

RF EXPOSURE EVALUATION REPORT

APPLICANT: Reliance Communications LLC

PRODUCT NAME: Orbic Trophy 5G UW

MODEL NAME: R667L5U

BRAND NAME: Orbic

FCC ID : 2ABGH-R667L5U

STANDARD(S) : FCC 47 CFR Part 2(2.1093)

IEC TR 63170:2018

RECEIPT DATE : 2024-01-29

TEST DATE : 2024-02-18 to 2024-06-07

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Changed History			
Version Date Reason for Change			
1.0	2024-04-17	First edition	
2.0	2024-06-18	Added mmW MIMO test data and replaced V1.0	



1. Power Density Summary

The maximum results of power density found during test as bellows:

<Highest Total Power Density>

Fraguency		Standalone Transmission	
	equency	Total PD over 4cm²	Limit (FCC Part 1.310)
Band		(mW/cm²)	(mW/cm ²)
EC ND	n260	0.436	1.0
5G NR	n261	0.237	1.0

Highest Simultaneous Transmission with Multiple transmitters	Total Exposure Radio	Limit
SAR & Power Density	0.811	1.0

Note:

- This device is in compliance with power density for general population or uncontrolled exposure limits (1.0 Mw/cm² specified in FCC 47 CFR Part 1.310), and had been tested in accordance with the measurement methods and procedures specified in TCBC workshop notes and IEC TR 63170.
- 2. When the test result is a critical value, we will use the measurement uncertainty give the judgment re sult based on the 95% Confidence intervals.



2. Technical Information

Note: Provide by applicant.

2.1. Applicant and Manufacturer Information

Applicant:	Reliance Communications LLC	
Applicant Address:	555 Wireless Blvd. Hauppauge, NY 11788, USA	
Manufacturer:	Unimaxcomm	
Manufacturer Address:	35F,HBC HuiLong Center Building-II Minzhi Street,Longhua,	
	Shenzhen, P.R. China 518110	

2.2. Equipment under Test (EUT) Description

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FL1-3, Building A, FeiYang Science Park, No.8 LongChang Road, Block67, BaoAn District, ShenZhen , GuangDong Province, P. R. China

Product Name:	Orbic Trophy 5G UW
EUT IMEI:	351352440028926
Hardware Version:	V1.0
Software Version:	R667L5U_v1.1.2_BVZ
Frequency Bands:	5G NR n260(120kHz): 37 GHz ~ 40 GHz
	5G NR n261(120kHz): 27.5 GHz ~ 28.35 GHz
Modulation Mode:	5G NR:
	DFT-s-OFDM/CP-OFDM, PI/2 BPSK
	QPSK, 16QAM, 64QAM
Channel Bandwidth:	50MHz, 100MHz
Maximum Number of Contiguous	8CC
Component Carriers:	OCC .
scs	120kHz
5G NR Operation:	NSA
Antenna Information:	Patch Array Antenna

Note: For a more detailed description, please refer to specification or user manual supplied by the applicant and/or manufacturer.



2.3. Environment of Test Site/Conditions

Normal Temperature (NT):	20-25 °C
Relative Humidity:	30-75 %

Test Frequency:	5G NR n260/261
Operation Mode:	Call established
Power Level:	TDD 5G NR n260/261(Maximum output power)

During SAR test, EUT is in Traffic Mode (Channel Allocated) at Normal Voltage Condition. A communication link is set up with a System Simulator (SS) by air link, and a call is established.

The EUT shall use its internal transmitter. The antenna(s), battery and accessories shall be those specified by the Factory. The EUT battery must be fully charged and checked periodically during the test to ascertain uniform power output. If a wireless link is used, the antenna connected to the output of the base station simulator shall be placed at least 50 cm away from the handset.

The signal transmitted by the simulator to the antenna feeding point shall be lower than the output power level of the handset by at least 35 Db.





3. RF Exposure Limits

3.1. Uncontrolled Environment

Uncontrolled Environments are defined as locations where there is the exposure of individuals who have no knowledge or control of their exposure. The general population/uncontrolled exposure limits are applicable to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Members of the general public would come under this category when exposure is not employment-related; for example, in the case of a wireless transmitter that exposes persons in its vicinity.

Limits for Maximum Permissible Exposure (MPE)

Frequency range (MHz)	Electric field strength (V/m)	Magnetic field strength (A/m)	Power density (mW/cm ²)	Averaging time (minutes)
	(A) Limits for Oc	ccupational/Controlled Expos	sures	
0.3-3.0	614	1.63	*(100)	6
3.0-30	1842/	f 4.89/1	*(900/f2)	6
30-300	61.4	0.163	1.0	6
300-1500			f/300	6
1500-100,000			5	6
	(B) Limits for Gene	ral Population/Uncontrolled I	Exposure	
0.3-1.34	614	1.63	*(100)	30
1.34-30	824/	2.19/1	*(180/f2)	30
30-300	27.5	0.073	0.2	30
300-1500			f/1500	30
1500-100,000			1.0	30

3.2. Controlled Environment

Controlled Environments are defined as locations where there is exposure that may be incurred by persons who are aware of the potential for exposure, (i.e. as a result of employment or occupation). In general, occupational/controlled exposure limits are applicable to situations in which persons are exposed as a consequence of their employment, who have been made fully aware of the potential for exposure and can exercise control over their exposure. The exposure category is also applicable when the exposure is of a transient nature due to incidental passage through a location where the exposure levels may be higher than the general population/uncontrolled limits, but the exposed person is fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

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4. Applied Reference Documents

Leading reference documents for testing:

		Method
Identity	Document Title	Determination
		/Remark
FCC 47 CFD Dort 2/2 1002)	Radio Frequency Radiation Exposure	No deviation
FCC 47 CFR Part 2(2.1093)	Evaluation: Portable Devices	No deviation
KDB 447498 D01v06	General RF Exposure Guidance	No deviation
KDB 865664 D02v01r02	RF Exposure Reporting	No deviation
	Measurement procedure for the evaluation of	
	power density related to human	
IEC TR 63170:2018	exposure to radio frequency fields from	No deviation
	wireless communication devices	
	operating between 6 GHz and 100 GHz	
The November 2019, TCB	PE Evposure Precedures	No deviation
Workshop presentation	RF Exposure Procedures	No deviation

Note: Additions to, deviation, or exclusions from the method shall be judged in the "method determination" column of add, deviate or exclude from the specific method shall be explained in the "Remark" of the above table.





5. Power Density Measurement System

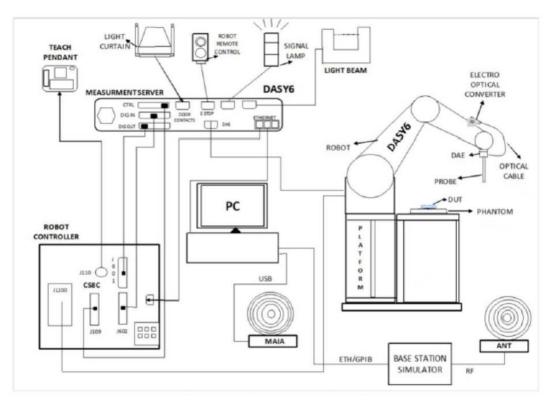


Fig 5.1 SPEAG DASY System Configurations

The DASY system for performance compliance tests is illustrated above graphically. This system consists of the following items:

- A standard high precision 6-axis robot with controller, a teach pendant and software.
- A data acquisition electronic (DAE) attached to the robot arm extension.
- A dosimetric probe equipped with an optical surface detector system.
- > The electro-optical converter (ECO) performs the conversion between optical and electrical signals
- A measurement server performs the time critical tasks such as signal filtering, control of the robot operation and fast movement interrupts.
- A probe alignment unit which improves the accuracy of the probe positioning.
- A computer operating Windows XP.
- > DASY software.
- Remove control with teach pendant and additional circuitry for robot safety such as warming lamps, etc.
- > The SAM twin phantom.
- A device holder.
- > Tissue simulating liquid.
- Dipole for evaluating the proper functioning of the system.
- Some of the components are described in details in the following sub-sections.





5.1. EUmmWave Probe

The probe designed allows measurement at distances as small as 2mm from the sensor to the surface of FUT. The typical senor to the tip of probe is 1.5mm.

EUT. The typical senor to the tip of probe is 1.5mm	
Frequency	750 MHz ~110 GHz
Probe Overall Length	320 mm
Probe Body Diameter	8.0 mm
Tip Length	23.0 mm
Tip Diameter	8.0 mm
Two dipoles Length of Probe	0.9 mm – Diode located
Dynamic Range	$<\!20$ V/m $-$ 10000 V/m with PRE-10 (min $<\!50$ V/m $-$ 3000 V/m)
Linearity	<0.2 dB
Position Precision	<0.2 mm
Distance between Diode Sensors and Probes tip	1.5 mm
Minimum Mechanical Separation between Probe Tip and a Surface	0.5 mm
Applications	E-field measurement of mm-Wave transmitters operating above 10 GHz in < 2mm distance from device (free-space) power density H-field and far-field analysis using total field reconstruction.
Compatibility	cDASY 6 + 5G Module SW1.0 and higher
	sensor 1,5mm calibrated
Fig 5.2 Photo of EUmmWave Probe	device



5.2. Data Acquisition Electronics (DAE)

The data acquisition electronics (DAE) consists of a highly sensitive electrometer-grade preamplifier with auto-zeroing, a channel and gain-switching multiplexer, a fast16 bit AD-converter and a command decoder and control logic unit. AD-converter and a command decoder and control logic unit. Transmission to the measurement server is accomplished through an optical downlink for data and status information as well as an optical uplink for commands and the clock. The input impedance of the DAE is 200MOhm; the inputs are symmetrical and floating. Common mode rejection is above 80 dB.



5.3. Robot

The SPEAG DASY system uses the high precision robots (DASY6: TX90XL) type from Stäubli SA (France). For the 6-axis controller system, the robot controller version (DASY6: CS8c) from Stäubli is used. The Stäubli robot series have many features that are important for our application:

High precision (repeatability ±0.035 mm)

High reliability (industrial design)

Jerk-free straight movements

Low ELF interference (the closed metallic construction shields against motor control fields)

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Fig 5.4 Photo of DASY6

5.4. Measurement Server

The measurement server is based on a PC/104 CPU board with CPU (DASY4: 166 MHz, Intel Pentium; DASY5: 400 MHz, Intel Celeron), chip disk (DASY4: 32 MB; DASY5: 128 MB), RAM (DASY4: 64 MB, DASY5: 128 MB). The necessary circuits for communication with the DAE electronic box, as well as the 16 bit AD converter system for optical detection and digital I/O interface are contained on the DASY I/O board, which is directly connected to the PC/104 bus of the CPU board.

The measurement server performs all the real-time data evaluation for field measurements and surface detection, controls robot movements and handles safety operations.





5.5. Data Storage and Evaluation

Data Storage

The DASY software stores the assessed data from the data acquisition electronics as raw data (in microvolt readings from the probe sensors), together with all the necessary software parameters for the data evaluation (probe calibration data, liquid parameters and device frequency and modulation data) in measurement files. The post-processing software evaluates the desired unit and format for output each time the data is visualized or exported. This allows verification of the complete software setup even after the measurement and allows correction of erroneous parameter settings. For example, if a measurement has been performed with an incorrect crest factor parameter in the device setup, the parameter can be corrected afterwards and the data can be reevaluated.

The measured data can be visualized or exported in different units or formats, depending on the selected probe type (e.g., [V/m], [A/m], [mW/g]). Some of these units are not available in certain situations or give meaningless results, e.g., a SAR-output in a non-lose media, will always be zero. Raw data can also be exported to perform the evaluation with other software packages.

Data Evaluation

The DASY post-processing software (SEMCAD) automatically executes the following procedures to calculate the field units from the microvolt readings at the probe connector. The parameters used in the evaluation are stored in the configuration modules of the software.

Probe parameters:	- Sensitivity	$Norm_i,a_{i0},a_{i1},a_{i2}$
	- Conversion factor	$ConvF_{i}$
	- Diode compression point	dcpi
Device parameters:	- Frequency	f
	- Crest factor	cf
Media parameters:	- Conductivity	σ
	- Density	ρ

These parameters must be set correctly in the software. They can be found in the component documents or they can be imported into the software from the configuration files issued for the DASY components. In the direct measuring mode of the multi-meter option, the parameters of the actual system setup are used. In the scan visualization and export modes, the parameters stored in the corresponding document files are used.

The first step of the evaluation is a linearization of the filtered input signal to account for the compression characteristics of the detector diode. The compensation depends on the input signal, the



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diode type and the DC-transmission factor from the diode to the evaluation electronics. If the exciting field is pulsed, the crest factor of the signal must be known to correctly compensate for peak power.

The formula for each channel can be given as:

$$V_i = U_i + U_i^2 \times \frac{cf}{dcp_i}$$

With Vi = compensated signal of channel i, (i = x, y, z)

Ui = input signal of channel i, (i = x, y, z)

cf = crest factor of exciting field (DASY parameter) dcpi = diode compression point (DASY parameter)

From the compensated input signals, the primary field data for each channel can be evaluated:

$$\text{E-field Probes:} E_i = \sqrt{\frac{V_i}{\text{Norm}_i \times \text{ConvF}}}$$

H-field Probes:
$$H_i = \sqrt{V_i} \times \frac{a_{i0} + a_{i1} + a_{i2}f^2}{f}$$

With V_i = compensated signal of channel i, (i = x, y, z)

Norm_i = sensor sensitivity of channel i, (i = x, y, z), $\mu V/(V/m)^2$ for E-field Probes

ConvF = sensitivity enhancement in solution

a_{ii} = sensor sensitivity factors for H-field probes

f = carrier frequency [GHz]

E_i = electric field strength of channel i in V/m

H_i = magnetic field strength of channel i in A/m

The RSS value of the field components gives the total field strength (Hermitian magnitude):

$$E_{tot} = \sqrt{E_x^2 + E_y^2 + E_z^2}$$

The primary field data are used to calculate the derived field units.

$$SAR = E_{tot}^2 \times \frac{\sigma}{\rho \times 1000}$$

with SAR = local specific absorption rate in mW/g

E_{tot} = total field strength in V/m

σ = conductivity in [mho/m] or [Siemens/m]

 ρ = equivalent tissue density in g/cm³

Note that the density is set to 1, to account for actual head tissue density rather than the density of the tissue simulating liquid.



5.6. Test Equipment List

Manufacturer	Name of Equipment	Type/Model	Serial No./	Calibration	
wanuracturer	Manufacturer Name of Equipment Type/Mode		SW Version	Last Cal.	Due Date
SPEAG	DOSIMETRIC ASSESSMENT	cDASY6	V2.0.2.34	N/A	N/A
SPEAG	SYSTEM Software	mmWave	V 2.0.2.34	IN/A	IN/A
SPEAG	5G Validation Source	30GHz	1077	2023.12.02	2026.12.01
SPEAG	EUmmMV Probe	EUmmMV4	9602	2023.11.02	2024.11.01
SPEAG	EUmmMV Probe	EUmmMV4	9602	2024.03.12	2025.03.11
SPEAG	Data Acquisition Electronics	DAE4	480	2023.09.19	2024.09.18
R&S	Spectrum Analyzer	N9030A	MY54170556	2023.10.07	2024.10.06
KTJ	Thermo meter	TA298	N/A	2023.11.22	2024.11.21

Note:

The calibration certificate of DASY can be referred to appendix E of this report.

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6. System Verification Source

The system verification sources at 30GHz and above comprise born-antennas and very stable signal generators.

9	
Model	Ka-band born antenna
Calibrated Frequency	30GHz and above at 10mm from the case surface
Frequency Accuracy	±100 MHz
E-field Polarization	Linear
Harmonics	-20dBc
Total Radio Power	14dBm
Power Stability	0.05 dB
Power Consumption	5W
Size	100 x 100 x 100 mm
Weight	1 kg

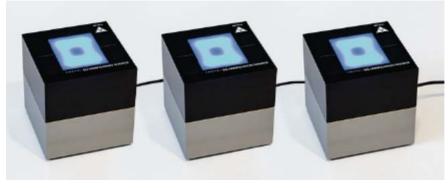


Fig 6.1 Photos of Verification Sources



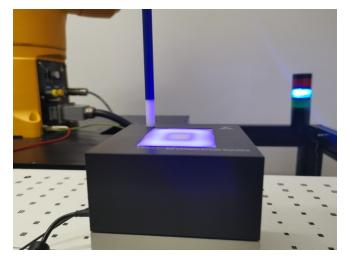
7. Power Density System Verification

General description

The EUT is replaced by a calibrated source, the same spatial resolution, measurement region and test separation used in the calibration was applied to system check. Through visual inspection into the measured power density distribution, both the spatially (shape) and numerically (level) have no noticeable difference. The measurement results should be within $\pm 10\%$ of the calibrated targets.

Frequency [GHz]	Grid step	Grid extent X/Y [mm]	Measurement points
10	$0.25 \left(\frac{\lambda}{4}\right)$	120/120	16×16
30	$0.25 \left(\frac{\bar{\lambda}}{4}\right)$	60/60	24×24
60	$0.25 \left(\frac{\hat{\lambda}}{4}\right)$	32.5/32.5	26×26
90	$0.25 \ (\frac{\lambda}{4})$	30/30	36×36

Setting for measurement of verification sources



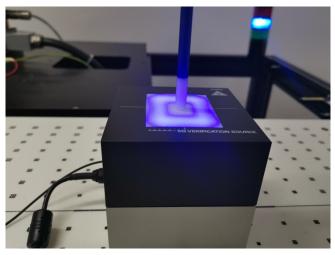


Fig 7.1 Photos of Verification Setup

Validation Results

After system check testing, the results of power density will be compared with the reference value derived from the certificate report. The deviation of system check should be within $\pm 10\%$.

<Validation Setup>

Frequency	5G Verification Source	Probe	DAE
(GHz)		S/N	S/N
30	30GHz-SN 1077	9602	480

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FL1-3, Building A, FeiYang Science Park, No.8 LongChang Road, Block67, BaoAn District, ShenZhen, GuangDong Province, P. R. China



< Validation Results>

Date	Frequency (GHz)	Test Distance (mm)	Measured 4cm² (W/m²)	Targeted 4cm² (W/m²)	Deviation (%)
2024.02.18	30	5.5	26.5	28.4	-6.7
2024.02.19	30	5.5	26.4	28.4	-7.0
2024.06.07	30	5.5	27.2	28.4	-4.2

Note: System checks the specific test data please refer to Annex C.

Computation of the Electric Field Polarization Ellipse

For the numerical description of an arbitrarily oriented ellipse in three-dimensional space, five parameters are needed: the semi-major axis (a), the semi-minor axis (b), two angles describing the orientation of the normal vector of the ellipse (ϕ , θ), and one angle describing the tilt of the semi-major axis (Ψ). For the two extreme cases, i.e. circular and linear polarizations, three parameters only (a, ϕ and θ) are sufficient for the description of the incident field.

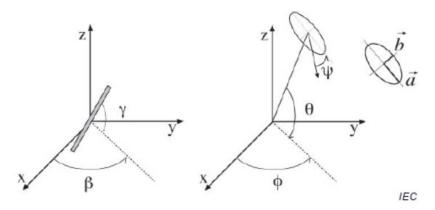


Fig 9.1 Illustration of the angles used for the numerical description of the sensor and the orientation of an ellipse in 3-D space

For the construction of the ellipse parameters from measured data, the problem can be reformulated as a nonlinear search problem. The semi-major and semi-minor axes of an elliptical field can be express as functions of the three angles (ϕ , θ and Ψ). The parameters can be uniquely determined towards minimizing the error based on least-squares for the given set of angles and the measured data. In this way, the numbers of three parameters is reduced from five to three, which means that least three sensors readings are necessary to gain sufficient information for the reconstruction of ellipse parameters. However, to suppress the noise and increase the reconstruction accuracy, it is desirable to have an over determined system of equations. The solution to use a probe consisting of two sensors angled by γ ₁ and γ ₂ toward the probe axis and to perform measurements at three angular positions of the probe, i.e. at β ₁, β ₂ and β ₃, results in over determination of two. If there is a need for more information or increased accuracy, more rotation angles can be added.

The reconstruction of ellipse parameters can be separated into linear and non-linear parts that are best solved by the givens algorithm combined with a downhill simplex algorithm. To minimize the mutual





coupling, sensor angles are set with a 90° shift ($\gamma_1 = \gamma_2 + 90^\circ$), and, to simplify, the first rotation angle of the probe (β_1) can be set to 0°.

> Total Field and Power Density Reconstruction

Computation of the power density in general requires knowledge of the electric and magnetic field amplitudes and phases in the plane of incidence. Reconstruction of these quantities from pseudo-vector E-field measurements is feasible, as they are constrained by Maxwell's equations. SPEAG have developed a reconstruction approach based on the Gerchberg-Saxton algorithm, which benefits from the availability of the E-field polarization ellipse information obtained with the EUmmWV2 probe.

The average of the reconstructed power density is evaluated over a circular area in each measurement plane. Two average power density values can be computed, the average total power density and the average incident power density, and the average total power density is used to determine compliance.

- |Re{S}| is the total Poynting vector
- n · $Re\{S\}$ is the normal Poything vector

The software post-processing reports to values, "S avg tot" and "S avg inc". "S avg tot" represents average total power density (all three xyz components included), and "S avg inc" represents average normal power density. The average total power density "S avg tot" is reported to determine the device compliance.





8. Antenna Information

8.1. Antenna Location

The location of antenna was recorded in annex B

ANT 1:

TRX: GSM 850, WCDMA Band V, LTE Band 5/12/13, 5G NR n5 (NSA)

PRX MIMO: LTE Band 2/4/7/66, 5G NR n2/66

ANT 2: PRX: LTE Band 48, 5G NR n48/77/78

ANT3: TRX: GSM 1900, WCDMA Band II/IV, LTE Band 2/4/7/66, 5G NR n2/66 (NSA)

DRX2: LTE Band 48, 5G NR n48/77/78

ANT4: TRX0: LTE Band 48, 5G NR n48/77/78(NSA)

ANT5: DRX: GSM 850/1900, WCDMA Band II/IV/V, LTE Band 2/4/5/7/12/13/66, 5G NR n2/5/66

ANT 7: ENDC TX: LTE Band 2/66

DRX: LTE Band 2/4/7/66, 5G NR n2/66 (NSA)

ANT 8: TX/RX: WLAN 2.4GHz/5GHz CH0, Bluetooth

RX: GPS

ANT9: TX/RX: WLAN 2.4GHz/5GHz CH1

ANT 10: TRX1(for ENDC): LTE Band 48, 5G NR n48/77/78(NSA)

NFC

Module: 5G n260/n261



8.2. Test Positions

> EUT Antenna Distance

Antenna Location	Front	Back	Left	Right	Тор	Bottom
QTM0	<5mm	<5mm	>25mm	<5mm	<25mm	>25mm

> Exclusion Evaluation for PD

Antenna	Measurement Plane						
Module	Front	Back	Left	Right	Тор	Bottom	
modulo	2mm	2mm	2mm	2mm	2mm	2mm	
QTM0	Yes	Yes	No	Yes	Yes	No	

Note:

- 1. From the Part0 report, beam IDs with the highest PD and corresponding input. power. limit were selected to be tested for each antenna module and frequency bands.
- 2. Referring to KDB 941225 D06, RF exposure must be measured for all sides and surfaces with a transmitting antenna located within 25mm from that surface or edge.



9. Power Density Assessment

> General Description

- 1. The 5G NR mmWave signal under testing was configured by the test tool of Qualcomm Software, and it is only limited to operate at EN-DC for 5G NR implementation according to the character of the device.
- 2. This device would be configured to maximum power when transmitting and tested at the maximum duty cycle for each RB configuration, modulation, bandwidth, and channel.
- 3. According to the manufacturer that summation for different antenna modules and exposure planes, the worst case would be selected for power density measurement.

mmWave EN-DC Combination

	200000000000000000000000000000000000000			
Sub-Category	EN-DC Combination	mmWave (FR2) 4G DL 4x4 MIMO	4G UL	5G-NR UL
1DL+FR2	DC_2A_n261A	2A	2A	n261A
1DL+FR2	DC_5A_n261A	-	5A	n261A
1DL+FR2	DC_13A_n261A	-	13A	n261A
1DL+FR2	DC_66A_n261A	66A	66A	n261A
2DL+FR2	DC_2A-2A_n261A	-	2A	n261A
2DL+FR2	DC_2A-5A_n261A	-	2A, 5A	n261A
2DL+FR2	DC_2A-13A_n261A	-	2A, 13A	n261A
2DL+FR2	DC_2A-66A_n261A	-	2A, 66A	n261A
2DL+FR2	DC_5A-66A_n261A	-	5A, 66A	n261A
2DL+FR2	DC_13A-66A_n261A	-	13A, 66A	n261A
2DL+FR2	DC_66A-66A_n261A	-	66A	n261A
1DL+FR2	DC_2A_n260A	2A	2A	n260A
1DL+FR2	DC_5A_n260A	-	5A	n260A
1DL+FR2	DC_13A_n260A	-	13A	n260A
1DL+FR2	DC_66A_n260A	66A	66A	n260A
2DL+FR2	DC_2A-5A_n260A	-	2A, 5A	n260A
2DL+FR2	DC_2A-13A_n260A	-	2A, 13A	n260A
2DL+FR2	DC_2A-66A_n260A	-	2A, 66A	n260A
2DL+FR2	DC_5A-66A_n260A	-	5A, 66A	n260A
2DL+FR2	DC_13A-66A_n260A	-	13A, 66A	n260A
2DL+FR2	DC_66A-66A_n260A	-	66A	n260A
1DL+FR2	DC_48A_n261A	48A	48A	n261A
1DL+FR2	DC_48A_n260A	48A	48A	n260A

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1DL+FR2	DC_2A_n261G	2A	2A	n261A, n261G
1DL+FR2	DC_5A_n261G	-	5A	n261A, n261G
1DL+FR2	DC_13A_n261G	-	13A	n261A, n261G
1DL+FR2	DC_66A_n261G	66A	66A	n261A, n261G
2DL+FR2	DC_2A-5A_n261G	ı	2A, 5A	n261A, n261G
2DL+FR2	DC_2A-13A_n261G	ı	2A, 13A	n261A, n261G
2DL+FR2	DC_2A-66A_n261G	ı	2A, 66A	n261A, n261G
2DL+FR2	DC_5A-66A_n261G	ı	5A, 66A	n261A, n261G
2DL+FR2	DC_13A-66A_n261G	1	13A, 66A	n261A, n261G
2DL+FR2	DC_66A-66A_n261G	-	66A	n261A, n261G
1DL+FR2	DC_2A_n260G	2A	2A	n260A, n260G
1DL+FR2	DC_5A_n260G	-	5A	n260A, n260G
1DL+FR2	DC_13A_n260G	-	13A	n260A, n260G
1DL+FR2	DC_66A_n260G	66A	66A	n260A, n260G
2DL+FR2	DC_2A-2A_n260G	-	2A	n260A, n260G
2DL+FR2	DC_2A-5A_n260G	-	2A, 5A	n260A, n260G
2DL+FR2	DC_2A-13A_n260G	-	2A, 13A	n260A, n260G
2DL+FR2	DC_2A-66A_n260G	-	2A, 66A	n260A, n260G
2DL+FR2	DC_5A-66A_n260G	ı	5A, 66A	n260A, n260G
2DL+FR2	DC_13A-66A_n260G	-	13A, 66A	n260A, n260G
2DL+FR2	DC_66A-66A_n260G	-	66A	n260A, n260G
1DL+FR2	DC_48A_n261G	48A	48A	n261A, n261G
1DL+FR2	DC_48A_n260G	48A	48A	n260A, n260G
1DL+FR2	DC_48A_n260G	48A	48A	n260A, n260G



> PD Measurement Plan

<n260>

Antenna Antenna		Beam ID		BW	Worst Position	Input Power Limit	N
Module	Group	1	2	(MHz)	from Part0	· (dBm)	Note
	AG0 (V)	18	-	100	Right Face	3.78	-
OTMO	AG1 (H)	140	-	100	Right Face	4.32	-
QTM0	MIMO	18	146	100	Right Face	0.92	TAV on
	MIMO	18	146	100	Right Face	0.92	TAV off

<n261>

Antenna Antenna		Beam ID		BW	Worst Position	Input Power Limit	N
Module	Group	1	2	(MHz)	from Part0	(dBm)	Note
	AG0 (V)	20	-	100	Right Face	1.0	-
OTMO	AG1 (H)	143	-	100	Right Face	0.78	-
QTM0	MIMO	20	148	100	Right Face	-2.34	TAV on
	MIMO	20	148	100	Right Face	-2.34	TAV off

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Test Results of RF Exposure

General Note

- The worst beam ID from Part 0 would be selected for power density testing according to the antenna information.
- 2. This device is enabled with Qualcomm Smart Transmit feature, it will manage and ensure LTE and 5G NR simultaneous transmission is compliant. The validation of the time-averaging algorithm and compliance under the TX varying transmission scenario for WWAN technologies are recorded in
- The default configuration is TAV on, when pushing the gm ext file to DUT EFS system, TAV will be disabled.

Test Results

<n260>

11200°							
Antenna	Antenna	Bea	m ID	Chanal	Signal	Exposure	Measured psPDtot+
Module	Group	1	2	Channel	Туре	Position	over 4cm ² (W/m ²)
	AG0 (V)	18	-	2254166	QPSK	Front Face	2.08
OTMO	AG0 (V)	18	-	2254166	QPSK	Back Face	0.90
QTM0	AG0 (V)	18	-	2254166	QPSK	Right Face	4.36
	AG0 (V)	18	-	2254166	QPSK	Top Face	0.19
	AG1 (H)	140	-	2254166	QPSK	Front Face	1.19
OTMO	AG1 (H)	140	-	2254166	QPSK	Back Face	1.36
QTM0	AG1 (H)	140	-	2254166	QPSK	Right Face	3.14
	AG1 (H)	140	-	2254166	QPSK	Top Face	0.85
				TAV on			
	MIMO	18	146	2254166	QPSK	Front Face	1.56
OTMO	MIMO	18	146	2254166	QPSK	Back Face	0.67
QTM0	MIMO	18	146	2254166	QPSK	Right Face	3.27
	MIMO	18	146	2254166	QPSK	Top Face	0.19
				TAV off			
	MIMO	18	146	2254166	QPSK	Front Face	1.86
QTM0	MIMO	18	146	2254166	QPSK	Back Face	1.63
Q I IVIU	MIMO	18	146	2254166	QPSK	Right Face	4.14
	MIMO	18	146	2254166	QPSK	Top Face	0.28

<n261>

Antenna	Antenna	Beam ID		Chamal	Signal	Exposure	Measured psPDtot+
Module	Group	1	2	Channel	Туре	Position	over 4cm² (W/m²)
	AG0 (V)	18	-	2077915	QPSK	Front Face	0.85
OTMO	AG0 (V)	18	-	2077915	QPSK	Back Face	1.17
QTM0	AG0 (V)	18	-	2077915	QPSK	Right Face	2.37
	AG0 (V)	18	-	2077915	QPSK	Top Face	0.38
OTMO	AG1 (H)	140	-	2077915	QPSK	Front Face	0.21
QTM0	AG1 (H)	140	-	2077915	QPSK	Back Face	0.08

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				1	ı				
	AG1 (H)	140	-	2077915	QPSK	Right Face	2.28		
	AG1 (H)	140	-	2077915	QPSK	Top Face	0.12		
	TAV on								
	MIMO	20	148	2077915	QPSK	Front Face	0.30		
OTMO	MIMO	20	148	2077915	QPSK	Back Face	0.41		
QTM0	MIMO	20	148	2077915	QPSK	Right Face	0.84		
	MIMO	20	148	2077915	QPSK	Top Face	0.13		
				TAV off					
	MIMO	20	148	2077915	QPSK	Front Face	0.77		
QTM0	MIMO	20	148	2077915	QPSK	Back Face	0.61		
Q I IVIU	MIMO	20	148	2077915	QPSK	Right Face	1.49		
	MIMO	20	148	2077915	QPSK	Top Face	0.14		



11. Simultaneous Transmission Assessment

11.1. Simultaneous Transmission Consideration

No.	Simultaneous Transmission Consideration	Head	Body-Worn	Hotspot
1	WWAN+WLAN 2.4GHz SISO/MIMO	Yes	Yes	Yes
2	WWAN+WLAN 5.2GHz/5.8GHz SISO/MIMO	Yes	Yes	Yes
3	WWAN+WLAN 5.3GHz/5.5GHz SISO/MIMO	Yes	Yes	No
4	WWAN+Bluetooth	Yes	Yes	Yes

Note: The co-location of WWAN+WLAN 2.4GHz/5GHz SISO would not be recorded since it is less than the combination of WWAN+WLAN 2.4GHz/5GHz MIMO.

11.2. Simultaneous Transmission Analysis

The EUT supports simultaneous transmission of multiple radios. RF exposure compliance in simultaneous transmission scenarios is evaluated in this section.

It must be noted here that Qualcomm Smart Transmit time-averaging algorithm was applied to only WWAN, where the time-averaged power level is controlled so that RF exposure is ≤ SAR_design_target for sub-6 WWAN and ≤ PD_design_target for 5G mmW NR. Since there is total design-related uncertainty arising from TxAGC and device-to-device variation, the worst-case RF exposure should be determined by accounting for this uncertainty in the corresponding design target, thus, with 1dB of device uncertainty for sub-6 WWAN and 2.1dB of device uncertainty for 5G mmW. Therefore, the worst-case RF exposure for this EUT is:

Worst-case Time-averaged RF Exposure for WWAN

110101 00	asc Time-averagea Iti Exposure i	101 1111/A11			
Title	WWAN Wireless System				
riue	Sub-6G	5G mmWave			
Maximum time-averaged power	P _{limit}	input.power.limit			
level		, ,			
Maximum time-averaged	SAR_design_target=0.8W/kg	PD design target = 6 W/m ²			
exposure	(1gSAR)	D_dcsign_target = 0 W/III			
Maximum Design-related	1.0 dB	2.1dB			
uncertainty	1.0 dB	2.106			
Weret age time granged DE		reported PD*			
Worst-case time-averaged RF	Reported SAR =1.0W/kg (1g)	=75%×PD_design_target+2.1dB			
exposure		= 7.5 W/m ²			

Note:

 The highest SAR value obtained from UL FCC SAR Test Report (Report No. SZ23040391S01). For scenarios where (P_{limit} + 1.0dB uncertainty) ≥ P_{max} (maximum RF tune-up output power),





time-averaged SAR exposure from Smart Transmit enabled EUT (at P_{limit}) cannot exceed reported SAR corresponding to P_{max} .

2. Smart Transmit allows only 75% of maximum PD exposure for this EUT using EFS entries listed in Trophy_mmw Power Density Simulation Report -Part0.

RF exposure compliance with WWAN+WLAN simultaneous transmission scenarios is demonstrated for various radio configurations using below equation:

Total norm. RF exposure = norm. RF exposure from Smart Transmit enabled WWAN (norm. SAR from 4G + norm. PD from 5G mmW) + norm. SAR from WLAN ≤ 1.0 normalized limit (1)

Smart Transmit algorithm in WWAN adds directly the time-averaged RF exposure from 4G and time-averaged RF exposure from 5G mmW, i.e.,

norm. RF exposure from Smart Transmit enabled WWAN: (normalized SAR exposure from 4G) + (normalized PD exposure from 5G mmW) ≤ 1.0 normalized limit (2)

In other words, Smart Transmit algorithm controls the total RF exposure from both 4G radio and 5G mmW NR to not exceed FCC limit. Smart transmit algorithm assumes hotspots are collocated (i.e., ignoring spatial distribution of hotspots) and directly adds normalized RF exposures from 4G and from 5G mmW, i.e..

If A = max normalized time-averaged SAR exposure from 4G,

B = max normalized time-averaged PD exposure from 5G mmW,

Then, equation (2) can be re-written as below because Smart Transmit assumes 4G hotspots are collocated with 5G mmW hotspot:

Smart Transmit enabled WWAN: x(t) * A + (1-x(t)) * B ≤ 1.0 normalized limit (3)

Here, "x(t)*A" represents percentage of normalized time-averaged RF exposure from 4G, and x(t) ranges between [0,1]; "(1-x(t))*B" is remaining percentage of RF exposure contribution from 5G mmW. Smart Transmit controls 'x' in real time such that the sum of these exposures never exceeds 1.0 normalized limit.

Note that mathematically:

$$(t) * A + (1-(t))*B \le max(A,B) \le 1.0 \text{ normalized limit for } x(t) \in [0,1] (4)$$

Therefore, if below equations (5a) and (5b) are proven:





A +norm.SAR from WLAN \leq 1.0 norm.limit (5a), B +norm.SAR from WLAN \leq 1.0 norm.limit (5b),

Then, based on equation (4), below condition is also proved:

 $[(t) * A + (1-(t))*B] + norm.SAR from WLAN \le 1.0 norm.limit (5c)$

Which is the same as equation (1), to demonstrate compliance for simultaneous transmission.

Additionally, it should be noted that in the absence of 5G mm, Smart Transmit limits the maximum RF exposure contributed from 4G to 100% normalized exposure (i.e., x=1.0 in equation 3), while with 5G mmW active, Smart Transmit limits the maximum RF exposure contributed from 5G mmW to 75% normalized exposure to guarantee at least 25% margin allocated to 4G LTE anchor to maintain the link (i.e., x=0.25 in equation 3). Therefore:

Smart Transmit enabled WWAN: A=max (normalized SAR exposure from 4G) ≤ 1.0 normalized limit (6a)

Smart Transmit enabled WWAN: B=max (normalized PD exposure from 5G mmW) ≤ 0.75 normalized limit (6b)

Thus, for compliance demonstration given by equation (1), below equation (7) obtained by combining equations (5a & 5b) and (6a & 6b), should be proven to guarantee simultaneous transmission compliance:

Total normalized RF exposure = norm. SAR from 4G WWAN + norm. SAR from WLAN < 1.0 normalized FCC limit (7a)

Total normalized RF exposure = 0.75*norm. PD from 5G mmW WWAN + norm. SAR from WLAN < 1.0 normalized FCC limit (7b)

The compliance for simultaneous transmission scenarios of WWAN (4G/5G mmW) radio enabled with Smart Transmit and WLAN without Smart Transmit is re-evaluated for all transmission scenarios supported by this EUT.

As described in equation (7), simultaneous transmission analysis for WWAN + WLAN is performed in two parts:

4G WWAN + WLAN (i.e., Eq. (7a) with compliance demonstration in SAR report SZ23040391S01 section 21.

5G mmW WWAN + WLAN (i.e., Eq. (7b) with compliance demonstration in section 11.1.





By combining above a. and b., the FCC requirement expressed in Eq. (1), re-written below, is met:

Total norm. RF exposure = norm. RF exposure from Smart Transmit enabled WWAN (norm. SAR from 4G + norm. PD from $5G \ mmW \ NR$) + norm. SAR from $WLAN \le 1.0$ normalized limit (1)

11.3. Total Exposure Radio Analysis

The fields generated by the antennas can be correlated or uncorrelated. At different frequencies, fields are always uncorrelated, and the aggregate power density contributions can be summed according to spatially averaged values of corresponding sources at any point in space, r, to determine the total exposure ratio (TER). Assuming I sources, the TER at each point in space is equal to

$$TER^{uncorr}(r) = \sum_{i=1}^{I} ER_i = \sum_{i=1}^{I} \frac{S_{av,i}(r, f_i)}{S_{lim}(f_i)}$$

Where $S_{av,i}$ is the power density for the source I operating at a frequency f_i and S_{lim} is the power density limit as specified by the relevant standard.

Exposure from transmitters operating above and below 6GHz, where 6GHz denotes the transmission frequency where the basic restrictions change from being defined in terms of SAR to being defined in terms of power density, therefore uncorrelated and the TER is determined as

$$TER^{uncorr}(r) = \sum_{i=1}^{I} ER_i = \sum_{i=1}^{I} \frac{S_{av,i}(r, f_i)}{S_{lim}(f_i)}$$

According to the FCC guidance in TCBC workshop and IEC TR 63170, the total exposure ratio calculated by taking ratio of maximum reported SAR divided by SAR limit and adding it to maximum measured power density by its limit. Numerical sum of the ratios should be less or equal to 1. Therefore the simultaneous transmission should be follows:

$$TER = \sum_{n=1}^{N} \frac{SAR_n}{SAR_{n,limit}} + \sum_{n=1}^{N} \frac{S_{m,avg}}{S_{m,limit}} < 1$$



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Total Exposure Ratio

<WLAN Summary for head>

Exposure	Maximum Reported SAR (W/kg)						
Position	WLAN 2.4GHz (ANT 8)	WLAN 2.4GHz (ANT 9)	WLAN 5GHz (ANT 8)	WLAN 5GHz (ANT 9)			
Right Cheek	0.223	0.080	0.274	0.263			
Right Tilt	0.233	0.038	0.376	0.297			
Left Cheek	0.523	0.186	0.457	0.396			
Left Tilt	0.400	0.067	0.473	0.492			

<WLAN Summary for body>

	Maximum Reported SAR								
Exposure		(W/kg)							
Position	WLAN 2.4GHz (ANT 8)	WLAN 2.4GHz (ANT 9)	WLAN 5GHz (ANT 8)	WLAN 5GHz (ANT 9)					
Front	0.146	0.122	0.171	0.084					
Back	0.239	0.439	0.486	0.419					
Left	0.027	0.015	0.014	0.017					
Right	0.157	0.216	0.208	0.129					
Тор	0.14	0.048	0.321	0.028					
Bottom	0	0	0	0					

<LTE + mmW+WLAN 2.4GHz MIMO for head>

_		Density //m²)		eported SAR /kg)	Total Exposure Ratio SAR/1.6 + PD/10		
•	Position 1 2 n260 n261		3	4	Summation	Summation	
Position			WLAN 2.4GHz WLAN 2.4GHz (ANT 8) (ANT 9)		1+3+4	2+3+4	
Right Cheek	2.08	0.85	0.223	0.080	0.397	0.274	
Right Tilt	2.08	0.85	0.233	0.038	0.377	0.254	
Left Cheek	2.08	0.85	0.523	0.186	0.651	0.528	
Left Tilt	2.08	0.85	0.400	0.067	0.500	0.377	

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<LTE + mmW+WLAN 2.4GHz MIMO for body>

_	Power Density (W/m²)			eported SAR (kg)	Total Exposure Ratio SAR/1.6 + PD/10		
Exposure Position	1	2	3	4	Summation	Summation 2+3+4	
1 osition	n260	n261	WLAN 2.4GHz	WLAN 2.4GHz	1+3+4		
			(ANT 8)	(ANT 9)			
Front	2.08	0.85	0.146	0.122	0.376	0.253	
Back	1.63	1.17	0.239	0.439	0.587	0.541	
Left	0	0	0.027	0.015	0.026	0.026	
Right	4.36	2.37	0.157	0.216	0.669	0.470	
Тор	0.85	0.38	0.14	0.048	0.203	0.156	
Bottom	0	0	0	0	0.000	0.000	

<LTE + mmW+WLAN 5GHz MIMO for head>

_	Power Density (W/m²)			eported SAR kg)	Total Exposure Ratio SAR/1.6 + PD/10		
Exposure Position	1 2		3 4		Summation	Summation	
1 Osition	n260	n261	WLAN 5GHz	WLAN 5GHz	1+3+4	2+3+4	
	11200	11201	(ANT 8)	(ANT 9)	. • .	, ,	
Right Cheek	2.08	0.85	0.274	0.263	0.544	0.421	
Right Tilt	2.08	0.85	0.376	0.297	0.629	0.506	
Left Cheek	2.08	0.85	0.457	0.396	0.741	0.618	
Left Tilt	2.08	0.85	0.473	0.492	0.811	0.688	

<LTE + mmW+WLAN 5GHz MIMO for body>

		Density ′m²)		eported SAR (kg)	Total Exposure Ratio SAR/1.6 + PD/10		
Exposure Position	1	2	3	4	Summation	Summation	
Position	000	004	WLAN 5GHz WLAN 5GHz		1+3+4	Summation 2+3+4	
	n260	n261	(ANT 8)	(ANT 9)	11314	2.3.4	
Front	2.08	0.85	0.171	0.084	0.367	0.244	
Back	1.63	1.17	0.486	0.419	0.729	0.683	
Left	0	0	0.014	0.017	0.019	0.019	
Right	4.36	2.37	0.208	0.129	0.647	0.448	
Тор	0.85	0.38	0.321	0.028	0.303	0.256	
Bottom	0	0	0	0	0.000	0.000	

Note:

1. The SAR results of WLAN were referred to the SAR report SZ23040391S01.



- The highest simulating psPD of 5G mmW recorded in above table are from the Trophy_mmw Power Density Simulation Report -Part0.
- The simultaneous transmission of mmW beam paired recorded in SZCR240300087101 Power
 Density Measurement Report would not be shown above because it is less than the single beam ID
 feature.
- 4. The mmw uses the PD data of the body (front & back) to replace the head and WLAN 2.4GHz/5GHz/Bluetooth co-transmission calculation.



12. Uncertainty Assessment

The budget is valid for evaluation distance $> \lambda / 2\pi$. For specific tests and configurations, the uncertainty can be considered smaller.

	1	Τ				T	
Error Description	Uncertainty ± %	Probability	Divisor	ci	Standard Uncertainty (±%)	ν _i orν _{eff}	
Uncertainty terms dependent on	the measureme	ent system			1	I	
Probe calibration	0.43	1	R	1	0.49	∞	
Probe correction	0.48	1.732	R	0.7	0.49	∞	
Isotropy	0.48	1.732	R	0.7	0.29	∞	
Multiple reflections	0.19	1.732	R	1	0.12	∞	
System linearity	0.24	1.732	R	1	0.12	∞	
Probe positioning	0.28	1.732	R	1	0.17	∞	
Sensor location	0.2	1.732	R	1	0.18	∞	
Amplitude and phase drift	0.02	1	R	1	0.0	∞	
Amplitude and phase noise	0.18	1.732	R	1	0.12	∞	
Data point spacing	0.06	1.732	R	1	0.08	∞	
Measurement area truncation	0.63	1.732	R	1	0.6	∞	
Reconstruction algorithms	0.04	1.732	R	1	0.05	∞	
Uncertainty terms dependent on	the DUT and er	nvironmental	factors				
Probe coupling with DUT	0.05	1.732	R	1	0.08	∞	
Modulation response	0.34	1.732	R	1	0.23	8	
Integration time	0.01	1	R	1	0.00	8	
DUT alignment	0.12	1.732	R	1	0.3	8	
RF ambient conditions	0.20	1.732	R	1	0.12	∞	
Immunity / secondary reception	0.03	1.732	R	1	0.04	∞	
Drift of the DUT	0.06	1	R	1	0.01	∞	
Combir	Combined standard uncertainty						
Cov	erage Factor for	95%		<u> </u>	K=2	N/A	
Expand	led standard und	ertainty			1.52 dB	IN/A	



Annex A General Information

Identification of the Responsible Testing Laboratory

· · · · · · · · · · · · · · · · · · ·	
Laboratory Name:	Shenzhen Morlab Communications Technology Co., Ltd.
Laboratory Address:	FL.1-3, Building A, FeiYang Science Park, No.8 LongChang
	Road, Block 67, BaoAn District, ShenZhen, GuangDong Province,
	P. R. China
Telephone:	+86 755 36698555
Facsimile:	+86 755 36698525

Identification of the Responsible Testing Location

Name:	Shenzhen Morlab Communications Technology Co., Ltd.
Address:	FL.3, Building A, FeiYang Science Park, No.8 LongChang Road,
	Block 67, BaoAn District, ShenZhen, GuangDong Province, P. R.
	China

3. Facilities and Accreditations

The FCC designation number is CN1192, the test firm registration number is 226174.

***** END OF MAIN REPORT *****

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