
SIMPL (Satlet Initial Mission Proofs and Lessons) Orbital Debris Assessment Report

Report Number

NWS-ISS01-ODAR-001-008

Prepared for

U.S. Federal Communications Commission (FCC)

Contract Number

Report Date

2015 11 03

Submitted by

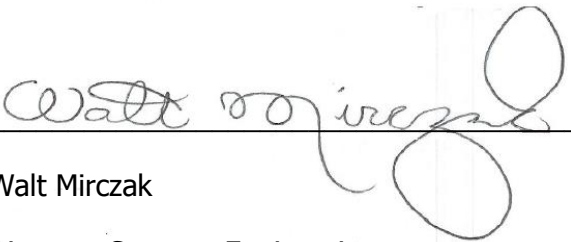
NOVAWURKS, INC.



1.0 DOCUMENTATION CONTROL INFORMATION

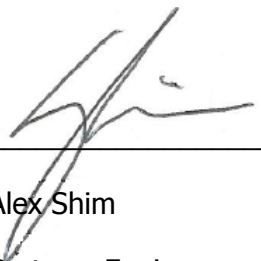
1. PROGRAM NAME					2. CONTRACT NUMBER				
NA					NA				
3. REPORT TITLE					4. PERFORMING ORGANIZATION REPORT NUMBER				
SIMPL (Satlet Initial Mission Proofs and Lessons) Orbital Debris Assessment Report					NWS-ISS01-ODAR-001-008				
5. REPORT TYPE		6. REPORT DATE		7. RELEVANT REPORTING PERIOD		8. CLIN/SUBCLIN/MILESTONE/TASK (WBS) NUMBER			
Rep		2015 11 3		NA		NA			
9. AUTHOR									
Alex Shim, Systems Engineer NovaWurks, Inc. 10772 Noel St. Los Alamitos, CA 90720									
10. PROGRAM SPONSOR					11. PROGRAM SPONSOR'S REPORT NUMBER				
NA									
12. EXPORT STATEMENT									
No ITAR controlled information exists in this document.									
13. DISTRIBUTION STATEMENT									
14. SECURITY CLASSIFICATION									
14.a REPORT			14.b ABSTRACT			14.c DOCUMENTATION PAGE (THIS PAGE)			
Unclassified			Unclassified			Unclassified			
15. PROPRIETARY STATEMENT									
16. INTENDED AUDIENCE									
16.a NovaWurks Engineering	16.b NovaWurks All	16.c FCC	16.d	16.e FOUO Government	16.f	16.g NovaWurks Partners (FOUO/NDA)	16.h NovaWurks Partners	16.i Industry	16.j General Public
Approved	Approved	Approved	NA	Approved	Approved	Approved	Approved	Approved	Approved
17. CONTACT INFO						18. NUMBER OF PAGES			
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2.0 SELF-ASSESSMENT OF THE ODAR USING THE FORMAT IN THE APPENDIX A.2 OF NASA-STD-8719.14

A self assessment is provided below in accordance with the assessment format provided in Appendix A.2 of NASA-STD-8719.14. In the final ODAR document, this assessment will reflect any inputs received from OSMA as well.

Orbital Debris Self-Assessment Report Evaluation: NovaWurks SIMPL

Requirement	Compliance Assessment	Comments
4.3-1a	Compliant	
4.3-1b	Compliant	
4.3-2	Compliant	
4.4-1	Compliant	
4.4-2	Compliant	
4.4-4	Compliant	
4.5-1	Compliant	
4.5-2	Compliant	
4.6-1 (a)	Compliant	
4.6-1 (b)	Compliant	
4.6-1 (c)	Compliant	
4.6-2	Compliant	
4.6-3	Compliant	
4.6-4	Compliant	
4.6-5	Compliant	
4.7-1	Compliant	
4.8-1	Not Applicable	

Table 2-1

2.1 Assessment Report Format

ODAR Technical Sections Format Requirements: This ODAR follows the format recommended in NASA-STD-8719.14, Appendix A.1 and includes the content indicated at a minimum in each section 2 through 8 below for the NovaWurks SIMPL (Satlet Initial Mission Proofs and Lessons) satellite. Sections 9 through 14 apply to the launch vehicle ODAR and are not covered here.

3.0 ODAR SECTION 1: PROGRAM MANAGEMENT AND MISSION OVERVIEW

Principal Investigator: Talbot Jaeger

Program Manager: Thomas Sanders

Schedule: NovaWurks will have LEO flight-qualified HISats ready early Q4 2014 with deliveries to integrator in early October 2015 for testing and integration. The schedule supports an expected cargo vehicle resupply launch on December 3rd 2015 with an ISS out-the-door and satellite deployment date of December 21st 2015.

Mission Overview

NovaWurks is planning to demonstrate an on-orbit assembly, ISS deployment, and LEO flight of the NovaWurks Hyper-Integrated Satlet (HISat) system. The proposed research utilizes a cargo vehicle flight to the ISS with at least six HISats and a small interface experiment packaged individually. The mission is named Satlet Initial Mission Proofs and Lessons, or SIMPL which is the first demonstration of a cellularized spacecraft architecture. The minimum expected duration of the mission is expected to be a minimum of two weeks to a maximum of four months. The ISS astronaut crew available during the month of December 2015 will assemble the HISats into a package of aggregated cells, also known as a PAC.

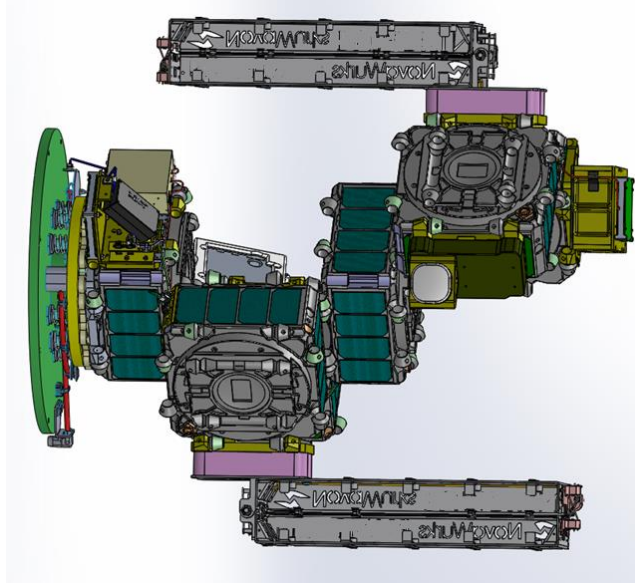


Figure 1 SIMPL – Assembled

After assembly, the PAC will be mounted on the JAXA Multi-Purpose Experiment Platform (MPEP), and placed on the JEM airlock slide table for transfer outside the ISS.

The SIMPL PAC will be deployed from the ISS for free flying operations. An approach similar to prior cubesat deployments will be utilized where a crewmember operates the JEM Remote Manipulating System (JRMS) – to grapple and position the PAC for deployment. As a free flyer, the PAC will conduct experiments for at least two weeks with a goal of maintaining operations through the duration of its orbital lifetime.

The NovaWurks SIMPL will be placed in a near circular orbit of 419 x 411 Km at an inclination of 51.65 degrees. The orbit parameters are subject to change closer to release due to ISS orbit degradation or raising.

Launch Vehicle and Launch Site: Atlas V, Kennedy Space Center – Cape Canaveral, FL

Proposed Launch date: Dec. 3rd 2015

Proposed Deployment date: Dec. 21st 2015

Mission Duration: Nominally two weeks for experimental testing of cellular technology with a maximum operating duration of no longer than four months. SIMPL will be expected to orbit for 325 days until reentry via atmospheric orbital decay. (Calculated) After the project goals and objectives have been completed, the spacecraft will be passivated to reduce the probability of an on-orbit hazard.

Launch and Deployment profile:

- **Flight Day 1 (Launch):** After a 10-minute flight sequence, Atlas V will launch the Cygnus CRS Orb-4 capsule into orbit on the same plane as the space station, but significantly below it. Cygnus will deploy its

solar arrays after separation from Atlas V. After a series of checks, ground controllers will command Cygnus to begin increasing its altitude. [HISats are soft-packed inside the Cygnus pressurized cargo area.]

- Flight Day 2 & 3: Cygnus will continue to increase its altitude to match that of the space station.
- Flight Day 4: NASA will make a go/no-go decision for Cygnus to berth with the station. Cygnus will first autonomously approach within 12 metres (39 ft) below the space station, where it will stop and hold. Astronauts aboard the station will then command Cygnus to a “free drift” mode, where they will then capture it with the station's robotic arm attached to the station's Nadir node.
- Flight Day 5 to Day 36: ISS Astronauts will open Cygnus hatch, unload the payload and fill it with disposal cargo.
- Day 36 $T_{\text{Deployment}}$ (est. $T + 18$ days) by ISS Crew Schedule: ISS astronauts will assemble the HISats into a PAC which will be mounted on the JAXA Multi-Purpose Experiment Platform (MPEP), and placed on the JEM airlock slide table for transfer outside the ISS.
- Day 36 $T_{\text{Deployment}}$ by JEM airlock Schedule: The SIMPL is transferred to the ISS exterior where a crewmember operates the JEM Remote Manipulating System (JRMS) – to grapple and position the PAC for deployment.
- Day 36 $T_{\text{Deployment}}$ by orbital deployment constraints: The NovaWurks SIMPL will be released into a near circular orbit of 419 x 411 Km at an inclination of 51.65 degrees with deployment occurring at a robot arm position and orientation that precludes SIMPL contacting the ISS on its deployment trajectory and any re-contact occurring over subsequent orbits.
- Day 36 $T_{\text{Deployment}}$ Immediately after deployment, several microswitches on the spacecraft/ISS interface plane will be closed, initiating a 30 minute internal timer in the spacecraft. All operations including boot up of the spacecraft processors, attitude control, and initiation of the amateur service communications are autonomous and do not need a ground command to start and will be autonomous.
- Day 36 $T_{\text{Deployment}}$ Mission Operations ($T_{\text{Deployment}} + 14$ days) The spacecraft will continue to operate as a OSCAR (Orbiting Satellite Carrying Amateur Radio) for a duration of two weeks until attitude control fluid is expended.
- $T_{\text{Deployment}} + 325$ days: The spacecraft will be in an uncontrolled attitude and tumbling. No substantial power generation from the spacecraft is expected and will not cause subsystems to start.

4.0 ODAR SECTION 2: SPACECRAFT DESCRIPTION

Physical description of the spacecraft

The assembled PAC conforms to the limitations of the JAXA MPEP occupying a volume no greater than 50 x 50 x 33 cm and weighing approximately 59.9 Kg. Attached to the PAC are two deployable solar panels, two radio units (with one deployable whip antenna) and one camera unit (See Figure 1).

Each HISat has a load bearing aluminum structure approximately 20 x 20 x 10 cm in dimension.

Total spacecraft mass at launch, including all propellants and fluids: 59.9 Kg

Dry mass of spacecraft at launch, excluding solid rocket motor propellants: 55.9 Kg

Description of all propulsion systems:

Each HISat contains an integral propulsion system of thrusters, valves, valve drivers, propellant, and propellant storage. The system is rated for 0-155 PSI service with a non-toxic propellant. All pressurized components are designed to 4x MEOP and according to MIL SPEC 1522A standards. A leak before burst design of each pressurized component ensures that there will be no brittle failures or burst conditions.

The HISat thrusters do not utilize heating elements and will not produce supersonic gas flow in any portion of the system.

HISat Pressure Vessels

Each HISat has two pressure vessels; the Main Outer Housing and the inner cylindrical tank. All pressure vessels consist of an aluminum pressure vessel verified to meet 1552A burst requirements and to exhibit a leak-before-burst failure mode. The safety factor for the outer housing was verified to be 2.6 while the inner cylindrical tank was verified to be 3. The tank is rated for 155 PSIA service with a designed 4x MEOP and 7.5x NOP.

Identification, including mass and pressure, of all fluids (Liquids and gases) planned to be on board and a description of the fluid loading plan or strategies

The only fluid/propellant used in HISats is the cold gas propellant. The propellant is a commonly used commercial refrigerant which has been accepted by the safety panel for ISS missions. The refrigerant poses no dangerous or hazardous condition for on-orbit and launch operations. It is a clear, colorless liquid and vapor with a faint ethereal odor and is a gas at ambient temperatures with the boiling point below -20°, freezing point above -100°C. It is non-flammable with 100% volatiles and is considered stable.

The total mass of the fluid in the PAC is 3 Kg and the nominal pressure is 80 PSI at room temperature with a service pressure of 0-155 PSI. The fluid is loaded into each HISat before launch and checked for leakage above the specified acceptable level. Moreover, the propellant will vaporize once released from the attitude thrusters in the vacuum conditions of the space environment.

Fluids in Pressurized Batteries: There are no fluids in the pressurized batteries. The PAC uses unpressurized standard COTS Lithium-Ion battery cells.

Description of active and/or passive attitude control systems with an indication of normal attitude of the spacecraft with respect to the velocity vector:

Two sets of active attitude control actuators are available in the PAC. There are cold gas thrusters, previously described, available and six reaction wheels which provide attitude stabilization and directional control. The actuators are supported by a suite of available sensors including sun sensors, star sensors, and gyroscopes. Active attitude control will be utilized to point and maintain the PAC throughout the mission duration. It is expected that the mission duration will be defined by the amount of available propellant left in the vehicle. The spacecraft is expected to expend all of the propellant from attitude control in two weeks. After the propellant is expended, the spacecraft will lose control and degrade its orbit through an uncontrolled tumble until re-entry. During this uncontrolled phase the spacecraft will not generate enough power to supply the subsystems, including communications.

Description of any range safety or other pyrotechnic devices: There are no pyrotechnic devices used on the PAC. There are three non explosive initiators which are used to deploy a whip antenna and the solar panels. The NEIs are classified as Category B – Non Hazardous as defined in the AFSPCMAN91-710 Section 13.6.6.

Description of the electrical generation and storage system: The PAC uses COTS Lithium-ion battery cells (108 total for the PAC) which are charged before payload integration to provide electrical energy during the mission. The batteries are charged using the mounted solar panels and an internal circuit on each HISat provides distributed power. The energy generated from the solar panels will be distributed into each HISat. The design meets the requirements of AFSPCMAN91-710 sections 19.2.1-19.2.5.

Identification of any other sources of stored energy not noted above: None

Identification of any radioactive materials on board: No radioactive materials on board

5.0 ODAR SECTION 3: ASSESSMENT OF SPACECRAFT DEBRIS RELEASED DURING NORMAL OPERATIONS

Identification of any object (>1 mm) expected to be released from the spacecraft any time after launch, including object dimensions, mass, and material:

There are no objects expected to be released from the spacecraft at any time after launch.

Rationale/necessity for release of each object: N/A

Time of release of each object, relative to launch time: N/A

Release velocity of each object with respect to spacecraft: N/A

Expected orbital parameters (apogee, perigee, and inclination) of each object after release: N/A

Calculated orbital life time of each object, including time spent in Low Earth Orbit (LEO): N/A

Assessment of spacecraft compliance with Requirements 4.3-1 and 4.3-2: Compliant

6.0 ODAR SECTION 4: ASSESSMENT OF SPACECRAFT INTENTIONAL BREAKUPS AND POTENTIAL FOR EXPLOSIONS

Potential causes of spacecraft breakup during deployment and mission operations:

There is no credible scenario which would result in the spacecraft to break up in normal deployment and operations.

Summary of failure modes and effects analysis of all credible failure modes which may lead to an accidental explosion:

A malfunction of the HISat battery protection circuit could possibly lead to a short circuit resulting in overheating and a remote possibility of a battery cell explosion. The failure modes and effects analysis is described in the assessment of spacecraft compliance with Requirements 4.4-1 through 4.4-4 below.

Detailed plan for any designed spacecraft breakup, including explosions and intentional collisions:

There are no plans for any designed spacecraft breakup in the SIMPL mission.

List of components which are passivated at EOM. List includes method of passivation and amount which cannot be passivated.

The battery cells will not be passivated due to the low risk of explosive rupturing. However, once the spacecraft is tumbling due to propellant depletion, the batteries are ultimately passivated in the natural progression of the mission. The batteries will become completely discharged with the solar arrays no longer pointed towards the sun.

The pressure vessels are also passivated through the natural progression of the mission due to the limited amount of propellant available. It is expected that the pressure vessels will be empty after two weeks of nominal operations and attitude control.

Rationale for all items which are required to be passivated, but cannot be due to their design:

Each HISat contains built in battery charge circuits which protect the cells from overcharge and also feature parallel configurations to limit the risk of battery failure. If the cells however, do explosively rupture, all of the debris will be contained by the previously described pressure vessels due to the lack of penetration energy.

Assessment of spacecraft compliance with Requirements 4.4-1 through 4.4-4:

4.4-1 Limiting the Probability of Accidental Explosion

There are a few very low probability failure modes which may theoretically reach a battery explosion condition. The following conditions are listed below:

Short Circuit

Flight batteries undergo extensive acceptance testing from the lot of batteries which are acquired from the vendor. In order to mitigate the possibility of internal short circuits, the cells have been tested through various environmental and functional testing. (Vibration, Shock, Thermal Vacuum)

HISat circuits are designed to be fail-safe in order to prevent the possibility of a short circuit and safety factors in the mechanical designs ensure that the possibility of structural failure is negligible.

Internal thermal rise due to high load discharge rate:

The HISat batteries are thermally managed. Cells are tested in a higher than normal temperature environment to verify any anomalies before launch. No significant thermal increase was detected due to a high load discharge rate.

All HISat batteries are contained in a pressure vessel. The risk of explosion from any high pressure/temperature failure scenario is mitigated by the leak before burst design of the tank. Therefore, three failures must occur for a possible explosion scenario. 1) A short circuit 2) Passive thermal management malfunction 3) Leak before burst design error.

Excessive discharge or short circuit due to external device failure

HISat battery holders are chamfered to prevent case insulation penetration of the cells. A Chromtherm thermal pad is placed on the top and bottom of each cell to prevent shorting and to provide good thermal conductivity.

Inoperable Vents

No design feature blocks the cell vents.

Crushing

The batteries are not subject to any crushing risk beyond catastrophic HISat crushing from an external source.

Low Level current leakage or short-circuit through battery pack case or due to moisture-based degradation of insulators

There is no moisture present in the cell area due to the presence of the coolant. The coolant does not conduct electricity and has been tested for many hours with the cells with no anomalies.

Excess temperatures due to orbital environment and high discharge combined

The passive thermal system maintains operational temperature of the PAC through natural circulation of the coolant therefore excess temperatures due to orbital environment and high discharge combined do not present an explosion hazard.

In addition to the FMEA, the manufacturer has performed various tests on each cell which did not result in any fire or explosion. Details of these tests are in the charts below.

No.	Items	Test Method and Condition	Criteria
1	Vibration Test	After standard charging, fixed the cell to vibration table and subjected to vibration cycling that the frequency is to be varied at the rate of 1Hz per minute between 10Hz an 55Hz, the excursion of the vibration is 1.6mm. The cell shall be vibrated for 30 minutes per axis of XYZ axes.	No leakage No fire
2	Drop Test	The cell is to be dropped from a height of 1 meter twice onto concrete ground.	No explosion, No fire, no leakage.

Item	Battery Condition	Test Method	Requirements
Crush	Fresh, Fully charged	Crush between two flat plates. Applied force is about 13kN(1.72Mpa) for 30min.	No explosion, No fire
Short Circuit (20°C)	Fresh, Fully charged	Each test sample battery, in turn, is to be short-circuited by connecting the (+) and (-) terminals of the battery with a Cu wire having a maximum resistance load of 0.1 Ω . Tests are to be conducted at room temperature($20 \pm 2^\circ\text{C}$).	No explosion, No fire The Temperature of the surface of the Cells are lower than 150°C
Short Circuit (60°C)	Fresh, Fully charged	Each test sample battery, in turn, is to be short-circuited by connecting the (+) and (-) terminals of the battery with a Cu wire having a maximum resistance load of 0.1 Ω . Tests are to be conducted at temperature($60 \pm 2^\circ\text{C}$).	No explosion, No fire The Temperature of the surface of the Cells are lower than 150°C
Impact	Fresh, Fully charged	A 56mm diameter bar is inlayed into the bottom of a 10kg weight. And the weight is to be dropped from a height of 1m onto a sample battery and then the bar will be across the center of the sample.	No explosion, No fire
Over-Discharged	Fresh, Fully charged	Discharge at a current of 1 CsA for 2.5h.	No explosion, No fire
Over-charged	Fresh, Fully charged	Charge at a current of 3 CsA to 10V.	No explosion, No fire

Table 1 Battery Manufacturer Test Results

In addition to the manufacturer tests, NovaWurks has conducted similar tests with the same results from the manufacturer to verify the safety of the cells. To ensure that the spacecraft does not pose a hazard, an extreme case was tested in which the battery pack was short-circuited in the flight configuration. No explosion, fire or leakage was observed due to the passivation strategy integral to the design of the batteries and the spacecraft.

7.0 ODAR SECTION 5: ASSESSMENT OF SPACECRAFT POTENTIAL FOR ON-ORBIT COLLISIONS

Requirement 4.5-1: Limiting debris generated by collisions with large objects when operating in Earth orbit:

An analysis was run in NASA DAS for Requirement 4.5-1. The program input required cross sectional area which was calculated from SIMPL's passively stable orientation and the orbit duration determined from the science and engineering tool provided. As shown in the results from the analysis below, the collision probability is 0 or negligible; therefore SIMPL is compliant for this requirement.

 2015; 17:32:01PM Processing Requirement 4.5-1: Return Status : Passed

=====

Run Data

=====

****INPUT****

```

Space Structure Name = SIMPL
Space Structure Type = Payload
Perigee Altitude = 400.060000 (km)
Apogee Altitude = 407.900000 (km)
Inclination = 51.650000 (deg)
RAAN = 0.000000 (deg)
Argument of Perigee = 0.000000 (deg)
Mean Anomaly = 0.000000 (deg)
Final Area-To-Mass Ratio = 0.002637 (m^2/kg)
Start Year = 2015.500000 (yr)
Initial Mass = 64.250000 (kg)
Final Mass = 60.660000 (kg)
Duration = 0.890000 (yr)
Station-Kept = False
Abandoned = True
PMD Perigee Altitude = -1.000000 (km)
PMD Apogee Altitude = -1.000000 (km)
PMD Inclination = 0.000000 (deg)
PMD RAAN = 0.000000 (deg)
PMD Argument of Perigee = 0.000000 (deg)
PMD Mean Anomaly = 0.000000 (deg)
  
```

****OUTPUT****

```

Collision Probability = 0.000000
Returned Error Message: Normal Processing
Date Range Error Message: Normal Date Range
Status = Pass
  
```

=====

===== End of Requirement 4.5-1 =====

Table 2 DAS Inputs and Outputs for 4.5-1

Requirement 4.5-2: Limiting debris generated by collisions with small objects when operating in Earth orbit

NASA DAS was used to determine the probability of whether collisions with small objects would compromise the spacecraft's ability for de-orbit operations. In the SIMPL mission, delta V maneuvers are not necessary to meet the 25 year de-orbit requirement. However, propellant venting is required for passivation purposes. In order for the propellant venting to malfunction, the internal electronics boards would need to be affected before compromising de-orbit abilities. Two areas of each HISat were analyzed, the carousel top which and the rest of the carousel body which shielded by the outer aluminum housing. The results of the analysis shown below indicate compliance to requirement 4.5-2.

=====	=====
Run Data	Spacecraft = SIMPL
=====	Critical Surface = Carousel Shielded by Housing
=====	=====
INPUT	**INPUT**
Space Structure Name = SIMPL	Apogee Altitude = 407.900000 (km)
Space Structure Type = Payload	Perigee Altitude = 400.060000 (km)
Perigee Altitude = 400.060000 (km)	Orbital Inclination = 51.650000 (deg)
Apogee Altitude = 407.900000 (km)	RAAN = 0.000000 (deg)
Inclination = 51.650000 (deg)	Argument of Perigee = 0.000000 (deg)
RAAN = 0.000000 (deg)	Mean Anomaly = 0.000000 (deg)
Argument of Perigee = 0.000000 (deg)	Final Area-To-Mass Ratio = 0.002637 (m ² /kg)
Mean Anomaly = 0.000000 (deg)	Start Year = 2015.500000 (yr)
Final Area-To-Mass Ratio = 0.002637 (m ² /kg)	Initial Mass = 64.250000 (kg)
Start Year = 2015.500000 (yr)	Final Mass = 60.660000 (kg)
Initial Mass = 64.250000 (kg)	Duration = 5.405000 (yr)
Final Mass = 60.660000 (kg)	Station-Kept = False
Duration = 5.405000 (yr)	Abandoned = True
Station-Kept = False	PMD Perigee Altitude = -1.000000 (km)
Abandoned = True	PMD Apogee Altitude = -1.000000 (km)
PMD Perigee Altitude = -1.000000 (km)	PMD Inclination = 0.000000 (deg)
PMD Apogee Altitude = -1.000000 (km)	PMD RAAN = 0.000000 (deg)
PMD Inclination = 0.000000 (deg)	PMD Argument of Perigee = 0.000000 (deg)
PMD RAAN = 0.000000 (deg)	PMD Mean Anomaly = 0.000000 (deg)
PMD Argument of Perigee = 0.000000 (deg)	
PMD Mean Anomaly = 0.000000 (deg)	
OUTPUT	**OUTPUT**
Collision Probability = 0.000000	Probability of Penetration = 0.000047
Returned Error Message: Normal Processing	Returned Error Message: Normal Processing
Date Range Error Message: Normal Date Range	Date Range Error Message: Normal Date Range
Status = Pass	
=====	

Table 3 DAS Inputs and Outputs for 4.5-2

8.0 ODAR SECTION 6: ASSESSMENT OF SPACECRAFT POST-MISSION DISPOSAL PLANS AND PROCEDURES

Description of spacecraft disposal option selected:

The SIMPL disposal strategy is passivation by mission progression, natural orbital decay, and an uncontrolled, tumbling re-entry. The SIMPL's orbit will naturally decay within 25 years (~ 325 days, best calculations) after mission operations satisfying requirement 4.6-1a. It is expected that all propellants will be depleted from two weeks of autonomous attitude control operations before any post-mission disposal operations. This will cause the spacecraft to lose attitude and start to tumble. In this tumbling state, the vehicle will expend all battery power remaining and will deplete the batteries to 0% depth of discharge.

At this point all subsystem functionality including RF communications will be ceased. Additionally the APRS service has an on/off capability and can be disabled at any time during the mission.

Identification of all systems or components required to accomplish any post mission disposal operation, including passivation and maneuvering:

The cross sectional area of the passively stabilized orientation is estimated to be 0.1752 m² and the final mass is 59.9 kg giving us an area to mass ratio of 0.029 m²/kg in the absolute worst case condition. This condition is highly improbable however shows the upper bounds in orbit lifetime. Ballistic numbers from a finer resolution NASA assessment concluded with A/M ratios of 0.011-0.0205 m²/kg during active attitude control and 0.0068-0.0076 m²/kg resulting in orbit lifetimes of 125-325 days.

Assessment of spacecraft compliance with Requirements 4.6-1 through 4.6-5

Requirement 4.6-1: Disposal for space structures passing through LEO

Using the area to mass ratio, an orbit lifetime analysis was run using the NASA DAS program. The output of the program is shown in the figure below. SIMPL complies with requirement 4.6-1 selecting the atmospheric reentry option by deorbiting within 5.4 years as a worst case scenario.

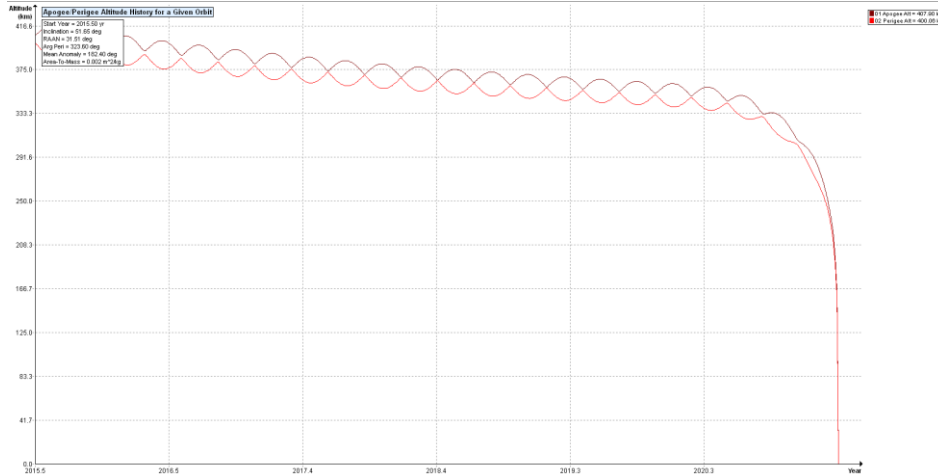


Table 4 DAS Orbit Degradation Chart

A more detailed analysis was performed by NASA in preparation for ISS safety reviews. When the dynamic exposure of SIMPL spacecraft surface area to the free stream velocity along the orbit was accounted for, the study concluded that a maximum worst-case lifetime was 325 days.

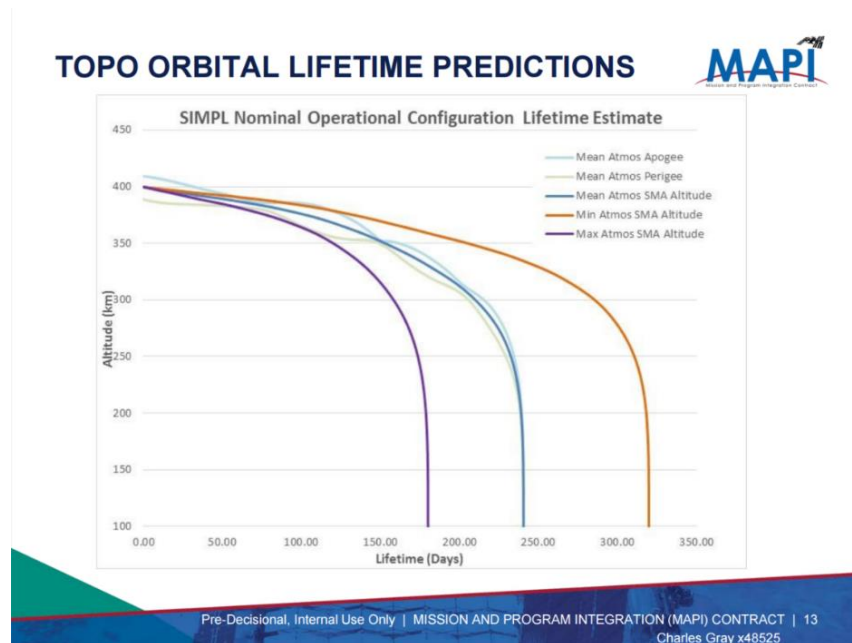


Table 5 NASA Orbit Degradation Chart

Requirements 4.6-2 and -3 are not applicable to SIMPL due to its orbit type.

Requirement 4.6-4 addresses the reliability of post mission disposal operations in Earth orbit. Since the SIMPL orbital lifetime requirement is met without any PAC operations, it is not relevant to reliability predictions.

9.0 ODAR SECTION 7: ASSESSMENT OF SPACECRAFT REENTRY HAZARDS

Requirement 4.7-1a states that for an uncontrolled reentry, the risk of human casualty from surviving debris shall not exceed 0.0001. (1:10,000) Component information was inputted into NASA DAS as accurately as possible with some values overestimated to provide margin and due to the limitations of the program. Program computations showed that the risk of human casualty from debris was 1:17300 thus satisfying the requirement 4.7-1.

Output						
Object	Compliance	Risk of Human	SubComponent	Demise	Total Debris	Kinetic
Name	Status	Casualty	Object	Altitude (km)	Casualty Area ...	Energy (J)
SIMPL	Compliant	1:17800			3.30	
			Solar Array	77.0	0.00	0
			Solar Converter	73.5	0.00	0
			Converter Boa...	73.1	0.00	0
			TT&C Antenna	77.0	0.00	0
			Housing 1	73.4	0.00	0

Table 6 DAS Results for Req. 4.7-1

Although the re-entry hazards analysis in DAS shows that SIMPL is compliant with the 1:10,000 requirement, there are few subcomponents where the demise altitude is at 0 Km. The following components are low mass and do not expect to pose a hazard or risk of human casualty.

Copper Pressure Seal – 14 grams with a debris casualty area of 3.3 m². Kinetic Energy: 0 J

The copper pressure seal is a thin, hollowed square of non-alloyed pure copper.

Gear – 2 grams with a debris casualty area of 2.23 m². Kinetic Energy: 0 J

The gears are cylindrical and utilized for propellant pumps internal to the spacecraft. They are constructed of silicon carbide.

Magnets – 5 grams with a 0 m² debris casualty area. Kinetic Energy: 0 J

Magnets are used in the stator portion of the reaction wheel motor. Each magnet is constructed from neodymium alloys.

Motor Frame –: 363 grams with a debris casualty area of 3.39 m², Kinetic Energy: 119 J

The motor frame is the stator portion of the reaction wheel motor and is constructed from steel.

A detailed investigation by NASA safety personnel indicated no hazard from re-entry with the items listed above. Additionally NOAA also has reviewed this document with no issues and granted Novawurks with a remote sensing license.

*****OUTPUT*****					
Item Number = 1					
name = SIMPL	name = Baseband board	name = Bearings	name = Gear 1	name = Connectors	name = Board 1
Demise Altitude = 77.997457	Demise Altitude = 73.701714	Demise Altitude = 73.574793	Demise Altitude = 68.066464	Demise Altitude = 69.083489	Demise Altitude = 73.544871
Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000
Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000

name = Solar Array	name = Lid	name = Motor Frame	name = Gear 2	name = Structural Frame Part #2	name = Board 2
Demise Altitude = 76.956371	Demise Altitude = 76.429847	Demise Altitude = 0.000000	Demise Altitude = 0.000000	Demise Altitude = 77.712441	Demise Altitude = 73.760605
Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 3.298234	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000
Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 105.802956	Impact Kinetic Energy = 0.365487	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000

name = Solar Converter	name = Batteries	name = Magnets	name = Housing	name = Solar Structure	name = Board 3
Demise Altitude = 73.532863	Demise Altitude = 71.691878	Demise Altitude = 0.000000	Demise Altitude = 69.433425	Demise Altitude = 72.710074	Demise Altitude = 73.890910
Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000
Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000

name = Converter Board	name = Avionics	name = Structural Frame Part #1	name = Screws Type 1	name = Solar Plate	name = Antenna
Demise Altitude = 73.141683	Demise Altitude = 76.279121	Demise Altitude = 70.907847	Demise Altitude = 69.393339	Demise Altitude = 75.880121	Demise Altitude = 73.968332
Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000
Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000

name = Screws	name = Seal	name = Nuts Type 1	name = SNAPS Plate	name = Board 4	
Demise Altitude = 75.673488	Demise Altitude = 0.000000	Demise Altitude = 69.902331	Demise Altitude = 75.880121	Demise Altitude = 73.845871	
Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	
Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.108927	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	

name = Valve	name = Power Transfer Assembly	name = Screws Type 2	name = Radio #1 Plate	name = Receiver Housing	
Demise Altitude = 75.603285	Demise Altitude = 63.401917	Demise Altitude = 69.925456	Demise Altitude = 74.826199	Demise Altitude = 76.782777	
Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	
Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	

name = Connector	name = Valves	name = Screws Type 3	name = Radio #2 Plate	name = Antenna Dielectric	
Demise Altitude = 75.565316	Demise Altitude = 68.077355	Demise Altitude = 70.315378	Demise Altitude = 75.880121	Demise Altitude = 76.691722	
Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	
Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	

name = Board G	name = Battery Mount	name = Pumps	name = Screws Type 4	name = Radio #2 Housing	===== End of Requirement 4.7-1
Demise Altitude = 73.183839	Demise Altitude = 75.139191	Demise Altitude = 69.726003	Demise Altitude = 70.648066	Demise Altitude = 74.148582	
Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	Debris Casualty Area = 0.000000	
Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	Impact Kinetic Energy = 0.000000	

name = SNAPS Camera					
Demise Altitude = 71.520878					
Debris Casualty Area = 0.000000					
Impact Kinetic Energy = 0.000000					

Table 6 DAS Inputs and Outputs for Req. 4.7-1

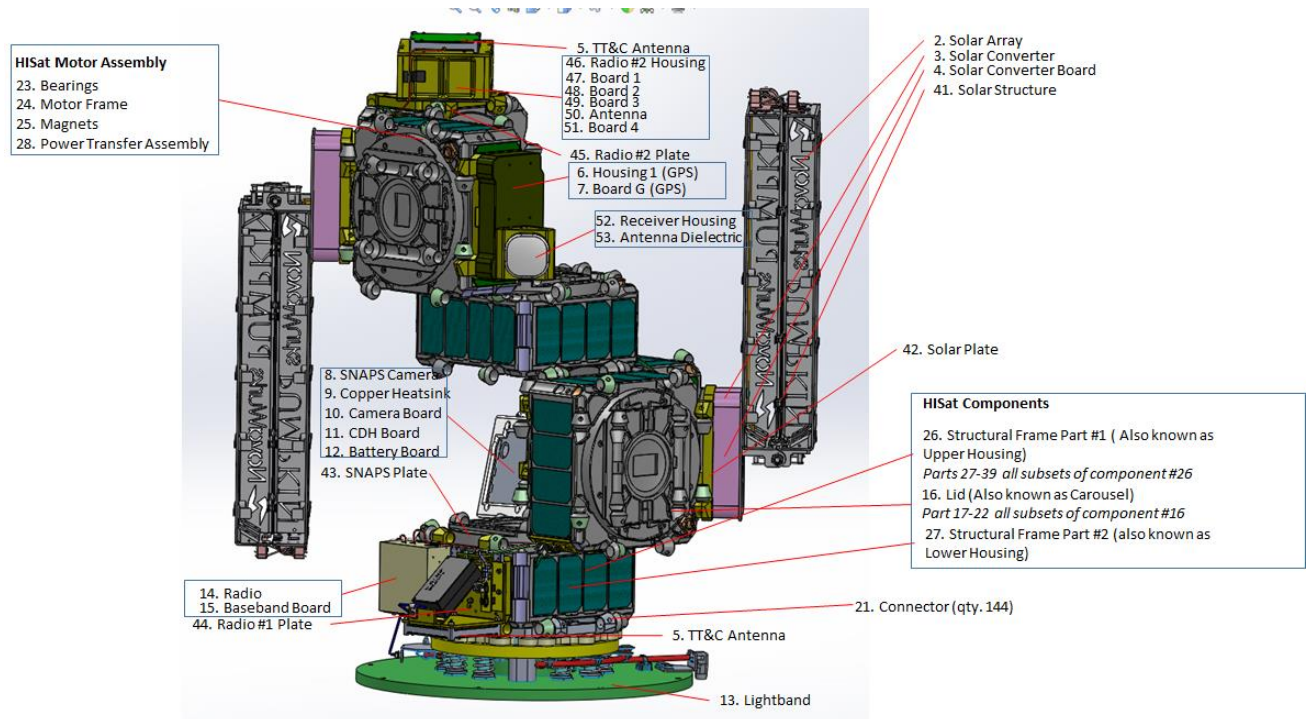


Figure 3 DAS Component Locations

10.0 ODAR SECTION 8: ASSESSMENT FOR TETHER MISSIONS

SIMPL does not have any Tether subsystems or Tethering capability, therefore this section is not applicable.

11.0 ACRONYMS AND ABBREVIATIONS

ADCS	Attitude Determination and Control subsystem
AFSPCMAN	Air Force Space Command Manual
COTS	Commercial Off The Shelf
DAS	Debris Assessment Software
Delta-V	delta velocity
EPS	Electric Power System
FMEA	Failure Modes Effects Analysis
LEO	Low Earth Orbit
LV	Launch Vehicle
MEOP	Maximum Expected Operating Pressure
NEI	Non-Explosive Initiator
NOP	Normal Operating Pressure
PACS	Package of Aggregated Cellular Satlets
S/C	Spacecraft
SIMPL	Satlet Initial Mission Proofs and Lessons
SGLS	Space-Ground link system
TBC	To Be Coordinated
TBD	To Be Determined
UDA	User Defined Adapter