

## **Exhibit No. 2**

### **Reradiation Analysis**

#### **Approach**

The approach taken for this analysis is to meet the NTIA requirements is as follows:

1. Determine the power density required to generate -140 dBm at a GPS input terminal (maximum power allowable) when connected to an isotropic antenna.
2. Determine the power density at 100 ft (~30 m) from our reradiating antenna systems. As each of the antennas will be located near the building wall, this calculation will meet the NTIA requirement showing compliance with the -140 dBm limit 100 feet from the building.
3. Determine the safety margin at 100 ft (~30m) referencing the -140 dBm requirement.

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#### **Maximum Power Allowable**

The maximum allowable power at a GPS receiver is -140 dBm when connected to an isotropic antenna.

$$-140 \text{ dB}_m = \underline{1 \times 10^{-17} \text{ W}}$$

To determine the maximum allowable power density ( $P_d$ ) at an antenna, it is known that:

$$P_d \times (\text{Effective Area}) = \text{Receiver Power}$$

Therefore,

$$\text{Maximum } P_d = \text{Max Allowable Receiver Power} / (\text{Antenna Effective Area})$$

Given that the Antenna Effective Area of an isotropic antenna is  $\lambda^2/4\pi$ ,

Then for **1574.42 MHz (L1)**:

$$\text{Effective Area} = (0.191\text{m})^2/4\pi = \underline{2.90 \times 10^{-3} \text{ m}^2}$$

And for **1277.60 MHz (L2)**:

$$\text{Effective Area} = (0.244\text{m})^2/4\pi = \underline{4.74 \times 10^{-3} \text{ m}^2}$$

Therefore, the maximum allowable power density for -140 dBm at a GPS receiver is:

At **1574.42 MHz (L1)**:

$$(P_d)_{\text{max}} = 1 \times 10^{-17} \text{ W} / 2.9 \times 10^{-3} \text{ m}^2 = \boxed{3.45 \times 10^{-15} \text{ W/m}^2}$$

At **1277.60 MHz (L2)**:

$$(P_d)_{\text{max}} = 1 \times 10^{-17} \text{ W} / 4.74 \times 10^{-3} \text{ m}^2 = \boxed{2.11 \times 10^{-15} \text{ W/m}^2}$$

## Exhibit No. 2 Reradiation Analysis

### AGS LRLAP Lab (Bldg NA) Transmit Power Calculations

The calculations apply to all antenna operating in building NA.

The maximum transmit antenna Gain (G) within 30° of horizontal is:

$$G = +0.9 \text{ dB}_{\text{ic}} = \underline{1.23} \text{ (numeric)}$$

<sup>1</sup>The Measured Power ( $T_x$ ) over 25 MHz at the antenna input is:

$$\text{For } \mathbf{1574.42 \text{ MHz (L1):}} \quad T_{L1} = -99.5 \text{ dB}_m = -129.5 \text{ dB}_w = \underline{1.122 \times 10^{-13} \text{ W}}$$

$$\text{And for } \mathbf{1277.60 \text{ MHz (L2):}} \quad T_{L2} = -103.5 \text{ dB}_m = -133.5 \text{ dB}_w = \underline{4.47 \times 10^{-14} \text{ W}}$$

The Power Density ( $P_d$ ) is:

$$P_d = T_x G / 4\pi r^2$$

Therefore, the Power Density at 100 ft (~30 m) and within 30° of horizontal is:

At **1574.42 MHz (L1):**

$$P_d = \frac{(1.122 \times 10^{-13} \text{ W})(1.23)}{4\pi(30)^2} = \boxed{1.22 \times 10^{-17} \text{ W/m}^2}$$

At **1277.60 MHz (L2):**

$$P_d = \frac{(4.47 \times 10^{-14} \text{ W})(1.23)}{4\pi(30)^2} = \boxed{4.86 \times 10^{-18} \text{ W/m}^2}$$

} **Nominal Power Density**

The **worst case** maximum transmit antenna Gain (G) at 90° of horizontal is:

$$G = +5.0 \text{ dB}_{\text{ic}} = \underline{3.16} \text{ (numeric)}$$

Therefore, the **worst case** Power Density at 100 ft (~30 m) and at 90° of horizontal is:

At **1574.42 MHz (L1):**

$$P_d = \frac{(1.122 \times 10^{-13} \text{ W})(3.16)}{4\pi(30)^2} = \boxed{3.14 \times 10^{-17} \text{ W/m}^2}$$

At **1277.60 MHz (L2):**

$$P_d = \frac{(4.47 \times 10^{-14} \text{ W})(3.16)}{4\pi(30)^2} = \boxed{1.25 \times 10^{-17} \text{ W/m}^2}$$

} **Worst Case Power Density**

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### **Reradiation Analysis**

**Note 1:** Power measurements were taken with a spectrum analyzer using a low noise pre-amplifier and are the maximum power across the 25 MHz Bandwidth. These measurements were taken at the coax terminal that connects to the transmit (or reradiating) antenna.

## Exhibit No. 2 Reradiation Analysis

### AGS LRLAP Portable (Dynamics Lab) Transmit Power Calculations

The maximum transmit antenna Gain (G) within 30° of horizontal is:

$$G = +0.9 \text{ dB}_{\text{ic}} = \underline{1.23} \text{ (numeric)}$$

<sup>1</sup>The Measured Power ( $T_x$ ) over 25 MHz at the antenna input is:

$$\text{For } \mathbf{1574.42 \text{ MHz (L1):}} \quad T_{L1} = -99.5 \text{ dB}_m = -129.5 \text{ dB}_w = \underline{1.122 \times 10^{-13} \text{ W}}$$

$$\text{And for } \mathbf{1277.60 \text{ MHz (L2):}} \quad T_{L2} = -101.5 \text{ dB}_m = -131.5 \text{ dB}_w = \underline{7.08 \times 10^{-14} \text{ W}}$$

The Power Density ( $P_d$ ) is:

$$P_d = T_x G / 4\pi r^2$$

Therefore, the Power Density at 100 ft (~30 m) and within 30° of horizontal is:

At **1574.42 MHz (L1):**

$$P_d = \frac{(1.122 \times 10^{-13} \text{ W})(1.23)}{4\pi(30)^2} = \boxed{1.22 \times 10^{-17} \text{ W/m}^2}$$

At **1277.60 MHz (L2):**

$$P_d = \frac{(7.08 \times 10^{-14} \text{ W})(1.23)}{4\pi(30)^2} = \boxed{7.70 \times 10^{-18} \text{ W/m}^2}$$

} **Nominal Power Density**

The **worst case** maximum transmit antenna Gain (G) at 90° of horizontal is:

$$G = +5.0 \text{ dB}_{\text{ic}} = \underline{3.16} \text{ (numeric)}$$

Therefore, the **worst case** Power Density at 100 ft (~30 m) and at 90° of horizontal is:

At **1574.42 MHz (L1):**

$$P_d = \frac{(1.122 \times 10^{-13} \text{ W})(3.16)}{4\pi(30)^2} = \boxed{3.14 \times 10^{-17} \text{ W/m}^2}$$

At **1277.60 MHz (L2):**

$$P_d = \frac{(7.08 \times 10^{-14} \text{ W})(3.16)}{4\pi(30)^2} = \boxed{1.98 \times 10^{-17} \text{ W/m}^2}$$

} **Worst Case Power Density**

## Exhibit No. 2 Reradiation Analysis

### Transmit Power Calculation Summary

From Page 1 of this exhibit, we identified that the Antenna Effective Area of an isotropic antenna is  $\lambda^2/4\pi$ ,

Then for **1574.42 MHz (L1)**:

$$\text{Effective Area} = (0.191\text{m})^2/4\pi = \underline{2.90 \times 10^{-3} \text{m}^2}$$

And for **1277.60 MHz (L2)**:

$$\text{Effective Area} = (0.244\text{m})^2/4\pi = \underline{4.74 \times 10^{-3} \text{m}^2}$$

Therefore, the **worst case** maximum equivalent isotropically radiated power at a distance of 100 feet (30 meters) from the building where the test is being conducted is as follows:

At **1574.42 MHz (L1)**:

$$(3.14 \times 10^{-17} \text{ W/m}^2)(2.90 \times 10^{-3} \text{m}^2) = 9.11 \times 10^{-20} \text{ W or } -190 \text{ dB}_w \Rightarrow \boxed{-160 \text{ dB}_m}$$

At **1277.60 MHz (L2)**:

$$(1.98 \times 10^{-17} \text{ W/m}^2)(4.74 \times 10^{-3} \text{m}^2) = 9.39 \times 10^{-20} \text{ W or } -190 \text{ dB}_w \Rightarrow \boxed{-160 \text{ dB}_m}$$

Both of which are no greater than the requirement of -140 dBm/24 MHz at a distance of 100 feet (30 meters) from the building where the test is being conducted.