3.30 dB | Disturbance Power |

Uncertainties reported are worst case for all CKC Laboratories' sites and represent expanded uncertainties expressed at approximately the $95 \%$ confidence level using a coverage factor of $\mathrm{k}=2$. Compliance is deemed to occur provided measurements are below the specified limits.

## Emissions Test Details

## TESTING PARAMETERS

Unless otherwise indicated, the following configuration parameters are used for equipment setup: The cables were routed consistent with the typical application by varying the configuration of the test sample. Interface cables were connected to the available ports of the test unit. The effect of varying the position of the cables was investigated to find the configuration that produced maximum emissions. Cables were of the type and length specified in the individual requirements. The length of cable that produced maximum emissions was selected.

The equipment under test (EUT) was set up in a manner that represented its normal use, as shown in the setup photographs. Any special conditions required for the EUT to operate normally are identified in the comments that accompany the emissions tables.

The emissions data was taken with a spectrum analyzer or receiver. Incorporating the applicable correction factors for distance, antenna, cable loss and amplifier gain, the data was reduced as shown in the table below. The corrected data was then compared to the applicable emission limits. Preliminary and final measurements were taken in order to ensure that all emissions from the EUT were found and maximized.

## CORRECTION FACTORS

The basic spectrum analyzer reading was converted using correction factors as shown in the highest emissions readings in the tables. For radiated emissions in $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$, the spectrum analyzer reading in $\mathrm{dB} \mu \mathrm{V}$ was corrected by using the following formula. This reading was then compared to the applicable specification limit. Individual measurements were compared with the displayed limit value in the margin column. The margin was calculated based on subtracting the limit value from the corrected measurement value; a positive margin represents a measurement exceeding the limit, while a negative margin represents a measurement less than the limit.

| SAMPLE CALCULATIONS |  |  |  |
| :--- | :--- | :--- | :---: |
|  | Meter reading | $(\mathrm{dB} \mu \mathrm{V})$ |  |
| + | Antenna Factor | $(\mathrm{dB} / \mathrm{m})$ |  |
| + | Cable Loss | $(\mathrm{dB})$ |  |
| - | Distance Correction | $(\mathrm{dB})$ |  |
| - | Preamplifier Gain | $(\mathrm{dB})$ |  |
| $=$ | Corrected Reading | $(\mathrm{dB} \mu \mathrm{V} / \mathrm{m})$ |  |

## TEST INSTRUMENTATION AND ANALYZER SETTINGS

The test instrumentation and equipment listed were used to collect the emissions data. A spectrum analyzer or receiver was used for all measurements. Unless otherwise specified, the following table shows the measuring equipment bandwidth settings that were used in designated frequency bands. For testing emissions, an appropriate reference level and a vertical scale size of 10 dB per division were used.

| MEASURING EQUIPMENT BANDWIDTH SETTINGS PER FREQUENCY RANGE |  |  |  |
| :---: | :---: | :---: | :---: |
| TEST | BEGINNING FREQUENCY | ENDING FREQUENCY | BANDWIDTH SETTING |
| CONDUCTED EMISSIONS | 150 kHz | 30 MHz | 9 kHz |
| RADIATED EMISSIONS | 9 kHz | 150 kHz | 200 Hz |
| RADIATED EMISSIONS | 150 kHz | 30 MHz | 9 kHz |
| RADIATED EMISSIONS | 30 MHz | 1000 MHz | 120 kHz |
| RADIATED EMISSIONS | 1000 MHz | $>1 \mathrm{GHz}$ | 1 MHz |

## SPECTRUM ANALYZER/RECEIVER DETECTOR FUNCTIONS

The notes that accompany the measurements contained in the emissions tables indicate the type of detector function used to obtain the given readings. Unless otherwise noted, all readings were made in the "positive peak" detector mode. Whenever a "quasi-peak" or "average" reading was recorded, the measurement was annotated with a "QP" or an "Ave" on the appropriate rows of the data sheets. In cases where quasi-peak or average limits were employed and data exists for multiple measurement types for the same frequency then the peak measurement was retained in the report for reference, however the numbering for the affected row was removed and an arrow or caret ("^") was placed in the far left-hand column indicating that the row above takes precedence for comparison to the limit. The following paragraphs describe in more detail the detector functions and when they were used to obtain the emissions data.

## Peak

In this mode, the spectrum analyzer or receiver recorded all emissions at their peak value as the frequency band selected was scanned. By combining this function with another feature called "peak hold," the measurement device had the ability to measure intermittent or low duty cycle transient emission peak levels. In this mode the measuring device made a slow scan across the frequency band selected and measured the peak emission value found at each frequency across the band.

## Quasi-Peak

Quasi-peak measurements were taken using the quasi-peak detector when the true peak values exceeded or were within 2 dB of a quasi-peak specification limit. Additional QP measurements may have been taken at the discretion of the operator.

## Average

Average measurements were taken using the average detector when the true peak values exceeded or were within 2 dB of an average specification limit. Additional average measurements may have been taken at the discretion of the operator. If the specification or test procedure requires trace averaging, then the averaging was performed using 100 samples or as required by the specification. All other average measurements are performed using video bandwidth averaging. To make these measurements, the test engineer reduces the video bandwidth on the measuring device until the modulation of the signal is filtered out. At this point, the measuring device is set into the linear mode and the scan time is reduced.


[^0]:    - Readings
    $\times$ QP Readings
    - Ambient

    1-15.247(d) / 15.209 Radiated Spurious Emissions

[^1]:    - Readings
    $\times$ QP Readings
    - Ambient

    1-15.247(d) / 15.209 Radiated Spurious Emissions

