## Ossia, Inc.

## REVISED EMC TEST REPORT TO 102580-4B

Cota WPT Source*<br>Model: Venus V2*<br>(*See Appendix A for Manufacturer Declaration)

## Tested to The Following Standards:

FCC Part 18 Subpart C Section 18.305 \& 18.307

Report No.: 102580-4C

Date of issue: June 12, 2019


This test report bears the accreditation symbol indicating that the testing performed herein meets the test and reporting requirements of ISO/IEC 17025 under the applicable scope of testing for CKC Laboratories, Inc.

We strive to create long-term, trust based relationships by providing sound, adaptive, customer first testing services. We embrace each of our customers' unique EMC challenges, not as an interruption to set processes, but rather as the reason we are in business.

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## ADMINISTRATIVE INFORMATION

## Test Report Information

## REPORT PREPARED FOR:

Usia, Inc.
1100 112 $^{\text {th }}$ Ave NE Suite 301
Bellevue WA 98004

Representative: Robert McDonald
Customer Reference Number: 13042

DATE OF EQUIPMENT RECEIPT:
REPORT PREPARED BY:

Terri Rayle
CKC Laboratories, Inc.
5046 Sierra Pines Drive
Mariposa, CA 95338

Project Number: 102580

DATES) OF TESTING:
December 20, 2017
December 20, 2017 and April 29-30, 2019

## Revision History

Original: Testing of the Cola WPT Source, Model: Venus V2 to FCC Part 18 Subpart C Section 18.305 \& 18.307. Revision A: To update the customer address.
Revision B: To replace radiated emissions datasheets, $9 \mathrm{kHz}-30 \mathrm{MHz}$ and $1-3 \mathrm{GHz}$.
Revision C: To add a statement in the Conditions During Test for Test Configuration notes.

## Report Authorization

The test data contained in this report documents the observed testing parameters pertaining to and are relevant for only the equipment provided by the client, tested in the agreed upon operational modes) and configurations) as identified herein. Compliance assessment remains the client's responsibility. This report may not be used to claim product endorsement by A2LA or any government agencies. This test report has been authorized for release under quality control from CKC Laboratories, Inc.


Steve Behm
Director of Quality Assurance \& Engineering Services
CKC Laboratories, Inc.

## Test Facility Information



Our laboratories are configured to effectively test a wide variety of product types. CKC utilizes first class test equipment, anechoic chambers, data acquisition and information services to create accurate, repeatable and affordable test results.

TEST LOCATION(S):
CKC Laboratories, Inc.
22116 23rd Drive S.E., Suite A
Canyon Park, Bothell, WA 98021

## Software Versions

| CKC Laboratories Proprietary Software | Version |
| :--- | :---: |
| EMITest Emissions | 5.03 .12 |
| EMITest Immunity | 5.03 .10 |

## Site Registration \& Accreditation Information

| Location | *NIST CB \# | FCC | JAPAN |
| :---: | :---: | :---: | :---: |
| Canyon Park, Bothell, WA | USO081 | US1022 | A-0148 |

*CKC's list of NIST designated countries can be found at: https://standards.gov/cabs/designations.html

LABORATORIES, INC.

## SUMMARY OF RESULTS

## Standard / Specification: FCC Part 18 Subpart C

| Test Procedure | Description | Modifications | Results |
| :--- | :--- | :---: | :---: |
| FCC Part 18.305 (b) | Radiated Emissions | NA | Pass |
|  |  |  |  |
| FCC Part 18.307 (b) | Conducted Emissions | NA | Pass |
|  |  |  |  |

NA = Not Applicable

## ISO/IEC 17025 Decision Rule

The declaration of pass or fail herein is based upon assessment to the specification(s) listed above, including where applicable, assessment of measurement uncertainties. For performance related tests, equipment was monitored for specified criteria identified in that section of testing.

## Modifications During Testing

This list is a summary of the modifications made to the equipment during testing.

## Summary of Conditions

The manufacturer declares the EUT has not been modified since the original collection of the data.

Modifications listed above must be incorporated into all production units.
L.ABORATORIES, INE.

## Conditions During Testing

This list is a summary of the conditions noted to the equipment during testing.

## Summary of Conditions

## Investigation of worst-case Radiated Emissions

Based on historical test data, the $2^{\text {nd }}, 3^{\text {rd }}$, and $4^{\text {th }}$ Harmonics of the fundamental frequency were identified as the worst-case emissions. The worst-case frequencies were maximized with the following boundary conditions established by the manufacturer:
-The minimum separation distance between the tile and client is 0.3 m
-The maximum separation distance between the tile and client is 1.0 m
-The maximum angle between the tile and client is 60 degrees

The following measurements were collected to narrow down the worst-case conditions, where $\mathbf{r}$ is the separation distance between the tile and client, $\varphi$ is the azimuth angle, and $\theta$ is the altitude angle.
$r=1.0 \mathrm{~m}, \varphi=0$ degrees, $\theta=0$ degrees
$r=1.0 \mathrm{~m}, \varphi=30$ degrees, $\theta=0$ degrees
$r=1.0 \mathrm{~m}, \varphi=60$ degrees, $\theta=0$ degrees
$r=1.0 \mathrm{~m}, \varphi=0$ degrees, $\theta=30$ degrees
$r=1.0 \mathrm{~m}, \varphi=0$ degrees, $\theta=60$ degrees
Note: $r$ is measured from the center of the front face on each device. The angles are measured from the tile's boresight line to a line connecting the center front face of each device. For the angle variation, the client was rotated to always be pointed at the center of the front face of the tile.

After these initial measurements at 1 m were collected, the worst-case margin was found to be the boresight condition ( $\varphi=0 \quad \theta=0$ ). Further investigation was performed by varying the separation in 10 cm increments from 0.3 to 1 m . After the new maximum was found, the worst-case was investigated in small increments of roughly 1 cm , but the overall worst-case separation distance was identified at 40 cm . Once the 40 cm worst case separation distance was established, the azimuth and altitude angles were varied in 10 degree increments. The boresight condition was still found to be worst-case.

All Radiated Emissions measurements included in the report were taken in the following configuration as worstcase:
$r=0.4 \mathrm{~m}, \varphi=0$ degrees, $\varphi=0$ degrees

EUT settings from manufacturer: 13 dBm , dynamic tuning
The fundamental operating frequency is 2.45 GHz .
Test configuration notes: The original testing was performed using power setting of +16 dBm , however the equipment was later reduced to power setting of +13 dBm . All radiated emissions testing was performed at power setting of +13 dBm . The AC conducted emissions testing was performed only at the original power setting of +16 dBm since emissions with the higher power setting represents worst case emissions. The manufacturer declares that the maximum power setting is fixed at +13 dBm and cannot be altered by the end user.

## EQUIPMENT UNDER TEST (EUT)

During testing, numerous configurations may have been utilized. The configurations listed below support compliance to the standard(s) listed in the Summary of Results section.

## Configuration 1: Radiated Emissions tested on 4/29/2019 (see Appendix A)

Equipment Tested:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Cota WPT Source | Ossia, Inc. | Venus v1 | 14 |

Support Equipment:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Cota WPT Client | Ossia, Inc. | VenusRx | 126 |
| Laptop | Apple | MacBook Pro A1398 | NA |
| Ethernet Switch | D-Link | DGS-1100-08 | NA |
| USB 2.0 Extension Cable | Blue Rigger | $32 \mathrm{ft}(10 \mathrm{~m})$ | NA |

## Configuration 2: Conducted Emissions tested on 12/20/2017 (see Appendix A)

Equipment Tested:

| Device | Manufacturer | Model \# | S/N |
| :--- | :--- | :--- | :--- |
| Venus Tile 14 | Ossia, Inc. | OL-10212 | NA |


| Support Equipment: |  |  | S/N |
| :--- | :--- | :--- | :--- |
| Device | Manufacturer | Model \# | NA |
| USB Active Extension Cable | Trip Litte | U026-20M | NA |
| Laptop | Apple | A1398 | 39 |
| Venus B4 Client | Ossia, Inc. | OL-10210 |  |

## FCC PART 18

### 18.305 Radiated Emissions

Test Notes: Radiated disturbances emanating from enclosure.

## Test Setup / Conditions / Data

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Ossia, Inc.
18.305(b) ISM Frequencies <500W

100740
Maximized Emissions
Michael Atkinson
EMITest 5.03.12

Date: 4/29/2019
Time: 18:01:16
Sequence\#: 19

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Test Conditions / Notes.

Temperature: $18-22^{\circ} \mathrm{C}$
Humidity: 25-45\%
Pressure: $102-103.5 \mathrm{kPa}$
Frequency: $9 \mathrm{kHz}-30 \mathrm{MHz}$

Method: FCC/OET MP-5 (February 1986)
Client is charging, client is 0.4 m away from tile, boresight configuration. 13 dBm setting. The 0.4 m separation distance was determined to be worst case configuration for Radiated Emissions (see report summary of conditions for justification of worst case).

Ferrite (Fair-Rite Brand) PN 0475164181 installed on power cord.
The Ethernet cable was terminated into an Ethernet switch at time of testing. The EUT was connected to a laptop remotely via a USB extension cable.

3 orthogonal polarities investigated, worst case reported.
Manufacturer declares the lowest frequency used within the ISM device is 1 MHz . All frequencies reported below
1 MHz are related to other portions of the equipment governed under separate requirements.

Ossia, Inc. WO\#\#: 100740 Sequence\#: 19 Date: 4/29/2019 18.305(b) ISM Frequencies <500W Test Distance: 3 Meters Para+Perp+GrPara


- Readings
$\times \quad$ QP Readings
$\times$ Ambient
$\times 1-18.305(\mathrm{~b})$ ISM Frequencies $<500 \mathrm{~W}$

O Peak Readings

* Average Readings

Software Version: 5.03.12

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02872 | Spectrum Analyzer | E4440A | $11 / 3 / 2017$ | $11 / 3 / 2019$ |
| T2 | ANP06540 | Cable | Heliax | $10 / 30 / 2017$ | $10 / 30 / 2019$ |
| T3 | ANP06515 | Cable | Heliax | $6 / 29 / 2018$ | $6 / 29 / 2020$ |
| T4 | AN00052 | Loop Antenna | 6502 | $5 / 7 / 2018$ | $5 / 7 / 2020$ |

Measurement Data: $\quad$ Reading listed by margin. Test Distance: 3 Meters

| \# | Freq <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \mathrm{T} 1 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 3 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{aligned} & \mathrm{T} 4 \\ & \mathrm{~dB} \\ & \hline \end{aligned}$ | Dist <br> Table | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \end{gathered}$ | Margin dB | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $59.161 \mathrm{k}$ <br> Ambient | 75.3 | +0.0 | +0.0 | +0.0 | +9.7 | Not Related to EUT ISM Device |  |  |  |  |
|  | $118.260 \mathrm{k}$ Ambient | 59.1 | +0.0 | +0.0 | +0.0 | +9.5 | Not Related to EUT ISM Device |  |  |  |  |
| 3 | 177.179k | 52.0 | +0.0 | +0.0 | +0.0 | +9.7 | -40.0 | 21.7 | 28.0 | -6.3 | Perp |
| 4 | 292.167 k | 49.1 | +0.0 | +0.0 | +0.0 | +9.6 | -40.0 | 18.7 | 28.0 | -9.3 | Perp |
| 5 | 356.979k | 46.1 | +0.0 | +0.0 | +0.0 | +9.7 | -40.0 | 15.8 | 28.0 | -12.2 | Perp |
| 6 | 336.072k | 43.0 | +0.0 | +0.0 | +0.0 | +9.6 | -40.0 | 12.6 | 28.0 | -15.4 | Perp |
| 7 | 402.974k | 42.8 | +0.0 | +0.0 | +0.0 | +9.7 | -40.0 | 12.5 | 28.0 | -15.5 | Perp |
| 8 | 17.385M | 33.1 | +0.0 | +0.0 | +0.2 | +8.5 | -40.0 | 1.8 | 28.0 | -26.2 | Groun |
| 9 | 19.705M | 33.0 | +0.0 | +0.0 | +0.2 | +8.1 | -40.0 | 1.3 | 28.0 | -26.7 | Perp |
| 10 | 7.699 M | 20.2 | +0.0 | +0.0 | +0.1 | +9.4 | -40.0 | -10.3 | 28.0 | -38.3 | Groun |

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)
Customer: Ossia, Inc.
Specification: 18.305(b) ISM Frequencies <500W
Work Order \#: 102580
Test Type:
Tested By:
Maximized Emissions
Date: 4/30/2019
Time: 09:45:53

Software:
EMITest 5.03.12
Sequence\#: 21

## Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Temperature: $18-22^{\circ} \mathrm{C}$
Humidity: 25-45\%
Pressure: $102-103.5 \mathrm{kPa}$

Frequency: $30-1000 \mathrm{MHz}$
Method: FCC/OET MP-5 (February 1986)
Client is charging, client is 0.4 m away from tile, boresight configuration. 13 dBm setting. The 0.4 m separation distance was determined to be worst case configuration for Radiated Emissions (see report summary of conditions for justification of worst case).

Ferrite (Fair-Rite Brand) PN 0475164181 installed on power cord by the manufacturer prior to testing.
The manufacturer declares the power cord is permanently installed and that the ferrite bead will be installed at the time of manufacturing.

The Ethernet cable was terminated into an Ethernet switch at time of testing. The EUT was connected to a laptop remotely via a USB extension cable.

Horizontal and Vertical antenna polarities investigated, worst case reported.

Ossia, Inc. WO\#: 100740 Sequence\#: 21 Date: 4/30/2019 18.305(b) ISM Frequencies $\mathbf{5 0 0 W}$ Test Distance: 3 Meters H+V


[^0]O Peak Readings

* Average Readings

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | AN02872 | Spectrum Analyzer | E4440A | $11 / 3 / 2017$ | $11 / 3 / 2019$ |
| T1 | ANP06540 | Cable | Heliax | $10 / 30 / 2017$ | $10 / 30 / 2019$ |
| T2 | ANP05305 | Cable | ETSI-50T | $10 / 24 / 2017$ | $10 / 24 / 2019$ |
| T3 | ANP05360 | Cable | RG214 | $1 / 31 / 2018$ | $1 / 31 / 2020$ |
| T4 | ANP06123 | Attenuator | 18N-6 | $4 / 5 / 2019$ | $4 / 5 / 2021$ |
| T5 | AN03628 | Biconilog Antenna | 3142E | $6 / 7 / 2017$ | $6 / 7 / 2019$ |

Measurement Data: Reading listed by margin. Test Distance: 3 Meters

| \# | Freq <br> MHz | Rdng $\mathrm{dB} \mu \mathrm{V}$ | $\begin{aligned} & \text { T1 } \\ & \text { T5 } \\ & \text { dB } \end{aligned}$ | $\begin{aligned} & \mathrm{T} 2 \\ & \mathrm{~dB} \end{aligned}$ | $\begin{array}{r} \mathrm{T} 3 \\ \mathrm{~dB} \end{array}$ | T4 <br> dB | Dist <br> Table | $\begin{gathered} \text { Corr } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \end{gathered}$ | $\begin{gathered} \text { Spec } \\ \mathrm{dB} \mu \mathrm{~V} / \mathrm{m} \end{gathered}$ | Margin dB | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 748.957 M | 24.0 | $\begin{array}{r} +0.3 \\ +22.5 \end{array}$ | +1.4 | +1.7 | +5.8 | -40.0 | 15.7 | 28.0 | -12.3 | Vert |
| 2 | 762.385M | 22.9 | $\begin{array}{r} +0.3 \\ +22.6 \\ \hline \end{array}$ | +1.4 | +1.7 | +5.8 | -40.0 | 14.7 | 28.0 | -13.3 | Vert |
| 3 | 759.466M | 22.6 | $\begin{array}{r} +0.3 \\ +22.6 \end{array}$ | +1.4 | +1.7 | +5.8 | -40.0 | 14.4 | 28.0 | -13.6 | Vert |
| 4 | 590.158M | 24.5 | $\begin{array}{r} +0.3 \\ +20.4 \\ \hline \end{array}$ | +1.3 | +1.5 | +5.8 | -40.0 | 13.8 | 28.0 | -14.2 | Vert |
| 5 | 546.955 M | 24.1 | $\begin{array}{r} +0.3 \\ +20.9 \\ \hline \end{array}$ | +1.2 | +1.4 | +5.8 | -40.0 | 13.7 | 28.0 | -14.3 | Vert |
| 6 | 614.094M | 22.9 | $\begin{array}{r} +0.3 \\ +21.2 \end{array}$ | +1.3 | +1.5 | +5.8 | -40.0 | 13.0 | 28.0 | -15.0 | Vert |
| 7 | 84.522M | 39.5 | $\begin{aligned} & +0.1 \\ & +6.6 \end{aligned}$ | $+0.5$ | +0.5 | +5.8 | -40.0 | 13.0 | 28.0 | -15.0 | Vert |
| 8 | 528.273M | 23.7 | $\begin{array}{r} +0.3 \\ +20.3 \end{array}$ | +1.2 | +1.4 | +5.8 | -40.0 | 12.7 | 28.0 | -15.3 | Vert |
| 9 | 84.300M | 38.3 | $\begin{aligned} & +0.1 \\ & +6.6 \end{aligned}$ | +0.5 | +0.5 | +5.8 | -40.0 | 11.8 | 28.0 | -16.2 | Horiz |
|  | $153.130 \mathrm{M}$ | 34.4 | $\begin{array}{r} +0.2 \\ +9.9 \\ \hline \end{array}$ | +0.6 | +0.7 | +5.8 | -40.0 | 11.6 | 28.0 | -16.4 | Vert |
| $\wedge$ | 153.082 M | 34.7 | $\begin{aligned} & \hline+0.2 \\ & +9.9 \end{aligned}$ | +0.6 | +0.7 | +5.8 | -40.0 | 11.9 | 28.0 | -16.1 | Vert |
|  | $153.127 \mathrm{M}$ | 34.2 | $\begin{array}{r} +0.2 \\ +9.9 \\ \hline \end{array}$ | +0.6 | +0.7 | +5.8 | -40.0 | 11.4 | 28.0 | -16.6 | Horiz |
| $\wedge$ | 153.200 M | 35.0 | $\begin{aligned} & +0.2 \\ & +9.9 \end{aligned}$ | +0.6 | +0.7 | +5.8 | -40.0 | 12.2 | 28.0 | -15.8 | Horiz |
| 14 | 505.504 M | 23.1 | $\begin{array}{r} +0.3 \\ +19.0 \\ \hline \end{array}$ | +1.2 | +1.3 | +5.8 | -40.0 | 10.7 | 28.0 | -17.3 | Vert |
| 15 | 460.550M | 24.2 | $\begin{array}{r} +0.2 \\ +17.8 \\ \hline \end{array}$ | +1.1 | +1.3 | +5.8 | -40.0 | 10.4 | 28.0 | -17.6 | Vert |
| 16 | 66.900 M | 35.9 | $\begin{aligned} & +0.1 \\ & +7.0 \end{aligned}$ | +0.4 | +0.4 | +5.8 | -40.0 | 9.6 | 28.0 | -18.4 | Horiz |
| $17$ | $85.151 \mathrm{M}$ | 35.1 | $\begin{aligned} & +0.1 \\ & +6.6 \end{aligned}$ | +0.5 | +0.5 | +5.8 | -40.0 | 8.6 | 28.0 | -19.4 | Vert |
|  | $\begin{aligned} & 202.700 \mathrm{M} \\ & \mathrm{QP} \\ & \hline \end{aligned}$ | $27.1$ | $\begin{array}{r} +0.2 \\ +10.2 \end{array}$ | +0.7 | +0.8 | +5.8 | -40.0 | 4.8 | 28.0 | -23.2 | Horiz |
| $\wedge$ | 202.700 M | 31.2 | $\begin{array}{r} +0.2 \\ +10.2 \\ \hline \end{array}$ | +0.7 | +0.8 | +5.8 | -40.0 | 8.9 | 28.0 | -19.1 | Horiz |

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Ossia, Inc.
18.305(b) ISM Frequencies <500W

100740
Maximized Emissions
Michael Atkinson
EMITest 5.03.12

Date: 4/30/2019
Time: 09:09:00
Sequence\#: 20

## Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Temperature: $18-22^{\circ} \mathrm{C}$
Humidity: 25-45\%
Pressure: $102-103.5 \mathrm{kPa}$

Frequency: $1-3 \mathrm{GHz}$
Method: FCC/OET MP-5 (February 1986)
Client is charging, client is 0.4 m away from tile, boresight configuration. 13 dBm setting. The 0.4 m separation distance was determined to be worst case configuration for Radiated Emissions (see report summary of conditions for justification of worst case).

Ferrite (Fair-Rite Brand) PN 0475164181 installed on power cord.
The Ethernet cable was terminated into an Ethernet switch at time of testing. The EUT was connected to a laptop remotely via a USB extension cable.

Horizontal and Vertical antenna polarities investigated, worst case reported.

Ossia, Inc. WO\#: 100740 Sequence\#f: 20 Date: 4/30/2019 18.305(b) ISM Frequencies 500 W Test Distance: 3 Meters Vert


[^1]- Peak Readings
* Average Readings

Software Version: 5.03.12

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02872 | Spectrum Analyzer | E4440A | $11 / 3 / 2017$ | $11 / 3 / 2019$ |
| T2 | ANP06540 | Cable | Heliax | $10 / 30 / 2017$ | $10 / 30 / 2019$ |
| T3 | ANP06515 | Cable | Heliax | $6 / 29 / 2018$ | $6 / 29 / 2020$ |
| T4 | AN01467 | Horn Antenna-ANSI <br> C63.5 Calibration | 3115 | $7 / 21 / 2017$ | $7 / 21 / 2019$ |
| T5 | AN03417 | Band Reject Filter | 3TNF- <br> $1500 / 3000-N / N$ | $11 / 15 / 2017$ | $11 / 15 / 2019$ |

Measurement Data: $\quad$ Reading listed by margin. Test Distance: 3 Meters


| $\begin{aligned} & 192552.900 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 20.9 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.7 | +28.3 | -40.0 | 12.4 | 28.0 | -15.6 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge 2552.900 \mathrm{M}$ | 42.5 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.7 | +28.3 | -40.0 | 34.0 | 28.0 | +6.0 | Horiz |
| $\begin{aligned} & 212331.200 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 21.2 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.5 | +28.1 | -40.0 | 12.3 | 28.0 | -15.7 | Horiz |
| $\begin{gathered} 222542.000 \mathrm{M} \\ \text { Ave } \\ \hline \end{gathered}$ | 20.9 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.7 | +28.2 | -40.0 | 12.3 | 28.0 | -15.7 | Vert |
| $\wedge 2542.000 \mathrm{M}$ | 43.6 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.7 | +28.2 | -40.0 | 35.0 | 28.0 | +7.0 | Vert |
| $\begin{aligned} & 242331.200 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 21.2 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.5 | +28.1 | -40.0 | 12.3 | 28.0 | -15.7 | Horiz |
| $\wedge 2331.200 \mathrm{M}$ | 40.4 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | $+0.4$ | +2.5 | +28.1 | -40.0 | 31.5 | 28.0 | +3.5 | Horiz |
| $\wedge 2331.200 \mathrm{M}$ | 40.4 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | $+0.4$ | +2.5 | +28.1 | -40.0 | 31.5 | 28.0 | +3.5 | Horiz |
| $\begin{aligned} & 27 \text { 2501.405M } \\ & \text { Ave } \end{aligned}$ | 20.9 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.4 | +2.7 | +28.1 | -40.0 | 12.2 | 28.0 | -15.8 | Horiz |
| $\wedge 2501.405 \mathrm{M}$ | 50.4 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.7 | +28.1 | -40.0 | 41.7 | 28.0 | +13.7 | Horiz |
| $\begin{gathered} 292517.044 \mathrm{M} \\ \text { Ave } \\ \hline \end{gathered}$ | 20.8 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.7 | +28.2 | -40.0 | 12.2 | 28.0 | -15.8 | Horiz |
| ^ 2517.044M | 50.3 | $\begin{aligned} & +0.0 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.4 | +2.7 | +28.2 | -40.0 | 41.7 | 28.0 | +13.7 | Horiz |
| $\begin{aligned} & 312512.000 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 20.9 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.7 | +28.1 | -40.0 | 12.2 | 28.0 | -15.8 | Vert |
| ^ 2512.000M | 53.0 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.7 | +28.1 | -40.0 | 44.3 | 28.0 | +16.3 | Vert |
| $\begin{aligned} & 332529.003 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 20.8 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | $+0.4$ | +2.7 | +28.2 | -40.0 | 12.2 | 28.0 | -15.8 | Horiz |
| $\wedge 2529.003 \mathrm{M}$ | 52.0 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | $+0.4$ | +2.7 | +28.2 | -40.0 | 43.4 | 28.0 | +15.4 | Horiz |
| $\begin{aligned} & 352522.564 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 20.8 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | $+0.4$ | +2.7 | +28.2 | -40.0 | 12.2 | 28.0 | -15.8 | Horiz |
| $\wedge 2522.564 \mathrm{M}$ | 52.2 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | $+0.4$ | +2.7 | +28.2 | -40.0 | 43.6 | 28.0 | +15.6 | Horiz |
| $\begin{aligned} & 37 \text { 2518.884M } \\ & \text { Ave } \end{aligned}$ | 20.8 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.7 | +28.2 | -40.0 | 12.2 | 28.0 | -15.8 | Horiz |
| $\wedge 2518.884 \mathrm{M}$ | 50.6 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.7 | +28.2 | -40.0 | 42.0 | 28.0 | +14.0 | Horiz |
| $\begin{aligned} & 392537.300 \mathrm{M} \\ & \text { Ave } \\ & \hline \end{aligned}$ | 20.8 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | $+0.4$ | +2.7 | +28.2 | -40.0 | 12.2 | 28.0 | -15.8 | Horiz |
| $\wedge 2537.300 \mathrm{M}$ | 46.8 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.7 | +28.2 | -40.0 | 38.2 | 28.0 | +10.2 | Horiz |
| $\begin{aligned} & 412366.000 \mathrm{M} \\ & \text { Ave } \\ & \hline \end{aligned}$ | 20.8 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.4 | +2.5 | +28.1 | -40.0 | 11.9 | 28.0 | -16.1 | Vert |
| $\wedge 2366.000 \mathrm{M}$ | 46.9 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.5 | +28.1 | -40.0 | 38.0 | 28.0 | +10.0 | Vert |
| $\begin{aligned} & 43 \text { 2377.200M } \\ & \text { Ave } \end{aligned}$ | 20.7 | $\begin{aligned} & \hline+0.0 \\ & +0.1 \end{aligned}$ | $+0.4$ | +2.6 | +28.1 | -40.0 | 11.9 | 28.0 | -16.1 | Horiz |
| $\wedge 2377.200 \mathrm{M}$ | 46.1 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | $+0.4$ | +2.6 | +28.1 | -40.0 | 37.3 | 28.0 | +9.3 | Horiz |

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| $\begin{gathered} 452398.375 \mathrm{M} \\ \text { Ave } \end{gathered}$ | 20.7 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.6 | +28.1 | -40.0 | 11.9 | 28.0 | -16.1 | Horiz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ^ 2398.375M | 51.1 | $\begin{aligned} & +0.0 \\ & +0.1 \\ & \hline \end{aligned}$ | +0.4 | +2.6 | +28.1 | -40.0 | 42.3 | 28.0 | +14.3 | Horiz |
| $\begin{aligned} & \hline 47 \text { 2239.200M } \\ & \text { Ave } \end{aligned}$ | 20.8 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.4 | +28.1 | -40.0 | 11.8 | 28.0 | -16.2 | Horiz |
| 2239.200M | 35.7 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.4 | +28.1 | -40.0 | 26.7 | 28.0 | -1.3 | Horiz |
| $\begin{aligned} & \hline 49 \text { 2154.600M } \\ & \text { Ave } \\ & \hline \end{aligned}$ | 20.5 | $\begin{aligned} & +0.0 \\ & +0.1 \\ & +0.1 \end{aligned}$ | +0.4 | +2.4 | +28.2 | -40.0 | 11.6 | 28.0 | -16.4 | Horiz |
| 2154.600 M | 32.3 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.4 | +28.2 | -40.0 | 23.4 | 28.0 | -4.6 | Horiz |
| $\begin{aligned} & \hline 512227.500 \mathrm{M} \\ & \text { Ave } \\ & \hline \end{aligned}$ | 20.5 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.4 | +28.2 | -40.0 | 11.6 | 28.0 | -16.4 | Horiz |
| ^ 2227.500 M | 38.2 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.4 | +28.2 | -40.0 | 29.3 | 28.0 | +1.3 | Horiz |
| $\begin{aligned} & 53 \text { 2256.000M } \\ & \text { Ave } \\ & \hline \end{aligned}$ | 20.6 | $\begin{aligned} & +0.0 \\ & +0.1 \end{aligned}$ | +0.4 | +2.4 | +28.1 | -40.0 | 11.6 | 28.0 | -16.4 | Vert |
| 2256.000 M | 38.0 | $\begin{aligned} & +0.0 \\ & +0.1 \\ & +0.1 \end{aligned}$ | +0.4 | +2.4 | +28.1 | -40.0 | 29.0 | 28.0 | +1.0 | Vert |

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)
Customer: Ossia, Inc.
Specification: 18.305(b) ISM Frequencies <500W
Work Order \#: 102580
Test Type:
Tested By:
Maximized Emissions
Date: 4/29/2019
Michael Atkinson
Time: 17:34:53

EMITest 5.03.12
Sequence\#: 18
Software:

## Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Temperature: $18-22^{\circ} \mathrm{C}$
Humidity: 25-45\%
Pressure: $102-103.5 \mathrm{kPa}$

Frequency: $3-10 \mathrm{GHz}$
Method: FCC/OET MP-5 (February 1986)
Client is charging, client is 0.4 m away from tile, boresight configuration. 13 dBm setting. The 0.4 m separation distance was determined to be worst case configuration for Radiated Emissions (see report summary of conditions for justification of worst case).

Ferrite (Fair-Rite Brand) PN 0475164181 installed on power cord by the manufacturer prior to testing.
The manufacturer declares the power cord is permanently installed and that the ferrite bead will be installed at the time of manufacturing.

The Ethernet cable was terminated into an Ethernet switch at time of testing. The EUT was connected to a laptop remotely via a USB extension cable.

Horizontal and Vertical antenna polarities investigated, worst case reported.

Ossia, Inc. WO\#: 100740 Sequence\#f: 18 Date: 4/29/2019
18.305(b) ISM Frequencies $<500 \mathrm{~W}$ Test Distance: 3 Meters $\mathrm{H}+\mathrm{V}$


## - Readings

$\times$ QP Readings

- Ambient
- 1-18.305(b) ISM Frequencies <500W

O Peak Readings<br>* Average Readings<br>Software Version: 5.03.12

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02872 | Spectrum Analyzer | E4440A | $11 / 3 / 2017$ | $11 / 3 / 2019$ |
| T2 | ANP06540 | Cable | Heliax | $10 / 30 / 2017$ | $10 / 30 / 2019$ |
| T3 | ANP06515 | Cable | Heliax | $6 / 29 / 2018$ | $6 / 29 / 2020$ |
| T4 | AN03116 | High Pass Filter | 11SH10-00313 | $1 / 22 / 2019$ | $1 / 22 / 2021$ |
| T5 | AN01467 | Horn Antenna-ANSI | 3115 | $7 / 21 / 2017$ | $7 / 21 / 2019$ |


| Measurement Data: | Reading listed by margin. |  |  |  | Test Distance: 3 Meters |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# Freq | Rdng | T1 | T2 | T3 | T4 | Dist | Corr | Spec | Margin | Polar |
| MHz | $\mathrm{dB} \mu \mathrm{V}$ | dB | dB | dB | dB | Table | $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$ | $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$ | dB | Ant |
| 1 9799.990M | 22.1 | +0.0 | +0.5 | +6.3 | +0.7 | -40.0 | 27.2 | 28.0 | -0.8 | Horiz |
| Ave |  | +37.6 |  |  |  |  |  |  |  |  |
| 27350.000 M | 18.1 | +0.0 | +1.0 | +5.4 | +0.6 | -40.0 | 21.7 | 28.0 | -6.3 | Vert |
| Ave |  | +36.6 |  |  |  |  |  |  |  |  |
| 3 3674.968M | 25.0 | +0.0 | +0.4 | +3.8 | +0.8 | -40.0 | 20.8 | 28.0 | -7.2 | Horiz |
|  |  | +30.8 |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 44900.000 \mathrm{M} \\ & \text { Ave } \\ & \hline \end{aligned}$ | 21.2 | +0.0 | +0.5 | +4.2 | +0.5 | -40.0 | 18.9 | 28.0 | -9.1 | Vert |
|  |  | +32.5 |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 5 \text { 3675.099M } \\ & \text { Ave } \\ & \hline \end{aligned}$ | 14.1 | +0.0 | +0.4 | +3.8 | +0.8 | -40.0 | 9.9 | 28.0 | -18.1 | Horiz |
|  |  | +30.8 |  |  |  |  |  |  |  |  |

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)
Customer: Ossia, Inc.
Specification: 18.305(b) ISM Frequencies <500W
Work Order \#: $\mathbf{1 0 2 5 8 0}$
Test Type:
Tested By:
Maximized Emissions
Date: 4/29/2019
Michael Atkinson
Time: 18:37:06

EMITest 5.03.12
Sequence\#: 19
Software:

## Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Temperature: $18-22^{\circ} \mathrm{C}$
Humidity: 25-45\%
Pressure: $102-103.5 \mathrm{kPa}$

Frequency: $10-18 \mathrm{GHz}$
Method: FCC/OET MP-5 (February 1986)
Client is charging, client is 0.4 m away from tile, boresight configuration. 13 dBm setting. The 0.4 m separation distance was determined to be worst case configuration for Radiated Emissions (see report summary of conditions for justification of worst case).

Ferrite (Fair-Rite Brand) PN 0475164181 installed on power cord by the manufacturer prior to testing.
The manufacturer declares the power cord is permanently installed and that the ferrite bead will be installed at the time of manufacturing.

The Ethernet cable was terminated into an Ethernet switch at time of testing. The EUT was connected to a laptop remotely via a USB extension cable.

Horizontal and Vertical antenna polarities investigated, worst case reported.

Ossia, Inc. WO\#: 100740 Sequence\#f: 19 Date: 4/29/2019
18.305(b) ISM Frequencies $<500 \mathrm{~W}$ Test Distance: 3 Meters $\mathrm{H}+\mathrm{V}$


## - Readings

$\times$ QP Readings

- Ambient
- 1-18.305(b) ISM Frequencies <500W

O Peak Readings<br>* Average Readings<br>Software Version: 5.03.12

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :--- | :--- | :--- | :--- | :--- | :--- |
|  | AN02872 | Spectrum Analyzer | E4440A | $11 / 3 / 2017$ | $11 / 3 / 2019$ |
| T1 | ANP06540 | Cable | Heliax | $10 / 30 / 2017$ | $10 / 30 / 2019$ |
| T2 | ANP06515 | Cable | Heliax | $6 / 29 / 2018$ | $6 / 29 / 2020$ |
| T3 | AN03116 | High Pass Filter | 11 SH10-00313 | $1 / 22 / 2019$ | $1 / 22 / 2021$ |
| T4 | AN01467 | Horn Antenna-ANSI <br>  | 3115 | $7 / 21 / 2017$ | $7 / 21 / 2019$ |
| C63.5 Calibration |  |  |  |  |  |
| T6 | AN03540 | Preamp | $83017 A$ | $3 / 25 / 2019$ | $3 / 25 / 2021$ |
| T7 | ANP06123 | Attenuator | $18 N-6$ | $4 / 5 / 2019$ | $4 / 5 / 2021$ |



Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Ossia, Inc.
18.305(b) ISM Frequencies <500W

102580
Maximized Emissions
Michael Atkinson
EMITest 5.03.12

Date: 4/30/2019
Time: 10:16:58
Sequence\#: 23

## Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

## Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 1 |  | S/N |

Test Conditions / Notes:
Temperature: $18-22^{\circ} \mathrm{C}$
Humidity: 25-45\%
Pressure: $102-103.5 \mathrm{kPa}$

Frequency: $18-25 \mathrm{GHz}$
Method: FCC/OET MP-5 (February 1986)
Client is charging, client is 0.4 m away from tile, boresight configuration. 13 dBm setting. The 0.4 m separation distance was determined to be worst case configuration for Radiated Emissions (see report summary of conditions for justification of worst case).

Ferrite (Fair-Rite Brand) PN 0475164181 installed on power cord by the manufacturer prior to testing.
The manufacturer declares the power cord is permanently installed and that the ferrite bead will be installed at the time of manufacturing.

The Ethernet cable was terminated into an Ethernet switch at time of testing. The EUT was connected to a laptop remotely via a USB extension cable.

Horizontal and Vertical antenna polarities investigated, worst case reported.

Ossia, Inc. WO\#: 100740 Sequence\#f: 23 Date: 4/30/2019
18.305(b) ISM Frequencies $<500 \mathrm{~W}$ Test Distance: 3 Meters $\mathrm{H}+\mathrm{V}$


## - Readings

$\times$ QP Readings

- Ambient
-1-18.305(b) ISM Frequencies <500W

O Peak Readings<br>* Average Readings<br>Software Version: 5.03.12

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :---: | :--- | :--- | :--- | :--- | :--- |
|  | AN02872 | Spectrum Analyzer | E4440A | $11 / 3 / 2017$ | $11 / 3 / 2019$ |
| T1 | AN02742 | Active Horn Antenna | AMFW-5F- | $10 / 16 / 2018$ | $10 / 16 / 2020$ |
|  |  |  | $18002650-20-10 P$ |  | $4 / 23 / 2020$ |
| T2 | AN02763-69 | Waveguide | Multiple | $4 / 23 / 2018$ | $3 / 13 / 2020$ |
| T3 | AN03122 | Cable | $32026-2-29801-$ | $3 / 13 / 2018$ |  |
|  |  |  | 36 |  | $3 / 13 / 2020$ |
| T4 | ANP06678 | Cable | $32026-29801-$ | $3 / 13 / 2018$ |  |
|  |  |  | $29801-144$ |  |  |

Measurement Data: $\quad$ Reading listed by margin. Test Distance: 3 Meters

| Freq <br> MHz | Rdng <br> $\mathrm{dB} \mu \mathrm{V}$ | T 1 <br> dB | T 2 <br> dB | T 3 <br> dB | T 4 <br> dB | Dist <br> Table | Corr <br> $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$ | Spec <br> $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$ | Margin <br> dB | Polar <br> Ant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 19599.935 <br> M | 49.3 | -13.0 | +1.9 | +2.3 | +8.5 | -40.0 | 9.0 | 28.0 | -19.0 | Vert |
| Ave |  |  |  |  |  |  |  |  |  |  |

## Test Setup Photo(s)



### 18.307 AC Conducted Emissions

Test Notes: Conducted Disturbances at Mains Terminals, LISN method.

## Test Setup / Conditions / Data

Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)

Customer:
Specification: Work Order \#: Test Type: Tested By:
Software:

Ossia, Inc.
18.307(b) AC Mains - Average

102580
Conducted Emissions
Michael Atkinson
EMITest 5.03.12

Date: 12/20/2017
Time: 18:37:32
Sequence\#: 28
115 VAC 60 Hz

Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

## Test Conditions / Notes:

Temperature: $23^{\circ} \mathrm{C}$
Humidity: 30\%
Pressure: 102.5 kPa

Frequency: $0.15-30 \mathrm{MHz}$
Method: FCC/OET MP-5 (February 1986)
Client 1 m away on table. 16 dBm , no RSSI.
Ferrite (Fair-Rite Brand) PN 0475164181 installed on power cord by the manufacturer prior to testing.
The manufacturer declares the power cord is permanently installed and that the ferrite bead will be installed at the time of manufacturing.

The manufacturer declares the setup used for this test is representative of worst case conducted emissions.

Ossia, Inc. WO\#: 102580 Sequence\#: 28 Date: 12/20/2017 18.307 (b) AC Mains - Average Test Lead: 115 VAC 60 Hz Line


|  | Sweep Data |
| :--- | :--- |
|  | Peak Readings |
| * | Readings |
|  | $\times$ QP Readings |
|  | Software Readings Version: 5.03 .12 |
|  | $2-18.307$ (b) AC Mains - Quasi-peak |

Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :---: | :--- | :--- | :--- | :--- | :--- |
| T1 | AN02871 | Spectrum Analyzer | E4440A | $2 / 24 / 2017$ | $2 / 24 / 2019$ |
| T2 | AN02611 | High Pass Filter | HE9615-150K- | $2 / 18 / 2016$ | $2 / 18 / 2018$ |
|  |  |  | Cable | Heliax | $10 / 30 / 2017$ |
| T3 | ANP06540 | Cable | Heliax | $1 / 21 / 2016$ | $1 / 21 / 2018$ |
| T4 | ANP06515 | Attenuator | $768-10$ | $4 / 12 / 2016$ | $4 / 12 / 2018$ |
| T5 | ANP06219 | 50uH LISN-Line1 | $3816 / 2$ | $3 / 7 / 2016$ | $3 / 7 / 2018$ |
|  | AN01311 | (N) |  |  |  |
| T6 | AN01311 | 50uH LISN-Line2 (L) | $3816 / 2$ | $3 / 7 / 2016$ | $3 / 7 / 2018$ |

Measurement Data: $\quad$ Reading listed by margin. $\quad$ Test Lead: Line


| 15 | $1.091 \mathrm{M}$ | 25.3 | $\begin{aligned} & +0.0 \\ & +9.1 \end{aligned}$ | $\begin{aligned} & \hline+0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.0 | +0.0 | 34.6 | 46.0 | -11.4 | Line |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 1.091 M | 41.9 | +0.0 | +0.2 | +0.0 | +0.0 | +0.0 | 51.2 | 46.0 | +5.2 | Line |
|  |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| 17 | 1.737 M | 24.8 | +0.0 | +0.2 | +0.0 | +0.1 | +0.0 | 34.3 | 46.0 | -11.7 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 1.737 M | 41.9 | +0.0 | +0.2 | +0.0 | +0.1 | +0.0 | 51.4 | 46.0 | +5.4 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 19 | 3.349 M | 24.1 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 33.5 | 46.0 | -12.5 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 3.349M | 36.2 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 45.6 | 46.0 | -0.4 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 21 | 766.523 k | 24.1 | +0.0 | +0.2 | +0.0 | +0.1 | +0.0 | 33.5 | 46.0 | -12.5 | Line |
| Ave |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| $\wedge$ | 766.523 k | 42.4 | +0.0 | +0.2 | +0.0 | +0.1 | +0.0 | 51.8 | 46.0 | +5.8 | Line |
|  |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| 23 | 2.340M | 23.4 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 32.8 | 46.0 | -13.2 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 2.340 M | 38.4 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 47.8 | 46.0 | +1.8 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 25 | 2.431 M | 23.0 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 32.4 | 46.0 | -13.6 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 2.431 M | 39.0 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 48.4 | 46.0 | +2.4 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 27 | 2.724 M | 22.4 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 31.8 | 46.0 | -14.2 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 2.724 M | 37.7 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 47.1 | 46.0 | +1.1 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 29 | 2.203 M | 21.5 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 30.9 | 46.0 | -15.1 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 2.203 M | 41.5 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 50.9 | 46.0 | +4.9 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 31 | 1.681 M | 20.5 | +0.0 | +0.2 | +0.0 | +0.1 | +0.0 | 30.0 | 46.0 | -16.0 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 1.681 M | 42.9 | +0.0 | +0.2 | +0.0 | +0.1 | +0.0 | 52.4 | 46.0 | +6.4 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 33 | 1.447 M | 20.6 | +0.0 | +0.2 | +0.0 | +0.0 | +0.0 | 29.9 | 46.0 | -16.1 | Line |
| Ave |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| $\wedge$ | 1.447 M | 41.6 | +0.0 | +0.2 | +0.0 | +0.0 | +0.0 | 50.9 | 46.0 | +4.9 | Line |
|  |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| 35 | 1.574 M | 18.9 | +0.0 | +0.2 | +0.0 | +0.0 | +0.0 | 28.2 | 46.0 | -17.8 | Line |
| Ave |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| $\wedge$ | 1.574 M | 40.8 | +0.0 | +0.2 | +0.0 | +0.0 | +0.0 | 50.1 | 46.0 | +4.1 | Line |
|  |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| 37 | 3.176M | 18.3 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 27.7 | 46.0 | -18.3 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |

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| 38 | $1.138 \mathrm{M}$ | 18.4 | $\begin{aligned} & +0.0 \\ & +9.1 \end{aligned}$ | $\begin{aligned} & +0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.0 | +0.0 | 27.7 | 46.0 | -18.3 | Line |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 1.138 M | 41.4 | +0.0 | +0.2 | +0.0 | +0.0 | +0.0 | 50.7 | 46.0 | +4.7 | Line |
|  |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| 40 | 1.070 M | 18.3 | +0.0 | +0.2 | +0.0 | +0.0 | +0.0 | 27.6 | 46.0 | -18.4 | Line |
| Ave |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| $\wedge$ | 1.070 M | 40.7 | +0.0 | +0.2 | +0.0 | +0.0 | +0.0 | 50.0 | 46.0 | +4.0 | Line |
|  |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| 42 | 2.863 M | 17.8 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 27.2 | 46.0 | -18.8 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 2.863 M | 34.8 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 44.2 | 46.0 | -1.8 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 44 | 858.978 k | 17.5 | +0.0 | +0.2 | +0.0 | +0.1 | +0.0 | 26.9 | 46.0 | -19.1 | Line |
| Ave |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| $\wedge$ | 858.978 k | 40.3 | +0.0 | +0.2 | +0.0 | +0.1 | +0.0 | 49.7 | 46.0 | +3.7 | Line |
|  |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| 46 | 1.871 M | 16.7 | +0.0 | +0.2 | +0.0 | +0.1 | +0.0 | 26.2 | 46.0 | -19.8 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 1.871 M | 40.8 | +0.0 | +0.2 | +0.0 | +0.1 | +0.0 | 50.3 | 46.0 | +4.3 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 48 | 3.178 M | 16.4 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 25.8 | 46.0 | -20.2 | Line |
| Ave |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 3.176 M | 34.5 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 43.9 | 46.0 | -2.1 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| $\wedge$ | 3.178 M | 33.8 | +0.0 | +0.1 | +0.0 | +0.1 | +0.0 | 43.2 | 46.0 | -2.8 | Line |
|  |  |  | +9.1 | +0.1 |  |  |  |  |  |  |  |
| 51 | 958.111 k | 15.0 | +0.0 | +0.2 | +0.0 | +0.1 | +0.0 | 24.4 | 46.0 | -21.6 | Line |
| Ave |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| $\wedge$ | 958.110 k | 40.4 | +0.0 | +0.2 | +0.0 | +0.1 | +0.0 | 49.8 | 46.0 | +3.8 | Line |
|  |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| 53 | 734.285k | 14.9 | +0.0 | +0.2 | +0.0 | +0.1 | +0.0 | 24.3 | 46.0 | -21.7 | Line |
| Ave |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| $\wedge$ | 734.284k | 40.5 | +0.0 | +0.2 | +0.0 | +0.1 | +0.0 | 49.9 | 46.0 | +3.9 | Line |
|  |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| 55 | 806.073 k | 14.3 | +0.0 | +0.2 | +0.0 | +0.1 | +0.0 | 23.7 | 46.0 | -22.3 | Line |
| Ave |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| $\wedge$ | 806.073 k | 41.7 | +0.0 | +0.2 | +0.0 | +0.1 | +0.0 | 51.1 | 46.0 | +5.1 | Line |
|  |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| 57 | 1.226 M | 14.3 | +0.0 | +0.2 | +0.0 | +0.0 | +0.0 | 23.6 | 46.0 | -22.4 | Line |
| Ave |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| $\wedge$ | 1.226 M | 41.0 | +0.0 | +0.2 | +0.0 | +0.0 | +0.0 | 50.3 | 46.0 | +4.3 | Line |
|  |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| 59 | 631.000k | 12.4 | +0.0 | +0.2 | +0.0 | +0.0 | +0.0 | 21.7 | 46.0 | -24.3 | Line |
| Ave |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| 60 | 504.800 k | 11.3 | +0.0 | +0.2 | +0.0 | +0.0 | +0.0 | 20.6 | 46.0 | -25.4 | Line |
| Ave |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| $\wedge$ | 504.800 k | 36.6 | +0.0 | +0.2 | +0.0 | +0.0 | +0.0 | 45.9 | 46.0 | -0.1 | Line |
|  |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| 62 | 414.800k | 10.6 | +0.0 | +0.2 | +0.0 | +0.0 | +0.0 | 19.9 | 47.6 | -27.7 | Line |
| Ave |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |
| 414.800k |  | 38.6 | +0.0 | +0.2 | +0.0 | +0.0 | +0.0 | 47.9 | 47.6 | +0.3 | Line |
|  |  |  | +9.1 | +0.0 |  |  |  |  |  |  |  |

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Test Location: CKC Laboratories • 22116 23rd Drive SE, Suite A • Bothell, WA 98021 • 1-800-500-4EMC (4362)

Customer:
Specification:
Work Order \#:
Test Type:
Tested By:
Software:

Ossia, Inc.
18.307(b) AC Mains - Average

102580
Conducted Emissions
Michael Atkinson
EMITest 5.03.12

Date: 12/20/2017
Time: 18:20:28
Sequence\#: 27
115 VAC 60 Hz

## Equipment Tested:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

## Support Equipment:

| Device | Manufacturer | Model \# |
| :--- | :--- | :--- |
| Configuration 2 |  | S/N |

Test Conditions / Notes:
Temperature: $23^{\circ} \mathrm{C}$
Humidity: 30\%
Pressure: 102.5 kPa

Frequency: $0.15-30 \mathrm{MHz}$
Method: FCC/OET MP-5 (February 1986)
Client 1 m away on table. 16 dBm , no RSSI.

Ferrite (Fair-Rite Brand) PN 0475164181 installed on power cord by the manufacturer prior to testing.
The manufacturer declares the power cord is permanently installed and that the ferrite bead will be installed at the time of manufacturing.

The manufacturer declares the setup used for this test is representative of worst case conducted emissions.

Ossia, Inc. WO\#: 102580 Sequence\#: 27 Date: $12 / 20 / 2017$ 18.307 (b) AC Mains - Average Test Lead: 115 VAC 60 Hz Return


Test Equipment:

| ID | Asset \# | Description | Model | Calibration Date | Cal Due Date |
| :---: | :--- | :--- | :--- | :--- | :--- |
|  | AN02871 | Spectrum Analyzer | E4440A | $2 / 24 / 2017$ | $2 / 24 / 2019$ |
| T1 | AN02611 | High Pass Filter | HE9615-150K- <br> $50-720 B$ | $2 / 18 / 2016$ | $2 / 18 / 2018$ |
| T2 | ANP06540 | Cable | Heliax | $10 / 30 / 2017$ | $10 / 30 / 2019$ |
| T3 | ANP06515 | Cable | Heliax | $1 / 21 / 2016$ | $1 / 21 / 2018$ |
| T4 | ANP06219 | Attenuator | $768-10$ | $4 / 12 / 2016$ | $4 / 12 / 2018$ |
| T5 | AN01311 | 50uH LISN-Line1 (N) | $3816 / 2$ | $3 / 7 / 2016$ | $3 / 7 / 2018$ |
|  | AN01311 | 50uH LISN-Line2 (L) | $3816 / 2$ | $3 / 7 / 2016$ | $3 / 7 / 2018$ |


| Measurement Data | Reading listed by margin. |  |  |  | Test Lead: Return |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \# Freq | Rdng | $\begin{aligned} & \text { T1 } \\ & \text { T5 } \end{aligned}$ | T2 | T3 | T4 | Dist | Corr | Spec | Margin | Polar |
| MHz | $\mathrm{dB} \mu \mathrm{V}$ | dB | dB | dB | dB | Table | $\mathrm{dB} \mu \mathrm{V}$ | $\mathrm{dB} \mu \mathrm{V}$ | dB | Ant |
| $\begin{aligned} & 1.996 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 30.6 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 39.9 | 46.0 | -6.1 | Retur |
| $\wedge 1.996 \mathrm{M}$ | 40.7 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 50.0 | 46.0 | +4.0 | Retur |
| $\begin{aligned} & 3 \quad 1.938 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 28.6 | $\begin{aligned} & +0.2 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 38.0 | 46.0 | -8.0 | Retur |
| $\wedge 1.938 \mathrm{M}$ | 40.5 | $\begin{aligned} & \hline+0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 49.9 | 46.0 | +3.9 | Retur |
| $\begin{aligned} & 5 \quad 1.469 \mathrm{M} \\ & \text { Ave } \\ & \hline \end{aligned}$ | 28.5 | $\begin{aligned} & +0.2 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +9.1 | +0.0 | 37.8 | 46.0 | -8.2 | Retur |
| $\wedge 1.469 \mathrm{M}$ | 41.9 | $\begin{aligned} & +0.2 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +9.1 | +0.0 | 51.2 | 46.0 | +5.2 | Retur |
| $\begin{aligned} & 7 \quad 1.117 \mathrm{M} \\ & \text { Ave } \end{aligned}$ | 26.5 | $\begin{aligned} & +0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.0 | +9.1 | +0.0 | 35.8 | 46.0 | -10.2 | Retur |
| $\wedge 1.117 \mathrm{M}$ | 42.4 | $\begin{aligned} & +0.2 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +9.1 | +0.0 | 51.7 | 46.0 | +5.7 | Retur |
| $\begin{aligned} & 9 \quad 1.646 \mathrm{M} \\ & \text { Ave } \\ & \hline \end{aligned}$ | 25.8 | $\begin{aligned} & +0.2 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 35.2 | 46.0 | -10.8 | Retur |
| $\begin{gathered} 10 \quad 1.765 \mathrm{M} \\ \text { Ave } \\ \hline \end{gathered}$ | 25.8 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 35.1 | 46.0 | -10.9 | Retur |
| $\wedge 1.765 \mathrm{M}$ | 40.5 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 49.8 | 46.0 | +3.8 | Retur |
| $\begin{gathered} 12586.760 \mathrm{k} \\ \text { Ave } \\ \hline \end{gathered}$ | 25.6 | $\begin{aligned} & \hline+0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.0 | +9.1 | +0.0 | 34.9 | 46.0 | -11.1 | Retur |
| $\begin{aligned} & 13 \begin{array}{l} 585.960 \mathrm{k} \\ \text { Ave } \end{array} \end{aligned}$ | 25.6 | $\begin{aligned} & +0.2 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +9.1 | +0.0 | 34.9 | 46.0 | -11.1 | Retur |
| $\wedge \quad 585.960 \mathrm{k}$ | 39.8 | $\begin{aligned} & \hline+0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.0 | +9.1 | +0.0 | 49.1 | 46.0 | +3.1 | Retur |
| $\wedge \quad 586.760 \mathrm{k}$ | 39.7 | $\begin{aligned} & +0.2 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +9.1 | +0.0 | 49.0 | 46.0 | +3.0 | Retur |
| $\begin{gathered} 16{ }^{2.014 \mathrm{M}} \\ \text { Ave } \end{gathered}$ | 24.2 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 33.5 | 46.0 | -12.5 | Retur |
| $\wedge \quad 2.014 \mathrm{M}$ | 41.9 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 51.2 | 46.0 | +5.2 | Retur |


|  | $e^{1.744 \mathrm{M}}$ | 23.7 | $\begin{aligned} & +0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 33.1 | 46.0 | -12.9 | Retur |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 1.744M | 41.4 | $\begin{aligned} & +0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 50.8 | 46.0 | +4.8 | Retur |
| 20 | $1.638 \mathrm{M}$ | 23.3 | $\begin{aligned} & \hline+0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 32.7 | 46.0 | -13.3 | Retur |
| $\wedge$ | 1.646M | 40.3 | $\begin{aligned} & +0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 49.7 | 46.0 | +3.7 | Retur |
| $\wedge$ | 1.638 M | 40.3 | $\begin{aligned} & \hline+0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 49.7 | 46.0 | +3.7 | Retur |
|  | $2.455 \mathrm{M}$ | 22.8 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 32.1 | 46.0 | -13.9 | Retur |
| $\wedge$ | 2.455 M | 37.7 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 47.0 | 46.0 | +1.0 | Retur |
|  | $1.912 \mathrm{M}$ | 22.3 | $\begin{aligned} & +0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 31.7 | 46.0 | -14.3 | Retur |
| $\wedge$ | 1.912 M | 41.5 | $\begin{aligned} & +0.2 \\ & +0.0 \end{aligned}$ | $+0.0$ | +0.1 | +9.1 | +0.0 | 50.9 | 46.0 | +4.9 | Retur |
|  | $1.828 \mathrm{M}$ | 22.2 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 31.5 | 46.0 | -14.5 | Retur |
| $\wedge$ | 1.828 M | 40.4 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 49.7 | 46.0 | +3.7 | Retur |
|  | $1.355 \mathrm{M}$ | 22.2 | $\begin{aligned} & +0.2 \\ & +0.0 \end{aligned}$ | $+0.0$ | +0.0 | +9.1 | +0.0 | 31.5 | 46.0 | -14.5 | Retur |
| $\wedge$ | 1.355 M | 40.6 | $\begin{aligned} & +0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.0 | +9.1 | +0.0 | 49.9 | 46.0 | +3.9 | Retur |
|  | $1.434 \mathrm{M}$ | 22.0 | $\begin{aligned} & +0.2 \\ & +0.0 \end{aligned}$ | $+0.0$ | +0.0 | +9.1 | $+0.0$ | 31.3 | 46.0 | -14.7 | Retur |
| $\wedge$ | 1.434 M | 40.7 | $\begin{aligned} & +0.2 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +9.1 | +0.0 | 50.0 | 46.0 | +4.0 | Retur |
|  | $\begin{aligned} & 2.201 \mathrm{M} \\ & \hline \end{aligned}$ | 21.9 | $\begin{aligned} & +0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | +0.1 | +9.1 | +0.0 | 31.2 | 46.0 | -14.8 | Retur |
| $\wedge$ | 2.201 M | 40.8 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 50.1 | 46.0 | +4.1 | Retur |
|  | $1.158 \mathrm{M}$ | 21.3 | $\begin{array}{r} +0.2 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 30.6 | 46.0 | -15.4 | Retur |
| $\wedge$ | 1.158 M | 40.8 | $\begin{array}{r} +0.2 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 50.1 | 46.0 | +4.1 | Retur |
|  | $\mathrm{e}^{2.322 \mathrm{M}}$ | 20.9 | $\begin{aligned} & +0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 30.2 | 46.0 | -15.8 | Retur |
| $\wedge$ | 2.322 M | 40.2 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 49.5 | 46.0 | +3.5 | Retur |
|  | $1.960 \mathrm{M}$ | 20.7 | $\begin{aligned} & +0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | +0.1 | +9.1 | +0.0 | 30.0 | 46.0 | -16.0 | Retur |
| $\wedge$ | 1.960 M | 39.7 | $\begin{array}{r} +0.1 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.1 | +9.1 | +0.0 | 49.0 | 46.0 | +3.0 | Retur |


|  | $3.226 \mathrm{M}$ <br> ve | 20.7 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 30.0 | 46.0 | -16.0 | Retur |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\wedge$ | 3.226 M | 36.2 | $\begin{aligned} & +0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 45.5 | 46.0 | -0.5 | Retur |
|  | $1.662 \mathrm{M}$ | 20.5 | $\begin{aligned} & +0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 29.9 | 46.0 | -16.1 | Retur |
| $\wedge$ | 1.662 M | 40.3 | $\begin{aligned} & \hline+0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 49.7 | 46.0 | +3.7 | Retur |
|  | 2.643M | 20.2 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 29.5 | 46.0 | -16.5 | Retur |
| $\wedge$ | 2.643 M | 36.1 | $\begin{aligned} & \hline+0.1 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 45.4 | 46.0 | -0.6 | Retur |
|  | $1.041 \mathrm{M}$ | 19.2 | $\begin{aligned} & +0.2 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +9.1 | +0.0 | 28.5 | 46.0 | -17.5 | Retur |
| $\wedge$ | 1.041 M | 40.2 | $\begin{aligned} & +0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.0 | +9.1 | +0.0 | 49.5 | 46.0 | +3.5 | Retur |
|  | $548.400 \mathrm{k}$ <br> ve | 19.1 | $\begin{aligned} & +0.2 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +9.1 | +0.0 | 28.4 | 46.0 | -17.6 | Retur |
| $\wedge$ | 548.400 k | 37.4 | $\begin{aligned} & +0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 46.7 | 46.0 | +0.7 | Retur |
|  | $1.204 \mathrm{M}$ | 18.6 | $\begin{array}{r} +0.2 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 27.9 | 46.0 | -18.1 | Retur |
| $\wedge$ | 1.204 M | 40.5 | $\begin{aligned} & +0.2 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.0 | +9.1 | $+0.0$ | 49.8 | 46.0 | +3.8 | Retur |
|  | $855.896 \mathrm{k}$ | 17.6 | $\begin{aligned} & +0.2 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 27.0 | 46.0 | -19.0 | Retur |
| $\wedge$ | 855.896k | 39.9 | $\begin{aligned} & +0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 49.3 | 46.0 | +3.3 | Retur |
|  | $1.005 \mathrm{M}$ <br> ve | 16.1 | $\begin{aligned} & \hline+0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | +0.0 | 25.5 | 46.0 | -20.5 | Retur |
| $\wedge$ | 1.005 M | 39.8 | $\begin{array}{r} +0.2 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.1 | +9.1 | +0.0 | 49.2 | 46.0 | +3.2 | Retur |
|  | $717.351 \mathrm{k}$ | 14.0 | $\begin{aligned} & +0.2 \\ & +0.0 \\ & \hline \end{aligned}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 23.4 | 46.0 | -22.6 | Retur |
| $\wedge$ | 717.351k | 40.4 | $\begin{aligned} & +0.2 \\ & +0.0 \end{aligned}$ | +0.0 | +0.1 | +9.1 | $+0.0$ | 49.8 | 46.0 | +3.8 | Retur |
|  | $751.627 \mathrm{k}$ | 12.4 | $\begin{aligned} & +0.2 \\ & +0.0 \\ & \hline \end{aligned}$ | $+0.0$ | +0.1 | +9.1 | $+0.0$ | 21.8 | 46.0 | -24.2 | Retur |
| $\wedge$ | 751.627k | 41.2 | $\begin{array}{r} +0.2 \\ +0.0 \\ \hline \end{array}$ | $+0.0$ | +0.1 | +9.1 | $+0.0$ | 50.6 | 46.0 | +4.6 | Retur |
|  | $636.060 \mathrm{k}$ | 10.0 | $\begin{aligned} & +0.2 \\ & +0.0 \end{aligned}$ | $+0.0$ | +0.0 | +9.1 | +0.0 | 19.3 | 46.0 | -26.7 | Retur |
| $\wedge$ | 636.060k | 39.3 | $\begin{array}{r} +0.2 \\ +0.0 \\ \hline \end{array}$ | +0.0 | +0.0 | +9.1 | +0.0 | 48.6 | 46.0 | +2.6 | Retur |

## Test Setup Photos)



## Appendix A: Manufacturer Declaration

At time of testing for the AC Conducted Emissions, the EUT was identified as:
Device: Venus Tile 14.
Model: OL-10212

At time of testing for the Radiated Emissions, the EUT was identified as:
Device: Cota WPT Source
Model: Venus v1

The manufacturer has chosen to use the following model name in its place.
The manufacturer declares that any differences between the names does not affect their EMC characteristics and therefore meets the level of testing equivalent to the tested model name:

## Device: Cota WPT Source

Model: Venus V2

## SUPPLEMENTAL INFORMATION

## Measurement Uncertainty

| Uncertainty Value | Parameter |
| :---: | :---: |
| 4.73 dB | Radiated Emissions |
| 3.34 dB | Mains Conducted Emissions |
| 3.30 dB | Disturbance Power |

Uncertainties reported are worst case for all CKC Laboratories' sites and represent expanded uncertainties expressed at approximately the $95 \%$ confidence level using a coverage factor of $\mathrm{k}=2$.

## Emissions Test Details

## TESTING PARAMETERS

Unless otherwise indicated, the following configuration parameters are used for equipment setup: The cables were routed consistent with the typical application by varying the configuration of the test sample. Interface cables were connected to the available ports of the test unit. The effect of varying the position of the cables was investigated to find the configuration that produced maximum emissions. Cables were of the type and length specified in the individual requirements. The length of cable that produced maximum emissions was selected.

The equipment under test (EUT) was set up in a manner that represented its normal use, as shown in the setup photographs. Any special conditions required for the EUT to operate normally are identified in the comments that accompany the emissions tables.

The emissions data was taken with a spectrum analyzer or receiver. Incorporating the applicable correction factors for distance, antenna, cable loss and amplifier gain, the data was reduced as shown in the table below. The corrected data was then compared to the applicable emission limits. Preliminary and final measurements were taken in order to ensure that all emissions from the EUT were found and maximized.

## CORRECTION FACTORS

The basic spectrum analyzer reading was converted using correction factors as shown in the highest emissions readings in the tables. For radiated emissions in $\mathrm{dB} \mu \mathrm{V} / \mathrm{m}$, the spectrum analyzer reading in $\mathrm{dB} \mu \mathrm{V}$ was corrected by using the following formula. This reading was then compared to the applicable specification limit. Individual measurements were compared with the displayed limit value in the margin column. The margin was calculated based on subtracting the limit value from the corrected measurement value; a positive margin represents a measurement exceeding the limit, while a negative margin represents a measurement less than the limit.

| SAMPLE CALCULATIONS |  |  |  |
| :--- | :--- | :--- | :---: |
|  | Meter reading | $(\mathrm{dB} \mu \mathrm{V})$ |  |
| + | Antenna Factor | $(\mathrm{dB} / \mathrm{m})$ |  |
| + | Cable Loss | $(\mathrm{dB})$ |  |
| - | Distance Correction | $(\mathrm{dB})$ |  |
| - | Preamplifier Gain | $(\mathrm{dB})$ |  |
| $=$ | Corrected Reading | $(\mathrm{dB} \mu \mathrm{V} / \mathrm{m})$ |  |

## TEST INSTRUMENTATION AND ANALYZER SETTINGS

The test instrumentation and equipment listed were used to collect the emissions data. A spectrum analyzer or receiver was used for all measurements. Unless otherwise specified, the following table shows the measuring equipment bandwidth settings that were used in designated frequency bands. For testing emissions, an appropriate reference level and a vertical scale size of 10 dB per division were used.

| MEASURING EQUIPMENT BANDWIDTH SETTINGS PER FREQUENCY RANGE |  |  |  |
| :---: | :---: | :---: | :---: |
| TEST | BEGINNING FREQUENCY | ENDING FREQUENCY | BANDWIDTH SETTING |
| CONDUCTED EMISSIONS | 150 kHz | 30 MHz | 9 kHz |
| RADIATED EMISSIONS | 9 kHz | 150 kHz | 200 Hz |
| RADIATED EMISSIONS | 150 kHz | 30 MHz | 9 kHz |
| RADIATED EMISSIONS | 30 MHz | 1000 MHz | 120 kHz |
| RADIATED EMISSIONS | 1000 MHz | $>1 \mathrm{GHz}$ | 1 MHz |

## SPECTRUM ANALYZER/RECEIVER DETECTOR FUNCTIONS

The notes that accompany the measurements contained in the emissions tables indicate the type of detector function used to obtain the given readings. Unless otherwise noted, all readings were made in the "positive peak" detector mode. Whenever a "quasi-peak" or "average" reading was recorded, the measurement was annotated with a "QP" or an "Ave" on the appropriate rows of the data sheets. In cases where quasi-peak or average limits were employed and data exists for multiple measurement types for the same frequency then the peak measurement was retained in the report for reference, however the numbering for the affected row was removed and an arrow or caret (" $\wedge$ ") was placed in the far left-hand column indicating that the row above takes precedence for comparison to the limit. The following paragraphs describe in more detail the detector functions and when they were used to obtain the emissions data.

## Peak

In this mode, the spectrum analyzer or receiver recorded all emissions at their peak value as the frequency band selected was scanned. By combining this function with another feature called "peak hold," the measurement device had the ability to measure intermittent or low duty cycle transient emission peak levels. In this mode the measuring device made a slow scan across the frequency band selected and measured the peak emission value found at each frequency across the band.

## Quasi-Peak

Quasi-peak measurements were taken using the quasi-peak detector when the true peak values exceeded or were within 2 dB of a quasi-peak specification limit. Additional QP measurements may have been taken at the discretion of the operator.

## Average

Average measurements were taken using the average detector when the true peak values exceeded or were within 2 dB of an average specification limit. Additional average measurements may have been taken at the discretion of the operator. If the specification or test procedure requires trace averaging, then the averaging was performed using 100 samples or as required by the specification. All other average measurements are performed using video bandwidth averaging. To make these measurements, the test engineer reduces the video bandwidth on the measuring device until the modulation of the signal is filtered out. At this point, the measuring device is set into the linear mode and the scan time is reduced.


[^0]:    - Readings
    $\times$ QP Readings
    - Ambient

    1-18.305(b) ISM Frequencies <500W

[^1]:    - Readings
    $\times$ QP Readings
    - Ambient

    1-18.305(b) ISM Frequencies <500W

