

Exhibit 1

1. Introduction

By the instant application (“Application”), BAE Systems Information and Electronic Systems Integration Inc. (“BAE Systems”) requests that the Commission grant special temporary authority (“STA”) to permit BAE Systems to operate the facilities (the “Facilities”) specified in the instant application. STA is requested for a period of six (6) months.

2. Purpose of the Operation/Program of Research/Objectives/Contributions

The testing to be conducted under the requested experimental authority at BAE Systems’ Nashua and Hudson, NH campus locations is a critical part of the development, manufacture and delivery of military systems provided to the Armed Forces in support of Homeland Security as well as war efforts. Specifically, in this STA Request, BAE Systems requests the use of a GPS re-radiation system to permit testing of GPS navigation systems inside its manufacturing facility, an engineering prototype lab, and a product development lab.

This GPS re-radiation system will permit BAE Systems to verify the proper installation and operation of the internal navigation system for a military target location system product. Presently, without the system, BAE Systems engineers must leave the facility to test products under development. Often these prototypes are not robust enough to allow exposure to weather; this greatly limits the testing operations and severely impacts the product development schedule. Additionally, outside testing is greatly limited due to restrictions in lab equipment that may be operated in that environment. If BAE Systems were permitted to operate the system, its engineers and technicians could work more efficiently. A wired repeater system would not be a feasible alternative as the receiver antenna is an integral part of the system under test.

Various commercial manufacturing operations are using in-building repeaters to streamline navigation system diagnosis and repair times. BAE Systems seeks to realize similar benefits and quickly provide products to the United States military forces.

At this time, there is currently no government contract information specifically associated with the requested frequency request. If and when the facilities are to be used to implement the requirements of a specific government contract, BAE Systems will notify the Commission.

3. Compliance with NTIA GPS Re-Radiation Criteria – Section 8.3.28 of NTIA Regulations

The system BAE Systems seeks to operate will re-radiate the GPS L1 (1575.42 MHz) and L2 (1227.60 MHz) signals. A common system (dual band) consisting of one active antenna, one passive antenna, and one amplifier will be used for both frequencies at each site. BAE Systems hereby confirms that the proposed operations are in full compliance with Section 8.3.28 of the NTIA regulations governing re-radiation of GPS signals. See Attachment 1 for the calculations demonstrating compliance with the NTIA criteria.

4. **Mitigation of Interference**

The manufacturing site is located in the basement level of an existing facility and the other two sites are located inside metal buildings. These buildings attenuate the already low power of GPS signals to a level below the useable threshold of its navigation systems.

5. **Other Issues**

A. **Directional Antenna Data.** The following is provided with respect to the directional antennas to be used in this experiment.

Width of Beam at Half-Power Point	Orientation in Horizontal Plane	Orientation in Vertical Plane
114°	0° (horizontally flat)	-180° (antennas will face downward)

B. **Stop Buzzers.**

Listed below are the “Stop Buzzer” 24/7 points of contact for the application of GPS re-radiation devices. *See Manual of Regulations and Procedures for Federal Radio Frequency Management § 8.3.28(9) (rev. Sept. 2006)*

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Compliance with NTIA GPS Re-Radiation Criteria – Section 8.3.28 of NTIA Regulations Maximum Equivalent Isotropically Radiated Power

The system BAE Systems seeks to operate re-radiates the GPS L1 (1575.42 MHz) and L2 (1227.60 MHz) signals. A common system (dual band) consisting of one active antenna, one passive antenna, and one amplifier will be used for both frequencies at each site. Calculations are performed based on Section 8.3.28 of the NTIA regulations,¹ wherein item 6 states “the maximum equivalent isotropically radiated power must be such that the calculated emissions are no greater than -140dBm/24 MHz at a distance of 100 feet (30 meters) from the building where the test is being conducted.” Additionally, building attenuation has been ignored. This calculation shows that the re-radiated signal strength in compliance with NTIA requirements. The calculations are performed for each of the repeater sites in parts A, B, and C below.

$$(1) P_{sig} = P_{Rec} + G_{rant} + G_{ramp} - L_l + G_{rramp} + G_{rrant} - L_s + 2.148$$

Where: P_{sig} = Re-radiated signal strength 100ft outside the building (EIRP)

P_{Rec} = Received power from GPS Satellites (-130 dBm)

G_{rant} = Roof active antenna, (Antcom PN: 2.3G1215A-XRS-4) = 4.7dB (L1)
And 3.3 dB (L2)

G_{ramp} = Roof active antenna amplifier gain = 33dB (L1) and 35dB (L2)

L_l = Coaxial cable attenuation, roof antenna to re-radiating amplifier

= (L1) 9.1dB/100ft x cable length

= (L2) 8.6 dB/100ft x cable length

G_{rramp} = Re-radiating amplifier, (Minicircuits PN: ZX60-2522M) = 23.5dB

G_{rrant} = Re-radiating antenna gain (Antcom PN: 2.3G1215P-XRS-4) = 5.36dB

L_s = Free space loss (equation 2 below)

2.148 = conversion from ERP to EIRP

$$(2) L_s = 36.6 + 20\log_{10}((D/5280)*1575) \quad - \text{ free space loss for L1}$$

$$L_s = 36.6 + 20\log_{10}((D/5280)*1227) \quad - \text{ free space loss for L2}$$

Where: D = Distance (d) from antenna to outer wall in feet + 100ft

¹ See *Manual of Regulations and Procedures for Federal Radio Frequency Management* P 8.3.28(6) (Rev. Sept 2006).

Part A

Determination of the signal strength at 100 feet from Building 2 in the south Nashua, NH facility;

Determination of the free space loss-

$$D = 80\text{ft} + 100\text{ft}$$

$$= 180\text{ft}$$

Inserting the values for D into equation (2) yields:

$$\begin{aligned} L_s &= 36.6 + 20\log_{10}((180/5280)*1575) && \text{- for L1} \\ &= 70.18 \text{ dBm} \end{aligned}$$

and

$$\begin{aligned} L_s &= 36.6 + 20\log_{10}((180/5280)*1227) && \text{- for L2} \\ &= 68.01 \text{ dBm} \end{aligned}$$

Determination of the cable loss for Building 2–

$$\begin{aligned} L1 &= 80\text{ft} * (9.1/100) && \text{-for L1} \\ &= 5.46\text{dB} \end{aligned}$$

$$\begin{aligned} L1 &= 80\text{ft} * (8.6/100) && \text{-for L2} \\ &= 5.16\text{dB} \end{aligned}$$

Inserting these values into equation 1 yields

$$\begin{aligned} P_{\text{sig (EIRP)}} &= -130 + 4.7 + 33 - 5.46 + 23.5 + 4.7 - 70.18 + 2.147 && \text{- for L1} \\ &= -137.59 \text{ dBm} && \text{- L1 signal strength at 100ft excluding building attenuation} \\ &\text{This value does not meet the requirements, so a 3dB attenuator will be included in} \\ &\text{this system to reduce the signal strength to below the required -140dBm.} \\ &= -137.59 - 3 \\ &= -140.59 \text{ dBm} \end{aligned}$$

And

$$\begin{aligned} P_{\text{sig (EIRP)}} &= -130 + 3.3 + 33 - 5.16 + 23.5 + 3.3 - 68.01 + 2.147 && \text{- for L2} \\ &= -137.92 \text{ dBm} && \text{- L2 signal strength at 100ft excluding building attenuation} \\ &\text{This value does not meet the requirements, applying the 3 dB of attenuation added} \\ &\text{to the system for L1 above yields:} \\ &= -137.92 - 3 \\ &= -140.92 \text{ dBm} \end{aligned}$$

Part B

Determination of signal strength at 100 feet from Building 6 at the south Nashua facility:

Determination of the free space loss-

$$D = 120 \text{ ft} + 100\text{ft}$$

$$= 220 \text{ feet}$$

Inserting the values for D into equation (2) yields:

$$\begin{aligned} L_s &= 36.6 + 20\text{Log}_{10}((220/5280)*1575) && \text{- for L1} \\ &= 72.94 \text{ dBm} \end{aligned}$$

and

$$\begin{aligned} L_s &= 36.6 + 20\text{Log}_{10}((220/5280)*1227) && \text{- for L2} \\ &= 70.77 \text{ dBm} \end{aligned}$$

Determination of the cable loss for Building 6–

$$L_l = 120\text{ft} * (9.1/100) \quad \text{-for L1}$$

$$= 10.92\text{dB}$$

$$L_l = 120\text{ft} * (8.6/100) \quad \text{-for L2}$$

$$= 10.32\text{dB}$$

Inserting these values into equation 1 yields

$$\begin{aligned} P_{\text{sig (EIRP)}} &= -130 + 4.7 + 33 - 10.92 + 23.5 + 4.7 - 72.94 + 2.147 && \text{- for L1} \\ &= -145.81 \text{ dBm} - \text{L1 signal strength at 100ft excluding building attenuation} \end{aligned}$$

And equation 1 computed for L2:

$$\begin{aligned} P_{\text{sig (EIRP)}} &= -130 + 3.3 + 33 - 10.32 + 23.5 + 3.3 - 70.77 + 2.147 && \text{- for L2} \\ &= -145.84 \text{ dBm} - \text{L2 signal strength at 100ft excluding building attenuation} \end{aligned}$$

Part C

Determination of signal strength at 100 feet from Building 2 at the Hudson, NH (Pope Technical Park) facility:

Determination of the free space loss-

$$D = 80 \text{ ft} + 100\text{ft}$$

$$= 180 \text{ feet}$$

Inserting the values for D into equation (2) yields:

$$L_s = 36.6 + 20\text{Log}_{10}((180/5280)*1575) \quad \text{- for L1}$$

$$= 71.20 \text{ dBm}$$

and

$$L_s = 36.6 + 20\text{Log}_{10}((180/5280)*1227) \quad \text{- for L2}$$

$$= 69.03 \text{ dBm}$$

Determination of the cable loss for Building 6–

$$L1 = 80\text{ft} * (9.1/100) \quad \text{-for L1}$$

$$= 7.28\text{dB}$$

$$L1 = 120\text{ft} * (8.6/100) \quad \text{-for L2}$$

$$= 6.88\text{dB}$$

Inserting these values into equation 1 yields

$$P_{\text{sig (EIRP)}} = -130 + 4.7 + 33 - 10.92 + 23.5 + 4.7 - 72.94 + 2.147 \quad \text{- for L1}$$
$$= -145.81 \text{ dBm} - \text{L1 signal strength at 100ft excluding building attenuation}$$

And equation 1 computed for L2:

$$P_{\text{sig (EIRP)}} = -130 + 3.3 + 33 - 10.32 + 23.5 + 3.3 - 70.77 + 2.147 \quad \text{- for L2}$$
$$= -145.84 \text{ dBm} - \text{L2 signal strength at 100ft excluding building attenuation}$$