Thales InFlyt Experience Experimentation Description for a Ku-band Airborne Earth Station Modular Connectivity Terminal (MCT) - Mobile Testing

Thales InFlyt Experience, with operations in Melbourne, FL and Irvine, CA is a global leader in providing leading-edge, connected inflight entertainment systems and services, including high-speed Internet connectivity. Thales is currently developing and testing an end-to-end, Ku-band satellite based connectivity solution including an airborne Modular Connectivity Terminal (or ESAA), that will serve multiple airline customers in the North American, South American, African, European, Caribbean, and Middle East regions. When operational, this solution will enable airline carriers to reach their full potential by offering global inflight coverage that supports the increasing demands of passengers' inflight connectivity needs and provides airlines access to critical real-time inflight data.

Experimental License Modification Request

Thales InFlyt Experience seeks a modification to its FCC experimental license for a Ku-band fixed earth station - (Call Sign WI2XIT; File Number 0306-EX-PL-2016; granted August 1, 2016) - to operate the MCT in mobile, land-based tests using SES Ku-band capacity on the following satellites:

- SES-1 at 101º W (for North America coverage)
- SES-4 at 22º W (for North America, South America, Africa, Europe, and Middle East coverage)
- SES-6 at 40.5° W (for South America and Caribbean coverage)
- AMC-9 at 83º W (for North American coverage)

Thales' static MCT testing as authorized by its experimental license referenced above, and described in Thales' Experimentation Description dated April 29, 2016, will not change.

Thales is requesting the license modification to conduct mobile MCT testing, on land only, within a 60-mile radius of Kissimmee, FL as shown in Figure 1 below.



Figure 1: Intended Areas (Land-Based Only) for Mobile Testing of Ku Modular Connectivity Terminal

Thales' mobile testing of the MCT within this area of central Florida will preclude any interference into NSF and NASA sites at the following locations in CONUS:

NSF	NASA
Green Bank, WV	White Sands, NM
Socorro, NM	Blossom Point, MD
Brewster, WA	
Owens Valley, CA	
Kitt Peak, AZ	
Pie Town, NM	
Los Alamos, NM	
Fort Davis, TX	
North Liberty, IA	
Hancock, NH	
St. Croix, USVI	
Mauna Kea, HI	

The MCT will use an antenna pointing and tracking algorithm (described later in this narrative) to precisely point to the intended satellite before establishing two-way communication links.

The Ku-band antenna will operate in the frequency ranges of 10.70-12.75 GHz (receive) and 13.75-14.50 GHz (transmit), with a maximum transmit EIRP of 46.0 dBW. The MCT transmit RF waveform will use various digital modulation and coding (modcod) formats as per the DVB-S2

standard, and the transmitted power spectral density will be compliant as per FCC 47 CFR 25.227. Note that since Thales' mobile testing operations will use a vehicle, the power spectral density rules in FCC 47 CFR 25.226 for Ku-band VMES may also apply, which are equal to those in 25.227.

The mobile testing will be conducted using a truck with the MCT mounted on a custom rig on the truck's flatbed. Terminal system test equipment, hardware, and software will also be carried in the truck, and the driver/operator will be in frequent contact via cellular phone with Thales and SES engineering and operations personnel. The driver/operator will also have the ability to quickly mute the terminal's transmit signal if necessary.

In the case of any inadvertent, reported interference, Thales will cease terminal transmissions as soon as possible upon notification to Thales' 24/7 point of contact (POC):

Martin Matura mobile: 321-292-0878 email: martin.matura@us.thalesgroup.com

The SES controlling Ku-band earth station to be used during mobile experimental testing is: FCC callsign E140059 – Mount Airy (Woodbine), MD 21771

The SES Network Operations Center (NOC) in Manassas, VA 24/7 phone number is: 703-330-3305 (option #1), or 1-866-244-5012 (option #1).

Mobile Testing Objectives

Parameters to be tested and verified in the mobile tests include:

- satellite link closure thresholds
- end-to-end system latency
- achievable information rates using various modulation/coding schemes
- antenna system gain and noise temperature performance versus design specification

- calibration and enhancement of the antenna pointing system's algorithm (tracking, pointing, and stabilization)

- end-to-end connectivity to SES's supporting terrestrial network, including connectivity to/from an Internet Service Provider (ISP)

Antenna Pointing and Tracking Methodology

The MCT's antenna positioning and control subsystems provide mechanical beam steering in azimuth and elevation using a software-based algorithm. The entire algorithm has 3 parts – tracking, pointing, and stabilization.

Tracking essentially lobes the beam around the satellite in an elliptical pattern. With perfect alignment the received signal strength is equal at all points on the ellipse and the centroid of power is at the major/minor axis intersection. Any misalignment causes the ellipse to have

unequal power at different points, and the centroid of power occurs somewhere inside of the ellipse. Where the centroid falls determines how far off-peak the antenna is, and in what direction. Offset is then added to get back to the center of the beam. More spins around the ellipse provide a better time average and eventually drives the offset to zero. This process is a trade-off of scan duration, how often scans are done, and how much offset is gotten on each pass.

When the antenna is peaked, the satellite's location in AZ/EL space is known, and its location in inertial space is calculated. That location is compared to data from the aircraft's inertial navigation system (INS) to obtain another offset.

Pointing is based on the aircraft's INS, obtained via the ARINC 429 data bus. (Note during mobile testing, a portable INS "black box" will be used to provide ARINC 429 data). Stabilization is done by nulling gyro rate output. If there is no motion, gyro output rate is 0. If there is motion, gyro output rate is non-zero, and the Az/El gimbals counter-rotate very quickly (on the order of kHz) to null the gyro output. While the scale factor of a gyro does drift over long periods of time, because the system is nulling the gyros to zero, this is a non-issue.

In general, the pointing and stabilization methodologies keep the antenna peaked on the intended satellite very accurately. Pointing accuracy is further improved by adding the offsets calculated during the tracking process. The methodologies provide sufficient observability into pointing error, and the control logic state machine and hardware implementation will mute the transmit signal within 100 milliseconds if pointing error exceeds 0.2°.

Proposed Transmission Plan and Worst-Case EIRP Spectral Density

The range of possible inbound carrier (terminal-to-satellite-to-gateway earth station) modulation and coding formats (modcods) is shown in Table 1 below. Thales expects that inbound carriers using the modcods shaded in blue, using Ku-band space segment resources on SES-1 at 101° WL, will be tested most often during the experimental operation of the MCT.

Modulation	FEC Rate	Spread Factor
SS-BPSK	1/2	2
BPSK	1/2	1
BPSK	2/3	1
QPSK	1/2	1
QPSK	2/3	1
8-PSK	2/3	1

Table 1: Range of Possible MODCODs for Inbound Carriers

Link Budget and EIRP SD Patterns

A representative clear-sky link budget for an inbound carrier over SES-1 is provided below. This 2.9 Msps, QPSK ½ carrier will produce the expected worst-case EIRP spectral density of 26.0 dBW/40 kHz, assuming a skew angle of approximately 35° from Melbourne, FL to SES-1 at 101° WL. Associated EIRP SD patterns follow the link budget.

The transmission parameters are:

Satellite: SES-1 @ 101° WL Uplink: Melbourne, FL (28.1°N/80.6°W) Modcod: QPSK, rate ½ FEC Symbol Rate: 2.9 Msps Information Rate: 2.9 Mbps Occupied BW: 3.6 MHz Antenna transmit gain (at 14.125 GHz): 33.6 dBi SSPB maximum output power (before losses): 28 watts SSPB-to-antenna flange insertion losses: 3.5 dB Transmit EIRP at antenna: 44.6 dBW (maximum 46.0 dBW) EIRP SD at antenna flange: -7.6 dBW/40 kHz Transmit EIRP SD: 26.0 dBW/40 kHz

Service Name	Experimental Inbound - MLB->Woodbine		
Coverage	2.9 Msps; QPSK 1/2		
Uplink earth station	a/c term		
Downlink earth station	Wash DC (Woodbine, MD)		
Sateilite name	SES-1 @ 101.0		
Modcod	DVBS2,normal frame,4-PSK (1/2),no pilots		
Link Input Parameters	<i>Up</i>	Down	Units
Site latitude	28.1N	38.9N	degrees
Site longitude	80.6W	77.0W	degrees
Site altitude	0.000	0.000	km
Frequency	14.125	11.825	GHz
Polarization	Circular	Circular	%
Rain model	Clear sky	Clear sky	
Rain zone or mm/h	0	0	
Availability (average year)	N/A	N/A	
Antenna aperture Antenna efficiency or gain (+ or - prefix) Coupling loss Antenna mispoint loss	0.4 +33.6 3.5 .2	10 65 0	metres % or dBi dB dB
Other path losses (site diversity gain -ve) LNB noise figure or temp (+ prefix) Antenna noise C/ACI C/ASI C/CCI HPA C/IM C/ACI C/ACI C/ACI	0 +100 135.00 26 42.60 26 15 27 44.96 27	0 dB or K K dB dB dB dB dB dB dB dB dB dB	dB
Upink station HPA output back-off Uplink power control available Number of carriers / HPA Required HPA power	0 0 1 28	dB W	

Satellite Input Parameters Satellite longitude Transponder type	Value 101.00W TWTA	Units degrees
G/T Reference SFD Reference Receive G/T Attenuator pad (gain step) Effective SFD Satellite ALC EIRP (saturation) Transponder bandwidth Input back off total Output back off total C/IM Carriers per transponder	5.5 -90.5 5.5 0 -90.50 0 49.5 36 6 3 18.00 AUTO	dB/K dBW/m2 dB/K dB dBW/m2 dB dBW MHz dB dB dB dB dB
Carrier/Link Input Parameters Modulation Required Eb/No Symbol rate	Value 4-PSK 2.5 2.9	Units dB Mbaud

Symbol rate	2.9	Mbau
Information rate overhead	0	%
FEC code rate	0.4944	
Spreading gain	0	dB
(1 + Roll off factor)	1.25	
Carrier spacing factor	1.25	
Bandwidth allocation step size	.5	MHz
Implementation loss	0	dB
System margin	1.5	dB

Calculations at Saturation		Value	Units
Gain 1m ^A 2 Uplink C/No Downlink C/No Total C/No Uplink EIRP for saturation		44.46 99.14 108.75 98.69 72.22	dB/m2 dB.Hz dB.Hz dB.Hz dBW
General Calculations	Up	Down	Units
Elevation True azimuth Compass bearing Path distance to satellite XPD during rain Propagation time delay Antenna efficiency Antenna gain Availability (average year) Link downtime (average year) Link downtime (worst month) Link downtime (worst month)	50,22 218,29 224,98 37062,74 0.00 0,123628 65,35 33,60 N/A N/A N/A N/A N/A	38.53 215.34 226.18 37893.93 0.00 0.126400 65.00 59.99 N/A N/A N/A N/A	degrees degrees km dB seconds % dBi % hours % hours

Uplink Calculation	Clear	Rain Up	Rain Dn	Units
Transmit EIRP	44.57	44.57	44.57	dBW
Uplink power control used	0.00	0.00	0.00	dB
Transponder input back-off (total)	6.00	6.00	6.00	dB
Input back-off per carrier	27.65	27.65	27.65	dB
Antenna mispoint	0.20	0.20	0.20	dB
Free space loss	206.83	206.83	206.83	dB
Atmospheric absorption	0.15	0.15	0.15	dB
Tropospheric scintillation	0.00	0.00	0.00	dB
Cloud attenuation	0.00	0.00	0.00	dB
Rain attenuation	0.00	0.00	0.00	dB
Total attenuation (gas-rain-cloud-scintillation)	0.15	0.15	0.15	dB
Other path losses	0.00	0.00	0.00	dB
C/No (thermal)	71.49	71.49	71.49	dB.Hz
C/N (thermal)	6.87	6.87	6.87	dB
C/ACI	26.00	26.00	26.00	dB
C/ASI	14.95	14.95	14.95	dB
C/CCI	26.00	26.00	26.00	dB
C/IM	15.00	15.00	15.00	dB
C/(N+I) [= Es/(No+Io)]	5.62	5.62	5.62	dB
Eb/(No+lo)	5.67	5.67	5.67	dB

Downlink Calculation Satellite EIRP total Transponder output back-off (total) Output back-off per carrier Satellite EIRP per carrier Antenna mispoint Free space loss Atmospheric absorption Tropospheric scintillation Cloud attenuation Rain attenuation Total attenuation (gas-rain-cloud-scintillation) Other path losses Noise increase due to precipitation Downlink degradation (DND) Total system noise Figure of mert (G/T) C/No (thermal) C/Acl C/Asl C/(N+1) [= Es/(No+lo)] Eb/(No+lo)	Clear 49.50 3.00 24.65 24.85 0.00 205.48 0.11 0.00 0.00 0.00 0.00 0.00 0.00 0.0	Rain 49.50 3.00 24.65 24.85 0.00 205.48 0.11 0.00 0.00 0.00 0.00 0.00 0.00 237.70 36.23 84.10 19.48 27.00 19.48 27.00 13.93 13.98	Up	Rain Dn 49.50 3.00 24.65 24.85 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 237.69 36.23 84.10 19.48 27.00 13.93 13.98	Units dBW dB dBW dB dB dB dB dB dB dB dB dB dB
Totals per Carrier (End-to-End) C/No (thermal) C/N (thermal) C/ACI C/ASI C/CCI C/II (total) C/(No+Io) C(No+Io) D(No(No+Io)) Implementation loss System margin Net Eb/(No+Io) Required Eb/(No+Io) Excess margin	Clean 71.26 6.64 23.46 13.24 13.24 13.24 10.10 69.65 5.02 5.07 0.00 1.50 3.57 2.50 1.07	Rain 71.26 6.64 23.46 13.84 23.46 13.24 10.10 69.65 5.07 0.00 1.50 2.50 1.07	Up	Rain Dn 71.26 6.64 23.46 13.24 13.24 10.10 69.65 5.02 5.07 5.07 0.00 1.50 3.57 2.50 1.07	Units dB.Hz dB dB dB dB dB dB dB dB dB dB
EIRP Density Calculations Flange transmit (up) Antenna off axis transmit toward 103W Satellite (down) Flange receive (down)	<i>Clear</i> -53.65 -22.57 -39.77 -185.36	Rain U -53.65 dBW/Hz -39.77 -185.36	Ip	Rain Dn -53.65 -39.77 -185.36	dBW/Hz dBW/Hz dBW/Hz
Earth Station Power Requirements EIRP per carrier Available uplink power control Total EIRP required Antenna gain Antenna feed flange power per carrier HPA output back off Waveguide loss Number of HPA carriers Total HPA power required Required HPA power				Value 44.57 0.00 44.57 33.60 10.97 0.00 3.5 1 14.4716 28.0000	Units dBW dB dBW dBi dBW dB dB dBW W
Space Segment Utilization Overall availability Information rate Information rate (inc overhead) Transmit rate Symbol rate Noise Bandwidth Occupied bandwidth Minimum allocated bandwidth required Allocated transponder bandwidth used Used transponder power Percentage transponder power used Max carriers / transponder Limited by: Power equivalent bandwidth usage			Valu N/A 2.8675 2.8675 5.8000 64.62 3.6250 3.6250 4.0000 0.717 11.11 24.85 0.68 9.00 Bandy 0.2462	<i>ie</i>	Units % Mbps Mbps Mbaud dB.Hz MHz MHz MHz MHz bps/Hz % dBW %



EIRP SD for 35° Skew Angle (to SES-1 @ 101°W) Az +/-10°

EIRP SD for 35° Skew Angle (to SES-1 @ 101°W) Az +/-90°

