

## OET 65 Definition of Terms and Formulas:

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### OET 65 Radiation Hazard Analysis

#### Definition of terms

The terms are used in the formulas here are defined as follows:

$S_{\text{surface}}$  = maximum power density at the antenna surface

$S_{\text{nf}}$  = maximum near-field power density

$S_{\text{t}}$  = power density in the transition region

$S_{\text{ff}}$  = power density (on axis)

$R_{\text{nf}}$  = extent of near-field

$R_{\text{ff}}$  = distance to the beginning of the far-field

$R$  = distance to point of interest

$P$  = power fed to the antenna

$A$  = physical area of the aperture antenna

$G$  = power gain in the direction of interest relative to an isotropic radiator

$D$  = maximum dimension of antenna (diameter if circular)

$\lambda$  = wavelength

$\eta$  = aperture efficiency, typically 0.65 to 0.75

#### Formulas

**Antenna Surface.** The maximum power density directly in front of an antenna (e.g., at the antenna surface) can be approximated by the following equation:

$$f_{S.\text{surface}}(P, A) := \frac{4 \cdot P}{A}$$

**Near-Field Region.** In the near-field or Fresnel region, of the main beam, the power density can reach a maximum before it begins to decrease with distance. The extent of the near-field can be described by the following equation (**D** and  $\lambda$  in same units):

$$f_{R.\text{nf}}(D, \lambda) := \frac{D^2}{4 \cdot \lambda}$$

The magnitude of the on-axis (main beam) power density varies according to location in the near-field. However, the maximum value of the near-field, on-axis, power density can be expressed by the following equation:

$$f_{S.\text{nf}}(P, D, \eta) := \frac{16 \cdot \eta \cdot P}{\pi \cdot D^2}$$

Aperture efficiency can be estimated, or a reasonable approximation for circular apertures can be obtained from the ratio of the effective aperture area to the physical area as follows:

$$f_{\eta}(G, D, \lambda) := \frac{\left(\frac{G \cdot \lambda^2}{4 \cdot \pi}\right)}{\left(\frac{\pi \cdot D^2}{4}\right)}$$

If the antenna gain is not known, it can be calculated from the following equation using the actual or estimated value for aperture efficiency:

$$f_G(A, \lambda, \eta) := \frac{4 \cdot \pi \cdot \eta \cdot A}{\lambda^2}$$

**Transition Region.** Power density in the transition region decreases inversely with distance from the antenna, while power density in the far-field (Fraunhofer region) of the antenna decreases inversely with the **square** of the distance. For purposes of evaluating RF exposure, the distance to the beginning of the far-field region (farthest extent of the transition region) can be approximated by the following equation:

$$f_{R,ff}(D, \lambda) := \frac{0.6 \cdot D^2}{\lambda}$$

The transition region will then be the region extending from **R<sub>nf</sub>** to **R<sub>ff</sub>**. If the location of interest falls within this transition region, the on-axis power density can be determined from the following equation:

$$f_{S,t}(S_{nf}, R_{nf}, R) := \frac{S_{nf} \cdot R_{nf}}{R}$$

**Far-Field Region.** The power density in the far-field or Fraunhofer region of the antenna pattern decreases inversely as the square of the distance. The power density in the far-field region of the radiation pattern can be estimated by the general equation discussed earlier:

$$f_{S,ff}(P, G, R) := \frac{P \cdot G}{4 \cdot \pi \cdot R^2}$$



## Table 1 - Mantarray M40:



### Table 1: Radiation from Mantarray M40 Antenna

#### Input Parameters

Antenna Aperture Major Axis:	$D_{maj} := 31 \cdot in$	$D_{maj} = 78.74 \cdot cm$
Antenna Aperture Minor Axis:	$D_{min} := 6.2 \cdot in$	$D_{min} = 15.748 \cdot cm$
Frequency of Operation:	$F := 30 \cdot GHz$	
Max Power into Antenna:	$P := 5.38 \cdot W$	
Aperture Efficiency:	$\eta := 1$	
Aperture Corner Horn Area:	$ca := 3.6 \cdot in^2$	

#### Calculated Values

Wavelength:	$\lambda := \frac{c}{F}$	$\lambda = 0.01 \cdot m$	
Area of Aperture:	$A_{apr} := (D_{maj} \cdot D_{min}) - ca$	$A_{apr} = 0.122 \cdot m^2$	$A_{apr} = 188.6 \cdot in^2$
Effective Aperture Diameter:	$D_{eff} := \sqrt{\frac{4 \cdot A_{apr}}{\pi}}$	$D_{eff} = 39.36 \cdot cm$	
Antenna Gain:	$G := \frac{\eta \cdot 4 \cdot \pi \cdot A_{apr}}{\lambda^2}$	$G = 1.531 \times 10^4$	$10 \cdot \log(G) = 41.85 \text{ dBi}$
Length of Near Field:	$R_{nf} := \frac{D_{maj}^2}{4 \cdot \lambda}$	$R_{nf} = 15.511 \cdot m$	
Beginning of Far Field:	$R_{ff} := 0.6 \cdot \frac{D_{maj}^2}{\lambda}$	$R_{ff} = 37.226 \cdot m$	

#### Power Density Calculations

Far Field:	100% Duty Cycle	Idle Mode	Normal Mode	High Capacity Mode
$S_{ff} := \frac{P \cdot G}{4 \cdot \pi \cdot R_{ff}^2}$	$S_{ff} = 0.473 \cdot \frac{mW}{cm^2}$	$S_{ff} \cdot 0.06\% = 0.028 \cdot \frac{mW}{cm^2}$	$S_{ff} \cdot 10\% = 0.047 \cdot \frac{mW}{cm^2}$	$S_{ff} \cdot 30\% = 0.142 \cdot \frac{mW}{cm^2}$
Near Field:	100% Duty Cycle	Idle Mode	Normal Mode	High Capacity Mode
$S_{nf} := \frac{16 \cdot \eta \cdot P}{\pi \cdot D_{maj}^2}$	$S_{nf} = 4.419 \cdot \frac{mW}{cm^2}$	$S_{nf} \cdot 0.06\% = 0.265 \cdot \frac{mW}{cm^2}$	$S_{nf} \cdot 10\% = 0.442 \cdot \frac{mW}{cm^2}$	$S_{nf} \cdot 30\% = 1.326 \cdot \frac{mW}{cm^2}$

Transition Region: Power density is less than the maximum near field region power density and greater than the minimum far field region power density.

Aperture:	100% Duty Cycle	Idle Mode	Normal Mode	High Capacity Mode
$S_{apr} := \frac{4 \cdot P}{A_{apr}}$	$S_{apr} = 17.686 \cdot \frac{mW}{cm^2}$	$S_{apr} \cdot 0.6\% = 0.106 \cdot \frac{mW}{cm^2}$	$S_{apr} \cdot 10\% = 1.769 \cdot \frac{mW}{cm^2}$	$S_{apr} \cdot 30\% = 5.306 \cdot \frac{mW}{cm^2}$



## Table 2 - Mantarray M32:

Table 2: Radiation from Mantarray M32 Antenna

### Input Parameters

Antenna Aperture Major Axis:	$D_{maj} := 24.8 \cdot in$	$D_{maj} = 62.992 \cdot cm$
Antenna Aperture Minor Axis:	$D_{min} := 6.2 \cdot in$	$D_{min} = 15.748 \cdot cm$
Frequency of Operation:	$F := 30 \cdot GHz$	
Max Power into Antenna:	$P := 5.38 \cdot W$	
Aperture Efficiency:	$\eta := 1$	

### Calculated Values

Wavelength:	$\lambda := \frac{c}{F}$	$\lambda = 0.01 \cdot m$	
Area of Reflector:	$A_{apr} := D_{maj} \cdot D_{min}$	$A_{apr} = 0.099 \cdot m^2$	$A_{apr} = 153.76 \cdot in^2$
Effective Aperture Diameter:	$D_{apr} := \sqrt{\frac{4 \cdot A_{apr}}{\pi}}$	$D_{apr} = 31.496 \cdot cm$	
Antenna Gain:	$G := \frac{\eta \cdot 4 \cdot \pi \cdot A_{apr}}{\lambda^2}$	$G = 1.248 \times 10^4$	$10 \cdot \log(G) = 40.963 \text{ dBi}$
Length of Near Field:	$R_{nf} := \frac{D_{maj}^2}{4 \cdot \lambda}$	$R_{nf} = 9.927 \cdot m$	
Beginning of Far Field:	$R_{ff} := 0.6 \cdot \frac{D_{maj}^2}{\lambda}$	$R_{ff} = 23.824 \cdot m$	

### Power Density Calculations

Far Field:	100% Duty Cycle	Idle Mode	Normal Mode	High Capacity Mode
$S_{ff} := \frac{P \cdot G}{4 \cdot \pi \cdot R_{ff}^2}$	$S_{ff} = 0.942 \cdot \frac{mW}{cm^2}$	$S_{ff} \cdot 0.06\% = 0.056 \cdot \frac{mW}{cm^2}$	$S_{ff} \cdot 10\% = 0.094 \cdot \frac{mW}{cm^2}$	$S_{ff} \cdot 30\% = 0.282 \cdot \frac{mW}{cm^2}$
Near Field:	100% Duty Cycle	Idle Mode	Normal Mode	High Capacity Mode
$S_{nf} := \frac{16 \cdot \eta \cdot P}{\pi \cdot D_{maj}^2}$	$S_{nf} = 6.905 \cdot \frac{mW}{cm^2}$	$S_{nf} \cdot 0.06\% = 0.414 \cdot \frac{mW}{cm^2}$	$S_{nf} \cdot 10\% = 0.691 \cdot \frac{mW}{cm^2}$	$S_{nf} \cdot 30\% = 2.072 \cdot \frac{mW}{cm^2}$

Transition Region: Power density is less than the maximum near field region power density and greater than the minimum far field region power density.

Main Reflector:	100% Duty Cycle	Idle Mode	Normal Mode	High Capacity Mode
$S_{ref} := \frac{4 \cdot P}{A_{apr}}$	$S_{apr} = 17.686 \cdot \frac{mW}{cm^2}$	$S_{apr} \cdot 0.6\% = 0.106 \cdot \frac{mW}{cm^2}$	$S_{apr} \cdot 10\% = 1.769 \cdot \frac{mW}{cm^2}$	$S_{apr} \cdot 30\% = 5.306 \cdot \frac{mW}{cm^2}$



The antennas will be operated in a controlled environment with access to the region near the radiator limited - typically vehicle roof mounted or aircraft tail or fuselage mounted. Antenna will be turned off for maintenance as necessary to protect workers or general population.