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<b>APPROVALS</b>		<b>TYPE</b> Test Procedure	
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Concurrence: Austin Williams  VP Space Vehicles		<b>SUPERSEDES SPEC DATED</b>  NA	
		<b>REV</b> 03	

**TITLE:** NanoACE Orbital Debris Assessment Report (ODAR) / End of Mission Plan (EOMP)

**Warnings and Disclaimers:**

All future revisions to this document shall be approved by the controlling organization prior to release.



**TABLE OF CONTENTS**

**ORBITAL DEBRIS SELF-ASSESSMENT: NANOACE MISSION .....6**

**1.0 PROGRAM MANAGEMENT AND MISSION OVERVIEW .....7**

1.1 Program Management.....7

1.2 Mission Overview.....7

1.2.1 Mission Design and Development Milestones .....7

1.2.2 Mission Overview.....7

**2.0 SPACECRAFT DESCRIPTION.....8**

2.1 Physical Description of Spacecraft .....8

2.1.1 Description of Propulsion Systems.....8

2.1.2 Description of attitude control system .....9

2.1.3 Description of normal attitude of the spacecraft with respect to the velocity vector.....9

2.1.4 Description of any range safety or other pyrotechnic devices .....9

2.1.5 Description of the electrical generation and storage system.....9

**3.0 ASSESSMENT OF SPACECRAFT DEBRIS RELEASED DURING NORMAL OPERATIONS .....10**

**4.0 ASSESSMENT OF SPACECRAFT POTENTIAL FOR EXPLOSIONS AND INTENTIONAL BREAKUPS .....11**

4.1 Potential causes of spacecraft breakup during deployment and mission operations .....11

4.2 Summary of failure modes and effects analysis of all credible failure modes .....11

4.3 Detailed plan for any designed spacecraft breakup .....11

4.4 List of components which shall be passivated at End of Mission (EOM).....11

4.5 Rationale for all items which are required to be passivated, but cannot be due to their design.....11

4.6 Assessment of spacecraft compliance with Requirements 4.4-1 through 4.4-4 .....12

**5.0 ASSESSMENT OF SPACECRAFT POTENTIAL FOR ON-ORBIT COLLISIONS 14**

5.1 Assessment of spacecraft compliance with Requirements 4.5-1 and 4.5-2:.....14

**6.0 ASSESSMENT OF SPACECRAFT POSTMISSION DISPOSAL PLANS AND PROCEDURES.....15**

6.1 Description of spacecraft disposal option selected.....15

6.2 Plan for any spacecraft maneuvers required to accomplish postmission disposal: .....15

6.3 Calculation of area-to-mass ratio after postmission disposal: .....15

6.4 Assessment of spacecraft compliance with Requirements 4.6-1 through 4.6-5:.....15

6.5 Detailed plan for passivating (depleting all energy sources) of the spacecraft: .....16

**7.0 ASSESSMENT OF SPACECRAFT REENTRY HAZARDS.....18**

7.1 Assessment of spacecraft compliance with Requirement 4.7-1: .....18

**8.0 ASSESSMENT FOR TETHER MISSIONS .....19**

**APPENDIX A – FMEA DETAILS AND SUPPORTING RATIONALE .....20**

Propulsion Module Failure: .....20

Battery Explosion Failure: .....21

**APPENDIX B - REQUIREMENT 4.5-1 DAS 2.0.1 LOG .....24**

**APPENDIX C - REQUIREMENT 4.6 DAS 2.0.1 LOG .....25**

**APPENDIX D - REQUIREMENT 4.7-1 DAS 2.0.1 LOG.....26**

## List of Figures

Figure 6.4 – NANOACE Deorbit Lifetime.....	15
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### List of Tables

Table 1.1 – Summary of Program Management Personnel ..... 7  
Table 1.2 – Summary of Mission Design and Development Milestones ..... 7  
Table 1.1 – Summary of Mission Parameters ..... 7  
Table 1.1 – Summary of Spacecraft Parameters ..... 8  
Table 3.0 – Summary of Spacecraft Debris Released During Normal Operations ..... 10

**ORBITAL DEBRIS SELF-ASSESSMENT: NANOACE MISSION**

Requirement	Launch Vehicle				Spacecraft			Comments
	Compliant	Not Compliant	Incomplete	Standard Non Compliant	Compliant	Not Compliant	Incomplete	
4.3-1.a			X		X			No debris released in LEO
4.3-1.b			X		X			No debris released in LEO
4.3-2			X		X			No debris released in GEO
4.4-1			X		X			Less than 0.001 probability
4.4-2			X		X			Design to passivate propulsion, electrical power system, and reaction wheels
4.4-3			X		X			No planned breakups
4.4-4			X		X			No planned breakups
4.5-1			X		X			Probability 0.000004 (requirement < 0.001)
4.5-2			X		X			Probability 0.00134 (requirement < 0.01)
4.6-1(a)			X		X			Predicted orbital lifetime 16.96 years
4.6-1(b)			X		X			N/A – using atmospheric entry
4.6-1(c)			X		X			N/A – using atmospheric entry
4.6-2			X		X			N/A – Not GEO
4.6-3			X		X			N/A – Not between LEO and GEO
4.6-4			X		X			Expected probability < 0.001
4.7-1			X		X			No pieces survive reentry
4.8-1					X			No tethers used

NANOACE is a rideshare on the launch. All of the other portions of the launch, not including the NANOACE vehicles, are not Tyvak.



## 2.0 SPACECRAFT DESCRIPTION

### 2.1 Physical Description of Spacecraft

The NANOACE vehicles have been designed to support a 1+ year mission in LEO, and it is compatible with the P-POD launch environments and designed to the requirements in the CubeSat Design Specification (CDS). The NANOACE vehicle is a 3U CubeSat with the core of the vehicle being 30cm x 10cm x 10cm with a mass of roughly 6 kg. The vehicle uses a total of four deployable solar panels and each is roughly 30cm x 10cm in size.

The NANOACE vehicle design uses subsystem modules built from printed circuit boards (PCB) or miniature enclosures mounted to the open frame primary structure. The open structure permits the vehicle to be built incrementally with open access for securing interconnects. The subsystems are placed within the vehicle to optimize mass properties, radiation protection, thermal heat rejection, power handling, vehicle orientation, and cabling length. The body mounted side panels attach directly to the primary structure and are used for thermal management and can be easily removed to get access to the interior of the vehicle. The vehicle is primarily constructed out of aluminum and PCB materials.

The NANOACE payload utilizes multiple sensors to support range determination at different operating distances. The NANOACE payload houses one IR and four visible cameras, as well as the docking mechanism, and electronics for image processing.

Parameter	Value
Total satellite mass at launch, including all propellants and fluids	~6.0 kg
Dry Mass of satellite at launch, excluding solid rocket motor propellants	~5.7kg
Identification, including mass and pressure, of all fluids	R236a (common refrigerant), 380 grams, 67 psig at room temp.
Fluids in Pressurized batteries	NONE. NANOACE uses unpressurized standard COTS Li-ion battery cells
Identification of any other sources of stored energy	NONE
Identification of any radioactive materials on board	NONE

*Table 1.1 – Summary of Spacecraft Parameters*

#### 2.1.1 Description of Propulsion Systems

The NANOACE cold gas propulsion system utilizes a mature design that was developed by VACCO Industries and tested extensively (70,000+ firings) in a vacuum by the US Air Force Research Lab and traces heritage to DARPA and Aerospace Corp programs. The highly integrated unit utilizes R236a as a propellant that is stored as liquid for volume efficiency. All sensor and control electronics are contained inside the unit and only requires power and serial data connections. Extensive materials compatibility testing and analyses have demonstrated that the propellant is compatible being immersed around the electronics. The NANOACE propulsion module is made out of aluminum and has eight thrusters located at the corners of the unit. The unit can hold roughly 380 grams of propellant.



### **2.1.2 Description of attitude control system**

The NANOACE attitude determination and control system consists of a processor, Inertial Reference Module (IRM), nano-Reaction Wheel Array (nRWA), GPS receiver, Sun sensors, magnetometers, and integrated torque coils. Primary attitude knowledge is provided by the IRM which hosts two star sensors and the inertial measurement unit (IMU). Primary attitude control is provided by the nRWA which consists of an orthogonal set of three wheels. Momentum management and vehicle detumble are provided by a set of three torque coils.

### **2.1.3 Description of normal attitude of the spacecraft with respect to the velocity vector**

The nominal attitude of the NANOACE vehicles has the long axis (z-axis) of the vehicle pointed along the velocity vector. The vehicle is rotated about the long axis to point the deployable panels in a zenith direction for energy collection. The NANOACE vehicle will spend a majority of their time in this attitude.

### **2.1.4 Description of any range safety or other pyrotechnic devices**

None.

### **2.1.5 Description of the electrical generation and storage system**

Energy generation is accomplished using four deployable solar panels and additional solar cells that are mounted on the core of the vehicle. Energy storage is accomplished using standard COTS Li-ion battery cells in a 3S2P (3 in series, 2 parallel) configuration. The cells are recharged by the solar cells mounted on the deployable and body panels. The power management and distribution is provided by the electrical power system and battery protection circuitry.

### 3.0 ASSESSMENT OF SPACECRAFT DEBRIS RELEASED DURING NORMAL OPERATIONS

No intentional release of any object > 1mm is expected.

Parameter	Value
Identification of any object (>1mm) expected to be released from the spacecraft at any time after launch	None
Rationale/necessity for release of object	N/A
Time of release of each object, relative to launch time	N/A
Release velocity of each object with respect to spacecraft	N/A
Expected orbital parameters of each object after release	N/A
Calculated orbital lifetime of each object	N/A
Compliance 4.3-1 Mission related debris passing through GEO	COMPLIANT
Compliance 4.3-2 Mission related debris passing through LEO	COMPLIANT

*Table 3.0 – Summary of Spacecraft Debris Released During Normal Operations*

## **4.0 ASSESSMENT OF SPACECRAFT POTENTIAL FOR EXPLOSIONS AND INTENTIONAL BREAKUPS**

### **4.1 Potential causes of spacecraft breakup during deployment and mission operations**

There is no credible scenario that would result in spacecraft breakup during normal deployment and operations.

### **4.2 Summary of failure modes and effects analysis of all credible failure modes**

In-mission failure of a battery cell protection circuit could lead to a short circuit resulting in overheating and a very remote possibility of battery cell explosion. The battery safety systems discussed in the FMEA (Appendix A, see requirement 4.4-1) describe the combined faults that must occur for any of seven (7) independent, mutually exclusive failure modes to lead to explosion.

Over-pressure due to temperature control failure or crushing of the propulsion tank could lead to vent or burst of the propulsion tank. The propulsion safety systems discussed in the FMEA (Appendix A, see requirement 4.4-1) describe the combined faults that must occur for any of the three (3) independent, mutually exclusive failure modes to lead to tank failure..

### **4.3 Detailed plan for any designed spacecraft breakup**

There are no planned breakups.

### **4.4 List of components which shall be passivated at End of Mission (EOM)**

The nRWA will be passivated at EOM through a series of commands to reduce wheel momentum to a minimum level and then to transition the vehicle to free drift mode.

The batteries will be passivated by discharging the cells to a minimum state and then disconnecting them from the solar panels and charging circuitry.

The propulsion tank will be depressurized by opening the valves at EOM.

### **4.5 Rational for all items which are required to be passivated, but cannot be due to their design**

None.

#### 4.6 Assessment of spacecraft compliance with Requirements 4.4-1 through 4.4-4

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**Requirement 4.4-1:** *Limiting the risk to other space systems from accidental explosions during deployment and mission operations while in orbit about Earth or the Moon:*

*For each spacecraft and launch vehicle orbital stage employed for a mission, the program or project shall demonstrate, via failure mode and effects analyses or equivalent analyses, that the integrated probability of explosion for all credible failure modes of each spacecraft and launch vehicle is less than 0.001 (excluding small particle impacts) (Requirement 56449).*

---

Compliance statement:

Required Probability: 0.001

Expected probability: 0.000 COMPLIANT

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**Requirement 4.4-2:** *Design for passivation after completion of mission operations while in orbit about Earth or the Moon:*

*Design of all spacecraft and launch vehicle orbital stages shall include the ability to deplete all onboard sources of stored energy and disconnect all energy generation sources when they are no longer required for mission operations or postmission disposal or control to a level which can not cause an explosion or deflagration large enough to release orbital debris or break up the spacecraft (Requirement 56450).*

---

Compliance statement:

The batteries will be passivated by discharging the cells to a minimum state and then disconnecting them from the solar panels and charging circuit. In the unlikely event that a battery cell does explosively rupture, the small size, mass, and potential energy of these batteries is such that while the spacecraft could be expected to vent gases, most debris from the battery rupture would be contained within the vehicle due to lack of penetration energy and also because the cells are housed in a substantial aluminum bracket.

The nRWA will be passivated at EOM through a series of commands to reduce wheel momentum to a minimum level and then to transition the vehicle to free drift mode.

The propulsion tank will be depressurized by opening the valves at EOM.

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***Requirement 4.4-3. Limiting the long-term risk to other space systems from planned breakups:***

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Compliance statement:

This requirement is not applicable. There are no planned breakups.

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***Requirement 4.4-4: Limiting the short-term risk to other space systems from planned breakups:***

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Compliance statement:

This requirement is not applicable. There are no planned breakups.

## 5.0 ASSESSMENT OF SPACECRAFT POTENTIAL FOR ON-ORBIT COLLISIONS

### 5.1 Assessment of spacecraft compliance with Requirements 4.5-1 and 4.5-2:

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**Requirement 4.5-1.** *Limiting debris generated by collisions with large objects when operating in Earth orbit: For each spacecraft and launch vehicle orbital stage in or passing through LEO, the program or project shall demonstrate that, during the orbital lifetime of each spacecraft and orbital stage, the probability of accidental collision with space objects larger than 10 cm in diameter is less than 0.001 (Requirement 56506).*

---

Compliance statement: (Large Object Impact and Debris Generation Probability)

Required Probability: 0.001

Expected probability: 0.000004 COMPLIANT

---

**Requirement 4.5-2.** *Limiting debris generated by collisions with small objects when operating in Earth or lunar orbit: For each spacecraft, the program or project shall demonstrate that, during the mission of the spacecraft, the probability of accidental collision with orbital debris and meteoroids sufficient to prevent compliance with the applicable postmission disposal requirements is less than 0.01 (Requirement 56507).*

---

Compliance statement: (Small Object Impact and Debris Generation Probability)

Required Probability: 0.01

Expected probability: 0.00134 COMPLIANT

## 6.0 ASSESSMENT OF SPACECRAFT POSTMISSION DISPOSAL PLANS AND PROCEDURES

### 6.1 Description of spacecraft disposal option selected

The satellite will de-orbit naturally by atmospheric re-entry. The propulsion system is not used for re-entry.

### 6.2 Plan for any spacecraft maneuvers required to accomplish postmission disposal:

None.

### 6.3 Calculation of area-to-mass ratio after postmission disposal:

Spacecraft Mass: ~5.7kg (dry mass)  
Cross-sectional Area: 0.08 m<sup>2</sup> (average of min and max areas).  
Area to mass ratio: (0.08 m<sup>2</sup>)/(5.7 kg) = 0.014 m<sup>2</sup>/kg

### 6.4 Assessment of spacecraft compliance with Requirements 4.6-1 through 4.6-5:

---

**Requirement 4.6-1.** *Disposal for space structures passing through LEO: A spacecraft or orbital stage with a perigee altitude below 2000 km shall be disposed of by one of three methods: (Requirement 56557)*

*a. Atmospheric reentry option:*

- *Leave the space structure in an orbit in which natural forces will lead to atmospheric reentry within 25 years after the completion of mission but no more than 30 years after launch; or*
- *Maneuver the space structure into a controlled de-orbit trajectory as soon as practical after completion of mission.*

*b. Storage orbit option:*

- *Maneuver the space structure into an orbit with perigee altitude greater than 2000 km and apogee less than GEO - 500 km.*

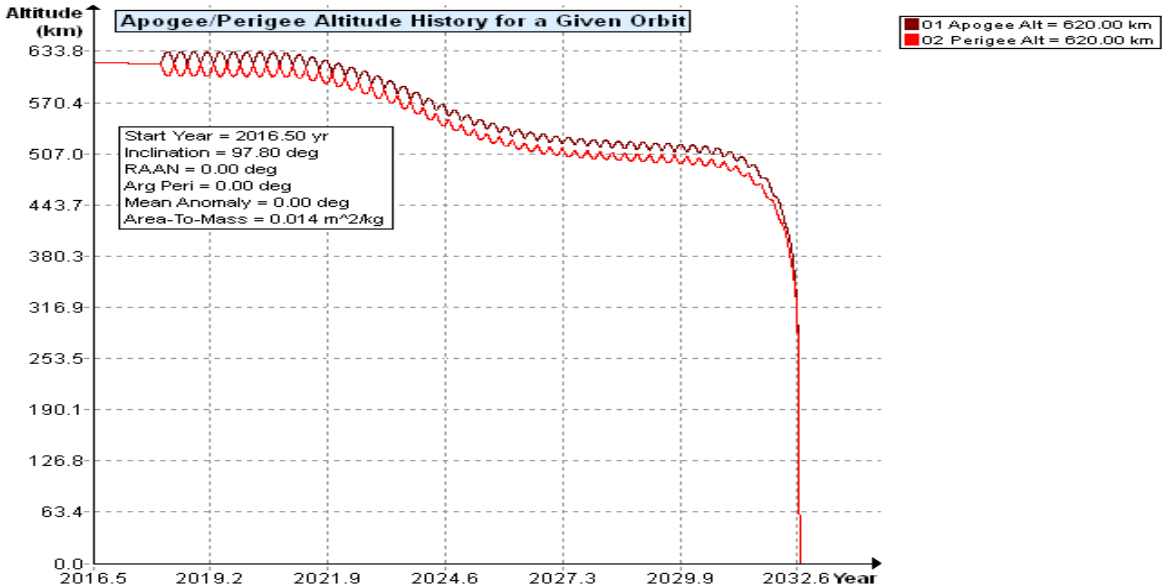
*c. Direct retrieval:*

- *Retrieve the space structure and remove it from orbit within 10 years after completion of mission*
- 

Compliance statement:

The orbital lifetime is predicted to be 16.96 years; COMPLIANT

*Figure 6.4 – NANOACE Deorbit Lifetime*



**Requirement 4.6-2. Disposal for space structures near GEO.**

Compliance statement:

Not applicable. NANOACE mission orbit is a LEO.

**Requirement 4.6-3. Disposal for space structures between LEO and GEO.**

Compliance statement:

Not applicable. NANOACE mission orbit is a LEO.

**Requirement 4.6-4. Reliability of Postmission Disposal Operations**

Compliance statement:

Not applicable. The satellite will reenter passively without the need for post mission disposal operations within the allowable timeframe.

**6.5 Detailed plan for passivating (depleting all energy sources) of the spacecraft:**

The nRWA will be passivated at EOM through a series of commands to reduce wheel momentum to a minimum level and then to transition the vehicle to free drift mode. The free drift



mode does not utilize any attitude control actuators, specifically the nRWA. The power service to the nRWA will also be deactivated so that no inadvertent switch to another attitude control mode can actuate the nRWA.

The propulsion tank will be depressurized by opening the plenum and thruster valve(s) at EOM.

The batteries will be passivated by permanently disconnecting solar array power from the battery module and discharging the cells to a minimum state under load of the spacecraft bus.

## 7.0 ASSESSMENT OF SPACECRAFT REENTRY HAZARDS

### 7.1 Assessment of spacecraft compliance with Requirement 4.7-1:

---

**Requirement 4.7-1.** *Limit the risk of human casualty: The potential for human casualty is assumed for any object with an impacting kinetic energy in excess of 15 joules:*

*a) For uncontrolled reentry, the risk of human casualty from surviving debris shall not exceed 0.0001 (1:10,000) (Requirement 56626).*

---

Compliance statement:

DAS v2.0.1 reports that NANOACE is COMPLIANT with the requirement. The vehicle is primarily composed of Aluminum and PCB (Fiberglass) material and none of the components is expected to survive re-entry. The predicted Total Debris Casualty Area is 0.00. Appendix D located in the back of this report contains the DAS 2.0.1 modeling input and results.

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**Requirement 4.7-1., b)** *For controlled reentry, the selected trajectory shall ensure that no surviving debris impact with a kinetic energy greater than 15 joules is closer than 370 km from foreign landmasses, or is within 50 km from the continental U.S., territories of the U.S., and the permanent ice pack of Antarctica (Requirement 56627).*

---

Compliance statement:

Not applicable. No controlled reentry planned.

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**Requirement 4.7-1., c)** *For controlled reentries, the product of the probability of failure of the reentry burn (from Requirement 4.6-4.b) and the risk of human casualty assuming uncontrolled reentry shall not exceed 0.0001 (1:10,000) (Requirement 56628).*

---

Compliance statement:

Not applicable. No controlled reentry planned.

## 8.0 ASSESSMENT FOR TETHER MISSIONS

Not applicable. There are no tethers in the NANOACE mission.

## APPENDIX A – FMEA DETAILS AND SUPPORTING RATIONALE

### Propulsion Module Failure:

**Effect:** All failure modes below might result in Propulsion explosion with the possibility of orbital debris generation. The pressure vessel burst pressure has been designed with 2.5 times operating pressure at maximum storage temperature.

**Probability:** Very Low. It is believed to be less than 0.1% given that multiple independent (not common mode) faults must occur for each failure mode to cause the ultimate effect (explosion).

**Failure mode 1:** Overpressure due to the Propellant Tank Heater (H2) failed powered. The propellant temperature is normally controlled by a thermostat circuit using a thermistor (T2) to sense temperature. Should H2 fail powered, propellant temperature could exceed the maximum qualification temperature of 70°C causing the propellant pressure to exceed the corresponding design pressure of 307 psia.

*Mitigation 1:* The Propulsion Module pressure boundary is designed and verified by analysis to withstand a Burst Pressure of 768 psia without external leakage. The system will be tested to a Proof Pressure of 461 psia.

*Mitigation 2:* The Propulsion Module Controller has a separate fail-safe circuit that will cut power to H2 should the pressure as measured by P2 rise above 315 psia.

*Combined faults required for realized failure:* Both the thermostat using T2 **AND** the fail-safe circuit using P2 must fail with H2 powered to realize the failure.

**Failure mode 2:** Overpressure due to the Gas Volume Heater (H1) failed powered. The propellant temperature is normally controlled by a thermostat circuit using a thermistor (T1) to sense temperature. Should H1 fail powered, propellant temperature could exceed the maximum qualification temperature of 70°C causing the propellant pressure to eventually exceed the corresponding design pressure of 307 psia.

*Mitigation 1:* The Propulsion Module Gas Volume pressure boundary is designed and verified by analysis to withstand a Burst Pressure of 768 psia without external leakage. The system will be tested to a Proof Pressure of 461 psia.

*Mitigation 2:* The Propulsion Module Controller has a separate fail-safe circuit that will cut power to H1 should the pressure as measured by P1 rise above 315 psia.

*Combined faults required for realized failure:* Both the thermostat using T1 **AND** the fail-safe circuit using P1 must fail with H1 powered to realize the failure.

### Failure Mode 3: Crushing.

*Mitigation 2:* This mode is negated by spacecraft design. There are no moving parts in the proximity of the propulsion module with sufficient kinetic energy to damage the unit.

*Combined faults required for realized failure:* A catastrophic failure must occur in an external system **AND** the failure must cause a collision sufficient to crush the tank leading to a pressure vessel or electronics failure.

### **Battery Explosion Failure:**

**Effect:** All failure modes below might result in battery explosion with the possibility of orbital debris generation. However, in the unlikely event that a battery cell does explosively rupture, the small size, mass, and potential energy, of these small batteries is such that while the spacecraft could be expected to vent gases, most debris from the battery rupture should be contained within the vessel due to the lack of penetration energy. The battery is housed within a substantial aluminum bracket.

**Probability:** Very Low. It is believed to be less than 0.1% given that multiple independent (not common mode) faults must occur for each failure mode to cause the ultimate effect (explosion).

#### **Failure mode 1:** Battery Internal short circuit.

*Mitigation 1:* Qualification and acceptance tests include vibration, thermal cycling, and vacuum tests followed by maximum system rate-limited charge and discharge to prove that no internal short circuit sensitivity exists.

*Mitigation 2:* Over/under voltage cell protection circuitry guards against stress conditions that can cause the development of internal shorts.

*Combined faults required for realized failure:* Environmental testing **AND** functional charge/discharge tests must both be ineffective in discovery of infant mortality failure rate (IMFR) related faults **OR** protection circuitry malfunctions and fails to protect cells from stress conditions.

#### **Failure Mode 2:** Internal thermal rise due to high load discharge rate.

*Mitigation 3:* Each cell includes an internal positive temperature coefficient (PTC) variable resistance device that reduces discharge current as cell temperature increases to prevent thermal runaway.

*Mitigation 4:* External under-voltage lockout circuitry disconnects battery when battery discharge voltage droop crosses a predefined threshold.

*Combined faults required for realized failure:* Spacecraft thermal design must be incorrect **AND** internal **AND** external over current detection and protection must fail for this failure mode to occur.

#### **Failure Mode 3:** Overcharging and excessive charge rate.

*Mitigation 5:* The satellite bus battery charging circuit design eliminates the possibility of the batteries being overcharged if circuits function nominally. This circuit will be extensively bench-tested and be proto-qualified for survival in vibration, and thermal-vacuum

environments. The charge circuit disconnects the incoming current when cell voltage indicates normal full charge at 4.2V and limits charge current within battery specification. If this circuit fails to operate, continuing or excessive charge current can cause gas generation. The batteries include overpressure release vents that allow gas to escape, virtually eliminating any explosion hazard.

*Combined faults required for realized failure:*

- 1) For overcharging: The charge control circuit must fail to limit charge voltage **AND** the PTC device must fail (or temperatures generated must be insufficient to cause the PTC device to modulate) **AND** the overpressure relief device must be inadequate to vent generated gasses at acceptable rates to avoid explosion.
- 2) For excessive charge rate: The charge control circuitry must fail to limit charge current **AND** the PTC device must fail (or temperatures generated must be insufficient to cause the PTC device to modulate) **AND** the overpressure relief device must be inadequate to vent generated gasses at acceptable rates to avoid explosion.

**Failure Mode 4:** Excessive discharge rate or short circuit due to external device failure or terminal contact with conductors not at battery voltage levels (due to abrasion or inadequate proximity separation).

*Mitigation 6:* This failure mode is negated by a) proto-qualification tested short circuit protection on each external circuit, b) design of battery packs and insulators such that no contact with nearby board traces or structure is possible without being caused by some other mechanical failure, c) obviation of such other mechanical failures by proto-qualification and acceptance environmental tests (shock, vibration, thermal cycling, and thermal-vacuum tests).

*Combined faults required for realized failure:* The PTC must fail **AND** an external load must fail/short-circuit **AND** external over-current detection and disconnect function must fail to enable this failure mode.

**Failure Mode 5:** Inoperable vents.

*Mitigation 7:* Battery vents are not inhibited by the battery holder design or the spacecraft.

*Combined effects required for realized failure:* The spacecraft design inhibits cell venting, or cell venting clearance is sensitive to environmental stress.

**Failure Mode 6:** Crushing.

*Mitigation 8:* This mode is negated by spacecraft design. There are no moving parts in the proximity of the batteries. Qualification and acceptance tests including vibration, thermal cycling, and vacuum tests will demonstrate cell venting clearance insensitivity to environmental stress.

*Combined faults required for realized failure:* A catastrophic failure must occur in an external system **AND** the failure must cause a collision sufficient to crush the batteries leading to an

internal short circuit **AND** the satellite must be in a naturally sustained orbit at the time the crushing occurs.

**Failure Mode 7:** Excess temperatures due to orbital environment and high discharge combined.

*Mitigation 9:* The spacecraft thermal design will negate this possibility. Thermal rise will be analyzed in combination with space environment temperatures showing that batteries do not exceed normal allowable operating temperatures which are well below temperatures of concern for explosions.

*Combined faults required for realized failure:* Thermal analysis **AND** thermal design **AND** mission simulations in thermal-vacuum chamber testing **AND** the PTC device must fail **AND** over-current monitoring and control must all fail for this failure mode to occur.

**Failure Mode 8:** Polarity Reversal Due to Over-Discharge

*Mitigation 10:* The spacecraft battery chemistry (Li-ion) is not susceptible to polarity reversal due to over-discharge.

*Combined faults required for realized failure:* Spacecraft battery module assembled with incorrect cell chemistry **AND** failure of cell protection circuitry

**APPENDIX B - REQUIREMENT 4.5-1 DAS 2.0.1 LOG**

08 24 2015; 08:43:03AM Processing Requirement 4.5-1: Return Status : Passed

=====  
Run Data  
=====**\*\*INPUT\*\***

Space Structure Name = NANOACE\_Satellite  
Space Structure Type = Payload  
Perigee Altitude = 620.000000 (km)  
Apogee Altitude = 620.000000 (km)  
Inclination = 97.800000 (deg)  
RAAN = 0.000000 (deg)  
Argument of Perigee = 0.000000 (deg)  
Mean Anomaly = 0.000000 (deg)  
Final Area-To-Mass Ratio = 0.014000 (m<sup>2</sup>/kg)  
Start Year = 2015.000000 (yr)  
Initial Mass = 6.000000 (kg)  
Final Mass = 5.710000 (kg)  
Duration = 1.000000 (yr)  
Station-Kept = False  
Abandoned = True  
PMD Perigee Altitude = -1.000000 (km)  
PMD Apogee Altitude = -1.000000 (km)  
PMD Inclination = 0.000000 (deg)  
PMD RAAN = 0.000000 (deg)  
PMD Argument of Perigee = 0.000000 (deg)  
PMD Mean Anomaly = 0.000000 (deg)

**\*\*OUTPUT\*\***

Collision Probability = 0.000004  
Returned Error Message: Normal Processing  
Date Range Error Message: Normal Date Range  
Status = Pass

=====

===== End of Requirement 4.5-1 =====



**APPENDIX C - REQUIREMENT 4.6 DAS 2.0.1 LOG**

08 24 2015; 08:43:29AM Processing Requirement 4.6 Return Status : Passed

=====  
Project Data  
=====**\*\*INPUT\*\***Space Structure Name = NANOACE\_Satellite  
Space Structure Type = PayloadPerigee Altitude = 620.000000 (km)  
Apogee Altitude = 620.000000 (km)  
Inclination = 97.800000 (deg)  
RAAN = 0.000000 (deg)  
Argument of Perigee = 0.000000 (deg)  
Mean Anomaly = 0.000000 (deg)  
Area-To-Mass Ratio = 0.014000 (m<sup>2</sup>/kg)  
Start Year = 2015.000000 (yr)  
Initial Mass = 6.000000 (kg)  
Final Mass = 5.710000 (kg)  
Duration = 1.000000 (yr)  
Station Kept = False  
Abandoned = True  
PMD Perigee Altitude = 616.904073 (km)  
PMD Apogee Altitude = 616.904073 (km)  
PMD Inclination = 97.818418 (deg)  
PMD RAAN = 356.403371 (deg)  
PMD Argument of Perigee = 16.252843 (deg)  
PMD Mean Anomaly = 0.000000 (deg)**\*\*OUTPUT\*\***Suggested Perigee Altitude = 616.904073 (km)  
Suggested Apogee Altitude = 616.904073 (km)  
Returned Error Message = Passes LEO reentry orbit criteria.Released Year = 2032 (yr)  
Requirement = 61  
Compliance Status = Pass

=====

===== End of Requirement 4.6 =====

**APPENDIX D - REQUIREMENT 4.7-1 DAS 2.0.1 LOG**

08 24 2015; 08:43:43AM \*\*\*\*\*Processing Requirement 4.7-1  
Return Status : Passed

\*\*\*\*\*INPUT\*\*\*\*

Item Number = 1

name = NANOACE\_satellite  
quantity = 1  
parent = 0  
materialID = 5  
type = Box  
Aero Mass = 5.710000  
Thermal Mass = 5.710000  
Diameter/Width = 0.100000  
Length = 0.300000  
Height = 0.100000

name = RPO\_camera\_nfov  
quantity = 1  
parent = 1  
materialID = 9  
type = Cylinder  
Aero Mass = 0.133000  
Thermal Mass = 0.133000  
Diameter/Width = 0.042000  
Length = 0.093000

name = RPO\_camera\_wfov  
quantity = 1  
parent = 1  
materialID = 9  
type = Cylinder  
Aero Mass = 0.103000  
Thermal Mass = 0.103000  
Diameter/Width = 0.031000  
Length = 0.052000

name = RPO\_camera\_ir  
quantity = 1  
parent = 1  
materialID = 9  
type = Cylinder  
Aero Mass = 0.336000  
Thermal Mass = 0.336000  
Diameter/Width = 0.045000  
Length = 0.093000

name = RPO\_subframe  
quantity = 1  
parent = 1  
materialID = 9  
type = Box  
Aero Mass = 0.085000  
Thermal Mass = 0.085000  
Diameter/Width = 0.100000  
Length = 0.100000  
Height = 0.020000

name = RPO\_lens\_baffle  
quantity = 3

```
parent = 1
materialID = 9
type = Cylinder
Aero Mass = 0.033000
Thermal Mass = 0.033000
Diameter/Width = 0.045000
Length = 0.050000
```

```
name = RPO_docking_mech
quantity = 1
parent = 1
materialID = 9
type = Cylinder
Aero Mass = 0.238000
Thermal Mass = 0.238000
Diameter/Width = 0.050000
Length = 0.050000
```

```
name = RPO_pcb
quantity = 1
parent = 1
materialID = 23
type = Flat Plate
Aero Mass = 0.069000
Thermal Mass = 0.069000
Diameter/Width = 0.100000
Length = 0.100000
```

```
name = RPO_end_panel
quantity = 1
parent = 1
materialID = 23
type = Flat Plate
Aero Mass = 0.307000
Thermal Mass = 0.025000
Diameter/Width = 0.100000
Length = 0.100000
```

```
name = battery
quantity = 6
parent = 9
materialID = 54
type = Cylinder
Aero Mass = 0.047000
Thermal Mass = 0.047000
Diameter/Width = 0.018000
Length = 0.065000
```

```
name = GPS_receiver
quantity = 1
parent = 1
materialID = 23
type = Box
Aero Mass = 0.024000
Thermal Mass = 0.024000
Diameter/Width = 0.100000
Length = 0.100000
Height = 0.016000
```

```
name = GPS_antenna
quantity = 2
parent = 1
materialID = 9
```

```
type = Flat Plate  
Aero Mass = 0.055000  
Thermal Mass = 0.055000  
Diameter/Width = 0.080000  
Length = 0.080000
```

```
name = sysproc_assembly  
quantity = 1  
parent = 1  
materialID = 23  
type = Flat Plate  
Aero Mass = 0.066000  
Thermal Mass = 0.066000  
Diameter/Width = 0.100000  
Length = 0.100000
```

```
name = rwa_mount_assembly  
quantity = 1  
parent = 1  
materialID = 23  
type = Flat Plate  
Aero Mass = 0.290000  
Thermal Mass = 0.050000  
Diameter/Width = 0.100000  
Length = 0.100000
```

```
name = rwa_motor_flywheel  
quantity = 3  
parent = 14  
materialID = 54  
type = Cylinder  
Aero Mass = 0.040000  
Thermal Mass = 0.040000  
Diameter/Width = 0.040000  
Length = 0.013000
```

```
name = rwa_motor  
quantity = 3  
parent = 14  
materialID = 54  
type = Cylinder  
Aero Mass = 0.030000  
Thermal Mass = 0.030000  
Diameter/Width = 0.040000  
Length = 0.013000
```

```
name = rwa_brackets  
quantity = 3  
parent = 14  
materialID = 9  
type = Box  
Aero Mass = 0.010000  
Thermal Mass = 0.010000  
Diameter/Width = 0.040000  
Length = 0.040000  
Height = 0.013000
```

```
name = irm_assembly  
quantity = 1  
parent = 1  
materialID = 23  
type = Box  
Aero Mass = 0.225000
```

Thermal Mass = 0.025000  
Diameter/Width = 0.100000  
Length = 0.100000  
Height = 0.050000

name = imu  
quantity = 1  
parent = 18  
materialID = 9  
type = Box  
Aero Mass = 0.018000  
Thermal Mass = 0.018000  
Diameter/Width = 0.024530  
Length = 0.038000  
Height = 0.011100

name = star camera  
quantity = 2  
parent = 18  
materialID = 9  
type = Cylinder  
Aero Mass = 0.091000  
Thermal Mass = 0.091000  
Diameter/Width = 0.030000  
Length = 0.047000

name = sband\_assembly  
quantity = 1  
parent = 1  
materialID = 23  
type = Box  
Aero Mass = 0.040000  
Thermal Mass = 0.040000  
Diameter/Width = 0.100000  
Length = 0.100000  
Height = 0.050000

name = sband\_transmitter  
quantity = 1  
parent = 1  
materialID = 9  
type = Box  
Aero Mass = 0.044000  
Thermal Mass = 0.044000  
Diameter/Width = 0.032000  
Length = 0.086000  
Height = 0.010000

name = sband\_antenna  
quantity = 2  
parent = 1  
materialID = 9  
type = Flat Plate  
Aero Mass = 0.144000  
Thermal Mass = 0.144000  
Diameter/Width = 0.100000  
Length = 0.100000

name = uhf\_assembly  
quantity = 1  
parent = 1  
materialID = 23  
type = Box

Aero Mass = 0.040000  
Thermal Mass = 0.040000  
Diameter/Width = 0.100000  
Length = 0.100000  
Height = 0.050000

name = uhf\_radio  
quantity = 1  
parent = 1  
materialID = 9  
type = Box  
Aero Mass = 0.030000  
Thermal Mass = 0.030000  
Diameter/Width = 0.036000  
Length = 0.083000  
Height = 0.004000

name = uhf\_antenna  
quantity = 1  
parent = 1  
materialID = 9  
type = Box  
Aero Mass = 0.052000  
Thermal Mass = 0.052000  
Diameter/Width = 0.098000  
Length = 0.098000  
Height = 0.007000

name = isl\_assembly  
quantity = 1  
parent = 1  
materialID = 9  
type = Box  
Aero Mass = 0.026000  
Thermal Mass = 0.026000  
Diameter/Width = 0.020000  
Length = 0.029000  
Height = 0.020000

name = battery\_assembly  
quantity = 1  
parent = 1  
materialID = 9  
type = Box  
Aero Mass = 0.218000  
Thermal Mass = 0.218000  
Diameter/Width = 0.100000  
Length = 0.100000  
Height = 0.050000

name = deploy\_panel\_assembly  
quantity = 4  
parent = 1  
materialID = 23  
type = Flat Plate  
Aero Mass = 0.119000  
Thermal Mass = 0.119000  
Diameter/Width = 0.100000  
Length = 0.300000

name = deploy\_panel\_edge\_stiffener  
quantity = 8  
parent = 1

```
materialID = 9
type = Box
Aero Mass = 0.008000
Thermal Mass = 0.008000
Diameter/Width = 0.005000
Length = 0.230000
Height = 0.003000

name = solar_cells
quantity = 48
parent = 1
materialID = 24
type = Flat Plate
Aero Mass = 0.010000
Thermal Mass = 0.010000
Diameter/Width = 0.050000
Length = 0.100000

name = body_panel_assembly
quantity = 4
parent = 1
materialID = 23
type = Flat Plate
Aero Mass = 0.119000
Thermal Mass = 0.119000
Diameter/Width = 0.100000
Length = 0.300000

name = propulsion_module
quantity = 1
parent = 1
materialID = 9
type = Box
Aero Mass = 0.882000
Thermal Mass = 0.882000
Diameter/Width = 0.100000
Length = 0.100000
Height = 0.100000

name = structure_assembly
quantity = 1
parent = 1
materialID = 9
type = Box
Aero Mass = 0.302000
Thermal Mass = 0.302000
Diameter/Width = 0.010000
Length = 1.200000
Height = 0.010000

*****OUTPUT****
Item Number = 1

name = NANOACE_satellite
Demise Altitude = 77.998105
Debris Casualty Area = 0.000000
Impact Kinetic Energy = 0.000000

*****
name = RPO_camera_nfov
Demise Altitude = 75.426027
Debris Casualty Area = 0.000000
Impact Kinetic Energy = 0.000000
```

```
*****  
name = RPO_camera_wfov  
Demise Altitude = 74.109379  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = RPO_camera_ir  
Demise Altitude = 72.256386  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = RPO_subframe  
Demise Altitude = 76.897129  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = RPO_lens_baffle  
Demise Altitude = 77.013293  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = RPO_docking_mech  
Demise Altitude = 72.148019  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = RPO_pcb  
Demise Altitude = 77.171379  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = RPO_end_panel  
Demise Altitude = 77.722301  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = battery  
Demise Altitude = 73.088925  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = GPS_receiver  
Demise Altitude = 77.761652  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = GPS_antenna  
Demise Altitude = 76.726574  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = sysproc_assembly
```



Demise Altitude = 77.204129  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000

\*\*\*\*\*

name = rwa\_mount\_assembly  
Demise Altitude = 77.444074  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000

\*\*\*\*\*

name = rwa\_motor\_flywheel  
Demise Altitude = 73.254972  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000

\*\*\*\*\*

name = rwa\_motor  
Demise Altitude = 74.182418  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000

\*\*\*\*\*

name = rwa\_brackets  
Demise Altitude = 76.939160  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000

\*\*\*\*\*

name = irm\_assembly  
Demise Altitude = 77.831918  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000

\*\*\*\*\*

name = imu  
Demise Altitude = 76.585871  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000

\*\*\*\*\*

name = star\_camera  
Demise Altitude = 73.940902  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000

\*\*\*\*\*

name = sband\_assembly  
Demise Altitude = 77.710840  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000

\*\*\*\*\*

name = sband\_transmitter  
Demise Altitude = 76.666082  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000

\*\*\*\*\*

name = sband\_antenna  
Demise Altitude = 75.658113  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000

```
*****  
name = uhf_assembly  
Demise Altitude = 77.710840  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = uhf_radio  
Demise Altitude = 76.963597  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = uhf_antenna  
Demise Altitude = 77.193285  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = isl_assembly  
Demise Altitude = 76.126590  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = battery_assembly  
Demise Altitude = 75.885933  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = deploy_panel_assembly  
Demise Altitude = 77.452254  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = deploy_panel_edge_stiffener  
Demise Altitude = 77.651246  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = solar_cells  
Demise Altitude = 77.922199  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = body_panel_assembly  
Demise Altitude = 77.452254  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = propulsion_module  
Demise Altitude = 72.291910  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000
```

```
*****  
name = structure_assembly
```

Demise Altitude = 76.864886  
Debris Casualty Area = 0.000000  
Impact Kinetic Energy = 0.000000

\*\*\*\*\*

===== End of Requirement 4.7-1 =====