## **OET 65 Radiation Hazard Analysis**

## **Definition of terms**

The terms are used in the formulas here are defined as follows:

Ssurface = maximum power density at the antenna surface Snf = maximum near-field power density St = power density in the transition region Sff = power density (on axis) Rnf = extent of near-field Rff = distance to the beginning of the far-field R = distance to point of interest P = power fed to the antenna A = physical area of the aperture antenna G = power gain in the direction of interest relative to an isotropic radiator D = maximum dimension of antenna (diameter if circular) I = wavelength h = aperture efficiency, typically 0.65 to 0.75

## **Formulas**

**Antenna Surface**. The maximum power density directly in front of an antenna (e.g., at the antenna surface) can be approximated by the following equation:

$$f_{S.surface}(P,A) \coloneqq \frac{4 \cdot P}{A}$$

**Near-Field Region**. In the near-field or Fresnel region, of the main beam, the power density can reach a maximum before it begins to decrease with distance. The extent of the near-field can be described by the following equation (**D** and I in same units):

$$f_{R.nf}(D,\lambda) \coloneqq \frac{D^2}{4 \cdot \lambda}$$

The magnitude of the on-axis (main beam) power density varies according to location in the near-field. However, the maximum value of the near-field, on-axis, power density can be expressed by the following equation:

$$f_{S.nf}(P,D,\eta) \coloneqq rac{16 \cdot \eta \cdot P}{\pi \cdot D^2}$$

Aperture efficiency can be estimated, or a reasonable approximation for circular apertures can be obtained from the ratio of the effective aperture area to the physical area as follows:

$$f_{\eta}(G, D, \lambda) \coloneqq \frac{\left(\frac{G \cdot \lambda^2}{4 \cdot \pi}\right)}{\left(\frac{\pi \cdot D^2}{4}\right)}$$

If the antenna gain is not known, it can be calculated from the following equation using the actual or estimated value for aperture efficiency:

$$f_G(A,\lambda,\eta) \coloneqq rac{4 \cdot \pi \cdot \eta \cdot A}{\lambda^2}$$

**Transition Region.** Power density in the transition region decreases inversely with distance from the antenna, while power density in the far-field (Fraunhofer region) of the antenna decreases inversely with the *square* of the distance. For purposes of evaluating RF exposure, the distance to the beginning of the far-field region (farthest extent of the transition region) can be approximated by the following equation:

$$f_{R.ff}(D,\lambda) \coloneqq rac{0.6 \cdot D^2}{\lambda}$$

The transition region will then be the region extending from **R** nf to **R** ff. If the location of interest falls within this transition region, the on-axis power density can be determined from the following equation:

$$f_{S.t}\left(S_{nf},R_{nf},R
ight)\coloneqqrac{S_{nf}ullet R_{nf}}{R}$$

**Far-Field Region.** The power density in the far-field or Fraunhofer region of the antenna pattern decreases inversely as the square of the distance. The power density in the far-field region of the radiation pattern can be estimated by the general equation discussed earlier:

$$f_{S.ff}(P,G,R) \coloneqq rac{P \cdot G}{4 \cdot \pi \cdot R^2}$$

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## <u>Results</u>

The relevant values will be calculated for a 12 inch antenna operating at 29.5 GHz using a 20 watt power amplifier.

$c \coloneqq 299792458 \cdot \frac{m}{s}$	$mW \coloneqq 1 \cdot 10^{-3} \cdot W$	
$R_t := 2.285 \cdot m$	$R_f \coloneqq 5.485 \cdot m$	
D:=12• <i>in</i>	$D = 0.305 \ m$	
$F \coloneqq 29.5 \cdot GHz$	$F = (2.95 \cdot 10^{10}) \frac{1}{s}$	
$P_a \coloneqq 20 \cdot W$	$P_a = 20 W$	
$L_{fs} := 10^{rac{.0}{10}}$	$L_{fs}\!=\!1$	
$P \coloneqq \frac{P_a}{L_{fs}}$	P = 20 W	
$\eta \coloneqq 0.57$	$\eta \!=\! 0.57$	
$\lambda := \frac{c}{F}$	$\lambda {=} 0.01 \; m$	
$A \coloneqq \pi \cdot \frac{D^2}{4}$	$A\!=\!0.073  m^2$	
$G \coloneqq f_G(A, \lambda, \eta)$	$G \!=\! 5.061 \cdot 10^3$	$10 \cdot \log(G) = 37.042$
$S_{surface} \coloneqq f_{S.surface}(P, A)$	$S_{surface}\!=\!109.64\;rac{mW}{cm^2}$	
$R_{nf} \! \coloneqq \! f_{R.nf}(D,\lambda)$	$R_{nf} = 2.285 \ m$	$10 \cdot \log \left( G \cdot \frac{P}{W} \right) = 50.052$
$S_{nf} \!\!\coloneqq\! f_{S.nf}(P,D,\eta)$	$S_{nf}\!=\!62.495\;rac{mW}{cm^2}$	
$R_{ff} \! \coloneqq \! f_{R.ff}(D,\lambda)$	$R_{f\!f}\!=\!5.485\;m$	$R_{ff} \!=\! 17.996 \; ft$
$S_t \! \coloneqq \! f_{S.t} \left( S_{nf}, R_{nf}, R_t \right)$	$S_t \!=\! 62.507 \; rac{mW}{cm^2}$	$S_{nf} \cdot R_{nf} = 142.829  \boldsymbol{m} \cdot \frac{\boldsymbol{m}W}{\boldsymbol{cm}^2}$

$$S_{ff} := f_{S.ff} \langle P, G, R_f \rangle \qquad S_{ff} = 26.772 \frac{mW}{cm^2}$$
$$R_{5mW} := \sqrt{\frac{(P \cdot G)}{4 \cdot \pi \cdot 5 \cdot \frac{mW}{cm^2}}} \qquad R_{5mW} = 12.692 m$$

$$R_{5mW} \!=\! 41.64 \; ft$$