# UltiSat, Inc. Six-Month Experimental Special Temporary Authorization ("STA") 

## Technical Appendix

I. BB45 Ka-band Radiation Hazard Analysis
II. BB45 X-band Radiation Hazard Analysis
III. BB45 EIRP Spectral Density Patterns
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## I. Radiation Hazard Analysis

## BB45 (Ka-band)

This analysis predicts the radiation levels around a proposed earth station complex, comprised of a single panel type antenna. This report is developed in accordance with the prediction methods contained in OET Bulletin No. 65, Evaluating Compliance with FCC Guidelines for Human Exposure to Radio Frequency Electromagnetic Fields, Edition 97-01, pp 26-30. The maximum level of non-ionizing radiation to which employees may be exposed is limited to a power density level of 5 milliwatts per square centimeter ( $5 \mathrm{~mW} / \mathrm{cm}^{2}$ ) averaged over any 6 minute period in a controlled environment and the maximum level of non-ionizing radiation to which the general public is exposed is limited to a power density level of 1 milliwatt per square centimeter ( 1 $\mathrm{mW} / \mathrm{cm}^{2}$ ) averaged over any 30 minute period in a uncontrolled environment. Note that the worse-case radiation hazards exist along the beam axis. Under normal circumstances, it is highly unlikely that the antenna axis will be aligned with any occupied area since that would represent a blockage to the desired signals, thus rendering the link unusable.

Earth Station Technical Parameter Table

| Antenna Aperture Size | 0.45 m |
| :--- | :--- |
| Antenna Effective Diameter | 0.45 m |
| Antenna Surface Area | 0.159 sq. meters |
| Antenna Isotropic Gain | 41.0 dBi |
| Number of Identical Adjacent Antennas 1 |  |
| Nominal Antenna Efficiency ( $\varepsilon$ ) | $65 \%$ |
| Nominal Frequency | 29.5 GHz |
| Nominal Wavelength ( $\lambda$ ) | 0.0102 meters |
| Maximum Transmit Power / Carrier | 12.5 Watts |
| Number of Carriers | 1 |
| Total Transmit Power | 25.0 Watts |
| W/G Loss from Transmitter to Feed | 1.0 dB |
| Total Feed Input Power | 9.93 Watts |
| Radome Losses | 1.0 dB |
| Effective RF Power at radome | 7.89 Watts |
| Near Field Limit | $\mathrm{R}_{\mathrm{nf}}=\mathrm{D}^{2} / 4 \lambda=4.98$ meters |
| Far Field Limit | $\mathrm{R}_{\mathrm{ff}}=0.6 \mathrm{D}^{2} / \lambda=11.95$ meters |
| Transition Region | $\mathrm{R}_{\mathrm{nf}} \mathrm{to} \mathrm{R}_{\mathrm{ff}}=4.98$ meters to 11.95 meters |

In the following sections, the power density in the above regions, as well as other critically important areas will be calculated and evaluated. The calculations are done in the order discussed in OET Bulletin 65.

### 1.0 At the Antenna Surface

The power density at the reflector surface can be calculated from the expression:
$\mathrm{PD}_{\mathrm{as}}=4 \mathrm{P} / \mathrm{A}=\mathbf{2 4 . 9 7} \mathrm{mW} / \mathrm{cm}^{2}(1)$
Where: $\mathrm{P}=$ total power at feed, milliwatts
$A=$ Total area of reflector, sq. cm

In the normal range of transmit powers for satellite antennas, the power densities at or around the reflector surface is expected to exceed safe levels. This area will not be accessible to the general public.

This antenna will incorporate a radome which has 1.0 dB of loss. The worst case power density at the surface of the radome is shown below:

$$
\begin{equation*}
\mathrm{PD}_{\text {radome }}=4 \mathrm{P}_{\mathrm{rad}} / \mathrm{A}=\mathbf{1 9 . 8} \mathrm{mW} / \mathrm{cm}^{2} \tag{2}
\end{equation*}
$$

Where: Prad = total power at feed less radome losses, milliwatts
$A=$ Total area of reflector, sq. cm (this would represent worst case)

Operators and technicians should receive training specifying this area as a high exposure area. Procedures must be established that will assure that all transmitters are rerouted or turned off before access by maintenance personnel to this area is possible.

### 2.0 On-Axis Near Field Region

The geometrical limits of the radiated power in the near field approximate a cylindrical volume with a diameter equal to that of the antenna. In the near field, the power density is neither uniform nor does its value vary uniformly with distance from the antenna. For the purpose of considering radiation hazard it is assumed that the on-axis flux density is at its maximum value throughout the length of this region. The length of this region, i.e., the distance from the antenna to the end of the near field, is computed as Rnf above.

The maximum power density in the near field is given by:

$$
\begin{aligned}
\mathrm{PD}_{\mathrm{nf}}=(16 \varepsilon \mathrm{P}) /\left(\pi \mathrm{D}^{2}\right)= & \mathbf{1 2 . 9 5} \mathrm{mW} / \mathrm{cm}^{2}(3) \\
& \text { from } 0 \text { to } 4.9 \text { meters }
\end{aligned}
$$

## Evaluation

Uncontrolled Environment: Does Not Meet Controlled Limits
Controlled Environment: Does Not Meet Uncontrolled Limits

### 3.0 On-Axis Transition Region

The transition region is located between the near and far field regions. As stated in Bulletin 65, the power density begins to vary inversely with distance in the transition region. The maximum power density in the transition region will not exceed that calculated for the near field region, and the transition region begins at that value. The maximum value for a given distance within the transition region may be computed for the point of interest according to:

```
PD tr = (PD nf )
where: }\quad\mp@subsup{PDDD }{nf}{}=\mathrm{ near field power density
    R
    R = distance to point of interest
PD
For: }\quad4.98<\textrm{R}<11.95\mathrm{ meters
```

We use Eq (4) to determine the safe on-axis distances required for the two occupancy conditions:

## Evaluation

$$
\begin{array}{ll}
\text { Uncontrolled Environment Safe Operating Distance, (meters), } \mathrm{R}_{\text {safeu: }} & 64.5 \\
\text { Controlled Environment Safe Operating Distance, (meters), } \mathrm{R}_{\text {safec: }} & 12.9
\end{array}
$$

### 4.0 On-Axis Far-Field Region

The on- axis power density in the far field region $\left(\mathrm{PD}_{\mathrm{ff}}\right)$ varies inversely with the square of the distance as follows:

```
PD
where: P = total power at feed
    G = Numeric Antenna gain in the direction of interest relative to isotropic radiator
    R= distance to the point of interest
For: R > R Rff = 9.23 meters
    PD
```

We use Eq (5) to determine the safe on-axis distances required for the two occupancy conditions:
Evaluation
Uncontrolled Environment Safe Operating Distance,(meters), $\mathrm{R}_{\text {safeu }}$ : $\quad$ See Section 3 Controlled Environment Safe Operating Distance,(meters), $\mathrm{R}_{\text {safec }}: \quad$ See Section 3

### 5.0 Off-Axis Levels at the Far Field Limit and Beyond

In the far field region, the power is distributed in a pattern of maxima and minima (sidelobes) as a function of the off-axis angle between the antenna center line and the point of interest. Off-axis power density in the far field can be estimated using the antenna radiation patterns prescribed for the antenna in use. Usually this will correspond to the antenna gain pattern envelope defined by the FCC or the ITU, which takes the form of:

$$
\begin{aligned}
& \mathrm{G}_{\text {off }}=32-25 \log (\Theta) \\
& \text { for } \Theta \text { from } 1 \text { to } 48 \text { degrees; }-10 \mathrm{dBi} \text { from } 48 \text { to } 180 \text { degrees } \\
& \text { (Applicable for commonly used satellite transmit antennas) }
\end{aligned}
$$

Considering that satellite antenna beams are aimed skyward, power density in the far field will usually not be a problem except at low look angles. In these cases, the off axis gain reduction may be used to further reduce the power density levels.

For example: At two (2) degrees off axis At the far-field limit, we can calculate the power density as:
$\mathrm{G}_{\text {off }}=32-25 \log (2)=32-7.52 \mathrm{dBi}=280.2$ numeric

$$
\mathrm{PD}_{2 \text { deg off-axis }}=\mathrm{PD}_{\mathrm{ffX}} 280.2 / \mathrm{G}=\mathbf{0 . 1 3} \mathrm{mW} / \mathrm{cm}^{2}(6)
$$

### 6.0 Off-Axis power density in the Near Field and Transitional Regions

According to Bulletin 65 , off-axis calculations in the near field may be performed as follows: assuming that the point of interest is at least one antenna diameter removed from the center of the main beam, the power density at that point is at least a factor of $100(20 \mathrm{~dB})$ less than the value calculated for the equivalent on-axis power density in the main beam. Therefore, for regions at least D meters away from the center line of the dish, whether behind, below, or in front under of the antenna's main beam, the power density exposure is at least 20 dB below the main beam level as follows:

$$
\mathrm{PD}_{\mathrm{nf}(\mathrm{fff}-\mathrm{xxis})}=\mathrm{PD}_{\mathrm{nf}} / 100=\mathbf{0 . 2 6 0} \mathrm{mW} / \mathrm{cm}^{2} \text { at } \mathrm{D} \text { off axis }(7)
$$

See Section 7 for the calculation of the distance vs. elevation angle required to achieve this rule for a given object height.

### 7.0 Evaluation of Safe Occupancy Area in Front of Antenna

The distance ( S ) from a vertical axis passing through the dish center to a safe off axis location in front of the antenna can be determined based on the dish diameter rule (Item 6.0). Assuming a flat terrain in front of the antenna, the relationship is:
$\mathrm{S}=(\mathrm{D} / \sin \alpha)+(2 \mathrm{~h}-\mathrm{D}-2) /(2 \tan \alpha)(8)$
Where: $\alpha=$ minimum elevation angle of antenna
$\mathrm{D}=$ dish diameter in meters
$\mathrm{h}=$ maximum height of object to be cleared, meters
For distances equal or greater than determined by equation (8), the radiation hazard will be below safe levels for all but the most powerful stations (>4 kilowatts RF at the feed).

For $\quad$| $\mathrm{D}=$ |  |
| :--- | :--- |
| $\mathrm{h}=$ | 0.569 meters |
| 2.0 meters, delta between antenna and object $>1 \mathrm{~m}$ |  |

Then:

| $\alpha$ | $S$ |
| :--- | :--- |
| 10 | 1.7 meters |
| 15 | 1.1 meters |
| 20 | 0.9 meters |
| 25 | 0.7 meters |
| 30 | 0.6 meters |

### 8.0 Summary of Results

The earth station site will be protected from uncontrolled access by virtue of the fact that it will be mounted on the top of an air vehicle. There will also be proper emission warning signs placed and all operating personnel will be aware of the human exposure levels at and around the earth station. The applicant agrees to abide by the conditions specified in Condition 18 provided below:
(18) - UltiSat Inc shall take all reasonable and customary measures to ensure that the MET does not create potential for harmful non-ionizing radiation to persons who may be in the vicinty of the MET when it is in operation. At a minimum, permanent warning label(s) shall be affixed to the MET warning of the radiation hazard and including a diagram showing the regions around the MET where the radiation levels could exceed $1.0 \mathrm{~mW} / \mathrm{cm} 2$. The operator of the MET shall be responsible for assuring that individuals do not stray into the region around the MET where there is a potential for exceeding the maximum permissible exposure limits required by Section 1.1310 of the Commission's rules 47 C.F.R § 1.1310. This shall be accomplished by means of signs, caution tape, verbal warnings, placement of the MET so as to minimize access to the hazardous region and/or any other appropriate means

The table below summarizes all of the above calculations.

| Parameter | Abbrevation | Value | Units | Formula |
| :---: | :---: | :---: | :---: | :---: |
| Antenna Diameter | D | 0.45 | meters |  |
| Antenna Centerline | h | 2 | meters |  |
| Antenna Surface Area | Sa | 0.159 | meter $^{2}$ |  |
| Antenna Ground Elevation | GE | 2 | meters |  |
| Frequency of Operation | f | 29.5 | GHz |  |
| Wavelength | $\lambda$ | 0.01017 | meters |  |
| HPA Output Power | $\mathrm{P}_{\text {HPA }}$ | 12.5 | Watts |  |
| HPA to Antenna Loss | $\mathrm{L}_{\text {Tx }}$ | 1 | dB |  |
| Radome Loss | $\mathrm{L}_{\text {rad }}$ | 1 | dB |  |
| Transmit Power at Flange | $\mathrm{P}_{\mathrm{F}}$ | 9.93 | Watts | $16 \text { PHPA/ } 10 \frac{-L_{r_{x}}}{10}$ |
| Power After Radome | $\mathrm{P}_{\text {Rad }}$ | 7.89 | Watts | $16 P F / /_{10} \frac{-\frac{L_{\text {pad }}}{10}}{}$ |
| Antenna Gain | $\mathrm{G}_{\text {es }}$ | 41.01 | dBi |  |
| Apeature Effeciency | $\eta$ | 0.65 |  |  |
| 1. Reflector Calculations |  |  |  |  |
| Antenna Surface Power Density | $P D_{\text {As }}$ | 249.72 | $\mathrm{W} / \mathrm{m}^{2}$ | $16 P F / \pi D^{2}$ |
|  |  | 24.97 | $\mathrm{mW} / \mathrm{cm}^{2}$ |  |
| Radome Surface Power Density | PD Rad | 198.36 | $\mathrm{W} / \mathrm{m}^{2}$ | $16 \mathrm{PRad} / \pi D^{2}$ |
|  |  | 19.84 | $\mathrm{mW} / \mathrm{cm}^{2}$ | Does Not meet Controlled Limits |
|  |  |  |  | Does Not meet Uncontrolled Limits |
| 2. On Axis Near Field Calculations |  |  |  |  |
| Extent of Near Field | $\mathrm{R}_{\mathrm{NF}}$ | 4.98 | meters | $D^{2} / 4 \lambda$ |
| Near Field Power Density | P DNF | 129.52 | $\mathrm{W} / \mathrm{m}^{2}$ | $16 \text { PRad } / \pi D^{2}$ |
|  |  | 12.95 | $\mathrm{mW} / \mathrm{cm}^{2}$ | Does Not meet Controlled Limits |
|  |  |  |  | Does Not meet Uncontrolled Limits |
| 3. On Axis Transition Region Calculations |  |  |  |  |
| Extent Of Transition Region, Minimum | $\mathrm{R}_{\text {TR }}$ | 4.98 | meters | $D^{2} / 4 \lambda$ |
| Extent Of Transition Region, Maximum | $\mathrm{R}_{\text {TR }}$ | 11.95 | meters | $0.6 D^{2} / \lambda$ |
| Worst Case Transition Region Power Density | $\mathrm{P}_{\text {DTR }}$ | 12.95 | $\mathrm{mW} / \mathrm{cm}^{2}$ | Does Not meet Controlled Limits |
|  |  |  |  | Does Not meet Uncontrolled Limits |
| Minimum Safe Distance, Uncontrolled Access | $\mathrm{R}_{\text {SU }}$ | 64.46 | meters | $P_{D N F} R N_{F} / 1 \mathrm{~mW} / \mathrm{cm}^{2}$ |
| Minimum Safe Distance, Controlled Access | $\mathrm{R}_{\mathrm{sc}}$ | 12.89 | meters | $P_{D N F} R N_{F} / 5 \mathrm{~mW} / \mathrm{cm}^{2}$ |
| 4. On Axis Far Field Calculations |  |  |  |  |
| Distance to Far Field | $\mathrm{R}_{\text {FF }}$ | 11.95 | meters | $0.6 D^{2} / \lambda$ |
| On Axis Power Density At Start of Far Field | P DFF | 55.48 | $\mathrm{W} / \mathrm{m}^{2}$ | $G_{E S} P R_{a d /}^{\prime \lambda} \lambda R F_{F}^{2}$ |
|  |  | 5.55 | $\mathrm{mW} / \mathrm{cm}^{2}$ | Does Not meet Controlled Limits |
|  |  |  |  | Does Not meet Uncontrolled Limits |
| 5. Off-Axis Far Field Power Density Calculations |  |  |  |  |
| Far Field Power Density at sampl $2^{\circ}$ Off-Axis |  | 0.12 | $\mathrm{mW} / \mathrm{cm}^{2}$ | $\mathrm{P}_{\mathrm{DFF}} /\left[G @ 2^{\circ} / G_{\text {es }}\right.$ <br> Meets Controlled Limits |
|  |  |  |  | Meets Uncontrolled Limits |
| 6. Off-Axis Power Density Calculations for the Near Field and Transitional Regions |  |  |  |  |
| Power Density Off Main Beam Axis at 1 Antenna | PDNF-off-axis | 0.13 | $\mathrm{mW} / \mathrm{cm}^{2}$ | $16 \text { PRad } / 100 \pi D_{N F}{ }^{2}$ |
| Diameter Removed |  |  |  | Meets Controlled Limits |
|  |  |  |  | Meets Uncontrolled Limits |
| 7. Off-Axis Safe Distances From Earth Station |  |  |  |  |
| Minimum Elevation Angle of Antenna | $\alpha_{\text {min }}$ | 10 | Degrees |  |
| Height of Object to be Cleared | h | 2 | meters |  |
| Height center of antenna is above the ground | $\mathrm{G}_{\mathrm{E}}$ | 2 | meters |  |
|  | $\alpha$ | S |  |  |
|  | $10^{\circ}$ | 6.99 m |  |  |
|  | $15^{\circ}$ | 4.63 m |  |  |
|  | $20^{\circ}$ | 3.45 m |  |  |
|  | $25^{\circ}$ | 2.73 m |  |  |
|  | $30^{\circ}$ | 2.24 m |  |  |

## II. Radiation Hazard Analysis

## BB45 (X-band)

This analysis predicts the radiation levels around a proposed earth station complex, comprised of a single panel type antenna. This report is developed in accordance with the prediction methods contained in OET Bulletin No. 65, Evaluating Compliance with FCC Guidelines for Human Exposure to Radio Frequency Electromagnetic Fields, Edition 97-01, pp 26-30. The maximum level of non-ionizing radiation to which employees may be exposed is limited to a power density level of 5 milliwatts per square centimeter ( $5 \mathrm{~mW} / \mathrm{cm}^{2}$ ) averaged over any 6 minute period in a controlled environment and the maximum level of non-ionizing radiation to which the general public is exposed is limited to a power density level of 1 milliwatt per square centimeter ( 1 $\mathrm{mW} / \mathrm{cm}^{2}$ ) averaged over any 30 minute period in a uncontrolled environment. Note that the worse-case radiation hazards exist along the beam axis. Under normal circumstances, it is highly unlikely that the antenna axis will be aligned with any occupied area since that would represent a blockage to the desired signals, thus rendering the link unusable.

## Earth Station Technical Parameter Table

| Antenna Aperture Size | 0.45 m |
| :--- | :--- |
| Antenna Effective Diameter | 0.45 m |
| Antenna Surface Area | 0.159 sq. meters |
| Antenna Isotropic Gain | 30.2 dBi |
| Number of Identical Adjacent Antennas 1 |  |
| Nominal Antenna Efficiency ( $\varepsilon$ ) | $71 \%$ |
| Nominal Frequency | 8.15 GHz |
| Nominal Wavelength ( $\lambda$ ) | 0.0368 meters |
| Maximum Transmit Power / Carrier | 25 Watts |
| Number of Carriers | 1 |
| Total Transmit Power | 25 Watts |
| W/G Loss from Transmitter to Feed | 1.0 dB |
| Total Feed Input Power | 19.9 Watts |
| Radome Losses | 1.0 dB |
| Effective RF Power at radome | 15.8 Watts |
| Near Field Limit | $\mathrm{R}_{\mathrm{nf}}=\mathrm{D}^{2} / 4 \lambda=1.38$ meters |
| Far Field Limit | $\mathrm{R}_{\mathrm{ff}}=0.6 \mathrm{D}^{2} / \lambda=3.30$ meters |
| Transition Region | $\mathrm{R}_{\mathrm{nf}}$ to $\mathrm{R}_{\mathrm{ff}}=1.38$ meters to 3.3 meters |

In the following sections, the power density in the above regions, as well as other critically important areas will be calculated and evaluated. The calculations are done in the order discussed in OET Bulletin 65.

### 1.0 At the Antenna Surface

The power density at the reflector surface can be calculated from the expression:

$$
\mathrm{PD}_{\mathrm{as}}=4 \mathrm{P} / \mathrm{A}=49.9 \mathrm{~mW} / \mathrm{cm}^{2}
$$

Where: $\mathrm{P}=$ total power at feed, milliwatts
$A=$ Total area of reflector, sq. cm

In the normal range of transmit powers for satellite antennas, the power densities at or around the reflector surface is expected to exceed safe levels. This area will not be accessible to the general public.

This antenna will incorporate a radome which has 1.0 dB of loss. The worst case power density at the surface of the radome is shown below:

$$
\begin{equation*}
\mathrm{PD}_{\text {radome }}=4 \mathrm{P}_{\mathrm{rad}} / \mathrm{A}=\mathbf{3 9 . 7} \mathrm{mW} / \mathrm{cm}^{2} \tag{2}
\end{equation*}
$$

Where: Prad = total power at feed less radome losses, milliwatts
$A=$ Total area of reflector, sq. cm (this would represent worst case)

Operators and technicians should receive training specifying this area as a high exposure area. Procedures must be established that will assure that all transmitters are rerouted or turned off before access by maintenance personnel to this area is possible.

### 2.0 On-Axis Near Field Region

The geometrical limits of the radiated power in the near field approximate a cylindrical volume with a diameter equal to that of the antenna. In the near field, the power density is neither uniform nor does its value vary uniformly with distance from the antenna. For the purpose of considering radiation hazard it is assumed that the on-axis flux density is at its maximum value throughout the length of this region. The length of this region, i.e., the distance from the antenna to the end of the near field, is computed as Rnf above.

The maximum power density in the near field is given by:

$$
\begin{aligned}
\mathrm{PD}_{\mathrm{nf}}=(16 \varepsilon \mathrm{P}) /\left(\pi \mathrm{D}^{2}\right)= & \mathbf{2 8 . 2} \mathrm{mW} / \mathrm{cm}^{2}(3) \\
& \text { from } 0 \text { to } 4.9 \text { meters }
\end{aligned}
$$

## Evaluation

Uncontrolled Environment: Does Not Meet Controlled Limits
Controlled Environment: Does Not Meet Uncontrolled Limits

### 3.0 On-Axis Transition Region

The transition region is located between the near and far field regions. As stated in Bulletin 65, the power density begins to vary inversely with distance in the transition region. The maximum power density in the transition region will not exceed that calculated for the near field region, and the transition region begins at that value. The maximum value for a given distance within the transition region may be computed for the point of interest according to:

```
PD tr = (PD nf )
where: }\quad\mp@subsup{PDDD }{nf}{}=\mathrm{ near field power density
    R
    R = distance to point of interest
PD
For: }\quad1.38<\textrm{R}<3.3\mathrm{ meters
```

We use Eq (4) to determine the safe on-axis distances required for the two occupancy conditions:

## Evaluation

### 4.0 On-Axis Far-Field Region

The on- axis power density in the far field region $\left(\mathrm{PD}_{\mathrm{ff}}\right)$ varies inversely with the square of the distance as follows:

$$
\begin{aligned}
& \mathrm{PD}_{\mathrm{ff}}= \mathrm{PG} /\left(4 \pi \mathrm{R}^{2}\right)=\text { dependent on } \mathrm{R}(5) \\
& \text { where: } \mathrm{P}=\text { total power at feed } \\
& \mathrm{G}=\text { Numeric Antenna gain in the direction of interest relative to isotropic radiator } \\
& \mathrm{R}=\text { distance to the point of interest } \\
& \text { For: } \quad \mathrm{R}>\mathrm{R}_{\mathrm{ff}}=3.3 \text { meters } \\
& \mathrm{PD}_{\mathrm{ff}}=\mathbf{1 2 . 1} \mathrm{mW} / \mathrm{cm}^{2} \text { at } \mathrm{R}_{\mathrm{ff}}
\end{aligned}
$$

We use Eq (5) to determine the safe on-axis distances required for the two occupancy conditions:

## Evaluation

Uncontrolled Environment Safe Operating Distance,(meters), $\mathrm{R}_{\text {safeu }}$ : $\quad$ See Section 3
Controlled Environment Safe Operating Distance,(meters), $\mathrm{R}_{\text {safec }}$ : See Section 3

### 5.0 Off-Axis Levels at the Far Field Limit and Beyond

In the far field region, the power is distributed in a pattern of maxima and minima (sidelobes) as a function of the off-axis angle between the antenna center line and the point of interest. Off-axis power density in the far field can be estimated using the antenna radiation patterns prescribed for the antenna in use. Usually this will correspond to the antenna gain pattern envelope defined by the FCC or the ITU, which takes the form of:
$\mathrm{G}_{\text {off }}=32-25 \log (\Theta)$
for $\Theta$ from 1 to 48 degrees; -10 dBi from 48 to 180 degrees
(Applicable for commonly used satellite transmit antennas)
Considering that satellite antenna beams are aimed skyward, power density in the far field will usually not be a problem except at low look angles. In these cases, the off axis gain reduction may be used to further reduce the power density levels.

For example: At two (2) degrees off axis At the far-field limit, we can calculate the power density as:
$\mathrm{G}_{\text {off }}=32-25 \log (2)=32-7.52 \mathrm{dBi}=280.2$ numeric

$$
\mathrm{PD}_{2 \text { deg off-axis }}=\mathrm{PD}_{\mathrm{ffX}} 280.2 / \mathrm{G}=3.2 \mathrm{~mW} / \mathrm{cm}^{2}(6)
$$

### 6.0 Off-Axis power density in the Near Field and Transitional Regions

According to Bulletin 65, off-axis calculations in the near field may be performed as follows: assuming that the point of interest is at least one antenna diameter removed from the center of the main beam, the power density at that point is at least a factor of $100(20 \mathrm{~dB})$ less than the value calculated for the equivalent on-axis power density in the main beam. Therefore, for regions at least D meters away from the center line of the dish, whether behind, below, or in front under of the antenna's main beam, the power density exposure is at least 20 dB below the main beam level as follows:

$$
\mathrm{PD}_{\mathrm{nf}(\text { off-axis })}=\mathrm{PD}_{\mathrm{nf}} / 100=\mathbf{0 . 2 8} \mathrm{mW} / \mathrm{cm}^{2} \text { at } \mathrm{D} \text { off axis (7) }
$$

See Section 7 for the calculation of the distance vs. elevation angle required to achieve this rule for a given object height.

### 7.0 Evaluation of Safe Occupancy Area in Front of Antenna

The distance (S) from a vertical axis passing through the dish center to a safe off axis location in front of the antenna can be determined based on the dish diameter rule (Item 6.0). Assuming a flat terrain in front of the antenna, the relationship is:

$$
\mathrm{S}=(\mathrm{D} / \sin \alpha)+(2 \mathrm{~h}-\mathrm{D}-2) /(2 \tan \alpha)(8)
$$

Where: $\alpha=$ minimum elevation angle of antenna
$\mathrm{D}=$ dish diameter in meters
$\mathrm{h}=$ maximum height of object to be cleared, meters
For distances equal or greater than determined by equation (8), the radiation hazard will be below safe levels for all but the most powerful stations (> 4 kilowatts RF at the feed).

For $\quad \mathrm{D}=\quad 0.569$ meters
$\mathrm{h}=\quad 2.0$ meters, delta between antenna and object $>1 \mathrm{~m}$
Then:

| $\alpha$ | $S$ |
| :--- | :--- |
| 10 | 7.0 meters |
| 15 | 4.6 meters |
| 20 | 3.4 meters |
| 25 | 2.7 meters |
| 30 | 2.3 meters |

### 8.0 Summary of Results

The earth station site will be protected from uncontrolled access by virtue of the fact that it will be mounted on the top of an air vehicle. There will also be proper emission warning signs placed and all operating personnel will be aware of the human exposure levels at and around the earth station. The applicant agrees to abide by the conditions specified in Condition 18 provided below:
(18) - UltiSat Inc shall take all reasonable and customary measures to ensure that the MET does not create potential for harmful non-ionizing radiation to persons who may be in the vicinty of the MET when it is in operation. At a minimum, permanent warning label(s) shall be affixed to the MET warning of the radiation hazard and including a diagram showing the regions around the MET so as to minimize access to the hazardous region and/or any other appropriate means.

The table on the following page summarizes all of the above calculations.

| Parameter | Abbrevation | Value | Units | Formula |
| :---: | :---: | :---: | :---: | :---: |
| Antenna Diameter | D | 0.45 | meters |  |
| Antenna Centerline | h | 2 | meters |  |
| Antenna Surface Area | Sa | 0.159 | meter $^{2}$ |  |
| Antenna Ground Elevation | GE | 2 | meters |  |
| Frequency of Operation | f | 8.15 | GHz |  |
| Wavelength | $\lambda$ | 0.03681 | meters |  |
| HPA Output Power | $\mathrm{P}_{\text {HPA }}$ | 25 | Watts |  |
| HPA to Antenna Loss | $\mathrm{L}_{\text {Tx }}$ | 1 | dB |  |
| Radome Loss | $\mathrm{L}_{\text {rad }}$ | 1 | dB |  |
| Transmit Power at Flange | $\mathrm{P}_{\mathrm{F}}$ | 19.86 | Watts | $16 \text { PHPA/ } / 10 \frac{-L_{x x}}{10}$ |
| Power After Radome | $\mathrm{P}_{\text {Rad }}$ | 15.77 | Watts | $F / 10 \frac{-L_{\text {ead }}}{10}$ |
| Antenna Gain | $\mathrm{G}_{\text {es }}$ | 30.2 | dBi |  |
| Apeature Effeciency | $\eta$ | 0.71 |  |  |
| 1. Reflector Calculations |  |  |  |  |
| Antenna Surface Povier Density | $P D_{\text {As }}$ | 499.44 | $\mathrm{W} / \mathrm{m}^{2}$ | $16 P F / \pi D^{2}$ |
|  |  | 49.94 | $\mathrm{mW} / \mathrm{cm}^{2}$ |  |
| Radome Surface Povier Density | PD ${ }_{\text {Rad }}$ | 396.72 | $\mathrm{W} / \mathrm{m}^{2}$ | $16 \mathrm{PRad} / \pi D^{2}$ |
|  |  | 39.67 | $\mathrm{mW} / \mathrm{cm}^{2}$ | Does Not meet Controlled Limits |
|  |  |  |  | Does Not meet Uncontrolled Limits |
| 2. On Axis Near Field Calculations |  |  |  |  |
| Extent of Near Field | $\mathrm{R}_{\mathrm{NF}}$ | 1.38 | meters | $D^{2} / 4 \lambda$ |
| Near Field Power Density | $\mathrm{P}_{\text {dNF }}$ | 281.64 | $\mathrm{W} / \mathrm{m}^{2}$ | $16 \mathrm{PRad} / \pi D^{i}$ |
|  |  | 28.16 | $\mathrm{mW} / \mathrm{cm}^{2}$ | Does Not meet Controlled Limits |
|  |  |  |  | Does Not meet Uncontrolled Limits |
| 3. On Axis Transition Region Calculations |  |  |  |  |
| Extent Of Transition Region, Minimum | $\mathrm{R}_{\text {TR }}$ | 1.38 | meters | $D^{2} / 4$ |
| Extent Of Transition Region, Maximum | $\mathrm{R}_{\text {TR }}$ | 3.30 | meters | $0.6 D^{2} / \lambda$ |
| Worst Case Transition Region Power Density | $\mathrm{P}_{\text {DTR }}$ | 28.16 | $\mathrm{mW} / \mathrm{cm}^{2}$ | Does Not meet Controlled Limits |
|  |  |  |  | Does Not meet Uncontrolled Limits |
| Minimum Safe Distance, Uncontrolled Access | Rsu | 38.74 | meters | $P_{D N F} R N F / 1 \mathrm{~mW}^{2} / \mathrm{cm}^{2}$ |
| Minimum Safe Distance, Controlled Access | $\mathrm{R}_{\text {sc }}$ | 7.75 | meters | $P_{D N F} R N F / 5 \mathrm{~mW} / \mathrm{cm}^{2}$ |
| 4. On Axis Far Field Calculations |  |  |  |  |
| Distance to Far Field | $\mathrm{R}_{\text {fF }}$ | 3.30 | meters | $0.6 D^{2} / \lambda$ |
| On Axis Power Density At Start of Far Field | P DFF | 120.64 | $\mathrm{W} / \mathrm{m}^{2}$ | $G_{E S} P R a d / 4 \lambda R F F^{2}$ |
|  |  | 12.06 | $\mathrm{mW} / \mathrm{cm}^{2}$ | Does Not meet Controlled Limits |
|  |  |  |  | Does Not meet Uncontrolled Limits |
| 5. Off-Axis Far Field Power Density Calculations |  |  |  |  |
| Far Field Power Density at sampl 2* Off-Axis |  | 3.23 | $\mathrm{mW} / \mathrm{cm}^{2}$ | $\mathrm{P}_{\mathrm{DFF}} /\left[G @ 2^{\circ} /_{G_{e s}}\right.$ <br> Meets Controlled Limits |
|  |  |  |  | Meets Uncontrolled Limits |
| 6. Off-Axis Power Density Calculations for the Near Field and Transitional Regions |  |  |  |  |
| Power Density Off Main Beam Axis at 1 Antenna | $\mathrm{P}_{\text {DNF-off-axis }}$ | 0.28 | $\mathrm{mW} / \mathrm{cm}^{2}$ | $16 \mathrm{PRad} / 100 \pi D_{N F}{ }^{2}$ |
| Diameter Removed |  |  |  | Meets Controlled Limits |
|  |  |  |  | Does not meet Uncontrolled Limits |
| 7. Off-Axis Safe Distances From Earth Station |  |  |  |  |
| Minimum Elevation Angle of Antenna | $\alpha_{\text {min }}$ | 10 | Degrees |  |
| Height of Object to be Cleared | h | 3 | meters |  |
| Height center of antenna is above the ground | $\mathrm{G}_{\mathrm{E}}$ | 2 | meters |  |
|  | $\alpha$ | S |  |  |
|  | $10^{\circ}$ | 6.99 m |  |  |
|  | $15^{\circ}$ | 4.63 m |  |  |
|  | $20^{\circ}$ | 3.45 m |  |  |
|  | $25^{\circ}$ | 2.73 m |  |  |
|  | $30^{\circ}$ | 2.24 m |  |  |

## III. BB45 Off-Axis EIRP Spectral Density Patterns

## A. Ka-band

1. 29.0 GHz









## 2. 30.0 GHz (Commercial)










## 3. 30.0 GHz (Military)










## 4. 31.0 GHz





ESD (dBW/Hz) 31.0 GHz, RCP, phi=90





ESD (dBW/Hz) 31.0 GHz,LCP, phi=90


## A. X-band

## 1. 7.90 GHz





ESD (dBW/Hz) 7.9 GHz, RCP, phi $=90^{\circ}$





2. 8.15 GHz








3. 8.40 GHz







ESD (dBW/Hz) 8.4 GHz, LCP, phi=90


IV. BB45 Gain Patterns

## A. Ka-band

1. 29.0 GHz



29.0GHz Co (RCP) and Cross Polarization (Hi-Res) Phi=90





2. 30.0 GHz



30.0 GHz Co (RCP) and Cross Polarization (Hi-Res) Phi=90





3. 31.0 GHz








